CO₂ SELECTIVE CERAMIC MEMBRANE FOR WATER-GAS-SHIFT REACTION WITH CONCOMITANT RECOVERY OF CO₂

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ABSTRACT

In this quarter, we have focused on the completion of the loose ends of the experimental study. A series of CO₂-affinity membranes (carbonaceous base) prepared previously were characterized and evaluated for their suitability for the proposed application The CO₂ permeance and selectivity are 0.5 to >3 m³/m²/hr/bar and 4 to 10 for CO₂ over nitrogen respectively. Based upon its performance dependence on temperature and pore size, we conclude that this type of CO₂ affinity membrane shows significant surface affinity to CO₂ over nitrogen even at the temperature as high as 220°C, which is within the typical operating condition for LTS-WGS. Future study should focus on mixture separations for CO/CO₂/H₂ to establish the selectivity of CO₂ over CO and H₂ which are present in the WGS reaction of the coal gasifier off-gas.

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1. INTRODUCTION

In this quarter, we have focused on the completion of the loose ends of the experimental study. There are two different types of CO_2 -affinity membranes have been explored throughout this project. One (Type I) is based upon the hydrotalcite based materials which have demonstrated a unique affinity to CO_2 at a high temperature in the presence of steam. The other one (Type II) is the carbonaceous microporous membrane which has demonstrated surface affinity to CO_2 . In this quarterly report, we will summarize the representative performance of the Type II membranes we have prepared and/or characterized during this period.

2. EXECUTIVE SUMMARY

In this quarter, we have focused on the completion of the loose ends of the experimental study. A series of CO₂-affinity membranes (carbonaceous base) prepared previously were characterized and evaluated for their suitability for the proposed application The CO₂ permeance and selectivity are 0.5 to >3 m³/m²/hr/bar and 4 to 10 for CO₂ over nitrogen respectively. Based upon its performance dependence on temperature and pore size, we conclude that this type of CO₂ affinity membrane shows significant surface affinity to CO₂ over nitrogen even at the temperature as high as 220°C, which is within the typical operating condition for LTS-WGS. Pore size reduction was attempted, showing no improvement in the CO₂ affinity. Future study should focus on mixture separations for CO/CO₂/H₂ to establish the selectivity of CO₂ over CO and H₂ which are present in the WGS reaction of the coal gasifier off-gas.

3. EXPERIMENTAL

- A series of Type II membranes (10"L) have been prepared using our commercial ceramic membranes as substrate. They are first deposited with selected precursors and then calcined at a selected temperature to form the desired pore size and surface properties. The single component gas permeation study was performed to measure their permeances of CO₂ and N₂ at 25, 120, 180 and in some cases 220°C.
- The protocol developed for 10"L was employed for the preparation of the 30"L membrane to evaluate its scale up possibility. The 30"L membranes were characterized for their CO₂ and N₂ permeances at a similar temperature range.
- 3. One of the 10"L membranes was deposited an additional layer to evaluate the potential improvement in selectivity via pore size reduction. The additional layer was prepared and characterized following a similar protocol as above.

4. RESULTS AND DISCUSSION

- Table 1 summarizes all the membranes prepared and characterized for this project. Their single component permeances (including He, H₂, N₂, and CO₂, and methane) at 23 to 220°C were presented. Then ideal selectivities were calculated.
- 2. CO_2 permeance vs selectivity (over N₂) at 120°C for all the 10"L membranes is presented in Figure 1. In general, the overall trend for permeance vs selectivity follows the familiar inverse relationship. When the CO₂ permeance is > $3m^3/m^2/hr/bar$, the selectivity for CO₂/N₂ ranges from 2 to 4. On the other hand, when the CO₂ permeance is <0.5 m³/m²/hr/bar, the selectivity between 6 and 12 is obtained. In comparison with the Knudsen selectivity of 0.798, our selectivities obtained here are definitely enhanced to much beyond the Knudsen selectivity.
- 3. Majority of the membrane tubes were prepared with a lab scale substrate, i.e., 10"L as presented in Table 1. Four 30" long tubes were prepared following the same protocol as the 10"L tubes. The permeance and selectivity obtained from the 30" L are in line

with the trend established by the 10" tubes. Thus, the scale-up from the lab scale (10"L) to the full scale of 30"L appears acceptable.

- 4. The permeances and selectivities at 180 to 220°C were presented in Figure 2. This temperature range is the usual temperature range for the LTS-WGS we proposed. Due to the number of data points at these temperatures were much fewer than those of the 120°C shown in Figure 1, the permeance vs selectivity trend was not well defined. However, the permeance and selectivity fell within the range of 0.5 to 2.5 m³/m²/hr/bar and 4 to 8, respectively. In comparison with the data obtained at a lower temperature, i.e., 120°C, the selectivity at the higher temperature is somewhat lower than that at the lower temperature.
- 5. Figures 3a to 3c show the effect of temperature on the CO_2 permeance from 120 to 180°C. It appears that CO₂ permeance decreases along with the temperature increase. For Figure 3a and 3b, about 50% reduction of the CO₂ permeance was observed along with the temperature increase in this range. The CO₂ permeance reduction ratio for Figure 3c, however, is <<50%. The helium permeance decreases in Figure 3b while increases in Figure 3c, so is the trend for the hydrogen permeance. It is possible that the majority of the pore size in Figure 3a and 3b are larger than those in Figure 3c; thus, the helium and hydrogen permeances are somewhat influenced by the Knudsen diffusion in Figure 3b, while the helium and hydrogen permeances are dominated by activated diffusion in Figure 3c. Since the CO_2 permeance reduction vs temperature in Figure 3a and 3b is much more sever than the theoretical prediction based upon the Knudsen diffusion (i.e., 7%), it is concluded that the permeance for CO₂ is at least partially contributed by another mechanism, surface diffusion. When the pore size is small enough as shown in Figure 3c, the surface diffusion contribution decreases while the molecular sieving becomes pronounced. Even with the pore size decreases shown in Figure 3c, no improvement in CO₂ selectivity was observed. Thus, it is believed that the separation mechanism for this type of material is contributed by both surface diffusion and molecular sieving. At the temperature range interested to us, both mechanisms are likely involved.

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6. Table 2 presents the permeance and selectivity for the membrane with an additional layer of deposition and calcination for the purpose of narrowing the pore size. The result indicates no improvement in selectivity although the permeance was reduced dramatically, from 1.88 to $0.035 \text{ m}^3/\text{m}^2/\text{hr/bar}$. This is consistent with the mechanisms proposed above. The pore size reduction theoretically could improve the selectivity although the difference in the kinetic diameters of CO₂ vs N₂ is very small. On the other hand, when the pore size becomes small enough, the surface diffusion contribution is diminished. Thus, the permeance is reduced dramatically while no clear sign of selectivity improvement is observed.

5. CONCLUSIONS

The Type II CO₂ affinity membranes prepared in this quarter demonstrated significant selectivity for CO₂/N₂, i.e., 4 to 10, up to 220°C, which is much beyond the Knudsen selectivity. Surface affinity of the membrane toward CO₂ was identified as the dominating mechanism at this operating temperature range. Pore size reduction was attempted, showing no improvement in the CO₂ affinity. Future study should focus on the mixture separations for CO/CO₂/H₂ to establish the selectivity of CO₂ over CO and H₂ which are present in the WGS reaction of the coal gasifier off-gas.

Bibliography:

None

Acronyoms :

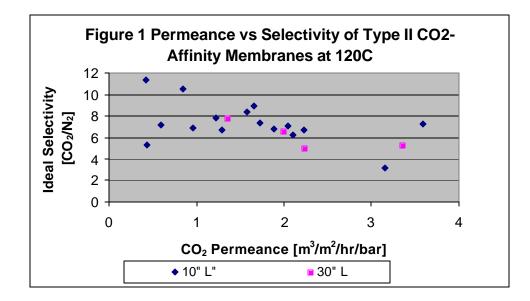
LTS:	Low temperature shift

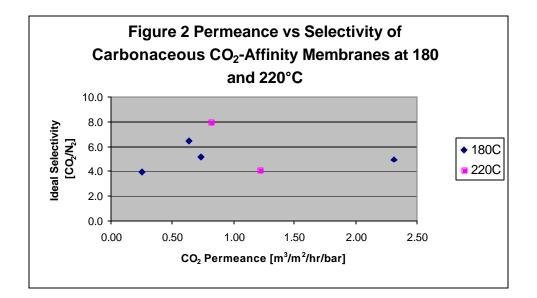
WGS: Water gas shift

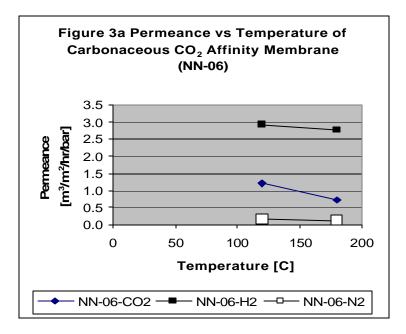
Table 1Summary of Type II CO2 Affinity Membranes and their Performance

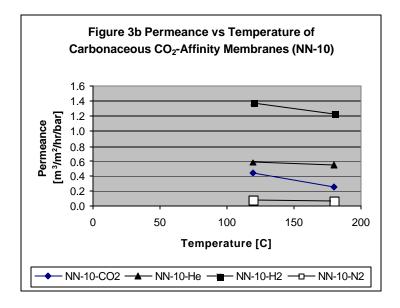
Characterization

Sample ID	Temp	Press	Perm	neance	-	/hr/bar]				electivity	
10" CO2 Affinity	[c] Membraen	[psi] s	He	H ₂	N2	CO ₂	CH4	He/N ₂	H_2/N_2 (CO2/N2 N	2/CH4
		00	0.054	0.040	0 7 4 0				- 4	- 4	
NN-01-2	23 120	30 30	2.051 1.765	3.846 4.198	0.748 0.330	4.011 2.239		2.7 5.3	5.1 12.7	5.4 6.8	
NN-02&03	120 180	20 20	1.231 1.483	2.816 3.039	0.080 0.097	0.846 0.633		15.3 15.2	35.1 31.2	10.6 6.5	
NN-06-03	180 120	20 20	1.203	2.753 2.939	0.140 0.155	0.730 1.216	0.098	8.6	19.6 19.0	5.2 7.8	1.4
NN-10-03	120	20	0.541	1.373	0.081	0.432	0.059	6.7	16.9	5.3	1.4
	180	20	0.585	1.227	0.064	0.254		9.1	19.1	4.0	1.4
NN-14	120	30	2.804	5.529	0.998	3.152		2.8	5.5	3.2	
NN-15	120	20	1.171	1.866	0.083	0.595	0.089	14.2	22.6	7.2	0.9
NN-47	120	20	3.429	7.344	0.276	1.880	0.157	12.4	26.6	6.8	1.8
NN-66	120	20	2.420	6.362	0.188	1.578	0.092	12.9	33.9	8.4	2.0
NN-71	120	20	0.707	1.804	0.037	0.418		19.2	48.9	11.3	
NN-80	120 180	20 20	2.868 3.215	7.464 7.285	0.494 0.470	3.585 2.315	0.523 0.458	5.8 6.8	15.1 15.5	7.3 4.9	0.9 1.0
	120	30	2.010	4.646	0.185	1.655	0.169	10.9	25.2	9.0	1.1
NN-81	120	20	2.642	6.129	0.289	2.048		9.1	21.2	7.1	
NN-82	120	20	1.654	4.349	0.234	1.726	0.112	7.1	18.6	7.4	2.1
NN-94	120 120	20 20	1.819 1.545	4.250 3.462	0.335 0.191	2.110 1.288	0.355 0.173	5.4 8.1	12.7 18.1	6.3 6.7	0.9 1.1
30" Length CO2	Affinity M	embranes									
NN-27	120	20	1.370	3.106	0.445	2.229		3.1	7.0	5.0	
NN-29	120 220	20 20	1.643 2.015	4.650 4.544	0.304 0.299	1.994 1.222	0.200 0.215	5.4 6.7	15.3 15.2	6.6 4.1	1.5 1.4
NN-30	120	20	0.990	2.956	0.176	1.360		5.6	16.8	7.7	
	220	20	0.879	2.082	0.103	0.821		8.5	20.1	7.9	
NN-49	120	20	2.136		0.632	3.354		3.4		5.3	









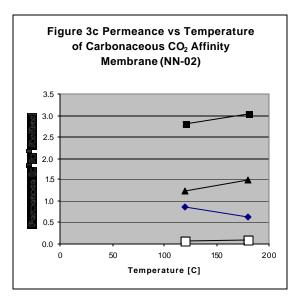


Table 2 Effect of Additional Layer Deposition on Performance of Type II CO² Affinity Membrane

Sample ID Notes	Temp	Press [psi]	Permeance		[m ³ /m ² /hr/bar]						
	[c]		He	H_2	N_2	CO ₂	CH4	He/N ₂	H_2/N_2	CO_2/N_2	N ₂ /CH ₄
NN-47	120	20	3.429	7.344	0.276	1.880	0.157	12.4	26.6	6.8	1.8
additonal deposition and firing	120	20	0.665	0.965	0.044	0.035	0.044	15.2	22.0	0.8	1.0