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SUR, A Program to Generate Error Covariance Files

F. C. Difilippo

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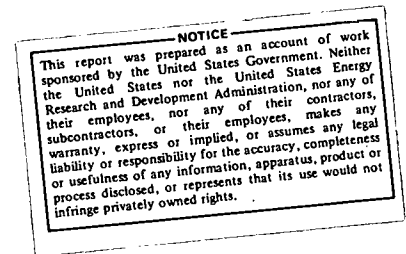
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Neutron Physics Division

SUR, A PROGRAM TO GENERATE ERROR COVARIANCE FILES

F. C. Difilippo*



*On assignment from Comisión Nacional de Energía Atómica, Argentina.

MARCH 1976

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Abstract

Covariance matrices were calculated for the ^{238}U , ^{241}Pu , and ^{239}Pu fission cross sections and for the ^{238}U , ^{240}Pu , ^{241}Pu , and ^{239}Pu capture cross sections. A computer program was written which uses the evaluated ENDF/B data files and the measured or evaluated (from other evaluations) cross sections for the calculation of the uncertainty files. An effort has been made to make the output of the program consistent with the ENDF/B error files format. A user's manual for the present code and references utilized in the covariance matrix calculations are given.

I. INTRODUCTION

The economic impact of nuclear data uncertainties in fast breeder as well as in thermal reactors has been the subject of many studies.¹⁻⁵ To evaluate the effect of group cross-section uncertainties in sensitivity calculations, the correlation both within the group structure and among different isotopes has to be calculated. Extensive discussions of this procedure are given in refs. 6-8.

II. CALCULATION OF RELATIVE COVARIANCE MATRICES

The relative covariance matrix elements are defined here as:

$$\text{COV}(I,J) = \left\langle \left(\frac{X_i^\ell - X_i}{X_i} \right) \left(\frac{X_j^\ell - X_j}{X_j} \right) \right\rangle, \quad (1)$$

where X_i^ℓ and X_j^ℓ are the group average cross sections for the i^{th} and j^{th} energy groups, respectively, for the ℓ^{th} data set. The cross sections X_i and X_j are the reference ("true") values, which by convention are taken to be the corresponding ENDF/B values. The bracket denotes a weighted average over the ensemble of data sets, having common data in the i^{th} and j^{th} groups, where weights, W_ℓ , have been assigned to each data set.

The ENDF/B-IV files, used as the reference data, were energy-weighted by a flat weighting function in producing the group-average cross sections. Details of calculations are given in Sect. III.

The present study of the error covariance matrix implies an "external" analysis of the data. Each data set, whether the results of a measurement or of an evaluation, is assigned an arbitrary weight and is compared with a reference line taken to be the ENDF/B-IV evaluation.

III. BRIEF DESCRIPTION OF THE PROGRAM

The calculations were done by the code SUR, which, in its present form, only handles error correlation for a given cross-section data set within a given energy range. A description of the main steps in the program follows.

Step 1: The program sets the energy limits of the group structure for several options: (1) constant lethargy interval, (2) decimal interval, or (3) a mixture of the first two.

Step 2: For the ratio measurements, the standard reference cross section was always the ENDF/B-IV evaluation.

Step 3: The measurements corresponding to the data set ℓ , inside a group j , are reduced to the mean energy of the group. This is implemented by approximating the shape of the cross section with a parabola determined by the evaluated cross sections in groups $j - 1$, j , $j + 1$. Then, all the measurements corresponding to the data set ℓ , inside group j , are averaged.

Step 4: Whenever there are not measurements in the l^{th} set of data, inside group j ; the program makes a linear interpolation of data set, l , values corresponding to the neighboring groups. Before implementing the interpolation, the program searches whether or not the data points for the interpolation procedure are within energy limits preset by the user. If not, the interpolation is not made.

Step 5: Calculation of $\text{COV}(I,J)$ is made. This is done by the formula

$$\text{COV}(I,J) = \frac{1}{\text{RR}} \sum_{K=1}^{\text{NA}} \left[\frac{\sigma(K,I) - \sigma(I)}{\sigma(I)} \right] \left[\frac{\sigma(K,J) - \sigma(J)}{\sigma(J)} \right] W(K) , \quad (2)$$

where

$$\text{RR} = \sum_{K=1}^{\text{NA}'} W(K) , \quad (3)$$

$\sigma(K,I)$, $\sigma(K,J)$ = measured or interpolated cross sections of data set K , in groups I and J ,

$\sigma(I)$, $\sigma(J)$ = evaluated cross sections of groups I and J ,

$W(K)$ = weight of data set K ,

NA = number of data sets with common, given or interpolated, measurement in groups I and J ,

NA' = number of data sets with measured or interpolated cross sections in group I or J , whichever is greater.

If there are not common data sets in groups I and J, the covariance is set to zero. If there are not data inside a group, the standard deviation for that group is set to the average of the corresponding values in neighboring groups.

Step 6: The program also calculates the correlation matrix [COR(I,J)] according to the formula

$$\text{COR}(I,J) = \frac{\text{COV}(I,J)}{\sqrt{\text{COV}(I,I) \text{COV}(J,J)}} \quad (4)$$

IV. DESCRIPTION OF THE INPUT-OUTPUT SPECIFICATIONS

A. Input

Card 1: NG,NAS,NAR,NL,IØP,MAT,MT,IP,IPØ,EMA,RLER,RLET,DELT,ECA,ID
[FORMAT(9I4,5E7.0,I1)]

NG: number of group;

NAS: number of cross-section data sets included in the error file evaluation;

NAR: number of ratio data sets included in the error file evaluation;

NL: number of energy limits preset to make linear interpolation between measurements in a given data set;

IØP: option

= 0, the word FISSION is printed;

= 1, the word CAPTURE is printed;

= 3, the word ALFA is printed;

MAT: material number according to ENDF/B specifications;

MT: reaction-type number according to ENDF/B specifications;
 IP: option
 = 0, part of the input is a cross-section ratio;
 ≠ 0, otherwise;
 IPØ: = 1, the output includes punched cards of the covariance matrix
 according to ENDF/B format;
 ≠ 1, otherwise;
 EMA: higher energy limit corresponding to group 1 (MeV) (group 1
 is the highest energy group);
 RLER: lethargy corresponding to the lower limit of group 1 (it is
 assumed that lethargy zero corresponds to 10 MeV);
 RLET: group lethargy interval;
 DELT: (MeV) increment corresponding to the first energy decade in the
 decimal group structure;
 ECA: (MeV) higher energy limit of the decimal group structure; if
 all the groups are decimal, ECA must be greater than EMA; if
 all the groups are of constant lethargy ECA must be lower than
 the lower limit of the last group;
 ID: ≠ 0, the output includes punched cards of the correlation
 matrix;
 = 0, otherwise.

Cards 2: NPE(ℓ), $\ell = 1, NA$; $NA = NAS + NAR$ [FORMAT (1415)]

Number of experimental points of set ℓ .

Cards 3: FORMAT (7E10.0)

Cross sections corresponding to the data set ℓ .

Cards 4: FØRMAT (7E10.0) (MeV)

Energies corresponding to the previous data set.

Cards 3 and Cards 4 must be repeated in a sequential order from $\ell = 1$ to $\ell = \text{NAS}$. Following these cards, one has to place a set of cards in the same format but now for the ratio measurements (only present if $\text{IP} = 0$).

Cards 5: ENDF/B evaluated cross section for group J ($J = 1, \text{NG}$)

[FØRMAT(6E12.0)]

Cards 6: (Only present if $\text{IP} = 0$.) FØRMAT (6E12.0), ENDF/B evaluated cross sections for group J ($J = 1, \text{NG}$) of the reference standard cross section corresponding to the ratio measurement. (It is assumed that all ratio measurements in the input are relative to the same cross section.)

Cards 7: FØRMAT (7E10.0)

Weight corresponding to each data set ℓ , ($\ell = 1, \text{NA}$).

Cards 8: FØRMAT (7E10.0). Energy limits for the interpolation procedure (see step 4 in Sect. III). These limits are preset by the user, based on his judgment on the validity of the interpolation scheme. The limits must be given in MeV and in decreasing order [EL(J), $J = 1, \text{NL}$].

B. Output

Printed output:

- (1) All the measured cross sections are ordered and displayed according to authors and group limits.
- (2) The evaluated and the measured cross sections (now reduced to the mean energy of the group interval) are ordered and displayed according to authors and group limits.
- (3) The covariance matrix.
- (4) The relative standard deviation.
- (5) The information contained in each punched card corresponding to the covariance matrix in the ENDF/B format.
- (6) The information contained in each punched card corresponding to the correlation matrix. The formats are the following:
 First NG cards (three values in each card):
 Lower energy limit (MeV) in group I, and the corresponding relative standard deviation in percent and reference cross sections (1X,E11.4,11X,E11.4,F11.4)
 The rest of the cards:
 COR(I,J), for each I, J varies from 1 to NG format 7E10.4.
 These cards are suitable for a three-dimensional plot of the correlation matrix.
- (7) The correlation matrix is printed as can be seen in Appendix B.

Punched card:

With the option (IPO = 1), the covariance matrix is punched out according to the ENDF/B format.

The correlation matrix output is punched out, under option.

V. LISTING OF THE PROGRAM AND SAMPLE PROBLEM

Data for the sample problem: [COV(I,J) for the ^{240}Pu capture cross section].

NG = 45; NAS = 4; NAR = 0; NL = 2; IOP = 1; MAT = 1265; MT = 102;

IP = 1; IPO = 1; EMA = 10.; RLER = 0.; RLET = 0.; DELT = 1.

ECA = 11.; ID = 1

NPE($\ell = 1,4$) : 29;6;36;36

EL(J = 1,2) = 11., .0001

```

**FTN,L,G,E,Y.
C *****LISTING OF THE PROGRAM SUR*****
C THIS PROGRAM CALCULATES THE COVARIANCE AND CORRELATION MATRICES OF
C CROSS SECTIONS.THE COVARIANCE MATRIX FILE IS PUNCHED ACCORDING TO THE
C EENDF/R FORMAT. THE CORRELATION MATRIX IN A FORMAT SUITABLE FOR 3-D PLOT
C
  DIMENSION SFE28(120),SFE25(120),SFM28(35,150),E(35,150),ER(35),NPE
  1(35),EV(120),SFM(35,120),NM(120),COV(120,120),NMAR(35,120),EL(12),
  2W(35),AUX(120,120),TITLE(18),STA(100)
  DIMENSION LABEL(120)
  DIMENSION NDER(28)
857 DC 125 I=1,35
  DC 125 J=1,150
  125 SFM28(I,J)=C.
C DATA INPUT
  READ 1,NG,NAS,NAR,NL,IOP,MAT,MT,IP,IPC,EMA,RLER,RLET,DELT,ECA,IO
  1 FORMAT(9I4,5E7.0,I1)
  IF(NG.EQ.0).CALL EXII
  NA=NAS+NAR
  READ 2,(NPE(I),I=1,NA)
  2 FORMAT(14I5)
  DO 3 I=1,NA
  JM=NPE(I)
  READ 4,(SFM28(I,J),J=1,JM)
  3 READ 4,(E(I,J),J=1,JM)
  4 FORMAT(10E8.0)
  READ 6,(SFE28(I),I=1,NG)
  6 FORMAT(10E8.0)
  IF(IP.NE.0) GO TO 253
  READ 6,(SFE25(I),I=1,NG)
  253 READ 4,(W(I),I=1,NA)
  READ 4,(EL(I),I=1,NL)
  READ 400,(TITLE(I),I=1,18)
  400 FORMAT(18A4)
C RATIO MEASUREMENT ARE REDUCED TO ABSOLUTE ONES, AND LOCATED IN THE SAME
C LOCATION, THEN WE LOCSE THE RATIOS. EV(I) ARE THE LIMITS OF GROUP I.
  EV(1)=EMA
  DEL=DELT
  NE=NG+1
  DO 243 I=2,NE
  IF(ECA.GT.EMA) GO TO 245
  EV(I)=10.*EXP(-RLER)
  IF(EV(I).GT.ECA) GO TO 244
  EV(K)=ECA-DEL
  IF(I.EQ.K) GO TO 243
  245 CONTINUE
  IF(ABS(EV(I-2)/EV(I-1)-2.).LT.1.E-03) DELT=DELT*.1
  EV(I)=EV(I-1)-DELT
  GO TO 243
  244 RLER=RLER+RLET
  K=I+1
  243 CONTINUE
  IF(IP.NE.0) GO TO 254
  NR=NAS+1
  DO 8 I=NR,NA
  JM=NPE(I)
  DO 8 J=1,JM
  K=1
  9 CCNTINUE
  IF(E(I,J).LE.EV(K).AND.E(I,J).GT.EV(K+1)) GO TO 10
  K=K+1
  IF(K.EQ.NE) GO TO 8
  GO TO 9
  10 IF(K.EQ.1) GO TO 845
  IF(K.EQ.NG) GO TO 846
  EK1=(EV(K+1)+EV(K+2))/2.
  EK2=(EV(K)+EV(K+1))/2.
  EK3=(EV(K)+EV(K-1))/2.
  AC=(SFE25(K+1)-SFE25(K))/((EK1-EK2)*(EK2-EK3))-(SFE25(K+1)-SFE25(K
  1-1))/((EK1-EK3)*(EK2-EK3))
  BC=(SFE25(K+1)-SFE25(K))/(EK1-EK2)-AC*(EK1+EK2)
  CC=SFE25(K+1)-AC*EK1*EK1-BC*EK1
  SF25=AC*E(I,J)**2+BC*E(I,J)+CC
  GO TO 87
  846 EK=(EV(K)+EV(K+1))/2.
  EK1=(EV(K-1)+EV(K))/2.
  SF25=SFE25(K)+(SFE25(K-1)-SFE25(K))/(EK1-EK)*(E(I,J)-EK)
  GO TO 87
  845 E1=(EV(1)+EV(2))/2.
  E2=(EV(2)+EV(3))/2.
  PE=(SFE25(1)-SFE25(2))/(E1-E2)
  SF25=SFE25(2)+PE*(E(I,J)-E2)
  E7 SFM28(I,J)=SFM28(I,J)*SF25
  8 CCNTINUE
C OUTPUT OF MEASURED DATA
  254 PRINT 11
  11 FORMAT(1H1,6H GROUP,3X,20H ENERGY LIMITS (MEV),8X,16H MEASURED VAL
  1UES//)
  DC 12 J=1,NG
  IF(IOP.EQ.0) PRINT 13,J,EV(J),EV(J+1)
  IF(IOP.EQ.1) PRINT 53,J,EV(J),EV(J+1)
  IF(IOP.EQ.3) PRINT 325,J,EV(J),EV(J+1)

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13 FORMAT(16,3X,1PE11.4,3X,1PE11.4,3X,7H AUTHOR,3X,7H ENERGY,7X,11H S
14 IGFSSION,7H WEIGHT)
13 FORMAT(16,3X,1PE11.4,3X,1PE11.4,3X,7H AUTHOR,3X,7H ENERGY,7X,11H S
14 IGCAPTURE,7H WEIGHT)
325 FORMAT(16,3X,1PE11.4,3X,1PE11.4,3X,7H AUTHOR,3X,7H ENERGY,7X,11H
1 ALFA,7H WEIGHT)
L=0
DO 14 I=1,NA
KN=NFE(I)
DO 14 K=1,KM
IF(E(I,K).GT.EV(J).OR.E(I,K).LE.EV(J+1)) GO TO 14
PRINT 16,I,E(I,K),SFM28(I,K),W(I)
16 FORMAT(4,3X,12,3X,1PE11.4,3X,1PE11.4,2X,FS,2)
L=1
14 CONTINUE
IF(L.EQ.0) PRINT 17
17 FORMAT(4,3X,15H NO MEASUREMENT)
12 CONTINUE
C THE MEASUREMENT OF AUTHOR I INSIDE GROUP J IS REDUCED TO THE MEAN ENERGY OF
C THE GROUP AND THEN AVERAGED. THE RESULTS ARE LOCATED IN SFM(I,J)
DO 18 J=1,12C
NM(J)=0
DO 18 I=1,35
18 SFM(I,J)=0.
DO 19 I=1,NA
KN=NFE(I)
DO 19 J=1,NG
NR=0.
DO 20 K=1,KM
IF(E(I,K).GT.EV(J).OR.E(I,K).LE.EV(J+1)) GO TO 20
IF(J.EQ.1) GO TO 354
IF(J.EQ.NG) GO TO 355
EJ1=(EV(J+1)+EV(J+2))/2.
EJ2=(EV(J)+EV(J+1))/2.
EJ3=(EV(J)+EV(J-1))/2.
AC=(SFE28(J+1)-SFE28(J))/((EJ1-EJ2)*(EJ2-EJ3))-
(SFE28(J+1)-SFE28(J-1))/((EJ1-EJ3)*(EJ2-EJ3))
BC=(SFE28(J+1)-SFE28(J))/(EJ1-EJ2)-AC*(EJ1+EJ2)
CC=SFE28(J+1)-AC*EJ1+EJ1-BC*EJ1
RK=SFM28(I,K)/(AC*E(I,K)**2+BC*E(I,K)+CC)
AC=RK*AC
BC=RK*BC
CC=RK*CC
SFM(I,J)=SFM(I,J)+AC*EJ2**2+BC*EJ2+CC
RR=RR+1.
GO TO 20
355 EJ=(EV(J+1)+EV(J))/2.
EJ1=(EV(J)+EV(J-1))/2.
PE=(SFE28(J-1)-SFE28(J))/(EJ1-EJ)
SFM(I,J)=SFM(I,J)+SFM28(I,K)-PE*(E(I,K)-EJ)
RR=RR+1.
GO TO 20
354 E1=(EV(1)+EV(2))/2.
E2=(EV(2)+EV(3))/2.
PE=(SFE28(1)-SFE28(2))/(E1-E2)
SFM(I,1)=SFM(I,1)+SFM28(I,K)-PE*(E(I,K)-E1)
RR=RR+1.
20 CONTINUE
IF(NR.GT.0.) SFM(I,J)=SFM(I,J)/RR
19 CONTINUE
C NUMBER OF REAL MEASUREMENTS NM(J) INTO EACH GROUP
DO 21 J=1,NG
DO 21 I=1,NA
NMAR(I,J)=1
IF(SFM(I,J).GT.0.) NM(J)=NM(J)+1
21 CONTINUE
C THOSE GROUP AND AUTHORS IN WHICH THERE ARE NO MEASUREMENT ARE MARKED
DO 457 J=1,NG
DO 457 I=1,NA
IF(SFM(I,J).EQ.0.) NMAR(I,J)=0
457 CONTINUE
C ASSIGNATION OF AUTHOR I MEASUREMENT IN GROUP J BY INTERPOLATION
C (IF POSSIBLE)
DO 110 J=1,NG
IF(J.EQ.1.OR.J.EQ.NG) GO TO 110
DO 110 I=1,NA
IF(SFM(I,J).NE.0.) GO TO 110
L=1
111 CONTINUE
IF(EV(J).LE.EL(L).AND.EV(J).GT.EL(L+1)) GO TO 112
L=L+1
GO TO 111
112 KAR=J-1
113 CONTINUE
IF(SFM(I,KAR).NE.0.) GO TO 114
KAR=KAR-1
IF(KAR.EQ.0) GO TO 110
IF(EV(KAR).LE.EL(L)) GO TO 113
114 IF(EV(KAR).GT.EL(L)) GO TO 110
KAB=J+1
115 CONTINUE
IF(SFM(I,KAB).NE.0.) GO TO 116
KAB=KAB+1
IF(KAB.GT.NG) GO TO 110
IF(EV(KAB).GT.EL(L+1)) GO TO 115

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116 IF(EV(KAB+1).LT.EL(L+1)) GO TO 110
EAR=(EV(KAR)+EV(KAR+1))/2.
EAB=(EV(KAB)+EV(KAB+1))/2.
EJ=(EV(J)+EV(J+1))/2.
IF(SFM(I,KAR).EQ.0..OR.SFM(I,KAB).EQ.0.) GO TO 110
SFM(I,J)=SFM(I,KAB)+(SFM(I,KAR)-SFM(I,KAB))/(EAR-EAB)*(EJ-EAB)
NM(J)=NM(J)+1
110 CONTINUE
C CALCULATION OF THE DIAGONAL TERMS OF COV(I,J)
DO 22 I=1,NG
DO 22 J=1,NG
22 COV(I,J)=0.
DO 23 J=1,NG
IF(NM(J).EQ.0) GO TO 23
RR=0.
DO 25 I=1,NA
IF(SFM(I,J).EQ.0.) GO TO 25
COV(J,J)=CCV(J,J)+(SFM(I,J)-SFE28(J))*2*W(I)
RR=RR+W(I)
25 CONTINUE
COV(J,J)=CCV(J,J)/RR
23 CONTINUE
DO 28 J=1,NG
IF(COV(J,J).NE.0.) GO TO 28
KAB=J+1
29 CONTINUE
IF(COV(KAB,KAB).EQ.0.) GO TO 30
GO TO 31
30 KAB=KAB+1
GO TO 29
31 KAR=J-1
32 CONTINUE
IF(COV(KAR,KAR).EQ.0.) GO TO 33
GO TO 34
33 KAR=KAR-1
GO TO 32
34 COV(J,J)=(CCV(KAB,KAB)+COV(KAR,KAR))/2.
28 CONTINUE
C OUTPUT OF DATA
PRINT 35
35 FORMAT(1H1,6H GROUP,3X,10H EVALUATED,3X,60H MEASURES AND INTERPOLA
TED VALUES REDUCED TO THE MESH ENERGY//)
DO 36 J=1,NG
IF(IOP.EQ.0) PRINT 37,J,SFE28(J)
IF(IOP.EQ.1) PRINT 54,J,SFE28(J)
IF(IOP.EQ.3) PRINT 326,J,SFE28(J)
37 FORMAT(16,3X,1PE11.4,3X,5H SIGE,8X,7H AUTHOR,18X,7H WEIGHT//)
326 FORMAT(16,3X,1PE11.4,3X,5H ALFA,8X,7H AUTHOR,18X,7H WEIGHT//)
54 FORMAT(16,3X,1PE11.4,3X,5H SIGC,8X,7H AUTHOR,18X,7H WEIGHT//)
IF(NM(J).EQ.0) PRINT 38
38 FORMAT(23X,12H NEITHER MEASUREMENT NOR INTERPOLATION//)
DO 36 I=1,NA
IF(SFM(I,J).EQ.0.) GO TO 36
IF(NMAR(I,J).EQ.0) PRINT 39,SFM(I,J),I,W(I)
IF(NMAR(I,J).NE.0) PRINT 40,SFM(I,J),I,W(I)
39 FORMAT(23X,1PE11.4,5X,14,3X,13H INTERPOLATED,2X,F5.2)
40 FORMAT(23X,1PE11.4,5X,14,3X,9H MEASURED,6X,F5.2)
36 CONTINUE
C CALCULATION OF COV(I,J) WITH I.NE.J
DO 41 I=1,NG
DO 41 J=1,NG
RR=0.
RRJ=0.
IF(I.EQ.J) GO TO 41
DO 42 K=1,NA
IF(SFM(K,I).EQ.0..OR.SFM(K,J).EQ.0.) GO TO 142
COV(I,J)=COV(I,J)+(SFM(K,I)-SFE28(I))*(SFM(K,J)-SFE28(J))*W(K)
142 IF(SFM(K,I).NE.0.) RRI=RRI+W(K)
IF(SFM(K,J).NE.0.) RRJ=RRJ+W(K)
42 CONTINUE
IF(RRI.GE.RRJ) RR=RRI
IF(RRI.LE.RRJ) RR=RRJ
IF(RR.NE.0.) COV(I,J)=COV(I,J)/RR
41 CONTINUE
C OUTPUT OF DATA
PRINT 499
499 FORMAT(1H1)
DO 357 I=1,NG
DO 357 J=1,NG
357 COV(I,J)=COV(I,J)/(SFE28(I)*SFE28(J))
DO 43 I=1,NG
PRINT 44,I,NG
44 FORMAT(9H COV(I,J),4X,3H I=,I3,4X,12H J FROM 1 TO, I3//)
PRINT 45,(COV(I,J),J=1,NG)
45 FORMAT(1P10E12.4)
43 CONTINUE
NG1=NG+1
DO 210 I=1,NG1
210 EV(I)=1000000.*EV(I)
E0=.00001
EM=20000000.
MI=0
FI=0.
MIA=33
RIA=1.
MTI=MT
C THE ORDER IN THE GROUPS ARE INVERTED

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```

MX=NG1/2
DO 212 I=1,MX
  EVT=EV(I)
  EV(I)=EV(NG1+1-I)
  EV(NG1+1-I)=EVT
212 MX=NG/2
DO 213 I=1,MX
  SFT=SFE28(I)
  SFE28(I)=SFE28(NG+1-I)
  SFE28(NG+1-I)=SFT
  EV(NG1+1)=200C0000.
  IF(EV(NG1).EQ.EV(NG1+1)) EV(NG1)=EV(NG1)-.001*EV(NG1)
  DO 214 I=1,NG
  DO 214 J=1,NG
214 AUX(NG+1-I,NG+1-J)=COV(I,J)
  DO 215 J=1,NG
  AUX(NG+1,J)=0.
215 AUX(NG+2,J)=0.
  PRINT 46,NG
  46 FORMAT(1H1,31H RELATIVE ERROR FROM GROUP 1 TO,13)
  DO 47 I=1,NG
  COV(I,1)=SQRT(COV(I,1))
  47 CCNTINUE
  PRINT 48,(COV(I,1),I=1,NG)
  48 FORMAT(10F10.5)
  PRINT 211
211 FORMAT(1H1,63H CARDS OUTPUT, WARNING THE ORDER IN THE GROUPS ARE NOW
  10W INVERTED//35H COV(I,J) CARDS IN THE ENDF/B FORMAT//)
  N3=NG+3
  LB=3
  N14=2*NG+14
  N7=NG+7
  DO 216 J=1,NG
  IF(J.EQ.1) PRINT 217,MI,MT1,MI,NG,MAT,MIA,MT
  IF(J.EQ.1.AND.IPO.EQ.1) PUNCH 217,MI,MT1,MI,NG,MAT,MIA,MT
  IF(J.GT.1) PRINT 217,N3,LB,N14,N7,MAT,MIA,MT
  IF(J.GT.1.AND.IPO.EQ.1) PUNCH 217,N3,LB,N14,N7,MAT,MIA,MT
217 FORMAT(22X,4I11,14,I2,I3)
  PRINT 218,E0,RI,EVL(J),RIA,EV(J+1),RI,MAT,MIA,MT
  IF(IPO.EQ.1) PUNCH 218,E0,RI,EV(J),RIA,EV(J+1),RI,MAT,MIA,MT
218 FORMAT(6E11.4,I4,I2,I3)
  PRINT 219,EM,RI,E0,RI,EV(I),AUX(I,J),MAT,MIA,MT
  IF(IPO.EQ.1) PUNCH 219,EM,RI,E0,RI,EV(I),AUX(I,J),MAT,MIA,MT
219 FORMAT(6E11.4,I4,I2,I3)
  NG2=NG+2
  I=2
221 CCNTINUE
  PRINT 220,EV(I),AUX(I,J),EV(I+1),AUX(I+1,J),EV(I+2),AUX(I+2,J),MAT
  1,MIA,MT
  IF(IPO.EQ.1) PUNCH 220,EV(I),AUX(I,J),EV(I+1),AUX(I+1,J),EV(I+2),A
  UX(I+2,J),MAT,MIA,MT
220 FORMAT(6E11.4,I4,I2,I3)
  I=I+3
  IF((NG2-I).GE.2) GO TO 221
  IF((NG2-I).EQ.1) GO TO 222
  IF((NG2-I).EQ.0) GO TO 223
  GO TO 230
222 PRINT 224,EV(I),AUX(I,J),EV(I+1),AUX(I+1,J),MAT,MIA,MT
  IF(IPO.EQ.1) PUNCH 224,EV(I),AUX(I,J),EV(I+1),AUX(I+1,J),MAT,MIA,MT
  IT
224 FORMAT(4E11.4,22X,I4,I2,I3)
  GO TO 230
223 PRINT 225,EV(I),AUX(I,J),MAT,MIA,MT
  IF(IPO.EQ.1) PUNCH 225,EV(I),AUX(I,J),MAT,MIA,MT
225 FORMAT(2E11.4,44X,I4,I2,I3)
230 CONTINUE
216 CCNTINUE
  IF(ID.NE.0) PUNCH 309, TITLE,NG
309 FORMAT(18A4/15)
  PRINT 310
310 FORMAT(1H1,41H CORRELATION MATRIX CARDS FOR THE DRAWING//)
  DO 300 I=1,NG
  ST=100.*SQRT(AUX(I,1))
  ENE=.000001*EV(I)
  PRINT 301,ENE,ST
  IF(ID.NE.0) PUNCH 301,ENE,ST,SFE28(I)
301 FORMAT(1X,E11.4,11X,E11.4,F11.4)
300 CCNTINUE
  ENE=EV(NE)/10**6
  IF(ID.NE.0) PUNCH 301,ENE
  DO 311 I=1,NG
  DO 311 J=1,NG
311 COV(I,J)=AUX(I,J)/SQRT(AUX(I,1)*AUX(J,1))
  DO 302 I=1,NG
  PRINT 305,(COV(I,J),J=1,NG)
  IF(ID.NE.0) PUNCH 303,(COV(I,J),J=1,NG)
303 FORMAT(8F9.5)
305 FORMAT(1X,7E10.4)
302 CCNTINUE
  DO 391 I=1,NG
391 STA(I)=100.*SQRT(AUX(I,1))
  PRINT 402, TITLE
402 FORMAT(1H1,18A4)
  DO 399 N=2,28
399 NDER(N)=4H
  DC 400 L=1,NG

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400 LABEL(L)=L
    L1=1
401 LM=L1+27
    IF(LM.GT.NG) LM=NG
    PRINT 405, (LABEL(L), L=L1, LM)
405 FCRMAT(29H0 I ELC(KEV) RSD CCRR*100 /14X3HPCT,1X10I4,1X10I4,
    1 1X8I4)
    PRINT 430
430 FORMAT(1H )
    DO 421 I=L1,NG
    ENE=EV(I)/1000.
    DC 405 L=L1,LM
    TEMP= COV(I,L)*100.
409 LABEL(L)=TEMP
410 PRINT 406, I, ENE, STA(I), (LABEL(L), L=L1, LM)
    IL=I+1-L1
    IF(IL.GT.28) GO TO 421
    NDER(IL)=4H
    PRINT 420, NDER
420 FORMAT(1H+, 17X10A4, 1X10A4, 1X8A4)
    NDER(IL)=4H
421 CONTINUE
    ENE= EV(NE)/1000.
    PRINT 406, NE, ENE
    L1=LM+1
    IF(L1.LE.NG) GO TO 401
406 FORMAT(1F 13.F8.2,F5.1, 1X10I4,1X10I4,1X8I4)
408 CONTINUE
    GO TO 897
    END

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Line	Value 1	Value 2	Category	Unit	Energy	Sig Capture	Weight
27	2.0000E-02	1.0000E-02	AUTHOR	1	ENERGY	SIGCAPTURE	WEIGHT
					1.0000E-00	1.0000E-00	9.00
					1.1200E-00	1.1200E-00	9.00
					1.3000E-00	1.3000E-00	9.00
					1.5000E-00	1.5000E-00	9.00
					1.7000E-00	1.7000E-00	9.00
					1.9000E-00	1.9000E-00	9.00
					2.1000E-00	2.1000E-00	9.00
					2.3000E-00	2.3000E-00	9.00
					2.5000E-00	2.5000E-00	9.00
					2.7000E-00	2.7000E-00	9.00
					2.9000E-00	2.9000E-00	9.00
					3.1000E-00	3.1000E-00	9.00
					3.3000E-00	3.3000E-00	9.00
					3.5000E-00	3.5000E-00	9.00
					3.7000E-00	3.7000E-00	9.00
					3.9000E-00	3.9000E-00	9.00
					4.1000E-00	4.1000E-00	9.00
					4.3000E-00	4.3000E-00	9.00
					4.5000E-00	4.5000E-00	9.00
					4.7000E-00	4.7000E-00	9.00
					4.9000E-00	4.9000E-00	9.00
					5.1000E-00	5.1000E-00	9.00
					5.3000E-00	5.3000E-00	9.00
					5.5000E-00	5.5000E-00	9.00
					5.7000E-00	5.7000E-00	9.00
					5.9000E-00	5.9000E-00	9.00
					6.1000E-00	6.1000E-00	9.00
					6.3000E-00	6.3000E-00	9.00
					6.5000E-00	6.5000E-00	9.00
					6.7000E-00	6.7000E-00	9.00
					6.9000E-00	6.9000E-00	9.00
					7.1000E-00	7.1000E-00	9.00
					7.3000E-00	7.3000E-00	9.00
					7.5000E-00	7.5000E-00	9.00
					7.7000E-00	7.7000E-00	9.00
					7.9000E-00	7.9000E-00	9.00
					8.1000E-00	8.1000E-00	9.00
					8.3000E-00	8.3000E-00	9.00
					8.5000E-00	8.5000E-00	9.00
					8.7000E-00	8.7000E-00	9.00
					8.9000E-00	8.9000E-00	9.00
					9.1000E-00	9.1000E-00	9.00
					9.3000E-00	9.3000E-00	9.00
					9.5000E-00	9.5000E-00	9.00
					9.7000E-00	9.7000E-00	9.00
					9.9000E-00	9.9000E-00	9.00
					1.0000E-00	1.0000E-00	9.00
					1.1000E-00	1.1000E-00	9.00
					1.2000E-00	1.2000E-00	9.00
					1.3000E-00	1.3000E-00	9.00
					1.4000E-00	1.4000E-00	9.00
					1.5000E-00	1.5000E-00	9.00
					1.6000E-00	1.6000E-00	9.00
					1.7000E-00	1.7000E-00	9.00
					1.8000E-00	1.8000E-00	9.00
					1.9000E-00	1.9000E-00	9.00
					2.0000E-00	2.0000E-00	9.00
					2.1000E-00	2.1000E-00	9.00
					2.2000E-00	2.2000E-00	9.00
					2.3000E-00	2.3000E-00	9.00
					2.4000E-00	2.4000E-00	9.00
					2.5000E-00	2.5000E-00	9.00
					2.6000E-00	2.6000E-00	9.00
					2.7000E-00	2.7000E-00	9.00
					2.8000E-00	2.8000E-00	9.00
					2.9000E-00	2.9000E-00	9.00
					3.0000E-00	3.0000E-00	9.00
					3.1000E-00	3.1000E-00	9.00
					3.2000E-00	3.2000E-00	9.00
					3.3000E-00	3.3000E-00	9.00
					3.4000E-00	3.4000E-00	9.00
					3.5000E-00	3.5000E-00	9.00
					3.6000E-00	3.6000E-00	9.00
					3.7000E-00	3.7000E-00	9.00
					3.8000E-00	3.8000E-00	9.00
					3.9000E-00	3.9000E-00	9.00
					4.0000E-00	4.0000E-00	9.00
					4.1000E-00	4.1000E-00	9.00
					4.2000E-00	4.2000E-00	9.00
					4.3000E-00	4.3000E-00	9.00
					4.4000E-00	4.4000E-00	9.00
					4.5000E-00	4.5000E-00	9.00
					4.6000E-00	4.6000E-00	9.00
					4.7000E-00	4.7000E-00	9.00
					4.8000E-00	4.8000E-00	9.00
					4.9000E-00	4.9000E-00	9.00
					5.0000E-00	5.0000E-00	9.00
					5.1000E-00	5.1000E-00	9.00
					5.2000E-00	5.2000E-00	9.00
					5.3000E-00	5.3000E-00	9.00
					5.4000E-00	5.4000E-00	9.00
					5.5000E-00	5.5000E-00	9.00
					5.6000E-00	5.6000E-00	9.00
					5.7000E-00	5.7000E-00	9.00
					5.8000E-00	5.8000E-00	9.00
					5.9000E-00	5.9000E-00	9.00
					6.0000E-00	6.0000E-00	9.00
					6.1000E-00	6.1000E-00	9.00
					6.2000E-00	6.2000E-00	9.00
					6.3000E-00	6.3000E-00	9.00
					6.4000E-00	6.4000E-00	9.00
					6.5000E-00	6.5000E-00	9.00
					6.6000E-00	6.6000E-00	9.00
					6.7000E-00	6.7000E-00	9.00
					6.8000E-00	6.8000E-00	9.00
					6.9000E-00	6.9000E-00	9.00
					7.0000E-00	7.0000E-00	9.00
					7.1000E-00	7.1000E-00	9.00
					7.2000E-00	7.2000E-00	9.00
					7.3000E-00	7.3000E-00	9.00
					7.4000E-00	7.4000E-00	9.00
					7.5000E-00	7.5000E-00	9.00
					7.6000E-00	7.6000E-00	9.00
					7.7000E-00	7.7000E-00	9.00
					7.8000E-00	7.8000E-00	9.00
					7.9000E-00	7.9000E-00	9.00
					8.0000E-00	8.0000E-00	9.00
					8.1000E-00	8.1000E-00	9.00
					8.2000E-00	8.2000E-00	9.00
					8.3000E-00	8.3000E-00	9.00
					8.4000E-00	8.4000E-00	9.00
					8.5000E-00	8.5000E-00	9.00
					8.6000E-00	8.6000E-00	9.00
					8.7000E-00	8.7000E-00	9.00
					8.8000E-00	8.8000E-00	9.00
					8.9000E-00	8.9000E-00	9.00
					9.0000E-00	9.0000E-00	9.00
					9.1000E-00	9.1000E-00	9.00
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					1.6000E-00	1.6000E-00	9.00
					1.7000E-00	1.7000E-00	9.00
					1.8000E-00	1.8000E-00	9.00
					1.9000E-00	1.9000E-00	9.00
					2.0000E-00	2.0000E-00	9.00
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					2.2000E-00	2.2000E-00	9.00
					2.3000E-00	2.3000E-00	9.00
					2.4000E-00	2.4000E-00	9.00
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					2.6000E-00	2.6000E-00	9.00
					2.7000E-00	2.7000E-00	9.00
					2.8000E-00	2.8000E-00	9.00
					2.9000E-00	2.9000E-00	9.00
					3.0000E-00	3.0000E-00	9.00
					3.1000E-00	3.1000E-00	9.00
					3.2000E-00	3.2000E-00	9.00
					3.3000E-00	3.3000E-00	9.00
					3.4000E-00	3.4000E-00	9.00
					3.5000E-00	3.5000E-00	9.00
					3.6000E-00	3.6000E-00	9.00
					3.7000E-00	3.7000E-00	9.00

GROUP EVALUATED MEASURES AND INTERPOLATED VALUES REDUCED TO THE MESN ENERGY

GROUP	EVALUATED	MEASURES AND INTERPOLATED VALUES REDUCED TO THE MESN ENERGY	AUTHOR	WEIGHT
1	5.1000E-03	SIGC		
		4.7000E-03	3	MEASURED 1.00
		4.7000E-03	4	MEASURED 1.00
2	5.8000E-03	SIGC		
		5.7000E-03	3	MEASURED 1.00
		5.3000E-03	4	MEASURED 1.00
3	6.9000E-03	SIGC		
		7.0000E-03	3	MEASURED 1.00
		6.0000E-03	4	MEASURED 1.00
4	8.5000E-03	SIGC		
		8.3000E-03	3	MEASURED 1.00
		7.1000E-03	4	MEASURED 1.00
5	1.1000E-02	SIGC		
		1.1000E-02	3	MEASURED 1.00
		8.5000E-03	4	MEASURED 1.00
6	1.5000E-02	SIGC		
		1.6000E-02	3	MEASURED 1.00
		1.1000E-02	4	MEASURED 1.00
7	2.4000E-02	SIGC		
		2.4000E-02	3	MEASURED 1.00
		1.7000E-02	4	MEASURED 1.00
8	4.0000E-02	SIGC		
		4.4000E-02	3	MEASURED 1.00
		3.3000E-02	4	MEASURED 1.00
9	7.5000E-02	SIGC		
		7.3000E-02	3	MEASURED 1.00
		6.4000E-02	4	MEASURED 1.00
10	1.1200E-01	SIGC		
		1.1000E-01	3	MEASURED 1.00
		1.1000E-01	4	MEASURED 1.00
11	1.2300E-01	SIGC		
		1.2000E-01	3	MEASURED 1.00
		1.2000E-01	4	MEASURED 1.00
12	1.3300E-01	SIGC		
		1.3000E-01	3	MEASURED 1.00
		1.2000E-01	4	MEASURED 1.00
13	1.4400E-01	SIGC		
		1.4000E-01	3	MEASURED 1.00
		1.9000E-01	4	MEASURED 1.00
14	1.5300E-01	SIGC		
		1.5000E-01	3	MEASURED 1.00
		2.1000E-01	4	MEASURED 1.00
15	1.6100E-01	SIGC		
		1.6000E-01	3	MEASURED 1.00
		2.3000E-01	4	MEASURED 1.00
16	1.6500E-01	SIGC		
		1.6000E-01	3	MEASURED 1.00
		2.5000E-01	4	MEASURED 1.00
17	1.8200E-01	SIGC		
		2.0200E-01	1	MEASURED 9.00
		1.8000E-01	3	MEASURED 1.00
		2.8000E-01	4	MEASURED 1.00
18	2.2200E-01	SIGC		
		2.9400E-01	1	MEASURED 9.00
		2.2000E-01	3	MEASURED 1.00
		3.5000E-01	4	MEASURED 1.00
19	2.7200E-01	SIGC		
		3.4600E-01	1	MEASURED 9.00
		2.7000E-01	3	MEASURED 1.00
		4.6000E-01	4	MEASURED 1.00
20	2.8800E-01	SIGC		
		3.8200E-01	1	MEASURED 9.00
		2.8000E-01	3	MEASURED 1.00
		4.9000E-01	4	MEASURED 1.00
21	3.1000E-01	SIGC		
		4.2000E-01	1	MEASURED 9.00
		3.0000E-01	3	MEASURED 1.00
		5.2000E-01	4	MEASURED 1.00
22	3.4100E-01	SIGC		
		4.6800E-01	1	MEASURED 9.00
		3.3000E-01	3	MEASURED 1.00
		5.7000E-01	4	MEASURED 1.00

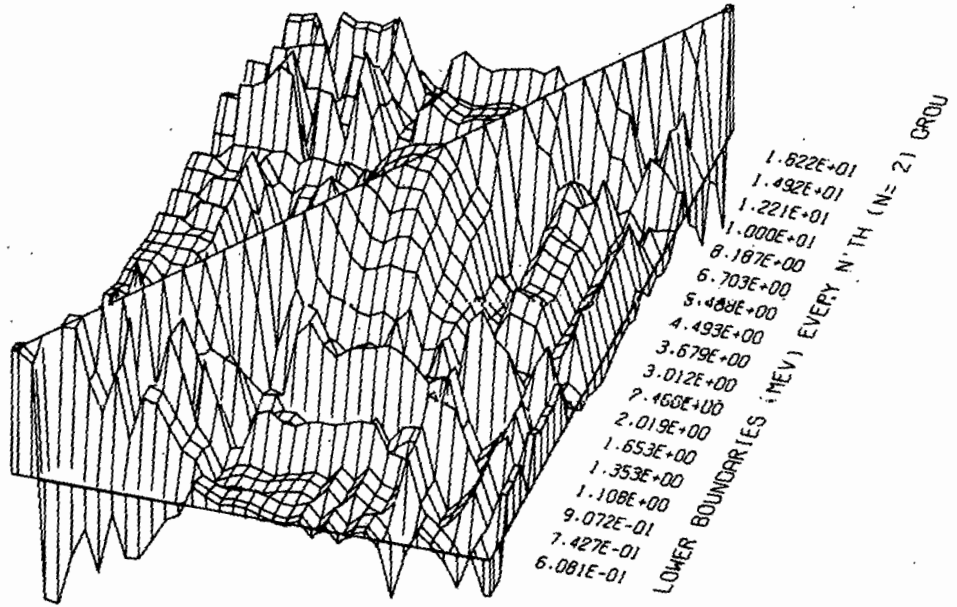
23	3.9000E-01	SIGC	AUTHOR		WEIGHT
		5.8300E-01		1	MEASURED
		3.7000E-01		3	MEASURED
		6.3000E-01		4	MEASURED
24	4.6100E-01	SIGC	AUTHOR		WEIGHT
		5.9200E-01		1	MEASURED
		4.2000E-01		3	MEASURED
		6.7000E-01		4	MEASURED
25	5.8300E-01	SIGC	AUTHOR		WEIGHT
		6.9099E-01		1	MEASURED
		4.7000E-01		3	MEASURED
		7.9999E-01		4	MEASURED
26	7.9500E-01	SIGC	AUTHOR		WEIGHT
		7.8999E-01		1	MEASURED
		3.9599E-01		2	MEASURED
		5.4999E-01		3	MEASURED
		9.4999E-01		4	MEASURED
27	1.0500E 00	SIGC	AUTHOR		WEIGHT
		9.9999E-01		1	MEASURED
		1.1200E 00		2	MEASURED
		7.2999E-01		3	MEASURED
		1.2500E 00		4	MEASURED
28	1.2400E 00	SIGC	AUTHOR		WEIGHT
		1.2800E 00		1	MEASURED
		1.3600E 00		2	MEASURED
		9.1999E-01		3	MEASURED
		1.5000E 00		4	MEASURED
29	1.2900E 00	SIGC	AUTHOR		WEIGHT
		1.3200E 00		1	MEASURED
		1.3600E 00		2	MEASURED
		9.6999E-01		3	MEASURED
		1.6000E 00		4	MEASURED
30	1.3600E 00	SIGC	AUTHOR		WEIGHT
		1.3600E 00		1	MEASURED
		1.3900E 00		2	MEASURED
		1.0300E 00		3	MEASURED
		1.7000E 00		4	MEASURED
31	1.4400E 00	SIGC	AUTHOR		WEIGHT
		1.3800E 00		1	MEASURED
		1.3900E 00		2	MEASURED
		1.1200E 00		3	MEASURED
		1.8000E 00		4	MEASURED
32	1.5500E 00	SIGC	AUTHOR		WEIGHT
		1.5499E 00		1	MEASURED
		1.2100E 00		3	MEASURED
		1.9999E 00		4	MEASURED
33	1.7000E 00	SIGC	AUTHOR		WEIGHT
		1.6700E 00		1	MEASURED
		1.3500E 00		3	MEASURED
		2.2000E 00		4	MEASURED
34	1.6400E 00	SIGC	AUTHOR		WEIGHT
		1.8899E 00		1	MEASURED
		1.5199E 00		3	MEASURED
		3.4999E 00		4	MEASURED
35	2.5400E 00	SIGC	AUTHOR		WEIGHT
		2.4097E 00		1	MEASURED
		1.8498E 00		3	MEASURED
		3.0996E 00		4	MEASURED
36	3.2300E 00	SIGC	AUTHOR		WEIGHT
		3.2184E 00		1	MEASURED
		2.3988E 00		3	MEASURED
		4.3978E 00		4	MEASURED
37	6.4100E 00	SIGC	AUTHOR		WEIGHT
38	6.2100E 00	SIGC	AUTHOR		WEIGHT
39	3.1400E 00	SIGC	AUTHOR		WEIGHT
40	5.1000E 00	SIGC	AUTHOR		WEIGHT
41	6.5900E 00	SIGC	AUTHOR		WEIGHT
42	6.6000E 00	SIGC	AUTHOR		WEIGHT
43	8.1600E 00	SIGC	AUTHOR		WEIGHT
44	7.8600E 00	SIGC	AUTHOR		WEIGHT
45	2.5040E 01	SIGC	AUTHOR		WEIGHT
		8.2543E 00		1	MEASURED
		2.7231E 01		1	MEASURED

VI. THE THREE-DIMENSIONAL CORRELATION MATRIX PLOT

As noted, part of the card output of the program can be used to generate a three-dimensional plot of the correlation matrix. This can be seen in Fig. 1, where this plot is shown for the ^{238}U fission cross section.

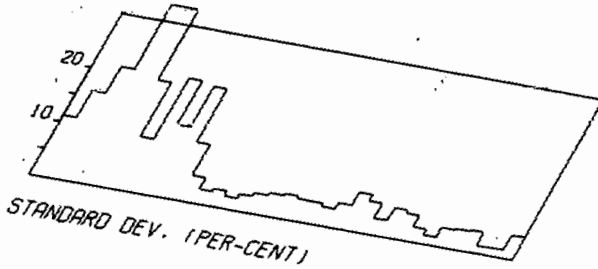
Several conclusions can be deduced from this plot:

- (1) A lot of structure can be seen. This corresponds to the fact that the cross section was analyzed with very much detail.
- (2) The standard deviation shows large uncertainties in the low-energy region. This reflects the lack of data in this region.
- (3) Positive correlation corresponds to differences in magnitude but not in shape; negative correlation corresponds to differences in shape. Then, differences in shape in the low-energy range can be detected. This reflects the fact that in this zone the cross section rises so fast that differences in cross-section values correspond to a large difference in shape.
- (4) The recent measurement of Behrens et al. correlates all the analyzed energy intervals.⁹



ELOW
CORRELATION MATRIX

EHIGH



MAT'L 1262 36 GROUPS REACT 18 TO REACT 18

REFERENCES

1. Greebler, P., et al., "Implications of Nuclear Data Uncertainties to Reactor Design," *Nuclear Data for Reactor*, Proc. Conf., Helsinki, 1970, IAEA, vol. I, 17.
2. Barré, Y., et al., "Roles Respectifs des Evaluations et des Experiences Integrales pour la Physique des Reacteurs Rapides," *Applications of Nuclear Data in Science and Technology*, Symp., Paris, 1973.
3. Usachev, L. N., et al., "Nuclear Data Sources and Their Implications on the Design of Fast Reactors," *Applications of Nuclear Data in Science and Technology*, Symp., Paris, 1973.
4. Hummel, H., et al., FRA-TM-54, ANL (1973).
5. Votinen, V. O., et al., "The Light-Water Industry. Nuclear Data Needs," Conf. on Nuclear Cross Sections and Technology, Washington, D.C., March 1975.
6. Minutes of the spring and fall 1973 meeting of the cross-section evaluation group and F. G. Perey. "Format and procedures for ENDF/B data covariance files."

7. Perey, F. G., et al., "Estimated Data Covariance Files of Evaluated Cross Section - Examples for U-235 and U-238," paper presented at ANS meeting, Atlanta, September 1974.
8. Perey, F. G., "Estimated Uncertainties in Nuclear Data. An Approach," Conf. on Nuclear Cross Sections and Technology, Washington, D.C., March 1975.
9. Behrens, J. W., et al., *Conf. of Nuclear Cross Sections and Technology*, paper GB-14, Washington, D.C., March 1975.

APPENDIX A. LIST OF REFERENCES USED IN THE CALCULATION
OF THE COVARIANCE MATRICES

^{238}U Fission: In this case the covariance [COV(I,J)] was calculated for 36 groups from 20 MeV to 550.24 keV in a 0.1 lethergy unit interval. The following set of references was used:

1. Nyer, W., Report LA-719 (1948).
One measurement at 14 MeV. Original data.
2. Uttley, C. A., et al., Report AERE NP/R 1996 (1956).
Two measurements at 14.1 and 15 MeV. Original data.
3. Smith, R. K., et al., *Bull. Am. Phys. Soc.* 2: 196 (1957).
Thirty seven measurements at 1-20 MeV. Results from Sowerby, M. G., et al., Report AERE-R7273 (1973).
4. Billand, P., et al., *Geneva Conf.* 16: 106 (1958).
One measurement at 13.6 MeV. Original data.
5. Flerov, N. N., et al., *J. Nucl. Energy* 11: 173 (1959).
One measurement at 14.6 MeV. Original data.
6. Mangialajo, M., et al., *Nucl. Phys.* 43: 124 (1963).
Eight measurements at 13.74-14.75 MeV. Original data.
7. Barral, R. C., et al., Report AFWL-TR-68-134 (1969).
One measurement at 14.6 MeV. Original data.
8. Henkel, R. L., et al., Report LA-1495 (1952) and Report LA-2122 (1957).
Thirty eight measurements at 1.3-6.92 MeV. Data renormalized to 0.5176b at 4.50 MeV.

9. Sailor, V. L., Report WASH-745, p. 31 (1958).
Four measurements at 8.8-13.86 MeV. Renormalized to 1.109 b at 13.86 MeV.
10. Adams, B., et al., *J. Nucl. Energy* 14: 85 (1961).
Fourteen measurements at 12.7-19.4 MeV. Renormalized to 1.125 b at 14 MeV.
11. Pankratov, V. M., et al., *J. Nucl. Energy* 16: 494 (1962).
Fifteen measurements at 10.6-20.4 MeV. Renormalized to 1.125 b at 14 MeV.
12. Pankratov, V. M., *At. Energ.* 14: 167 (1963).
Thirty six measurements at 5.1-22.5 MeV. Renormalized to 1.125 b at 14 MeV.
13. Emma, V., et al., *Nucl. Phys.* 63: 641 (1965).

The following are ratio measurements relative to the ^{235}U fission cross section. They were reduced to ^{238}U fission data utilizing the ^{235}U fission cross-section ENDF/B-IV evaluation.

14. Nyer, W., Report LA-938 (1950).
One measurement at 14 MeV.
15. Jarvis, G. A., et al., Report LA-1571 (1953).
One measurement at 2.5 MeV.
16. Lamphere, R. W., *Phys. Rev.* 104: 1654 (1956).
Eighty eight measurements at 0.573-2.995 MeV, measurement multiplied by 0.95.

17. Uttley, C. A., et al., Report AERE NP/R 1996 (1956).
One measurement at 14.1 MeV.
18. Kalinin, S. P., et al., *Geneva Conf.* 16: 136 (1958).
Twenty measurements at 2.95-8.30 MeV.
19. Berezin, A. A., et al., *J. Nucl. Energy* 11: 175 (1960).
One measurement at 14.6 MeV.
20. Smirenkin, G. N., et al., *At. Energ.* 13: 974 (1962).
One measurement at 2.5 MeV.
21. Stein, W. E., et al., p. 627 in *Proc. Conf. Neutron Cross Sections and Technology*, vol. I, Washington, D.C., 1968.
Fourteen measurements at 1.5-5 MeV.
22. White, P. H., et al., *J. Nucl. Energy* 21: 671 (1967).
Three measurements at 2.25-14.1 MeV.
23. Grundl, J. A., *Nucl. Sci. Eng.* 30: 39 (1967).
Sixteen measurements at 1.68-8.07 MeV.
24. Poenitz, W. P., et al., *J. Nucl. Energy* 26: 483 (1972).
Three measurements at 2-3 MeV.
25. Meadows, J. W., *Nucl. Sci. Eng.* 49: 310 (1972).
Twenty one measurements at 0.898-5.33 MeV.
26. Behrens, J. W., et al., *Conf. of Nuclear Cross Sections and Technology*, paper GB-14, Washington, D.C., March 1975.
White source, 30.23-0.1077 MeV.

^{238}U Capture. In this case the covariance [COV(I,J)] was calculated for 91 groups for energies ranging from 10 MeV to 100 eV. From 10 MeV down to 4.095 keV, 0.1 lethargy unit intervals were used. The energy range

between 4.095 keV and 100 eV was divided in decimal intervals. The following set of references was used:

1. Rose, B., Report AERE NP/R 1743 (1955). See also *J. Nucl. Energy* 8: 197 (1959).
Eleven measurements at 29-840 keV. Original data.
2. Broda, E., et al., Report BR-754. Reported by Rose in ref. 1.
Seven measurements at 400 keV-4.05 MeV. Data revised by Davey in ref. 19.
3. English and Gueron, National Research Council of Canada, Montreal Laboratory Report MC-69. Reported by Rose in ref. 1.
Two measurements at 220-850 keV. Original data.
4. Macklin, R. L., et al., *Phys. Rev.* 107: 504 (1957).
One measurement at 25 keV. Original data.
5. Lyon, W. S., et al., *Phys. Rev.* 114: 1619 (1959).
One measurement at 195 keV. Original data.
6. Bilpuch, E. G., *Ann. Phys.* 10: 455 (1960).
Thirteen measurements at 2.55-217 keV. Data revised by Davey in ref. 19.
7. Given, B. G., et al., *Phys. Rev.* 120: 556 (1960).
Seven measurements at 0.175-1 MeV. Data revised by Davey in ref. 19.
8. Gibbons, J. H., et al., *Phys. Rev.* 122: 182 (1961).
Two measurements at 30-65 keV. Original data.

9. Bergginst, I., *Ark. Fys.* 23: 425 (1963).
Eight measurements at 18-300 keV. Data revised by Davey in ref. 19.
10. de Saussure, G., et al., Report ORNL-3360 (1963).
Two measurements at 30-64 keV. Data revised by Davey in ref. 19.
11. Macklin, R. L., et al., Report WASH-1046, p. 88 (1963).
Sixteen measurements at 8.8-54.7 keV. Data according to a recent evaluation of σ (Ta) in ref. 19.
12. Tolstikov, V. A., et al., *J. Nucl. Energy* 18: 599 (1964).
Eleven measurements at 15-180 keV. Corrected by non- $1/v$ ^{10}B behavior and normalized to the Belanova (ref. 13) value. Data from Sowerby (ref. 20).
13. Belanova, T. A., et al., *J. Nucl. Energy* 20: 411 (1966).
One measurement at 22.8 keV as corrected by Miller et al. in *Nucl. Sci. Eng.* 35: 295 (1969).
14. Menlove, H. O., et al., *Nucl. Sci. Eng.* 33: 24 (1968).
Nine measurements at 24-503 keV. Original data.
15. Moxon, M. C., Report AERE-R6074 (1969).
White source, time of flight; 0.50-100 keV. Results average in decimal intervals. Date revised in 1970 (ref. 20).
16. Fricke, M. P., et al., IAEA Conf., Helsinki (1970).
White source, time of flight; 1-100 keV. Results average in decimal intervals, 100-752 keV point results. Original data.
17. de Saussure, G., et al., *Nucl. Sci. Eng.* 51: 385 (1973).
White source, time of flight; 0.100-100 keV. Results average over decimal intervals. Original data.

18. Langner, I., et al., Report KFK-880 (1968).
Evaluation.
19. Davey, W. G., *Nucl. Sci. Eng.* 39: 337 (1970).
Evaluation.
20. Sowerby, M. G., et al., Report AERE-R7273 (1973).
Evaluation.
21. Ponitkin, Y. G., et al., Report IAEA-CN-26, Helsinki (1970).
Ten measurements at 24-145 keV. Original data.
22. Ponitkin, Y. G., et al., *At. Energ.* 33: 782 (1972).
Two measurements at 132-160 keV. Original data.
23. Block, R. C., et al., Conf-720901, vol. II, p. 1107 (1972).
One measurement at 24 keV. Original data.
24. Chelnokov, V. B., et al., "Neutron cross section for radioactive capture," preprint USSR Institute of Physics and Power Engineering (1973).
Ten measurements at 3.3-35 keV. Original data.
25. Ryves, T. B., et al., *J. Nucl. Energy* 27: 519 (1973).
Four measurements at 157-624 keV. Original data.
26. Pearlstein, S., et al., UKAEA Progress Report (1973).
Eleven measurements at 200-1750 keV. Original data.
27. Spencer, R. R., et al., private communication, 1975.

The following are ratio measurements relative to the ^{235}U fission cross section. They were reduced to ^{238}U capture data utilizing the ^{235}U fission cross-section ENDF/B-IV evaluation.

28. Linenberg, G. A., et al., Report LA-467 (1946).
Thirteen measurements at 0.005-5.9 MeV. Original data.
29. Barry, J. F., et al., *J. Nucl. Energy* 18: 481 (1964).
Thirteen measurements at 0.127-7.6 MeV. Original data.
30. Weston, L. W., et al., Report EANDC 330, p. 64 (1963).
See also ref. 10.
Two measurements at 30-64 keV. Original data.
31. Poenitz, W. P., *Nucl. Sci. Eng.* 49: 383 (1970) and *Trans. Am. Nucl. Soc.* 12: 279 (1968).
Thirteen measurements at 30 keV-1.4 MeV. Original data.
32. Sowerby, M. G., et al., Report AERE-R7273 (1973).
Evaluation.

^{239}Pu Capture: In this case the covariance [COV(I,J)] was calculated for 36 groups for energies ranging from 1 MeV to 100 eV. The energy range was divided in decimal intervals. The following set of references was used:

1. Sowerby, M. G., et al., *At. Energy Rev.* 10(4): 453 (1972).
IAEA.
2. Gwin, R., et al., *Nucl. Sci. Eng.* 45: 25 (1971).
3. Schomberg, M. G., et al., p. 315 in *Proc. Conf. Nuclear Data for Reactors*, vol. I, IAEA, Helsinki, 1970.
4. Czirr, J. R., et al., p. 331 in *Proc. Conf. Nuclear Data for Reactors*, vol. I, IAEA, Helsinki, 1970.

5. Belyaer, F. N., et al., p. 336 in *Proc. Conf. Nuclear Data for Reactors*, vol. I, IAEA, Helsinki, 1970.
6. Farrell, J. A., et al., p. 543 in *Proc. Conf. Nuclear Data for Reactors*, vol. I, IAEA, Helsinki, 1970.
7. Kononov, V. N., et al., p. 345 in *Proc. Conf. Nuclear Data for Reactors*, vol. I, IAEA, Helsinki, 1970.
8. Ryabov, Yu. V., et al., p. 345 in *Proc. Conf. Nuclear Data for Reactors*, vol. I, IAEA, Helsinki, 1970.
9. Weston, L. W., et al., memorandum to R. E. Chrien, 1972.
10. Gwin, R., et al., to be published in *Nuclear Science Engineering*.

^{239}Pu Fission: In this case the covariance [COV(I,J)] was calculated for 45 groups for energies ranging from 10 MeV to 100 eV. The energy range was divided in decimal intervals. The following set of references was used:

1. Sowerby, M. G., et al., Report AERE-R-7273, UKAEA (1973).
2. Hunter, R. E., et al., Report LA-5172 (1973).
3. Gwin, R., to be published in *Nuclear Science Engineering*.
4. Weston, L. W., memorandum to R. E. Chrien, 1972.
5. James, G. D., p. 267 in *Proc. Conf. Nuclear Data for Reactors*, vol. I, IAEA, Helsinki, 1970.
6. Gwin, R., et al., *Nucl. Sci. Eng.* 45: 25 (1971).
7. Shunk, E. R., et al., p. 979 in *Proc. Conf. Neutron Cross Section Technology*, vol. II, CONF-660303, 1966.
8. Blons, J., *Nucl. Sci. Eng.* 51: 95 (1973).

9. Schomberg, M. G., et al., p. 315 in *Proc. Conf. Nuclear Data for Reactors*, vol. I, IAEA, Helsinki, 1970.

^{240}Pu and ^{241}Pu Capture. ^{241}Pu Fission: In this case the covariance was calculated for 45 groups for energies ranging from 10 MeV to 100 eV. The following sets of references were used:

^{240}Pu Capture Cross Section

1. Weston, L. W., and Todd, J. H., "Measurement of the Neutron Capture Cross Sections of the Actinides," Proceedings of the Conference on Nuclear Cross Sections and Technology, Washington, D.C., 1975, to be published.
100 eV to 300 keV with weight of 9 on the variance.
2. Hockenbury, R. W., Moyer, W. R., and Block, R. C., *Nucl. Sci. Eng.* 49: 153-161 (1972).
6 to 30 keV with weight of 9 on the variance.
3. Prince, A., *Conf. Nucl. Data for Reactors*, CN-26/91, Helsinki, 1970.
1 keV to 10 MeV with weight of 1 on the variance (model calculation).
4. Yiftah, S., Schmidt, J. J., Caner, M., and Segev, M., p. 123 in *Fast Reactor Physics*, vol. I, IAEA, Vienna, 1968.
1 keV to 10 MeV with weight of 1 on the variance (model calculation).

^{241}Pu Capture Cross Section

1. Weston, L. W., and Todd, J. H., "Neutron Fission and Absorption Cross Sections for ^{239}Pu and ^{241}Pu ," *Trans. Am. Nucl. Soc.* 15(1): 480 (1972).
100 eV to 200 keV with weight of 9 on the variance.
2. Caner, M., and Yiftah, S., p. 735 in *Conf. Nucl. Data for Reactors*, vol. II, IAEA, Vienna, 1970.
100 eV to 10 MeV with weight of 1 on the variance (model calculation).
3. Prince, A., *Conf. Nucl. Data for Reactors*, CN-26/91, Helsinki, 1970.
80 keV to 10 MeV with weight of 1 on the variance (model calculation).

 ^{241}Pu Fission Cross Section (all references with weight of 1 on the variance)

1. Weston, L. W., and Todd, J. H., same reference as with ^{241}Pu capture.
100 eV to 200 keV.
2. Simpson, O. D., et al., p. 910 in *Proc. Conf. on Neutron Cross Section and Technology*, vol. II, Washington, D.C., 1966.
100 eV to 10 keV.
3. Blons, J., et al., p. 469 in *Conf. Nucl. Data for Reactors*, vol. I, Vienna, 1970.
4. Migneco, E., Theohald, J. P., and Wartena, J. A., p. 437 in *Conf. Nuclear Data for Reactors*, vol. I, Vienna, 1970.
100 eV to 2 keV.

5. Smith, H. L., Smith, R. K., and Henkel, R. L., *Phys. Rev.* 125: 1329 (1962).
200 keV to 10 MeV.
6. Zabo, I., et al., *Neutron Standards and Flux Normalization*, p. 256, Argonne National Laboratory (1970).
20 keV to 1 MeV.
7. White, P. H., and Warner, G. P., *J. Nucl. Energy* 21: 671 (1967).
40 keV to 6 MeV.
8. Butler, D. K., and Sjoblom, R. L., *Phys. Rev.* 124: 1129 (1961).
300 keV to 2 MeV.

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APPENDIX B. STANDARD DEVIATION AND CORRELATION MATRICES
CORRESPONDING TO DIFFERENT CROSS SECTIONS

U238 FISSION 36 GROUPS

I	ELO(KEV)	RSD PCT	CORR*100																																			
			1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28								
1	550.24	11.1	100	91	-95	-97	-57	-33	-66	-17	-51	-49	-32	-14	-8	15	10	4	6	6	3	0	0	3	-7	3	-8	1	4	-6								
2	608.11	16.0	91	100	-99	-97	-58	-35	-68	-17	-49	-32	-18	-11	11	5	3	4	6	3	0	0	3	-7	3	-7	1	4	-5									
3	672.06	21.0	-95	-99	100	-99	-59	-35	-69	-17	-53	-50	-33	17	11	-12	-7	-3	-5	-6	-3	0	0	-3	7	-3	8	-1	-4	6								
4	742.74	34.1	-97	-97	99	100	-59	-35	-69	18	53	50	33	16	10	-13	-8	-4	-6	-6	-3	0	0	-3	7	-3	8	-1	-4	6								
5	820.86	31.6	-57	-58	59	100	30	94	8	44	86	59	18	4	-15	-8	-6	-8	-12	-7	-6	-2	-6	5	-4	9	-1	-5	6									
6	907.19	19.8	-33	-35	35	100	36	-39	28	26	-11	58	29	-6	-3	24	30	22	20	26	28	27	30	34	13	11	6	6	6									
7	1002.60	9.8	-66	-68	69	100	36	-39	28	26	-11	58	29	-6	-3	24	30	22	20	26	28	27	30	34	13	11	6	6	6									
8	1108.04	21.0	-17	-17	17	18	8	-39	17	100	27	7	44	-50	-21	-36	-23	-46	-54	-44	-35	-29	-35	-39	-30	-41	-28	-33	-15	0								
9	1224.57	12.9	-51	-53	53	53	44	28	63	27	100	63	39	33	29	-14	-18	-8	-8	-14	-20	-16	-13	-19	-1	-27	-13	-6	-5	7								
10	1353.36	20.4	-49	-49	50	50	86	26	81	7	63	100	67	26	12	-15	-16	-10	-10	-19	-20	-20	-14	-17	-3	-20	-7	-4	-5	6								
11	1495.69	10.5	-32	-32	33	33	59	-11	54	44	39	67	100	-14	-1	-10	-8	-29	-35	-38	-38	-40	-34	-39	-20	-44	-23	-16	-15	4								
12	1663.00	4.7	-14	-18	17	16	18	58	22	-50	33	26	-14	100	52	-15	-18	30	43	27	18	27	31	32	36	31	23	11	18	7								
13	1826.84	2.6	-8	-11	11	10	4	29	10	-21	29	12	-1	52	100	6	42	47	43	21	3	20	24	21	47	6	5	6	7	3								
14	2018.97	3.1	15	11	-12	-13	-15	-6	-16	-36	-14	-15	-10	-15	6	100	47	24	13	10	1	-8	-2	-7	-2	-11	-2	26	-10	-2								
15	2231.31	2.2	10	5	-7	-8	-8	-3	-9	-23	-18	-16	-8	-18	42	47	100	50	36	33	27	25	30	24	36	5	8	20	-5	-1								
16	2465.97	3.1	4	3	-3	-4	-6	24	-5	-46	-8	-10	-29	30	47	24	50	100	80	59	50	53	58	56	56	27	21	21	6	1								
17	2725.32	3.6	6	4	-5	-6	-8	30	-8	-54	-8	-10	-35	43	43	13	36	80	100	81	68	64	71	73	63	34	25	18	6	-2								
18	3011.94	4.2	6	6	-6	-6	-12	22	-10	-44	-14	-19	-38	27	21	10	33	59	81	100	92	78	84	86	67	38	29	16	0	-6								
19	3328.71	4.4	3	3	-3	-3	-7	20	-6	-35	-20	-20	-38	18	3	1	27	50	68	92	100	89	91	91	67	46	36	13	-1	-6								
20	3678.79	4.0	0	0	0	0	-6	26	-3	-29	-16	-20	-40	27	20	-8	25	53	64	78	89	100	97	95	82	60	45	2	-6	-13								
21	4065.70	4.0	0	0	0	0	-2	28	0	-35	-13	-14	-34	31	24	-2	30	58	71	84	91	97	100	97	86	58	45	3	-11	-16								
22	4493.29	3.4	3	3	-3	-3	-6	27	-5	-39	-19	-17	-39	32	21	-7	24	56	73	86	91	96	97	100	83	60	44	2	-7	-15								
23	4968.85	4.8	-7	-7	7	7	5	30	8	-30	-1	-3	-20	36	47	-2	36	56	63	67	67	82	86	83	100	60	46	-10	-26	-27								
24	5488.12	6.9	3	3	-3	-3	-4	34	-4	-41	-27	-20	-44	31	6	-11	5	27	34	38	46	60	58	60	60	100	75	-15	-35	-44								
25	6065.30	5.7	-8	-7	8	8	9	34	10	-28	-13	-7	-23	23	5	-2	8	21	25	29	36	45	45	44	46	75	100	22	-15	-17								
26	6703.20	3.0	1	1	-1	-1	1	13	-1	-33	-6	-4	-16	11	6	26	20	21	18	16	13	2	3	2	-10	-15	22	100	70	63								
27	7408.18	5.3	4	4	-4	-4	-5	11	-6	-15	-5	-5	-15	18	7	-10	-5	6	6	0	-1	-6	-11	-7	-26	-35	-15	70	100	91								
28	8187.31	4.8	-6	-5	6	6	6	6	6	0	7	6	4	7	3	-2	-1	1	-2	-6	-6	-13	-16	-15	-27	-44	-17	63	81	100								
29	9048.38	2.6	-44	-43	44	45	50	65	59	-24	52	49	12	66	34	-14	-10	19	23	17	17	24	27	23	33	30	46	23	13	9								
30	10000.00	1.6	-8	-8	8	8	9	61	11	-67	10	9	-32	77	38	-2	-2	37	47	37	32	39	41	42	40	51	56	46	33	17								
31	1081.71	3.4	12	12	-12	-12	-14	57	-16	-65	-14	-13	-44	56	26	4	2	33	42	34	29	32	33	37	30	46	38	21	20	3								
32	12214.03	3.7	3	3	-3	-3	-4	30	-4	-46	-4	-4	-31	47	24	1	1	29	37	29	25	29	30	32	24	30	44	52	31	4								
33	13498.59	3.9	-7	-7	7	7	9	8	10	-1	9	8	5	11	7	-2	-4	3	6	4	3	3	4	4	8	3	7	5	2	0								
34	14918.25	1.4	-27	-26	26	27	30	33	35	-10	31	30	13	40	21	-8	-7	10	11	8	9	13	15	12	23	15	0	-22	-12	-7								
35	16487.21	1.5	-1	-1	1	1	1	43	-1	-59	-1	-1	-35	58	28	0	0	31	39	31	27	31	33	35	33	41	19	3	9	-3								
36	18221.17	4.2	-28	-28	28	29	32	3	38	32	33	32	39	0	1	-9	-8	-12	-16	-14	-10	-8	-7	-12	0	-14	-7	-15	-13	0								
37	19980.00																																					

I	ELO(KEV)	RSD PCT	CORR*100							
			29	30	31	32	33	34	35	36
29	9048.38	2.6	100	70	40	38	13	44	37	21
30	10000.00	1.6	70	100	69	66	10	22	58	-14
31	1081.71	3.4	40	69	100	39	2	1	51	-25
32	12214.03	3.7	38	66	39	100	10	20	54	-50
33	13498.59	3.9	13	10	2	10	100	17	14	-7
34	14918.25	1.4	44	22	1	20	17	100	71	-20
35	16487.21	1.5	37	58	51	54	14	71	100	-65
36	18221.17	4.2	21	-14	-25	-50	-7	-20	-65	100
37	19980.00									

35	5488.11	47.0	10	8	3	8	11	5	8	10	1	8	31	8	35	18	20	21	30	33	35	35	33	31	27	19	28	30	30	41	
36	6065.30	72.5	21	16	10	15	20	15	13	14	0	9	38	10	42	20	18	19	30	36	35	35	34	33	31	22	33	35	35	46	
37	6703.20	90.9	20	15	10	15	20	15	12	14	-1	9	37	10	40	19	16	18	20	29	35	34	34	33	32	31	22	32	34	46	
88	7408.18	91.8	21	17	10	15	20	15	13	14	0	10	40	10	42	21	19	20	31	36	36	37	35	34	33	23	34	36	36	48	
89	8187.30	122.0	21	16	10	14	19	15	12	13	1	10	40	10	40	20	19	19	30	34	21	21	21	21	22	18	25	26	26	34	
90	9048.37	137.2	21	17	10	15	19	15	13	14	2	11	42	10	41	21	20	20	31	35	21	22	22	22	23	18	26	27	26	35	
9110000.00	127.8		24	21	11	16	18	15	14	14	6	12	50	11	45	26	27	25	35	37	23	24	23	24	25	19	27	28	27	36	
9211052.00																															

I	ELD(KEV)	RSD PCT	CORR*100																																	
			57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84						
57	333.74	15.6	100	93	53	52	90	74	75	74	87	63	50	61	72	75	61	49	48	35	31	30	28	23	27	28	33	31	30	29						
58	368.84	14.7	53	100	50	48	88	75	74	72	83	59	48	57	68	71	58	46	45	32	22	24	21	21	22	21	30	29	27	27						
59	407.63	14.7	53	50	100	98	56	65	60	59	54	58	79	87	76	72	73	63	77	38	29	31	29	30	26	26	35	35	33	42						
60	450.50	14.4	52	48	98	100	54	63	57	56	51	56	77	36	75	71	72	61	75	38	28	30	29	30	26	26	34	35	33	41						
61	497.88	12.9	90	88	56	54	100	75	78	74	84	59	45	63	77	80	66	53	50	37	32	32	29	24	26	28	33	33	30	30						
62	550.24	15.1	74	75	65	63	75	100	92	93	82	76	63	58	73	75	57	41	50	28	17	20	18	22	18	16	26	26	24	30						
63	608.11	19.5	75	74	60	57	78	92	100	93	87	75	62	55	70	72	54	41	46	25	20	21	19	20	17	17	23	23	22	27						
64	672.06	20.5	74	72	59	56	74	93	93	100	88	82	63	54	69	71	52	38	44	24	19	20	19	20	17	17	22	22	21	26						
65	742.74	19.5	67	83	54	51	84	82	87	88	100	75	60	59	72	75	58	46	45	32	27	27	25	23	24	25	29	29	27	28						
66	820.66	24.9	63	59	58	56	59	76	75	82	75	100	65	52	63	67	50	39	42	21	15	16	15	16	14	14	19	19	18	23						
67	907.19	24.0	50	48	79	77	45	63	62	63	60	65	100	71	63	61	59	60	63	32	23	24	23	24	22	22	28	28	27	34						
68	1002.60	27.7	61	57	87	86	63	58	55	54	59	52	71	100	87	83	83	77	76	55	48	47	43	36	39	42	50	48	45	45						
69	1108.04	26.4	72	68	76	75	77	73	70	69	72	63	63	87	100	94	82	66	65	48	42	42	37	32	34	37	43	42	40	43						
70	1224.67	29.8	75	71	72	71	80	75	72	71	75	67	61	83	94	100	81	67	62	46	40	40	35	29	32	34	41	40	37	37						
71	1353.36	26.3	61	58	73	72	66	57	54	52	58	50	59	83	32	81	100	86	78	57	51	51	46	39	42	45	53	52	48	48						
72	1495.69	18.9	49	46	63	61	53	41	41	38	46	39	60	77	66	67	86	100	83	69	64	65	60	52	56	59	67	64	61	59						
73	1653.00	12.8	48	45	77	75	50	50	46	44	45	42	63	76	65	62	78	83	100	77	69	72	72	73	71	71	78	75	74	79						
74	1826.84	12.8	35	32	38	38	37	28	25	24	32	21	32	55	48	46	57	69	77	100	86	88	87	86	88	87	92	98	97	94						
75	2018.97	17.5	31	22	29	28	32	17	20	19	27	15	23	48	42	40	51	64	69	86	100	99	97	86	90	96	90	86	85	80						
76	2231.31	22.0	30	24	31	30	32	20	21	20	27	16	24	47	42	40	51	65	72	88	99	100	98	89	91	95	93	89	87	83						
77	2465.97	24.3	28	21	29	29	29	18	19	19	25	15	23	43	37	35	46	60	72	87	97	98	100	93	96	99	94	89	89	86						
78	2725.32	26.4	23	21	30	30	24	22	20	20	23	16	24	36	32	29	39	52	73	86	86	89	93	100	97	94	96	90	91	92						
79	3011.94	33.0	27	22	26	26	26	18	17	17	24	14	22	39	34	32	42	56	71	88	90	91	96	97	100	98	97	90	92	89						
80	3328.71	42.0	28	21	26	26	28	16	17	17	25	14	22	42	37	34	45	59	71	87	95	95	99	94	98	100	95	89	90	86						
81	3676.79	49.5	33	30	35	34	33	26	23	22	29	19	28	50	43	41	53	67	78	92	90	93	94	96	97	95	100	93	93	90						
82	4065.76	58.4	31	29	35	35	33	26	23	22	29	19	28	48	42	40	52	64	75	98	85	89	89	90	90	90	89	93	100	99	96					
83	4493.29	56.0	30	27	33	33	30	24	22	21	27	18	27	45	40	37	48	61	74	97	85	87	89	91	92	90	93	99	100	97						
84	4965.65	50.6	29	27	42	41	30	30	27	26	28	23	34	45	40	37	48	59	79	94	80	83	86	92	89	86	90	96	97	100						
85	5488.11	47.0	39	36	52	51	41	36	32	31	37	29	44	62	54	51	64	73	86	97	81	83	83	84	85	84	89	96	95	95						
86	6065.30	72.5	45	43	70	69	51	47	44	41	43	38	56	75	65	63	77	79	79	66	54	56	48	41	39	43	54	60	55	58						
87	6703.20	90.9	44	43	69	68	50	47	43	41	42	37	56	73	64	62	76	78	78	66	54	56	48	41	39	42	53	60	55	57						
88	7408.18	91.8	46	45	71	69	51	47	44	41	43	38	57	76	66	64	78	80	80	67	54	56	48	41	40	44	54	61	56	58						
89	8187.30	122.0	33	33	67	66	38	44	41	39	34	37	55	57	50	47	58	56	67	42	31	34	29	30	24	25	34	39	36	45						
90	9048.37	137.2	34	34	68	67	39	45	41	39	34	37	56	58	50	48	59	56	67	42	30	32	29	29	24	25	33	39	36	45						
9110000.00	127.8		35	34	67	67	38	43	40	38	35	38	58	59	51	48	57	53	65	37	23	23	23	25	23	23	29	33	32	40						
9211052.00																																				

I	ELD(KEV)	RSD PCT	CORR*100						
			85	86	87	88	89	90	91
85	5488.11	47.0	100	72	72	74	53	54	52
86	6065.30	72.5	72	100	69	99	78	77	67
87	6703.20	90.9	72	99	100	99	78	77	66
88	7408.18	91.8	74	99	99	100	77	77	69
89	8187.30	122.0	53	78	78	77	100	99	90
90	9048.37	137.2	54	77	77	77	99	100	93
9110000.00	127.8		52	67	66	69	90	93	100
9211052.00									

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I	E.O.(KEV)	RSD PCT	CORR*100																												
			1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	
1	0.10	6.2	100	86	98	30	54	15	63	-7	-59	-25	-5	-46	20	-1	-53	33	1	-37	-34	-3	-8	9	-7	1	-12	12	10	-13	
2	0.20	5.3	86	100	87	-4	24	-11	19	-36	-77	-50	-38	-70	6	25	-43	58	20	-30	-46	-19	-6	-6	7	9	-1	-2	-4	3	
3	0.30	7.5	58	87	100	35	57	22	59	-2	-60	-19	-1	-40	30	11	-43	42	11	-24	-33	-8	5	-3	3	-9	8	6	-9		
4	0.40	3.4	30	-4	35	100	89	84	68	85	12	78	84	67	82	-2	21	7	-30	24	12	21	14	26	-28	-27	-3	16	22	-22	
5	0.50	4.1	54	24	57	89	100	70	63	70	-27	61	72	40	83	2	8	22	-8	-22	3	9	22	14	17	-19	-22	2	8	13	-4
6	0.60	6.3	15	-11	22	84	70	100	52	88	7	82	87	71	67	-17	7	-8	-22	-12	1	1	9	8	-9	-12	3	2	5	-4	
7	0.70	4.4	63	19	59	68	52	100	39	13	25	44	17	29	-33	-37	-22	-47	-14	13	8	14	10	-13	-18	-16	24	27	-30		
8	0.80	6.6	-7	-36	-2	85	70	68	39	100	17	97	98	88	69	-24	21	-16	-47	14	13	8	14	10	-13	-18	5	2	7	-5	
9	0.90	4.3	-59	-77	-60	12	-27	7	13	17	100	26	17	51	-10	-10	36	-46	17	45	33	20	1	26	-26	-16	-13	22	25	-27	
10	1.00	7.9	-25	-50	-19	78	61	82	25	97	26	100	95	94	70	-15	38	-20	-44	25	26	14	18	9	-12	-20	9	0	4	-2	
11	2.00	8.6	-5	-38	-1	84	72	67	44	98	17	95	100	88	65	-30	17	-22	-50	10	18	14	14	9	-12	-17	6	1	6	-4	
12	3.00	6.0	-46	-70	-40	67	40	71	17	88	51	94	88	100	52	-15	46	-24	-31	40	31	17	18	10	-13	-21	9	0	5	-3	
13	4.00	5.2	20	6	30	82	83	67	29	69	-10	70	65	52	100	43	54	36	-16	46	23	19	19	13	-16	-23	7	3	8	-6	
14	5.00	8.7	-1	25	11	-2	2	-17	-33	-24	-10	15	-30	-15	43	100	74	72	56	75	20	11	13	-3	1	-9	13	-9	-6	9	
15	6.00	5.0	-53	-43	-43	21	8	7	-37	21	36	38	-17	46	54	70	100	35	12	87	42	26	21	9	-13	-23	12	-1	4	0	
16	7.00	3.8	33	58	42	7	22	-8	-22	-16	-46	-20	-22	-24	36	72	35	100	22	43	-20	-3	8	0	-1	-7	7	-4	-1	3	
17	8.00	6.4	1	20	11	-30	-41	-22	-8	-47	17	-44	-50	-31	-16	56	12	42	100	47	-1	-8	-3	-13	14	11	5	-10	-12	13	
18	9.00	6.6	-37	-30	-24	24	3	12	-18	14	45	25	-10	40	46	75	87	23	47	100	36	20	14	9	-11	-16	6	1	5	-3	
19	10.00	3.7	-34	-46	-33	12	9	1	-1	13	33	26	18	31	23	20	48	-20	-1	36	100	64	21	6	-9	-21	14	-4	0	2	
20	20.00	3.3	-3	-19	-6	21	22	1	19	8	20	14	14	17	19	11	26	-3	-8	20	64	100	47	33	-41	-58	19	7	21	-15	
21	30.00	0.4	-8	-6	-8	14	14	9	0	14	1	18	14	18	19	13	21	8	-3	14	21	47	100	0	-17	-81	81	-46	-22	31	
22	40.00	2.6	-9	-7	-3	26	17	8	27	10	26	9	19	10	13	-3	9	0	-13	5	6	33	0	100	-58	-57	88	97	-80		
23	50.00	2.0	-3	-8	-19	-9	-27	-13	-28	-12	-2	-12	-12	-13	-16	-1	-13	-1	14	-11	-9	-41	-17	-58	100	71	42	-78	-91	73	
24	60.00	0.6	-1	9	3	-27	-2	-12	-15	-18	-16	-20	-17	-21	-23	-9	-23	-7	11	-16	-21	-58	-81	-57	71	100	-33	-12	-37	20	
25	70.00	0.6	-12	-1	-3	2	3	-16	5	-13	9	9	6	9	7	13	12	7	13	2	6	14	19	81	-57	42	-43	100	-89	-74	72
26	80.00	2.4	12	-2	8	16	8	2	22	0	0	0	1	0	3	-9	-1	-4	-10	1	-4	7	-46	88	-78	-12	-89	100	96	-85	
27	90.00	1.6	10	-4	6	22	13	5	27	7	25	4	6	5	8	-6	4	-1	-12	5	0	21	-22	97	-91	-37	-74	96	100	-85	
28	100.00	4.0	-13	3	-9	-22	-12	-4	-30	-5	-27	-2	-4	-3	-6	9	0	3	13	-3	2	-15	31	-80	73	20	72	-85	-85	100	
29	200.00	2.1	-6	-5	-6	11	11	7	0	11	1	14	11	14	15	11	17	6	-2	11	17	38	80	0	-13	-65	65	-37	-18	26	
30	300.00	2.6	-7	-5	-6	11	12	8	0	11	1	15	11	15	15	11	17	7	-3	11	17	39	81	0	-14	-66	66	-38	-18	25	
31	400.00	4.5	-5	-4	-5	9	9	6	0	9	1	11	9	11	12	8	13	5	-2	8	13	30	64	0	-11	-52	52	-30	-14	18	
32	500.00	3.0	-7	-5	-6	11	12	8	0	11	1	15	11	15	15	11	17	7	-3	11	17	39	81	0	-14	-66	66	-38	-18	26	
33	600.00	2.3	-6	-5	-6	11	11	7	0	11	1	14	11	14	15	11	17	6	-2	11	17	38	80	0	-13	-65	65	-37	-18	24	
34	700.00	1.5	-6	-4	-5	10	10	7	0	10	1	13	10	13	14	10	15	6	-2	10	15	35	73	0	-12	-59	59	-34	-16	21	
35	800.00	0.4	-6	-4	-6	10	11	7	0	10	1	13	10	13	14	10	16	6	-2	10	16	35	74	0	-12	-60	60	-34	-17	25	
36	900.00	0.5	-6	-5	-6	11	11	7	0	11	1	14	11	14	15	10	17	6	-2	11	16	37	78	0	-13	-64	64	-36	-18	26	
37	1000.00	2.2	-5	-4	-6	-9	-9	-6	0	-1	-12	-9	-9	-11	-12	-8	-13	-5	-2	-5	-13	-31	-64	0	11	-52	-52	-30	14	-23	
38	2000.00	0.6	-6	-4	-6	10	11	7	0	10	1	13	10	13	14	10	16	6	-2	10	16	35	74	0	-13	-61	61	-35	-17	22	
39	3000.00	0.5	-7	-5	-6	11	12	8	0	11	1	15	11	15	15	11	17	7	-3	11	17	39	81	0	-14	-65	65	-38	-18	26	
40	4000.00	1.0	-4	-3	-4	7	7	4	0	7	1	9	7	9	9	7	10	4	-1	7	10	24	50	0	-8	-41	41	-23	-11	19	
41	5000.00	2.2	3	2	-2	-5	-5	-3	0	-5	0	-6	-5	-6	-6	-4	-7	-3	1	-4	-7	-16	-35	0	6	28	-28	16	8	-7	
42	6000.00	1.5	-5	-4	-5	10	10	6	0	10	1	12	10	12	13	9	14	5	-2	5	14	32	68	0	-11	-56	56	-32	-15	19	
43	7000.00	5.2	-6	-4	-5	10	10	7	0	10	1	13	10	13	13	10	15	6	-2	10	15	34	72	0	-12	-58	58	-33	-16	21	
44	8000.00	4.4	-6	-4	-6	10	11	7	0	11	1	13	10	13	14	10	16	6	-2	10	16	36	75	0	-13	-61	61	-35	-17	22	
45	9000.00	3.0	-7	-5	-6	11	12	7	0	11	1	15	11	14	15	11	17	6	-2	11	17	38	81	0	-14	-66	66	-37	-18	25	
46	10000.00																														

I	E.O.(KEV)	RSD PCT	CORR*100																
			29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45
29	200.00	2.1	100	97	66	98	93	80	97	99	-88	82	78	75	-26	73	78	83	95
30	300.00	2.6	97	100	80	99	98	91	89	95	-77	92	99	59	-46	86	90	93	96
31	400.00	4.5	66	80	100	76	88	97	46	59	-24	96	78	0	-89	99	98	96	85
32	500.00	3.0	58	99	76	100	97	88	92	97	-81	90	99	64	-40	82	87	91	98
33	600.00	2.3	53	98	88	97	100	96	82	89	-66	97	98	46	-59	92	95	97	99
34	700.00	1.5	80	91	97	88	96	100	64	75	-44	99	89	21	-78	99	99	99	94
35	800.00	0.4	57	89	46	92	82	64	100	98	-97	67	91	88	-2	55	61	68	85
36	900.00	0.5	59	95	59	97	89	75	98	100	-92	77	96	80	-17	67	73	78	92
37	1000.00	2.2	-88	-77	-24	-81	-66	-44	-97	-92	100	-48	-79	-96	-20	-34	-41	-49	-71
38	2000.00	0.6	82	92	96	90	97	59	67	77	-48	100	91	25	-75	98	99	99	95
39	3000.00	0.5	58	99	78	99	98	89	91	96	-79	91	100	61	-43	84	88	92	95
40	4000.00	1.0	75	59	0	64	46	21	88	80	-96	25	61	100	43	9	18	27	52
41	5000.00	2.2	-26	-46	-89														

PU 239 CAPTURE 36 GROUPS

I	ELO(KEV)	RSD PCT	CORR*100																												
			1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	
1	0.10	9.2	100	51	-21	-24	45	-21	-10	28	-10	-42	-30	-31	31	-10	-36	33	-44	0	6	-29	12	36	31	24	23	17	13	-37	
2	0.20	11.5	51	100	30	-5	73	-29	20	52	19	-11	-9	-7	47	19	19	13	-52	-49	10	-38	13	23	18	18	13	15	13	-22	
3	0.30	11.3	-21	30	100	-11	-10	26	25	-16	-11	-8	-3	30	-24	-37	27	-24	23	-17	-24	2	-5	-20	-21	-20	-19	-16	-3	20	
4	0.40	22.6	-24	-5	-11	100	33	5	87	41	87	53	29	52	-32	-9	-12	-22	2	-40	12	26	5	4	-1	-2	-4	-3	7	-3	
5	0.50	7.2	45	73	-10	33	100	-13	44	88	62	20	2	4	41	13	-6	33	-58	-57	35	-31	1	11	14	13	14	10	0	-12	
6	0.60	11.5	-21	-29	26	5	-13	100	15	2	18	54	51	73	-28	-22	17	53	65	40	-4	47	6	-13	-24	-21	-27	-15	10	17	
7	0.70	11.1	-10	20	25	87	44	15	100	45	84	34	11	53	-37	-25	-7	-25	6	-57	-7	9	6	-4	-13	-11	-16	-9	10	6	
8	0.80	18.0	28	52	-16	41	88	2	45	100	67	35	9	15	55	32	21	48	-31	-38	49	3	11	14	11	14	8	14	10	-12	
9	0.90	19.3	-10	19	-11	87	62	18	84	67	100	56	27	57	-13	1	2	6	-6	-46	10	9	2	4	0	-2	-2	-3	4	-4	
10	1.00	11.7	-42	-11	-3	53	20	54	34	35	56	100	91	75	-1	22	23	42	25	12	43	51	10	0	-9	-7	-12	-4	13	2	
11	2.00	8.8	-30	-9	-3	29	2	51	11	9	27	91	100	69	-2	19	16	43	26	32	41	51	14	8	-5	-5	-12	-4	19	-5	
12	3.00	12.4	-31	-7	30	52	4	73	53	15	57	75	69	100	-38	-17	22	25	45	15	1	53	4	4	-6	-14	-14	-16	12	-4	
13	4.00	7.4	31	47	-24	-32	41	-28	-37	55	-13	-1	-2	-38	100	74	49	53	-29	4	53	1	24	26	19	28	15	29	20	-21	
14	5.00	6.8	-19	19	-37	-9	13	-22	-25	32	1	22	19	-17	74	100	67	27	5	3	24	10	36	18	-2	10	-9	17	36	-9	
15	6.00	6.5	-36	19	27	-12	-6	17	-7	21	2	23	16	22	49	67	100	24	39	10	2	34	28	11	-6	4	-11	10	29	-3	
16	7.00	5.7	33	13	-24	-22	33	53	-25	48	6	42	43	25	53	27	24	100	7	44	47	32	19	23	15	20	11	20	18	-20	
17	8.00	6.7	-44	-52	23	2	-58	65	6	-31	-6	25	26	45	-29	5	39	7	100	47	-32	60	26	-13	-39	-27	-46	-16	32	23	
18	9.00	10.5	0	-49	-17	-40	-57	40	-57	-38	-48	12	32	15	4	3	10	44	47	100	16	59	5	16	10	1	2	-3	10	-18	
19	10.00	8.8	6	10	-24	12	35	-4	-7	49	10	43	41	1	53	24	2	47	-32	16	100	37	0	16	22	20	22	17	-2	-17	
20	20.00	9.7	-29	-38	2	26	-31	47	9	3	9	51	51	53	1	10	34	32	60	59	37	100	26	21	3	5	-6	7	30	-17	
21	30.00	0.7	12	13	-5	5	1	6	11	2	10	14	4	4	24	36	28	19	26	5	0	26	100	56	3	42	-13	60	96	-31	
22	40.00	7.9	36	23	-20	4	11	-13	-4	14	4	0	10	4	26	18	11	23	-13	16	16	21	56	100	80	79	61	67	53	-96	
23	50.00	11.6	31	18	-21	-1	14	-24	-13	11	0	-9	-5	-6	19	-2	-6	15	-39	10	22	3	3	80	100	84	95	62	-4	-89	
24	60.00	9.8	24	18	-20	-2	13	-21	-11	14	-2	-7	-5	-14	28	10	4	20	-27	1	20	5	42	79	84	100	82	94	23	-73	
25	70.00	11.5	23	13	-19	-4	14	-27	-16	8	-2	-12	-14	15	-9	-11	11	-46	2	22	-6	-13	61	55	82	100	62	-27	-72		
26	80.00	10.5	17	15	-16	-3	10	-15	-9	14	-3	-4	-4	-16	29	17	10	20	-16	-3	17	7	60	67	62	54	62	100	39	-54	
27	90.00	10.6	13	13	-3	7	0	10	10	10	4	13	19	12	20	36	29	18	32	10	-2	30	96	53	-4	23	-27	39	100	-31	
28	100.00	14.3	-37	-22	20	-3	-12	17	6	-12	-4	-2	-5	-4	-21	-9	-3	-20	23	-18	-17	-17	-31	-96	-89	-73	-72	-54	-31	100	
29	200.00	3.2	6	5	-7	-2	5	-10	-6	5	-2	-4	-6	-9	10	0	0	6	-15	-2	5	-2	8	24	34	42	38	40	-1	-23	
30	300.00	9.6	6	5	-7	-2	5	-10	-6	5	-2	-4	-6	-9	10	0	0	6	-15	-2	5	-2	8	24	34	42	38	40	-1	-23	
31	400.00	4.1	6	5	-7	-2	5	-10	-6	5	-2	-4	-6	-9	10	0	0	6	-15	-2	5	-2	8	24	34	42	38	40	-1	-23	
32	500.00	27.4	-6	-5	7	2	-5	10	6	-5	2	4	6	9	-10	0	0	-6	15	2	-5	2	-8	-24	-34	-42	-38	-40	1	23	
33	600.00	47.6	-6	-5	7	2	-5	10	6	-5	2	4	6	9	-10	0	0	-6	15	2	-5	2	-8	-24	-34	-42	-38	-40	1	23	
34	700.00	81.2	-6	-5	7	2	-5	10	6	-5	2	4	6	9	-10	0	0	-6	15	2	-5	2	-8	-24	-34	-42	-38	-40	1	23	
35	800.00	133.1	-6	-5	7	2	-5	10	6	-5	2	4	6	9	-10	0	0	-6	15	2	-5	2	-8	-24	-34	-42	-38	-40	1	23	
36	900.00	174.6	-6	-5	7	2	-5	10	6	-5	2	4	6	9	-10	0	0	-6	15	2	-5	2	-8	-24	-34	-42	-38	-40	1	23	
37	1000.00																														

I	ELO(KEV)	RSD PCT	CORR*100							
			29	30	31	32	33	34	35	36
29	200.00	3.2	100	100	100	-100	-100	-99	-100	-99
30	300.00	9.6	100	100	100	-99	-100	-100	-100	-100
31	400.00	4.1	100	100	100	-100	-100	-100	-100	-100
32	500.00	27.4	-100	-99	-100	100	100	100	100	100
33	600.00	47.6	-100	-100	-100	100	100	100	100	99
34	700.00	81.2	-99	-100	-100	100	100	100	100	99
35	800.00	133.1	-100	-100	-100	100	100	100	100	100
36	900.00	174.6	-99	-100	-100	100	99	99	100	100
37	1000.00									

FU 240 CAPTURE 45 GROUPS

I ELO(KEV)	RSD PCT	CORR*100																												
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	
1	0.10	8.8	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
2	0.20	5.0	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
3	0.30	21.2	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
4	0.40	2.5	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
5	0.50	6.6	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
6	0.60	1.5	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
7	0.70	17.1	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
8	0.80	4.1	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
9	0.90	17.0	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
10	1.00	13.4	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2
11	2.00	11.5	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36	-36
12	3.00	21.1	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59	59
13	4.00	10.9	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13	-13
14	5.00	11.0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15	6.00	8.3	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22
16	7.00	7.9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
17	8.00	8.7	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12	12
18	9.00	10.1	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14	14
19	10.00	9.7	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22	-22
20	20.00	11.8	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2	-2
21	30.00	21.0	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72	72
22	40.00	29.2	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79	79
23	50.00	48.5	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83	83
24	60.00	39.3	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77
25	70.00	38.1	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76	76
26	80.00	36.3	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73	73
27	90.00	32.2	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69	69
28	100.00	34.1	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77	77
29	200.00	19.0	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47	47
30	300.00	36.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
31	400.00	30.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
32	500.00	26.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
33	600.00	22.7	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
34	700.00	9.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35	800.00	2.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
36	900.00	1.8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
37	1000.00	10.5	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
38	2000.00	14.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
39	3000.00	20.6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40	4000.00	19.4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
41	5000.00	16.1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
42	6000.00	11.8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
43	7000.00	9.3	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
44	8000.00	6.2	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
45	9000.00	7.8	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
46	10000.00																													

I ELO(KEV)	RSD PCT	CORR*100																
		29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45
29	200.00	19.0	100	36	36	36	36	35	-25	-25	-35	-31	-36	-35	-36	-35	-25	
30	300.00	36.5	36	100	99	99	99	99	-66	-66	-97	-89	-99	-98	-99	-97	-99	
31	400.00	30.3	36	99	100	99	99	99	-69	-69	-98	-87	-99	-97	-99	-98	-99	
32	500.00	26.4	36	99	99	100	99	99	-66	-66	-97	-89	-99	-98	-99	-98	-99	
33	600.00	22.7	36	99	99	99	100	99	-64	-64	-96	-90	-99	-98	-99	-97	-99	
34	700.00	9.2	35	99	98	99	99	100	-57	-57	-93	-94	-98	-97	-98	-95	-99	
35	800.00	2.4	-25	-66	-69	-66	-64	-57	100	99	82	26	70	51	70	79	62	
36	900.00	1.8	-25	-66	-69	-66	-64	-57	99	100	82	26	70	51	70	79	62	
37	1000.00	10.5	-35	-97	-98	-97	-96	-93	82	100	76	98	91	98	99	95	99	
38	2000.00	14.3	-31	-89	-87	-89	-90	-94	26	26	76	100	86	96	86	78	91	
39	3000.00	20.6	-36	-99	-99	-99	-99	-98	70	70	98	86	100	97	99	98	99	
40	4000.00	19.4	-35	-98	-97	-98	-98	-99	51	51	91	96	97	100	97	92	99	
41	5000.00	16.1	-36	-99	-99	-99	-99	-98	70	70	98	86	99	97	100			

PU241 CAPTURE 45 GROUPS

I ELO(KEV)	RSD PCT	CORR*100																												
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	
1	0.10 17.7	100	31	-76	-96	-95	-59	90	97	-92	-99	49	2	11	-83	59	-95	-86	88	-97	-94	48	-94	-82	-84	-94	1	-77	-94	
2	0.20 6.8	31	100	37	-6	0	57	69	50	6	-18	98	95	97	26	94	-3	19	71	-8	0	98	0	27	24	1	59	19	-15	
3	0.30 10.7	-76	37	100	90	92	97	-41	-61	95	84	18	62	54	99	6	91	98	-37	89	99	-19	92	99	90	93	39	88	81	
4	0.40 25.0	-96	-6	90	100	99	77	-76	-89	99	99	-25	23	14	94	-37	99	96	-73	99	99	-18	99	94	95	99	14	85	94	
5	0.50 15.9	-95	0	92	99	100	81	-72	-86	99	98	-20	29	19	96	-31	99	97	-69	99	99	-42	81	94	93	82	49	82	67	
6	0.60 5.6	-59	57	97	77	81	100	-18	-41	85	69	40	79	73	93	29	79	91	-14	76	81	42	81	94	93	82	49	82	67	
7	0.70 7.8	90	69	-41	-76	-72	-18	100	97	-67	-83	82	44	53	-81	88	-74	-56	99	-77	-72	81	-72	-49	-52	-71	27	-49	-78	
8	0.80 12.1	97	50	-61	-89	-86	-41	97	100	-82	-94	66	22	31	-70	74	-88	-74	96	-90	-86	64	-86	-69	-71	-85	13	-66	-89	
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