

# **ANL Critical Assembly Covariance Matrix Generation**

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**Nuclear Engineering Division**

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Since the advent of the nuclear power industry, experiments have been performed at various research facilities throughout the world dealing with specific physics and criticality issues. To archive and evaluate this vast quantity of highly specific (and expensive to produce) information in a single standardized format, two separate international projects have been initiated; they are the International Reactor Physics Experiment Evaluation Project (IRPhEP) and the International Criticality Safety Benchmark Evaluation Project (ICSBEP).

Uncertainties from these evaluated benchmark reports can be used to generate a covariance matrix, which in turn, can be used to make gross data adjustments to nuclear cross sections to better fit experimentally measured integral data from these experiments.

This report discusses the generation of a covariance matrix for selected critical assemblies that were carried out by Argonne National Laboratory (ANL) using four critical facilities – all of which are now decommissioned. The four different ANL critical facilities are: ZPR-3 located at ANL-West (now Idaho National Laboratory, INL), ZPR-6 and ZPR-9 located at ANL-East (Illinois) and ZPPR located at ANL-West.

There is reactivity uncertainty data reported for 33 Argonne National Laboratory (ANL) critical configurations available in the ICSBEP database. Shown in Table 1 are the ICSBEP identification names and assembly configuration “names” for the 33 ANL benchmark evaluations considered in this report.

Table 1. ANL Benchmark Evaluations used to develop the ANL Correlation Matrix.

ICSBEP ID Name	Configuration
<b>ZPR-3</b>	
IEU-MET-FAST-015	ASSEMBLY 6F
IEU-MET-FAST-016	ASSEMBLY 11
IEU-COMP-FAST-004	ASSEMBLY 12
HEU-MET-FAST-055	ASSEMBLY 23
IEU-MET-FAST-012	ASSEMBLY 41
MIX-COMP-FAST-003	ASSEMBLY 48
MIX-COMP-FAST-003	ASSEMBLY 48B
MIX-COMP-FAST-004	ASSEMBLY 56B
<b>ZPR-6</b>	
IEU-COMP-INTER-005	ASSEMBLY 6A
MIX-COMP-FAST-001	ASSEMBLY 7
MIX-COMP-FAST-002	ASSEMBLY 7 HIGH 240PU CORE
PU-MET-INTER-002	ASSEMBLY 10
<b>ZPR-9</b>	
IEU-MET-FAST-013	ASSEMBLY 1

IEU-MET-FAST-014	ASSEMBLY 2
IEU-MET-FAST-014	ASSEMBLY 3
HEU-MET-FAST-060	ASSEMBLY 4
HEU-MET-FAST-067	ASSEMBLY 5
HEU-MET-FAST-067	ASSEMBLY 6
HEU-MET-FAST-070	ASSEMBLY 7
HEU-MET-FAST-070	ASSEMBLY 8
HEU-MET-FAST-070	ASSEMBLY 9
IEU-MET-FAST-010	ASSEMBLY 34 (U9 BENCHMARK) L11
HEU-MET-INTER-001	ASSEMBLY 34 (URANIUM/IRON BENCHMARK) L303
<b>ZPPR-20</b>	
HEU-MET-FAST-075	PHASE C
HEU-MET-MIXED-012	PHASE D
SUB-HEU-MET-MIXED-001	PHASE D subcritical
SUB-HEU-MET-FAST-001	PHASE E subcritical
<b>ZPPR-21</b>	
PU-MET-FAST-033	PHASE A
MIX-MET-FAST-011	PHASE B
MIX-MET-FAST-011	PHASE C
MIX-MET-FAST-011	PHASE D
MIX-MET-FAST-011	PHASE E
HEU-MET-FAST-061	PHASE F

The approximate experiment dates of the assemblies considered are shown in Figure 1 (shown as ✕'s) along with the operational history of each specific machine (shown as solid lines). Each horizontal line represents the operational history for each machine. As seen from Figure 2, these machines were operated from the mid-fifties to the early nineties.

### ANL Critical Assembly Dates

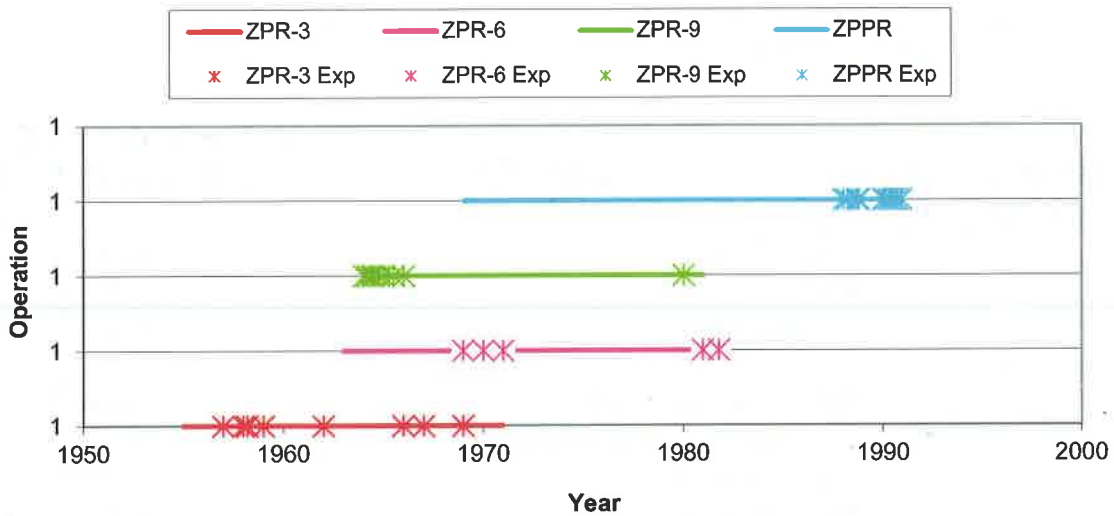


Figure 1. Dates of Critical Machine Operation and Specific Critical Configuration Loadings.

For each configuration, a summary of the reactivity uncertainties are included as a special table in the benchmark document. Three examples of the tabular uncertainty data for ZPR-9 Assembly 1, ZPR-9 Assembly 4 and ZPR-6 Assembly 10 are shown in Tables 2 - 4. This data is subdivided into three general classes: “Measurement Technique”, “Geometry” and “Composition”. The “Total” value at the bottom of each table is a quadrature sum of the individual (uncorrelated) entries for all three classes. As would be expected, the majority of the uncertainty type differences will occur in the composition class. (Uncertainty data for all 33 assemblies considered are given in Appendix B.)

Table 2. Uncertainties for ZPR-9 Assembly 1 (IEU-MET-FAST-013).

A CYLINDRICAL ASSEMBLY OF U METAL (93% <sup>235</sup> U) AND DEPLETED URANIUM WITH ALUMINUM REFLECTORS		
Source of Uncertainty	Uncertainty Type	Uncertainty in Excess Reactivity (% $\Delta k$ )
Measurement Technique		
	Data Fitting	0.0002
	Ih to $\Delta k$	0.0093
	Temperature	0.0037
Geometry		
	Matrix Interface Gap	<0.0001
	Nominal Plate Dimensions	<0.0001
	Matrix Tube Pitch	0.0450
	Room Return	0.0520
Composition		
	Enriched Uranium	0.0732
	Depleted Uranium	0.0036
	Kel-F	0.0008
	Aluminum	0.0124
	Humidity	0.0001
	Total	0.1018

Table 3. Uncertainties for ZPR-9 Assembly 4 (HEU-MET-FAST-060).

A CYLINDRICAL ASSEMBLY OF U METAL (93% 235U) AND TUNGSTEN WITH ALUMINUM REFLECTORS		
Source of Uncertainty	Uncertainty Type	Uncertainty in Excess Reactivity (% $\Delta k$ )
Measurement Technique		
	Data Fitting	0.0002
	Ih to $\Delta k$	0.0083
	Temperature	0.0041
Geometry		
	Matrix Interface Gap	0.0046
	Nominal Plate Dimensions	0.0037
	Matrix Tube Pitch	0.0342
	Room Return	0.0427
	Uranium Axial Distribution	0.0375
Composition		
	Enriched Uranium	0.0891
	Kel-F	0.0004
	Tungsten	0.0179
	Aluminum	0.0165
	Humidity	0.0001
	Total	0.1142

Table 4. Uncertainties for ZPR-6 Assembly 10 (PU-MET-INTER-002).

A CYLINDRICAL PLUTONIUM/CARBON/STAINLESS STEEL ASSEMBLY WITH STAINLESS STEEL AND IRON REFLECTORS		
Source of Uncertainty	Uncertainty Type	Uncertainty in Excess Reactivity (% $\Delta k$ )
Measurement Technique		
	Excess in $I_h$ (including temperature uncertainty)	0.0020
	$I_h$ to $\Delta k$	0.0034
Geometry		
	Matrix Interface Gap	0.0073
	Nominal Plate Dimensions	0.0058
	Matrix Tube Pitch	0.0374
	PSR Blades	0.0003
	Room Return	0.0017
Composition		
	Plutonium	0.0333
	Graphite	0.0160
	Stainless Steel and Iron	0.1151
	Humidity	0.0001
	Total	0.1270

Shown in Table 5 are the “Total” uncertainties, by configuration, for all 33 configurations considered; these “Total” uncertainties are shown graphically in Figure 2.

Table 5. Total Uncertainties for all Assemblies Considered.

<b>Assembly</b>	<b>ICSBEP Number</b>	<b>Total Uncertainty in Excess Reactivity (% <math>\Delta k</math>)</b>
ZPR-3/6F	IEU-MET-FAST-015	0.1130
ZPR-3/11	IEU-MET-FAST-016	0.1197
ZPR-3/12	IEU-COMP-FAST-004	0.1070
ZPR-3/23	HEU-MET-FAST-055	0.2031
ZPR-3/41	IEU-MET-FAST-012	0.1759
ZPR-3/48	MIX-COMP-FAST-003	0.0687
ZPR-3/48B	MIX-COMP-FAST-003	0.0680
ZPR-3/56B	MIX-COMP-FAST-004	0.1153
ZPR-6/6A	IEU-COMP-INTER-005	0.0939
ZPR-6/7	MIX-COMP-FAST-001	0.0867
ZPR-6/7 High Pu	MIX-COMP-FAST-002	0.0855
ZPR-6/10	PU-MET-INTER-002	0.1270
ZPR-9/1	IEU-MET-FAST-013	0.1018
ZPR-9/2	IEU-MET-FAST-014	0.1009
ZPR-9/3	IEU-MET-FAST-014	0.1015
ZPR-9/4	HEU-MET-FAST-060	0.1142
ZPR-9/5	HEU-MET-FAST-067	0.1120
ZPR-9/6	HEU-MET-FAST-067	0.1176
ZPR-9/7	HEU-MET-FAST-070	0.1220
ZPR-9/8	HEU-MET-FAST-070	0.1249
ZPR-9/9	HEU-MET-FAST-070	0.1183
ZPR-9/34 U9	IEU-MET-FAST-010	0.1222
ZPR-9/34 U/Fe	HEU-MET-INTER-001	0.1086
ZPPR-20/C	HEU-MET-FAST-075	0.1645
ZPPR-20/D	HEU-MET-MIXED-012	0.1104
ZPPR-20/Dsub	SUB-HEU-MET-MIXED-001	0.3168
ZPPR-20/Esub	SUB-HEU-MET-FAST-001	0.7159
ZPPR-21A	PU-MET-FAST-033	0.1507
ZPPR-21/B	MIX-MET-FAST-011	0.1434
ZPPR-21/C	MIX-MET-FAST-011	0.1474
ZPPR-21/D	MIX-MET-FAST-011	0.1518
ZPPR-21/E	MIX-MET-FAST-011	0.1655
ZPPR-21/F	HEU-MET-FAST-061	0.1766

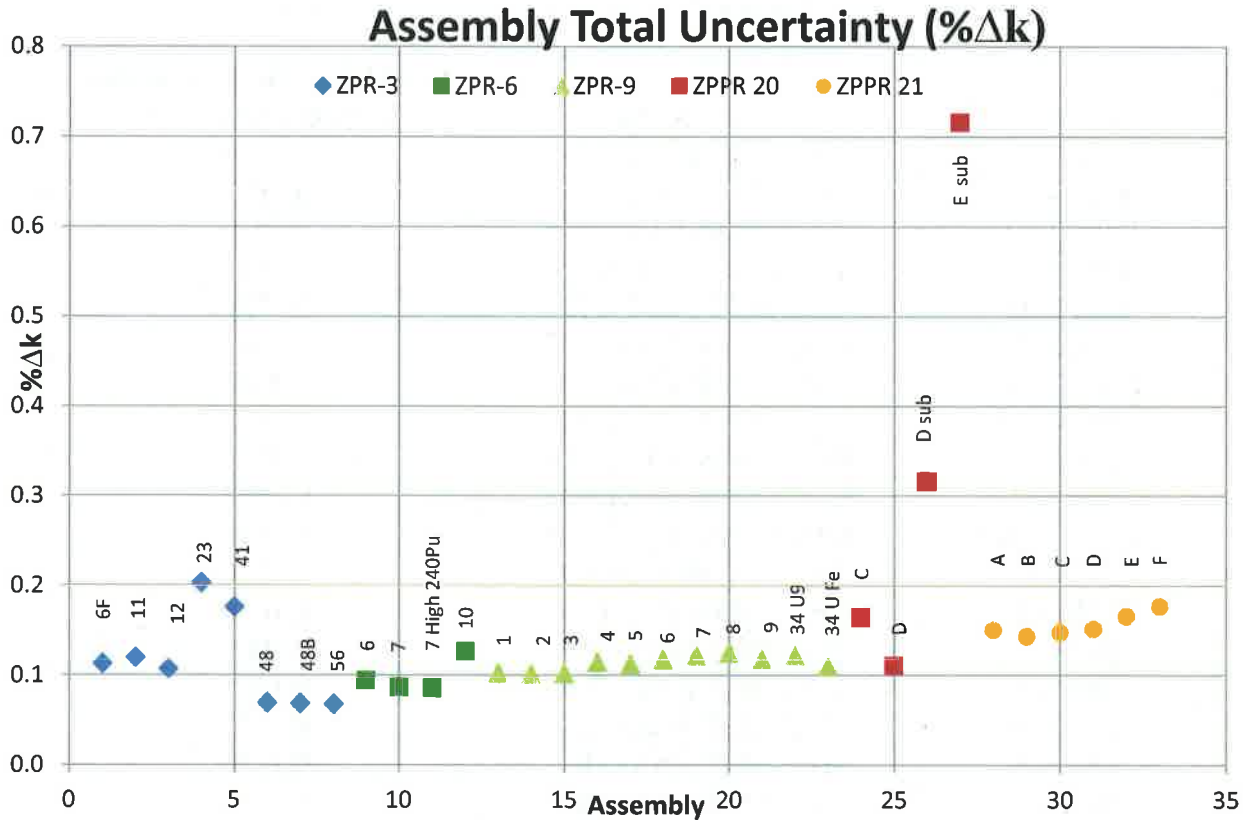


Figure 2. Assembly Total Uncertainties by Specific Machine.

As seen from Figure 2, the two ZPPR20 subcritical assemblies have the largest uncertainties, mainly due to measurement technique uncertainties (see Tables B22 and B23). The relatively large difference in the ZPR-3 assemblies 23 and 41 from other ZPR-3 assembly's results mainly from a large "Uranium Axial Distribution" uncertainty involving only these two ZPR-3 assemblies (see "EU Piece Sizes" in Tables B43 and B5). In addition, the concave nature of the ZPPR21 set of experiments in Figure 2 is due to the semi-linear decrease of plutonium atoms with a correspondingly semi-linear increase of uranium atoms in the A→F series (see Figure 3).



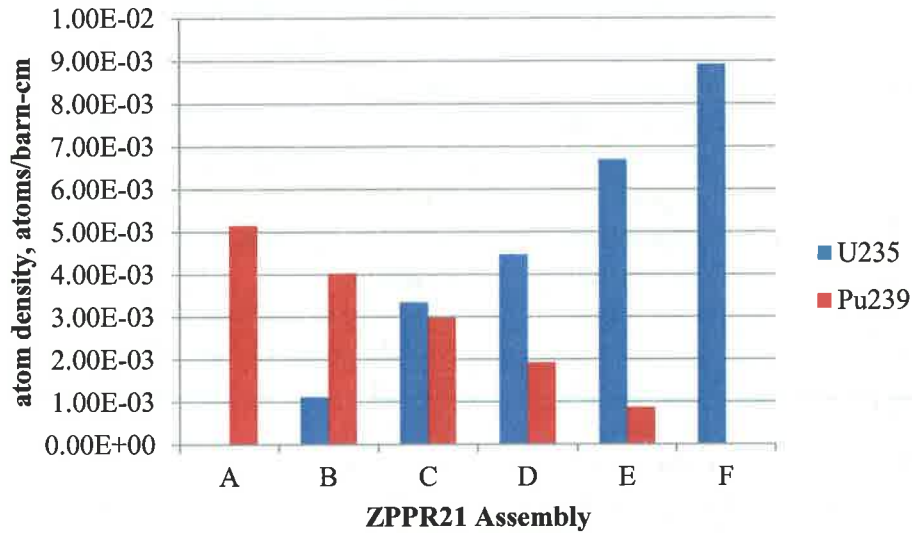


Figure 3 U235 and Pu239 Atom Densities for ZPPR21 Assemblies.

Upon evaluating each configuration and combining uncertainties that are the same (but with different descriptions), the distinct uncertainties shown in Table 6 were obtained. It turns out that there were 62 totally uncorrelated types of uncertainty considered in the three major uncertainty classes (Measurement Technique, Geometry and Composition) for the 33 ANL configurations. Because of the varying makeup of these assemblies, most of these uncertainty types (48 out of 62) are composition related.

Table 6. Distinct Uncertainty Types in ANL Critical Assemblies.

Number	Uncertainty Class	Type
1	Measurement Technique	Excess Reactivity
2	Measurement Technique	Inhours to $\Delta k$
3	Measurement Technique	Temperature
4	Measurement Technique	Reproducibility
5	Geometry	Room Return
6	Geometry	13 Unknown Reflector Positions
7	Geometry	Matrix Interface Gap
8	Geometry	Matrix Tube Pitch
9	Geometry	Missing Axial Reflector Drawer
10	Geometry	Nominal Plate, Drawer Dimensions
11	Geometry	Aluminum Perforations
12	Geometry	Uranium Axial Distribution
13	Geometry	PSR Axial Position
14	Geometry	PSR Blades
15	Composition	Aluminum in Core
16	Composition	Aluminum in Pu-Al Plates
17	Composition	Aluminum in Matrix Tubes
18	Composition	Aluminum Drawers

19	Composition	Aluminum in Reflectors
20	Composition	Autorod Blade
21	Composition	Beryllium
22	Composition	Beryllium Oxide in Reflectors
23	Composition	Beryllium Oxide in SP-100 rods
24	Composition	Depleted Lithium Plates in core
25	Composition	Lithium Hydride in Shield
26	Composition	Graphite
27	Composition	Graphite in Ax/Rad Refl.
28	Composition	Molybdenum in Pu-U-Mo Plates
29	Composition	Nickel
30	Composition	Niobium
31	Composition	Rhenium
32	Composition	Sand
33	Composition	Sodium
34	Composition	Sodium Carbonate
35	Composition	Tungsten
36	Composition	Zirconium
37	Composition	Hydrogen in Zirconium
38	Composition	Steel Plates in the Core
39	Composition	Steel in the Cans
40	Composition	Steel in Drawers
41	Composition	Steel in Matrix Tubes
42	Composition	Steel in Reflectors
43	Composition	Steel in Shield
44	Composition	Iron Oxide Plates
45	Composition	Enriched Uranium
46	Composition	Depleted Uranium in Pu-U-Mo Plates
47	Composition	Depleted Uranium in Core
48	Composition	Depleted Uranium in Reflectors
49	Composition	Depleted Uranium in Blanket
50	Composition	Depleted Uranium in Shield
51	Composition	Depleted Uranium Oxide Plates
52	Composition	Plutonium
53	Composition	PSR Blades
54	Composition	"Control" Boron Carbide
55	Composition	Polyethylene in core
56	Composition	Borated Polyethylene in reflector
57	Composition	Borated Polyethylene in shield
58	Composition	Kel-F on core fuel
59	Composition	Kel-F on core DU fuel
60	Composition	Kel-F on core BeO plates
61	Composition	Kel-F on reflector BeO plates
62	Composition	Humidity

There are a total of 2046 (33 x 62) possible uncertainty entries from the ANL benchmark calculations. However, because of the diverse nature of these ANL assemblies, approximately 70% of the possible entries in this overall uncertainty matrix are zero.

In probability theory and statistics, covariance is a measure of how much two variables change together. A perfect correlation gives a 1.0 value, whereas no correlation gives a 0.0 value. The procedure used to determine covariance factors between sets of data has been set forth separately by both Ivanova and Ishikawa, References 1 and 2. In Ishikawa's report there are two types of errors, "common" and "independent", whereas Ivanova uses the equivalent terms "systematic" and "random". Covariance factors involve only "common" or "systematic" errors. In this report, we follow the mathematical terminology as described by Ishikawa.

According Equation 7 of Ishikawa's report, the covariance factor ( $\rho_{A,B}$ ) for data from assembly A and assembly B is defined as the sum over all uncertainty types "i" (see Table 6) of the common fractional uncertainty for assembly A ( $\sigma_{Common,i} / \sigma_{Total}$ ) times the common fractional uncertainty for assembly B ( $\sigma_{Common,i} / \sigma_{Total}$ ); mathematically, this relationship is

$$\rho_{A,B} = \sum_i \frac{\sigma_{Common,A,i}}{\sigma_{Total,A}} * \frac{\sigma_{Common,B,i}}{\sigma_{Total,B}}$$

The "Total" uncertainties ( $\sigma_{Total}$ ) for each ANL assembly were shown numerically in Table 5 and graphically in Figure 2.

Notice that in the above equation that the numerators are common (or systematic) uncertainties, and therefore do not include any random uncertainties. In this analysis, common uncertainties are defined as the published uncertainties times a common factor between the two uncertainty types. For example, uranium plates that come from the same fuel "melt" will have a common factor of 1.0, whereas, plates from two different manufactures (or melts) will have a common factor of 0.0.

As an illustrative example, we will calculate the  $\rho_{A,B}$  for highly-enriched uranium fuel in the core region for ZPR-9 Assemblies 1 (Table 2) and 4 (Table 3). As seen from the above equation, the correlation factor is  $(0.0732/0.1018) * (0.0891/0.1142) * (\text{a common factor between the two types of uranium plates})$ . Since the same types of highly-enriched uranium plates were used in both configurations, this makes the common factor between the plates in each assembly 1.0. Thus, the highly-enriched uranium fuel correlation factor for ZPR-9 Assembly 1 and ZPR-9 Assembly 4 is **0.5610**.

By reviewing the sorted ratio of ( $\sigma_i / \sigma_{Total}$ ) for all assemblies, it becomes apparent that there are a relative few uncertainty types (out of 62 total) that are important in calculating the correlation coefficients. In this analysis, there were only 14 uncertainty types deemed to be important; the types considered are shown in Table 7. Of these 14 uncertainty types, two are related to measurement technique (Excess Reactivity and Inhours to  $\Delta k$ ), three are related to geometry (Room Return, Matrix Interface Gap and Matrix Tube Pitch) while the remaining nine are related to composition. Except for matrix tube materials and steel in cans, the composition related terms deal with either uranium and/or plutonium. Using only these 14 uncertainty types gets within 10 percent of the overall  $\sigma_{Total}$  values while reducing unnecessary calculational time and effort.

Table 7. Major Uncertainty Type Weighting Matrices.

Number	Number (out of 62)	Weighting Matrix No.	Major Uncertainty Type
1	1	1	Excess Reactivity
2	2	1	Inhours to $\Delta k$
3	5	1	Room Return
4	7	1	Matrix Interface Gap
5	8	1	Matrix Tube Pitch
6	17	1	Aluminum in Matrix Tubes
7	41	2	Steel in Matrix Tubes
8	39	3	Steel in the Cans
9	45	3	Enriched Uranium
10	47	3	Depleted Uranium in Core
11	49	3	Depleted Uranium in Blanket
12	51	3	Depleted Uranium Oxide Plates
13	52	4	Plutonium
14	46	4	Depleted Uranium in Pu-U-Mo Plates

In the above estimate for the  $\rho_{A,B}$  for highly-enriched uranium fuel in the core region for ZPR-9 Assemblies 1 and 4, a common factor of 1.0 was assumed. In this overall analysis, four different types of common factor matrices were used (see Table 7). Matrix 1 had 1's only for each machine with no interactions with other machines, while Matrix 2 was made especially for steel in matrix tubes. In addition, Matrix 3 had not only 1's only for each machine, but 1's for interactions with all other machines. This results because most of the plates were made at ANL-East with the same composition fuel. Matrix 4 was specially made up for plutonium containing plates; it attempts to take into account plates from various independent vendors. These common-factor matrices are shown in Appendix A1.

When these common-factor matrices were used with the basic uncertainty data and summed over all 14 uncertainty types from Table 7, the covariance matrix shown graphically in Figure 4 was obtained. (All diagonal terms are unity by definition.) Instead of showing just numbers in a table, it was thought that a color coding scheme gives greater insight into the relationships between assemblies. Figure 5 is a copy of Figure 4, but with the actual covariance values in each grid location.

In Figures 4 and 5 there are several ranges where the correlation coefficients are very small; this usually happens when one assembly had enriched uranium as the fissile material and the other assembly had plutonium as the fissile material.

Finally, Appendix A contains ancillary figures and tables related to the generation and interpretation of Figures 4 and 5, while Appendix B shows basic uncertainty values for all the evaluated ANL benchmarks.

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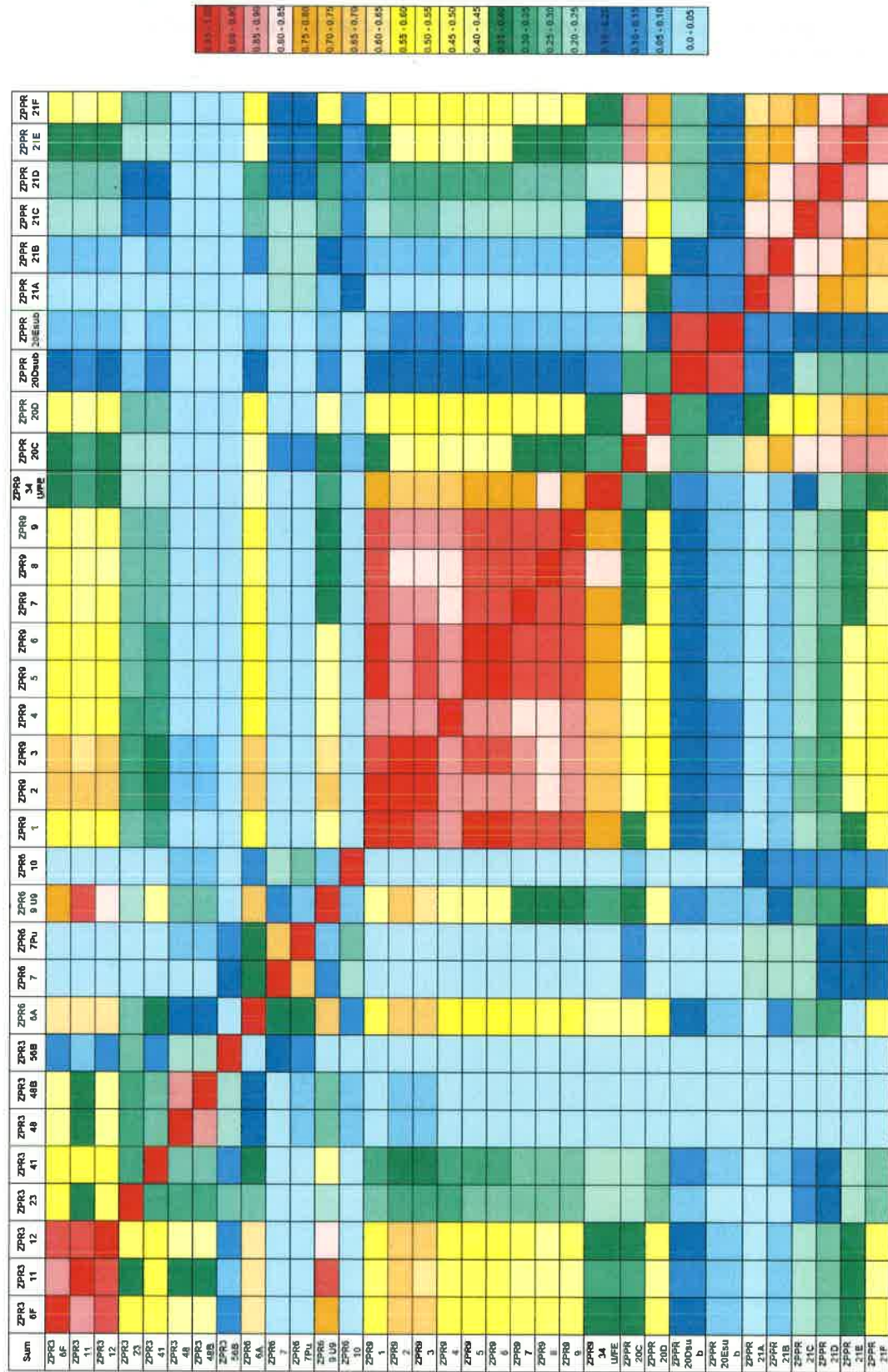


Figure 4. Overall Covariance Factors for ANL Critical Assemblies.





## References

- 1) Tatiana Ivanova, et. al., “Towards validation of criticality calculations for systems with MOX powders,” Annals of Nuclear Energy, 36 (2009) 305-309.
- 2) M. Ishikawa, “How to Determine Error Matrix of Integral Data, Appendix A,” Draft, November 25, 2011. **(MORE definition is needed for this reference.)**

## Appendix A. Supplementary Figures and Tables

Appendix A contains ancillary figures and tables related to the generation and interpretation of Figures 4 and 5. Appendix A.1 shows the weighting matrices, while Appendix A.2 shows fractional covariance matrices. Fractional covariance matrices are the ratio of the individual uncertainty type matrix to the total covariance matrix. (Diagonal terms are the squared ratio of the individual uncertainty type uncertainty to the total uncertainty.) These fractional matrices indicate which uncertainty type in the overall covariance term. These fractional covariance matrices are also shown using a color scheme instead of actual numbers. Also included in Appendix A are additional calculated quantities for each assembly considered in this report (Appendix A.3), plus a section dealing with how the enriched uranium covariance matrix changes with assumed common factors (Appendix A.4). The last section of Appendix A (Appendix A.5) shows correlation coefficients for all 62 uncertainty types plus combined correlation coefficients for the three major grouping (measurement technique, geometry and composition) in addition to the total correlation coefficient matrix when 62 terms are assumed.

### A.1 Weighting Matrices

Shown in Figures A1-A4 are the “common” weighting matrices for the 14 major uncertainty types. Which matrix goes with which uncertainty type is shown in Table A1. (Table A1 is a reformatting of Table 7 from the main text.)

Table A1. Matrix Figure for Major Uncertainty Types.

Major Uncertainty Type Weighting Matrix	Matrix Figure
Excess Reactivity	A1
Inhours to $\Delta k$	A1
Room Return	A1
Matrix Interface Gap	A1
Matrix Tube Pitch	A1
Aluminum in Matrix Tubes	A1
Steel in Matrix Tubes	A2
Steel in the Cans	A3
Enriched Uranium	A3
Depleted Uranium in Core	A3
Depleted Uranium in Blanket	A3



Depleted Uranium Oxide Plates	A3
Plutonium	A4
Depleted Uranium in Pu-U-Mo Plates	A4

As seen from Figure A1, excess reactivity, room return, etc., uncertainty types were assumed only a function of a specific machine. Thus, there are 1's associated with each specific machine and no correlation between machines.

Shown in Figure A2 is the weighting matrix for stainless steel tubes. There were aluminum tubes in ZPR-9 assemblies 1-9, but steel tubes in ZPR-9 assembly 34; all other machines had stainless steel tubes. Thus, ZPR-9 assemblies 1-9 do not correlate with any other machine. In addition, ZPR-3 also does not correlate to any other machine because it used a different steel composition than the other steel-tubed machines.

As seen from Figure A3, enriched uranium, depleted uranium, etc., uncertainty types were assumed not a function of a specific machine. Most of the uranium plates were made at ANL and the only mass differences occur because of plate sizing. Thus, there are 1's everywhere.

As seen from Figure A4, the varying weighting terms attempted to distinguish plutonium-containing plates from various vendors.

## A.2 Fractional Covariances

Shown in Figures A5 – A18 are the fractions of the covariance data due to the 14 uncertainty types considered. Thus, if the values in all the non-diagonal matrix locations were added, the sum in each cell would be 1.0. The diagonal terms are the individual uncertainty type squared divided by the total uncertainty squared and will also sum to 1.0. (Recall that the total uncertainty is the quadrature sum of the individual uncertainties.) Thus, the diagonal terms are uncertainty fractions, not covariance fractions. From these figures, the relative importance of each uncertainty type can be assessed relatively easily. As would be expected, the enriched uranium and plutonium terms would be very important. In addition, the steel matrix type will also be important because of the large steel mass associated with the tubes. Due to the color shading in these figures, the relative importance of each uncertainty type can be easily assessed.

## A.3 Additional Calculated Parameters

Shown in Tables A2 – A6 are several calculated quantities for the 33 critical assemblies considered in this report. These parameters include core and total spectral indices (ratios of fission rates for U238/U235 [28f/25f] and U238/Pu239 [28f/49f]), energy-dependent fission fractions (fast, intermediate and thermal), core and total leakage fractions, volume, U235 and Pu239 enrichment, and k-eff calculated over experimental (C/E) values using various ENDF/B cross section datasets.

## A.4 Common Matrix Variations

Shown in Figures A1-A4 are the common matrices used in this report for the 14 major uncertainty types (see also Table A1). Shown in this section of the appendix is an example of

what the covariance matrix for enriched uranium would look like if non-unity values were assumed in the common matrix. Figure A19 shows what the enriched uranium covariance matrix would look like if there was no commonality between any assembly; as expected, only large numbers would occur along the diagonal in assemblies that contained enriched uranium. Figures A20 – A22 show the corresponding plots for 25%, 50% and 100% commonality. These figures show the obvious fact that the higher the commonality, the higher the covariance factors will be. In addition, these figures also show graphically how the enriched uranium covariance factors spread over assemblies as commonality values increase.

### A.5 Covariance Matrices for All 62 Uncertainty Types

Shown in Figures A23 – A84 are the individual covariance matrices for the 62 uncertainty types given in Table 6 (and in the same order as Table 6). Which weighting matrix goes with each uncertainty type (and related class) is shown in Table A.2. Weighting matrix assignments may, at times, seem arbitrary, but each type was looked at in terms of appropriateness in order to make a suitable engineering judgment. (Some choices were made assuming each machine is independent, while other composition-related choices used material compositions to assign the common matrix weighting.)

Table A.2. Distinct Uncertainty Types in ANL Critical Assembly Weighting Matrices.

Number	Uncertainty Class	Type	Weighting Matrix No.
1	Measurement Technique	Excess Reactivity	1
2	Measurement Technique	Inhours to $\Delta k$	1
3	Measurement Technique	Temperature	1
4	Measurement Technique	Reproducibility	1
5	Geometry	Room Return	1
6	Geometry	13 Unknown Reflector Positions	1
7	Geometry	Matrix Interface Gap	1
8	Geometry	Matrix Tube Pitch	1
9	Geometry	Missing Axial Reflector Drawer	1
10	Geometry	Nominal Plate, Drawer Dimensions	1
11	Geometry	Aluminum Perforations	1
12	Geometry	Uranium Axial Distribution	1
13	Geometry	PSR Axial Position	1
14	Geometry	PSR Blades	1
17	Composition	Aluminum in Matrix Tubes	1
20	Composition	Autorod Blade	1
27	Composition	Graphite in Ax/Rad Refl.	1
29	Composition	Nickel	1
30	Composition	Niobium	1
31	Composition	Rhenium	1
32	Composition	Sand	1
33	Composition	Sodium	1
35	Composition	Tungsten	1

36	Composition	Zirconium	1
37	Composition	Hydrogen in Zirconium	1
53	Composition	PSR Blades	1
54	Composition	“Control” Boron Carbide	1
55	Composition	Polyethylene in core	1
56	Composition	Borated Polyethylene in reflector	1
57	Composition	Borated Polyethylene in shield	1
62	Composition	Humidity	1
41	Composition	Steel in Matrix Tubes	2
15	Composition	Aluminum in Core	3
16	Composition	Aluminum in Pu-Al Plates	3
18	Composition	Aluminum Drawers	3
19	Composition	Aluminum in Reflectors	3
21	Composition	Beryllium	3
22	Composition	Beryllium Oxide in Reflectors	3
23	Composition	Beryllium Oxide in SP-100 rods	3
24	Composition	Depleted Lithium Plates in core	3
25	Composition	Lithium Hydride in Shield	3
26	Composition	Graphite	3
34	Composition	Sodium Carbonate	3
38	Composition	Steel Plates in the Core	3
39	Composition	Steel in the Cans	3
40	Composition	Steel in Drawers	3
42	Composition	Steel in Reflectors	3
43	Composition	Steel in Shield	3
44	Composition	Iron Oxide Plates	3
45	Composition	Enriched Uranium	3
47	Composition	Depleted Uranium in Core	3
48	Composition	Depleted Uranium in Reflectors	3
49	Composition	Depleted Uranium in Blanket	3
50	Composition	Depleted Uranium in Shield	3
51	Composition	Depleted Uranium Oxide Plates	3
58	Composition	Kel-F on core fuel	3
59	Composition	Kel-F on core DU fuel	3
60	Composition	Kel-F on core BeO plates	3
61	Composition	Kel-F on reflector BeO plates	3
28	Composition	Molybdenum in Pu-U-Mo Plates	4
46	Composition	Depleted Uranium in Pu-U-Mo Plates	4
52	Composition	Plutonium	4

The diagonal terms are the quadrature-fraction of the uncertainty type to the total uncertainty. These numbers have to be a quadrature-fraction because the individual terms are added in quadrature. For example, the enriched uranium uncertainty for ZPR-3 Assembly 6F is 0.0784 % $\Delta$ k and the total uncertainty is 0.1130 % $\Delta$ k. This makes the enriched uranium quadrature-fraction for ZPR-3 Assembly 6F 0.4817 (i.e.  $0.0784^2/1130^2$ ). Also shown in Tables 85-87 are the covariance matrices for the three broad groups of uncertainties: measurement techniques, geometry and composition. Like the individual uncertainty types, the group diagonal terms are also quadrature-fractions. From Figures 85-87, it is seen that the composition component is almost always the largest of the three broad group covariance matrices.

Finally, shown in Figure 88 is the total covariance matrix. As expected, Figure 88 is similar to Figures 4 and 5. (Recall that Figures 4 and 5 were generated using the 14 major uncertainty types, while Figure 88 was generated using all 62 uncertainty types.) Figure 88 will have relatively - higher values than Figure 5 because it includes all the uncertainty types.

## **Appendix B. Basic Uncertainty Data**

Appendix B contains the benchmark summary uncertainty tables for each of the 33 assemblies considered in this report.



	ZP1C	ZP1D	ZP2C	ZP2D	ZP3C	ZP3D	ZP4C	ZP4D	ZP5C	ZP5D	ZP6C	ZP6D	ZP7C	ZP7D	ZP8C	ZP8D	ZP9C	ZP9D	ZP10C	ZP10D	ZP11C	ZP11D	ZP12C	ZP12D	ZP13C	ZP13D	ZP14C	ZP14D	ZP15C	ZP15D	ZP16C	ZP16D	ZP17C	ZP17D			
ZP1C	1																																				
ZP1D		1																																			
ZP2C			1																																		
ZP2D				1																																	
ZP3C					1																																
ZP3D						1																															
ZP4C							1																														
ZP4D								1																													
ZP5C									1																												
ZP5D										1																											
ZP6C											1																										
ZP6D												1																									
ZP7C													1																								
ZP7D														1																							
ZP8C															1																						
ZP8D																1																					
ZP9C																	1																				
ZP9D																		1																			
ZP10C																			1																		
ZP10D																				1																	
ZP11C																					1																
ZP11D																						1															
ZP12C																							1														
ZP12D																								1													
ZP13C																									1												
ZP13D																										1											
ZP14C																											1										
ZP14D																												1									
ZP15C																													1								
ZP15D																														1							
ZP16C																															1						
ZP16D																																1					
ZP17C																																	1				
ZP17D																																		1			

Figure A2. Common Factor Matrix Number 2.







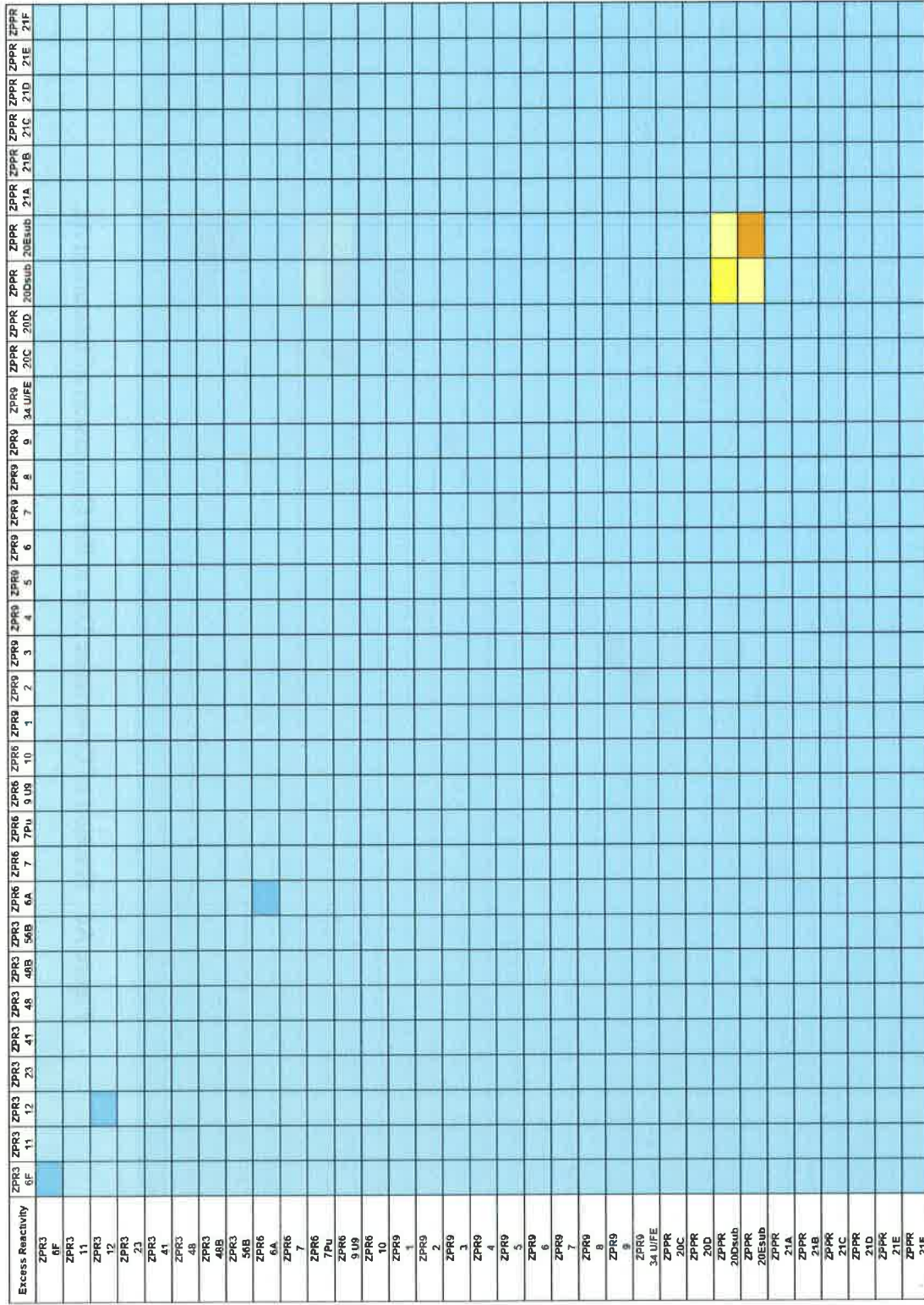


Figure A5. Fraction of Covariance Due to Excess Reactivity.

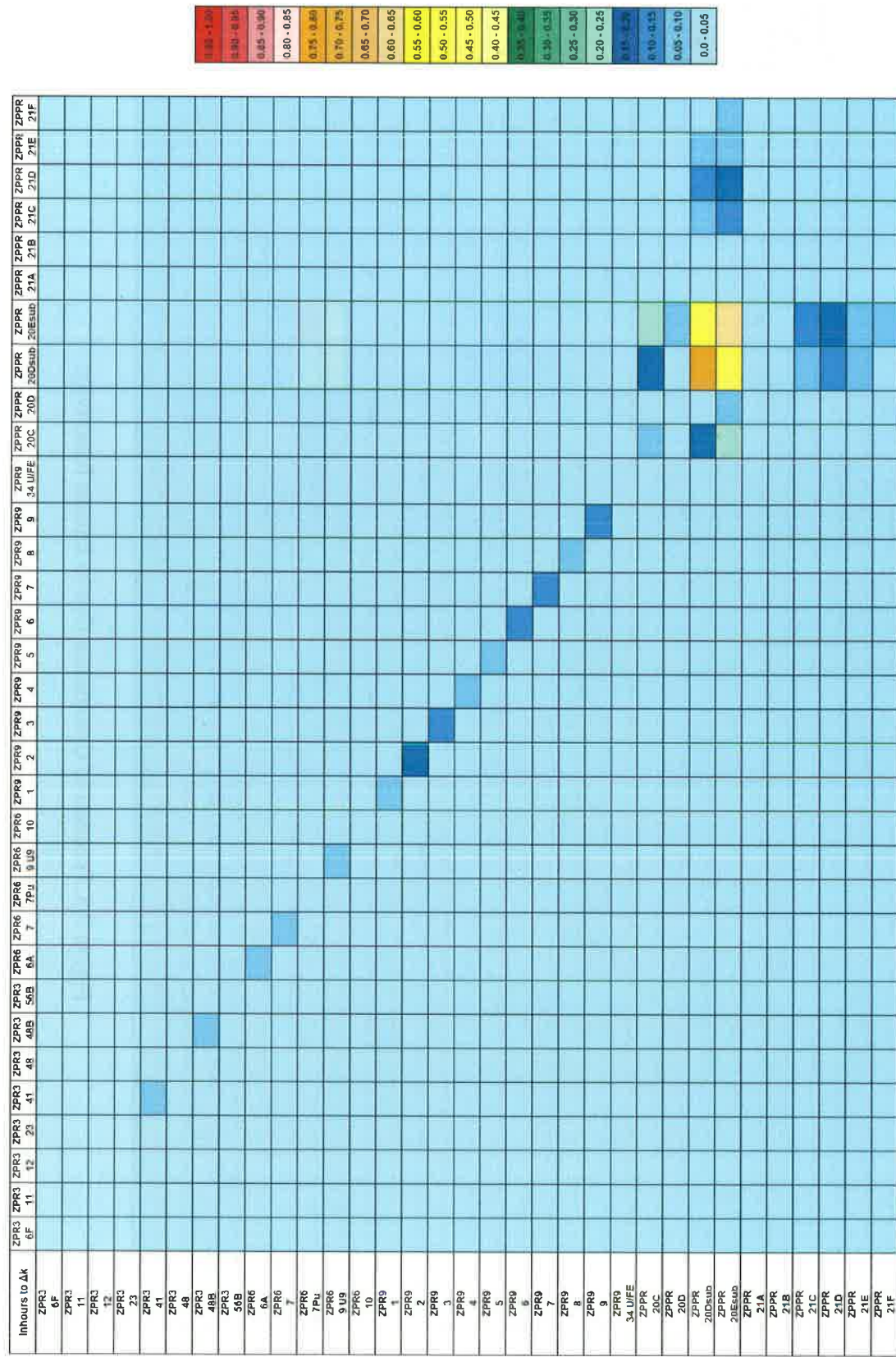


Figure A6. Fraction of Covariance Due to the Conversion of Inhours to  $\Delta k$ .

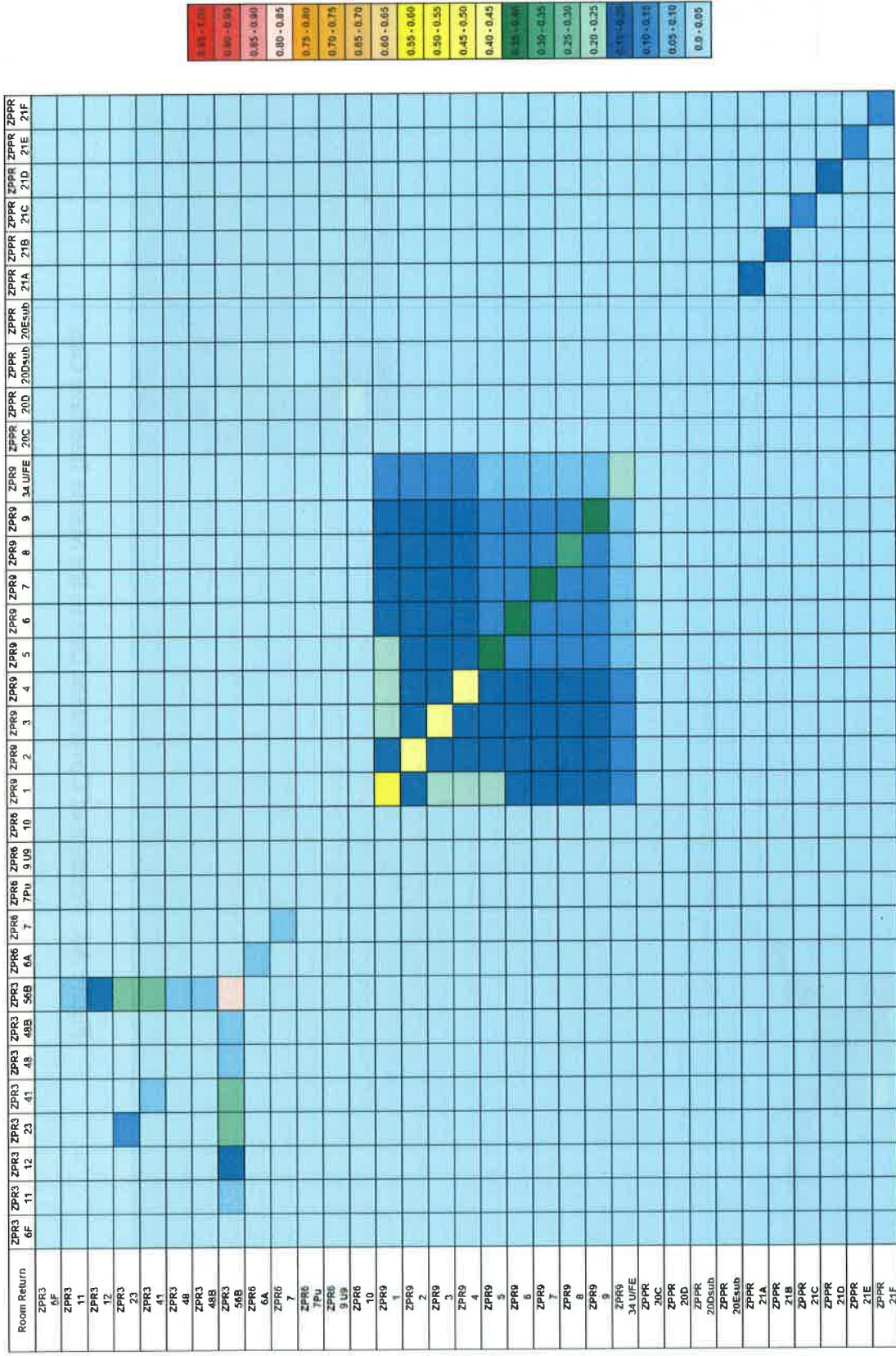


Figure A7. Fraction of Covariance Due to Room Return.



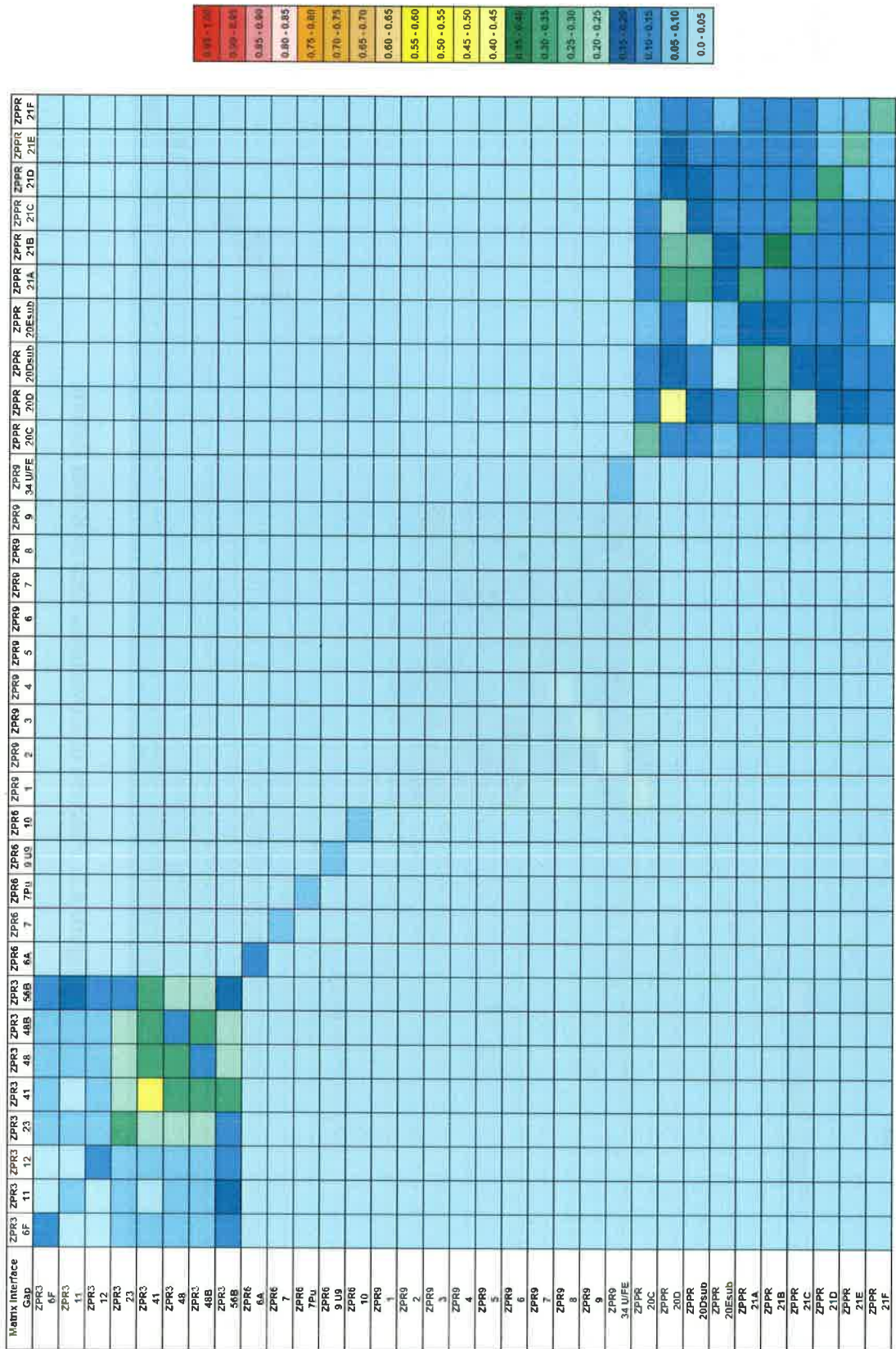


Figure A8. Fraction of Covariance Due to the Matrix Interface Gap.

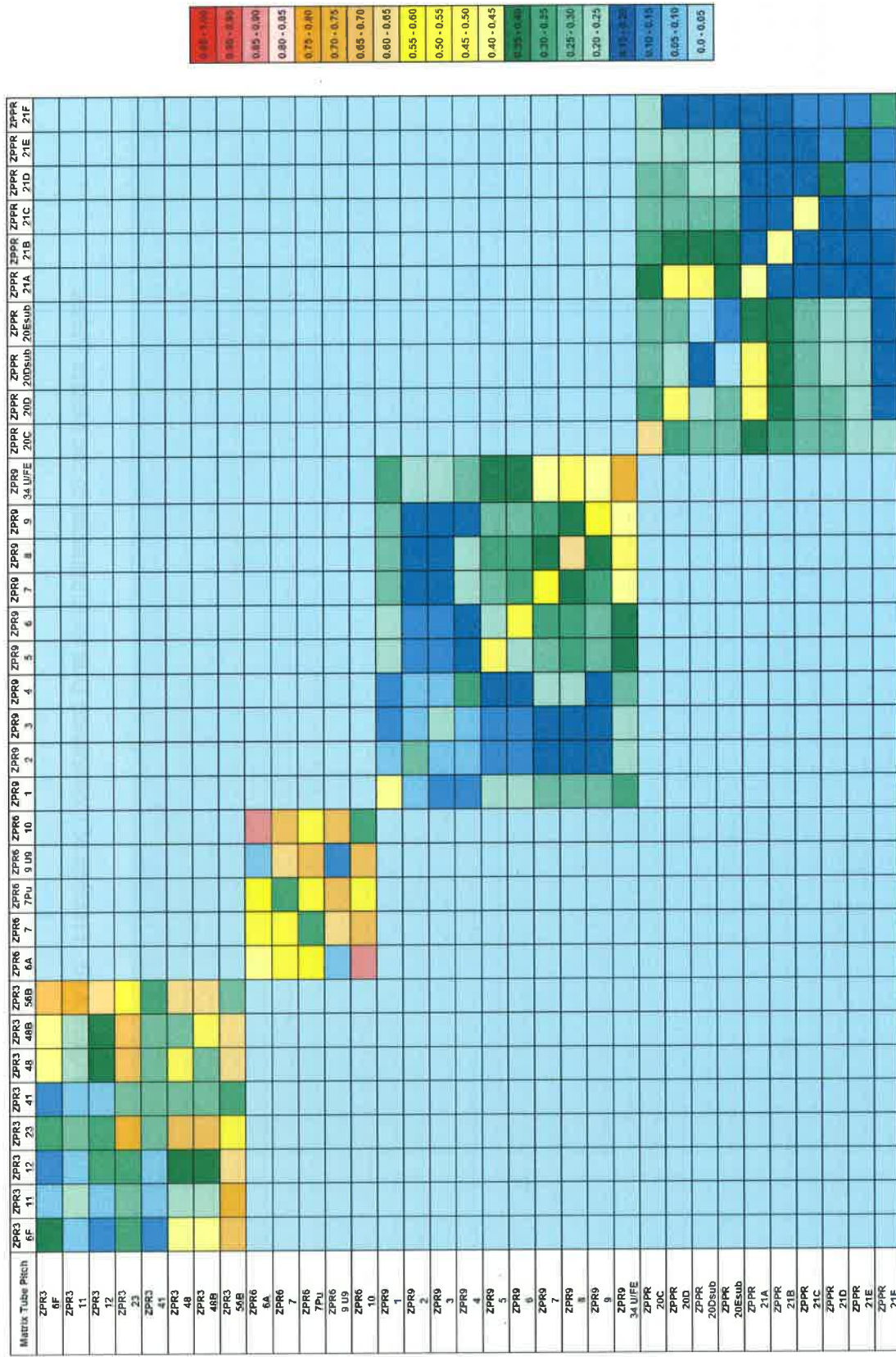


Figure A9. Fraction of Covariance Due to the Matrix Tube Pitch.

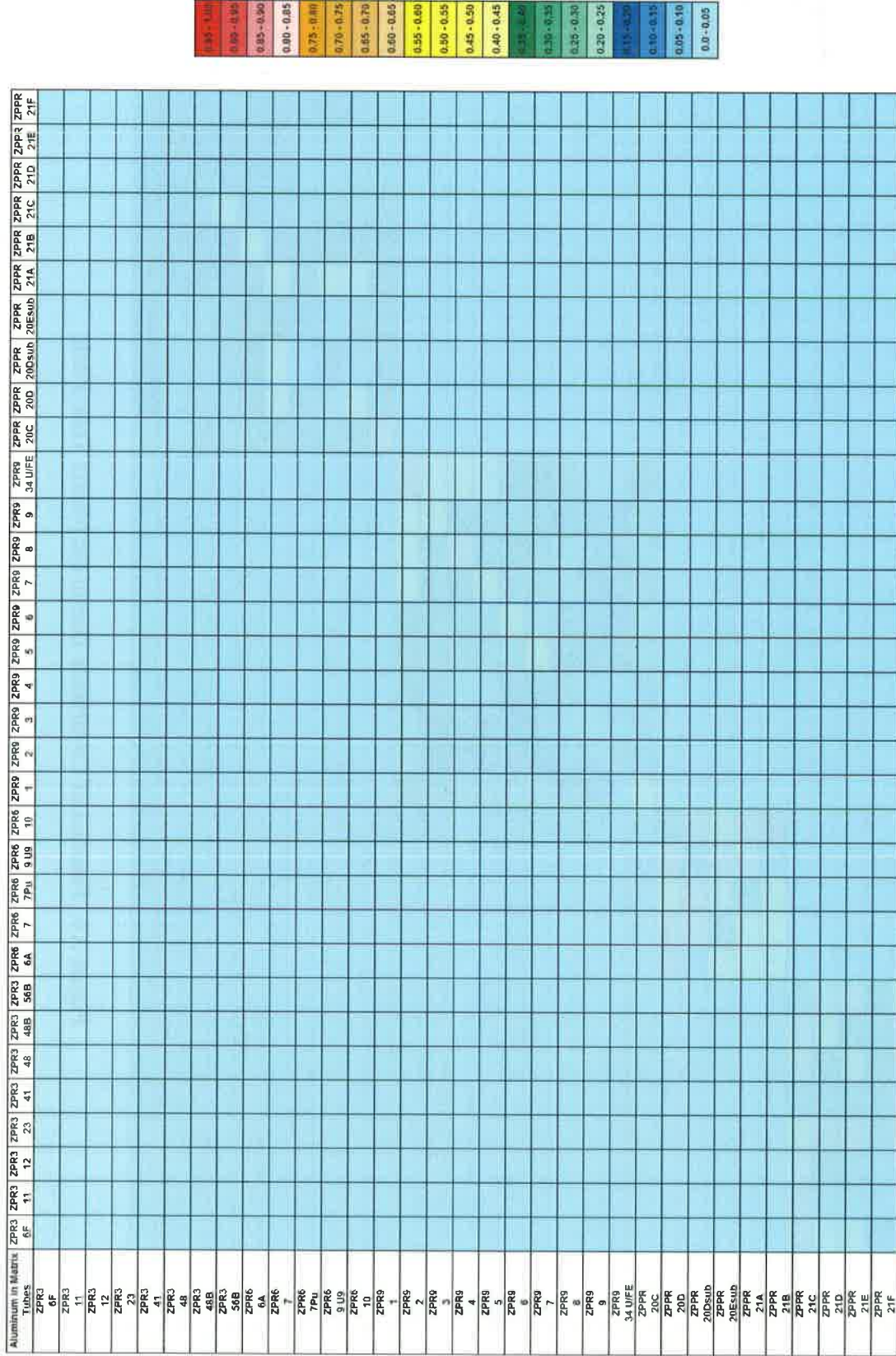


Figure A10. Fraction of Covariance Due to Aluminum in the Matrix Tubes.



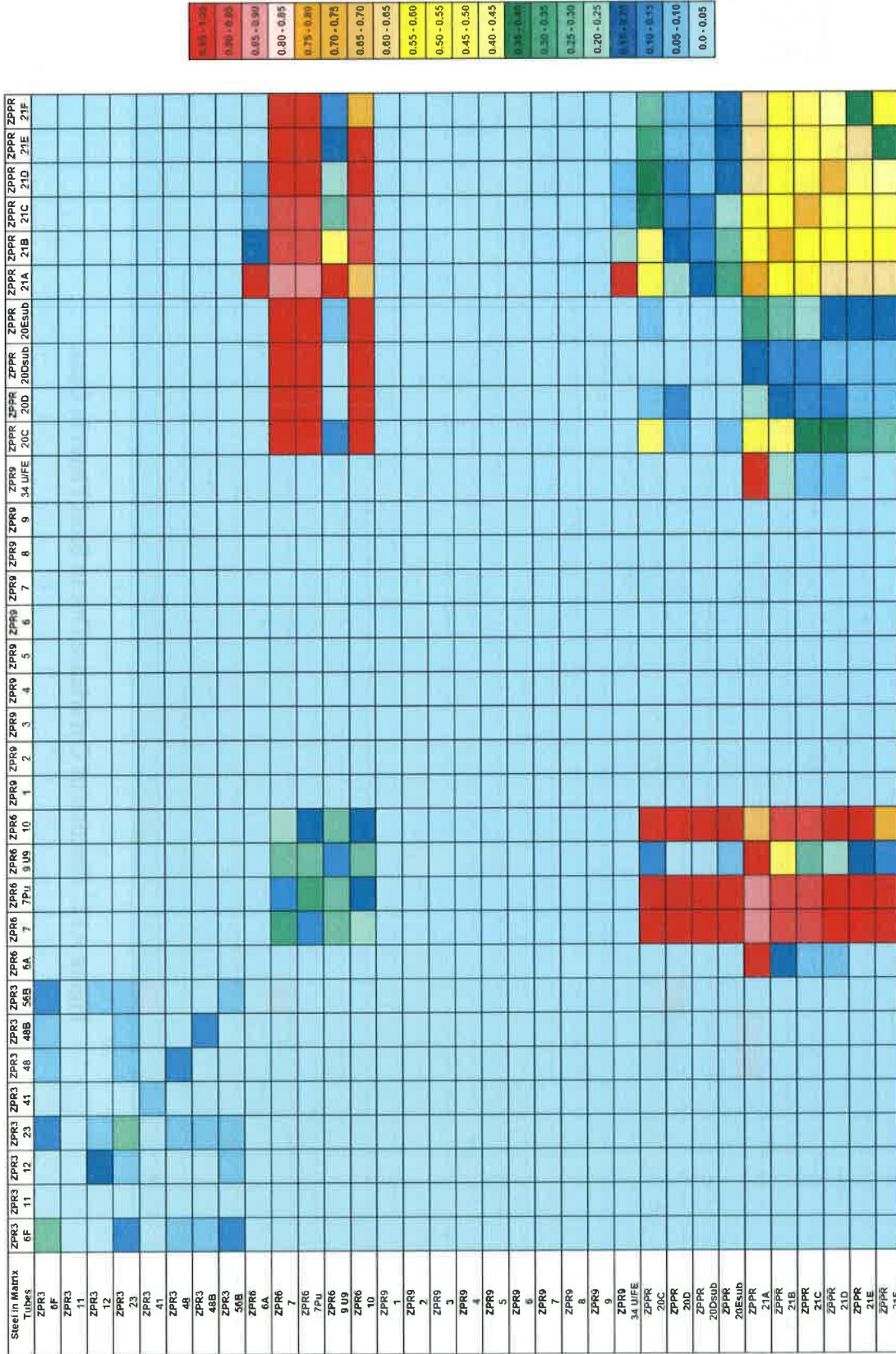


Figure A11. Fraction of Covariance Due to Steel in the Matrix Tubes.

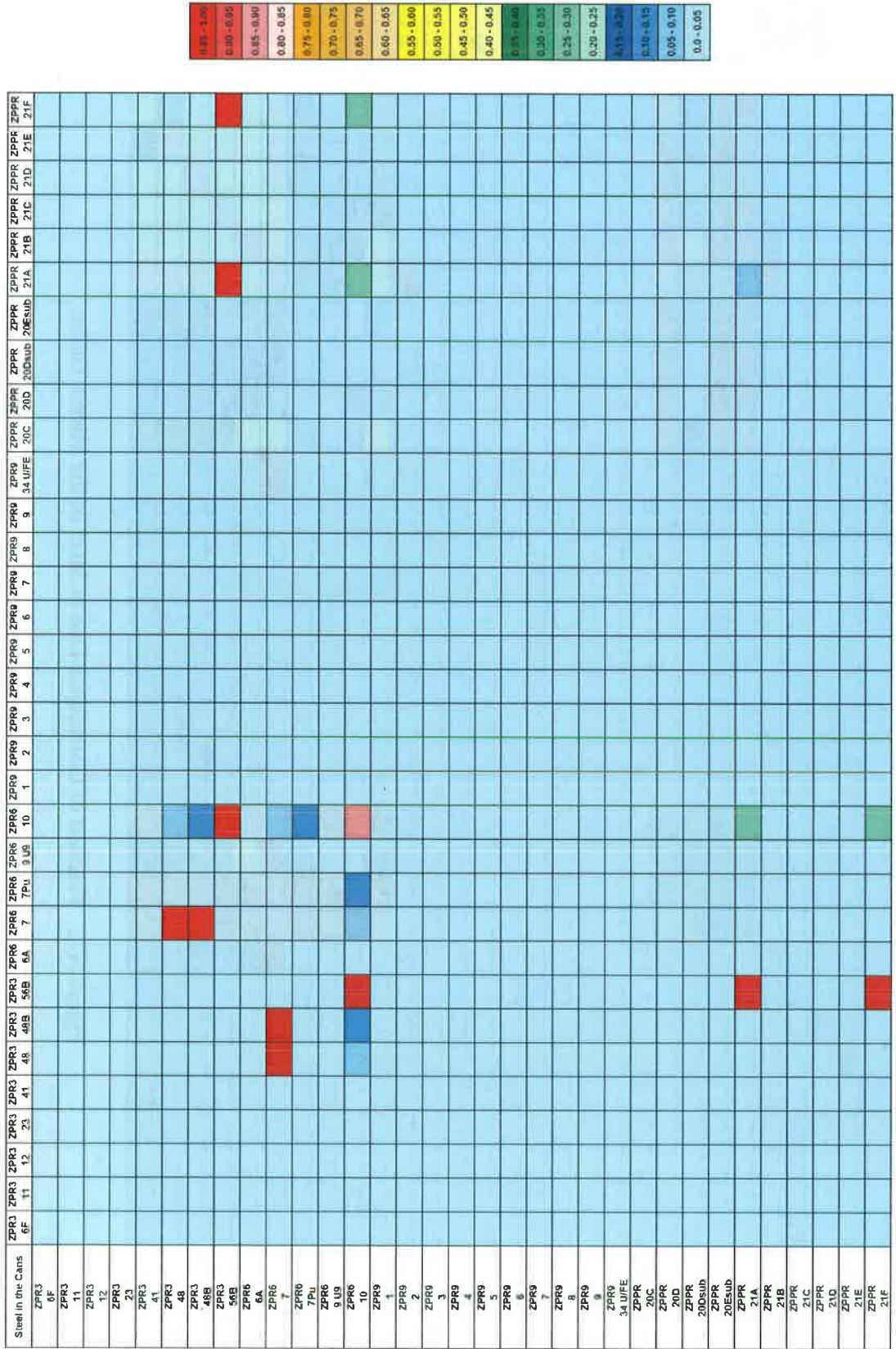


Figure A12. Fraction of Covariance Due to Steel Plates in Cans.



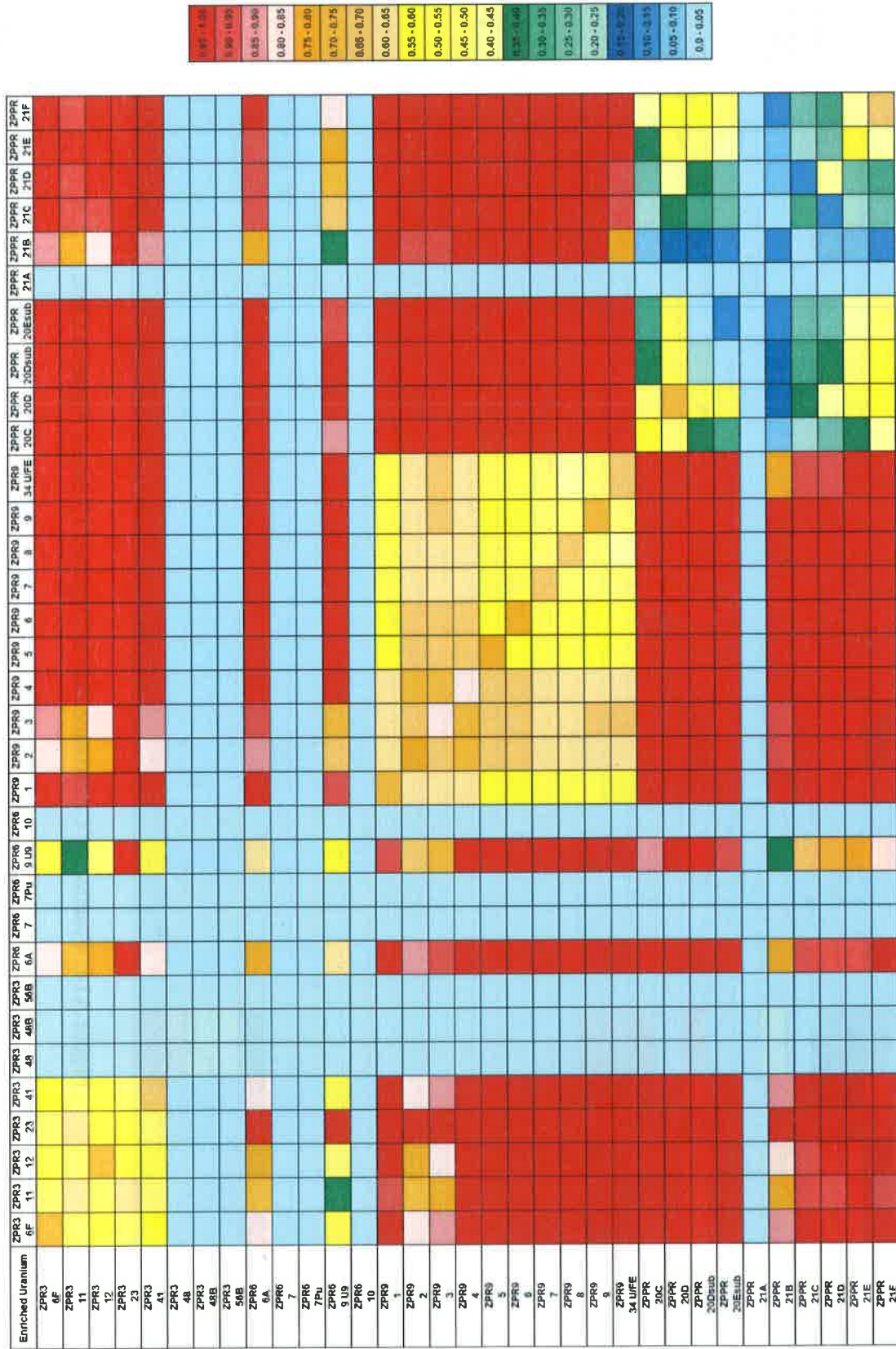


Figure A13. Fraction of Covariance Due to Enriched Uranium Plates.



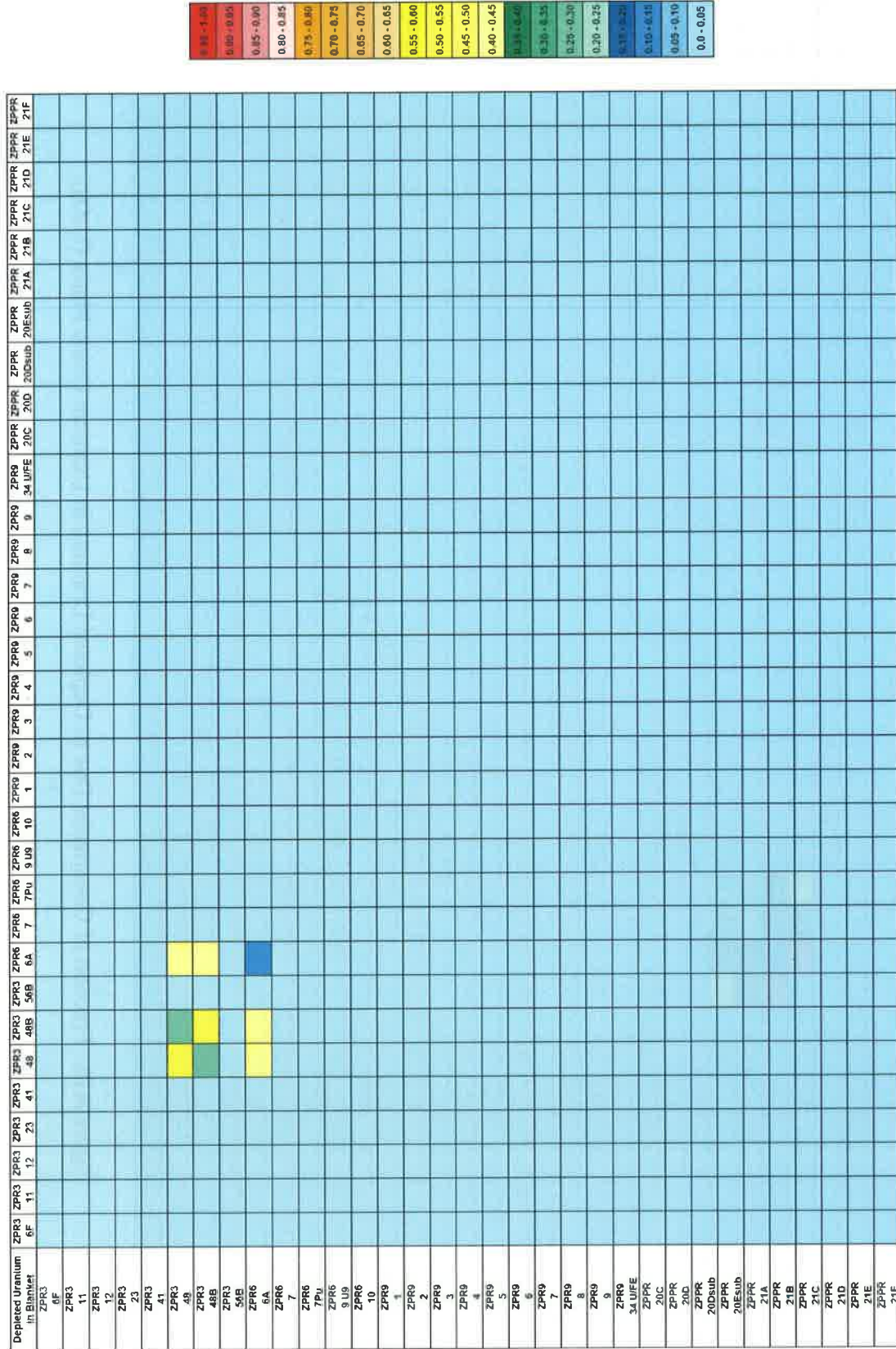


Figure A15. Fraction of Covariance Due to Depleted Uranium Plates in Blanket.



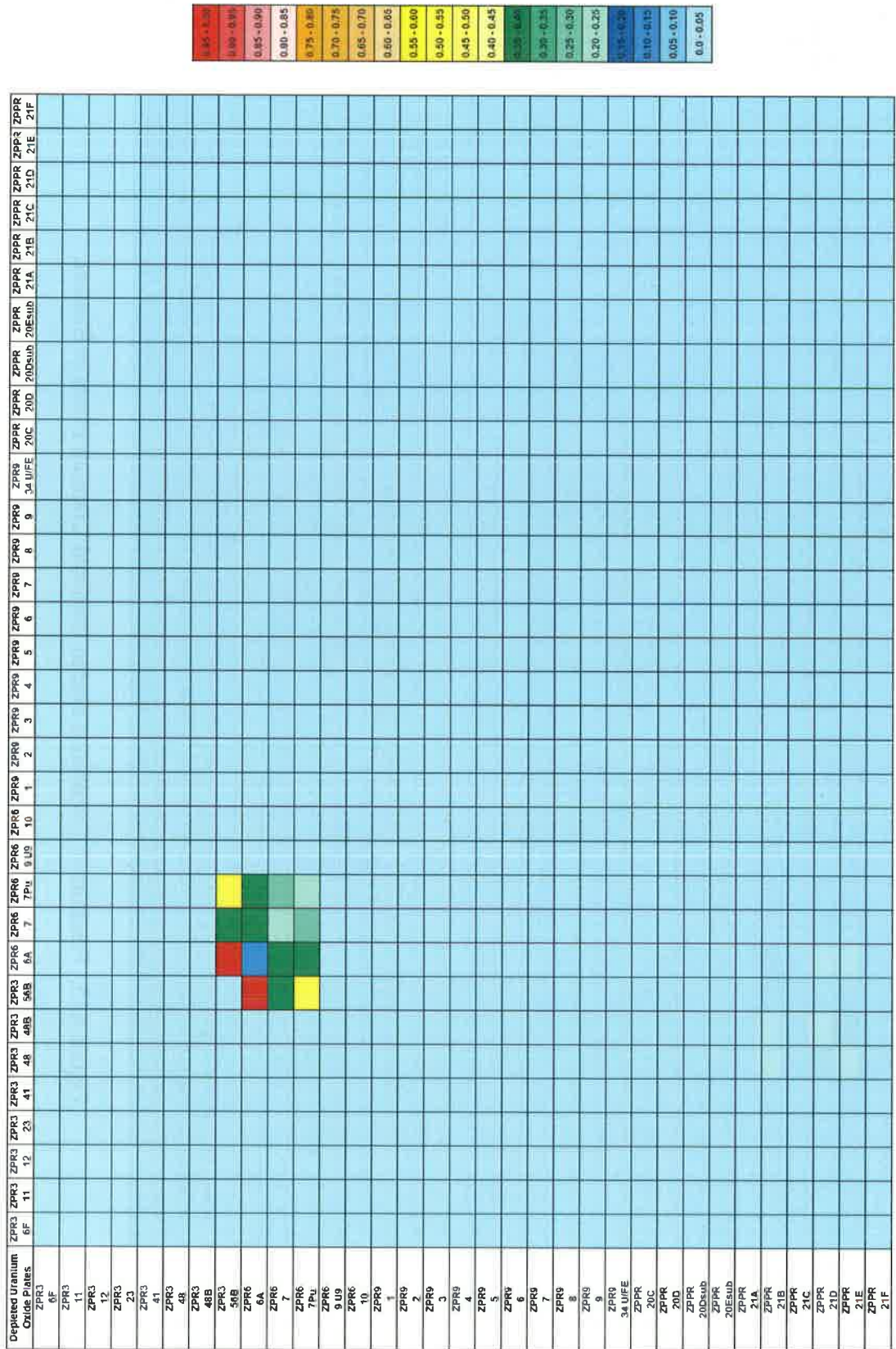


Figure A16. Fraction of Covariance Due to Depleted Uranium in Uranium Oxide Plates (U<sub>3</sub>O<sub>8</sub>).

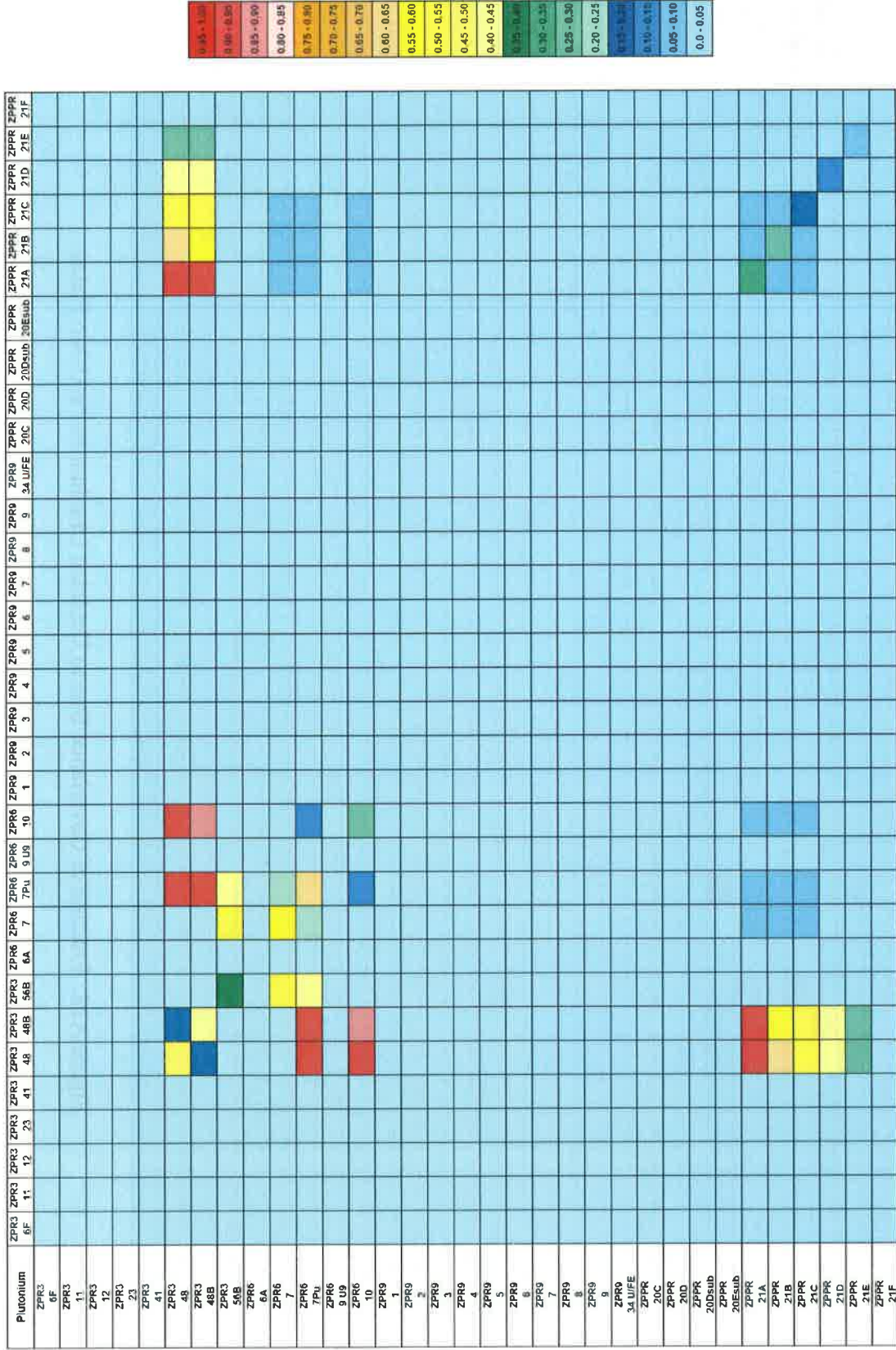


Figure A17. Fraction of Covariance Due to Plutonium Plates.

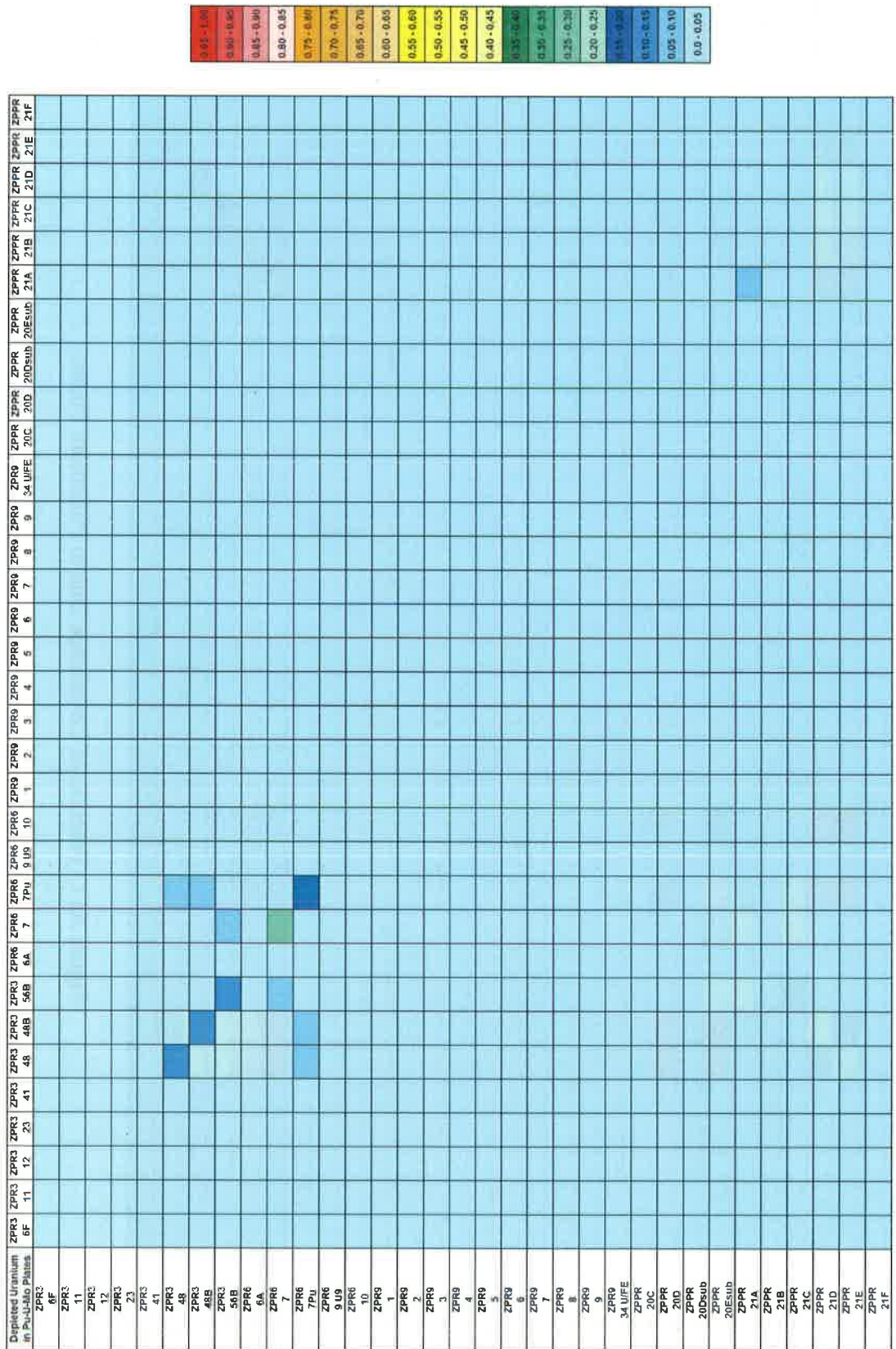


Figure A18. Fraction of Covariance Due to Depleted Uranium in Pu-U-Mo Plates.

Table A.2 Miscellaneous Quantities for ZPR-3 Assemblies.

Item \ Assembly Name	ZPR-3/6F	ZPR-3/11	ZPR-3/12	ZPR-3/23	ZPR-3/41	ZPR-3/48	ZPR-3/48B	ZPR-3/56B
Core Spectral Index, 28f/25f	-	-	-	0.0720	0.0379	-	-	-
Core Spectral Index, 28f/49f	-	-	-	-	-	-	-	-
Total Spectral Index, 28f/25f	-	-	-	0.0028	0.0043	-	-	-
Total Spectral Index, 28f/49f	-	-	-	-	-	-	-	-
Fission Fraction - Fast	0.8290	0.7970	0.6660	0.8110	0.7330	0.6310	0.6300	0.5900
Fission Fraction - Inter	0.1710	0.2030	0.3340	0.1890	0.2670	0.3690	0.3700	0.4100
Fission Fraction - Thermal	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Core Leakage Fraction	-	-	-	0.4264	0.3050	-	-	-
Total Leakage Fraction	-	-	-	0.0733	0.0361	-	-	-
Core Volume, cc	-	-	-	4.22E+05	4.42E+05	-	-	-
<sup>235</sup> U Enrichment	-	-	-	0.9330	0.1697	-	-	-
<sup>239</sup> Pu Enrichment	-	-	-	-	-	-	-	-
C/E(keff) w/ ENDF/B-VII.0	1.0040	0.9992	1.0025	-	-	1.0003	1.0005	1.0029
C/E(keff) w/ ENDF/B-VI	-	-	-	1.0059	-	-	-	-
C/E(keff) w/ ENDF/B-V	-	-	-	-	1.0015	-	-	-

Table A.3 Miscellaneous Quantities for ZPR-6 Assemblies.

Item \ Assembly Name	ZPR-6/6A	ZPR-6/7	ZPR-6/7Pu	ZPR-6/9 U9	ZPR-6/10
Core Spectral Index, 28f/25f	-	0.0218	0.0221	0.0304	-
Core Spectral Index, 28f/49f	-	0.0235	0.0240	-	0.0000
Total Spectral Index, 28f/25f	-	0.0155	0.0156	0.0047	-
Total Spectral Index, 28f/49f	-	0.0026	0.0025	-	0.0000
Fission Fraction - Fast	0.4570	0.5610	0.5650	0.7730	0.3270
Fission Fraction - Inter	0.5420	0.4390	0.4350	0.2270	0.6720
Fission Fraction - Thermal	0.0000	0.0000	0.0000	0.0000	0.0000
Core Leakage Fraction	-	0.2258	0.2323	0.1909	0.3749
Total Leakage Fraction	-	0.0194	0.0184	0.0325	0.0461
Core Volume, cc	-	3.12E+06	2.92E+06	4.03E+05	4.22E+05
235U Enrichment	-	0.0022	0.0022	0.0896	-
239Pu Enrichment	-	0.8680	0.8537	-	0.9533
C/E(keff) w/ ENDF/B-VII.0	0.9992	1.0012	-	-	-
C/E(keff) w/ ENDF/B-VI	0.9992	1.0061	1.0034	1.0147	1.0381
C/E(keff) w/ ENDF/B-V	0.9781	-	-	-	-



Table A.4 Miscellaneous Quantities for ZPR-9 Assemblies.

Item \ Assembly Name	ZPR-9/1	ZPR-9/2	ZPR-9/3	ZPR-9/4	ZPR-9/5	ZPR-9/6	ZPR-9/7	ZPR-9/8	ZPR-9/9	ZPR-9/34 U/FE
Core Spectral Index, 28f/25f	0.0389	0.0356	0.0339	0.0417	0.0403	0.0432	0.0392	0.0392	0.0373	0.0133
Core Spectral Index, 28f/49f	-	-	-	-	-	-	-	-	-	-
Total Spectral Index, 28f/25f	0.0389	0.0356	0.0339	0.0417	0.0403	0.0432	0.0392	0.0392	0.0373	0.0001
Total Spectral Index, 28f/49f	-	-	-	-	-	-	-	-	-	-
Fission Fraction - Fast	0.7780	0.7430	0.7170	0.7090	0.5410	0.6740	0.5540	0.5580	0.5210	0.6000
Fission Fraction - Inter	0.2220	0.2570	0.2830	0.2910	0.4600	0.3260	0.4350	0.4330	0.4660	0.4000
Fission Fraction - Thermal	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0100	0.0090	0.0130	0.0000
Core Leakage Fraction	0.3033	0.2535	0.2326	0.3182	0.3162	0.3428	0.3241	0.3284	0.3154	0.3646
Total Leakage Fraction	0.2964	0.2467	0.2267	0.3086	0.3072	0.3328	0.2610	0.3047	0.1875	0.0828
Core Volume, cc	1.60E+05	2.24E+05	2.87E+05	1.09E+05	2.05E+05	2.61E+05	1.24E+05	1.63E+05	1.11E+05	2.25E+06
235U Enrichment	0.1182	0.1567	0.2074	0.9324	0.9324	0.9324	0.9324	0.9324	0.9324	0.9324
239Pu Enrichment	-	-	-	-	-	-	-	-	-	-
C/E(keff) w/ ENDF/B-VII.0	-	-	-	-	-	-	-	1.0121	-	-
C/E(keff) w/ ENDF/B-VI	1.0110	1.0099	1.0094	1.0167	1.0056	1.0133	1.0017	1.0034	0.9968	1.0163
C/E(keff) w/ ENDF/B-V	-	-	-	-	-	-	-	-	-	-

Table A.5 Miscellaneous Quantities for ZPPR-20 Assemblies.

Item \ Assembly Name	ZPPR-20/C	ZPPR-20/D	ZPPR-20/D sub	ZPPR-20/E sub
Core Spectral Index, 28f/25f	-	-	-	-
Core Spectral Index, 28f/49f	-	-	-	-
Total Spectral Index, 28f/25f	-	-	-	-
Total Spectral Index, 28f/49f	-	-	-	-
Fission Fraction - Fast	0.7230	0.4280	0.4420	0.7700
Fission Fraction - Inter	0.2740	0.4830	0.4680	0.2160
Fission Fraction - Thermal	0.0040	0.0890	0.0900	0.0140
Core Leakage Fraction	-	-	-	-
Total Leakage Fraction	-	-	-	-
Core Volume, cc	-	-	-	-
<sup>235</sup> U Enrichment	-	-	-	-
<sup>239</sup> Pu Enrichment	-	-	-	-
C/E(keff) w/ ENDF/B-VII.0	-	-	-	-
C/E(keff) w/ ENDF/B-VI	1.0095	1.0029	1.0122	1.0090
C/E(keff) w/ ENDF/B-V	-	-	-	-

Table A.6 Miscellaneous Quantities for ZPPR-21 Assemblies.

Item \ Assembly Name	ZPPR-21A	ZPPR-21/B	ZPPR-21/C	ZPPR-21/D	ZPPR-21/E	ZPPR-21/F
Core Spectral Index, 28f/25f	0.0826	0.0747	0.0810	0.0736	0.1720	0.0839
Core Spectral Index, 28f/49f	0.0702	0.0000	0.0000	0.0000	0.0001	-
Total Spectral Index, 28f/25f	0.0826	0.0747	0.1745	0.0736	0.0782	0.0839
Total Spectral Index, 28f/49f	0.0702	0.0649	0.1450	0.0620	0.0639	-
Fission Fraction - Fast	0.7810	0.7810	0.7910	0.7350	0.7550	0.7830
Fission Fraction - Inter	0.2150	0.2150	0.2070	0.2600	0.2420	0.2140
Fission Fraction - Thermal	0.0040	0.0040	0.0020	0.0050	0.0030	0.0020
Core Leakage Fraction	0.5924	0.5665	0.5518	0.5210	0.5105	0.5068
Total Leakage Fraction	0.1653	0.1340	0.1429	0.1069	0.1198	0.1368
Core Volume, cc	4.61E+04	4.67E+04	4.67E+04	4.67E+04	4.67E+04	4.67E+04
235U Enrichment	0.0022	0.1843	0.3948	0.4611	0.9827	0.6207
239Pu Enrichment	0.9393	0.9358	0.9296	0.9169	0.8760	-
C/E(keff) w/ ENDF/B-VII.0	-	-	-	-	-	-
C/E(keff) w/ ENDF/B-VI	1.0003	1.0038	0.9974	1.0003	1.0015	1.0027
C/E(keff) w/ ENDF/B-V	-	-	-	-	-	-

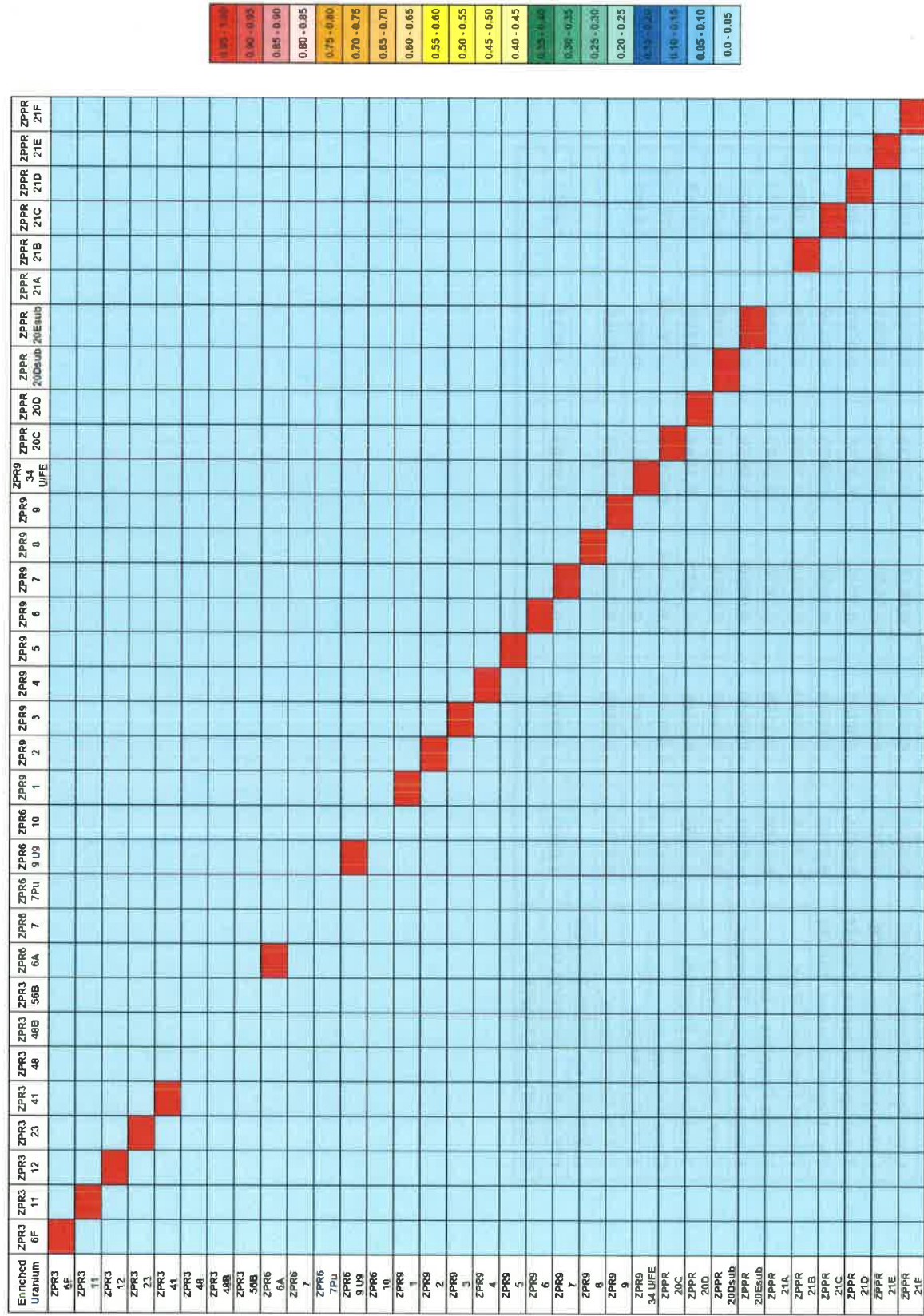


Figure A19. Enriched Uranium Covariance Matrix with 0% Common.

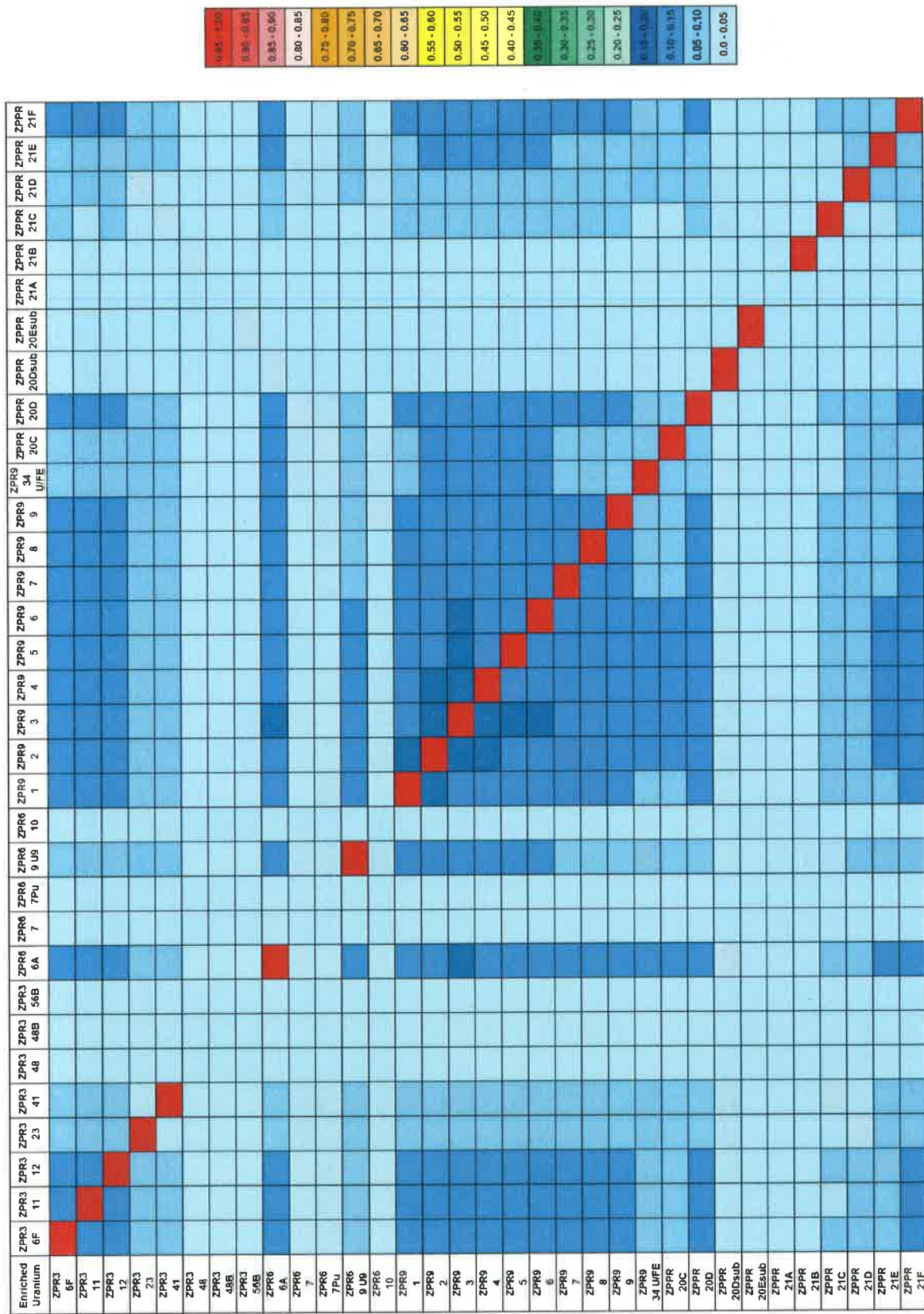


Figure A20. Enriched Uranium Covariance Matrix with 25% Common.



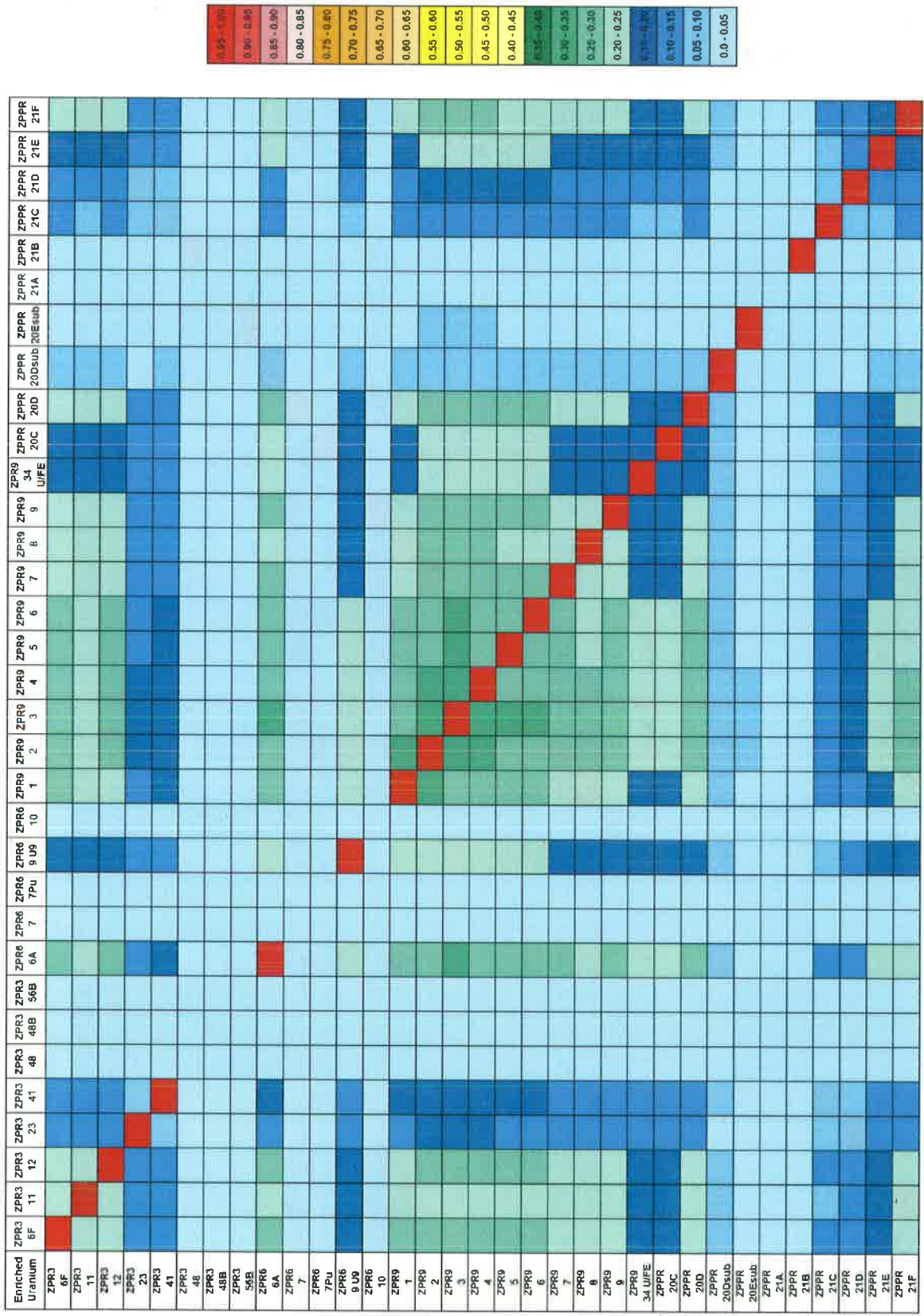


Figure A21. Enriched Uranium Covariance Matrix with 50% Common.

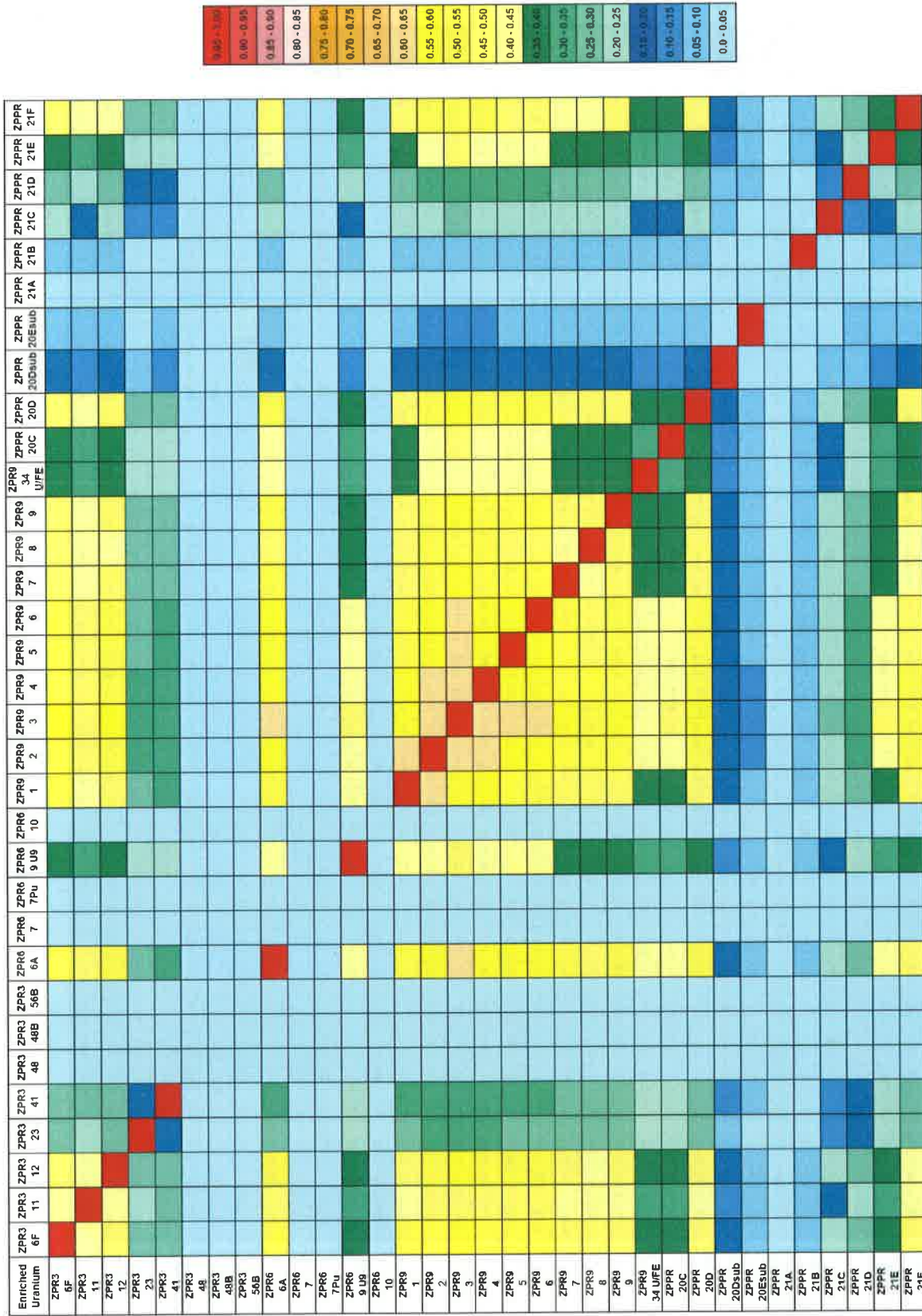


Figure A22. Enriched Uranium Covariance Matrix with 100% Common.















Room Return	ZPR3 6F	ZPR3 11	ZPR3 12	ZPR3 23	ZPR3 41	ZPR3 48	ZPR3 48B	ZPR3 56B	ZPR6 6A	ZPR6 7	ZPR6 7PU	ZPR6 9U9	ZPR6 10	ZPR9 1	ZPR9 2	ZPR9 3	ZPR9 4	ZPR9 5	ZPR9 6	ZPR9 7	ZPR9 8	ZPR9 9	ZPR9 3A LIFE	ZPR9 20C	ZPR9 20D	ZPR9 20E	ZPR9 21A	ZPR9 21B	ZPR9 21C	ZPR9 21D	ZPR9 21E	ZPR9 21F
ZPR3 6F	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 23	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.08	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 48B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 50B	0.01	0.01	0.02	0.08	0.04	0.02	0.02	0.66	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 6A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 7PU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 9U9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.26	0.13	0.22	0.19	0.20	0.19	0.19	0.19	0.18	0.09	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.13	0.13	0.18	0.16	0.16	0.15	0.15	0.14	0.15	0.08	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.22	0.18	0.18	0.16	0.16	0.15	0.15	0.14	0.15	0.08	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.19	0.16	0.16	0.14	0.14	0.14	0.13	0.13	0.13	0.07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.20	0.16	0.16	0.14	0.14	0.14	0.13	0.13	0.14	0.07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.19	0.13	0.13	0.14	0.13	0.13	0.13	0.12	0.13	0.07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.19	0.16	0.16	0.13	0.13	0.13	0.12	0.12	0.13	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.13	0.14	0.14	0.13	0.13	0.13	0.12	0.12	0.12	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.13	0.14	0.14	0.13	0.13	0.13	0.12	0.12	0.12	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.13	0.14	0.14	0.13	0.13	0.13	0.12	0.12	0.12	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 3A LIFE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.09	0.08	0.08	0.07	0.07	0.07	0.06	0.06	0.07	0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 20C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 20D	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 20E	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 21A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 21B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 21C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 21D	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 21E	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 21F	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	



Figure A27. ANL Benchmark Room Return Covariance Matrix.









Matrix Tube Pitch	ZPR3 6F	ZPR3 11	ZPR3 12	ZPR3 23	ZPR3 41	ZPR3 48	ZPR3 48B	ZPR3 56B	ZPR6 6A	ZPR6 7	ZPR6 7Pu	ZPR6 9U9	ZPR6 10	ZPR9 1	ZPR9 2	ZPR9 3	ZPR9 4	ZPR9 5	ZPR9 6	ZPR9 7	ZPR9 8	ZPR9 9	ZPR9 34 UJFE	ZPR9 20C	ZPR9 20D	ZPR9 20D <sub>max</sub>	ZPR9 20E <sub>max</sub>	ZPR9 21A	ZPR9 21B	ZPR9 21C	ZPR9 21D	ZPR9 21E	ZPR9 21F
ZPR3 6F	0.13	0.08	0.11	0.16	0.08	0.17	0.17	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 11	0.06	0.05	0.07	0.11	0.04	0.10	0.10	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 12	0.11	0.07	0.09	0.15	0.05	0.14	0.14	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 23	0.16	0.11	0.15	0.25	0.09	0.23	0.24	0.14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 41	0.06	0.04	0.05	0.09	0.03	0.06	0.06	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 48	0.17	0.10	0.14	0.23	0.08	0.21	0.22	0.13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 48B	0.17	0.10	0.14	0.24	0.08	0.22	0.22	0.13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 56B	0.10	0.06	0.09	0.14	0.05	0.13	0.13	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 6A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.11	0.20	0.30	0.06	0.13	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.30	0.22	0.22	0.06	0.14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 7Pu	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.33	0.22	0.22	0.07	0.15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 9U9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	0.06	0.07	0.02	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.13	0.14	0.15	0.04	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.26	0.07	0.10	0.13	0.21	0.22	0.25	0.26	0.25	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26
ZPR9 2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.07	0.07	0.06	0.08	0.12	0.13	0.15	0.17	0.15	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
ZPR9 3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.10	0.06	0.06	0.07	0.11	0.12	0.14	0.15	0.13	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14	0.14
ZPR9 4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.13	0.08	0.07	0.09	0.14	0.15	0.17	0.19	0.17	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18	0.18
ZPR9 5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.21	0.12	0.11	0.14	0.23	0.24	0.27	0.30	0.27	0.28	0.28	0.28	0.28	0.28	0.28	0.28	0.28	0.28	0.28	0.28
ZPR9 6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.22	0.13	0.12	0.15	0.24	0.25	0.28	0.31	0.28	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30
ZPR9 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.25	0.15	0.14	0.17	0.27	0.28	0.33	0.35	0.32	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34
ZPR9 8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.28	0.17	0.16	0.18	0.30	0.31	0.36	0.40	0.30	0.38	0.38	0.38	0.38	0.38	0.38	0.38	0.38	0.38	0.38	
ZPR9 9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.25	0.15	0.13	0.17	0.27	0.28	0.32	0.35	0.32	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34
ZPR9 34 UJFE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.26	0.16	0.14	0.18	0.28	0.30	0.34	0.38	0.34	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35
ZPR9 20C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20D	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20E <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21D	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21E	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21F	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



Figure A30. ANL Benchmark Matrix Tube Pitch Covariance Matrix.













































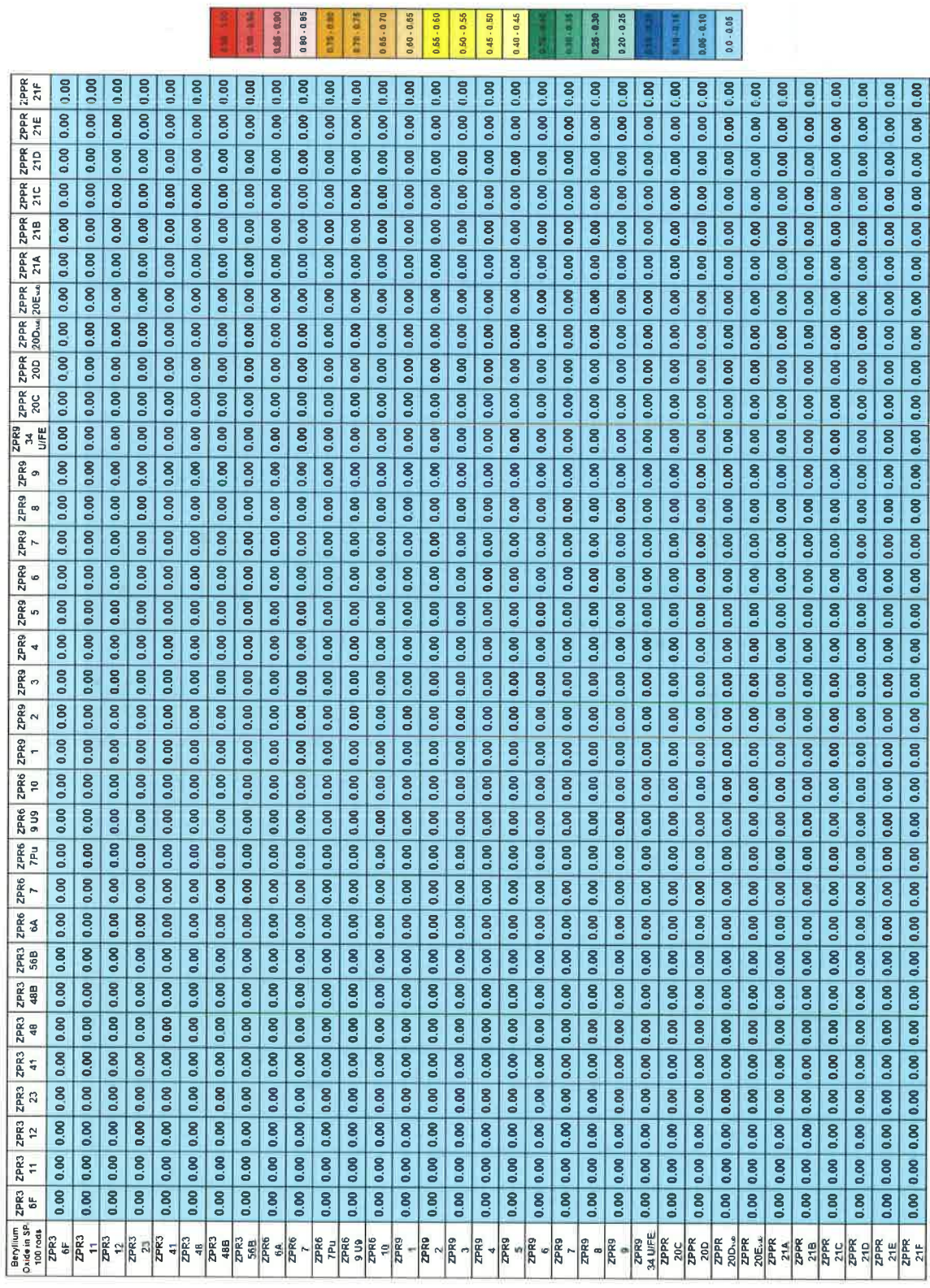


Figure A45. ANL Benchmark Beryllium Oxide in SP-100 Rods Covariance Matrix.







































































Enriched Uranium	ZPR3 0F	ZPR3 11	ZPR3 12	ZPR3 23	ZPR3 41	ZPR3 48	ZPR3 48B	ZPR3 50B	ZPR6 6A	ZPR6 7	ZPR6 7Pu	ZPR6 9	ZPR6 9U	ZPR6 10	ZPR6 1	ZPR6 2	ZPR6 3	ZPR6 4	ZPR6 5	ZPR6 6	ZPR6 7	ZPR6 8	ZPR6 9	ZPR6 34	ZPR6 34 UFE	ZPR6 20C	ZPR6 20D	ZPR6 20E	ZPR6 20F	ZPR6 21A	ZPR6 21B	ZPR6 21C	ZPR6 21D	ZPR6 21E	ZPR6 21F
ZPR3 0F	0.48	0.42	0.47	0.27	0.29	0.00	0.00	0.00	0.52	0.00	0.00	0.00	0.00	0.00	0.50	0.55	0.57	0.54	0.53	0.52	0.47	0.46	0.48	0.38	0.39	0.48	0.17	0.09	0.00	0.07	0.22	0.28	0.35	0.46	
ZPR3 11	0.42	0.37	0.41	0.23	0.25	0.00	0.00	0.00	0.46	0.00	0.00	0.00	0.00	0.00	0.44	0.48	0.50	0.48	0.46	0.48	0.41	0.40	0.42	0.33	0.34	0.42	0.15	0.08	0.00	0.06	0.18	0.24	0.34	0.40	
ZPR3 12	0.47	0.41	0.46	0.26	0.28	0.00	0.00	0.00	0.50	0.00	0.00	0.00	0.00	0.00	0.49	0.53	0.56	0.53	0.51	0.51	0.46	0.45	0.47	0.37	0.37	0.47	0.16	0.09	0.00	0.07	0.21	0.27	0.37	0.45	
ZPR3 23	0.27	0.23	0.26	0.15	0.16	0.00	0.00	0.00	0.29	0.00	0.00	0.00	0.00	0.00	0.28	0.30	0.31	0.30	0.29	0.29	0.26	0.25	0.27	0.21	0.21	0.27	0.09	0.05	0.00	0.04	0.12	0.15	0.21	0.25	
ZPR3 41	0.29	0.25	0.28	0.16	0.17	0.00	0.00	0.00	0.31	0.00	0.00	0.00	0.00	0.00	0.30	0.33	0.34	0.33	0.32	0.31	0.28	0.28	0.29	0.23	0.23	0.29	0.10	0.05	0.00	0.04	0.13	0.17	0.23	0.27	
ZPR3 48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 48B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 50B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 6A	0.52	0.45	0.50	0.29	0.31	0.00	0.00	0.00	0.55	0.00	0.00	0.00	0.00	0.00	0.54	0.58	0.61	0.58	0.56	0.56	0.50	0.49	0.51	0.41	0.41	0.51	0.16	0.10	0.00	0.08	0.23	0.30	0.41	0.49	
ZPR6 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 7Pu	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 9U	0.39	0.34	0.38	0.22	0.24	0.00	0.00	0.00	0.42	0.00	0.00	0.00	0.00	0.00	0.41	0.44	0.46	0.44	0.43	0.43	0.37	0.37	0.39	0.31	0.31	0.39	0.14	0.07	0.00	0.06	0.18	0.23	0.31	0.37	
ZPR6 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 1	0.50	0.44	0.49	0.28	0.30	0.00	0.00	0.00	0.54	0.00	0.00	0.00	0.00	0.00	0.52	0.52	0.59	0.56	0.55	0.54	0.49	0.48	0.50	0.40	0.40	0.50	0.17	0.09	0.00	0.08	0.22	0.29	0.40	0.47	
ZPR9 2	0.55	0.48	0.53	0.30	0.33	0.00	0.00	0.00	0.58	0.00	0.00	0.00	0.00	0.00	0.62	0.62	0.64	0.61	0.60	0.59	0.53	0.52	0.54	0.43	0.43	0.55	0.15	0.10	0.00	0.08	0.24	0.32	0.43	0.52	
ZPR9 3	0.67	0.50	0.65	0.31	0.34	0.00	0.00	0.00	0.81	0.00	0.00	0.00	0.00	0.00	0.69	0.64	0.67	0.64	0.62	0.62	0.65	0.64	0.66	0.46	0.46	0.67	0.20	0.10	0.00	0.09	0.26	0.33	0.45	0.64	
ZPR9 4	0.54	0.48	0.53	0.30	0.33	0.00	0.00	0.00	0.58	0.00	0.00	0.00	0.00	0.00	0.56	0.61	0.64	0.61	0.59	0.59	0.53	0.51	0.54	0.43	0.43	0.54	0.15	0.10	0.00	0.08	0.24	0.31	0.43	0.51	
ZPR9 5	0.53	0.46	0.51	0.29	0.32	0.00	0.00	0.00	0.56	0.00	0.00	0.00	0.00	0.00	0.55	0.60	0.62	0.60	0.57	0.57	0.51	0.50	0.52	0.41	0.42	0.52	0.14	0.10	0.00	0.08	0.23	0.30	0.42	0.50	
ZPR9 6	0.62	0.46	0.51	0.29	0.31	0.00	0.00	0.00	0.68	0.00	0.00	0.00	0.00	0.00	0.64	0.69	0.62	0.60	0.67	0.67	0.61	0.60	0.62	0.41	0.42	0.62	0.18	0.10	0.00	0.08	0.23	0.30	0.42	0.50	
ZPR9 7	0.47	0.41	0.46	0.25	0.28	0.00	0.00	0.00	0.50	0.00	0.00	0.00	0.00	0.00	0.49	0.53	0.55	0.53	0.51	0.51	0.46	0.45	0.47	0.37	0.37	0.47	0.16	0.09	0.00	0.07	0.21	0.27	0.37	0.44	
ZPR9 8	0.46	0.40	0.45	0.25	0.28	0.00	0.00	0.00	0.49	0.00	0.00	0.00	0.00	0.00	0.48	0.52	0.54	0.51	0.50	0.50	0.45	0.44	0.45	0.35	0.35	0.46	0.16	0.08	0.00	0.07	0.20	0.26	0.36	0.43	
ZPR9 9	0.48	0.42	0.47	0.27	0.29	0.00	0.00	0.00	0.51	0.00	0.00	0.00	0.00	0.00	0.50	0.54	0.56	0.54	0.52	0.52	0.47	0.45	0.47	0.35	0.35	0.48	0.17	0.09	0.00	0.07	0.21	0.28	0.38	0.45	
ZPR9 34 UFE	0.34	0.33	0.37	0.21	0.23	0.00	0.00	0.00	0.41	0.00	0.00	0.00	0.00	0.00	0.40	0.43	0.45	0.43	0.41	0.41	0.37	0.36	0.36	0.30	0.30	0.39	0.13	0.07	0.00	0.06	0.17	0.22	0.30	0.38	
ZPRR 20C	0.51	0.34	0.37	0.21	0.23	0.00	0.00	0.00	0.41	0.00	0.00	0.00	0.00	0.00	0.40	0.43	0.45	0.43	0.42	0.42	0.37	0.36	0.36	0.30	0.30	0.39	0.13	0.07	0.00	0.06	0.17	0.22	0.30	0.38	
ZPRR 20D	0.48	0.42	0.47	0.27	0.29	0.00	0.00	0.00	0.51	0.00	0.00	0.00	0.00	0.00	0.50	0.55	0.57	0.54	0.52	0.52	0.47	0.46	0.48	0.38	0.38	0.48	0.17	0.09	0.00	0.07	0.21	0.28	0.38	0.46	
ZPRR 20E	0.17	0.15	0.16	0.09	0.10	0.00	0.00	0.00	0.13	0.00	0.00	0.00	0.00	0.00	0.17	0.19	0.20	0.19	0.18	0.19	0.18	0.16	0.17	0.13	0.13	0.17	0.06	0.03	0.00	0.03	0.07	0.10	0.13	0.18	
ZPRR 20E	0.09	0.08	0.09	0.05	0.05	0.00	0.00	0.00	0.10	0.00	0.00	0.00	0.00	0.00	0.09	0.10	0.10	0.10	0.10	0.10	0.09	0.08	0.08	0.07	0.07	0.08	0.03	0.02	0.00	0.01	0.04	0.05	0.07	0.08	
ZPRR 21A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPRR 21B	0.07	0.06	0.07	0.04	0.04	0.00	0.00	0.00	0.08	0.00	0.00	0.00	0.00	0.00	0.08	0.08	0.09	0.08	0.08	0.08	0.07	0.07	0.07	0.06	0.06	0.07	0.03	0.01	0.00	0.01	0.03	0.04	0.06	0.07	
ZPRR 21C	0.22	0.15	0.21	0.12	0.13	0.00	0.00	0.00	0.23	0.00	0.00	0.00	0.00	0.00	0.22	0.24	0.25	0.24	0.23	0.23	0.21	0.20	0.21	0.17	0.17	0.21	0.07	0.04	0.00	0.03	0.10	0.12	0.17	0.20	
ZPRR 21D	0.28	0.24	0.27	0.15	0.17	0.00	0.00	0.00	0.30	0.00	0.00	0.00	0.00	0.00	0.29	0.32	0.33	0.31	0.30	0.30	0.27	0.26	0.26	0.22	0.22	0.28	0.10	0.05	0.00	0.04	0.12	0.16	0.22	0.26	
ZPRR 21E	0.55	0.34	0.37	0.21	0.23	0.00	0.00	0.00	0.41	0.00	0.00	0.00	0.00	0.00	0.40	0.43	0.45	0.43	0.42	0.42	0.37	0.36	0.36	0.30	0.30	0.39	0.13	0.07	0.00	0.06	0.17	0.22	0.30	0.38	
ZPRR 21F	0.48	0.40	0.45	0.25	0.27	0.00	0.00	0.00	0.49	0.00	0.00	0.00	0.00	0.00	0.47	0.52	0.54	0.51	0.50	0.50	0.44	0.43	0.45	0.35	0.35	0.46	0.16	0.08	0.00	0.07	0.20	0.26	0.36	0.43	

0.91 - 0.95  
0.86 - 0.90  
0.81 - 0.85  
0.76 - 0.80  
0.71 - 0.75  
0.66 - 0.70  
0.61 - 0.65  
0.56 - 0.60  
0.51 - 0.55  
0.46 - 0.50  
0.41 - 0.45  
0.36 - 0.40  
0.31 - 0.35  
0.26 - 0.30  
0.21 - 0.25  
0.16 - 0.20  
0.11 - 0.15  
0.06 - 0.10

Figure A67. ANL Benchmark Enriched Uranium Covariance Matrix.





Depleted Uranium in Core	ZPR3 6F	ZPR3 11	ZPR3 12	ZPR3 23	ZPR3 41	ZPR3 48	ZPR3 48B	ZPR3 56B	ZPR6 6A	ZPR6 7	ZPR6 7Pu	ZPR6 9	ZPR6 9U9	ZPR6 10	ZPR9 1	ZPR9 2	ZPR9 3	ZPR9 4	ZPR9 5	ZPR9 6	ZPR9 7	ZPR9 8	ZPR9 9	ZPR9 34 UIFE	ZPR9 20C	ZPR9 20D	ZPR9 20E...	ZPR9 21A	ZPR9 21B	ZPR9 21C	ZPR9 21D	ZPR9 21E	ZPR9 21F	
ZPR3 6F	0.22	0.35	0.27	0.00	0.12	0.17	0.17	0.00	0.12	0.00	0.00	0.00	0.00	0.00	0.02	0.13	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 11	0.35	0.54	0.42	0.00	0.18	0.27	0.27	0.00	0.18	0.00	0.00	0.57	0.00	0.00	0.03	0.20	0.15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 12	0.27	0.42	0.33	0.00	0.14	0.21	0.21	0.00	0.14	0.00	0.00	0.44	0.00	0.02	0.15	0.12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 23	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 41	0.12	0.19	0.15	0.00	0.07	0.10	0.10	0.00	0.07	0.00	0.00	0.20	0.00	0.01	0.07	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 48	0.17	0.27	0.21	0.00	0.10	0.13	0.13	0.00	0.09	0.00	0.00	0.28	0.00	0.01	0.10	0.07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 48B	0.17	0.27	0.21	0.00	0.10	0.13	0.14	0.00	0.09	0.00	0.00	0.28	0.00	0.01	0.10	0.07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 56B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 7	0.12	0.19	0.14	0.00	0.07	0.09	0.09	0.00	0.06	0.00	0.00	0.19	0.00	0.01	0.07	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 7Pu	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 9 U9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 1	0.02	0.03	0.02	0.00	0.01	0.01	0.01	0.00	0.01	0.00	0.00	0.03	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 2	0.13	0.20	0.16	0.00	0.07	0.10	0.10	0.00	0.07	0.00	0.00	0.21	0.00	0.00	0.07	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 3	0.10	0.15	0.12	0.00	0.05	0.07	0.07	0.00	0.05	0.00	0.00	0.15	0.00	0.01	0.05	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 34 UIFE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20D	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20E...	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20E...	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21A	0.01	0.02	0.01	0.00	0.01	0.01	0.01	0.00	0.01	0.00	0.00	0.02	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21B	0.01	0.02	0.01	0.00	0.01	0.01	0.01	0.00	0.01	0.00	0.00	0.02	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21C	0.01	0.02	0.01	0.00	0.01	0.01	0.01	0.00	0.01	0.00	0.00	0.02	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21D	0.01	0.02	0.01	0.00	0.01	0.01	0.01	0.00	0.01	0.00	0.00	0.02	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21E	0.01	0.02	0.01	0.00	0.01	0.01	0.01	0.00	0.01	0.00	0.00	0.02	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21F	0.02	0.03	0.02	0.00	0.01	0.01	0.01	0.00	0.01	0.00	0.00	0.03	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



Figure A69. ANL Benchmark Depleted Uranium in the Core Covariance Matrix.



Depleted Uranium in Reflectors	ZPR3 6F	ZPR3 11	ZPR3 12	ZPR3 23	ZPR3 41	ZPR3 48	ZPR3 56B	ZPR3 6A	ZPR3 7	ZPR3 7PU	ZPR3 9 U9	ZPR6 10	ZPR9 1	ZPR9 2	ZPR9 3	ZPR9 4	ZPR9 5	ZPR9 6	ZPR9 7	ZPR9 8	ZPR9 9	ZPR9 9 UFE	ZPR9 20C	ZPR9 20C	ZPR9 20D	ZPR9 20D	ZPR9 20E	ZPR9 21A	ZPR9 21B	ZPR9 21C	ZPR9 21D	ZPR9 21E	ZPR9 21F	
ZPR3 6F	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 12	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 23	0.00	0.00	0.00	0.06	0.04	0.00	0.00	0.04	0.05	0.06	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 41	0.00	0.00	0.00	0.04	0.02	0.00	0.00	0.03	0.03	0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 48	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 48B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR3 56B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 6A	0.00	0.00	0.00	0.04	0.03	0.00	0.00	0.03	0.03	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 7	0.00	0.00	0.00	0.04	0.03	0.00	0.00	0.03	0.03	0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 7PU	0.00	0.00	0.00	0.05	0.03	0.00	0.00	0.04	0.04	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 9 U9	0.00	0.00	0.00	0.05	0.03	0.00	0.00	0.04	0.04	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR6 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 34 UFE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20D	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20E	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21D	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21E	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21F	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

























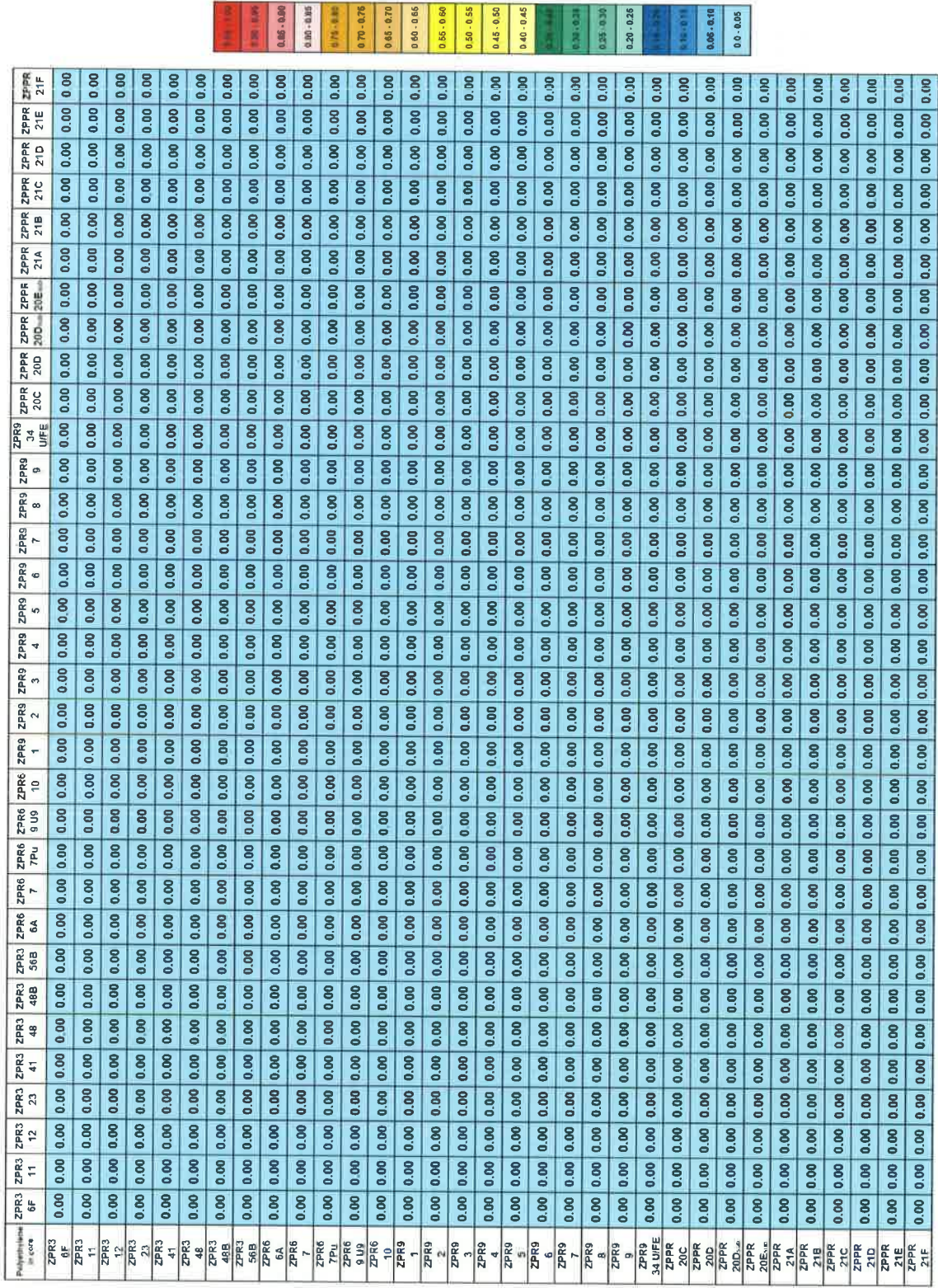


Figure A77. ANL Benchmark Polyethylene in Core Covariance Matrix.



























Geometry	ZPR3 6F	ZPR3 11	ZPR3 12	ZPR3 23	ZPR3 41	ZPR3 48	ZPR3 48B	ZPR3 56B	ZPR6 6A	ZPR6 7PU	ZPR6 9U9	ZPR6 10	ZPR6 9U9	ZPR6 10	ZPR9 1	ZPR9 2	ZPR9 3	ZPR9 4	ZPR9 5	ZPR9 6	ZPR9 7	ZPR9 8	ZPR9 9	ZPR9 34 UFE	ZPR9 20C	ZPR9 20D	ZPR9 20D <sub>max</sub>	ZPR9 20E <sub>max</sub>	ZPR9 21A	ZPR9 21B	ZPR9 21C	ZPR9 21D	ZPR9 21E	ZPR9 21F	
ZPR3 6F	0.21	0.13	0.13	0.28	0.17	0.28	0.17	0.11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 11	0.13	0.08	0.11	0.17	0.11	0.17	0.11	0.11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 12	0.13	0.11	0.15	0.24	0.14	0.24	0.14	0.16	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 23	0.28	0.17	0.24	0.74	0.65	0.35	0.35	0.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 41	0.17	0.11	0.14	0.65	0.73	0.25	0.25	0.14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 48	0.28	0.17	0.24	0.38	0.25	0.38	0.38	0.24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 48B	0.28	0.17	0.24	0.38	0.25	0.38	0.38	0.25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR3 56B	0.17	0.11	0.14	0.30	0.18	0.24	0.25	0.79	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 6A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.21	0.21	0.22	0.07	0.14	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.21	0.23	0.23	0.07	0.15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 7PU	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.22	0.23	0.23	0.07	0.15	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 9U9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.07	0.07	0.07	0.02	0.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.14	0.15	0.15	0.05	0.10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.48	0.25	0.32	0.32	0.41	0.41	0.41	0.43	0.46	0.44	0.35	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.25	0.26	0.24	0.24	0.28	0.29	0.30	0.31	0.30	0.24	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.12	0.24	0.24	0.23	0.28	0.27	0.29	0.30	0.28	0.22	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.32	0.24	0.23	0.34	0.29	0.31	0.32	0.31	0.32	0.31	0.28	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR9 5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.41	0.29	0.28	0.25	0.37	0.35	0.41	0.43	0.41	0.35	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 6	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.41	0.29	0.27	0.25	0.38	0.38	0.41	0.44	0.41	0.37	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.43	0.30	0.29	0.31	0.41	0.41	0.46	0.48	0.45	0.41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 8	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.46	0.31	0.30	0.32	0.43	0.44	0.48	0.52	0.48	0.44	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.44	0.30	0.29	0.31	0.41	0.41	0.45	0.48	0.45	0.41	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 34 UFE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.39	0.24	0.22	0.25	0.36	0.37	0.41	0.44	0.41	0.40	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 20C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.47	0.44	0.11	0.09	0.37	0.36	0.37	0.36	0.33	0.29	0.29	
ZPR9 20D	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.44	0.45	0.16	0.08	0.37	0.36	0.37	0.36	0.33	0.30	0.30	
ZPR9 20D <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.15	0.16	0.06	0.03	0.13	0.13	0.13	0.13	0.12	0.11	0.11	0.11
ZPR9 20E <sub>max</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21A	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21B	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21C	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21D	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21E	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
ZPR9 21F	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00



Figure A86. ANL Benchmark Geometry Covariance Matrix.



Component	ZPR3 6F	ZPR3 11	ZPR3 12	ZPR3 23	ZPR3 41	ZPR3 48	ZPR3 50B	ZPR3 6A	ZPR6 7Fu	ZPR6 9UB	ZPR6 10	ZPR9 1	ZPR9 2	ZPR9 3	ZPR9 4	ZPR9 5	ZPR9 6	ZPR9 7	ZPR9 8	ZPR9 9	ZPR9 34 UFE	ZPR9 34 UFE	ZPR20 20C	ZPR20 20D	ZPR20 20E	ZPR21 21A	ZPR21 21B	ZPR21 21C	ZPR21 21D	ZPR21 21E	ZPR21 21F		
ZPR3 6F	0.79	0.78	0.80	0.35	0.43	0.21	0.02	0.63	0.00	0.00	0.75	0.00	0.52	0.67	0.88	0.54	0.53	0.53	0.47	0.46	0.48	0.39	0.35	0.48	0.17	0.09	0.00	0.09	0.23	0.29	0.39	0.48	
ZPR3 11	0.78	0.82	0.85	0.24	0.45	0.27	0.00	0.64	0.00	0.00	0.91	0.00	0.47	0.65	0.85	0.48	0.46	0.41	0.40	0.42	0.33	0.34	0.42	0.15	0.08	0.00	0.08	0.21	0.26	0.35	0.43		
ZPR3 12	0.80	0.85	0.84	0.29	0.44	0.23	0.01	0.65	0.00	0.00	0.82	0.01	0.81	0.69	0.87	0.53	0.52	0.51	0.48	0.45	0.47	0.37	0.47	0.16	0.09	0.01	0.09	0.22	0.28	0.38	0.47		
ZPR3 23	0.33	0.24	0.29	0.28	0.21	0.03	0.03	0.02	0.29	0.06	0.06	0.27	0.00	0.28	0.30	0.32	0.30	0.29	0.26	0.28	0.27	0.22	0.21	0.27	0.09	0.05	0.00	0.04	0.12	0.16	0.21	0.25	
ZPR3 41	0.43	0.45	0.44	0.21	0.10	0.10	0.00	0.39	0.03	0.03	0.47	0.00	0.31	0.40	0.39	0.33	0.32	0.31	0.28	0.28	0.29	0.23	0.23	0.29	0.10	0.05	0.00	0.05	0.14	0.17	0.24	0.28	
ZPR3 48	0.21	0.27	0.23	0.03	0.10	0.80	0.55	0.01	0.07	0.26	0.07	0.01	0.10	0.07	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.02	0.01	0.02		
ZPR3 48B	0.21	0.27	0.23	0.03	0.10	0.56	0.60	0.01	0.10	0.06	0.28	0.07	0.01	0.08	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.02	0.01	0.02		
ZPR3 56B	0.02	0.00	0.01	0.02	0.00	0.01	0.01	0.21	0.05	0.18	0.13	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
ZPR6 6A	0.63	0.64	0.66	0.29	0.28	0.16	0.05	0.75	0.21	0.18	0.62	0.00	0.55	0.65	0.66	0.68	0.66	0.50	0.49	0.51	0.42	0.42	0.42	0.42	0.42	0.18	0.10	0.02	0.11	0.26	0.32	0.43	0.52
ZPR6 7	0.00	0.00	0.00	0.06	0.03	0.01	0.01	0.39	0.21	0.77	0.49	0.06	0.00	0.01	0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.13	0.03	0.01	0.01	0.23	0.22	0.21	0.20	0.18	0.16	
ZPR6 7Fu	0.00	0.00	0.00	0.05	0.03	0.07	0.06	0.13	0.12	0.48	0.76	0.07	0.11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.12	0.03	0.01	0.01	0.22	0.21	0.20	0.19	0.17	0.15	
ZPR6 9UB	0.75	0.81	0.82	0.27	0.47	0.28	0.00	0.82	0.08	0.07	0.97	0.02	0.44	0.66	0.82	0.44	0.43	0.43	0.38	0.37	0.39	0.31	0.35	0.40	0.14	0.08	0.07	0.15	0.25	0.31	0.38	0.46	
ZPR9 10	0.00	0.00	0.01	0.00	0.00	0.07	0.07	0.02	0.00	0.06	0.11	0.02	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.00	0.00	0.03	0.08	0.02	0.01	0.01	0.21	0.13	0.12	0.12	0.11	0.13	
ZPR9 1	0.52	0.47	0.51	0.28	0.31	0.01	0.01	0.55	0.00	0.00	0.44	0.00	0.53	0.71	0.81	0.68	0.56	0.51	0.48	0.51	0.40	0.40	0.50	0.37	0.09	0.00	0.08	0.22	0.29	0.40	0.48		
ZPR9 2	0.67	0.68	0.69	0.30	0.40	0.10	0.10	0.65	0.01	0.00	0.65	0.00	0.71	0.71	0.73	0.64	0.62	0.62	0.67	0.54	0.58	0.44	0.43	0.55	0.18	0.10	0.00	0.09	0.25	0.32	0.44	0.53	
ZPR9 3	0.66	0.65	0.67	0.32	0.39	0.07	0.08	0.66	0.01	0.00	0.82	0.00	0.61	0.73	0.75	0.63	0.66	0.65	0.60	0.57	0.61	0.45	0.45	0.67	0.20	0.10	0.00	0.09	0.26	0.33	0.46	0.55	
ZPR9 4	0.54	0.48	0.53	0.30	0.33	0.00	0.00	0.58	0.00	0.00	0.44	0.00	0.58	0.64	0.66	0.65	0.63	0.63	0.58	0.56	0.60	0.44	0.43	0.54	0.19	0.10	0.00	0.08	0.24	0.31	0.43	0.51	
ZPR9 5	0.53	0.46	0.52	0.29	0.32	0.00	0.00	0.56	0.00	0.00	0.43	0.01	0.66	0.82	0.65	0.63	0.62	0.61	0.56	0.53	0.67	0.42	0.42	0.52	0.18	0.10	0.02	0.08	0.23	0.30	0.42	0.50	
ZPR9 6	0.53	0.46	0.51	0.29	0.31	0.00	0.00	0.56	0.00	0.00	0.43	0.00	0.68	0.82	0.65	0.63	0.61	0.61	0.56	0.53	0.67	0.42	0.42	0.52	0.18	0.10	0.00	0.08	0.23	0.30	0.42	0.50	
ZPR9 7	0.47	0.41	0.48	0.26	0.28	0.00	0.00	0.50	0.00	0.00	0.30	0.00	0.61	0.67	0.60	0.68	0.66	0.62	0.49	0.53	0.39	0.39	0.37	0.47	0.18	0.09	0.00	0.07	0.21	0.27	0.37	0.44	
ZPR9 8	0.46	0.40	0.45	0.26	0.28	0.00	0.00	0.49	0.00	0.00	0.37	0.00	0.48	0.54	0.67	0.55	0.53	0.53	0.49	0.48	0.50	0.37	0.38	0.47	0.18	0.09	0.00	0.07	0.20	0.26	0.36	0.43	
ZPR9 9	0.48	0.42	0.47	0.27	0.29	0.00	0.00	0.51	0.00	0.00	0.39	0.00	0.51	0.68	0.61	0.69	0.67	0.53	0.50	0.54	0.39	0.38	0.48	0.17	0.09	0.00	0.07	0.21	0.28	0.38	0.45		
ZPR9 34 UFE	0.39	0.33	0.37	0.23	0.23	0.00	0.00	0.42	0.01	0.01	0.31	0.03	0.40	0.44	0.45	0.44	0.42	0.42	0.36	0.37	0.39	0.30	0.31	0.36	0.14	0.07	0.02	0.09	0.21	0.25	0.33	0.37	
ZPR20 20C	0.38	0.34	0.37	0.21	0.23	0.00	0.00	0.42	0.13	0.12	0.35	0.08	0.40	0.43	0.45	0.43	0.42	0.42	0.37	0.38	0.38	0.31	0.32	0.45	0.15	0.09	0.32	0.38	0.48	0.53	0.68	0.81	
ZPR20 20D	0.48	0.42	0.47	0.27	0.29	0.00	0.00	0.52	0.03	0.03	0.40	0.02	0.50	0.55	0.57	0.54	0.52	0.47	0.47	0.48	0.35	0.35	0.45	0.55	0.18	0.10	0.08	0.16	0.30	0.36	0.45	0.52	
ZPR20 20E	0.17	0.15	0.16	0.09	0.10	0.00	0.00	0.18	0.01	0.01	0.14	0.01	0.17	0.19	0.20	0.19	0.18	0.16	0.15	0.14	0.13	0.11	0.11	0.13	0.19	0.07	0.04	0.02	0.05	0.10	0.12	0.13	0.18
ZPR21 21A	0.09	0.08	0.08	0.05	0.05	0.00	0.00	0.10	0.01	0.01	0.08	0.01	0.09	0.10	0.10	0.10	0.10	0.10	0.09	0.09	0.09	0.07	0.09	0.10	0.04	0.02	0.03	0.06	0.07	0.08	0.10	0.11	
ZPR21 21B	0.00	0.00	0.01	0.00	0.00	0.03	0.00	0.02	0.23	0.22	0.07	0.21	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	0.32	0.08	0.02	0.03	0.67	0.99	0.66	0.52	0.46	0.40	
ZPR21 21C	0.09	0.08	0.08	0.04	0.05	0.02	0.00	0.11	0.22	0.21	0.15	0.13	0.05	0.09	0.08	0.08	0.08	0.07	0.07	0.07	0.07	0.05	0.35	0.10	0.05	0.08	0.59	0.85	0.64	0.61	0.57	0.51	
ZPR21 21D	0.23	0.21	0.22	0.12	0.14	0.02	0.00	0.26	0.21	0.20	0.26	0.12	0.22	0.25	0.26	0.26	0.23	0.23	0.21	0.20	0.21	0.21	0.48	0.30	0.10	0.07	0.55	0.84	0.67	0.67	0.66	0.63	
ZPR21 21E	0.29	0.26	0.28	0.16	0.17	0.02	0.00	0.32	0.20	0.19	0.31	0.12	0.25	0.32	0.33	0.31	0.30	0.30	0.27	0.26	0.28	0.25	0.53	0.35	0.12	0.08	0.52	0.81	0.67	0.69	0.70	0.68	
ZPR21 21F	0.36	0.35	0.35	0.21	0.24	0.01	0.00	0.43	0.18	0.17	0.35	0.11	0.40	0.44	0.46	0.43	0.42	0.42	0.37	0.36	0.35	0.33	0.68	0.45	0.18	0.10	0.48	0.57	0.66	0.70	0.74	0.74	
ZPR21 21F	0.48	0.43	0.47	0.26	0.28	0.02	0.00	0.52	0.16	0.15	0.46	0.13	0.48	0.53	0.55	0.51	0.50	0.44	0.43	0.45	0.45	0.37	0.61	0.62	0.18	0.11	0.40	0.51	0.63	0.68	0.74	0.78	

Figure A87. ANL Benchmark Composition Covariance Matrix.





## APPENDIX B. BASIC UNCERTAINTIES IN ANL CRITICALS

Shown in Tables B1-B26 are the published uncertainties for all 33 configurations under consideration. These uncertainties were taken from the benchmark uncertainty summary table. Buried in the body of each benchmark report are further breakdowns of specific uncertainty types. For example, the summary table may contain one entry for depleted uranium, but the body of the report may include depleted uranium uncertainties in core, reflector and blanket locations. (The one entry will be the quadrature sum of all the individual entries.) These detailed uncertainties were used in the evaluation of covariances. (The list of all distinct uncertainty types used in this covariance analysis was given in Table 6 in the main body of this report.)

Table B1. Uncertainties for ZPR-3 Assembly 6F (IEU-MET-FAST-015).

<b>A SPHERICAL ASSEMBLY OF HIGHLY ENRICHED URANIUM, DEPLETED URANIUM, ALUMINUM AND STEEL WITH AN AVERAGE 235U ENRICHMENT OF 47 ATOM %</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, %<math>\Delta k</math></b>
Measurement Technique	Excess Reactivity	0.0062
	Inhour to $\Delta k$ Conversion	0.0002
	Temperature Uncertainty	0.0005
	Temperature Distribution	0.0010
	Reproducibility	0.0034
	Geometry	Matrix Interface Gap
Nominal Plate, Drawer Dimensions		0.0277
Matrix Tube Pitch		0.0410
Composition	HEU Plates	0.0784
	Depleted Uranium Plates	0.0540
	Aluminum Plates	0.0044
	Stainless Steel Plates	0.0009
	Aluminum Drawers	0.0009
	Steel in Matrix Tubes	0.0310
	Steel in DP Drawers	0.0004
	Humidity	0.0001
	Total	0.1129



Table B2. Uncertainties for ZPR-3 Assembly 11 (IEU-MET-FAST-016).

<b>A CYLINDRICAL ASSEMBLY OF HIGHLY ENRICHED URANIUM AND DEPLETED URANIUM WITH AN AVERAGE <sup>235</sup>U ENRICHMENT OF 12 ATOM % AND A DEPLETED URANIUM REFLECTOR</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, %<math>\Delta k</math></b>
Measurement Technique	Excess Reactivity	0.0054
	Inhour to $\Delta k$ Conversion	0.0002
	Temperature Uncertainty	0.0009
	Temperature Distribution	0.0010
	Reproducibility	0.0034
	Geometry	
	Matrix Interface Gap	0.0106
	Nominal Plate, Drawer Dimensions	0.0191
	Matrix Tube Pitch	0.0254
Composition		
	HEU Plates	0.0730
	Depleted Uranium Plates	0.0886
	Steel in Matrix Tubes	0.0012
	Steel in Drawers	0.0003
	Humidity	0.0001
	Total	0.1198

Table B3. Uncertainties for ZPR-3 Assembly 12 (IEU-COMP-FAST-004).

<b>A CYLINDRICAL ASSEMBLY OF HIGHLY ENRICHED URANIUM, DEPLETED URANIUM AND GRAPHITE WITH AN AVERAGE 235U ENRICHMENT OF 21 ATOM %</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, %<math>\Delta k</math></b>
Measurement Technique	Excess Reactivity	0.0052
	Inhour to $\Delta k$ Conversion	0.0004
	Temperature Uncertainty	0.0026
	Temperature Distribution	0.0010
	Reproducibility	0.0034
	Geometry	
Geometry	Matrix Interface Gap	0.0116
	Nominal Plate, Drawer Dimensions	0.0225
	Matrix Tube Pitch	0.0329
Composition		
	HEU Plates	0.0726
	Depleted Uranium Plates	0.0642
	Graphite Plates	0.0062
	Steel in Matrix Tubes	0.0160
	Steel in Drawers	0.0004
	Humidity	0.0001
	Total	0.1070



Table B4. Uncertainties for ZPR-3 Assembly 23 (HEU-MET-FAST-055).

<b>A CYLINDRICAL ASSEMBLY OF U METAL (93% 235U) AND ALUMINUM REFLECTED BY DEPLETED-URANIUM</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, % <math>\Delta k</math></b>
Measurement Technique		
	Data Fitting	0.0011
	Inhours to $\Delta k$	0.0067
	Temperature	0.0022
Geometry		
	Matrix Interface Gap	0.0500
	Nominal Plate Dimensions	0.0500
	Matrix Tube Pitch	0.1023
	Room Return	0.0200
	EU Piece Sizes	0.1213
Composition		
	Enriched Uranium	0.0782
	Al plates	0.0093
	Depleted Uranium in Reflectors	0.0503
	Kel-F	0.0110
	Steel in Matrix Tubes	0.0412
	Steel in Drawers	0.0005
	Impurities in Steel	0.0080
	Humidity	0.0001
	Total	0.2031

Table B5. Uncertainties for ZPR-3 Assembly 41 (IEU-MET-FAST-012).

<b>A CYLINDRICAL ASSEMBLY OF U METAL (16% <sup>235</sup>U), ALUMINUM, AND STEEL, REFLECTED BY DEPLETED-URANIUM</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, % <math>\Delta k</math></b>
Measurement Technique	Data Fitting	0.0009
	Inhours to $\Delta k$	0.0070
	Temperature	0.0041
Geometry	Matrix Interface Gap	0.0500
	Nominal Plate Dimensions	0.0500
	Matrix Tube Pitch	0.0300
	Room Return	0.0080
	Aluminum Perforations	0.0400
	EU Piece Sizes	0.1226
Composition	Enriched Uranium	0.0733
	Aluminum	0.0015
	Depleted Uranium	0.0532
	Kel-F	0.0008
	Stainless Steel	0.0081
	Humidity	0.0001
	Total	0.1759



Table B6. Uncertainties for ZPR-3 Assemblies 48 and 48B (MIX-COMP-FAST-003).

<b>CYLINDRICAL ASSEMBLIES OF MIXED (PU,U), GRAPHITE AND SODIUM WITH A DEPLETED URANIUM BLANKET</b>			
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, %<math>\Delta k</math></b>	
		<b>ZPR-3/48</b>	<b>ZPR-3/48B</b>
Measurement Technique			
	Experimentalist's Estimate	0.0010	0.0020
	Inhour to $\Delta k$ Conversion	0.0030	0.0050
	Temperature Uncertainty	0.0065	0.0065
	Reproducibility	0.0025	0.0025
Geometry			
	Matrix Interface Gap	0.0200	0.0200
	Nominal Plate, Drawer Dimensions	0.0200	0.0200
	Matrix Tube Pitch	0.0318	0.0318
Composition			
	Plutonium	0.0305	0.0285
	Uranium in Pu-U-Mo Plates	0.0071	0.0073
	Molybdenum in Pu-U-Mo Plates	0.0002	0.0002
	Aluminum in Pu-Al Plates	0.0006	0.0005
	Sodium Plates	0.0013	0.0013
	Graphite Plates	0.0023	0.0023
	Depleted Uranium Plates	0.0421	0.0421
	Steel in Matrix Tubes	0.0088	0.0088
	Steel in Drawers	0.0004	0.0004
	Steel in Cans (Pu, Na)	0.0005	0.0005
	Kel-F Coating	0.0019	0.0019
	Humidity	0.0001	0.0001
	Total	0.0687	0.0680

Table B7. Uncertainties for ZPR-3 Assembly 56B (MIX-COMP-FAST-004).

<b>A CYLINDRICAL ASSEMBLY OF MIXED (PU,U), OXIDE AND SODIUM WITH A NICKEL-SODIUM REFLECTOR</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, %<math>\Delta k</math></b>
Measurement Technique		
	Experimentalist's Estimate	0.0006
	Inhour to $\Delta k$ Conversion	0.0031
	Temperature Uncertainty	0.0036
	Reproducibility	0.0024
Geometry		
	Matrix Interface Gap	0.0192
	Nominal Plate, Drawer Dimensions	0.0192
	Matrix Tube Pitch	0.0321
Composition		
	Plutonium	0.0436
	Uranium in Pu-U-Mo Plates	0.0137
	Molybdenum in Pu-U-Mo Plates	0.0004
	Sodium Plates	0.0024
	Sodium Carbonate Plates	0.0057
	Iron Oxide Plates	0.0037
	Depleted U3O8 Plates	0.0171
	Nickel Plates	0.0155
	Steel in Matrix Tubes	0.0083
	Steel in Drawers	0.0013
	Steel in Cans (Pu, Na)	0.0029
	Kel-F Coating	0.0007
	Humidity	0.0001
	Total	0.0674



Table B8. Uncertainties for ZPR-6 Assembly 6A (IEU-COMP-INTER-005/IEU-COMP-FAST-001).

A CYLINDRICAL ASSEMBLY WITH URANIUM OXIDE FUEL AND SODIUM WITH A THICK DEPLETED-URANIUM BLANKET		
Source of Uncertainty	Uncertainty Type	Uncertainty in Excess Reactivity % $\Delta k$
Measurement Technique	Measurement Uncertainty	0.0050
	Inhours to Delta k	0.0082
	Temperature	0.0044
Geometry	Matrix Interface Gap	0.0097
	Nominal Plate Dimensions	0.0097
	Matrix Tube Pitch	0.0395
	Room Return	0.0082
Composition	Enriched Uranium Plates	0.0697
	Depleted U Plates in the Core	0.0236
	Uranium Oxide Plates	0.0299
	Sodium	0.0025
	Iron Oxide Plates	0.0130
	Steel Plates in the Core	0.0016
	Uranium in Blanket	0.0122
	Non-Matrix Steel	0.00002
	Steel in the Matrix Tubes	0.0025
	Kel-F Paint	0.0104
	PSR Control Rods (blades)	0.0115
	Thermocouple	0.0037
	Humidity	0.0001
	Total	0.0940

Table B9. Uncertainties for ZPR-6 Assembly 7 (MIX-COMP-FAST-001).

<b>A CYLINDRICAL ASSEMBLY WITH MIXED (PU,U)-OXIDE FUEL AND SODIUM WITH A THICK DEPLETED-URANIUM REFLECTOR</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity % <math>\Delta k</math></b>
Measurement Technique		
	Data Fitting	0.0031
	Inhours to $\Delta k$	0.0047
	Temperature	0.0029
Geometry		
	Matrix Interface Gap	0.0058
	Nominal Plate Dimensions	0.0058
	Matrix Tube Pitch	0.0405
	Room Return	0.0042
Composition		
	Plutonium	0.0455
	Depleted Uranium in Pu-U-Mo Plates	0.0239
	Molybdenum in Pu-U-Mo	0.0007
	Sodium	0.0010
	Iron Oxide Plates	0.0081
	Uranium Oxide Plates	0.0377
	Uranium in Reflector	0.0152
	Steel in the Matrix Tubes	0.0244
	Steel in the Drawers	0.0018
	Steel in the Cans	0.0015
	Kel-F Paint	0.0256
	PSR Control Rods	0.0116
	Humidity	0.0001
	Total	0.0867

Table B10. Uncertainties for ZPR-6 Assembly 7 High 240Pu Core (MIX-COMP-FAST-002).

<b>A CYLINDRICAL ASSEMBLY WITH MIXED (PU,U)-OXIDE FUEL AND A CENTRAL HIGH 240PU ZONE</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity % <math>\Delta k</math></b>
Measurement Technique		
	Experimentalists' Estimate	0.0029
	Inhours to $\Delta k$ conversion	0.0023
Geometry		
	Matrix Interface Gap	0.0058
	Nominal Plate Dimensions	0.0058
	Matrix Tube Pitch	0.0404
	Room Return	0.0034
Composition		
	Plutonium	0.0468
	Uranium in Pu-U-Mo Plates	0.0131
	Molybdenum	0.0005
	Sodium	0.0013
	Iron Oxide Plates	0.0133
	Uranium Oxide Plates	0.0360
	Uranium in Reflector	0.0157
	Steel in the Matrix Tubes	0.0233
	Steel in the Drawers	0.0030
	Steel in the Cans	0.0029
	Kel-F Paint	0.0007
	PSR Control Blades	0.0090
	Autorod Blade	0.0292
	Humidity	0.0001
	Total	0.0855



Table B11. Uncertainties for ZPR-6 Assembly 10 (PU-MET-INTER-002).

<b>A CYLINDRICAL PLUTONIUM/CARBON/STAINLESS STEEL ASSEMBLY WITH STAINLESS STEEL AND IRON REFLECTORS</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity (% <math>\Delta k</math>)</b>
Measurement Technique		
	Excess in $I_h$ (including temperature uncertainty)	0.0020
	$I_h$ to $\Delta k$	0.0034
Geometry		
	Matrix Interface Gap	0.0073
	Nominal Plate Dimensions	0.0058
	Matrix Tube Pitch	0.0374
	PSR Blades	0.0003
	Room Return	0.0017
Composition		
	Plutonium	0.0333
	Graphite	0.0160
	Stainless Steel and Iron	0.1151
	Humidity	0.0001
	Total	0.1270

Table B12. Uncertainties for ZPR-9 Assembly 1 (IEU-MET-FAST-013).

<b>A CYLINDRICAL ASSEMBLY OF U METAL (93% <sup>235</sup>U) AND DEPLETED URANIUM WITH ALUMINUM REFLECTORS</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity (%<math>\Delta k</math>)</b>
Measurement Technique	Data Fitting	0.0002
	Ih to $\Delta k$	0.0093
	Temperature	0.0037
Geometry	Matrix Interface Gap	<0.0001
	Nominal Plate Dimensions	<0.0001
	Matrix Tube Pitch	0.0450
	Room Return	0.0520
Composition	Enriched Uranium	0.0732
	Depleted Uranium	0.0036
	Kel-F	0.0008
	Aluminum	0.0124
	Humidity	0.0001
	Total	0.1018

Table B13. Uncertainties for ZPR-9 Assemblies 2 and 3 (IEU-MET-FAST-014).

<b>CYLINDRICAL ASSEMBLIES OF U METAL AND TUNGSTEN WITH ALUMINUM REFLECTORS</b>			
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity (% <math>\Delta k</math>)</b>	
		<b>ZPR-9/2</b>	<b>ZPR-9/3</b>
<b>Measurement Technique</b>			
	Data Fitting	0.0002	0.0002
	Ih to $\Delta k$	0.0181	0.0116
	Temperature	0.0041	0.0041
<b>Geometry</b>			
	Matrix Interface Gap	0.0046	0.0046
	Nominal Plate Dimensions	0.0037	0.0037
	Matrix Tube Pitch	0.0265	0.0240
	Room Return	0.0427	0.0427
<b>Composition</b>			
	Enriched Uranium	0.0794	0.0829
	Depleted Uranium	0.0274	0.0206
	Kel-F	0.0023	0.0021
	Tungsten	0.0101	0.0183
	Aluminum	0.0110	0.0096
	Steel	0.0001	0.0001
	Humidity	0.0001	0.0001
	<b>Total</b>	<b>0.1009</b>	<b>0.1016</b>



Table B15. Uncertainties for ZPR-9 Assembly 4 (HEU-MET-FAST-060).

<b>A CYLINDRICAL ASSEMBLY OF U METAL (93% 235U) AND TUNGSTEN WITH ALUMINUM REFLECTORS</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity (% <math>\Delta k</math>)</b>
Measurement Technique	Data Fitting	0.0002
	Ih to $\Delta k$	0.0083
	Temperature	0.0041
Geometry	Matrix Interface Gap	0.0046
	Nominal Plate Dimensions	0.0037
	Matrix Tube Pitch	0.0342
	Room Return	0.0427
	Uranium Axial Distribution	0.0375
Composition	Enriched Uranium	0.0891
	Kel-F	0.0004
	Tungsten	0.0179
	Aluminum	0.0165
	Humidity	0.0001
	Total	0.1142

Table B16. Uncertainties for ZPR-9 Assemblies 5 and 6 (HEU-MET-FAST-067).

<b>HEU (93% <sup>235</sup>U) CYLINDRICAL CORES WITH TUNGSTEN, GRAPHITE, AND ALUMINUM DILUENTS WITH A DENSE ALUMINUM REFLECTOR</b>			
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity (% Δk)</b>	
		<b>ZPR-9/5</b>	<b>ZPR-9/6</b>
<b>Measurement Technique</b>			
	Data Fitting	0.0002	0.0002
	Ih to Δk	0.0094	0.0126
	Temperature	0.0037	0.0036
<b>Geometry</b>			
	Matrix Interface Gap	0.0046	0.0046
	Nominal Plate Dimensions	0.0037	0.0037
	Matrix Tube Pitch	0.0533	0.0584
	Room Return	0.0427	0.0427
<b>Composition</b>			
	Enriched Uranium	0.0848	0.0888
	Kel-F	0.0010	0.0008
	Tungsten	0.0171	0.0142
	Graphite (Carbon)	0.0083	
	Aluminum	0.0138	0.0176
	DP Rod Steel	0.0001	0.0001
	Humidity	0.0001	0.0001
	<b>Total</b>	<b>0.1120</b>	<b>0.1176</b>

Table B17. Uncertainties for ZPR-9 Assemblies 7, 8 and 9 (HEU-MET-FAST-070).

<b>CYLINDRICAL CORES WITH HEU (93% 235U), TUNGSTEN, AND ALUMINUM OR ALUMINUM OXIDE WITH A DENSE ALUMINUM, ALUMINUM OXIDE, OR BERYLLIUM OXIDE REFLECTOR</b>				
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity (%<math>\Delta k</math>)</b>		
		<b>ZPR-9/7</b>	<b>ZPR-9/8</b>	<b>ZPR-9/9</b>
Measurement Technique				
	Data Fitting	0.0002	0.0002	0.0002
	Ih to $\Delta k$	0.0175	0.0081	0.0123
	Temperature	0.0036	0.0036	0.0036
Geometry				
	Matrix Interface Gap	0.0046	0.0046	0.0046
	Nominal Plate Dimensions	0.0037	0.0037	0.0037
	Matrix Tube Pitch	0.0701	0.0788	0.0667
	Room Return	0.0427	0.0427	0.0427
Composition				
	Enriched Uranium	0.0824	0.0824	0.0815
	Kel-F	0.0005	0.0019	0.0005
	Tungsten	0.0186	0.0174	0.0198
	Beryllium	-	0.0137	-
	Aluminum	0.0255	0.0127	0.0214
	DP Rod Steel	0.0001	0.0001	0.0001
	Humidity	0.0001	0.0001	0.0001
	Total	0.1220	0.1249	0.1182



Table B18. Uncertainties for ZPR-9 Assembly 34 Loading 11 U9 Benchmark  
(IEU-MET-FAST-010).

<b>A CYLINDRICAL ASSEMBLY OF U METAL (9% <sup>235</sup>U) WITH A THICK DEPLETED-URANIUM REFLECTOR</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, % <math>\Delta k</math></b>
Measurement Technique	Data Fitting	0.0002
	Inhours to $\Delta k$	0.0072
	Temperature	0.0038
Geometry	Matrix Interface Gap	0.0063
	Plate Axial Position	0.0063
	Matrix Tube Pitch	0.0168
	Room Return	0.0028
Composition	Enriched Uranium	0.0691
	Depleted Uranium in Core	0.0940
	Depleted Uranium in Reflectors	0.0262
	Kel-F	0.0064
	Steel in Matrix Tubes	0.0124
	Steel in Drawers	0.0006
	Humidity	0.0001
	Total	0.1222

Table B19. Uncertainties for ZPR-9 Assembly 34 Loading 303 Uranium/Iron Benchmark  
(HEU-MET-INTER-001).

<b>A 235U(93%)/IRON CYLINDER REFLECTED BY STAINLESS STEEL</b>			
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Excess Reactivity, % <math>\Delta k</math></b>	
Measurement Technique	Data Fitting	0.0002	
	Inhours to $\Delta k$	0.0032	
	Temperature	0.0043	
Geometry	Matrix Interface Gap	0.0081	
	Plate Axial Position	0.0081	
	Matrix Tube Pitch	0.0647	
	PSR Axial Position	0.0001	
	Room Return	0.0198	
	13 Unknown Reflector Positions	0.0027	
	Missing Axial Reflector Drawer	0.0075	
Composition	Enriched Uranium	0.0595	
	Depleted Uranium in Shield	0.0021	
	Iron and Steel in Core	0.0457	
	Steel in Reflectors	0.0363	
	Steel in Shield	0.0002	
	Aluminum in Core	0.0065	
	Aluminum in Reflectors	0.0067	
	PSR Blades	0.0136	
	Kel-F	0.0029	
	Humidity	0.0001	
		<b>Total</b>	<b>0.1097</b>

Table B20. Uncertainties for ZPPR-20 Phase C (HEU-MET-FAST-075).

<b>A CYLINDRICAL ASSEMBLY OF U METAL REFLECTED BY BERYLLIUM OXIDE</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, % <math>\Delta k</math></b>
Measurement Technique		
	Data Fitting	0.0022
	Dollars to $\Delta k$	0.0135
	Temperature	0.0050
Geometry		
	Matrix Interface Gap	0.0431
	Nominal Plate Dimensions	0.0340
	Matrix Tube Pitch	0.0981
	Room Return	0.0058
Composition		
	Uranium	0.0908
	Rhenium	0.0040
	Depleted Lithium	0.0019
	Niobium	0.0026
	Sodium	0.0007
	Beryllium Oxide	0.0181
	Kel-F	0.0011
	Beryllium metal	0.0003
	Lithium hydride	0.0001
	Tungsten	0.0001
	“Control” Boron Carbide	0.0009
	Borated Polyethylene Shield	0.0001
	Stainless Steel	0.0747
	Humidity	0.0001
	Total	0.1641



Table B21. Uncertainties for ZPPR-20 Phase D (HEU-MET-MIXED-012).

<b>A CYLINDRICAL ASSEMBLY OF POLYETHYLENE-MODERATED U METAL REFLECTED BY BERYLLIUM OXIDE AND POLYETHYLENE</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, % <math>\Delta k</math></b>
Measurement Technique		
	Data Reduction	0.0003
	Dollars to $\Delta k$	0.0016
	Temperature	0.0050
Geometry		
	Matrix Interface Gap	0.0426
	Nominal Plate Dimensions	0.0330
	Matrix Tube Pitch	0.0507
	Room Return	0.0001
Composition		
	Uranium	0.0765
	Rhenium	0.0103
	Niobium	0.0052
	Beryllium Oxide	0.0101
	Kel-F	0.0041
	Polyethylene	0.0061
	Lithium hydride	0.0001
	“Control” Boron Carbide	0.0192
	PSR Boron Carbide	0.0003
	Stainless Steel	0.0129
	Humidity	0.0001
	Total	0.1104

Table B22. Uncertainties for ZPPR-20 Phase D Subcritical (SUB-HEU-MET-MIXED-001).

<b>A CYLINDRICAL ASSEMBLY OF POLYETHYLENE-MODERATED U M ETAL REFLECTED BY BERYLLIUM OXIDE AND POLYETHYLENE</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, % <math>\Delta k</math></b>
<b>Measurement Technique</b>		
	Data Reduction	0.1670
	Dollars to $\Delta k$	0.2447
	Temperature	0.0050
<b>Geometry</b>		
	Matrix Interface Gap	0.0426
	Nominal Plate Dimensions	0.0340
	Matrix Tube Pitch	0.0507
	Room Return	0.0001
<b>Composition</b>		
	Uranium	0.0765
	Rhenium	0.0103
	Niobium	0.0015
	Beryllium Oxide	0.0101
	Kel-F	0.0041
	Polyethylene	0.0061
	Lithium hydride	0.0001
	“Control” Boron Carbide	0.0269
	Stainless Steel	0.0129
	Humidity	0.0001
	<b>Total</b>	<b>0.3168</b>

Table B23. Uncertainties for ZPPR-20 Phase E Subcritical (SUB-HEU-MET-FAST-001).

<b>A CYLINDRICAL ASSEMBLY OF U METAL REFLECTED BY BERYLLIUM OXIDE AND SAND</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, % <math>\Delta k</math></b>
<b>Measurement Technique</b>		
	Data Reduction	0.5396
	Dollars to $\Delta k$	0.4497
	Temperature	0.0050
<b>Geometry</b>		
	Matrix Interface Gap	0.0456
	Nominal Plate Dimensions	0.0340
	Matrix Tube Pitch	0.0738
	Room Return	0.0039
<b>Composition</b>		
	Uranium	0.0920
	Rhenium	0.0040
	Depleted Lithium	0.0006
	Niobium	0.0010
	Beryllium Oxide	0.0107
	Kel-F	0.0007
	Sand	0.0025
	Sodium Carbonate	0.0003
	“Control” Boron Carbide	0.0232
	Borated Polyethylene Shield	0.0001
	Stainless Steel	0.0344
	Humidity	0.0001
	<b>Total</b>	<b>0.7159</b>



Table B24. Uncertainties for ZPPR-21 Phase A (PU-MET-FAST-033).

<b>A CYLINDRICAL ASSEMBLY OF PU METAL REFLECTED BY GRAPHITE</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, % <math>\Delta k</math></b>
Measurement Technique	Data Fitting	0.0003
	Dollars to $\Delta k$	0.0012
	Temperature	0.0050
Geometry	Matrix Interface Gap	0.0469
	Nominal Plate Dimensions	0.0360
	Matrix Tube Pitch	0.0594
	Room Return	0.0236
Composition	Plutonium	0.0466
	Aluminum in Fuel	0.0002
	Molybdenum in Fuel	0.0004
	Depleted Uranium	0.0074
	Kel-F	0.0017
	Zirconium	0.0064
	Graphite	0.0334
	Lithium Hydride	0.0004
	Borated Polyethylene	0.0001
	Stainless Steel	0.1083
	Humidity	0.0001
	<b>Total</b>	<b>0.1507</b>

Table B25. Uncertainties for ZPPR-21 Phases B-E (MIX-MET-FAST-011).

<b>CYLINDRICAL ASSEMBLIES OF MIXED FISSILE PU AND U METAL REFLECTED BY GRAPHITE</b>					
Source of Uncertainty	Uncertainty Type	Uncertainty in Excess Reactivity, % $\Delta k$			
		ZPPR-21B	ZPPR-21C	ZPPR-21D	ZPPR-21E
Measurement Technique					
	Data Fitting	0.0004	0.0005	0.0005	0.0006
	Dollars to $\Delta k$	0.0005	0.0036	0.0068	0.0046
	Temperature	0.0050	0.0050	0.0050	0.0033
Geometry					
	Matrix Interface Gap	0.0469	0.0469	0.0469	0.0469
	Nominal Plate Dimensions	0.0360	0.0360	0.0360	0.0360
	Matrix Tube Pitch	0.0565	0.0572	0.0565	0.0565
	Room Return	0.0215	0.0201	0.0215	0.0215
Composition					
	Plutonium	0.0369	0.0275	0.0181	0.0086
	Aluminum in Fuel	0.0002	0.0001	0.0001	0.0000
	Molybdenum in Fuel	0.0004	0.0004	0.0004	0.0004
	Enriched Uranium	0.0152	0.0457	0.0609	0.0914
	Depleted Uranium	0.0071	0.0069	0.0071	0.0071
	Kel-F	0.0020	0.0020	0.0020	0.0020
	Zirconium Mass	0.0031	0.0030	0.0031	0.0031
	Hydrogen in Zirconium	0.0108	0.0114	0.0108	0.0108
	Graphite Mass	0.0325	0.0338	0.0325	0.0325
	Boron in Graphite	0.0102	0.0102	0.0102	0.0102
	Lithium Hydride	0.0004	0.0004	0.0004	0.0004
	Borated Polyethylene	0.0001	0.0001	0.0001	0.0001
	Stainless Steel wt.%	0.0080	0.0080	0.0080	0.0080
	Stainless Steel Mass	0.1021	0.1010	0.1021	0.1021
	Humidity	0.0001	0.0001	0.0001	0.0001
	Total	0.1435	0.1478	0.1519	0.1656

Table B26. Uncertainties for ZPPR-21 Phase F (HEU-MET-FAST-061).

<b>A CYLINDRICAL ASSEMBLY OF U METAL REFLECTED BY GRAPHITE</b>		
<b>Source of Uncertainty</b>	<b>Uncertainty Type</b>	<b>Uncertainty in Excess Reactivity, % <math>\Delta k</math></b>
<b>Measurement Technique</b>		
	Data Fitting	0.0007
	Dollars to $\Delta k$	0.0028
	Temperature	0.0033
<b>Geometry</b>		
	Matrix Interface Gap	0.0469
	Nominal Plate Dimensions	0.0360
	Matrix Tube Pitch	0.0529
	Room Return	0.0209
<b>Composition</b>		
	Enriched Uranium	0.1162
	Depleted Uranium	0.0070
	Kel-F	0.0046
	Zirconium	0.0161
	Graphite	0.0333
	Lithium Hydride	0.0004
	Borated Polyethylene	0.0001
	Stainless Steel	0.0976
	Humidity	0.0001
	<b>Total</b>	<b>0.1766</b>







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