WEST END ASSEMBLY HALL PLATFORM
DESIGN CALCULATIONS

D-ZERO ENGINEERING NOTE # 3823.115- EN-441

January 3, 1996

Russ Rucinski
RD/DØ Mech.

Approved :

A handwritten signature in black ink, appearing to read 'Russ Rucinski', is written over a horizontal line. The signature is stylized and cursive.

This engineering note documents design calculations done for the bayonet feed can platform installed at the far west end of the assembly hall. The platform is mounted off of a cast concrete wall directly south of where the shielding block wall is stacked.

SUMMARY

A summary of the loading, reaction forces and stresses is shown on the page 3. As can be seen, the calculated stresses are very small, maximum value = 2540 psi. The material used is structural steel tubing, ASTM A500 Gr. B, with a minimum yield strength of 46 ksi and minimum ultimate tensile strength of 58 ksi.

The reaction forces for the upper two members will be carried together by a 1/2" mounting plate. The mounting plate is attached to the wall by four 1/2" Hilti wedge anchors. The allowables for each wedge anchor are 2400 lbs. tensile, 1960 lbs. shear. The major reaction load for the top members is a combined 3627 lbs. tensile load which can easily be handled by the four bolt pattern. Some small moment reactions not listed on the summary page add negligible (400 lbs.) force couples to the axial loading. The bottom members are also attached to a mounting plate that is bolted to the wall. See page 15 for Hilti wedge anchor data.

ANALYSIS DETAILS

A finite element program was run on a SDRC/IDEAS package for the structure. The printout and displays on pages 3 through 6 are from that run. Beam elements with 3" x 6" x 3/16" wall rectangular tubing properties were used. The model used 114 nodes placed at 3" spacing which yielded 112 beam elements between the nodes. The largest maximum Von Mises stress calculated was 2.54 ksi. This is at least a factor of ten below the allowable. The allowable tensile, shear, and bending stress for these members are 27 ksi, 18.4 ksi, and 30.4 ksi respectively. [See D-Zero engineering note 3823.115-EN-417 HX support bracket Design Calcs. for allowables and similar structure.

The loads used were generated by hand calcs. on pages 7 through 9. They consist of:

400 lbs. for each bayonet can, 800 lbs. total

882 lbs. for support of the west end piping

A 50 lbs./ft² floor loading, 478 lbs.

Gravity on the members, 295 lbs. weight

This is a grand total vertical y direction loading of 2455 lbs. This corresponds well to the summation of y reaction forces of 2520 lbs. on the finite element reaction force printout.

A fabrication sketch of the platform is shown on page 10. The platform was detailed for 4 x 8 x 1/4" rectangular tubing, because that was the free stock available at the D-Zero assembly building. Since that fab. sketch was made, we found and chose to make the platform out of 3" x 6" x 3/16" rectangular tubing. The calculations were done for that choice. A formal "as built" detail drawing is being made. The D-Zero drawing number is 3823.115-MC-317494 and is kept in the electronic drawing control system. Some overall layout views are included on pages 11 through 14 to give some perspective to the platform's intended use.

SUMMARY OF LOADS, REACTIONS, AND STRESSES

RESULTS: 3- B.C. 1, LOAD 1, STRESS_3

MAGNITUDE - MIN: 2.58E+02 MAX: 2.54E+03

Data component: VON MISES STRESS at maximum point
MAX DEFLECTION = .03 in.

/dks4d3s7/ms_rucinski/westplatform2

VALUE OPTION: ACTUAL

GRAVITY ALSO APPLIED
STRUCTURE WT. ≈ 295 LBS.

SCALE: NODE SPACING @ 3"

MOMENT REACTIONS NOT SHOWN HERE.
SEE PRINTOUT MAX MOMENTS ≈ 4000 IN-LBS

6

I-DEAS Master Series 2.1: Simulation
/dks4d3s7/ms_rucinski/westplatform2

04-Jan-96 09:03:36

Node	Reacti-X	Reacti-Y	Reacti-Z	Reacti-RX	Reacti-RY	Reacti-RZ
103	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
104	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
105	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
106	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
107	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
108	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
109	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
110	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
111	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
112	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
113	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
114	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
Total	0.000E+00	2.520E+03	0.000E+00	6.315E+03	-1.013E+03	-7.009E+03
	91	89	91	91	90	1
Maximum	2.526E+03	1.438E+03	3.910E+01	4.048E+03	5.517E+02	0.000E+00
	89	1	89	1	89	91
Minimum	-2.617E+03	0.000E+00	-3.901E+01	0.000E+00	-1.029E+03	-4.302E+03
Average	0.000E+00	2.250E+01	0.000E+00	5.638E+01	-9.049E+00	-6.258E+01

10" BOLT SPACING
 ∴ ~ 400 LB FORCE
 COUPLE & ANCHORS

ode	Reacti-X	Reacti-Y	Reacti-Z	Reacti-RX	Reacti-RY	Reacti-RZ
49	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
50	-1.010E+03	5.684E+02	-2.657E+01	5.792E+02	-7.360E+02	-2.439E+02
51	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
52	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
53	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
54	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
55	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
56	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
57	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
58	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
59	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
60	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
61	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
62	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
63	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
64	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
65	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
66	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
67	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
68	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
69	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
70	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
72	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
73	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
74	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
75	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
76	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
77	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
78	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
79	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
80	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
81	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
82	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
83	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
84	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
85	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
86	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
87	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
88	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00	0.000E+00
89	-2.617E+03	1.438E+03	-3.901E+01	6.115E+02	-1.029E+03	-2.801E+02
90	1.101E+03	2.346E+02	2.649E+01	1.076E+03	5.517E+02	-2.183E+03
91	2.526E+03	2.785E+02	3.910E+01	4.048E+03	1.999E	

LOADS FOR WEST END PLATFORM• VLPC BAYONET FEED CAN:

$$\text{TOP PLATE: } \frac{\pi D^2}{4} \times t \times \rho_{ss} = \frac{\pi (20 \text{ in})^2}{4} (.625) (.283 \frac{\text{lb}}{\text{in}^3})$$

$$= 56 \text{ lbs}$$

$$\text{PIPE SHELL} = 20 \text{ " SCH. 5S } \times 31 \text{ ' } (39.8 \frac{\text{lb}}{\text{ft}})$$

$$= 103 \text{ lbs}$$

$$\text{BOTTOM HEAD} \approx 50 \text{ lbs}$$

Cu RAD SHIELD

$$\text{Cu SHELL} = \pi (16 \text{ "}) (28 \text{ in}) (.0625 \text{ in}) (.317 \frac{\text{lb}}{\text{in}^3})$$

$$= 28 \text{ lbs.}$$

$$\text{Cu LIPS} = \frac{\pi (16 \text{ "})^2}{4} (.0625) (.317) (2 \text{ lbs}) = 8 \text{ lbs}$$

$$6 \text{ - BRONESS} \approx 120 \text{ lbs}$$

$$\text{TOTAL DEAD WT.} = 56 + 103 + 50 + 28 + 8 + 120 = 365 \text{ lbs}$$

$$\approx \boxed{400 \text{ lbs.}}$$

$$\bullet \text{ SOLENOID FEED CAN: } \approx \boxed{400 \text{ lbs}}$$

• DISTRIBUTED LOADS

$$8 \times 4 \times \frac{1}{4} \text{ MEMBERS @ } 19.02 \frac{\text{lb}}{\text{ft.}}$$

$$\text{TOTAL WT.} = 29 \text{ ft} \times 19 \frac{\text{lb}}{\text{ft}} = \boxed{553 \text{ lbs.}}$$

SUCTION HEADER + OTHER PIPES SPANNING
FROM BRACKETS.

$$\approx \underline{875 \text{ *}} \text{ FOR 12.5 FE OF SPAN.}$$

{ SEE WEST PIPING LOADS 12-20-95 }

- ADDITIONAL 50 lb/ft^2 LOADING.

$$\text{FLOOR AREA} = \left(\frac{62.25 \text{ ft}}{12} \right) \left(\frac{27.8125 + 4}{12} \text{ ft} \right)$$

$$= 13.75 \text{ ft}^2$$

$$\text{CAN AREAS} = \frac{\pi D^2}{4} \times 2 = \frac{\pi \left(\frac{20}{12} \right)^2}{4} \times 2 = 4.36 \text{ ft}^2$$

$$\text{NET AREA} = 9.4 \text{ ft}^2$$

$$\text{NET } 50 \text{ lb/ft}^2 \text{ LOADING} = \boxed{470 \text{ lbs}}$$

- INTEGRATING THESE LOADS INTO MODEL:

APPLY 200 lbs POINT LOAD TO ① & ②
@ SOLENOID & VLPC CAN LOCATIONS.

APPLY GRAVITY TO ALL MEMBERS 19.02 ft

$$\text{APPLY DISTRIBUTED; } \frac{875 \text{ lbs}}{27.8125 \text{ in}} = 31.5 \frac{\text{lbs}}{\text{in}} \text{ TO } \textcircled{5}$$

FOR PIPE LOADING

$$\text{APPLY DISTRIBUTED; } \frac{470 \text{ lbs}}{(62.25)2 + (62.25 - 9.25) \text{ in}} = 2.65 \frac{\text{lbs}}{\text{in}} \text{ TO } \textcircled{1} \textcircled{2} \textcircled{3}$$

SINCE ~~N~~ BEARING,
WILL DOUBLE GRAVITY,

FOR 50 lb/ft^2
LOAD

TOTAL LOADS

$$31.5 \text{ #/IN.} \times (30 \text{ IN.}) = 882 \text{ #'S}$$

$$2.655367 \text{ #/IN} \times 180 \text{ IN} = 478 \text{ #'S}$$

$$\text{GRAVITY} \approx 295 \text{ #'S} \quad \text{FOR } 3 \times 6 \times 1/4 \text{ TUBG}$$

$$\text{CANS} \quad 4 \text{ LOADS} \times 200 = 800 \text{ #'S}$$

$$\Sigma \text{ LOADS} \mid \approx 2455 \text{ #'S}$$

Y DIRECTION

OLD
RUNS
DISREGARD.

~~BASED ON LOW STRESSES & LOADINGS, I WILL
DECREASE THE 45° ANGLE TO 30°.~~

~~THIS CHANGES THE VERTICAL CENTER TO CENTER
SPACING ON THE MOUNTING PADS~~

~~FROM 50.163" (MODEL) 22
TO 26.105~~

~~THEREFORE % TENSION/COMPRESSION WILL DOUBLE~~

$$(1363 + 782)(2) = 4290 \text{ #}$$

$$(1406 + 738)(2) = 4288 \text{ #}$$

~~A FOUR BOLT PATTERN FOR THE PLATES
IS ADEQUATE BASED ON HX BRACKET DESIGN.~~

~~LOOK @ BENDING MOMENTS.~~

$$R_z = 247 \text{ IN.-LBS}$$

$$R_y = 310 \text{ IN.-LBS}$$

$$R_z = 2358 \text{ IN.-LBS} @ 10\frac{1}{2}'' \text{ SPACING}$$

~~225 # FORCE COUPLE~~

~~NEGIGIBLE. OK.~~

FABRICATION DETAIL SKETCH

NOTE: THIS DETAIL IS DRAWN FOR $4 \times 8 \times \frac{1}{4}$ TUBE MEMBERS

$3 \times 6 \times \frac{3}{16}$ TUBE MEMBERS WERE ACTUALLY USED.

USED MIN. $\frac{3}{16}$ FILLET OR $\frac{3}{16}$ FULL PENETRATION R. RUGINSKI
 GROOVE WELDS AT ALL JOINTS AS
 APPROPRIATE.

1-3-95

ITEM	PART NO.	QUANTITY	DESCRIPTION	DATE	BY
PARTS LIST					
1	1	1	PIPE, 1/2" DIA.		
2	1	1	FLANGE, 1/2"		
3	1	1	VALVE, 1/2"		
4	1	1	PIPE, 1/2" DIA.		
5	1	1	FLANGE, 1/2"		
6	1	1	VALVE, 1/2"		
7	1	1	PIPE, 1/2" DIA.		
8	1	1	FLANGE, 1/2"		
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97	1	1	PIPE, 1/2" DIA.		
98	1	1	FLANGE, 1/2"		
99	1	1	VALVE, 1/2"		
100	1	1	PIPE, 1/2" DIA.		

(F)

Setting Details			Anchor Size					
			HKB ¼"	HKB ⅜"	HKB ½"	HKB ⅝"	HKB ¾"	HKB 1"
BD = D drill bit size = anchor diameter			¼"	⅜"	½"	⅝"	¾"	1"
E depth of embedment (minimum/standard)			1½"/2"	1⅝"/2½"	2¼"/3½"	2¾"/4"	3¼"/4¾"	4½"/6"
HD hole depth (E + 1 *D) min./std.			1⅝" / 2¼"	2" / 2⅞"	2¾" / 4"	3⅝" / 4⅝"	4" / 5½"	5½" / 7"
DC wedge clearance hole			⅝"	7/16"	9/16"	11/16"	13/16"	1⅝"
L anchor length min./max.			1¾" / 4½"	2¼" / 7"	2¾" / 7"	3¾" / 10"	4¾" / 12"	6" / 12"
TL thread length std./extra thread length			¾" / 3"	⅞"/1⅝" / 4"	1¼" / 4"	1½" / 3½"/4½"	1½" / 3½"/4½"	2¼" / 4½"
M Installation torque (ft. lb.) guide values	Stainless	min. E	4	20	40	85	150	235
	Steel	std. E	7	30	75	110	200	450
	Carbon	min. E	4	20	40	85	150	250
	Steel	std. E	7	25	65	110	235	450
BMT Min. Base Material Thickness (inches)			3" or 1.3E whichever number is greater					

Listings

Conforms to the description in Federal Specification FF-S-325, Group II, Type 4, Class 1 for concrete expansion anchors.
 UL listed, "Pipe Hangers" (¾" - 1½" diameters). International Conference of Building Officials, ICBO Evaluation Report #4627.
 Factory Mutual listed "Pipe Hangers" ¾" KB II w/rod coupler.
 Southern Building Code Congress International, SBCCI Report #8913
 City of Los Angeles Research Report #24946

Anchor Program Standard Kwik Bolt II Sizes

Item Number	Description	Hole Dia. (In.)	Anchor Length (In.)	Min. Embed. Depth (In.)	Thread Length	Hilti Drill Bit	Qty. Per Box/Ctn.	Std. Emb. (In.)	Allowable Working Loads 4000 psi Concrete	
									Tension (lbs.)	Shear (lbs.)
000453597	KB II 14-134	¼"	1¾"	1⅝"	¾"	TE-C+ ¼-6	100/900	2"	630	530*
000453605	KB II 14-214	¼"	2¼"				100/900			
000453613	KB II 14-314	¼"	3¼"				100/400			
000453621	KB II 38-214	⅜"	2¼"	1⅝"	⅞"	TE-C+ ⅜-6	100/500	1⅝"	750	1470*
000453639	KB II 38-3	⅜"	3	1⅝"	1⅝"	TE-C+ ⅜-6	100/400	2½"	1370	1470*
000453647	KB II 38-334	⅜"	3¾"				100/400			
000453654	KB II 38-5	⅜"	5				50/200			
000453662	KB II 12-234	½"	2¾"	2¼"	1¼"	TE-C+ ½-6	50/200	3½"	2400	2450*
000453670	KB II 12-334	½"	3¾"			TE-C+ ½-12	50/200			
000453688	KB II 12-412	½"	4½"				50/200			
000453696	KB II 12-512	½"	5½"				25/125			
000453704	KB II 58-334	⅝"	3¾"	2¾"	1½"	TE-C+ ⅝-6	25/100	4"	3290	3840**
000453712	KB II 58-434	⅝"	4¾"			TE-C+ ⅝-12	25/75			
000453720	KB II 58-6	⅝"	6				25/75			
000453738	KB II 58-7	⅝"	7				25/75			
000453746	KB II 34-434	¾"	4¾"	3¼"	1½"	TE-C+ ¾-8	20/80	4¾"	4800	5120**
000453753	KB II 34-512	¾"	5½"			TE-C+ ¾-12	20/80			
000453761	KB II 34-7	¾"	7				10/40			
000453779	KB II 34-8	¾"	8				10/40			
000454124	KB II 1-6	1	6	4½"	2¼"	TE-FY1-13	5/25	6"	7070	9200
000454132	KB II 1-9	1	9				5/20			

*Values shown are for shear plane acting through the anchor bolt shank. When the shear plane is acting through the anchor bolt threads, reduce shear values by 20%

**Values shown are for a shear plane acting through the anchor bolt shank. When the shear plane is acting through the anchor bolt threads, reduce the shear value by 12%.

All other values shown are for shear plane acting through either body or threads.