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PROGRAMS FOR CALCULATING RELATIVE  
INTENSITIES IN THE VIBRATIONAL  
STRUCTURE OF ELECTRONIC BAND SYSTEMS

Berkeley, California

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Richard N. Zare  
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PROGRAMS FOR CALCULATING RELATIVE INTENSITIES  
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ABSTRACT

Source-deck listings of two computer programs are given for the calculation of relative intensities in the vibrational structure of an electronic transition. The first program finds turning points of an electronic potential-energy curve by direct numerical evaluation of the Klein action integrals in the RKR procedure. The second program uses these turning points to construct an effective potential for the molecule with rotational quantum number  $J$ . The radial Schrödinger equation then is solved for this potential to yield vibrational-rotational wavefunctions from which the program calculates Franck-Condon factors,  $r$ -centroids, and relative intensities.

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† Now at Harvard University, Cambridge, Massachusetts.

## INTRODUCTION

This report supplements a previous paper,<sup>1</sup> hereafter referred to as I, which describes the calculation of relative intensities in the vibrational structure of an electronic transition. All computer programs used in I are documented herein.

Much of the programming was done by Mr. J. V. V. Kasper or in collaboration with him. The programs presented are not in final polished form and the author assumes the responsibility for all remaining errors that have gone undetected. No systematic attempt has been made to test all possible branches in these programs. However, these programs have been running successfully for over six months.

Much of the programming logic has been mentioned before in I. Comment cards have been liberally used in the Fortran source deck listings so that a description of the methods used in each program is self-contained. Comment cards also describe fully the preparation of data cards for each program. To further aid the user, sample data decks, which were successfully tested, are included. The output from these sample decks is displayed in the Appendix.

These programs are written for an IBM 709/7090/7094 installation. All source decks shown are photographic reproductions of machine listings.

## PROGRAM FOR FINDING TURNING POINTS OF A POTENTIAL BY RKR PROCEDURE

### Remarks

The input may be either in the form of spectroscopic constants for the electronic state, or the actual  $G(v)$  and  $B_v$  spectroscopic data. In the former case, the program requires about 3 sec per pair of turning points, whereas in the latter case<sup>2</sup> it is 5 sec. It is also possible to use a combination of input modes, i. e., vibrational constants and rotational  $B_v$  data, or vice versa.

When giving  $G(v)$  data, the zero-point energy may be assigned by the user, or found from extrapolation by the program. This latter feature allows the use of zero-line measurements or tabulated  $\Delta G(v)$  data.

### Limitations

(a) If tabulated  $G(v)$  or  $B_v$  data are used that have anomalous behavior, it is possible for the interpolation procedures NTRPSR or NTRPDP to fail.

(b) If less than eight  $G(v)$  or  $B_v$  data points are to be read in, NUST in subroutine RKR must be modified.

(c) Since errors tend to accumulate in the calculation of the turning points for each higher vibrational level, the potential curve is less accurate as the dissociation limit is approached.

### Listing

Table I lists the source decks and Table II gives a sample data deck for the RKR program.

Table I. Source-deck listing for RKR program.

```
CMAIN FINDS TURNING POINTS FOR A MOLECULE BY RYDBERG-KLEIN-REES METHOD MAIN 000
C ALL INPUT IS IN WAVE NUMBERS AND ANGSTROMS. MAIN 001
C USER SPECIFIES CHOICE BETWEEN MASS UNITS BASED ON C12 = 12, OR MAIN 002
C O16 = 16. MAIN 003
C THE FOLLOWING COMMENT CARDS DESCRIBE THE PREPARATION OF DATA CARDSMAIN 004
C
C DIMENSION XI(200),YI(200),XO(3000),V(3000),S(3000),KV(200), MAIN 005
Z ETRIAL(200),QIRA(2),QIEN(3),QIMS(2),ZIMS(2),ZIRA(2), MAIN 006
Z ZIEN(3),ECALC(200),XPRN(5),VPRN(5),DTFRMT(10), MAIN 007
Z G(200),BV(200),FMT(24),U(200),RMIN(200),RMAX(200), MAIN 008
Z DUFMT(10),BVF(200) MAIN 009
COMMON XI,YI,XO,V,XH,NSTA,N,MSTA,M,XMIN,XMAX,INSC,MBEG,NUSED,S, MAIN 010
Z NI,NS,MAXIT,FACM,ZMU,DE,WE,WEXE,WEYE,WEZE,WETE,BE,ALPHAE, MAIN 011
Z GAMMAE,DELTAE,AS,BS,MQ,STEP,U,BV,G,ICK,H,ITR,HDES,EPSLNE MAIN 012
C MAIN 013
C FIRST CARD IN DATA HAS A ONE IN COLUMN 1 IF A PPOBLEM FOLLOWS. MAIN 014
C VERY LAST CARD IN DATA MUST BE A BLANK CARD..... MAIN 015
C MAIN 016
C MAIN 017
1 CALL TIME(BEGIN) MAIN 018
WRITEOUTTAPE6,140,BEGIN MAIN 019
140 FORMAT (9H0 TIME = F10.5) MAIN 020
READINPUTTAPE5,100,ITEST MAIN 021
100 FORMAT (I1) MAIN 022
2 IF (ITEST) 3,400,3 MAIN 023
C MAIN 024
C NEXT TWO CARDS IN DATA HAVE NAME OF PROBLEM IN COLUMNS 1-72, MAIN 025
C WHERE CARRIAGE CONTROL IS IN COLUMN 1. NEXT CARD HAS IIMS AND MAIN 026
C MASSES OF THE TWO ATOMS, OR IIMS AND REDUCED MASS IN FIRST MASS MAIN 027
C FIELD WITH SECOND BLANK. MAIN 028
C IIMS = 1, MASS UNITS ARE BASED ON C12 = 12. MAIN 029
C IIMS = 2, MASS UNITS ARE BASED ON O16 = 16. MAIN 030
C MAIN 031
3 READINPUTTAPE5,101,(FMT(I),I=1,24) MAIN 032
101 FORMAT (12A6) MAIN 033
READINPUTTAPE5,102,IIMS,ZMAS1,ZMAS2 MAIN 034
102 FORMAT (I4,2F10.0) MAIN 035
C MAIN 036
C NEXT CARD IN DATA HAS IQHK, AND NUMBER OF LEVELS, EACH MAIN 037
C IN I4 FORMAT, AS WELL AS THE FORMAT STATEMENT WHICH CONTROLS THE MAIN 038
C READING OF THE LEVELS (IN COLUMNS 13-72)--FOR EXAMPLE- (4E16.8). MAIN 039
C IQHK = 0 IF THE FOLLOWING CARDS CONTAIN THE TABULATED G CURVE. MAIN 040
C IF A PARTICULAR VALUE IS TO BE INTERPOLATED, SET G(I) = -10. MAIN 041
C IF IT IS DESIRED TO USE CONSTANTS TO GENERATE THE ENTIRE MAIN 042
C G CURVE, IQHK MUST NOT BE EQUAL TO ZERO. MAIN 043
C A HOLLERITH TEXT MUST BE PUNCHED IN COLUMNS 13-72, MAIN 044
C AS IT WILL BE PRINTED, E.G., (1H ) MAIN 045
C THE NEXT CARD IN SUCH A CASE CONTAINS MAIN 046
C WE,WEXE,WEYE,WEZE,AND WETE. MAIN 047
C MAIN 048
5 READINPUTTAPE5,103,IQHK, N,(DTFRMT(I),I=1,10) MAIN 049
103 FORMAT(2I4,4X,10A6) MAIN 050
IIEN = 2 MAIN 051
6 IF (IQHK) 8,7,8 MAIN 052
8 READINPUTTAPE5,114,WE,WEXE,WEYE,WEZE,WETE MAIN 053
114 FORMAT (5E10.0) MAIN 054
GO TO 9 MAIN 055
7 READINPUTTAPE5,DTFRMT,(G(I),I=1,N) MAIN 056
C MAIN 057
```



Table I. (Contd.)

C	THE ZERO POINT ENERGY MAY BE FOUND BY EXTRAPOLATION, OR IT MAY BE	MAIN 058
C	FIXED BY THE USER FROM HIS TABULATED G(V) CURVE.	MAIN 059
C	NEXT CARD CONTAINS IOPEV.	MAIN 060
C	SET IOPEV = 0, IF THE ZERO POINT ENERGY IS TO BE FOUND BY	MAIN 061
C	EXTRAPOLATION, AND THE G(V) CURVE IS TO BE RAISED OR LOWERED	MAIN 062
C	ACCORDINGLY.	MAIN 063
C	THIS IS PARTICULARLY USEFUL IF DELTA G(V) DATA IS TO BE USED.	MAIN 064
C	SET IOPEV = 1, IF THE TABULATED G(V) CURVE IS TO BE USED UNCHANGED	MAIN 065
C	SET IOPEV = 2, IF THE G(V) CURVE IS TO BE CONSTRUCTED FROM CONSTAN	MAIN 066
C		MAIN 067
C	9 READ INPUT TAPE 5, 100, IOPEV	MAIN 068
C		MAIN 069
C	THE NEXT SET OF CARDS CONTAINS THE BV CURVE WITH THE SAME	MAIN 070
C	RESTRICTIONS AS FOR G CURVE ABOVE. NUMBER OF VALUES HERE MUST BE	MAIN 071
C	EQUAL TO THE NUMBER ABOVE	MAIN 072
C		MAIN 073
C	READINPUTTAPES,103,IBHK, N,(DUFMT(I),I=1,10)	MAIN 074
C	IIEB = 2	MAIN 075
C	30 IF (IBHK) 31,32,31	MAIN 076
C	31 READINPUTTAPES,114,BE,ALPHA E,GAMMA E,DELTA E,EPSLNE	MAIN 077
C	GO TO 33	MAIN 078
C	32 READINPUTTAPES,DUFMT,(BV(I),I=1,N)	MAIN 079
C		MAIN 080
C	THE ROTATIONAL CONSTANT BE MAY BE FOUND BY EXTRAPOLATION, OR IT	MAIN 081
C	MAY BE FIXED BY THE USER.	MAIN 082
C	NEXT CARD CONTAINS IOPA AND BEQUIL.	MAIN 083
C	SET IOPA = 0, IF THE VALUE OF BE IS TO BE FOUND BY EXTRAPOLATION	MAIN 084
C	FROM THE BV DATA READ IN. LEAVE BEQUIL BLANK.	MAIN 085
C	SET IOPA = 1, IF THE VALUE OF BE IS TO BE GIVEN BY BEQUIL.	MAIN 086
C	SET IOPA = 2, IF ROTATIONAL CONSTANTS ARE USED. LEAVE BEQUIL	MAIN 087
C	BLANK.	MAIN 088
C		MAIN 089
C	33 READ INPUT TAPE 5,102,IOPA,BEQUIL	MAIN 090
C		MAIN 091
C	NEXT DATA CARD CONTAINS RE, THE INTERNUCLEAR EQUILIBRIUM DISTANCE.	MAIN 092
C		MAIN 093
C	READ INPUT TAPE 5,106,RE	MAIN 094
C	106 FORMAT(F10.0)	MAIN 095
C		MAIN 096
C	NEXT DATA CARD CONTAINS VSTART,VFIN,AND HDDED WHERE	MAIN 097
C	TURNING POINTS ARE CALCULATED FROM VIBRATIONAL LEVEL VSTART TO	MAIN 098
C	VFIN IN STEPS OF HDDED E.G. FROM 0.5 TO 20.5 IN STEPS OF 1.0.	MAIN 099
C		MAIN 100
C	READ INPUT TAPE 5,114,VSTART,VFIN,HDDED	MAIN 101
C		MAIN 102
C	NEXT CARD CONTAINS IOPFG.	MAIN 103
C	SET IOPFG = 1, IF INTERMEDIATE STEPS IN THE EVALUATION OF THE	MAIN 104
C	KLEIN ACTION INTEGRALS ARE TO BE PRINTED.	MAIN 105
C	SET IOPFG = 0, IF INTERMEDIATE PRINT-OUT IS TO BE SKIPPED.	MAIN 106
C	NORMALLY THE USER SHOULD SET IOPFG = 0.	MAIN 107
C		MAIN 108
C	READ INPUT TAPE 5,100,IOPFG	MAIN 109
C	THIS TERMINATES COMMENT CARDS ON THE PREPARATION OF DATA.	MAIN 110
C	IF NO FURTHER PROBLEMS FOLLOW, REMEMBER TO ADD A BLANK CARD TO	MAIN 111
C	THE DATA DECK.	MAIN 112
C		MAIN 113
C		MAIN 114
C	QIRA(2) = 6HANGST.	MAIN 115

Table I. (Contd.)

	QIEN(2) = 6H1/CM	MAIN 116
	QIMS(1) = 6HC12=12	MAIN 117
	QIMS(2) = 6HO16=16	MAIN 118
C		MAIN 119
C	PRINT HEADING	MAIN 120
C		MAIN 121
	WRITEOUTPUTTAPE6,101,(FMT(I),I=1,24)	MAIN 122
C		MAIN 123
C	PRINT THE MASSES AND THEIR UNITS.	MAIN 124
C		MAIN 125
	10 IF (ZMAS2) 12,12,11	MAIN 126
	11 WRITEOUTPUTTAPE6,121,QIMS(IIMS),ZMAS1,ZMAS2	MAIN 127
	121 FORMAT (///40H THE MASSES OF THE TWO ATOMS, BASED ON A6, 6H, ARE	MAIN 128
	Z F10.6, 5H AND F10.6///)	MAIN 129
	GO TO 20	MAIN 130
	12 WRITEOUTPUTTAPE6,111,QIMS(IIMS),ZMAS1	MAIN 131
	111 FORMAT (///46H THE REDUCED MASS OF THE TWO ATOMS, BASED ON A6,	MAIN 132
	Z 5H, IS F10.6///)	MAIN 133
C		MAIN 134
C		MAIN 135
C		MAIN 136
C	PRINT G(V) DATA, OR VIBRATIONAL CONSTANTS	MAIN 137
C		MAIN 138
	20 IF (IQHK) 22,21,22	MAIN 139
	22 WRITEOUTPUTTAPE6,DIFRMT	MAIN 140
	WRITEOUTPUTTAPE6,116,WE,WEXE,WEYE,WEZE,WETE	MAIN 141
	116 FORMAT (63H0 THE G(V) CURVE IS CONSTRUCTED FROM THE FOLLOWING INP	MAIN 142
	ZT DATA. // 7H WE = F10.3,8H, WEXE =F10.4,8H, WEYE =E10.5,8H, WEZ	MAIN 143
	ZE =E10.5,8H, WETE =E10.5 )	MAIN 144
	GO TO 40	MAIN 145
	21 WRITEOUTPUTTAPE6,122,QIEN(I IEN)	MAIN 146
	122 FORMAT (32H THE INPUT G VALUES, ENERGY IN A6,	MAIN 147
	Z 18H, ARE GIVEN BELOW. //)	MAIN 148
	WRITEOUTPUTTAPE6,115,(G(I),I=1,N)	MAIN 149
	115 FORMAT (1X10F11.3)	MAIN 150
	WRITEOUTPUTTAPE6,128	MAIN 151
	128 FORMAT (20X48HVALUES OF -10. ARE TO BE FOUND BY INTERPOLATION.)	MAIN 152
C		MAIN 153
C	PRINT BV DATA, OR ROTATIONAL CONSTANTS	MAIN 154
C		MAIN 155
	40 IF (IBHK) 41,42,41	MAIN 156
	41 WRITEOUTPUTTAPE6,DUFMT	MAIN 157
	WRITEOUTPUTTAPE6,120,BE,ALPHAE,GAMMAE,DELTA E,EPSLNE	MAIN 158
	120 FORMAT (64H0 THE BV(V) CURVE IS CONSTRUCTED FROM THE FOLLOWING INP	MAIN 159
	ZUT DATA. //7H BE = 1PE11.5,10H, ALPHAE = E11.4,10H, GAMMAE =	MAIN 160
	Z E11.4,10H, DELTA E = E11.4, 10H, EPSLNE = E11.4)	MAIN 161
	GO TO 43	MAIN 162
	42 WRITEOUTPUTTAPE6,127,QIEN(I IEB)	MAIN 163
	127 FORMAT (33H THE INPUT BV VALUES, ENERGY IN A6,	MAIN 164
	Z 18H, ARE GIVEN BELOW. //)	MAIN 165
	WRITEOUTPUTTAPE6,129,(BV(I),I=1,N)	MAIN 166
	129 FORMAT (1X10F11.6)	MAIN 167
	WRITEOUTPUTTAPE6,128	MAIN 168
C		MAIN 169
C	PRINT HEADING	MAIN 170
43	WRITEOUTPUTTAPE6,101,(FMT(I),I=1,24)	MAIN 171
C		MAIN 172
	200 IF (ZMAS2) 201,201,202	MAIN 173

Table I. (Contd.)

201	ZMU = ZMAS1	MAIN 174
	GO TO 204	MAIN 175
202	ZMU = ZMAS1*ZMAS2/(ZMAS1+ZMAS2)	MAIN 176
204	ZIMS(1) = 1.0	MAIN 177
	ZIMS(2) = .9996784	MAIN 178
	ZIRA(1) = 1.0	MAIN 179
	ZIRA(2) = 1.889766	MAIN 180
	ZMU = ZMU * ZIMS(IIMS)	MAIN 181
	ZIEN(1) = ZMU * 3.643668E3	MAIN 182
	ZIEN(2) = ZMU * 1.6610826E-2	MAIN 183
	ZIFN(3) = ZMU * 1.339776E2	MAIN 184
	FACM = 60.201702/ZMU	MAIN 185
206	XI(1) = 0.5	MAIN 186
207	DO 208 I = 2,N	MAIN 187
	IL = I - 1	MAIN 188
	XI(I) = XI(IL) + 1.0	MAIN 189
208	CONTINUE	MAIN 190
	ZERO = 0.0	MAIN 191
	WRITEOUTPUTTAPE7,101,(FMT(I),I=1,24)	MAIN 192
	WRITEOUTPUTTAPE7,138,RE,ZERO	MAIN 193
138	FORMAT (1XF9.7,F10.3)	MAIN 194
210	CALL RKR(RMIN,RMAX,VSTART,VFIN,HDED,NFIN,EV1,U,IQHK,IBHK,IOPEV, Z IOPA,BEQUIL,IOPFG)	MAIN 195
	GO TO 1	MAIN 196
400	CALL EXIT	MAIN 197
	END	MAIN 198
		MAIN 199



Table I. (Contd.)

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189	DO 190 I = 1,JJ	RKR 058
	IJ = IG(I)	RKR 059
	Z(IJ) = BI(I)	RKR 060
190	CONTINUE	RKR 061
191	IF (JK) 196,196,192	RKR 062
192	CALL NTRPSR (RMIN,RMAX,EV,BI,HDES,IK,JK,VNIN,VN,INSC,MBEG,NUST)	RKR 063
	LOC = 9	RKR 064
193	IF (INSC) 288,194,288	RKR 065
194	DO 195 I = 1,JK	RKR 066
	IK = IB(I)	RKR 067
	BV(IK) = BI(I)	RKR 068
195	CONTINUE	RKR 069
196	IF (IQHK) 204,203,204	RKR 070
204	EV1 = -GFUNCF(0.5)	RKR 071
	IOPEV = 0	RKR 072
	DO 170 I = 1,N	RKR 073
	Z(I) = GFUNCF(Y(I)) + EV1	RKR 074
170	CONTINUE	RKR 075
	GO TO 211	RKR 076
203	INTG = INTQ	RKR 077
	MBEG = 1	RKR 078
	M = 1	RKR 079
	UEV(1) = 0.	RKR 080
	HDES = 1.	RKR 081
	EV1 = -EV1	RKR 082
	IF (EV1) 211,206,206	RKR 083
206	CALL NTRPSR(Y,Z,UEV,EV,HDES,N,M,VNIN,VN,INSC,MBEG,NUST)	RKR 084
	LOC = 1	RKR 085
208	IF (INSC) 288,210,288	RKR 086
210	EV1 = EV(1)	RKR 087
C	EV1 NOW CONTAINS THE ZERO POINT ENERGY BY EXTRAPOLATION.	RKR 088
211	IF (IBHK) 171,207,171	RKR 089
171	EV(1) = BE	RKR 090
	DO 172 I = 1,N	RKR 091
	BV(I) = BFUNCF(Y(I))	RKR 092
172	CONTINUE	RKR 093
	GO TO 205	RKR 094
207	IF (IOPA) 2071,2072,2071	RKR 095
2071	EV(1) = BEQUIL	RKR 096
	GO TO 205	RKR 097
2072	CALL NTRPSR (Y,BV,UEV,EV,HDES,N,M,VNIN,VN,INSC,MBEG,NUST)	RKR 098
C	EV(1) NOW CONTAINS BE BY EXTRAPOLATION	RKR 099
	LOC = 7	RKR 100
	IF (INSC) 288,205,288.	RKR 101
205	V(1) = 0.	RKR 102
	G(1) = 0.	RKR 103
	BO(1) = EV(1)	RKR 104
	DO 209 I = 1,N	RKR 105
	V(I+1) = Y(I)	RKR 106
	G(I+1) = Z(I)	RKR 107
	BO(I+1) = BV(I)	RKR 108
209	CONTINUE	RKR 109
	NP = N + 1	RKR 110
	IF (IOPEV) 2091,2092,2091	RKR 111
2091	CONTINUE	RKR 112
	EV1 = EV1 + G(2)	RKR 113
2092	DO 213 I = 2,NP	RKR 114
	G(I) = G(I) - EV1	RKR 115

Table I. (Contd.)

Y(I) = V(I)	RKR	116
Z(I) = G(I)	RKR	117
BV(I) = BO(I)	RKR	118
213 CONTINUE	RKR	119
IF (IOPEV) 2131,2132,2131	RKR	120
2131 EV1 = -G(2)	RKR	121
2132 IF (NPROB-17) 2133,2134,2133	RKR	122
2134 M = 1	RKR	123
EV(1) = DE	RKR	124
CALL NTRPSR (Z,Y,EV,UEV,HDES,NP,M,VNIN,VN,INSC,MBEG,NUST)	RKR	125
LOC = 2	RKR	126
IF (INSC) 288,2135,288	RKR	127
2135 NP = NP + 1	RKR	128
Y(NP) = UEV	RKR	129
V(NP) = UEV	RKR	130
Z(NP) = DE	RKR	131
G(NP) = DE	RKR	132
BO(NP) = 0.	RKR	133
BV(NP) = 0.	RKR	134
2133 Y(1) = 0.	RKR	135
Z(1) = 0.	RKR	136
BV(1) = BO(1)	RKR	137
VMIN = VSTA	RKR	138
VN = VFIN	RKR	139
HDES = HDED	RKR	140
M = 0	RKR	141
WRITEOUTTAPE6,113,(Y(I),Z(I),I=1,NP)	RKR	142
113 FORMAT (33H0 THE G(V) VALUES USED BELOW ARE / 6(4X1HV10X1HG4X) //	RKR	143
Z 6(1XF7.3,F12.4))	RKR	144
WRITEOUTTAPE6,108,(Y(I),BV(I),I=1,NP)	RKR	145
108 FORMAT (33H0 THE BV(V) VALUES USED BELOW ARE / 6(4X1HV9X2HBV4X) //	RKR	146
Z 6(1XF7.3,F12.7))	RKR	147
IF (IQHK) 215,212,215	RKR	148
215 M = XFIXF((VFIN-VSTA)/HDED) + 1	RKR	149
DO 217 I = 1,M	RKR	150
OEV(I) = VSTA + FLOATF(I-1)*HDED	RKR	151
OV(I) = GFUNCF(OEV(I))	RKR	152
217 CONTINUE	RKR	153
INSC = 0	RKR	154
GO TO 218	RKR	155
212 CALL NTRPDP(V,G,OEV,OV,HDED,NP,M,VSTA,VFIN,INSC,MBEG,NUST)	RKR	156
LOC = 2	RKR	157
WRITEOUTTAPE6,106,HDES,VMIN,VN,MBEG,NUST,INSC,NP,M	RKR	158
106 FORMAT (6H0HDES=1PE15.7,7H, VMIN=E15.7,5H, VN=E15.7,7H, MBEG=15/	RKR	159
Z9X7H, NUST=15,7H, INSC=15,4H, N=15,4H, M=15)	RKR	160
218 WRITEOUTTAPE6,109	RKR	161
109 FORMAT (54H0 OUTPUT V,G--LEVELS AT WHICH TURNING POINTS ARE FOUND/	RKR	162
Z 6(4X1HV10X1HG4X) //)	RKR	163
WRITEOUTTAPE6,107,(OEV(I),OV(I),I=1,M)	RKR	164
107 FORMAT (6(1XF7.3,F12.4))	RKR	165
214 IF (INSC) 288,216,288	RKR	166
216 DO 219 I = 1,M	RKR	167
TEMP(I) = OEV(I)	RKR	168
U(I) = OV(I)	RKR	169
219 CONTINUE	RKR	170
C	RKR	171
C INTEGRATION CONSTANTS	RKR	172
C	RKR	173

Table I. (Contd.)

	STEP = .9	RKR	174
	MZ(1) = 101	RKR	175
	MZ(2) = 81	RKR	176
	MZ(3) = 61	RKR	177
	IZ(1) = 8	RKR	178
D	XGAUS(1,1) = .019855071751232	RKR	179
D	XGAUS(1,2) = .101666761293186	RKR	180
D	XGAUS(1,3) = .237233795041836	RKR	181
D	XGAUS(1,4) = .408282678752175	RKR	182
D	XGAUS(1,5) = 1. - XGAUS(1,4)	RKR	183
D	XGAUS(1,6) = 1. - XGAUS(1,3)	RKR	184
D	XGAUS(1,7) = 1. - XGAUS(1,2)	RKR	185
D	XGAUS(1,8) = 1. - XGAUS(1,1)	RKR	186
D	AGAUS(1,1) = .050614268145188	RKR	187
D	AGAUS(1,2) = .111190517226687	RKR	188
D	AGAUS(1,3) = .156853322938944	RKR	189
D	AGAUS(1,4) = .181341891689181	RKR	190
D	AGAUS(1,5) = AGAUS(1,4)	RKR	191
D	AGAUS(1,6) = AGAUS(1,3)	RKR	192
D	AGAUS(1,7) = AGAUS(1,2)	RKR	193
D	AGAUS(1,8) = AGAUS(1,1)	RKR	194
	IZ(2) = 6	RKR	195
D	XGAUS(2,1) = .033765242898424	RKR	196
D	XGAUS(2,2) = .169395306766868	RKR	197
D	XGAUS(2,3) = .380690406958402	RKR	198
D	XGAUS(2,4) = 1. - XGAUS(2,3)	RKR	199
D	XGAUS(2,5) = 1. - XGAUS(2,2)	RKR	200
D	XGAUS(2,6) = 1. - XGAUS(2,1)	RKR	201
D	AGAUS(2,1) = .085662246189585	RKR	202
D	AGAUS(2,2) = .180380786524070	RKR	203
D	AGAUS(2,3) = .233956967286345	RKR	204
D	AGAUS(2,4) = AGAUS(2,3)	RKR	205
D	AGAUS(2,5) = AGAUS(2,2)	RKR	206
D	AGAUS(2,6) = AGAUS(2,1)	RKR	207
	IZ(3) = 4	RKR	208
D	XGAUS(3,1) = .069431844202974	RKR	209
D	XGAUS(3,2) = .330009478207572	RKR	210
D	XGAUS(3,3) = 1. - XGAUS(3,2)	RKR	211
D	XGAUS(3,4) = 1. - XGAUS(3,1)	RKR	212
D	AGAUS(3,1) = .173927422568727	RKR	213
D	AGAUS(3,2) = .326072577431273	RKR	214
D	AGAUS(3,3) = AGAUS(3,2)	RKR	215
D	AGAUS(3,4) = AGAUS(3,1)	RKR	216
D	ZG(1) = ZG(3)	RKR	217
	WRITEOUTPUTTAPE6,100	RKR	218
100	FORMAT (1H1)	RKR	219
224	DO 280 I = 1,M	RKR	220
D	TEMPI = OEV(I)	RKR	221
	NUS2 = NUST/2	RKR	222
	NB = NUS2 + 1	RKR	223
	NF = N - NB + 1	RKR	224
	DO 225 J = NB,NF	RKR	225
	IF (TEMPI - V(J)) 235,235,225	RKR	226
225	CONTINUE	RKR	227
	ISG = NF + 1	RKR	228
	GO TO 237	RKR	229
235	ISG = J	RKR	230
237	NSTA = ISG - NUS2	RKR	231

Table I. (Contd.)

D	VMIN = 0.	RKR	232
	FEG = 0.	RKR	233
	GEG = 0.	RKR	234
	LT = 1	RKR	235
	IZGD = 0	RKR	236
	GDO = 0.	RKR	237
	FDO = 0.	RKR	238
	ISG = 0	RKR	239
	ISB = 0	RKR	240
C		RKR	241
C	COMMENCE FINDING TURNING POINTS BY INTEGRATION	RKR	242
C		RKR	243
	CALL TIME (BEGIA)	RKR	244
D	226 BS = VMIN + (TEMPI - VMIN) * STEP	RKR	245
	227 IF (LT-3) 228,228,301	RKR	246
	228 MQ = MZ(LT)	RKR	247
	223 KM = (MQ-1)/2	RKR	248
	TMIN = VMIN	RKR	249
	TS = BS	RKR	250
	A = (TS-TMIN)/FLOATF(MQ-1)	RKR	251
	MX = 0	RKR	252
	IF (IQHK) 401,229,401	RKR	253
	229 CALL NTRPSR(Y,Z,UEV,EV,A,NP,MX,TMIN,TS,INSC,MBEG,NUST)	RKR	254
	230 LOC = 3	RKR	255
	231 IF (INSC) 288,232,288	RKR	256
	232 IF (GDO) 236,233,236	RKR	257
	233 MX = 0	RKR	258
	IF (IBHK) 403,239,403	RKR	259
	239 CALL NTRPSR(Y,BV,UEV,BI,A,NP,MX,TMIN,TS,INSC,MBEG,NUST)	RKR	260
	LOC = 4	RKR	261
	234 IF (INSC) 288,236,288	RKR	262
	236 DO 238 J = 1,MQ	RKR	263
	DENQ = U(I) - EV(J)	RKR	264
	IF (DENQ) 292,292,241	RKR	265
	241 UEV(J) = 1./SQRTF(DENQ)	RKR	266
	EV(J) = BI(J) * UEV(J)	RKR	267
	238 CONTINUE	RKR	268
	FSUM = UEV(1) + 4.*UEV(2) + UEV(MQ)	RKR	269
	GSUM = EV(1) + 4.*EV(2) + EV(MQ)	RKR	270
	240 DO 242 J = 2,KM	RKR	271
	FSUM = FSUM + 4.*UEV(2*J) + 2.*UEV(2*J-1)	RKR	272
	GSUM = GSUM + 4.*EV(2*J) + 2.*EV(2*J-1)	RKR	273
	242 CONTINUE	RKR	274
	FEG2 = A*FSUM/3.	RKR	275
	GEG2 = A*GSUM/3.	RKR	276
	250 IF (LT - 1) 262,262,254	RKR	277
	301 IZDO = (LT-1)/3	RKR	278
	IF (IZDO - 3) 304,304,303	RKR	279
	303 IZDO = 3	RKR	280
	304 NGAS = IZ(IZDO)	RKR	281
	DO 306 J = 1,NGAS	RKR	282
D	XG(J) = (BS-VMIN) * XGAUS(IZDO,J) + VMIN	RKR	283
	UEV(J) = XG(J)	RKR	284
	306 CONTINUE	RKR	285
	MST = 1	RKR	286
D	EPSH = TEMPI - XG(NGAS)	RKR	287
	FEPS = EPSH	RKR	288
	IF (EPSH(1)) 276,307,308	RKR	289



Table I. (Contd.)

307	IF (EPSH(2)) 276,276,308	RKR 290
308	IF (IQHK) 405,309,405	RKR 291
309	CALL NTRPDP(V,G,XG,YG,EP SH,NP,NGAS,VMIN,BS,INSC,MST,NUST)	RKR 292
	LOC = 5	RKR 293
310	IF (INSC) 288,311,288	RKR 294
311	IF (IZGD) 312,312,340	RKR 295
312	IF (GDO) 318,314,318	RKR 296
314	MST = 1	RKR 297
	IF (IBHK) 407,315,407	RKR 298
315	CALL NTRPSR (Y,BV,UEV,BI,FEPS,NP,NGAS,TMIN,TS,INSC,MST,NUST)	RKR 299
	LOC = 6	RKR 300
316	IF (INSC) 288,318,288	RKR 301
318	FSUM = 0.0	RKR 302
	GSUM = 0.0	RKR 303
	DO 320 J = 1,NGAS	RKR 304
	IF (IQHK) 718,317,718	RKR 305
D 317	DENQ(J) = OV(I) - YG(J)	RKR 306
718	IF (DENQ(J)) 292,292,323	RKR 307
323	XG(J) = AGAUS(IZDO,J)/SQRTF(DENQ(J))	RKR 308
	YG(J) = BI(J) * XG(J)	RKR 309
	FSUM = FSUM + XG(J)	RKR 310
	GSUM = GSUM + YG(J)	RKR 311
320	CONTINUE	RKR 312
	IF (BI(NGAS)-BI(1)) 322,321,322	RKR 313
321	IZGD = 1	RKR 314
D 322	BSV = BS - VMIN	RKR 315
	FEG2 = BSV * FSUM	RKR 316
324	GEG2 = BSV * GSUM	RKR 317
	GO TO 254	RKR 318
340	FSUM = 0.0	RKR 319
	DO 342 J = 1,NGAS	RKR 320
D	DENQ = OV(I) - YG(J)	RKR 321
	IF (DENQ) 292,292,341	RKR 322
341	XG(J) = AGAUS(IZDO,J)/SQRTF(DENQ)	RKR 323
	FSUM = FSUM + XG(J)	RKR 324
342	CONTINUE	RKR 325
	GSUM = BI(NGAS) * FSUM	RKR 326
	GO TO 322	RKR 327
254	IF (FEG2/FEG - 1.E-6) 255,255,256	RKR 328
255	FDO = 1.	RKR 329
256	IF (GEG2/GEG - 1.E-6) 257,257,258	RKR 330
257	GDO = 1.	RKR 331
258	IF (ABS(FEG2/FEG1) - .9) 260,260,259	RKR 332
259	FDO = 1.	RKR 333
260	IF (ABS(GEG2/GEG1) - .9) 262,262,261	RKR 334
261	GDO = 1.	RKR 335
262	LT = LT + 1	RKR 336
	FEG1 = FEG2	RKR 337
	GEG1 = GEG2	RKR 338
264	IF (FDO) 269,266,269	RKR 339
266	FEG = FEG + FEG2	RKR 340
268	IF (GDO) 272,270,272	RKR 341
269	IF (GDO) 276,270,276	RKR 342
270	GEG = GEG + GEG2	RKR 343
D 272	VMIN = BS	RKR 344
	IF (IOPFG) 273,274,273	RKR 345
273	CALL TIME (AFTEA)	RKR 346
	XTIQ = (AFTEA-BEGIA)*60.	RKR 347

Table I. (Contd.)

BEGIA = AFTEA	RKR	348
WRITEOUTPUTTAPE6,110,FEG,GEG,XTIQ	RKR	349
110 FORMAT (6X6HFEG = 1PE15.7, 8H, GEG = E15.7,10X9HPEQUIRED OPF8.5,	RKR	350
Z 9H SECONDS.)	RKR	351
274 IF (LT-20) 226,226,290	RKR	352
276 F = FEG * FAC	RKR	353
GF = GEG / FAC	RKR	354
RMAX(I) = SQRTF(F*F + F/GF) + F	RKR	355
RMIN(I) = RMAX(I) - 2.*F	RKR	356
CALL TIME(AFTER)	RKR	357
XTIQ = 60.*(AFTER-BEGIN)	RKR	358
BEGIN = AFTER	RKR	359
WRITEOUTPUTTAPE6,104,TEMPI,U(I),RMIN(I),RMAX(I),XTIQ,BI(NGAS)	RKR	360
Z ,F,GF	RKR	361
104 FORMAT (10H0 FOR V = F7.3,6H, G = F10.3,14H 1/CM, RMIN = F10.7,	RKR	362
Z 12H AND RMAX = F10.7,27H ANGSTROMS. THIS REQUIRED F8.5,	RKR	363
Z 9H SECONDS. / 20X12H ALSO, BV = F12.7 /20X49H THE KLEIN ARKR	364	
ZCTION INTEGRALS F AND G ARE EQUAL TO 2E15.8///)	RKR	365
WRITEOUTPUTTAPE7,105,RMIN(I),U(I),RMAX(I),U(I)	RKR	366
105 FORMAT (1XF9.7,F10.3 / 1XF9.7,F10.3)	RKR	367
280 CONTINUE	RKR	366
DO 284 I = 1,N	RKR	369
Z(I) = Z(I+1)	RKR	370
Y(I) = Y(I+1)	RKR	371
BV(I) = BV(I+1)	RKR	372
284 CONTINUE	RKR	373
WRITEOUTPUTTAPE6,100	RKR	374
286 RETURN	RKR	375
288 ZOC(1) = 6H EV1	RKR	376
ZOC(2) = 6HG(LEV)	RKR	377
ZOC(3) = 6HS.P.EV	RKR	378
ZOC(4) = 6HS.P.BV	RKR	379
ZOC(5) = 6HD.P.EV	RKR	380
ZOC(6) = 6HD.P.BV	RKR	381
ZOC(7) = 6H BV1	RKR	382
ZOC(8) = 6HG FILL	RKR	383
ZOC(9) = 6HBVFILL	RKR	384
WRITEOUTPUTTAPE6,102,ZOC(LOC),U(I)	RKR	385
102 FORMAT (26H0 NTRPDP UNSUCCESSFUL FOR A6, 11H, WHEN U = E16.8)	RKR	386
INTG = 1	RKR	387
GO TO 286	RKR	388
290 WRITEOUTPUTTAPE6,103	RKR	389
103 FORMAT (20H0 TEG REACHED MAXIT )	RKR	390
INTG = 1	RKR	391
GO TO 286	RKR	392
292 INTG = 1	RKR	393
WRITEOUTPUTTAPE6,111	RKR	394
111 FORMAT (22H0 DENQ IS NOT POSITIVE)	RKR	395
GO TO 286	RKR	396
401 MX = MQ	RKR	397
DO 402 J = 1,MQ	RKR	398
UEV(J) = TMIN + FLOATF(J-1) * A	RKR	399
EV(J) = GFUNCF(UEV(J))	RKR	400
402 CONTINUE	RKR	401
GO TO 232	RKR	402
403 MX = MQ	RKR	403
DO 404 J = 1,MQ	RKR	404
UEV(J) = TMIN + FLOATF(J-1) * A	RKR	405

Table I. (Contd.)

BI(J) = BFUNCF(UEV(J))	RKR 406
404 CONTINUE	RKR 407
GO TO 236	RKR 408
405 CALL DGUNC (XG,DENQ,NGAS,TEMPI)	RKR 409
GO TO 311	RKR 410
407 DO 408 J = 1,NGAS	RKR 411
BI(J) = BFUNCF(UEV(J))	RKR 412
408 CONTINUE	RKR 413
GO TO 318	RKR 414
END	RKR 415

Table I. (Contd.)

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CNTRPSR INTERPOLATION PROGRAM (BY SUCCESSIVE RANGES) SINGLE PREC. NTRPS000
C NTRPS001
C THE METHOD OF LAGRANGE IS USED. THE INPUT POINTS NEED NOT BE NTRPS002
C EQUALLY SPACED. THERE ARE TWO MODES OF INPUT AVAILABLE. THE NTRPS003
C FIRST OCCURS WHEN M = 0. THE ABSCISSAE ARE THEN GENERATED FROM NTRPS004
C XMIN,XMAX,AND XH. AT EXIT M = NO. OF POINTS FOUND, AND XO NTRPS005
C CONTAINS THE ABSCISSAE. M WILL BE CHECKED TO INSURE THAT THE NTRPS006
C DIMENSION IS NOT EXCEEDED. MDIMM = THE DIMENSION OF THE XO, YO NTRPS007
C ARRAYS. THE SECOND MODE OCCURS WHEN M IS POSITIVE. THE M NTRPS008
C ABSCISSAE ARE THEN ASSUMED TO HAVE BEEN GENERATED PRIOR TO NTRPS009
C ENTRY. THE STARTING INDEX FOR THE OUTPUT ARRAY MUST BE NTRPS010
C SPECIFIED. THE FIRST POINT FOUND WILL BE AT XO(MBEG). XH MUST NTRPS011
C BE GIVEN SINCE THE ORDINATE FOR ANY POINT CLOSER THAN .01*XH TO NTRPS012
C AN INPUT POINT IS TAKEN AS THAT FOR THE INPUT POINT. -NUSED- IS NTRPS013
C THE NUMBER OF POINTS USED FOR EACH INTERPOLATED POINT. *NUSED* NTRPS014
C MUST BE EVEN AND LESS THAN OR EQUAL TO -N-. NUSED = 8 IS NTRPS015
C SUGGESTED. ANY POINT FARTHER THAN NUSED/2 POINTS FROM EITHER ENDNTRPS016
C IS FOUND FROM THE NUSED/2 ON EACH SIDE. NTRPSR WILL SCALE AND NTRPS017
C RESCALE IN ORDER TO AVOID OVERFLOW. IF THE FIRST SCALING DOES NTRPS018
C NOT SUCCEED, NTRPSR WILL TRY UP TO 7 TIMES MORE BEFORE RETURNING NTRPS019
C IN THE ERROR MODE. (INSC = 1) NTRPS020
C INPUT IS XI,YI,(XO),XH,N,M,(XMIN),(XMAX),MBEG,NUSED. NTRPS021
C OUTPUT IS (XO),YO,INSC. NTRPS022
C INSC = 0 IF PROGRAM WAS SUCCESSFUL. IF NOT, INSC = 1. NTRPS023
C NTRPS024
C SUBROUTINE NTRPSR(XJ,YJ,XO,YO,XN,N,K,XNIN,XNAX,INSC,MBEG,NUSED) NTRPS025
C DIMENSION XI(200),YI(200),XO(3000),YO(3000),XJ(200),YJ(200), NTRPS026
C Z NUMB(200) NTRPS027
C MDIMM = 3000 NTRPS028
C XMAX = XNAX NTRPS029
C XMIN = XNIN NTRPS030
C XH = ABSF(XN) NTRPS031
C M = K NTRPS032
C IREV = 0 NTRPS033
C IREX = 0 NTRPS034
C M IS ZERO, IF XH, XMIN, XMAX ARE TO BE USED. IF M IS NOT = TO NTRPS035
C ZERO, THEN XO(I), I = 1,M WILL BE USED AS ABSCISSA. NTRPS036
C 200 IF (M) 270,201,206 NTRPS037
C 201 M = XINTF(ABSF((XMAX-XMIN)/XH)) + 1 NTRPS038
C IF M IS MORE THAN DIMENSION OF XO, RETURN IN ERROR MODE. NTRPS039
C IF (M+MBEG-MDIMM-2) 202,272,272 NTRPS040
C 202 MF = MBEG + M - 1 NTRPS041
C IF (XMAX - XMIN) 203,204,204 NTRPS042
C 203 XMIN = XNAX NTRPS043
C XMAX = XNIN NTRPS044
C IREV = 1 NTRPS045
C 204 DO 205 I = MBEG,MF NTRPS046
C XO(I) = FLOATF(I-MBEG) * XH + XMIN NTRPS047
C 205 CONTINUE NTRPS048
C 206 DO 207 I = 1,N NTRPS049
C XI(I) = XJ(I) NTRPS050
C 207 CONTINUE NTRPS051
C MF = MBEG + M - 1 NTRPS052
C MSTA = MBEG NTRPS053
C MUST = NUSED/2 NTRPS054
C NS = MUST + 1 NTRPS055
C NF = N - NS + 1 NTRPS056
C NFP = NF + 1 NTRPS057
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Table I. (Contd.)

DO 208 I = NS,NFP	NTRPS058
NUMB(I) = 0	NTRPS059
208 CONTINUE	NTRPS060
IF (XO(MF) - XO(MBEG)) 209,211,211	NTRPS061
209 M2 = M/2	NTRPS062
M2F = MBEG + M2 - 1	NTRPS063
DO 210 I = MBEG,M2F	NTRPS064
K = MF + MBEG - I	NTRPS065
TEMP = XO(I)	NTRPS066
XO(I) = XO(K)	NTRPS067
XO(K) = TEMP	NTRPS068
210 CONTINUE	NTRPS069
IREV = 1	NTRPS070
211 IF (XI(N)-XI(1)) 212,216,216	NTRPS071
212 N2 = N/2	NTRPS072
DO 214 I = 1,N2	NTRPS073
K = N + 1 - I	NTRPS074
TEMP = XJ(I)	NTRPS075
TEMS = YJ(I)	NTRPS076
XJ(I) = XJ(K)	NTRPS077
YJ(I) = YJ(K)	NTRPS078
XJ(K) = TEMP	NTRPS079
YJ(K) = TEMS	NTRPS080
214 CONTINUE	NTRPS081
IREX = 1	NTRPS082
216 IF (NF-NS) 236,218,218	NTRPS083
218 DO 226 J = MBEG,MF	NTRPS084
DO 224 I = NS,NF	NTRPS085
220 IF (XO(J) - XI(I)) 222,222,224	NTRPS086
222 NUMB(I) = NUMB(I) + 1	NTRPS087
GO TO 226	NTRPS088
224 CONTINUE	NTRPS089
NUMB(NFP) = NUMB(NFP) + 1	NTRPS090
226 CONTINUE	NTRPS091
GO TO 238	NTRPS092
236 NUMB(NFP) = M	NTRPS093
238 M = 0	NTRPS094
239 DO 250 L = NS,NFP	NTRPS095
IF (NUMB(L)) 250,250,242	NTRPS096
242 M = NUMB(L)	NTRPS097
NSTA = L - NUST	NTRPS098
GO TO 100	NTRPS099
246 IF (INSC) 274,248,274	NTRPS100
248 MSTA = MSTA + M	NTRPS101
250 CONTINUE	NTRPS102
240 K = MSTA - MBEG	NTRPS103
IF (IREV) 256,256,252	NTRPS104
252 M2F = K/2 + MBEG - 1	NTRPS105
DO 254 I = MBEG,M2F	NTRPS106
J = MF + MBEG - I	NTRPS107
TEMP = XO(I)	NTRPS108
TEMS = YO(I)	NTRPS109
XO(I) = XO(J)	NTRPS110
YO(I) = YO(J)	NTRPS111
XO(J) = TEMP	NTRPS112
YO(J) = TEMS	NTRPS113
254 CONTINUE	NTRPS114
256 IF (IREX) 262,262,258	NTRPS115

Table I. (Contd.)

258	DO 260 I = 1,N2	NTRPS116
	J = N + 1 - I	NTRPS117
	TEMP = XJ(I)	NTRPS118
	TEMS = YJ(I)	NTRPS119
	XJ(I) = XJ(J)	NTRPS120
	YJ(I) = YJ(J)	NTRPS121
	XJ(J) = TEMP	NTRPS122
	YJ(J) = TEMS	NTRPS123
260	CONTINUE	NTRPS124
262	RETURN	NTRPS125
270	WRITEOUTPUTTAPE6,2101	NTRPS126
2101	FORMAT (44H0 ERROR IN INPUT TO NTRPSR. M IS NEGATIVE. )	NTRPS127
	INSC = 1	NTRPS128
	GO TO 240	NTRPS129
272	H = (XMAX-XMIN)/FLOATF(MDIMM-MBEG)	NTRPS130
	WRITEOUTPUTTAPE6,2102,H	NTRPS131
2102	FORMAT (58H0 ERROR IN INPUT TO NTRPSR. MINIMUM ALLOWABLE SPACING	NTRPS132
	8IS 1PE12.3)	NTRPS133
	INSC = 1	NTRPS134
	GO TO 240	NTRPS135
274	WRITEOUTPUTTAPE6,2103,L	NTRPS136
2103	FORMAT (43H0 INTR1 WAS UNABLE TO INTERPOLATE IN RANGE I3)	NTRPS137
	GO TO 240	NTRPS138
100	NCON = 1	NTRPS139
	REFA = 1.414214	NTRPS140
	NFIN = NSTA + NUSED - 1	NTRPS141
	DO 98 I = NSTA,NFIN	NTRPS142
	XI(I) = XJ(I)	NTRPS143
	YI(I) = YJ(I)	NTRPS144
98	CONTINUE	NTRPS145
	NSTA1 = NSTA + 1	NTRPS146
	XSCALE = (XI(NFIN) - XI(NSTA))/10.	NTRPS147
	YMAX = YI(NSTA)	NTRPS148
	YMIN = YI(NSTA)	NTRPS149
1001	DO 1002 I = NSTA1,NFIN	NTRPS150
	YMAX = MAX1F(YMAX,YI(I))	NTRPS151
	YMIN = MIN1F(YMIN,YI(I))	NTRPS152
1002	CONTINUE	NTRPS153
91	YSCALE = YMAX - YMIN	NTRPS154
1003	DO 1004 I = NSTA,NFIN	NTRPS155
	XI(I) = XI(I)/XSCALE	NTRPS156
	YI(I) = (YI(I)-YMIN)/YSCALE + .5	NTRPS157
1004	CONTINUE	NTRPS158
	XH = ABSF(XN)/XSCALE	NTRPS159
	MFIN = MSTA + M - 1	NTRPS160
	MTA = MSTA	NTRPS161
1005	EPSIL = .01*XH	NTRPS162
101	DO 110 II = MTA,MFIN	NTRPS163
	XO(II) = XO(II)/XSCALE	NTRPS164
	YO(II) = 0.0	NTRPS165
	PNUM = 1.0	NTRPS166
1011	DO 107 I = NSTA,NFIN	NTRPS167
C	FIND XO(II)-XI(I) FOR NUMERATOR AND CHECK FOR NEARNESS.	NTRPS168
	XNUM = XO(II) - XI(I)	NTRPS169
1012	IF (ABSF(XNUM )-EPSIL) 102,102,103	NTRPS170
102	YO(II) = YI(I)	NTRPS171
	GO TO 109	NTRPS172
C	PNUM = PRODUCT OF ALL XNUM	NTRPS173

Table I. (Contd.)

C	103	PNUM = PNUM*XNUM	NTRPS174
		CONSTRUCT DENOMINATOR AND SUM	NTRPS175
		PDEN = 1.0	NTRPS176
	104	DO 106 J = NSTA,NFIN	NTRPS177
	1043	IF (I-J) 105,106,105	NTRPS178
	105	PDEN = (XI(I) - XI(J))*PDEN	NTRPS179
	1051	IF QUOTIENT OVERFLOW 1103,106	NTRPS180
	106	CONTINUE	NTRPS181
		DEN = PDEN*XNUM	NTRPS182
		YO(II) = YI(I)/DEN + YO(II)	NTRPS183
		IF ACCUMULATOR OVERFLOW 1121, 107	NTRPS184
	107	CONTINUE	NTRPS185
		YO(II) = YO(II)*PNUM	NTRPS186
	109	YO(II) = (YO(II)-.5)*YSCALE + YMIN	NTRPS187
		XO(II) = XO(II) * XSCALE	NTRPS188
	110	CONTINUE	NTRPS189
		INSC = 0	NTRPS190
		GO TO 246	NTRPS191
	1103	WRITEOUTPUTTAPE6,1104,NCON,XSCALE	NTRPS192
		WRITEOUTPUTTAPE6,1108,II,I,J	NTRPS193
	1104	FORMAT (8H NCON = I3, 11H, XSCALE = F10.7)	NTRPS194
	1108	FORMAT (26H OVERFLOW OCCURRED AT II= I4,4H I= I3,4H J= I3)	NTRPS195
		NCON = NCON + 1	NTRPS196
	1105	DO 1106 I = NSTA,NFIN	NTRPS197
		XI(I) = XI(I)/REFA	NTRPS198
	1106	CONTINUE	NTRPS199
		XO(II) = XO(II) * XSCALE	NTRPS200
		MTA = II	NTRPS201
		XH = XH /REFA	NTRPS202
		XSCALE = XSCALE*REFA	NTRPS203
		IF (NCON-8) 1005,1005,1107	NTRPS204
	1107	INSC = 1	NTRPS205
		GO TO 246	NTRPS206
	1121	WRITEOUTPUTTAPE6,1122	NTRPS207
	1122	FORMAT (48H0 ACCUMULATOR OVERFLOW. DEN MUST BE TOO SMALL. )	NTRPS208
		INSC = 1	NTRPS209
		GO TO 246	NTRPS210
		FREQUENCY 1051(1,9),1001(50),1003(50),101(500),1011(50),	NTRPS211
	1	1012(0,0,1),104(50),1043(1,0,1)	NTRPS212
		END	NTRPS213

Table I. (Contd.)

```

CNTRPDP  INTERPOLATION PROGRAM(BY SUCCESSIVE RANGES) DOUBLE PRECISION.  NTRPD000
C
C      THE METHOD OF LAGRANGE IS USED.  THE INPUT POINTS NEED NOT BE  NTRPD001
C      EQUALLY SPACED.  THERE ARE TWO MODES OF INPUT AVAILABLE.  THE  NTRPD002
C      FIRST OCCURS WHEN M = 0.  THE ABSCISSAE ARE THEN GENERATED FROM  NTRPD003
C      XMIN,XMAX,AND XH.  AT EXIT M = NO. OF POINTS FOUND, AND XO  NTRPD004
C      CONTAINS THE ABSCISSAE.  M WILL BE CHECKED TO INSURE THAT THE  NTRPD005
C      DIMENSION IS NOT EXCEEDED.  MDIMM = THE DIMENSION OF THE XO, YO  NTRPD006
C      ARRAYS.  THE SECOND MODE OCCURS WHEN M IS POSITIVE.  THE M  NTRPD007
C      ABSCISSAE ARE THEN ASSUMED TO HAVE BEEN GENERATED PRIOR TO  NTRPD008
C      ENTRY.  THE STARTING INDEX FOR THE OUTPUT ARRAY MUST BE  NTRPD009
C      SPECIFIED.  THE FIRST POINT FOUND WILL BE AT XO(MBEG).  XH MUST  NTRPD010
C      BE GIVEN SINCE THE ORDINATE FOR ANY POINT CLOSER THAN .01*XH TO  NTRPD011
C      AN INPUT POINT IS TAKEN AS THAT FOR THE INPUT POINT.  -NUSED- IS  NTRPD012
C      THE NUMBER OF POINTS USED FOR EACH INTERPOLATED POINT.  *NUSED*  NTRPD013
C      MUST BE EVEN AND LESS THAN OR EQUAL TO -N-.  NUSED = 8 IS  NTRPD014
C      SUGGESTED.  ANY POINT FARTHER THAN NUSED/2 POINTS FROM EITHER END  NTRPD015
C      IS FOUND FROM THE NUSED/2 ON EACH SIDE.  NTRPSR WILL SCALE AND  NTRPD016
C      RESCALE IN ORDER TO AVOID OVERFLOW.  IF THE FIRST SCALING DOES  NTRPD017
C      NOT SUCCEED, NTRPSR WILL TRY UP TO 7 TIMES MORE BEFORE RETURNING  NTRPD018
C      IN THE ERROR MODE.  (INSC = 1)  NTRPD019
C      INPUT IS XI,YI,(XO),XH,N,M,(XMIN),(XMAX),MBEG,NUSED.  NTRPD020
C      OUTPUT IS (XO),YO,INSC.  NTRPD021
C      INSC = 0 IF PROGRAM WAS SUCCESSFUL.  IF NOT, INSC = 1.  NTRPD022
C  NTRPD023
C  NTRPD024
SUBROUTINE NTRPDP(XJ,YJ,XO,YO,XN,N,K,XNIN,XNAX,INSC,MDEG,NUSED)  NTRPD025
D  DIMENSION XI(200),YI(200),XJ(200),YJ(200),XO(200),YO(200),XMIN(1),  NTRPD026
Z      XMAX(1),XNUM(1),EPSIL(1)  NTRPD027
D  DIMENSION NUMB(200)  NTRPD028
D  MDIMM = 200  NTRPD029
D  XMAX = XNAX  NTRPD030
D  XMIN = XNIN  NTRPD031
D  XH = XN  NTRPD032
D  M = K  NTRPD033
C  M IS ZERO, IF XH IS TO BE USED.  IF NOT, XH=(XMAX-XMIN)/(M-1).  NTRPD034
200 IF (M) 270,201,205  NTRPD035
D 201 M = INTF((XMAX - XMIN)/XH) + 1.  NTRPD036
C  IF M IS MORE THAN DIMENSION OF XO, RETURN IN ERROR MODE.  NTRPD037
202 IF (M+MBEG-MDIMM-2) 203,272,272  NTRPD038
203 MF = MBEG + M - 1  NTRPD039
D  DO 204 I = MBEG,MF  NTRPD040
D  XO(I) = FLOATF(I-MBEG) * XH + XMIN  NTRPD041
204 CONTINUE  NTRPD042
205 DO 206 I = 1,N  NTRPD043
D  XI(I) = XJ(I)  NTRPD044
206 CONTINUE  NTRPD045
D  MF = MBEG + M - 1  NTRPD046
D  MSTA = MBEG  NTRPD047
D  MUST = NUSED/2  NTRPD048
D  NS = MUST + 1  NTRPD049
D  NF = N - NS + 1  NTRPD050
D  NFP = NF + 1  NTRPD051
D  DO 207 I = NS,NFP  NTRPD052
D  NUMB(I) = 0  NTRPD053
207 CONTINUE  NTRPD054
209 IF (NF-NS) 236,210,210  NTRPD055
210 DO 226 J = MBEG,MF  NTRPD056
D  DO 224 I = NS,NF  NTRPD057

```



Table I. (Contd.)

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214	IF (XO(J) - XI(I))	216,215,224	NTRPD058
215	IF (XO(J+20) - XI(I+200))	216,216,224	NTRPD059
216	NUMB(I) = NUMB(I) + 1		NTRPD060
	GO TO 226		NTRPD061
224	CONTINUE		NTRPD062
	NUMB(NFP) = NUMB(NFP) + 1		NTRPD063
226	CONTINUE		NTRPD064
	GO TO 238		NTRPD065
236	NUMB(NFP) = M		NTRPD066
238	M = 0		NTRPD067
239	DO 250 L = NS,NFP		NTRPD068
	IF (NUMB(L))	250,250,242	NTRPD069
242	M = NUMB(L)		NTRPD070
	NSTA = L - NUST		NTRPD071
	GO TO 100		NTRPD072
246	IF (INSC)	274,248,274	NTRPD073
248	MSTA = MST A + M		NTRPD074
250	CONTINUE		NTRPD075
240	K = MST A - MBEG		NTRPD076
	RETURN		NTRPD077
270	WRITEOUTPUTTAPE6,2101		NTRPD078
2101	FORMAT (44H0 ERROR IN INPUT TO NTRPSR. M IS NEGATIVE. )		NTRPD079
	INSC = 1		NTRPD080
	GO TO 240		NTRPD081
272	H = (XMAX-XMIN)/FLOATF(MDIMM-MBEG)		NTRPD082
	WRITEOUTPUTTAPE6,2102,H		NTRPD083
2102	FORMAT (58H0 ERROR IN INPUT TO NTRPSR. MINIMUM ALLOWABLE SPACING		NTRPD084
	8IS 1PE12.3)		NTRPD085
	INSC = 1		NTRPD086
	GO TO 240		NTRPD087
274	WRITEOUTPUTTAPE6,2103,L		NTRPD088
2103	FORMAT (43H0 INTR1 WAS UNABLE TO INTERPOLATE IN RANGE I3)		NTRPD089
	GO TO 240		NTRPD090
100	NCON = 1		NTRPD091
	REFA = 1.414214		NTRPD092
	NFIN = NSTA + NUSED - 1		NTRPD093
	DO 98 I = NSTA,NFIN		NTRPD094
D	XI(I) = XJ(I)		NTRPD095
D	YI(I) = YJ(I)		NTRPD096
98	CONTINUE		NTRPD097
	NSTA1 = NSTA + 1		NTRPD098
	XSCALE = (XI(NFIN) - XI(NSTA))/10.		NTRPD099
	YMAX = YI(NSTA)		NTRPD100
	YMIN = YI(NSTA)		NTRPD101
1001	DO 1002 I = NSTA1,NFIN		NTRPD102
	YMAX = MAX1F(YMAX,YI(I))		NTRPD103
	YMIN = MIN1F(YMIN,YI(I))		NTRPD104
1002	CONTINUE		NTRPD105
D 91	YSCALE = YMAX - YMIN		NTRPD106
1003	DO 1004 I = NSTA,NFIN		NTRPD107
D	XI(I) = XI(I)/XSCALE		NTRPD108
D	YI(I) = (YI(I)-YMIN)/YSCALE + .5		NTRPD109
1004	CONTINUE		NTRPD110
D	XH = XN /XSCALE		NTRPD111
	MFIN = MST A + M - 1		NTRPD112
	MTA = MST A		NTRPD113
D1005	EPSIL = .01*XH		NTRPD114
101	DO 110 II = MTA,MFIN		NTRPD115

Table I. (Contd.)

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D	XO(II) = XO(II)/XSCALE	NTRPD116
D	YO(II) = 0.0	NTRPD117
D	PNUM = 1.0	NTRPD118
1011	DO 107 I = NSTA,NFIN	NTRPD119
C	FIND XO(II)-XI(I) FOR NUMERATOR AND CHECK FOR NEARNESS.	NTRPD120
D	XNUM = XO(II) - XI(I)	NTRPD121
1012	IF (ABSF(XNUM )-EPSIL) 102,1013,103	NTRPD122
1013	IF (ABSF(XNUM(2))-EPSIL(2)) 102,102,103	NTRPD123
D 102	YO(II) = YI(I)	NTRPD124
	GO TO 109	NTRPD125
C	PNUM = PRODUCT OF ALL XNUM	NTRPD126
D 103	PNUM = PNUM*XNUM	NTRPD127
C	CONSTRUCT DENOMINATOR AND SUM	NTRPD128
D	PDEN = 1.0	NTRPD129
104	DO 106 J = NSTA,NFIN	NTRPD130
1043	IF (I-J) 105,106,105	NTRPD131
D 105	PDEN = (XI(I) - XI(J))*PDEN	NTRPD132
1051	IF QUOTIENT OVERFLOW 1103,106	NTRPD133
106	CONTINUE	NTRPD134
D	DEN = PDEN*XNUM	NTRPD135
D	YO(II) = YI(I)/DEN + YO(II)	NTRPD136
	IF ACCUMULATOR OVERFLOW 1121, 107	NTRPD137
107	CONTINUE	NTRPD138
D	YO(II) = YO(II)*PNUM	NTRPD139
D 109	YO(II) = (YO(II)-.5)*YSCALE + YMIN	NTRPD140
D	XO(II) = XO(II) * XSCALE	NTRPD141
110	CONTINUE	NTRPD142
	INSC = 0	NTRPD143
	GO TO 246	NTRPD144
1103	WRITEOUTPUTTAPE6,1104,NCON,XSCALE	NTRPD145
	WRITEOUTPUTTAPE6,1108,II,I,J	NTRPD146
1104	FORMAT (8H NCON = I3, 11H, XSCALE = F10.7)	NTRPD147
1108	FORMAT (26H OVERFLOW OCCURRED AT II= I4,4H I= I3,4H J= I3)	NTRPD148
	NCON = NCON + 1	NTRPD149
1105	DO 1106 I = NSTA,NFIN	NTRPD150
D	XI(I) = XI(I)/REFA	NTRPD151
1106	CONTINUE	NTRPD152
D	XO(II) = XO(II) * XSCALE	NTRPD153
	MTA = II	NTRPD154
D	XH = XH /REFA	NTRPD155
D	XSCALE = XSCALE*REFA	NTRPD156
	IF (NCON-8) 1005,1005,1107	NTRPD157
1107	INSC = 1	NTRPD158
	GO TO 246	NTRPD159
1121	WRITEOUTPUTTAPE6,1122	NTRPD160
1122	FORMAT (48H0 ACCUMULATOR OVERFLOW. DEN MUST BE TOO SMALL. )	NTRPD161
	INSC = 1	NTRPD162
	GO TO 246	NTRPD163
	FREQUENCY 1051(1,9),1001(50),1003(50),101(500),1011(50),	NTRPD164
1	1012(0,0,1),104(50),1043(1,0,1)	NTRPD165
	END	NTRPD166

Table I. (Contd.)

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CDGUNC	FINDS G(V) - G(V-X)	DGUNC000
	SUBROUTINE DGUNC (XG,DENQ,NGAS,TEMPI)	DGUNC001
D	DIMENSION XG(20),DENQ(20)	DGUNC002
	DIMENSION UEV(3000),EV(3000),BV(200),BI(3000),TEMP(200),U(200),	DGUNC003
Z	Y(200),Z(200)	DGUNC004
	COMMON Y,TEMP,UEV,EV,Q,NST,N,MST,M,XMIN,XMAX,INSC,MBEG,NUST,BI,	DGUNC005
Z	NI,NS,MAXIT,FACM,ZMU,DE,WE,WEXE,WEYE,WEZE,WETE,BE,ALPHAE,	DGUNC006
Z	GAMMAE,DELTAE, VNIN,BQ,MQ,SPEP, U,BV,Z,ICK,H, K,HDES	DGUNC007
Z	,EPSLNE	DGUNC008
	V = TEMPI	DGUNC009
	VA = V*V	DGUNC010
	VB = VA*V	DGUNC011
	VC = VB*V	DGUNC012
205	DO 210 I = 1,NGAS	DGUNC013
D	Y = TEMPI - XG(I)	DGUNC014
	X = Y	DGUNC015
	XA = X*X	DGUNC016
	XB = XA*X	DGUNC017
	XC = XB*X	DGUNC018
	DENQ(I) = WE*X + (XA-2.*V*X)*WEXE + ((VA*X-V*XA)*3.+XB) * WEYE	DGUNC019
Z	+ ((VB*X+V*XB)*4.-6.*VA*XA-XC) * WEZE	DGUNC020
Z	+ ((VC*X-V*XC)*5.+(VA*XB-VB*XA)*10.) * WETE	DGUNC021
210	CONTINUE	DGUNC022
	RETURN	DGUNC023
	END	DGUNC024

CTIME		TIME 000
C	DISCARD THIS SUBROUTINE IF YOUR 709/7090/7094 INSTALLATION HAS	TIME 001
C	AN ON-LINE CLOCK ADDRESSABLE BY CALL TIME(X)	TIME 002
	SUBROUTINE TIME(X)	TIME 003
1	X = 0.0	TIME 004
	RETURN	TIME 005
	END	TIME 006

---

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Table II. Sample data deck for RKR program.

---

---

```
*      DATA
1
1 RKR PROCEDURE APPLIED TO THE X STATE OF SILICON NITRIDE   TEST PROGRAM
  MOLECULAR CONSTANTS ARE TAKEN FROM JENKINS AND DE LASZLO
  2 9.33526
  1 10   (42H TURNING POINTS ARE GENERATED BY CONSTANTS)
1151.680 6.560
2
  1 10   (42H TURNING POINTS ARE GENERATED BY CONSTANTS)
0.7310  0.00567
2
1.5718
0.5      9.5      1.0
```

---

---

## PROGRAM FOR CALCULATING RELATIVE INTENSITIES

Remarks

The input to this program is extremely flexible. The potential may be generated by subroutine POTGEN or may be read in. The output is Franck-Condon factors, relative intensities (quantum/sec) scaled to ten, relative intensities (energy/sec) scaled to ten, and the off-diagonal matrix elements  $\langle v'J' | r | v''J'' \rangle / \langle v'J' | v''J'' \rangle$  and  $\langle v'J' | r^2 | v''J'' \rangle / \langle v'J' | v''J'' \rangle$ , commonly known as the r-centroid and the square of the r-centroid. The heart of this program is subroutine SCHR which solves the radial Schrödinger equation for its eigenvalues and wavefunctions. This program has been described in detail elsewhere.<sup>3</sup> About 0.9 min is required to calculate all the above-named quantities for ten vibrational levels of the lower state with four vibrational levels of the upper state.<sup>2</sup>

Limitations

Presently the program will calculate at one time the Franck-Condon factors, etc., of only four specified vibrational levels of the upper state with the vibrational levels of the lower state. Also the same (J', J'') pair must be used for each transition. This is due to lack of additional space in core storage. The program may be easily modified to allow more flexible usage.

Listing

Table III lists the source decks and Table IV gives a sample data deck for the relative-intensity program.

Table III. Source-deck listing for relative-intensity program.

```

CMAIN COMPUTES INTENSITY DISTRIBUTION FOR ELECTRONIC TRANSITIONS.      MAIN 000
C THIS PROGRAM USES D2 NU SCHR AND SIMPSONS RULE TO FIND                MAIN 001
C THE FRANCK CONDON OVERLAP FACTORS AND CORRECTS FOR                   MAIN 002
C FREQUENCY DEPENDENCE AND SCALES TO TEN.                             MAIN 003
C THE POTENTIAL MAY BE GENERATED INTERNALLY. OTHERWISE                MAIN 004
C POINTS ON THE POTENTIAL CURVE ARE READ IN. THEY ARE INTERPOLATED    MAIN 005
C TO ANY DESIRED SPACING (LESS THAN 2000 POINTS). D2 NU SCHR          MAIN 006
C IS USED TO FIND THE ENERGY LEVELS. NTRPSR IS USED TO INTERPOLATE   MAIN 007
C THE GIVEN POTENTIAL POINTS. THE 2 POINTS AT SMALLEST R ARE         MAIN 008
C FITTED EXACTLY TO A FUNCTION OF THE FORM A/X**12+ C. SIMILARLY      MAIN 009
C THE TWO POINTS AT GREATEST R ARE FITTED EXACTLY TO A FUNCTION OF   MAIN 010
C THE FORM A/X**B. THESE ARE THEN USED TO EXTRAPOLATE THE            MAIN 011
C POTENTIAL TO THE GIVEN LIMITS. A SUBROUTINE POTGEN MUST BE         MAIN 012
C INCLUDED. THIS WILL COMPUTE THE POTENTIAL CURVE OR WILL BE A       MAIN 013
C DUMMY TO SATISFY ENTRY REQUIREMENTS.                                MAIN 014
C                                                                        MAIN 015
C DIMENSION XI(200,2),YI(200,2),XO(2000),V(2000,2),S(2000)          MAIN 016
Z      ,SU(2000,4),ETRIAL(200,2) ,QIRA(2),QIEN(3),QIMS(2)            MAIN 017
Z      ,ZIMS(2),ZIRA(2),ZIEN(3),ECALC(200,2),XPRN(5),VPRN(5)        MAIN 018
Z      ,DTFRMT(10),DUFMT(10),BVF(100,2),RESULT(100,4)             MAIN 019
Z      ,KV(100,2),N(2),NL(2),DE(2),PRFMT(10),PNFT(4)               MAIN 020
Z      ,DIV(4),WE(2),RE(2),RCNTRD(100,4),RRCN(100,4)              MAIN 021
Z      ,DDIV(4)                                                      MAIN 022
C COMMON XI,YI,XO,V,XH,NSTÄ,N,MSTA,M,XMIN,XMAX,INSC,MBEG,NUSED,S,    MAIN 023
Z      NI,NS,MAXIT,FACM,ZMU,DE,WE,WEXE,SU                          MAIN 024
C                                                                        MAIN 025
C THE FOLLOWING COMMENT CARDS DESCRIBE THE PREPARATION OF DATA.     MAIN 026
C                                                                        MAIN 027
C FIRST CARD IN DATA HAS A ONE IN COLUMN 1 IF A PROBLEM FOLLOWS.   MAIN 028
C VERY LAST CARD IN DATA MUST BE A BLANK CARD.....                MAIN 029
C                                                                        MAIN 030
C 1 CALL TIME(BEGIN)                                                 MAIN 031
C WRITEOUTPUTTAPE6,160,BEGIN                                         MAIN 032
C 160 FORMAT (9H0 TIME = F10.5)                                       MAIN 033
C READINPUTTAPE5,100,ITEST                                           MAIN 034
C 100 FORMAT (I1)                                                     MAIN 035
C 2 IF (ITEST) 3,400,3                                               MAIN 036
C                                                                        MAIN 037
C NEXT CARD IN DATA HAS NAME OF PROBLEM IN COLUMNS 1-72, WHERE    MAIN 038
C CARRIAGE CONTROL IS IN COLUMN 1. SECOND CARD HAS IIMS AND         MAIN 039
C MASSES OF THE TWO ATOMS.                                           MAIN 040
C IF ZMAS2 = 0, ZMAS1 IS TAKEN AS THE REDUCED MASS IN THE IIMS UNITS MAIN 041
C IIMS = 1, MASS UNITS ARE BASED ON C12 = 12..                       MAIN 042
C IIMS = 2, MASS UNITS ARE BASED ON O16 = 16.                         MAIN 043
C                                                                        MAIN 044
C 3 READINPUTTAPE5,101                                               MAIN 045
C 101 FORMAT (72H1 PROBLEM NAME DATE                                  MAIN 046
Z      )                                                              MAIN 047
C READINPUTTAPE5,102,IIMS,ZMAS1,ZMAS2                                MAIN 048
C 102 FORMAT (I4,2F10.0)                                             MAIN 049
C                                                                        MAIN 050
C NEXT CARD IN DATA HAS IIRA, IIEN, AND THE NUMBER OF POINTS, EACH MAIN 051
C IN I4 FORMAT, AS WELL AS THE FORMAT STATEMENT WHICH CONTROLS THE MAIN 052
C READING OF THE POINTS (IN COLUMNS 13-72)--FOR EXAMPLE- (4E16.8). MAIN 053
C IIEN = 1, ENERGY IS IN ATOMIC UNITS. (1 A.U. = 27.1961 E.V.)    MAIN 054
C IIEN = 2, ENERGY IS IN 1/CM.                                       MAIN 055
C IIEN = 3, ENERGY IS IN ELECTRON VOLTS. (1 E.V. = 8065.68 1/CM) MAIN 056
C IIRA = 1, DISTANCE IS IN ATOMIC UNITS. (1 A.U. = .529166 ANG.)    MAIN 057

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Table III. (Contd.)

C	IIRA = 2, DISTANCE IS IN ANGSTROMS.	MAIN 058
C	FOLLOWING CARDS CONTAIN THE INPUT POTENTIAL POINTS.	MAIN 059
C	IF IT IS DESIRED TO USE A FUNCTION TO GENERATE THE WHOLE	MAIN 060
C	POTENTIAL CURVE, THE FIRST 12 COLUMNS OF THE IIPA, ETC. CARD	MAIN 061
C	MUST BE BLANK. A HOLLERITH TEXT MUST BE PUNCHED IN 13-72, AS	MAIN 062
C	IT WILL BE PRINTED. THE NEXT CARD IN SUCH A CASE CONTAINS	MAIN 063
C	XMIN,XMAX,ETC.	MAIN 064
C	FIRST TIME THROUGH IS THE GROUND STATE	MAIN 065
C	THE SECOND TIME THROUGH IS THE UPPER STATE	MAIN 066
C	A MAXIMUM OF FOUR LEVELS OF THE UPPER STATE CAN BE USED IN	MAIN 067
C	COMPUTING INTENSITIES AT ONE TIME.	MAIN 068
C	THE SAME VALUE OF IIEEN,IIRA,NDE,XH,XMIN,XMAX,IIRA1,NEI	MAIN 069
C	,IIEEN1 MUST BE USED FOR BOTH THE GROUND AND UPPER STATE	MAIN 070
C		MAIN 071
	IKON = 1	MAIN 072
	5 READINPUTTAPES,103,IIRA,IIEEN,N(IKON),(DTFRMT(I),I=1,10)	MAIN 073
103	FORMAT (3I4, 10A6)	MAIN 074
	6 IF (IIRA) 7,8,7	MAIN 075
	7 NIKON = N(IKON)	MAIN 076
	READINPUTTAPES,DTFRMT,(XI(I,IKON),YI(I,IKON),I=1,NIKON)	MAIN 077
C		MAIN 078
C	NEXT CARD CONTAINS NDE AND THE DISSOCIATION ENERGY WHERE NDE IS	MAIN 079
C	ZERO IF ZERO PT OF POTENTIAL CURVE IS AT R=INFINITY, OR ONE IF AT	MAIN 080
C	R=REQUILIBRIUM. DISSOCIATION ENERGY HAS SAME UNITS AS POTENTIAL.	MAIN 081
C		MAIN 082
	READINPUTTAPES,105,NDE,DE(IKON)	MAIN 083
105	FORMAT (I4,F10.0)	MAIN 084
	GO TO 17	MAIN 085
C		MAIN 086
C	NEXT DATA CARD CONTAINS XMIN,XMAX,XH,IIRA, WHERE IIRA GIVES THE	MAIN 087
C	UNITS FOR THE MIN AND MAX DISTANCES AND THE SPACING XH.	MAIN 088
C		MAIN 089
	8 READINPUTTAPES,104,DE(IKON),WE(IKON),RE(IKON)	MAIN 090
	17 READINPUTTAPES,104,XMIN,XMAX,XH,IIRA1	MAIN 091
104	FORMAT(3F10.0,I4)	MAIN 092
C		MAIN 093
C	NEXT CARD HAS NO. AND IIEEN OF EXPECTED ENERGY LEVELS, AND NET	MAIN 094
C	WHICH HAS THE SAME INTERPRETATION FOR ETRIAL(I) AS NDE DOES FOR	MAIN 095
C	THE POTENTIAL CURVE ABOVE.	MAIN 096
C	IT ALSO CONTAINS THE VARIABLE FORMAT FOR READING ENERGY LEVELS	MAIN 097
C		MAIN 098
	READINPUTTAPES,106,NL(IKON),IIEEN1,NET,(DUFMT(I),I=1,10)	MAIN 099
106	FORMAT (3I4, 10A6)	MAIN 100
	IF (NL) 15,15,14	MAIN 101
	14 NLIKON = NL(IKON)	MAIN 102
C		MAIN 103
C	READ IN ENERGY LEVELS	MAIN 104
C		MAIN 105
	READINPUTTAPES,DUFMT,(KV(I,IKON),ETRIAL(I,IKON),I=1,NLIKON)	MAIN 106
C		MAIN 107
C	GO BACK TO STATEMENT 5 AND READ IN UPPER STATE	MAIN 108
C		MAIN 109
	15 GO TO (1501,1502), IKON	MAIN 110
1501	IKON = 2	MAIN 111
	GO TO 5	MAIN 112
C		MAIN 113
C	AFTER BOTH THE LOWER AND UPPER STATES ARE READ IN,	MAIN 114
C	D2 NU SCHR MODIFIED FOR THE 709/7090/7094 IS DESCRIBED IN	MAIN 115

Table III. (Contd.)

C	R. N. ZARE AND J. K. CASHION, UCRL-10881, 1963	MAIN 116
C	FOR THIS PROGRAM THE CONSTANTS ARE USED AS FOLLOWS	MAIN 117
C	IF NI = 1, PRINTS ITERATIONS, OTHERWISE NOT	MAIN 118
C	IF NS = 1, PRINTS WAVEFUNCTION EVERY IPSIQ POINTS, OTHERWISE NOT	MAIN 119
C	IF NS = 33, PRINTS EIGENVALUES AND NODE COUNT	MAIN 120
C	EPS IS THE CONVERGENCE CRITERION	MAIN 121
C	EPS IS IN THE SAME UNITS AS THE POTENTIAL CURVE	MAIN 122
C	MAXIT IS THE MAXIMUM NUMBER OF TIMES SCHR WILL TRY TO SATISFY THE	MAIN 123
C	CONVERGENCE CRITERION	MAIN 124
C		MAIN 125
1502	LLIM = 100	MAIN 126
	KLIM = 2	MAIN 127
	READ INPUT TAPE 5,107,NI,NS,IPSIQ,MAXIT,EPS	MAIN 128
107	FORMAT(4I4,E10.0)	MAIN 129
C		MAIN 130
C	NEXT TWO CARDS ARE THE VALUES OF J FOR THE LOWER AND UPPER STATE	MAIN 131
C		MAIN 132
	READINPUTTAPE5,144,JROTL,JROTU	MAIN 133
144	FORMAT(I3)	MAIN 134
C		MAIN 135
C	NEXT SIX CARDS ARE THE ROTATIONAL CONSTANTS, BE, ALPHAE, GAMMAE,	MAIN 136
C	FOR THE LOWER AND UPPER STATES.	MAIN 137
C	THE ROTATIONAL CONSTANTS ARE IN WAVE NUMBERS	MAIN 138
C		MAIN 139
	READ INPUT TAPE 5,2000,BE1,AE1,GE1,BE2,AE2,GE2	MAIN 140
2000	FORMAT(E20.8)	MAIN 141
C		MAIN 142
C	NEXT DATA CARD CONTAINS TE, OR THE CORRESPONDING QUANTITY IF THE	MAIN 143
C	FIRST POTENTIAL IS NOT THE GROUND STATE. TE IS IN WAVE NUMBERS	MAIN 144
C		MAIN 145
	READ INPUT TAPE 5,2000,TE	MAIN 146
C		MAIN 147
C	NEXT CARD CONTAINS NPOT.	MAIN 148
C	THE POTENTIAL IS PRINTED AT EVERY NPOT POINT.	MAIN 149
C	NPOT = 5 IS SUGGESTED TO THE USER.	MAIN 150
C		MAIN 151
	READ INPUT TAPE 5,144,NPOT	MAIN 152
C		MAIN 153
C	THIS TERMINATES COMMENT CARDS ON THE PREPARATION OF DATA.	MAIN 154
C	IF NO FURTHER PROBLEMS FOLLOW, REMEMBER TO ADD A BLANK CARD TO THE	MAIN 155
C	DATA DECK	MAIN 156
C		MAIN 157
C		MAIN 158
	QIRA(1) = 6HA.U.	MAIN 159
	QIRA(2) = 6HANGST.	MAIN 160
	QIEN(1) = 6HA.U.	MAIN 161
	QIEN(2) = 6H1/CM	MAIN 162
	QIEN(3) = 6HE.V.	MAIN 163
	QIMS(1) = 6HC12=12	MAIN 164
	QIMS(2) = 6H016=16	MAIN 165
	PRFMT(1) = 6H(1H06X	MAIN 166
	PRFMT(2) = 6H3HV--4	MAIN 167
	PRFMT(3) = 6H(11X5H	MAIN 168
	PRFMT(4) = 6HV- = I	MAIN 169
	PRFMT(5) = 6H3,11X)	MAIN 170
	PRFMT(6) = 3H//)	MAIN 171
	PNFT(1) = 6H3HV--1	MAIN 172
	PNFT(2) = 6H3HV--2	MAIN 173



Table III. (Contd.)

	PNFT(3) = 6H3HV--3	MAIN 174
	PNFT(4) = 6H3HV--4	MAIN 175
C		MAIN 176
C	OUTPUT IS IN WAVE NUMBERS AND ANGSTROMS	MAIN 177
C	PRINT HEADING	MAIN 178
C		MAIN 179
	WRITEOUTPUTTAPE6,101	MAIN 180
C		MAIN 181
C	PRINT THE MASSES AND THEIR UNITS.	MAIN 182
C		MAIN 183
	10 IF (7MAS2) 12,12,11	MAIN 184
	11 WRITEOUTPUTTAPE6,121,QIMS(IIMS),ZMAS1,ZMAS2	MAIN 185
	121 FORMAT (////40H THE MASSES OF THE TWO ATOMS, BASED ON A6, 6H, ARE	MAIN 186
	Z F10.6, 5H AND F10.6///)	MAIN 187
	GO TO 20	MAIN 188
	12 WRITEOUTPUTTAPE6,111,QIMS(IIMS),ZMAS1	MAIN 189
	111 FORMAT (////46H THE REDUCED MASS OF THE TWO ATOMS, BASED ON A6,	MAIN 190
	Z 5H, IS F10.6///)	MAIN 191
		MAIN 192
C	PRINT THE INPUT POTENTIAL, THE DISSOCIATION ENERGY, AND UNITS,	MAIN 193
C	IF READ IN.	MAIN 194
C		MAIN 195
C		MAIN 196
	IKON = 1	MAIN 197
	20 IF (IIRA) 21,22,21	MAIN 198
	21 WRITEOUTPUTTAPE6,122,QIRA(IIRA),QIEN(IIEN)	MAIN 199
	122 FORMAT (35H THE INPUT POTENTIAL POINTS, R IN A6, 15H AND ENERGY I	MAIN 200
	ZN A6, 18H, ARE GIVEN BELOW. // 1X 5(6X1HR10X1HV4X) //)	MAIN 201
	NIKON = N(IKON)	MAIN 202
	WRITEOUTPUTTAPE6,114,(XI(I,IKON),YI(I,IKON),I=1,NIKON)	MAIN 203
	114 FORMAT (1X F10.6,F12.4,F10.6,F12.4,F10.6,F12.4,F10.6,F12.4,	MAIN 204
	Z F10.6,F12.4)	MAIN 205
	WRITEOUTPUTTAPE6,123,DE(IKON)	MAIN 206
	123 FORMAT (47HC DISSOCIATION ENERGY IN SAME UNITS AS ABOVE IS E20.8)	MAIN 207
	GO TO 23	MAIN 208
	22 WRITEOUTPUTTAPE6,127	MAIN 209
	127 FORMAT (50H THE POTENTIAL FUNTION IS GENERATED INTERNALLY. )	MAIN 210
	WRITEOUTPUTTAPE6,DTRMT	MAIN 211
C		MAIN 212
C	PRINT RMIN, RMAX, THE SPACING, AND THE UNITS.	MAIN 213
C		MAIN 214
	23 WRITEOUTPUTTAPE6,124,XMIN,XMAX,XH,QIRA(IIRA1)	MAIN 215
	124 FORMAT (//// 9H RMIN = F10.7, 9H, RMAX = F10.7, 12H, SPACING =	MAIN 216
	Z F10.7, 9H, ALL IN A6)	MAIN 217
C		MAIN 218
C	PRINT THE TRIAL ENERGY LEVELS AND THEIR UNITS.	MAIN 219
C		MAIN 220
	IF (NL) 25,25,24	MAIN 221
	24 NLIKON = NL(IKON)	MAIN 222
	WRITEOUTPUTTAPE6,125,QIEN(IIEN1),(KV(I,IKON),ETRIAL(I,IKON),I=1,NL	MAIN 223
	1IKON)	MAIN 224
	125 FORMAT (////29H THE TRIAL ENERGY LEVELS IN A6,16HARE GIVEN BELOW.	MAIN 225
	Z //1X 5(5HLEVEL3X6HENERGY6X)// (1H I4,1PE16.7,I4,E16.7,	MAIN 226
	Z I4,E16.7,I4,E16.7,I4,E16.7))	MAIN 227
	GO TO 18	MAIN 228
	25 WRITEOUTPUTTAPE6,161,DE(IKON),WE(IKON),RE(IKON)	MAIN 229
	161 FORMAT (7H DE = F10.2,7H, WE = F10.3,11H, AND RE = F10.6)	MAIN 230
C		MAIN 231
C	PRINT THE CONVERGENCE CRITERION.	MAIN 231

Table III. (Contd.)

C	18 GO TO (1801,1802),IKON	MAIN 232
	1801 IKON = 2	MAIN 233
	GO TO 20	MAIN 234
	1802 WRITEOUTPUTTAPE6,126,EPS,QIEN(IIEN)	MAIN 235
	126 FORMAT (////43H CONVERGENCE CRITERION IS ERROR LESS THAN E9.2,	MAIN 236
	Z 2XA6)	MAIN 237
C		MAIN 238
C	PRINT HEADING	MAIN 239
	WRITEOUTPUTTAPE6,101	MAIN 240
C		MAIN 241
	200 IF (ZMAS2) 201,201,202	MAIN 242
	201 ZMU = ZMAS1	MAIN 243
	GO TO 204	MAIN 244
	202 ZMU = ZMAS1*ZMAS2/(ZMAS1+ZMAS2)	MAIN 245
	204 ZIMS(1) = 1.0	MAIN 246
	ZIMS(2) = .9996784	MAIN 247
	ZIRA(1) = 1.0	MAIN 248
	ZIRA(2) = 1.889766	MAIN 249
	ZMU = ZMU * ZIMS(IIMS)	MAIN 250
	ZIEN(1) = ZMU * 3.643668E3	MAIN 251
	ZIEN(2) = ZMU * 1.6610826E-2	MAIN 252
	ZIEN(3) = ZMU * 1.339776E2	MAIN 253
	FACM = 60.201702/ZMU	MAIN 254
	IPOTGN = 0	MAIN 255
	N2 = N(2)	MAIN 256
	NL2 = NL(2)	MAIN 257
	210 IF (IIRA) 214,212,214	MAIN 258
C	POTGEN MUST GENERATE THE ENTIRE POTENTIAL CURVE. IN ADDITION,	MAIN 259
C	IT MUST SET THE VALUES OF IIRA,IIEN,M,NDE, AND DE. NDE WILL BE	MAIN 260
C	USED TO SET THE HEIGHT OF THE POTENTIAL CURVE.	MAIN 261
	212 CALL POTGEN (IPOTGN,DE,NDE,IIRA,IIEN,RE,ETRIAL,KV,NL,IIEN1,NET,WE,	MAIN 262
	1ZMU,XMAX,XMIN,XH,FACM,XO,V,M)	MAIN 263
	IF (IPOTGN-10) 213,213,1	MAIN 264
	213 CALL POTGEN(IPOTGN,DE(2),NDE,IIRA,IIEN,RE(2),ETRIAL(1,2),KV(1,2),	MAIN 265
	1NL(2),IIEN1,NET,WE(2),ZMU,XMAX,XMIN,XH,FACM,XO,V(1,2),M)	MAIN 266
	IF (IPOTGN - 10) 226,226,1	MAIN 267
	214 DO 216 I = 1,N	MAIN 268
	YI(I) = YI(I)*ZIEN(IIEN)	MAIN 269
	XI(I) = XI(I)*ZIRA(IIRA)	MAIN 270
	216 CONTINUE	MAIN 271
	DE = DE*ZIEN(IIEN)	MAIN 272
	DE(2) = DE(2)*ZIEN(IIEN)	MAIN 273
	220 DO 222 I = 1,N2	MAIN 274
	YI(I,2) = YI(I,2) *ZIEN(IIEN)	MAIN 275
	XI(I,2) = XI(I,2)*ZIRA(IIRA)	MAIN 276
	222 CONTINUE	MAIN 277
	226 XMIN = XMIN*ZIRA(IIRA1)	MAIN 278
	XMAX = XMAX*ZIRA(IIRA1)	MAIN 279
	XH = XH *ZIRA(IIRA1)	MAIN 280
	EPS = EPS * ZIEN(IIEN)	MAIN 281
	NL2 = NL(2)	MAIN 282
	DO 235 I = 1,NL2	MAIN 283
	ETRIAL(I,2) = ETRIAL(I,2)*ZIEN(IIEN1)	MAIN 284
	235 CONTINUE	MAIN 285
	236 DO 238 I = 1,NL	MAIN 286
	ETRIAL(I) = ETRIAL(I)*ZIEN(IIEN1)	MAIN 287
	238 CONTINUE	MAIN 288
		MAIN 289

Table III. (Contd.)

C	CHECK FOR RESCALING OF POTENTIAL TO ZERO AT R=INFINITY	MAIN 290
239	IF (NDE) 308,244,240	MAIN 291
240	IF (IPOTGN) 244,241,244	MAIN 292
241	DO 242 I = 1,N	MAIN 293
	YI(I) = YI(I) - DE	MAIN 294
242	CONTINUE	MAIN 295
	DO 243 I = 1,N2	MAIN 296
	YI(I,2) = YI(I,2) - DE(2)	MAIN 297
243	CONTINUE	MAIN 298
244	IF (NET) 300,247,245	MAIN 299
245	DO 246 I = 1,NL	MAIN 300
	ETRIAL(I) = ETRIAL(I)-DE+(BE1-AE1*(FLOATF(I-1)+.5)+GE1*(FLOATF(I-1	MAIN 301
	1)+.5)**2)*FLOATF(JROTL*(JROTL+1))/FACM	MAIN 302
246	CONTINUE	MAIN 303
	DO 2461 I = 1,NL2	MAIN 304
	ETRIAL(I,2) = ETRIAL(I,2)-DE(2)+(BE2-AE2*(FLOATF(I-1)+.5)+GE2*(FLO	MAIN 305
	1ATF(I-1)+.5)**2)*FLOATF(JROTU*(JROTU+1))/FACM	MAIN 306
2461	CONTINUE	MAIN 307
247	DO 248 I = 1,NL	MAIN 308
	ECALC(I) = ETRIAL(I)	MAIN 309
248	CONTINUE	MAIN 310
	DO 2481 I = 1,NL2	MAIN 311
	ECALC(I,2) = ETRIAL(I,2)	MAIN 312
2481	CONTINUE	MAIN 313
	IF (IPOTGN) 250,249,250	MAIN 314
249	NUSED = 8	MAIN 315
	CALL TIME(AFTER)	MAIN 316
	XTIQ = 60. * (AFTER-BEGIN)	MAIN 317
	BEGIN = AFTER	MAIN 318
	WRITEOUTPUTTAPE6,131,XTIQ	MAIN 319
131	FORMAT (23HO TIME BEFORE POTFIT = F10.5)	MAIN 320
	IKON = 1	MAIN 321
2490	CALL POTFIT(XI(1,IKON),YI(1,IKON),N(1,IKON),XO,V(1,IKON),M,XH,	MAIN 322
	Z XMIN,XMAX,INSC,NUSED,FACM)	MAIN 323
	IF (INSC) 1,2491,1	MAIN 324
2491	CALL TIME(AFTER)	MAIN 325
	XTIQ = 60. * (AFTER-BEGIN)	MAIN 326
	BEGIN = AFTER	MAIN 327
	WRITEOUTPUTTAPE6,132,XTIQ	MAIN 328
132	FORMAT (20HO TIME FOR POTFIT = F10.5)	MAIN 329
		MAIN 330
C	PRINT THE POTENTIAL CURVE GENERATED (ANGSTROMS AND 1/CM)	MAIN 331
250	WRITEOUTPUTTAPE6,108	MAIN 332
108	FORMAT (37HO THE POTENTIAL FUNCTION GENERATED IS ///	MAIN 333
	Z 1X 5(3X 4HR(A) 6X 7HV(1/CM) 2X))	MAIN 334
252	NPOT4 = NPOT*4	MAIN 335
	NPOT5 = NPOT*5	MAIN 336
254	DO 270 I = 1,M,NPOT5	MAIN 337
256	IF (M-I-NPOT4) 258,262,262	MAIN 338
258	JFIN = (M-I)/NPOT	MAIN 339
260	IF (JFIN) 272,272,264	MAIN 340
262	JFIN = 5	MAIN 341
264	DO 266 J = 1,JFIN	MAIN 342
	IPRN = I + NPOT*(J-1)	MAIN 343
	XPRN(J) = XO(IPRN)*.529166	MAIN 344
	VPRN(J) = (V(IPRN,IKON)+DE(1,IKON))*FACM	MAIN 345
266	CONTINUE	MAIN 346
	IF (VPRN(1) - 1.E6) 268,269,269	MAIN 347

Table III. (Contd.)

269	WRITEOUTPUTTAPE6,141,(XPRN(J),VPRN(J),J=1,JFIN),IPRN	MAIN 348
141	FORMAT (1XOPF10.6,1PE12.5,4(OPF10.6,1PE12.5),4XI5)	MAIN 349
	GO TO 270	MAIN 350
268	WRITEOUTPUTTAPE6,109,(XPRN(J),VPRN(J),J=1,JFIN),IPRN	MAIN 351
109	FORMAT (1X F10.6,F12.4,F10.6,F12.4,F10.6,F12.4,F10.6,F12.4,	MAIN 352
	Z F10.6,F12.4,4XI5)	MAIN 353
270	CONTINUE	MAIN 354
272	CALL TIME(AFTER)	MAIN 355
	XTIQ = 60. * (AFTER-BEGIN)	MAIN 356
	BEGIN = AFTER	MAIN 357
	WRITEOUTPUTTAPE6,135,XTIQ	MAIN 358
135	FORMAT (32H0 TIME FOR PRINT OF POTENTIAL = F9.4,9H SECONDS.)	MAIN 359
	GO TO (2721,2729), IKON	MAIN 360
2721	IKON = 2	MAIN 361
	WRITEOUTPUTTAPE6,101	MAIN 362
	GO TO 2490	MAIN 363
2729	DO 2728 J = 1,M	MAIN 364
	V(J,1) = FLOATF(JROTL*(JRÖTL+1))/XO(J)**2+V(J,1)	MAIN 365
	IF ACCUMULATOR OVERFLOW 2724,2725	MAIN 366
2724	V(J,1) = 1.0E+30	MAIN 367
2725	V(J,2) = FLOATF(JROTU*(JROTU+1))/XO(J)**2+V(J,2)	MAIN 368
	IF ACCUMULATOR OVERFLOW 2727,2728	MAIN 369
2727	V(J,2) = 1.0E+30	MAIN 370
2728	CONTINUE	MAIN 371
2722	MTEMQ = M	MAIN 372
	LLK = 0	MAIN 373
	KLK = 0	MAIN 374
C	FIND THE ENERGY LEVELS THROUGH USE OF SCHR.	MAIN 375
274	NLIKON = NL(IKON)	MAIN 376
	DO 285 I = 1,NLIKON	MAIN 377
276	IF (SCHR(NI,NS,MAXIT,EPS,IPSIQ,V(1,IKON),XO,S ,M ,XMIN,	MAIN 378
	Z XMAX,KV(I,IKON),ECALC(I,IKON),FACM)-1.) 284,278,300	MAIN 379
278	LLK = LLK + 1	MAIN 380
280	IF (LLK-LLIM) 284,284,304	MAIN 381
284	M = MIEMQ	MAIN 382
	DO 281 J = 1,M	MAIN 383
	XO(J) = FLOATF(J-1)*XH + XMIN	MAIN 384
281	CONTINUE	MAIN 385
	BVSUM = S(1)**2/XO(1)**2 + 4.*S(2)**2/XO(2)**2 + S(M)**2/XO(M)**2	MAIN 386
	KSIMP = M - 1	MAIN 387
	DO 287 J = 3,KSIMP,2	MAIN 388
	BVSUM = 2.*S(J)**2/XO(J)**2 + 4.*S(J+1)**2/XO(J+1)**2 + BVSUM	MAIN 389
287	CONTINUE	MAIN 390
	GO TO (2875,2871), IKON	MAIN 391
2871	DO 2872 J = 1,M	MAIN 392
	SU(J,I) = S(J)	MAIN 393
2872	CONTINUE	MAIN 394
	GO TO 2878	MAIN 395
2875	DO 2877 IK = 1,NL2	MAIN 396
	DO 2876 J = 1,M	MAIN 397
	XO(J) = (FLOATF(J-1)*XH+XMIN)*SU(J,IK)	MAIN 398
2876	CONTINUE	MAIN 399
2879	CONTINUE	MAIN 400
	CALL SIMP(S,SU(1,IK),M,XH,RESULT(I,IK))	MAIN 401
	CALL SIMP(S,XO,M,XH,RCNTRD(I,IK))	MAIN 402
2877	CONTINUE	MAIN 403
	DO 2882 IK = 1,NL2	MAIN 404
	DO 2881 J = 1,M	MAIN 405

Table III. (Contd.)

	XO(J) = (FLOATF(J-1)*XH+XMIN)**2*SU(J,IK)	MAIN 406
2881	CONTINUE	MAIN 407
	CALL SIMP(S,XO,M,XH,RRCN(I,IK))	MAIN 408
2882	CONTINUE	MAIN 409
2878	BVF(I,IKON) = FACM * BVSUM * XH / 3.	MAIN 410
	ECALC(I,IKON) = DE(IKON) * FACM + ECALC(I,IKON)	MAIN 411
	CALL TIME(AFTER)	MAIN 412
	XTIQ = 60. * (AFTER-BEGIN)	MAIN 413
	BEGIN = AFTER	MAIN 414
	WRITEOUTPUTTAPE6,162,ECALC(I,IKON),BVF(I,IKON),XTIQ	MAIN 415
162	FORMAT (30H0 SCHR FINDS ENERGY LEVEL G = F11.5,15H 1/CM AND BV =	MAIN 416
Z	F11.7,9H 1/CM IN F7.4,9H SECONDS. )	MAIN 417
285	CONTINUE	MAIN 418
	GO TO (2852,2851),IKON	MAIN 419
2851	IKON = 1	MAIN 420
	GO TO 2722	MAIN 421
2852	WRITEOUTPUTTAPE6,101	MAIN 422
	WRITEOUTPUTTAPE6,110,LLK	MAIN 423
110	FORMAT (38H0 PROGRAM SUCCESSFUL. (MAXIT REACHED 12, 7H TIMES) )	MAIN 424
	WRITEOUTPUTTAPE6,128	MAIN 425
128	FORMAT (35H0 THE BELOW IS FOR THE LOWER STATE. )	MAIN 426
	WRITEOUTPUTTAPE6,133	MAIN 427
133	FORMAT (54H0VIB. NO. GIVEN ENERGY CALC. ENERGY DIFFERENCE	MAIN 428
Z	13X43HGIVEN DELTA G CALC. DELTA G DIFFERENCE /44X	MAIN 429
Z	26HDIFFERENCE = CALC. - GIVEN //)	MAIN 430
286	DO 288 I = 1,NL	MAIN 431
	ETRIAL(I) = (ETRIAL(I) + DE) * FACM	MAIN 432
	DIFF = ECALC(I) - ETRIAL(I)	MAIN 433
	IF (I-1) 290,290,292	MAIN 434
292	DGT = ETRIAL(I) - ETRIAL(I-1)	MAIN 435
	DGC = ECALC(I) - ECALC(I-1)	MAIN 436
	DIFDE = DGC - DGT	MAIN 437
	WRITEOUTPUTTAPE6,136,DGT,DGC,DIFDE	MAIN 438
136	FORMAT ( 64X3F15.5)	MAIN 439
290	WRITEOUTPUTTAPE6,134,KV(I),ETRIAL(I),ECALC(I),DIFF	MAIN 440
134	FORMAT (I8, 3F15.5)	MAIN 441
288	CONTINUE	MAIN 442
	WRITEOUTPUTTAPE6,130	MAIN 443
130	FORMAT (1H128X8HVIB. NO.3X9HCALC. BV //)	MAIN 444
	DO 294 I = 1,NL	MAIN 445
	WRITEOUTPUTTAPE6,129,KV(I),BVF(I)	MAIN 446
129	FORMAT (28XI7,3F15.8)	MAIN 447
294	CONTINUE	MAIN 448
	WRITEOUTPUTTAPE6,101	MAIN 449
	WRITEOUTPUTTAPE6,137	MAIN 450
137	FORMAT (35H0 THE BELOW IS FOR THE UPPER STATE. )	MAIN 451
	WRITEOUTPUTTAPE6,138	MAIN 452
138	FORMAT (54H0VIB. NO. GIVEN ENERGY CALC. ENERGY DIFFERENCE	MAIN 453
Z	/44X26HDIFFERENCE = CALC. - GIVEN //)	MAIN 454
	DO 388 I = 1,NL2	MAIN 455
	ETRIAL(I,2) = (ETRIAL(I,2) + DE(2)) * FACM	MAIN 456
	DIFF = ECALC(I,2)-ETRIAL(I,2)	MAIN 457
	WRITEOUTPUTTAPE6,134,KV(I,2),ETRIAL(I,2),ECALC(I,2),DIFF	MAIN 458
388	CONTINUE	MAIN 459
	WRITEOUTPUTTAPE6,130	MAIN 460
	DO 394 I = 1,NL2	MAIN 461
	WRITEOUTPUTTAPE6,129,KV(I,2),BVF(I,2)	MAIN 462
394	CONTINUE	MAIN 463

Table III. (Contd.)

	DO 510 J = 1,NL	MAIN 464
	DO 510 IK = 1,NL2	MAIN 465
	RCNTRD(J,IK) = RCNTRD(J,IK)*0.529166/RESULT(J,IK)	MAIN 466
	RRCN(J,IK) = RRCN(J,IK)*0.529166**2/RESULT(J,IK)	MAIN 467
	RESULT(J,IK) = RESULT(J,IK)**2	MAIN 468
510	CONTINUE	MAIN 469
	WRITE OUTPUT TAPE 6,500	MAIN 470
500	FORMAT(24H1 FRANCK-CONDON FACTORS )	MAIN 471
	PRFMT(2) = PNFT(NL2)	MAIN 472
	WRITE OUTPUT TAPE 6,PRFMT,(KV(J,2),J = 1,NL2)	MAIN 473
	DO 520 J = 1,NL	MAIN 474
	WRITE OUTPUT TAPE 6,508,KV(J),(RESULT(J,ILK),ILK = 1,NL2)	MAIN 475
508	FORMAT(6X,I4,4(10X,E10.4,10X))	MAIN 476
520	CONTINUE	MAIN 477
	WRITE OUTPUT TAPE 6,514	MAIN 478
514	FORMAT(32H1 R-CENTROID FACTORS (ANGSTROMS) )	MAIN 479
	WRITE OUTPUT TAPE 6,PRFMT,(KV(J,2),J = 1,NL2)	MAIN 480
	DO 516 J = 1,NL	MAIN 481
	WRITE OUTPUT TAPE 6,508,KV(J),(RCNTRD(J,ILK),ILK = 1,NL2)	MAIN 482
516	CONTINUE	MAIN 483
	WRITE OUTPUT TAPE 6,517	MAIN 484
517	FORMAT(17H1 R**2-CENTROIDS )	MAIN 485
	WRITE OUTPUT TAPE 6,PRFMT,(KV(J,2),J = 1,NL2)	MAIN 486
	DO 518 J = 1,NL	MAIN 487
	WRITE OUTPUT TAPE 6,508,KV(J),(RRCN(J,ILK),ILK = 1,NL2)	MAIN 488
518	CONTINUE	MAIN 489
C		MAIN 490
C	CORRECT FOR FREQUENCY DEPENDENCE	MAIN 491
C	AND SCALE TO TEN	MAIN 492
C		MAIN 493
	DO 5121 IK = 1,NL2	MAIN 494
	DIV(IK) = 0.0	MAIN 495
	DDIV(IK) = 0.0	MAIN 496
	DO 5121 J = 1,NL	MAIN 497
	RESULT(J,IK) = RESULT(J,IK) *(TE+ECALC(IK,2)-ECALC(J,1))**3	MAIN 498
	RCNTRD(J,IK) = RESULT(J,IK)*(TE+ECALC(IK,2)-ECALC(J,1))	MAIN 499
5121	CONTINUE	MAIN 500
	DO 5022 IK = 1,NL2	MAIN 501
	DO 5022 J = 1,NL	MAIN 502
	DIV(IK) = MAX1F(DIV(IK),RESULT(J,IK))	MAIN 503
	DDIV(IK) = MAX1F(DDIV(IK),RCNTRD(J,IK))	MAIN 504
5022	CONTINUE	MAIN 505
	DO 5023 IK = 1,NL2	MAIN 506
	DO 5023 J = 1,NL	MAIN 507
	RESULT(J,IK) = RESULT(J,IK)/DIV(IK)*10.0	MAIN 508
	RCNTRD(J,IK) = RCNTRD(J,IK)/DDIV(IK)*10.0	MAIN 509
5023	CONTINUE	MAIN 510
	WRITE OUTPUT TAPE 6,5024	MAIN 511
5024	FORMAT(48H1 RELATIVE INTENSITY(QUANTUM/SEC) SCALED TO TEN )	MAIN 512
	WRITE OUTPUT TAPE 6,PRFMT,(KV(J,2),J = 1,NL2)	MAIN 513
	DO 5026 J = 1,NL	MAIN 514
	WRITE OUTPUT TAPE 6,509,KV(J),(RESULT(J,ILK),ILK = 1,NL2)	MAIN 515
509	FORMAT(6X,I4,4(12X,F6.3,12X))	MAIN 516
5026	CONTINUE	MAIN 517
	WRITE OUTPUT TAPE 6,5030	MAIN 518
5030	FORMAT(47H1 RELATIVE INTENSITY(ENERGY/SEC) SCALED TO TEN )	MAIN 519
	WRITE OUTPUT TAPE 6,PRFMT,(KV(J,2),J = 1,NL2)	MAIN 520
	DO 5027 J = 1,NL	MAIN 521

Table III. (Contd.)

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5027	WRITE OUTPUT TAPE 6,509,KV(J),(RCNTRD(J,ILK),ILK = 1,NL2)	MAIN 522
	CONTINUE	MAIN 523
	WRITE OUTPUT TAPE 6,5031	MAIN 524
5031	FORMAT(12H1 CONSTANTS )	MAIN 525
	WRITE OUTPUT TAPE 6,144,JROTL,JROTU	MAIN 526
	WRITE OUTPUT TAPE 6,2000,TE,BE1,BE2,AE1,AE2,GE1,GE2	MAIN 527
	GO TO 1	MAIN 528
300	KLK = KLK + 1	MAIN 529
301	IF (KLK-KLIM) 284,302,302	MAIN 530
302	WRITEOUTPUTTAPE6,112,KLIM	MAIN 531
112	FORMAT (26H0 SCHR NOT SUCCESSFUL FOR I2, 28HTH TIME, GO TO NEXT PR	MAIN 532
	ZOBLEM. )	MAIN 533
	GO TO 1	MAIN 534
304	WRITEOUTPUTTAPE6,113,LLIM,I	MAIN 535
113	FORMAT (28H0 SCHR DID NOT CONVERGE FOR I2,17HTH TIME WHEN I = I3)	MAIN 536
306	GO TO 1	MAIN 537
308	WRITEOUTPUTTAPE6,120,NDE	MAIN 538
120	FORMAT (25H0 ERROR IN INPUT. NDE = I10)	MAIN 539
	GO TO 1	MAIN 540
400	CALL EXIT	MAIN 541
	END	MAIN 542

CPOTFIT	USING NTRPSR,MINFIT,MAXFIT	POTFT000
	SUBROUTINE POTFIT (XI,YI,N,XO,V,M,XH,XMIN,XMAX,INSC,NUSED,FACM)	POTFT001
	DIMENSION XI(400),YI(400),XO(2000),V(2000)	POTFT002
248	MBEG = 1	POTFT003
	XMAXT = XMAX	POTFT004
	XMINT = XMIN	POTFT005
C	CHECK FOR EXTRAPOLATION AT SMALL R.	POTFT006
250	IF (XMIN - XI(1)) 252,254,254	POTFT007
252	XMAX = XI(1)	POTFT008
	CALL MINFIT (XI,YI,N,XO,V,M,XH,XMIN,XMAX,INSC,FACM)	POTFT009
	IF (INSC) 712,253,712	POTFT010
253	MT = M	POTFT011
	XMIN = XO(MT) + XH	POTFT012
	MBEG = M + 1	POTFT013
C	PREPARE TO INTERPOLATE.	POTFT014
254	M = 0	POTFT015
	XMAX = XMAXT	POTFT016
	NL = N-1	POTFT017
256	IF ( XMAX-XI(NL))260,260,258	POTFT018
258	XMAX = XI(NL)	POTFT019
260	CALL NTRPSR(XI,YI,XO,V,XH,N,M,XMIN,XMAX,INSC,MBEG,NUSED)	POTFT020
C	CHECK FOR EXTRAPOLATION AT LARGE R.	POTFT021
	IF (INSC) 712,262,712	POTFT022
262	IF (XMAXT-XMAX) 267,267,264	POTFT023
264	MBEG = M + MBEG	POTFT024
	XMIN = XO(MBEG-1) + XH	POTFT025
	XMAX = XMAXT	POTFT026
266	CALL MAXFIT (XI,YI,N,XO,V,M,XH,XMIN,XMAX,INSC,FACM,MBEG)	POTFT027
267	XMIN = XMINT	POTFT028
	M = M + MBEG - 1	POTFT029
712	RETURN	POTFT030
	END	POTFT031

Table III. (Contd.)

UCRL-10925

```
CMINFIT      Y = A/X**12+ C
SUBROUTINE MINFIT (X,Y,N,XO,V,M,XH,XMIN,XMAX,INSC,FACM)
DIMENSION X (400),Y (400),XO(2000),V(2000)
R12FUF(X) = A/X**12 + C
M = XFIXF((XMAX-XMIN)/XH) + 1
A = (Y(1)-Y(2))/(1./X(1)**12 - 1./X(2)**12)
C = Y(1) - A/X(1)**12
212 DO 214 I = 1,M
XO(I) = FLOATF(I-1)*XH + XMIN
V (I) = R12FUF(XO(I))
214 CONTINUE
A = A*FACM*.529166**12
C = C*FACM
WRITEOUTPUTTAPE6,101,A,C
101 FORMAT (70H0 LEFT END OF POTENTIAL FUNCTION IS FOUND FROM Y=A/X**1
Z2+C, WHERE A = 1PE14.7, 9H AND C = [14.7 )
RETURN
END
```

```
CMAXFIT      Y = A/X**B
SUBROUTINE MAXFIT (X,Y,N,XO,V,M,XH,XMIN,XMAX,INSC,FACM,MBEG)
DIMENSION X (400),Y (400),XO(2000),V(2000)
R6FUNF(X) = A/X**B
L = N - 1
B = LOGF(Y(L)/Y(N))/LOGF(X(N)/X(L))
A = Y(N) * X(N)**B
M = XFIXF((XMAX-XMIN)/XH) + 1
MFIN = MBEG + M - 1
202 DO 204 I = MBEG,MFIN
XO(I) = FLOATF(I-MBEG)*XH + XMIN
V(I) = R6FUNF(XO(I))
204 CONTINUE
A = A*FACM*.529166**B
WRITEOUTPUTTAPE6,206,A,B
206 FORMAT (68H0 RIGHT END OF POTENTIAL FUNCTION IS FOUND FROM Y=A/X**
ZB, WHERE A = E14.7, 9H AND B = E14.7)
RETURN
END
```



Table III. (Contd.)

```

CNTRPSR  INTERPOLATION PROGRAM (BY SUCCESSIVE RANGES)  SINGLE PREC.  NTRPS000
C
C      THE METHOD OF LAGRANGE IS USED.  THE INPUT POINTS NEED NOT BE  NTRPS001
C      EQUALLY SPACED.  THERE ARE TWO MODES OF INPUT AVAILABLE.  THE  NTRPS002
C      FIRST OCCURS WHEN M = 0.  THE ABSCISSAE ARE THEN GENERATED FROM  NTRPS003
C      XMIN,XMAX,AND XH.  AT EXIT M = NO. OF POINTS FOUND, AND XO  NTRPS004
C      CONTAINS THE ABSCISSAE.  M WILL BE CHECKED TO INSURE THAT THE  NTRPS005
C      DIMENSION IS NOT EXCEEDED.  MDIMM = THE DIMENSION OF THE XO, YO  NTRPS006
C      ARRAYS.  THE SECOND MODE OCCURS WHEN M IS POSITIVE.  THE M  NTRPS007
C      ABSCISSAE ARE THEN ASSUMED TO HAVE BEEN GENERATED PRIOR TO  NTRPS008
C      ENTRY.  THE STARTING INDEX FOR THE OUTPUT ARRAY MUST BE  NTRPS009
C      SPECIFIED.  THE FIRST POINT FOUND WILL BE AT XO(MBEG).  XH MUST  NTRPS010
C      BE GIVEN SINCE THE ORDINATE FOR ANY POINT CLOSER THAN .01*XH TO  NTRPS011
C      AN INPUT POINT IS TAKEN AS THAT FOR THE INPUT POINT.  -NUSED- IS  NTRPS012
C      THE NUMBER OF POINTS USED FOR EACH INTERPOLATED POINT.  *NUSED*  NTRPS013
C      MUST BE EVEN AND LESS THAN OR EQUAL TO -N-.  NUSED = 8 IS  NTRPS014
C      SUGGESTED.  ANY POINT FARTHER THAN NUSED/2 POINTS FROM EITHER END  NTRPS015
C      IS FOUND FROM THE NUSED/2 ON EACH SIDE.  NTRPSR WILL SCALE AND  NTRPS016
C      RESCALE IN ORDER TO AVOID OVERFLOW.  IF THE FIRST SCALING DOES  NTRPS017
C      NOT SUCCEED, NTRPSR WILL TRY UP TO 7 TIMES MORE BEFORE RETURNING  NTRPS018
C      IN THE ERROR MODE.  (INSC = 1)  NTRPS019
C      INPUT IS XI,YI,(XO),XH,N,M,(XMIN),(XMAX),MBEG,NUSED.  NTRPS020
C      OUTPUT IS (XO),YO,INSC.  NTRPS021
C      INSC = 0 IF PROGRAM WAS SUCCESSFUL.  IF NOT, INSC = 1.  NTRPS022
C  NTRPS023
C  NTRPS024
SUBROUTINE NTRPSR(XJ,YJ,XO,YO,XN,N,K,XNIN,XNAX,INSC,MBEG,NUSED)  NTRPS025
DIMENSION XI(400),YI(400),XO(2000),YO(2000),XJ(400),YJ(400),NUMB(4  NTRPS026
100)  NTRPS027
MDIMM = 2000  NTRPS028
XMAX = XNAX  NTRPS029
XMIN = XNIN  NTRPS030
XH = ABSF(XN)  NTRPS031
M = K  NTRPS032
IREV = 0  NTRPS033
IREX = 0  NTRPS034
C      M IS ZERO, IF XH, XMIN, XMAX ARE TO BE USED.  IF M IS NOT = TO  NTRPS035
C      ZERO, THEN XO(I), I = 1,M WILL BE USED AS ABSCISSA.  NTRPS036
200 IF (M) 270,201,206  NTRPS037
201 M = XINTF(ABSF((XMAX-XMIN)/XH)) + 1  NTRPS038
C      IF M IS MORE THAN DIMENSION OF XO, RETURN IN ERROR MODE.  NTRPS039
IF (M+MBEG-MDIMM-2) 202,272,272  NTRPS040
202 MF = MBEG + M - 1  NTRPS041
IF (XMAX - XMIN) 203,204,204  NTRPS042
203 XMIN = XNAX  NTRPS043
XMAX = XNIN  NTRPS044
IREV = 1  NTRPS045
204 DO 205 I = MBEG,MF  NTRPS046
XO(I) = FLOATF(I-MBEG) * XH + XMIN  NTRPS047
205 CONTINUE  NTRPS048
206 DO 207 I = 1,N  NTRPS049
XI(I) = XJ(I)  NTRPS050
207 CONTINUE  NTRPS051
MF = MBEG + M - 1  NTRPS052
MSTA = MBEG  NTRPS053
NUST = NUSED/2  NTRPS054
NS = NUST + 1  NTRPS055
NF = N - NS + 1  NTRPS056
NFP = NF + 1  NTRPS057

```

Table III. (Contd.)

DO 208 I = NS,NFP	NTRPS058
NUMB(I) = 0	NTRPS059
208 CONTINUE	NTRPS060
IF (XO(MF) - XO(MBEG)) 209,211,211	NTRPS061
209 M2 = M/2	NTRPS062
M2F = MBEG + M2 - 1	NTRPS063
DO 210 I = MBEG,M2F	NTRPS064
K = MF + MBEG - I	NTRPS065
TEMP = XO(I)	NTRPS066
XO(I) = XO(K)	NTRPS067
XO(K) = TEMP	NTRPS068
210 CONTINUE	NTRPS069
IREV = 1	NTRPS070
211 IF (XI(N)-XI(1)) 212,216,216	NTRPS071
212 N2 = N/2	NTRPS072
DO 214 I = 1,N2	NTRPS073
K = N + 1 - I	NTRPS074
TEMP = XJ(I)	NTRPS075
TEMS = YJ(I)	NTRPS076
XJ(I) = XJ(K)	NTRPS077
YJ(I) = YJ(K)	NTRPS078
XJ(K) = TEMP	NTRPS079
YJ(K) = TEMS	NTRPS080
214 CONTINUE	NTRPS081
IREX = 1	NTRPS082
216 IF (NF-NS) 236,218,218	NTRPS083
218 DO 226 J = MBEG,MF	NTRPS084
DO 224 I = NS,NF	NTRPS085
220 IF(XO(J)-XJ(I))222,222,224	NTRPS086
222 NUMB(I) = NUMB(I) + 1	NTRPS087
GO TO 226	NTRPS088
224 CONTINUE	NTRPS089
NUMB(NFP) = NUMB(NFP) + 1	NTRPS090
226 CONTINUE	NTRPS091
GO TO 238	NTRPS092
236 NUMB(NFP) = M	NTRPS093
238 M = 0	NTRPS094
239 DO 250 L = NS,NFP	NTRPS095
IF (NUMB(L)) 250,250,242	NTRPS096
242 M = NUMB(L)	NTRPS097
NSTA = L - NUST	NTRPS098
GO TO 100	NTRPS099
246 IF (INSC) 274,248,274	NTRPS100
248 MSTA = MSTA + M	NTRPS101
250 CONTINUE	NTRPS102
240 K = MSTA - MBEG	NTRPS103
IF (IREV) 256,256,252	NTRPS104
252 M2F = K/2 + MBEG - 1	NTRPS105
DO 254 I = MBEG,M2F	NTRPS106
J = MF + MBEG - I	NTRPS107
TEMP = XO(I)	NTRPS108
TEMS = YO(I)	NTRPS109
XO(I) = XO(J)	NTRPS110
YO(I) = YO(J)	NTRPS111
XO(J) = TEMP	NTRPS112
YO(J) = TEMS	NTRPS113
254 CONTINUE	NTRPS114
256 IF (IREX) 262,262,258	NTRPS115

Table III. (Contd.)

258	DO 260 I = 1,N2	NTRPS116
	J = N + 1 - I	NTRPS117
	TEMP = XJ(I)	NTRPS118
	TEMS = YJ(I)	NTRPS119
	XJ(I) = XJ(J)	NTRPS120
	YJ(I) = YJ(J)	NTRPS121
	XJ(J) = TEMP	NTRPS122
	YJ(J) = TEMS	NTRPS123
260	CONTINUE	NTRPS124
262	RETURN	NTRPS125
270	WRITEOUTPUTTAPE6,2101	NTRPS126
2101	FORMAT (44H0 ERROR IN INPUT TO NTRPSR. M IS NEGATIVE. )	NTRPS127
	INSC = 1	NTRPS128
	GO TO 240	NTRPS129
272	H = (XMAX-XMIN)/FLOATF(MDIMM-MBEG)	NTRPS130
	WRITEOUTPUTTAPE6,2102,H	NTRPS131
2102	FORMAT (58H0 ERROR IN INPUT TO NTRPSR. MINIMUM ALLOWABLE SPACING	NTRPS132
	8IS 1PE12.3)	NTRPS133
	INSC = 1	NTRPS134
	GO TO 240	NTRPS135
274	WRITEOUTPUTTAPE6,2103,L	NTRPS136
2103	FORMAT (43H0 INTR1 WAS UNABLE TO INTERPOLATE IN RANGE 13)	NTRPS137
	GO TO 240	NTRPS138
100	NCON = 1	NTRPS139
	REFA = 1.414214	NTRPS140
	NFIN = NSTA + NUSED - 1	NTRPS141
	DO 98 I = NSTA,NFIN	NTRPS142
	XI(I) = XJ(I)	NTRPS143
	YI(I) = YJ(I)	NTRPS144
98	CONTINUE	NTRPS145
	NSTA1 = NSTA + 1	NTRPS146
	XSCALE = (XI(NFIN) - XI(NSTA))/10.	NTRPS147
	IF (XSCALE) 995,991,995	NTRPS148
991	XSCALE = 1.	NTRPS149
995	YMAX = YI(NSTA)	NTRPS150
	YMIN = YI(NSTA)	NTRPS151
1001	DO 1002 I = NSTA1,NFIN	NTRPS152
	YMAX = MAX1F(YMAX,YI(I))	NTRPS153
	YMIN = MIN1F(YMIN,YI(I))	NTRPS154
1002	CONTINUE	NTRPS155
91	YSCALE = YMAX - YMIN	NTRPS156
	IF (YSCALE) 915,915,1003	NTRPS157
915	YSCALE = 1.	NTRPS158
1003	DO 1004 I = NSTA,NFIN	NTRPS159
	XI(I) = XI(I)/XSCALE	NTRPS160
	YI(I) = (YI(I)-YMIN)/YSCALE + .5	NTRPS161
1004	CONTINUE	NTRPS162
	XH = ABSF(XN)/XSCALE	NTRPS163
	MFIN = MSTA + M - 1	NTRPS164
	MTA = MSTA	NTRPS165
1005	EPSIL = .01*XH	NTRPS166
101	DO 110 II= MTA,MFIN	NTRPS167
	XO(II) = XO(II)/XSCALE	NTRPS168
	YO(II) = 0.0	NTRPS169
	PNUM = 1.0	NTRPS170
1011	DO 107 I = NSTA,NFIN	NTRPS171
C	FIND XO(II)-XI(I) FOR NUMERATOR AND CHECK FOR NEARNESS.	NTRPS172
	XNUM = XO(II) - XI(I)	NTRPS173

Table III. (Contd.)

1012	IF (ABS(XNUM )-EPSIL) 102,102,103	NTRPS174
102	YO(II) = YI(I)	NTRPS175
	GO TO 109	NTRPS176
C	PNUM = PRODUCT OF ALL XNUM	NTRPS177
103	PNUM = PNUM*XNUM	NTRPS178
C	CONSTRUCT DENOMINATOR AND SUM	NTRPS179
	PDEN = 1.0	NTRPS180
104	DO 106 J = NSTA,NFIN	NTRPS181
1043	IF (I-J) 105,106,105	NTRPS182
105	PDEN = (XI(I) - XI(J))*PDEN	NTRPS183
1051	IF QUOTIENT OVERFLOW 1103,106	NTRPS184
106	CONTINUE	NTRPS185
	DEN = PDEN*XNUM	NTRPS186
	YO(II) = YI(I)/DEN + YO(II)	NTRPS187
	IF ACCUMULATOR OVERFLOW 1121, 107	NTRPS188
107	CONTINUE	NTRPS189
	YO(II) = YO(II)*PNUM	NTRPS190
109	YO(II) = (YO(II)-.5)*YSCALE + YMIN	NTRPS191
	XO(II) = XO(II) * XSCALE	NTRPS192
110	CONTINUE	NTRPS193
	INSC = 0	NTRPS194
	GO TO 246	NTRPS195
1103	WRITEOUTPUTTAPE6,1104,NCON,XSCALE	NTRPS196
	WRITEOUTPUTTAPE6,1108,II,I,J	NTRPS197
1104	FORMAT (8H NCON = I3, 11H, XSCALE = F10.7)	NTRPS198
1108	FORMAT (26H OVERFLOW OCCURRED AT II= I4,4H I= I3,4H J= I3)	NTRPS199
	NCON = NCON + 1	NTRPS200
1105	DO 1106 I = NSTA,NFIN	NTRPS201
	XI(I) = XI(I)/REFA	NTRPS202
1106	CONTINUE	NTRPS203
	XO(II) = XO(II) * XSCALE	NTRPS204
	MTA = II	NTRPS205
	XH = XH /REFA	NTRPS206
	XSCALE = XSCALE*REFA	NTRPS207
	IF (NCON-8) 1005,1005,1107	NTRPS208
1107	INSC = 1	NTRPS209
	GO TO 246	NTRPS210
1121	WRITEOUTPUTTAPE6,1122	NTRPS211
1122	FORMAT (48H0 ACCUMULATOR OVERFLOW. DEN MUST BE TOO SMALL. )	NTRPS212
	INSC = 1	NTRPS213
	GO TO 246	NTRPS214
	FREQUENCY 1051(1,9),1001(50),1003(50),101(500),1011(50),	NTRPS215
1	1012(0,0,1),104(50),1043(1,0,1)	NTRPS216
	END	NTRPS217

Table III. (Contd.)

CSIMP		SIMPS000
C	INTEGRATION OF A PRODUCT S*SS BY SIMPSONS RULE.	SIMPS001
	SUBROUTINE SIMP(S,SS,N,H,RESULT)	SIMPS002
	DIMENSION S(2000),SS(2000)	SIMPS003
	SUM = 0.0	SIMPS004
	DO 1 J = 2,N,2	SIMPS005
1	SUM = SUM + 2.0*S(J)*SS(J) + 4.0*S(J-1)*SS(J-1)	SIMPS006
	RESULT = SUM*H/3.0	SIMPS007
	RETURN	SIMPS008
	END	SIMPS009

CTIME		TIME 000
C	DISCARD THIS SUBROUTINE IF YOUR 709/7090/7094 INSTALLATION HAS	TIME 001
C	AN ON-LINE CLOCK ADDRESSABLE BY CALL TIME(X)	TIME 002
	SUBROUTINE TIME(X)	TIME 003
1	X = 0.0	TIME 004
	RETURN	TIME 005
	END	TIME 006

CPOTGEN	THIS IS A DUMMY SUBROUTINE	POTGN000
C	POTGN GENERATES THE POTENTIAL.	POTGN001
	SUBROUTINE POTGN(IPOTGN,DE,NDE,IIRA,IIEN,RE,ETRIAL,KV,NL,IIEN1,	POTGN002
Z	NET,WE,ZMU,XMAX,XMIN,XH,FACM,XO,V,M)	POTGN003
1	IPOTGN = 10	POTGN004
	RETURN	POTGN005
	END	POTGN006



Table III. (Contd.)

62	Y(3)=Y(3)/PM	SCHRV058
	GI= V(M+1) - E	SCHRV059
	GO TO 46	SCHRV060
C	.....TEST FOR CROSSING PT.	SCHRV061
70	IF(ABS(P(M))-ABS(P(M+1))) 90, 90, 72	SCHRV062
72	IF(M-2) 90,90,81	SCHRV063
81	Y= Y(2)	SCHRV064
82	Y(2)=Y(3)	SCHRV065
84	M=M-1	SCHRV066
86	GO TO 46	SCHRV067
C		SCHRV068
90	PM=P(M)	SCHRV069
	MSAVE = M	SCHRV070
92	YIN=Y(2)/PM	SCHRV071
94	DO 96 J=M,N	SCHRV072
96	P(J)=P(J)/PM	SCHRV073
C		SCHRV074
C	.....START OUTWARD INTEGRATION	SCHRV075
C		SCHRV076
100	P(1)=1.E-20	SCHRV077
102	Y=0.	SCHRV078
104	GI=V-E	SCHRV079
106	Y(2)=(1.-HV*GI)*P	SCHRV080
	K = 0	SCHRV081
108	DO 132 I=2,M	SCHRV082
110	Y(3)=Y(2)+((Y(2)-Y)+H2*GI*P(I-1))	SCHRV083
112	GI=V(I)-E	SCHRV084
114	P(I)=Y(3)/(1.-HV*GI)	SCHRV085
C	.....TEST FOR OVERFLOW	SCHRV086
116	IF(K)118,130,118	SCHRV087
118	K=0	SCHRV088
	I1=I-1	SCHRV089
	PM=P(I1)	SCHRV090
	DO 120 J=1,I1	SCHRV091
120	P(J)=P(J)/PM	SCHRV092
122	Y=Y/PM	SCHRV093
124	Y(2)=Y(2)/PM	SCHRV094
126	Y(3)=Y(3)/PM	SCHRV095
	GI=V(I1)-E	SCHRV096
	GO TO 110	SCHRV097
C		SCHRV098
130	Y=Y(2)	SCHRV099
132	Y(2)=Y(3)	SCHRV100
C		SCHRV101
C	.....FINISHED OUTWARD INTEGRATION	SCHRV102
134	PM=P(M)	SCHRV103
	IF(PM)135,149,135	SCHRV104
135	YOUT=Y/PM	SCHRV105
136	YM=Y(3)/PM	SCHRV106
138	DO 140 J=1,M	SCHRV107
140	P(J)=P(J)/PM	SCHRV108
C		SCHRV109
C	.....CORRECTION	SCHRV110
C		SCHRV111
142	DF=0.	SCHRV112
144	DO 146 J=1,N	SCHRV113
146	DF=DF-P(J)**2	SCHRV114
148	F=(-YOUT-YIN+2.*YM)/H2+(V(M)-E)	SCHRV115

Table III. (Contd.)

	DOLD=DE	SCHRV116
	IF(K)149,150,149	SCHRV117
149	F=9.999999E+29	SCHRV118
	DF=-F	SCHRV119
	DE=ABSF(.0001*E)	SCHRV120
	GO TO 152	SCHRV121
150	DE=-F/DF	SCHRV122
152	IF(NI-1)164,162,164	SCHRV123
156	FORMAT(1H0 I4, 2X, 1P4E16.7,5X,29H THE CROSSING PT. OCCURS A	SCHRV124
	1T I4)	SCHRV125
162	EPRIN = E*FACM	SCHRV126
	DEPRIN = DE*FACM	SCHRV127
	WRITEOUTPUTTAPE6,156,IT,EPRIN,F,DF,DEPRIN,MSAVE	SCHRV128
164	EOLD = E	SCHRV129
	E=E+DE	SCHRV130
166	TEST=MAX1F(ABSF(DOLD)-ABSF(DE),TEST)	SCHRV131
168	IF(TEST)171,170,170	SCHRV132
170	IF( ABSF( E-EOLD) - ABSF(EPS)) 172,172,171	SCHRV133
171	CONTINUE	SCHRV134
	SCHR=1.	SCHRV135
	GO TO 173	SCHRV136
C	.....CONVERGED-COUNT NODES	SCHRV137
172	SCHR=0.	SCHRV138
173	KV=0	SCHRV139
	NL=N-2	SCHRV140
174	DO 192 J=3,NL	SCHRV141
176	IF(P(J))178,177,177	SCHRV142
177	IF(P(J-1))180,192,192	SCHRV143
178	IF(P(J-1))192,270,184	SCHRV144
C	POS. NODE	SCHRV145
180	IF(P(J+1))192,182,182	SCHRV146
182	IF(P(J-2))190,192,192	SCHRV147
C	NEG. NODE	SCHRV148
184	IF(P(J+1))186,192,192	SCHRV149
186	IF(P(J-2))192,190,190	SCHRV150
C	FALSE NODE DUE TO UNDERFLOW	SCHRV151
270	IF(P(J+1))280,192,192	SCHRV152
280	IF(P(J-2))192,192,190	SCHRV153
190	KV=KV+1	SCHRV154
192	CONTINUE	SCHRV155
C	.....NORMALIZE	SCHRV156
200	SN=SQRTF(-H*DF)	SCHRV157
202	DO 204 J=1,N	SCHRV158
204	S(J)=P(J)/SN	SCHRV159
C	.....PRINT SOLUTION	SCHRV160
208	E = E*FACM	SCHRV161
	IF(NS-1)236,210,236	SCHRV162
210	IPSIA = IPSIQ * 300	SCHRV163
	IPSIB = IPSIQ * 49	SCHRV164
	IPSIC = IPSIQ * 250	SCHRV165
	IPSID = IPSIQ * 50	SCHRV166
	DO 234 JF=1,N,IPSIA	SCHRV167
214	FORMAT(47H1SCHR- SOLUTION OF RADIAL SCHR. EQUATION FOR V= 13, 7H.	SCHRV168
	X E= 1PE15.7 /20H0 I S(I) 5(20H I S(I) )	SCHRV169
218	WRITEOUTPUTTAPE6,214,KV,E	SCHRV170
220	JL=XMINOF(JF+IPSIB,N)	SCHRV171
222	DO 234 J=JF,JL,IPSIQ	SCHRV172
224	IL=XMINOF(J+IPSIC,N)	SCHRV173



Table III. (Contd.)

228	FORMAT(6(I5,1PE15.7))	SCHRV174
232	WRITEOUTPUTTAPE6,228,(I,S(I),I=J,IL,IPSID)	SCHRV175
234	CONTINUE	SCHRV176
236	E0=E	SCHRV177
	IF(NS-33) 874,875,874	SCHRV178
875	WRITEOUTPUTTAPE6,876,KV,E	SCHRV179
876	FORMAT(50H0 SOLUTION OF RADIAL SCHRODINGER EQUATION FOR V = I3,	SCHRV180
	1 7H E = 1PE15.7 )	SCHRV181
874	CONTINUE	SCHRV182
250	RETURN	SCHRV183
	FREQUENCY 52(0,1,0),70(0,0,1),72(0,0,1),94(100),55(50),108(100),11	SCHRV184
	16(0,1,0),138(100),144(200),152(1,0,0), 202(200)	SCHRV185
	END	SCHRV186

Table III. (Contd.)

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	COUNT 80		EFMT 000
	LBL EFMT		EFMT 001
	REM NU EFM,EFM AND LFM FOR FORTRAN 2		EFMT 002
	REM		EFMT 003
	ENTRY EFM		EFMT 004
	ENTRY EFMT		EFMT 005
LFM	OCT 476000000004		EFMT 006
	TTR 1,4		EFMT 007
EFMT	CLA 1,4		EFMT 008
	STA SETN+1		EFMT 009
	CLA TTR		EFMT 010
	TXI EFM+1,4,-1		EFMT 011
EFM	CLA HPR		EFMT 012
	STO OVER+2		EFMT 013
	OCT 476000000002		EFMT 014
SET	CLA X	TTR ANALY	EFMT 015
	STO 8		EFMT 016
	TTR 1,4		EFMT 017
X	TTR ANALY		EFMT 018
ANALY	SXD SAVEX,1		EFMT 019
	LXD 0,1		EFMT 020
	TTR *+14,1		EFMT 021
	TTR MQO	MQ OVER	EFMT 022
SAVEX	PZE	SAVE XA IN DEC.,THEN ACC.	EFMT 023
	TTR ACMQ	11	EFMT 024
	TTR AC	10	EFMT 025
	TTR MQ	9	EFMT 026
ZERO	PZE		EFMT 027
	TTR ACMQO	AC AND MQ OVER	EFMT 028
	TTR ACO		EFMT 029
AC	CLA ZERO		EFMT 030
	TTR RETRN		EFMT 031
ACMQ	CLA ZERO	3	EFMT 032
	TTR MQ		EFMT 033
MQ	LDQ ZERO	1, MQ UNDER	EFMT 034
RETRN	LXD SAVEX,1		EFMT 035
	STO SAVEX		EFMT 036
	CLA 0		EFMT 037
	STA *+2		EFMT 038
	CLA SAVEX		EFMT 039
	TTR **		EFMT 040
ACMQO	ORA MAX		EFMT 041
MQO	STO SAVEA		EFMT 042
	LLS 0		EFMT 043
	LDQ MAX		EFMT 044
	LRS 0		EFMT 045
	TTR OVER+1		EFMT 046
ACO	ORA MAX		EFMT 047
OVER	STO SAVEA		EFMT 048
	CLA 0		EFMT 049
	HPR 63	PAUSE OVERFLOW	EFMT 050
	CLA SAVEA	PRESS START TO CONTINUE	EFMT 051
	TTR RETRN		EFMT 052
SAVEA	PZE		EFMT 053
THREE	PZE 0,0,3		EFMT 054
TTR	TTR SETN		EFMT 055
HPR	HPR 63		EFMT 056
SETN	ANA THREE		EFMT 057
	STO -		EFMT 058
	TTR OVER+3		EFMT 059
MAX	OCT 37777777777		EFMT 060
	END		EFMT 061

Table IV. Sample data deck for relative-intensity program.

```

*      DATA
1
1 SILICON NITRIDE INTENSITY DISTRIBUTION          TEST PROGRAM
  2 9.33526
    2 2 25 (2F10.0)
1.3613170 12376.760
1.3686189 11369.400
1.3764643 10348.920
1.3849046 9315.320
1.3941121 8268.600
1.4041987 7208.760
1.4154399 6135.800
1.4281304 5049.720
1.4428560 3950.520
1.4605683 2838.200
1.4834289 1712.760
1.5188710 574.200
1.5718000 0.
1.6311431 574.200
1.6788244 1712.760
1.7140474 2838.200
1.7442476 3950.520
1.7715936 5049.720
1.7970281 6135.800
1.8211572 7208.760
1.8442578 8268.600
1.8666328 9315.320
1.8883695 10348.920
1.9096753 11369.400
1.9305798 12376.760
  1 50488.0
1.100      2.100      0.001      2
  10      2      1 (8X12,F10.0)
          0 574.200
          1 1712.760
          2 2838.200
          3 3950.520
          4 5049.720
          5 6135.800
          6 7208.760
          7 8268.600
          8 9315.320
          9 10348.920
    2 2 25 (2F10.0)
1.3841050 10068.404
1.3882994 9287.577
1.3935768 8499.421
1.3999376 7699.832
1.4074129 6885.047
1.4160805 6051.643
1.4261043 5196.535
1.4377249 4316.981
1.4514711 3410.577
1.4682963 2475.260
1.4903674 1509.307
1.5254273 511.333
1.5800000 0.
1.6445856 511.333

```

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Table IV. (Contd.)

1.6996278	1509.307				
1.7421381	2475.260				
1.7798702	3410.577				
1.8149804	4316.981				
1.8404052	5176.535				
1.8806691	6051.643				
1.9119547	6885.047				
1.9423804	7699.832				
1.9719579	8499.421				
2.0006375	9287.577				
2.0283271	10068.404				
1	15872.0				
1.100	2.100	0.001			2
4	2	1	(8X12,F10.0)		
	0	511.333			
	1	1509.307			
	2	2475.260			
	3	3410.577			
6	6	10	10	0.001	
0.7310					
0.00567					
0.7235					
0.01037					
24300.0					
5					

---

---

APPENDIX: COMPUTER OUTPUT OF SAMPLE DATA DECKS

Table V shows the computer output when the sample data deck given in Table II is run with the RKR program compiled from Table I; Table VI shows the computer output when the sample data deck given in Table IV is run with the relative-intensity program compiled from Table III.

Table V. RKR program output.

RKR PROCEDURE APPLIED TO THE X STATE OF SILICON NITRIDE TEST PROGRAM  
MOLECULAR CONSTANTS ARE TAKEN FROM JENKINS AND DE LASZLO

THE REDUCED MASS OF THE TWO ATOMS, BASED ON  $O_{16}=16$ , IS 9.335260

TURNING POINTS ARE GENERATED BY CONSTANTS

THE  $G(V)$  CURVE IS CONSTRUCTED FROM THE FOLLOWING INPUT DATA.

WE = 1151.680; WEXR = 6.5600; WEYE = , WEZE = , WETE = .  
TURNING POINTS ARE GENERATED BY CONSTANTS

THE  $BV(V)$  CURVE IS CONSTRUCTED FROM THE FOLLOWING INPUT DATA.

BE = 7.31000E-01; ALPHA = 5.6700E-03, GAMMA = -0. , DELTA = -0. , EPSLNE = -0.

RKR PROCEDURE APPLIED TO THE X STATE OF SILICON NITRIDE TEST PROGRAM  
MOLECULAR CONSTANTS ARE TAKEN FROM JENKINS AND DE LASZLO

NUMBER IN BESRRR = 8.

THE  $G(V)$  VALUES USED BELOW ARE

V	G	V	G	V	G	V	G	V	G	V	G
0.500	6135.7999	0.500	574.2000	1.500	1712.7599	2.500	2838.1999	3.500	3950.5199	4.500	5049.7198
5.500	6135.7999	6.500	7208.7599	7.500	8268.5997	8.500	9315.3197	9.500	10348.3197		

THE  $BV(V)$  VALUES USED BELOW ARE

V	BV	V	BV	V	BV	V	BV	V	BV	V	BV
0.500	0.7310000	0.500	0.7281650	1.500	0.7224950	2.500	0.7168250	3.500	0.7111550	4.500	0.7054850
5.500	0.6948150	6.500	0.6941450	7.500	0.5884750	8.500	0.6828050	9.500	0.6771350		

OUTPUT V,G--LEVELS AT WHICH TURNING POINTS ARE FOUND

V	G	V	G	V	G	V	G	V	G	V	G
0.500	574.2000	1.500	1712.7600	2.500	2838.2000	3.500	3950.5199	4.500	5049.7199	5.500	6135.7999
6.500	7208.7599	7.500	8268.5999	8.500	9315.3198	9.500	10348.9198				

Table V. (Contd.)

FGR V = 0.500,	G = 574.200 1/CM, RMIN = 1.5188710 AND RMAX = 1.6311431 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.7281650	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.56136035E-01 0.22658374E-01	
FGR V = 1.500,	G = 1712.760 1/CM, RMIN = 1.4834289 AND RMAX = 1.6788244 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.7224950	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.97697736E-01 0.39229474E-01	
FGR V = 2.500,	G = 2838.200 1/CM, RMIN = 1.4605683 AND RMAX = 1.7140474 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.7168250	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.12673954E-00 0.50625280E-01	
FGR V = 3.500,	G = 3950.520 1/CM, RMIN = 1.4428560 AND RMAX = 1.7442476 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.7111550	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.15069580E-00 0.59878376E-01	
FGR V = 4.500,	G = 5049.720 1/CM, RMIN = 1.4281304 AND RMAX = 1.7715936 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.7054850	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.17173158E-00 0.67876304E-01	
FGR V = 5.500,	G = 6135.800 1/CM, RMIN = 1.4154399 AND RMAX = 1.7970281 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.6998150	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.19079412E-00 0.75009913E-01	
FGR V = 6.500,	G = 7208.760 1/CM, RMIN = 1.4041987 AND RMAX = 1.8211572 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.6941450	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.20847923E-00 0.81524249E-01	
FGR V = 7.500,	G = 8268.600 1/CM, RMIN = 1.3941121 AND RMAX = 1.8442578 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.6884750	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.22507283E-00 0.87539440E-01	
FGR V = 8.500,	G = 9315.320 1/CM, RMIN = 1.3849045 AND RMAX = 1.8666328 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.6828050	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.24086412E-00 0.93173706E-01	
FGR V = 9.500,	G = 10348.920 1/CM, RMIN = 1.3764643 AND RMAX = 1.8883695 ANGSTROMS. THIS REQUIRED 0.	SECONDS.
	ALSC; BV = 0.6771350	
	THE KLEIN ACTION INTEGRALS F AND G ARE EQUAL TO 0.25595257E-00 0.98470822E-01	

Table VI. Relative-intensity program output.

SILICON NITRIDE INTENSITY DISTRIBUTION

TEST PROGRAM

THE REDUCED MASS OF THE TWO ATOMS, BASED ON O16=16, IS 9.335260

THE INPUT POTENTIAL POINTS, R IN ANGST. AND ENERGY IN 1/CM, ARE GIVEN BELOW.

R	V	R	V	R	V	R	V	R	V
1.361317	12376.7599	1.368619	11369.3999	1.376464	10348.9199	1.384905	9315.3199	1.394112	8268.6000
1.404199	7208.7599	1.415440	6135.2000	1.428130	5049.7200	1.442856	3950.5200	1.460568	2838.2000
1.483429	1712.7600	1.513871	574.2000	1.571800	0.	1.631143	574.2000	1.678824	1712.7600
1.714047	2838.2000	1.744246	3950.5200	1.771594	5049.7200	1.797928	6135.8000	1.821157	7208.7599
1.844258	8268.6000	1.866633	9315.3199	1.888569	10348.9199	1.909675	11359.3999	1.930590	12376.7599

DISSOCIATION ENERGY IN SAME UNITS AS ABOVE IS 0.50488000E 05

RMIN = 1.1000000, RMAX = 2.1000000, SPACING = 0.0010000, ALL IN ANGST.

THE TRIAL ENERGY LEVELS IN 1/CM ARE GIVEN BELOW.

LEVEL	ENERGY	LEVEL	ENERGY	LEVEL	ENERGY	LEVEL	ENERGY	LEVEL	ENERGY
0	5.7419999E 02	1	1.7127600E 03	2	2.8382000E 03	3	3.9505200E 03	4	5.0497200E 03
5	6.1358000E 03	6	7.2087600E 03	7	8.2686000E 03	8	9.3153199E 03	9	1.0348920E 04

THE INPUT POTENTIAL POINTS, R IN ANGST. AND ENERGY IN 1/CM, ARE GIVEN BELOW.

R	V	R	V	R	V	R	V	R	V
1.384105	10068.4039	1.398299	9287.5769	1.392577	8499.4209	1.399938	7699.8320	1.407413	6885.0470
1.416090	6051.6429	1.426104	5196.5350	1.437725	4316.9810	1.451471	3410.5770	1.468296	2475.2600
1.490367	1509.3070	1.525427	511.3330	1.580000	0.	1.644586	511.3330	1.699528	1509.3070
1.742138	2475.2600	1.779870	3410.5770	1.814980	4316.9810	1.848405	5196.5350	1.880569	6051.6429
1.911955	6885.0470	1.942380	7699.8320	1.971958	8499.4209	2.000637	9287.5769	2.028327	10068.4039

DISSOCIATION ENERGY IN SAME UNITS AS ABOVE IS 0.15871999E 05

RMIN = 1.1000000, RMAX = 2.1000000, SPACING = 0.0010000, ALL IN ANGST.

THE TRIAL ENERGY LEVELS IN 1/CM ARE GIVEN BELOW.

LEVEL	ENERGY	LEVEL	ENERGY	LEVEL	ENERGY	LEVEL	ENERGY
0	5.1133299E 02	1	1.5093070E 03	2	2.4752600E 03	3	3.4105770E 03

CONVERGENCE CRITERION IS ERROR LESS THAN 1.00E-03 1/CM



Table VI. (Contd.)

SILICON NITRIDE INTENSITY DISTRIBUTION

TEST PROGRAM

TIME BEFORE POTFIT = 0.

LEFT END OF POTENTIAL FUNCTION IS FOUND FROM  $Y=A/X*12+C$ , WHERE A = 6.5624240E 05 AND C = -5.4312680E 04

RIGHT END OF POTENTIAL FUNCTION IS FOUND FROM  $Y=A/X**B$ , WHERE A = -0.1843505E 06 AND B = 0.2396292E 01

TIME FOR POTFIT = 0.

THE POTENTIAL FUNCTION GENERATED IS

R(A)	V(I/CM)	R(A)	V(I/CM)	R(A)	V(I/CM)	R(A)	V(I/CM)	R(A)	V(I/CM)	
1.100000	205274.6602	1.105000	194199.1992	1.110000	183756.4551	1.115000	173907.6738	1.120000	164616.6484	21
1.125000	155849.4902	1.130000	147574.5371	1.135000	139762.1484	1.140000	132384.6191	1.145000	125415.9453	46
1.150000	118831.8906	1.155000	112609.6572	1.160000	106727.9414	1.165000	101166.7441	1.170000	95907.3340	71
1.175000	90932.1533	1.180000	86224.7275	1.185000	81769.5977	1.190000	77552.2588	1.195000	73559.1143	96
1.200000	69777.3779	1.205000	66195.0381	1.210000	62800.8188	1.215000	59584.1284	1.220000	56535.0068	121
1.225000	53644.0340	1.230000	50902.5591	1.235000	48302.1587	1.240000	45835.0869	1.245000	43494.0078	146
1.250000	41272.0205	1.255000	39162.6240	1.260000	37159.6997	1.265000	35257.4858	1.270000	33450.5459	171
1.275000	31737.7573	1.280000	30102.3035	1.285000	28551.6296	1.290000	27077.4470	1.295000	25675.7041	196
1.300000	24342.5852	1.305000	23074.4841	1.310000	21867.9983	1.315000	20719.9128	1.320000	19627.2021	221
1.325000	18586.9966	1.330000	17596.5886	1.335000	16653.4219	1.340000	15755.0769	1.345000	14899.2701	246
1.350000	14087.8391	1.355000	13306.7396	1.360000	12566.0364	1.365000	11859.6443	1.370000	11185.7922	271
1.375000	10535.2366	1.380000	9907.3490	1.385000	9304.0481	1.390000	8725.9846	1.395000	8171.7239	296
1.400000	7639.0359	1.405000	7128.5466	1.410000	6641.1568	1.415000	6175.7377	1.420000	5730.6632	321
1.425000	5305.6486	1.430000	4900.7443	1.435000	4515.9311	1.440000	4150.6864	1.445000	3804.0929	346
1.450000	3475.4547	1.455000	3164.4078	1.460000	2870.5324	1.465000	2593.6631	1.470000	2333.3247	371
1.475000	2089.1022	1.480000	1860.5940	1.485000	1647.3567	1.490000	1448.9069	1.495000	1264.9209	396
1.500000	1095.0128	1.505000	938.8093	1.510000	795.9440	1.515000	666.0608	1.520000	548.8205	421
1.525000	443.9079	1.530000	350.0660	1.535000	269.6675	1.540000	199.6944	1.545000	140.7352	446
1.550000	92.4844	1.555000	54.5443	1.560000	26.9235	1.565000	9.0385	1.570000	0.7111	471
1.575000	1.6714	1.580000	11.6533	1.585000	30.3970	1.590000	57.6488	1.595000	93.1608	496
1.600000	136.6916	1.605000	188.0049	1.610000	246.8704	1.615000	313.0620	1.620000	386.3606	521
1.625000	466.5507	1.630000	553.4224	1.635000	646.7746	1.640000	746.4041	1.645000	852.1140	546
1.650000	963.7133	1.655000	1081.0151	1.660000	1203.8379	1.665000	1332.0043	1.670000	1465.3398	571
1.675000	1603.6760	1.680000	1746.8437	1.685000	1894.6728	1.690000	2047.0255	1.695000	2203.7491	596
1.700000	2364.6935	1.705000	2529.7126	1.710000	2698.6600	1.715000	2871.4026	1.720000	3047.8218	621
1.725000	3227.7375	1.730000	3411.0101	1.735000	3597.5085	1.740000	3787.1060	1.745000	3979.6739	646
1.750000	4175.0509	1.755000	4373.2339	1.760000	4574.1024	1.765000	4777.5763	1.770000	4983.5575	671
1.775000	5192.0093	1.780000	5402.7653	1.785000	5615.6592	1.790000	5830.5624	1.795000	5047.3519	696
1.800000	6265.8502	1.805000	6486.0188	1.810000	6707.8674	1.815000	6931.3579	1.820000	7156.4438	721
1.825000	7383.1766	1.830000	7611.3573	1.835000	7840.8148	1.840000	8071.4157	1.845000	8303.0166	746
1.850000	8535.4229	1.855000	8768.7688	1.860000	9003.0602	1.865000	9238.2977	1.870000	9474.4625	771
1.875000	9711.5092	1.880000	9949.3544	1.885000	10187.8752	1.890000	10426.3159	1.895000	10666.2990	796
1.900000	10905.8453	1.905000	11145.4172	1.910000	11385.3303	1.915000	11629.5367	1.920000	11871.5869	821
1.925000	12111.5048	1.930000	12349.3149	1.935000	12585.0442	1.940000	12818.7108	1.945000	13050.3424	846
1.950000	13279.9598	1.955000	13507.5880	1.960000	13733.2465	1.965000	13956.9574	1.970000	14178.7441	871
1.975000	14392.6281	1.980000	14616.6288	1.985000	14832.7671	1.990000	15047.0646	1.995000	15259.5416	896
2.000000	15470.2192	2.005000	15679.1121	2.010000	15886.2465	2.015000	16091.6366	2.020000	16295.3030	921
2.025000	16497.2644	2.030000	16697.5393	2.035000	16896.1458	2.040000	17093.1035	2.045000	17288.4270	946
2.050000	17482.1350	2.055000	17674.2454	2.060000	17864.7749	2.065000	18053.7412	2.070000	18241.1592	971
2.075000	18427.0457	2.080000	18611.4172	2.085000	18794.2893	2.090000	18975.6775	2.095000	19155.5991	996

TIME FOR PRINT OF POTENTIAL = 0. SECONDS.

Table VI. (Contd.)

SILICON NITRIDE INTENSITY DISTRIBUTION

TEST PROGRAM

LEFT END OF POTENTIAL FUNCTION IS FOUND FROM  $Y=A/X^{**12}+C$ , WHERE A = 1.0824779E 06 AND C = -2.7700926E 04

RIGHT END OF POTENTIAL FUNCTION IS FOUND FROM  $Y=A/X^{**8}$ , WHERE A = -0.3839180E 07 AND B = 0.9183305E 01

TIME FOR PROFIT = 0.

THE POTENTIAL FUNCTION GENERATED IS

R(A)	V(I/CM)	R(A)	V(I/CM)	R(A)	V(I/CM)	R(A)	V(I/CM)	R(A)	V(I/CM)	
1.100000	333082.3633	1.105000	314813.2291	1.110000	297587.8828	1.115000	281342.2344	1.120000	266016.6016	21
1.125000	251555.0938	1.130000	237905.4756	1.135000	225018.8730	1.140000	212849.5664	1.145000	201354.6758	46
1.150000	190494.2188	1.155000	180230.5879	1.160000	170528.6445	1.165000	161355.5965	1.170000	152679.9531	71
1.175000	144473.3438	1.180000	136708.4023	1.185000	129359.6260	1.190000	122403.0869	1.195000	115816.3584	96
1.200000	109578.3477	1.205000	103669.2451	1.210000	98070.4512	1.215000	92764.4902	1.220000	87734.9345	121
1.225000	82966.3320	1.230000	78444.1611	1.235000	74154.7754	1.240000	70085.3184	1.245000	66223.6875	146
1.250000	62550.4990	1.255000	59079.0308	1.260000	55775.1885	1.265000	52637.4688	1.270000	49655.9048	171
1.275000	46025.0479	1.280000	44134.9478	1.285000	41576.0977	1.290000	39144.4199	1.295000	36832.2319	196
1.300000	34633.2397	1.305000	32541.4956	1.310000	30551.3860	1.315000	28657.6079	1.320000	26855.1719	221
1.325000	25139.3435	1.330000	23505.6565	1.335000	21949.8940	1.340000	20468.0662	1.345000	19055.4048	246
1.350000	17711.3640	1.355000	16429.5110	1.360000	15207.7144	1.365000	14042.9445	1.370000	12932.3400	271
1.375000	11873.1987	1.380000	10862.9611	1.385000	9884.9602	1.390000	9016.0759	1.395000	8309.4109	296
1.400000	7692.5469	1.405000	7136.3415	1.410000	6625.4777	1.415000	6150.2122	1.420000	5705.0557	321
1.425000	5285.9261	1.430000	4889.3934	1.435000	4513.5172	1.440000	4157.3465	1.445000	3820.1700	346
1.450000	3501.1172	1.455000	3199.1960	1.460000	2913.7604	1.465000	2644.3413	1.470000	2390.4904	371
1.475000	2151.8147	1.480000	1927.9307	1.485000	1718.4811	1.490000	1523.1176	1.495000	1341.4402	396
1.500000	1173.1340	1.505000	1017.8584	1.510000	875.2619	1.515000	744.9872	1.520000	626.6684	421
1.525000	519.9307	1.530000	424.1486	1.535000	339.1136	1.540000	264.4832	1.545000	199.8984	446
1.550000	145.0051	1.555000	99.4539	1.560000	62.9005	1.565000	35.0074	1.570000	15.4422	471
1.575000	3.8795	1.580000	-0.	1.585000	3.4838	1.590000	14.0343	1.595000	31.3561	496
1.600000	55.1595	1.605000	85.1637	1.610000	121.0958	1.615000	162.6905	1.620000	209.6907	521
1.625000	261.8466	1.630000	318.9180	1.635000	380.6708	1.640000	446.8793	1.645000	517.3263	546
1.650000	591.7890	1.655000	670.0799	1.660000	752.0042	1.665000	837.3752	1.670000	926.0130	571
1.675000	1017.7440	1.680000	1112.4018	1.685000	1209.8268	1.690000	1309.8631	1.695000	1412.3639	596
1.700000	1517.1861	1.705000	1624.2155	1.710000	1733.2920	1.715000	1844.2893	1.720000	1957.0878	621
1.725000	2071.5687	1.730000	2187.6226	1.735000	2305.1423	1.740000	2424.0285	1.745000	2544.1825	646
1.750000	2665.5164	1.755000	2787.9460	1.760000	2911.3916	1.765000	3035.7765	1.770000	3161.0305	671
1.775000	3287.0844	1.780000	3413.3755	1.785000	3541.3351	1.790000	3669.4180	1.795000	3798.0745	696
1.800000	3927.2545	1.805000	4056.9131	1.810000	4187.0065	1.815000	4317.4925	1.820000	4448.3563	721
1.825000	4579.5283	1.830000	4710.9673	1.835000	4842.6364	1.840000	4974.5015	1.845000	5106.5333	746
1.850000	5238.6945	1.855000	5370.9554	1.860000	5503.3289	1.865000	5635.3083	1.870000	5768.3916	771
1.875000	5901.0767	1.880000	6033.3647	1.885000	6166.7785	1.890000	6299.7972	1.895000	6432.9152	796
1.900000	6564.1324	1.905000	6699.4464	1.910000	6832.8605	1.915000	6966.3713	1.920000	7099.9904	821
1.925000	7233.7340	1.930000	7367.5164	1.935000	7501.6541	1.940000	7635.3669	1.945000	7770.2760	846
1.950000	7904.9041	1.955000	8039.7776	1.960000	8174.9232	1.965000	8310.3715	1.970000	8446.1519	871
1.975000	8582.2997	1.980000	8718.3488	1.985000	8855.8389	1.990000	8993.3083	1.995000	9131.3016	896
2.000000	9269.8649	2.005000	9417.9734	2.010000	9563.9174	2.015000	9706.2119	2.020000	9844.9547	921
2.025000	9980.2441	2.030000	10112.1746	2.035000	10240.8367	2.040000	10366.3202	2.045000	10488.7103	946
2.050000	10608.0906	2.055000	10724.5422	2.060000	10838.1436	2.065000	10948.9719	2.070000	11057.1008	971
2.075000	11162.6027	2.080000	11265.5474	2.085000	11366.0016	2.090000	11464.0341	2.095000	11559.7064	996

TIME FOR PRINT OF POTENTIAL = 0. SECONDS.

SCHR FINDS ENERGY LEVEL G = 510.74768 I/CM AND BV = 0.7193588 I/CM IN 0. SECONDS.

SCHR FINDS ENERGY LEVEL G = 1508.87561 I/CM AND BV = 0.7079762 I/CM IN 0. SECONDS.

SCHR FINDS ENERGY LEVEL G = 2475.04663 I/CM AND BV = 0.6975725 I/CM IN 0. SECONDS.

Table VI. (Contd.)

SCHR FINDS ENERGY LEVEL G =	3410.83838	1/CM AND BV =	0.6871293	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	574.28906	1/CM AND BV =	0.7281663	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	1712.95313	1/CM AND BV =	0.7224968	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	2838.48242	1/CM AND BV =	0.7168278	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	3950.87549	1/CM AND BV =	0.7111584	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	5050.12109	1/CM AND BV =	0.7054850	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	6136.20654	1/CM AND BV =	0.6998171	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	7209.21094	1/CM AND BV =	0.6941557	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	8269.12012	1/CM AND BV =	0.6884710	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	9315.89746	1/CM AND BV =	0.6827840	1/CM IN	0.	SECONDS.
SCHR FINDS ENERGY LEVEL G =	10349.67578	1/CM AND BV =	0.6770849	1/CM IN	0.	SECONDS.

## SILICON NITRIDE INTENSITY DISTRIBUTION TEST PROGRAM

PROGRAM SUCCESSFUL. (MAXIT REACHED 0 TIMES)

THE BELOW IS FOR THE LOWER STATE.

VIB. NO.	GIVEN ENERGY	CALC. ENERGY	DIFFERENCE DIFFERENCE = CALC. - GIVEN	GIVEN DELTA G	CALC. DELTA G	DIFFERENCE
0	574.20011	574.28906	0.08895			
1	1712.76016	1712.95313	0.19296	1138.56004	1138.66406	0.10402
2	2838.20023	2838.48242	0.28220	1125.44006	1125.52930	0.08923
3	3950.51993	3950.87549	0.35556	1112.31970	1112.39207	0.07336
4	5049.72003	5050.12109	0.40106	1099.20010	1099.24561	0.04550
5	6135.79974	6136.20654	0.40680	1086.07971	1086.08545	0.00574
6	7208.75989	7209.21094	0.45105	1072.96014	1073.00439	0.04425
7	8268.59961	8269.12012	0.52051	1059.83972	1059.90918	0.06946
8	9315.31982	9315.89746	0.57764	1046.72021	1046.77734	0.05713
9	10348.91968	10349.67578	0.75610	1033.59985	1033.77832	0.17847

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Table VI. (Contd.)

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VIB. NO.	CALC. EV
0	0.72816626
1	0.72249678
2	0.71682784
3	0.71115841
4	0.70548503
5	0.69981708
6	0.69415566
7	0.68847096
8	0.68278404
9	0.67708492

SILICON NITRIDE INTENSITY DISTRIBUTION

TEST PROGRAM

THE BELOW IS FOR THE UPPER STATE.

VIB. NO.	GIVEN ENERGY	CALC. ENERGY	DIFFERENCE DIFFERENCE = CALC. - GIVEN
0	511.33312	510.74768	-0.58544
1	1509.30696	1508.87561	-0.43135
2	2475.26004	2475.04663	-0.21341
3	3410.57684	3410.83838	0.26154

VIB. NO.	CALC. BV
0	0.71835880
1	0.70797616
2	0.69757245
3	0.68712933

Table VI. (Contd.)

## FRANCK-COONON FACTORS

V''	V' = 0	V' = 1	V' = 2	V' = 3
0	0.9812E 00	0.1862E-01	0.9118E-04	0.4651E-04
1	0.1691E-01	0.9232E 00	0.5966E-01	0.2385E-07
2	0.1760E-02	0.5015E-01	0.8193E 00	0.1274E-00
3	0.8185E-04	0.7427E-02	0.9868E-01	0.6680E 00
4	0.4064E-05	0.5441E-03	0.1995E-01	0.1549E-00
5	0.1551E-06	0.3818E-04	0.2149E-02	0.4233E-01
6	0.1278E-07	0.2180E-05	0.2003E-03	0.6418E-02
7	0.3751E-09	0.1336E-06	0.1611E-04	0.7658E-03
8	0.1501E-09	0.1471E-07	0.8705E-06	0.8276E-04
9	0.4100E-09	0.3401E-08	0.1801E-06	0.4551E-05

## R-CENTROID FACTORS (ANGSTROMS)

V''	V' = 0	V' = 1	V' = 2	V' = 3
0	0.1592E 01	0.1300E 01	0.2791E 01	0.1710E 01
1	0.1906E 01	0.1593E 01	0.1393E 01	0.1489E 03
2	0.1733E 01	0.1864E 01	0.1603E 01	0.1442E 01
3	0.1911E 01	0.1763E 01	0.1842E 01	0.1611E 01
4	0.1894E 01	0.1898E 01	0.1786E 01	0.1830E 01
5	0.2009E 01	0.1904E 01	0.1892E 01	0.1804E 01
6	0.1988E 01	0.1980E 01	0.1915E 01	0.1890E 01
7	0.2056E 01	0.1994E 01	0.1962E 01	0.1927E 01
8	0.1321E 01	0.1838E 01	0.2078E 01	0.1953E 01
9	0.1439E 01	0.1261E 01	0.1788E 01	0.2129E 01

## R\*\*2-CENTROIDS

V''	V' = 0	V' = 1	V' = 2	V' = 3
0	0.2503E 01	0.1611E 01	0.6121E 01	0.2761E 01
1	0.3532E 01	0.2542E 01	0.1872E 01	0.4512E 03
2	0.3044E 01	0.3406E 01	0.2579E 01	0.2059E 01
3	0.3587E 01	0.3137E 01	0.3341E 01	0.2609E 01
4	0.3615E 01	0.3560E 01	0.3209E 01	0.3311E 01
5	0.3977E 01	0.3640E 01	0.3550E 01	0.3268E 01
6	0.3616E 01	0.3890E 01	0.3673E 01	0.3552E 01
7	0.4176E 01	0.3977E 01	0.3838E 01	0.3711E 01
8	0.1626E 01	0.3451E 01	0.4265E 01	0.3812E 01
9	0.2080E 01	0.1449E 01	0.3291E 01	0.4440E 01

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Table VI. (Contd.)

RELATIVE INTENSITY(QUANTUM/SEC) SCALED TO TEN

V''	V' = 0	V' = 1	V' = 2	V' = 3
0	10.000	0.232	0.001	0.001
1	0.149	10.000	0.836	0.000
2	0.013	0.471	10.000	2.188
3	0.001	0.060	1.044	10.000
4	0.000	0.004	0.182	2.011
5	0.000	0.000	0.017	0.474
6	0.000	0.000	0.001	0.052
7	0.000	0.000	0.000	0.036
8	0.000	0.000	0.000	0.001
9	0.000	0.000	0.000	0.000

RELATIVE INTENSITY(ENERGY/SEC) SCALED TO TEN

V''	V' = 0	V' = 1	V' = 2	V' = 3
0	10.000	0.243	0.002	0.001
1	0.142	10.000	0.875	0.000
2	0.012	0.449	10.000	2.291
3	0.000	0.054	0.996	10.000
4	0.000	0.003	0.165	1.918
5	0.000	0.000	0.014	0.431
6	0.000	0.000	0.001	0.053
7	0.000	0.000	0.000	0.035
8	0.000	0.000	0.000	0.000
9	0.000	0.030	0.000	0.000

CONSTANTS

0  
0  
0.24299999E 05  
0.73100000E 00  
0.72350000E 00  
0.56694999E-02  
0.10370000E-01  
-0.  
-0.

TIME = 0.

REFERENCES

1. R. N. Zare, Lawrence Radiation Laboratory Report UCRL-11110, November 1963, J. Chem. Phys. (to be published).
2. All timing information refers to IBM 7094.
3. R. N. Zare and J. K. Cashion, Lawrence Radiation Laboratory Report UCRL-10881, July 1963 (unpublished).

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