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# 6H-SiC Photoconductive Switches Triggered at Below Bandgap Wavelengths

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## ABSTRACT

Semi-insulating silicon carbide (SiC) is an attractive material for application as high voltage, photoconductive semiconductor switches (PCSS) due to its large bandgap, high critical electric field strength, high electron saturation velocity and high thermal conductivity. The critical field strength of 300 MV/m for 6H-SiC makes it particularly attractive for compact, high voltage, fast switching applications. To realize the benefits of the high bulk electric field strength of SiC and diffuse switch current, carriers must be excited throughout the bulk of the photo switch. Photoconducting switches with opposing electrodes were fabricated on “a” plane, vanadium compensated, semi-insulating, 6H-SiC substrates. The PCSS devices were switched by optically exciting deep extrinsic levels lying within the 6H-SiC bandgap. The SiC photoswitches were tested up to a bias voltage of 11000 V with a corresponding peak current of 150 A. The 6H-SiC substrates withstood average electric fields up to 27 MV/m. Minimum PCSS dynamic resistances of 2 and 10  $\Omega$  were obtained with 13 mJ optical pulses at 532 and 1064 nm wavelengths, respectively.

Index Terms - Photoconducting devices, photoconductivity, light triggered switches, semiconductor switches, silicon carbide.

## 1 INTRODUCTION

**THE** 6H-SiC polytype has a wide band-gap (3 eV), high critical field strength (300-400 MV/m), high-saturated electron velocity ( $2.0 \times 10^7$  cm/s) and high thermal conductivity (4.9 W/cm °C). These material properties make semi-insulating 6H-SiC an attractive semiconductor material for the Photoconductive Semiconductor Switch (PCSS) application. Previous SiC PCSS work [1-3] used high resistivity, low impurity SiC polytypes and focused on lateral geometry surface switches that used above band-gap wavelengths of light to trigger the switches. The performance and switch life of lateral geometry PCSS are limited by surface flashover, surface carrier mobility and high current density. PCSS with opposing electrical contacts deposited on vanadium compensated, semi-insulating, 6H-SiC substrates can be triggered using below band-gap light to excite carriers from extrinsic levels throughout the bulk of the material. This results in diffuse photocurrent and switch hold off voltages determined by the bulk breakdown field strength of 6H-SiC. The bulk switching capability and semi-insulating nature of 6H-SiC are enabled by the addition of the dopant vanadium. Vanadium is an amphoteric impurity that can act as a deep acceptor, or a deep donor. The local Fermi level in the 6H-SiC is determined by the relative densities of the impurities, nitrogen, boron and vanadium present in the material.

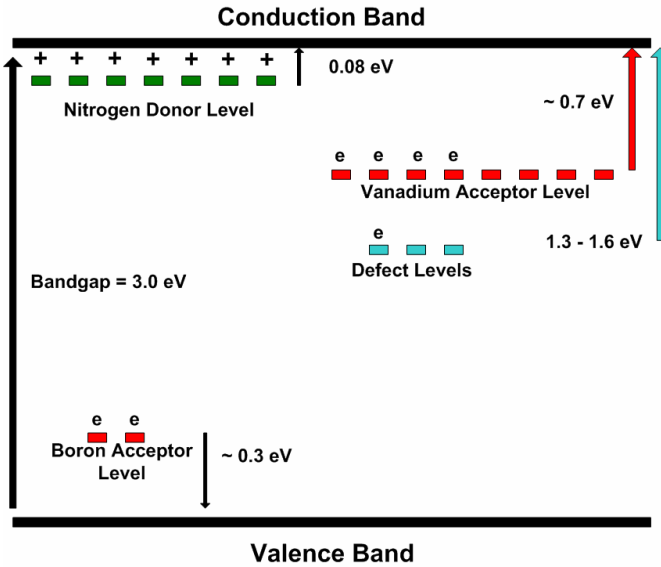
Vanadium acts as a deep acceptor when the nitrogen donor impurity density sufficiently exceeds the boron acceptor impurity density, which is the case for the 6H-SiC material we have tested.

Another feature of this material is that the Fermi level will be pinned close to the vanadium acceptor level. The deep (0.7 eV below conduction band) vanadium acceptor levels accept electrons donated from the shallow (0.08 eV below conduction band) nitrogen donor levels resulting in semi-insulating 6H-SiC material. The electrons residing in the extrinsic vanadium acceptor levels can be excited into the conduction band by photons with energies exceeding 0.7 eV. Figure 1 [4] depicts the extrinsic levels in the 6H-SiC bandgap. The Boron acceptor levels and defect levels are also shown in Figure 1. The defect levels include silicon vacancies and the UD-1 defect [4].

## 2 PCSS TEST APPARATUS AND PROCEDURE

Five PCSS devices were fabricated from samples of 400  $\mu\text{m}$  thick, 1.2 cm per side, square substrates of “a” plane, vanadium compensated, semi-insulating 6H-SiC. The four facets of the substrate were cleaved/polished to enhance optical coupling into the bulk of the substrate. The contacts consist of a 0.8 cm diameter, circular metalization centered on opposing sides of the substrate. The metalization formed an ohmic contact and consisted of layers of nickel, titanium,

platinum and gold. The metal deposition and anneal were performed at SemiSouth Laboratories Inc. in Starksville, MS. Indium coated copper electrodes were brazed to the substrate metalizations to facilitate electrical connection. The finished 6H-SiC PCSS assembly is shown in Figure 2. The 6H-SiC PCSS assembly was prepared for photoconductivity measurements by cleaning the PCSS facets to remove any



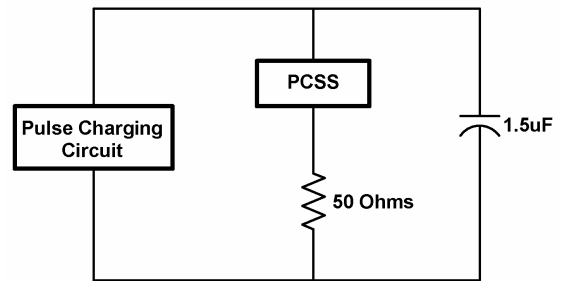
**Figure 1.** Vanadium acceptor and nitrogen donor levels in vanadium compensated 6H-SiC.

organic residue. All four PCSS facets were inspected by microscope and given identification marks prior to photoconductivity tests. Photoconductivity tests were performed using 1064 nm and frequency doubled 532 nm wavelength light from a Q-switched Nd:YAG laser with an 8 ns at full wave half maximum (FWHM) output pulse. The optical pulse was focused and aligned to obtain as uniform as possible light pulse over a rectangular area measuring 1 cm wide by 400  $\mu\text{m}$  high. The optical pulse was then centered on the PCSS facet. Photoconductivity tests were performed using optical pulse energies ranging from 1 to 14 mJ. The optical energy was increased in 1-mJ increments using a waveplate-polarizer pair. PCSS facets were inspected for damage by microscope between optical pulse energy increments.



**Figure 2.** Vanadium compensated, semi-insulating, 6H-SiC PCSS assembly.

The photoconductivity of the PCSS was measured using the circuit shown in Figure 3. The test circuit was constructed on 0.125 inch thick, 56 g (2 oz) Cu printed circuit board. The load resistor and storage capacitor were positioned on opposite sides of the 2.5 inch long, 1.9 inch wide circuit board and were constructed from a series and parallel combination of components to minimize circuit inductance. The total circuit inductance was estimated to be 12 nH. The 1.5  $\mu\text{F}$  capacitor of the test circuit was pulse charged to bias voltages ranging from 250 V to 4.25 kV in 30  $\mu\text{s}$ . The PCSS was optically triggered after a 30  $\mu\text{s}$  flat top interval of the pulse bias voltage. The voltage across the PCSS was measured differentially using a pair of calibrated, fast (250 MHz bandwidth), high voltage (5 kV) probes. The tips of the voltage probes were inserted in pin sockets soldered onto the switch electrode connections. The load voltage was measured using a fast (35 ps rise time), low impedance (250  $\Omega$ ) high voltage probe. The PCSS current was obtained by dividing the load voltage by the load resistance. Dynamic switch resistance is another important switching parameter. Dynamic switch resistance is a measure of how well the applied optical pulse has reduced the bulk resistivity of the 6H-SiC substrate. The dynamic switch resistance is calculated by dividing the switch voltage by the load current.



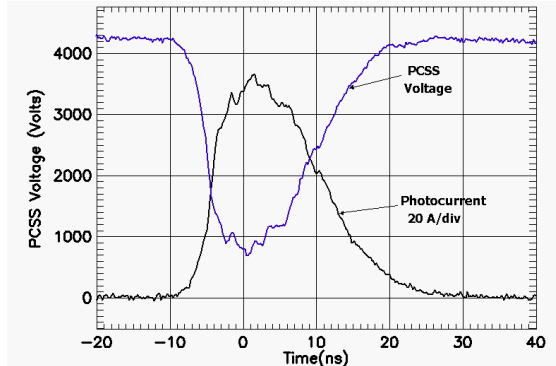
**Figure 3.** Simple schematic for PCSS photoconductivity test circuit.

### 3 EXPERIMENTAL RESULTS

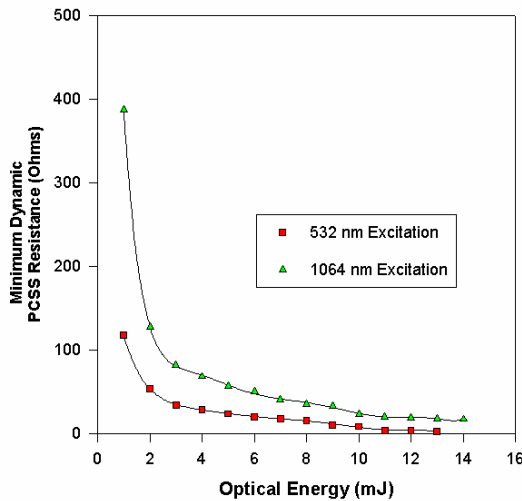
#### 3.1 Minimum Dynamic Resistance

The PCSS voltage and current for a 4.25 kV charge voltage and optical pulse energy of 13 mJ at 1064 nm are shown in Figure 4. The PCSS voltage starts at 4.25 kV and collapses to approximately 750 Volts in 10 ns, while the PCSS current increases from zero to 70 A. The PCSS current pulse is similar in temporal profile to the 1064 nm optical trigger pulse. However, the photocurrent has a 16 ns FWHM pulse-width indicating a carrier recombination time of a few nanoseconds, or, less. The minimum dynamic PCSS resistance for the pulse shown in Figure 4 is 11  $\Omega$ . The minimum dynamic PCSS resistance is approximately constant for fixed optical pulse energy, regardless of the charge voltage. Switch minimum dynamic PCSS resistance as a function of optical pulse energy for 1064 and 532 nm wavelengths is shown in Figure 5. The switch minimum dynamic PCSS resistance decreases rapidly with optical pulse energy for both optical wavelengths. The PCSS attains a

lower minimum dynamic resistance at all optical energies for excitation with 532 nm light compared to excitation with 1064 nm light. This is a result of charge carriers being excited from additional extrinsic levels by the 532 nm wavelength.



**Figure 4.** PCSS voltage and current for bias voltage of 4.25 kV and 13 mJ optical trigger at 1064 nm.



**Figure 5.** Minimum dynamic PCSS resistance as function of optical trigger energy for 532 and 1064 nm.

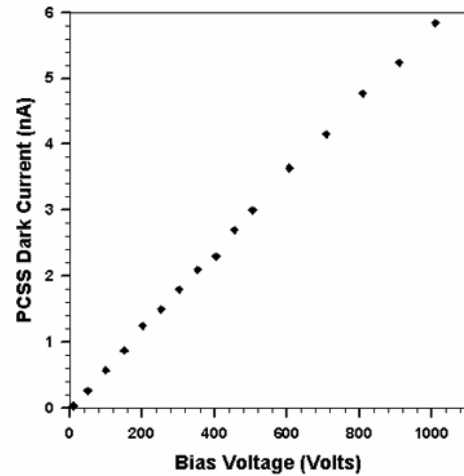
### 3.2 PCSS DARK CURRENT

The dark current through four of the PCSS devices was measured by a picoammeter while applying a dc voltage bias across the PCSS; picoammeter series combination. The voltage across the PCSS was monitored with a precision (1%) 1000 M $\Omega$ , resistive divider. The dark current varied linearly with the dc bias voltage for all four of the PCSS devices. The dark resistivity of the PCSS devices ranged from  $10^{12}$  to  $10^{13}$   $\Omega$ -cm. Results for a typical dark current measurement is shown in Figure 6. The dark current for this PCSS ranged from a small fraction of a nanoampere up to 5.8 nA at the highest dc bias of 1000 V, as shown in Figure 6. The PCSS dark resistance and resistivity were calculated to be 170 G $\Omega$  and  $3.2 \times 10^{12}$   $\Omega$ -cm for this PCSS. The ratio of the dark resistance to the minimum dynamic PCSS resistance of Figure 5 (2  $\Omega$ ) is  $8.5 \times 10^{10}$ . The resistivity has been reduced by almost eleven orders of magnitude by exciting extrinsic levels in the bulk of the Vanadium compensated 6H-SiC. The dark

current results are similar to previous measurements for semi-insulating 6H-SiC [5].

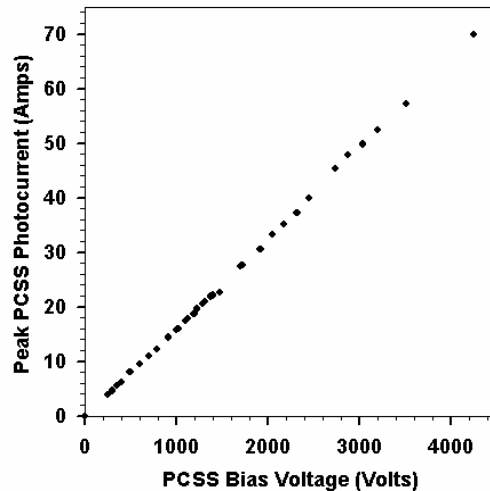
### 3.3 PCSS PHOTOCURRENTS

The peak photocurrent in the PCSS has been measured as a function of bias voltage and optical pulse energy for both 532 and 1064 nm wavelengths. The peak photocurrent varies linearly with the bias voltage for fixed optical pulse energy as shown in Figure 7. The slope of the linear variation of peak



**Figure 6.** Variation of PCSS dark current with bias voltage.

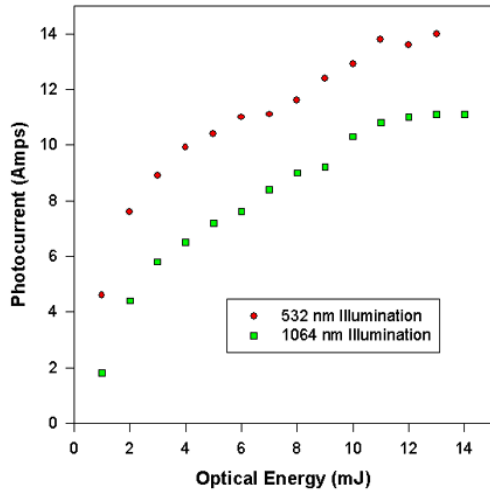
photocurrent with bias voltage decreases with when the fixed optical pulse energy is reduced. This is what should be expected since we are optically modulating the PCSS resistance.



**Figure 7.** Peak PCSS photocurrent versus bias voltage for 13 mJ optical excitation at 1064 nm.

The saturation of the peak PCSS photocurrent with increasing optical pulse energy for fixed bias voltage of 750 Volts is shown in Figure 8. The peak PCSS photocurrent for illumination with 532 nm was consistently 3- 4 A higher than the peak photocurrent obtained with 1064 nm illumination for this PCSS. This is a result of the 532 nm wavelength (2.33 eV) exciting additional deep extrinsic levels compared to the

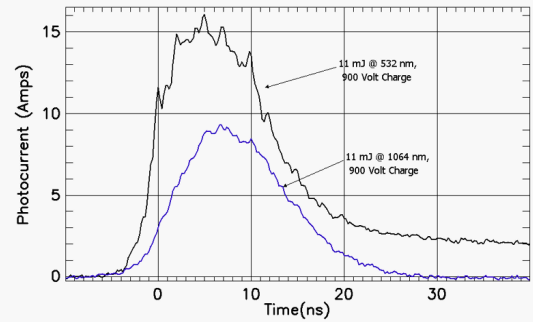
1064 nm wavelength (1.17 eV). A consistent difference in peak PCSS photocurrent with excitation wavelength was observed in all the PCSS devices tested. However, the magnitude of the difference in peak PCSS photocurrent for different excitation wavelengths varied from 2 A up to 6 Amps. An explanation for the variation of the difference in peak photocurrents for 532 and 1064 nm excitation for different PCSS devices is that the impurity densities in the PCSS substrates vary. The substrates are cut from the a-plane of the 6H-SiC crystal. The sections that were originally cut from the 6H-SiC crystal measured 3.6 cm in the crystal growth (c) direction. The sections were then cut into 1.2 cm long substrates. We would expect variation in substrate impurity density along the growth direction because the impurity densities usually decrease during crystal growth. We expect somewhat different performance from substrate to substrate since we are exciting carriers from extrinsic (impurity) levels.



**Figure 8.** Peak PCSS photocurrent versus optical excitation energy for 750 Volt bias.

The nature of some of the different extrinsic levels being excited at the 1064 and 532 nm optical wavelengths is illustrated in Figure 9. The PCSS photocurrents for 11 mJ optical excitation at 532 and 1064 nm wavelengths show a significant difference in amplitude and pulse shape. The most notable difference is the long tail on the photocurrent excited at 532 nm. The current tail persists and for one PCSS took approximately one millisecond to decay to zero. We believe crystal defects, that act as electron traps [4, 6] located 1.3-1.6 eV below the conduction band, are contributing the carriers in the photocurrent tail. Electrons are captured by the traps and thermally excited back into the conduction band resulting in a long decay time. The electron trap level has a recovery time of from a few to up to 200  $\mu$ s. It also appears that the electron traps are filled prior to optical excitation based on the much faster rate of rise of photocurrent excited at 532 nm. However, the electron trap level contributes only 2 of 15 A peak photocurrent at 532 nm excitation in Figure 9. We should expect that the electrons excited from vanadium acceptor level, that we believe constitutes the entire photocurrent at

1064 nm, will also be excited at 532 nm. In addition, there appears to be at least a third component of photocurrent with a rapid rise and decay time that is present in the photocurrent at 532 nm. We believe that the additional carriers are holes being excited into the valence band from vanadium acceptor levels that have not been ionized. A significant fraction of vanadium acceptor levels are not ionized because the Fermi level is pinned close to the vanadium acceptor level. In addition, Vanadium acceptor



**Figure 9.** PCSS photocurrent temporal pulse for 11 mJ optical excitation at 532 and 1064 nm wavelengths.

levels are returned to the neutral state after electrons that they had captured are excited into the conduction band. Electrons can be excited from the valence band into the neutral vanadium acceptor levels that lie 2.3 eV above the valence band by 532 nm (2.33 eV) wavelength light. Electrons that are excited into the neutral vanadium acceptor levels leave holes in the valence band that contribute to the conduction current of the PCSS.

We can estimate the triggering efficiency of the PCSS device from switching measurements at 13 mJ, 1064 nm optical excitation. We believe that the charge carriers are electrons excited from the vanadium acceptor level by the 1064 nm wavelength. The switch carrier density is given by:

$$n(t) = \frac{I_{sw}(t)}{q\mu a_{sw} V_{sw}(t)} \quad (1)$$

where  $V_{sw}$ ,  $I_{sw}$ ,  $l$ , and  $a_{sw}$  are the switch voltage, current, length, and area,  $q$  is the elementary charge of an electron and  $\mu$  is the electron mobility. Our switch length and area are 400  $\mu$ m and 0.5  $cm^2$ , respectively. The electron mobility is estimated to be 200  $cm^2/V$ -s. The peak carrier density is calculated using equation (1) from the minimum dynamic resistance (10  $\Omega$ ) measurements. The peak number of electron carriers excited in the switch is calculated to be  $2.5 \times 10^{14}/cm^3$  at 13 mJ excitation. The peak in carrier density corresponds to the peak optical intensity. The peak photon density injected into the switch volume is given by:

$$n_{ph} = \frac{P_{pk} \tau_r}{hvLwd} \quad (2)$$

where  $P_{pk}$ ,  $\tau_r$ , and  $hv$  are the peak optical power, electron recombination time and photon energy, respectively.  $L$ ,  $w$  and

d are the dimensions defining the switch volume irradiated by the optical pulse. The peak optical power is  $1.625 \times 10^6$  W for 13 mJ excitation at 1064 nm. The electron recombination is estimated to be  $\sim 2$  ns from our switching measurements. The switch volume irradiated by the optical pulse is  $0.04 \text{ cm}^3$ . The peak photon density is calculated to be  $4.35 \times 10^{17} / \text{cm}^3$ . The ratio of peak photon to electron density is 1740. One electron is excited into the conduction band for every 1740 photons injected into the switch volume. The triggering efficiency is 0.000575, which is the inverse of the peak photon to electron ratio.

### 3.4 PCSS ABSORPTION

Optical transmission was measured at 532 and 1064 nm by measuring the optical energies incident on the front facet and exiting the rear facet of a PCSS device. The absorption coefficient was calculated from the transmission measurements assuming only linear absorption was occurring. Absorption coefficients of  $1.29$  and  $1.59 \text{ cm}^{-1}$  were calculated at 9 mJ applied optical energy for the 1064 and 532 nm wavelengths, respectively. One would expect a much larger absorption coefficient for 532 nm excitation compared to 1064 nm excitation, considering the minimum dynamic switch resistance is almost five times lower for 532 nm excitation at 9 mJ (see Figure 5). However, the absorption coefficient includes all optical loss mechanisms. The optical loss due to photon absorption at extrinsic levels may be small in comparison to other loss mechanisms since the impurity densities are approximately one part in a million of the bulk material. The dominant optical loss mechanisms could be scattering at the substrate surface and electrode metalization. In addition, the peak applied optical power density at 9 mJ excitation is  $16 \text{ MW/cm}^2$ , which could be high enough to begin to produce nonlinear loss mechanisms.

### 3.5 ELECTRICAL FAILURE OF PCSS

A single PCSS device was tested to electrical failure of the 6H-SiC substrate. The charge circuit was modified to produce a  $3 \mu\text{s}$  rise time and the load resistor was reduced to 9 Ohms. The 1064 nm, 9 mJ, optical pulse was applied after a  $5 \mu\text{s}$  flat top interval of the pulse bias voltage. The PCSS device was submerged in a transparent liquid dielectric to prevent tracking around the edge of the device. The PCSS suffered catastrophic failure after the sixth switching operation at a pulsed bias voltage of 11 kV. Failure was abrupt without any degradation in switching performance. Linear switch operation was observed at all charge voltages. No signs of nonlinear, avalanche, or “lock-on” [7] effects were observed. In fact, PCSS failure occurred after recovery from conduction at the 11 kV bias voltage.

The 11 kV bias produces an average electric field of 27.4 MV/m in the 6H-SiC substrate. Failure occurred through the bulk of the substrate directly under the edge of the device metalization, the location of greatest electric field enhancement. A peak field of 200 MV/m was numerically calculated for the failure point from the geometry of the failed

device. We believe that making use of oxide coatings and SiC etching techniques will allow for PCSS device operations at significantly higher average electric fields.

### 3.6 DIFFERENCES IN PCSS DEVICES

The five PCSS devices fell into one of two categories based on minimum dynamic resistance. Four devices achieved a minimum dynamic on resistance of  $10 - 11 \Omega$  at 13 mJ optical excitation at 1064 nm. The remaining device had minimum dynamic on resistance of  $2-3 \Omega$  at optical excitation energies of 13 mJ at 1064 nm. There was no visible difference in the switch facets. It was concluded that the difference in PCSS minimum dynamic resistance for the two switch categories was a result of differences in impurity densities. The density of the vanadium (V), nitrogen (N), boron (B), and aluminum (Al) impurities were measured using Secondary Ion Mass Spectroscopy (SIMS) for the “low” resistance switch and one of the four “high” resistance switches. Aluminum is an intentional p-type dopant in 6H-SiC. The Al density was an order of magnitude lower than the N, V and B density and was assumed to have negligible effect on the switching process. The low resistance switch substrate had a higher density of N and lower density of V and B than the high resistance switch substrate. The lower resistance was attributed to the higher N density. The vanadium acceptor levels trap the electrons donated by the N levels. These are the electrons that are excited into the conduction band. The more electrons trapped by the vanadium acceptor levels, the lower the on resistance. The impurity density measurements have indicated a path toward optimizing the impurity levels in the vanadium compensated, 6H-SiC.

## 4 CONCLUSION

Bulk PCSS have been constructed from a-plane, vanadium compensated, semi-insulating 6H-SiC. The PCSS were switched on by optically exciting charge carriers from extrinsic levels using 532 and 1064 nm wavelength light. Operation in this manner allows for diffuse current conduction and the ability to take advantage of the high breakdown electric field of the bulk 6H-SiC material. PCSS resistance was reduced from  $170 \text{ G}\Omega$  to  $2$  and  $11 \Omega$  by applying 13 mJ optical energy pulses at 532 and 1064 nm wavelengths, respectively. Photoconductivity measurements were performed to a bias voltage level of 4.25 kV corresponding to an average electric of 10 MV/m between PCSS contacts. A slowly decaying current component with recombination times up to  $200 \mu\text{s}$  were observed for 532 nm wavelength excitation. A single PCSS was tested to electrical failure at an average field of 27.4 MV/m in the 6H-SiC substrate. The failure occurred at the point of highest electric field enhancement. We will utilize material processing techniques to achieve higher field operation of the PCSS devices. This initial work indicates that a compact, high voltage, high current switch can be developed from exciting the extrinsic levels in vanadium compensated, 6H-SiC substrates.

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## REFERENCES

- [1] S. Dogan, A. Teke, D. Huang, H. Morkoc, C. Roberts, J. Parish, B. Ganguly, M. Smith, R. Myers and S. Saddow, "4H-SiC photoconductive switching devices for use in high-power applications", *Appl. Phys. Letts.*, Vol. 82, pp. 3107-3109, 2003.
- [2] S. Sheng, M. Spencer, X. Tang, P. Zhou and G. Harris, "Polycrystalline cubic silicon carbide photoconductive switch", *IEEE Electron Device Letts.*, Vol. 18, pp 372-374, 1997.
- [3] K. Zhu, S. Dogan, Y. Moon, J. Leach, F. Yun, D. Johnstone, H. Morkoc, G. Li and B. Ganguly "Effect of n<sup>+</sup>-GaN subcontact layer on 4H-SiC high-power photoconductive switch", *Appl. Phys. Letts.* 86, p. 261108, 2005.
- [4] M. Bickermann, D. Hofmann, T. Straubinger, R. Weingartner and A. Winnacker, "Preparation of semi-insulating Silicon Carbide by Vanadium doping during PVT bulk crystal growth", *Materials Science Forum*, Vol. 433-436, pp. 51-54, 2003.
- [5] P. Cho, J. Goldhar, C. Lee, S. Saddow and P. Neudeck, "Photoconductive and photovoltaic response of high-dark-resistivity 6H-SiC devices", *J. Appl. Phys.*, Vol. 77, pp. 1591-1599, 1995.
- [6] T. Dalibor, G. Pensl, H. Matsunami, T. Kimoto, W. Choyke, A. Schonert and N. Nordell, "Deep defect centers in Silicon Carbide monitored with deep level transient spectroscopy", *Physica Status Solidi (A) Appl. Research*, Vol.162, pp. 199-225, 1997.
- [7] G.Loubriel, M. O'Malley and F. Zutavern, "Toward pulsed power uses for photoconductive semiconductor switches: closing switches", 6<sup>th</sup> IEEE Pulsed Power Conference, Arlington, VA, pp. 145-148, 1987.

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