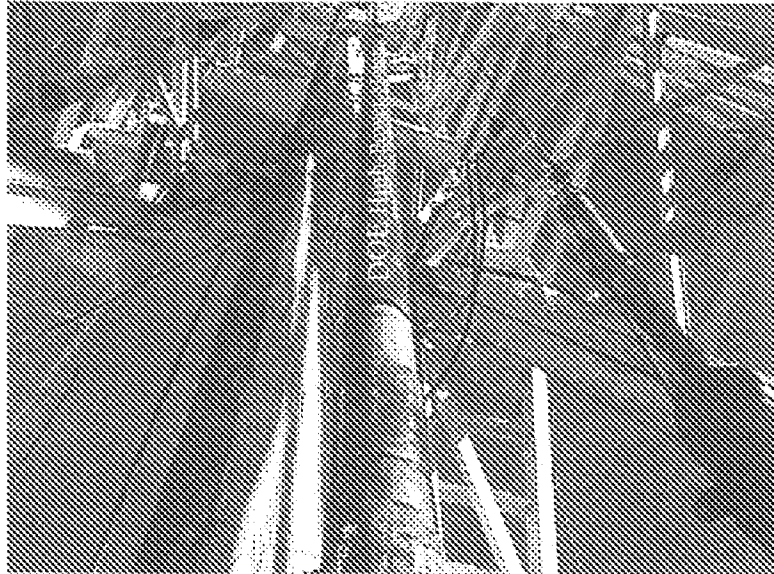


DOE High-Power Slim-Hole Drilling System



Prepared for

Mr. Roy C. Long
DEPARTMENT OF ENERGY
3610 Collins Ferry Road
Morgantown, West Virginia 26507-0880

By

Dr. William C. Maurer
John H. Cohen
J. Chris Hetmaniak
Curtis Leilko
MAURER ENGINEERING INC.
2916 West T.C. Jester, Houston, Texas 77018-7098
Tel: 713-683-8227 • Fax: 713-683-6418
E-mail: mel@maureng.com • <http://www.maureng.com>

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DOE HIGH-POWER SLIM-HOLE DRILLING SYSTEM

EXECUTIVE SUMMARY

Introduction

This project used a systems approach to improve slim-hole drilling performance. A high power mud motor, having a double-length power section, and hybrid PDC/TSP drill bit were developed to deliver maximum horsepower to the rock while providing a long life down hole. This high-power slim-hole drilling system drills much faster than conventional slim-hole motor and bit combinations and holds significant potential to reduce slim-hole drilling costs.

The oil and gas industries have been faced with downward price pressures since the 1980s. These pressures are not expected to be relieved in the near future. To maintain profitability, companies have had to find ways to reduce the costs of producing oil and gas. Drilling is one of the more costly operations in the production process.

One method to reduce costs of drilling is to use smaller more mobile equipment. Slim holes have been drilled in the past using this principle. These wells can save money not only from the use of smaller drilling equipment, but also from reduced tubular costs. Stepping down even one casing size results in significant savings. However, slim holes have not found wide spread use for three reasons. First, until recently, the price of oil has been high so there were no forces to move the industry in this direction. Second, small roller bits and motors were not very reliable and they drilled slowly, removing much of the economic benefit. The third and final reason was the misconception that large holes were needed every where to deliver the desired production.

Several factors have changed that will encourage the use of slim holes. The industry now favors any method of reducing the costs of producing oil and gas. In addition, the industry now understands that large holes are not always needed. Gas, in particular, can have high production rates in smaller holes. New materials now make it possible to manufacture improved bits and motors that drill for long periods at high rates. All that remains is to gather all the elements together and demonstrate the savings of slim hole drilling.

Technical Approach

This project used new and improved materials along with advanced designs to improve the performance of two key down hole components. The components are the drill bit and the mud motor that drives the bit. By combining thermally stable cutters (TSP) with the more conventional poly crystalline compact (PDC) cutters a new hybrid bit was produced that extends the range of rock hardnesses that can be drilled. This new bit is run

on a motor that produces twice the torque and thus twice the power of conventional motors. This allows more weight to be applied to the bit which in turn allows the rock to be drilled faster.

Mud motors convert hydraulic power in the drill mud (pressure and flow) to mechanical power (rotary speed and torque). To increase the power output of a motor the speed or torque must be increased and a corresponding increase in flow or pressure. An analysis of this energy system shows that the best way to achieve higher power is to increase torque and pressure.

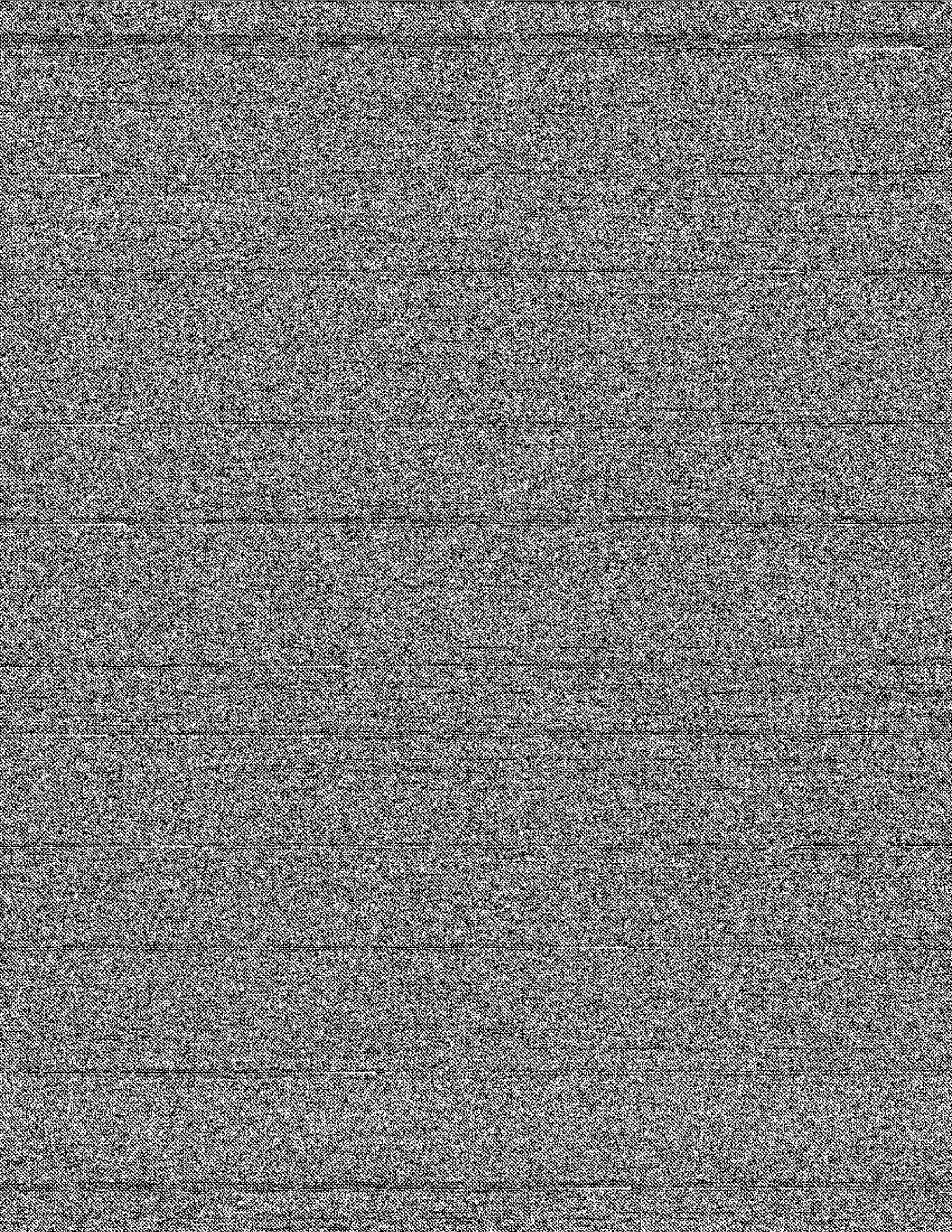
The torque output of a motor is proportional to the pressure drop across the motor. The only way to increase the pressure drop is to increase the per stage pressure drop or increase the number of stages. Materials used to manufacture the stator of a mud motor limit the increase in per stage pressure drop so the best way to increase motor power is to increase the number of stages.

Two conventional 3-3/8 in. stator sections were welded together using a proprietary process, and a special rotor machined to form a single long power section. This power section was combined with a modified bearing pack. The modified bearing pack used high strength metal-to-metal radial bearings, stronger roller thrust bearings, and a titanium flex shaft to improving the strength of a conventional bearing pack. The titanium flex shaft replaces the conventional flex coupling used to transmit the rotary power from the power section to the bearing pack shaft.

The increased power of the DOE high-power motor must be utilized by the bit to drill rock. Current PDC bits are a great improvement over small roller bits. The small bearings in these slim-hole roller bits fail quickly and thus can not drill very far. The PDC bits can drill soft to medium hard formations and last a long time. However, in hard abrasive formations or softer formations with hard stringers these bits fail. If slim hole drilling is to succeed this limitation must be overcome. TSP cutters are much more wear resistant than PDC cutters so they can drill hard abrasive rock. Their size however, makes them subject to bit balling in soft sticky formation like shales. Combining the two cutter types produces a bit that can drill quickly through soft formations but not wear out when drilling hard abrasive formations. This bit extends the range of rock types that can be drill and thus can eliminate the need to make trips for bit changes.

Testing

Following design and manufacture, the high-power slim-hole drilling system was subjected to laboratory dynamometer and drilling tests. The dynamometer tests were used to measure the performance of the high power motor for comparison to conventional designs. The data from these tests were used to plot performance curves that were later used in drilling and field tests. Life test were also conducted on the dynamometer to identify reliability problems so they could be corrected before field testing. The drilling tests evaluated the hybrid bit and high-power motor as a system. These data provided correct



Slim hole drilling can save significant dollars through reduced rig and equipment size along with reduce tubular costs. The DOE high-power slim-hole system overcomes the problems that occurred in the past with conventional motors and bits making slim holes much more competitive and practical to drill in today's market. The hybrid bit and high-power motor should be commercialized. This will require a marketing effort to make bit and motor companies realize the benefits that can be achieved with slim hole drilling.

1. INTRODUCTION

1.1 Background

The oil and gas industry has undergone significant restructuring over the last two decades in response to downward price pressures. This has included an intense effort to reduce drilling costs. A study conducted by Maurer Engineering on deep gas wells¹ found that drilling rate and bit life have the greatest impact on overall well costs. For an average deep well (> 15,000 ft.), 48 percent of the rig time is spent rotating the bit and 22% tripping the drill pipe to replace or change out components of the bottomhole assembly (Figure 1.1). This indicates that the primary focus of research and development should be on increasing penetration life and extending BHA component life. As shown in Table 1.1, doubling the penetration rate will reduce well costs by 13%.

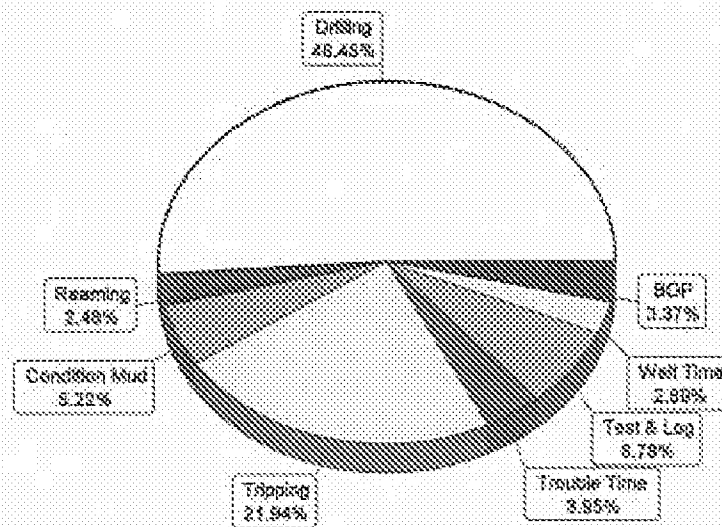


Figure 1.1. Time Study Of Wells > 14,000 Feet Deep¹

In addition to increasing drilling rate and BHA component life, past experience has shown that use of slim holes can provide further savings by reducing the size and therefore the costs of the drilling rig and the tubular goods (casing and production tubing) used to complete the well. During the 1950s and 1960s, over 3000 slim holes were drilled worldwide². These slim holes lowered well costs by 27 to 75% in many areas. Although significant savings were realized, the industry nevertheless largely abandoned slim holes in favor of larger diameter wells in the 1970s and 1980s. The primary reasons for this were: 1) the shorter life obtained by small diameter roller bits compared to larger bits due to bearing deficiencies; 2) high oil prices which increased the desire to maximize production rates; and 3) the general misconception that large holes were needed. In light

of today's economic climates, many companies are now re-examining the use of slim hole drilling because improved small diameter motors equipped with advanced shear bit technology have reduced costs by 30 to 40%³.

Table 1.1 Cost Reductions Due to a Factor of 2 Change¹

DRILLING PARAMETER	PERCENTAGE COST REDUCTION
Penetration Rate	13.0
Rig Day Rate	10.0
Casing Materials	8.0
Bit Life	7.5
Casing Time	5.5
"Other" Time	4.0
Trip Time	3.0

There are three basic types of slim-hole drilling systems (Figure 1.2):

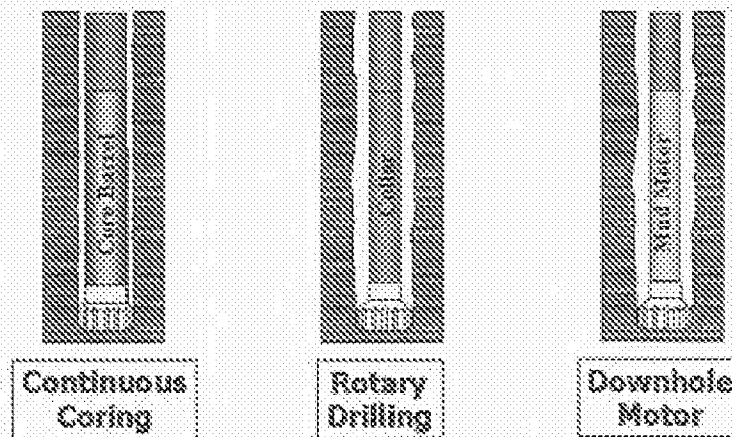


Figure 1.2. Basic Slim-hole Drilling Systems

Continuous Coring systems use slim-hole mining core barrels to continuously core entire wells or substantial sections of wells. Although wireline retrievable core barrels are used to increase overall drilling speed, the overall process is usually slower than conventional drilling. As a result, the method is used in new drilling areas where geologists need cores to define geology. Depth has not been a limiting factor, as specialty slim-hole

coring rigs have been built capable of drilling to 14,000 feet.

Rotary slim-hole rigs rotate PDC and natural diamond bits at speeds of 300 to 800 rpm. Special small diameter strings have been designed for these rotary slim-hole rigs. Typical drill pipe is 3.5 x 2.92 in. for drilling with bits 8½ to 4¾ in. and 2.25 x 1.89 in. for bits 4¾ to 3 inches.

Twist-offs of the small-diameter drill pipe have been a problem with the rotary system. Special controls are required to control the torque on the drill pipe and maintain correct weight on bit.

Downhole Motor systems utilize slim-hole motors to rotate TSP, PDC, natural diamond, and roller-cone bits at speeds of 300 to 2000 rpm. These motors drill at high rates and eliminate drill-string twist-offs by eliminating drill-string rotation.

Downhole motors add an additional expense to the drilling operation that must be offset by improved drilling performance. If improved performance is not observed, then cost performance calculations are difficult because motor cost is being compared to the intangible of "will a drill-string failure occur."

1.2 OBJECTIVES

The overall objective of this project is to implement new high-power slim-hole motors and drill bits into slim-hole gas well drilling applications. The development of these motors and bits is critical to overcome problems such as twist-offs and slow drilling rates associated with existing rotary slim-hole systems as well as the short motor and drill bit lives of current state-of-the-art tools.

Conventional motors drill most formations 2 to 3 times faster than rotary or continuous coring systems due to greater power transfer to the drill bit. New high-power motors and hybrid TSP/PDC bits under study and development at Maurer Engineering Inc. (MEI) drill 3 to 5 times faster than conventional motors. These new slim-hole motors and bits should reduce drilling costs by 30 to 50 percent in many areas by increasing drilling rates and by reducing casing costs.

Other DOE sponsored work on improved TSP diamond cutters has shown that bits built with these cutters could save 15 percent on overall well costs and 7.5 percent on drilling costs³. These dramatic costs due to increased production rate and bit life would be further increased if used with the high-power motor.

1.3 SCOPE OF WORK

To achieve the objectives stated above, Maurer Engineering will utilize the results of the GRI project including the design of the high-power motors and bits. Field test sites will

be selected, and motors and bits will then be designed and manufactured for these sites. During Phase I, the motors and bits were extensively laboratory tested at MEI's Drilling Research Center, including motor tests on a dynamometer test stand and drilling tests on a motor drilling test stand.

Additional high-power slim-hole motors and bits were manufactured and field tested during Phase II. The bits were tailored to the formations to be drilled at the Amoco Catoosa shallow well test site and at other deeper gas well sites. The drilling data from these field tests were analyzed in detail using MEI computer programs. A detailed final report has now been prepared to allow service companies and operators to implement this technology into their gas well drilling operations.

Phase I-Task Summary

- Task 1. Design High-Power Motor
- Task 2. Fabrication of SH High-Power Motor
- Task 3. Conduct High-Power Motor Dynamometer Tests
- Task 4. Design Large Cutter TSP Bit
- Task 5. Fabrication of TSD Drill Bit
- Task 6. Laboratory Testing of the SH High-Power Drilling System

Phase II-Task Summary

- Task 7. Test Plan and Required Information for the National Environmental Policy Act
- Task 8. Plan/Conduct Shallow Field Tests
- Task 9. Slim-Hole Drilling System Redesign
- Task 10. Manufacture Field Grade Motor/Bits
- Task 11. Dynamometer Test Field Motors
- Task 12. Conduct Laboratory Drilling Tests
- Task 13. Conduct Field Drilling Tests

2. HIGH-POWER HYBRID DRILL BITS

This chapter describes the development of the hybrid PDC/TSP slim-hole drill bits. Being drag bits, PDC/TSP bits do not have bearings to prematurely wear out like those found in smaller diameter roller bits. However, without the new design features incorporated into the hybrid bit to last longer and drill harder, more abrasive formations, the economic benefits of higher power slim-hole motors could not be effectively realized.

2.1 Polycrystalline Diamond & Thermally Stable Cutters

Polycrystalline diamond cutter (PDC) bits work well on motors in soft to medium hard rocks (up to 15,000 psi compressive strength). The PDC cutters consist of a thin layer of small synthetic diamond bonded to a tungsten-carbide substrate as shown in Figure 2.1.

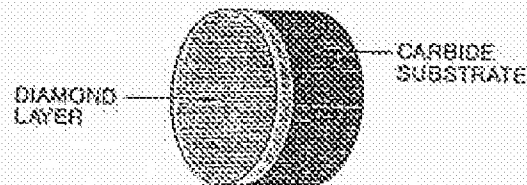


Figure 2.1. PDC Cutter

Early PDCs had a weak bond between the diamond layer and the carbide substrate. Although sufficient for most rotary drilling applications, these early cutters suffered from diamond layer de-bonding (cutter failure) when used on motors because of the higher rotary speeds. Improved bonding techniques have allowed PDC bits to gain increased use on downhole motors.

Two types of PDC bits are commonly used today. Steel body bits have pressed-in tungsten-carbide studs with PDC cutters attached. Matrix bits have PDCs brazed directly to the bit body (Figure 2.2). Steel-body bits are less expensive to manufacture than matrix bits, but often suffer erosion problems when used with abrasive drilling muds or on long bit runs. Hard metal coatings have been used to solve this problem, but add to the bit's cost and manufacturing complexity. Matrix bits are manufactured by infiltrating a molten cobalt/nickel binder (1100°C) into tungsten-carbide powder, making them very erosion resistant and ideal for high-performance drilling motors.

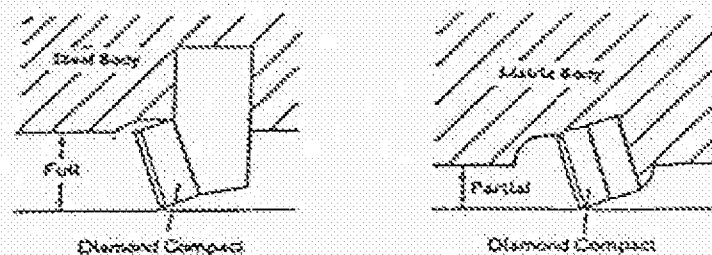


Figure 2.2. PDC Cutter Mounting Techniques

PDC cutters have been very successful in drilling medium-strength rocks such as shale, but they wear out rapidly when drilling hard rock. The major cause of premature wear in hard rock is the thermal limitations of PDC material as shown in Figure 2.3.

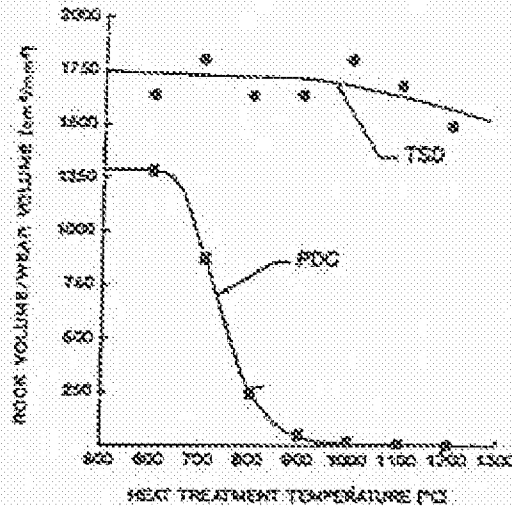


Figure 2.3. Effect of Temperature on Granite Drilling Tests.⁵

PDC cutters fail at high temperatures because the cobalt binder holding the diamonds together expands more rapidly than the diamond carbon lattice, thereby causing the PDC cutters to thermally fracture (Figure 2.4).

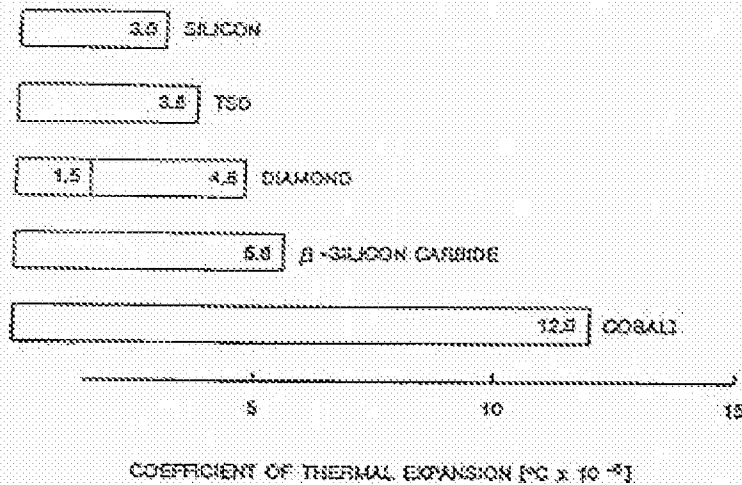


Figure 2.4. Coefficient of expansion for diamond and cobalt.⁶

General Electric (Geoset) and De Beers (SYNDAX 3) have developed thermally stable diamond cutters (TSP) in which the cobalt binder is removed to allow them to operate at much higher temperatures (Figure 2.3). The high-temperature capability of these TSP cutters allows them to be cast directly into matrix bits as shown in Figures 2.5 and 2.6.

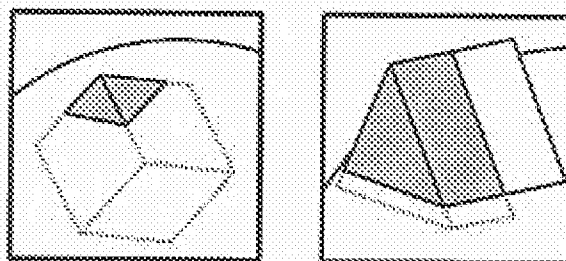


Figure 2.5. TSP Cutters In Matrix

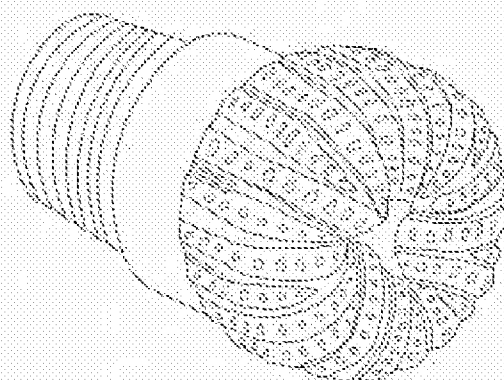


Figure 2.6. TSP Bit

TSP matrix bits are ideally suited for high performance motor drilling. Wear tests run at Sandia National Laboratories show that TSPs are more wear resistant than PDCs. In the Sandia tests, cutters held in an instrumented holder are used to mill off the top of a Sierra White granite rock. The wear of the cutter is then plotted against the volume of rock removed (Figure 2.7). The data show that TSP is approximately seven times more wear resistant than PDC. Figure 2.8 shows that these bits can drill in excess of 90 meters (300 ft) before wearing out in granite, an igneous rock that is much harder than the sedimentary rocks normally encountered in oil or gas wells.

The key to the successful use of hybrid bits is to match the torque/speed characteristics of bits to downhole motors, thereby optimizing use of motor power by maximizing drilling rate and bit life. This can be done using computer programs that predict

bit and motor performance or with empirical data from laboratory and/or field drilling.

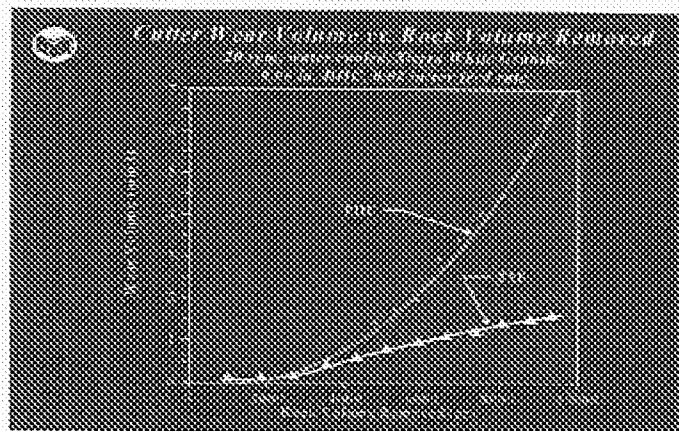


Figure 2.7. Sandia Wear Test.

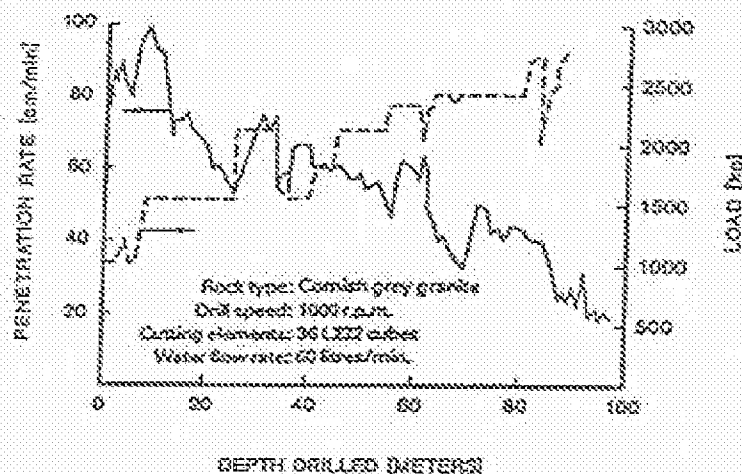


Figure 2.8. TSP Drilling Data In Granite.⁴

Many large manufacturers of bits have developed very sophisticated computer software that can accurately predict the forces generated on cutters and bits as they drill through different formations. These programs are used to predict the resultant loads on bits so that anti-whirl pads can be correctly placed on bit bodies. These same programs can be used to make bit designs that match the torque and speed characteristics of motors.

Motor manufacturers use computer programs to calculate the torque and speed characteristics of different designs. Recent work has focused on Finite Element programs to optimize the rotor/stator shapes and the rubber compounds for different applications. These data are used to match the motor and bit.

Laboratory and field test data can also be used to match motors and bits either to

confirm computer output or as an alternative. This can often be more precise because of manufacturing or material variations. MEI considers it essential to confirm predicted motor performance by testing motors on a dynamometer test stand. Significant differences have been observed between predicted and measured performance.

Confirmation of bit performance is very important primarily because prediction of formation characteristics is very difficult. Small changes in depth, water content, or surrounding stress fields can significantly alter rock behavior.

The motors and bits developed in this project made use of a combination of computer software predictions and empirical data from laboratory drilling and dynamometer tests.

2.2 TSP Drill Bit Design Factors

MEI previously conducted a multi-phase study to improve TSP bits for deep gas drilling. This work showed that the primary design parameters that control drilling rate and bit life are 1) cutter orientation, 2) cutter size, and 3) density or number of cutters on the bit (Figure 2.9). Test results show that large cutters set with an exposed sharp edge or point drill the fastest. Bits with a high density of cutters have the longest life because the redundant cutters reduce the work load and thus reduce the wear and breakage.

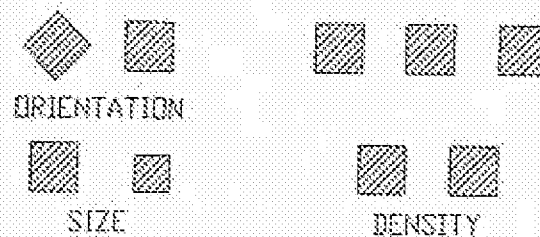


Figure 2.9. TSP Cutter Variables

Thirteen different TSP bits (Table 2.1) were tested on the Drilling Research Center (DRC) drilling test stand shown in Figure 2.10.

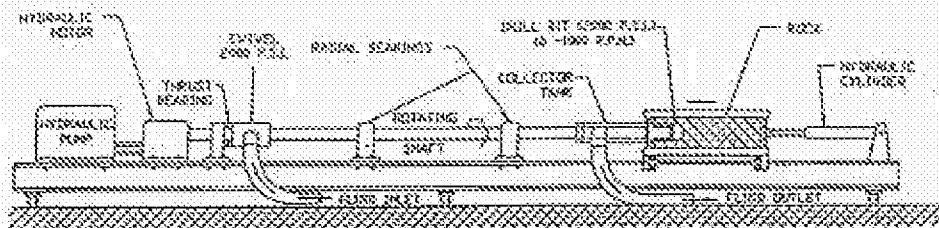


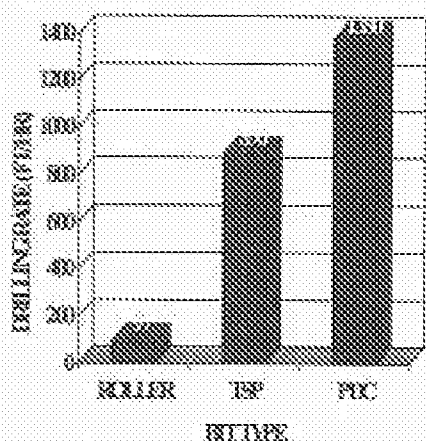
Figure 2.10. DRC Drilling Test Stand.

TABLE 2.1. Test Bits TSP Bit Study

	Bit No.	TSP Shape	TSP Density	TSP Setting	TSP Size mm
Phase I	1	Cube	Heavy	Corner	3 x 3 x 3
	2	Cube	Light	Corner	3 x 3 x 3
	3	Cube	Heavy	Face	3 x 3 x 3
	4	Cube	Light	Face	3 x 3 x 3
	5	Cube	Heavy	Corner	5 x 5 x 5
	6	Cube	Light	Corner	5 x 5 x 5
Phase II	7	PDC	Light	N/A	13 mm
	8	Roller Tooth	N/A	N/A	N/A
	9	Roller Carbide	N/A	N/A	N/A
	10	Cube	Heavy	Corner	5 x 5 x 5
	11	Rectangular	Heavy	Corner	7 x 7 x 5
	12	Hexagonal	Heavy	Corner	3 x 3 x 2.5
	13	Round	Heavy	Face	5 x 5 x 5

These laboratory tests showed that PDC and TSP bits operating at motor speeds of 300 rpm drilled at rates of 1380 and 890 ft/hr (421 and 271 m/hr), respectively, compared to 97 ft/hr (30 m/hr) for roller bits operating at 100 rpm (Figure 2.11). Although the PDC bits drilled faster than TSP bits, PDC bits are not as well suited for use on high-power motors because of thermal limitations of these cutters.

The tests also showed that large TSP cutters (5mm x 5mm x 5mm) drill very fast and eliminated cutter breakage - a problem encountered on earlier tests with smaller dimension cutters (3mmx3mm x 3mm) (Figure 2.12).



Bit Diameter	3 in.
Bit Weight	7,000 lbs.
Bit Pressure	200 psi
Rotary Speed	0-800 rpm
Rock	Leuders Limestone
Flow Rate	60 gpm
Drilling Fluid	Water

Figure 2.11. Effect Of Bit Type On Drilling Rate (Leuders Limestone).

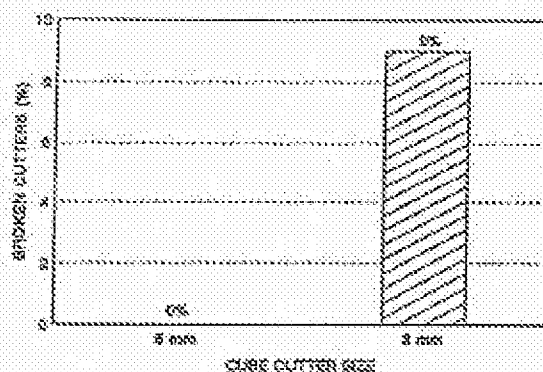


Figure 2.12. Effect of Cutter Breakage (Leuders Limestone)

Based on the above results, MEI selected the four large TSP cutters shown in Figure 2.13 (dimensions in millimeters) for testing in Phase II.

To our knowledge, the 7mm x7mm x5 mm *rectangular* cutter is the largest TSP cutter ever tested in a drill bit. Early TSP bits used 2-mm cube cutters that were much smaller than the 8 mm and 13 mm round PDC cutters commonly used on oil-field bits. The large TSP cutters being tested approach the size of PDC cutters as shown in Figure 2.14.

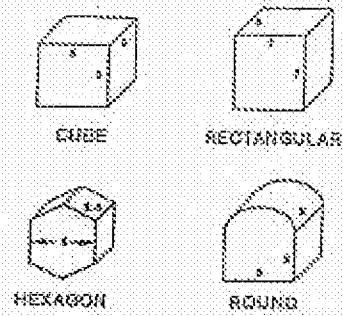


Figure 2.13. TSP Cutter Tested.

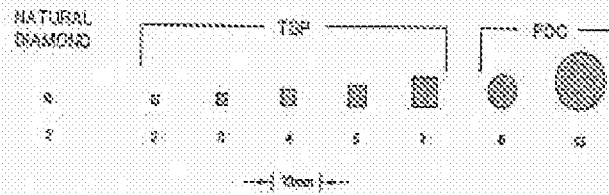


Figure 2.14. Diamond Sizes.

The four large TSP cutter designs shown in **Figure 2.13** were incorporated into 7.6 cm (3-in.) diameter test bits (**Figure 2.15**). These test bits were tested on a 2 $\frac{1}{4}$ -in. SlimDrill motor using the Drilling Research Center (DRC) motor drilling test stand shown in **Figure 2.16**.

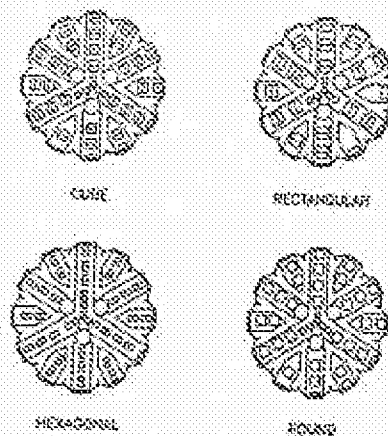


Figure 2.15. TSP Test Bits.

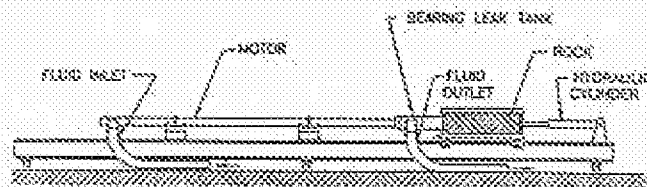


Figure 2.16. DRC Motor Drilling Test Stand.

At 70 gpm (265 l/min), the 2 $\frac{1}{2}$ -in. motor delivered 56 hp at 2340 rpm. This is an overpowered condition for the 2 $\frac{1}{2}$ -in motor.

The experimental TSP bits drilled at maximum rates of 200 to 550 ft/hr (61 to 168 m/hr) as shown in Figure 2.17.

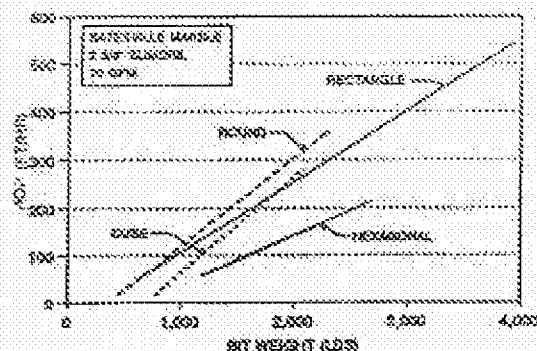


Figure 2.17. Rop vs. Bit Weight For TSP Bits.

The rectangular cutter bit drilled the fastest [550 ft/hr (168 m/hr)], due to the large cutter size. The round cutter bit drilled at rates up to 350 ft/hr (107 m/hr), showing that round cutters also have significant potential. The round cutters eliminate sharp edges and corners that earlier tests showed were initiation points for failures.

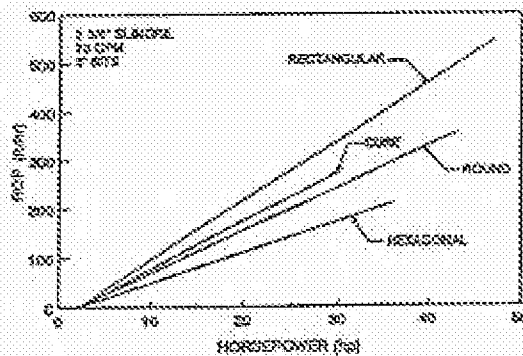


Figure 2.18. Drilling Rate vs. Power.

Drilling rates of the TSP bits increased linearly with motor power output, showing that higher power motors are highly beneficial (Figure 2.18).

At the higher power levels (20 to 45 hp), the TSP bits drilled at rates of 200 to 550 ft/hr (61 to 168 m/hr) in Batesville marble (uniaxial compression strength = 15,000 psi). Field drilling rates in this type of rock would typically be about 50 to 100 ft/hr (15 to 30 m/hr) with roller bits operating at 80 to 120 rpm. These tests show that high-power bits can be manufactured using TSP cutters and matrix style bit bodies.

2.3 BIT CLEANING TESTS

There are two fundamental elements to drilling. The rock must first be broken and then flushed from the hole with the drilling fluid (Figure 2.19).

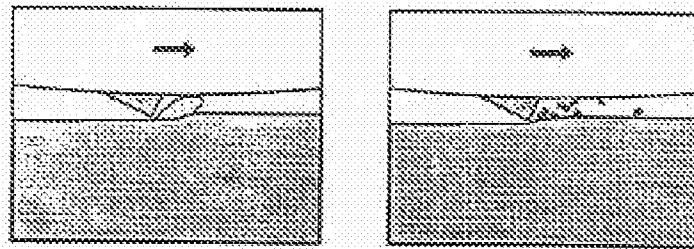


Figure 2.19. Two Elements of Drilling

Conventional diamond bits have small fluid passages for cleaning, thus restricting the free flow of cuttings. If cutters are set up on blades, there is more area for the drilling fluid and cuttings to flow out from under the bit (Figure 2.20).

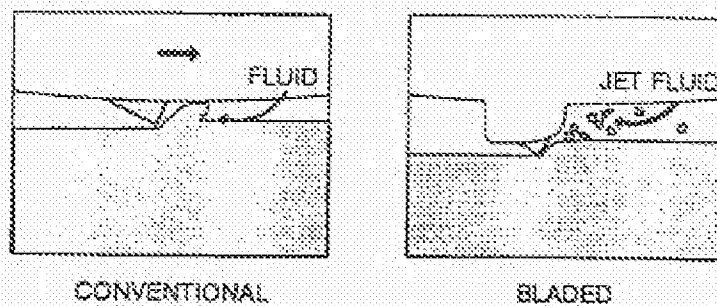
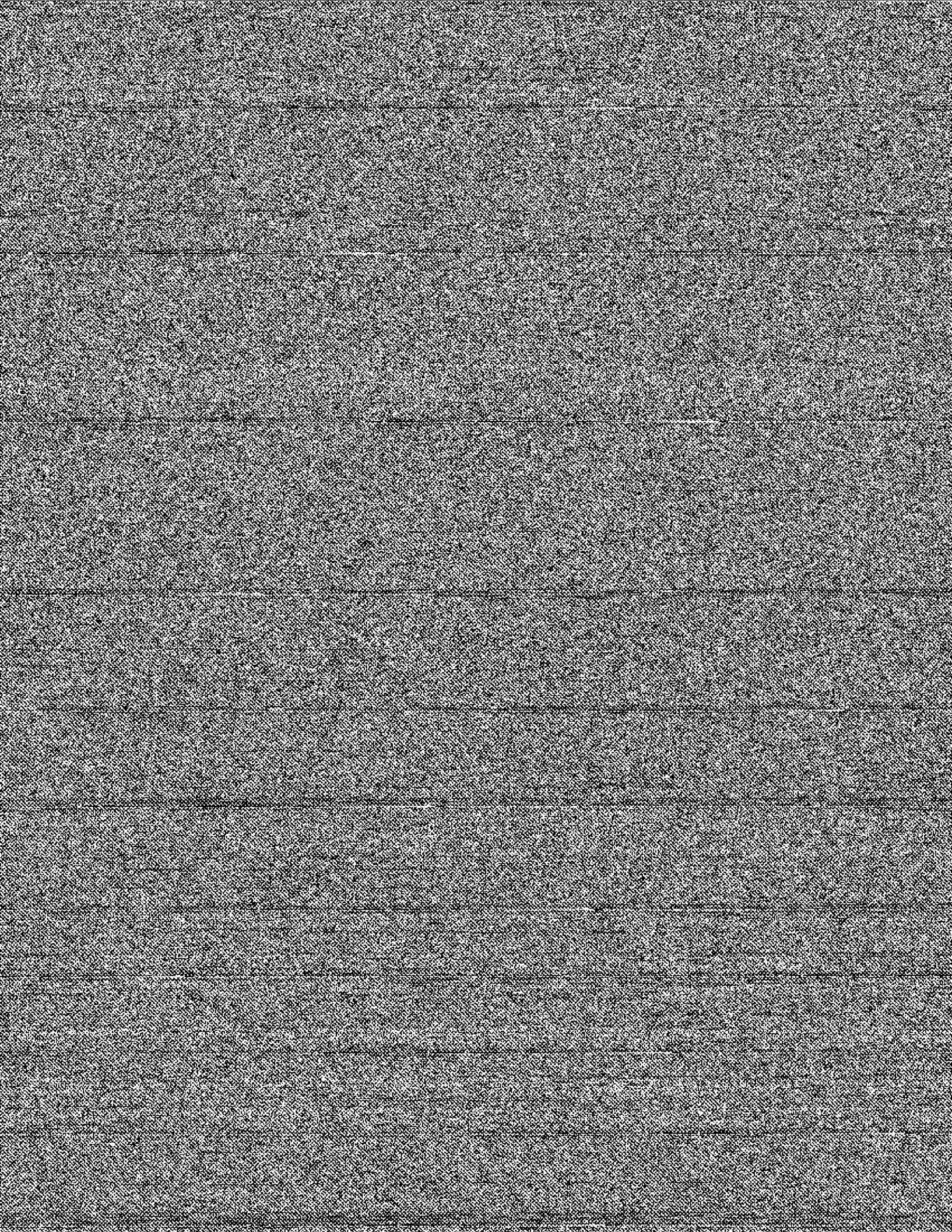


Figure 2.20. Conventional and Bladed Bit Designs.

Bits with enhanced cleaning designs are shown in Figure 2.21 and 2.22. Figure 2.21 is a bit with side rakes on the cutters to help push the cuttings away from the center of the bit to the annulus. Figure 2.22 shows a bit set with the cutters on blades and fluid nozzles so hydraulic horsepower on the bit can be better controlled.



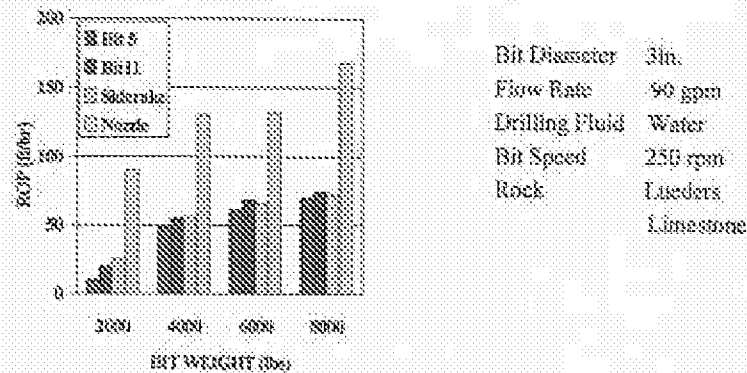


Figure 2.23. Improved Cleaning Bit Test Results

The major bit manufacturers are now making PDC bits using new smaller 8-mm cutters. These new smaller cutters are possible now because the brazed joint between the diamond compact and the carbide stud that is mounted into the bit has been improved. The new brazes have higher strengths (100 to 150 Ksi shear) requiring less braze area to hold at drilling loads. The 8-mm PDCs allow bit designs in smaller sizes with more redundant cutters. This reduces the work and wear on individual cutters, making them last longer. These new PDC bits are also candidates for use on the DOE higher power motors in soft to medium hard formations. TSP cutters will still perform better in harder formations where increased heat from the drilling process can damage the PDC material.

2.4 TSP Bit Field Test Results

Six field tests were conducted using large cutter TSP bits. These tests are listed in the Table 2.2, below, and a discussion of each test follows.

Table 2.2. TSP Bit Field Tests

Test No.	Bit Size	Cutter Size (mm)	Location
1	7-7/8	5x5x5	Wyoming
2	5-1/2	5 round	California
3	4-1/2	5 round	Mississippi
4	4-1/2	5 round	Mississippi
5	5-7/8	7x7x5	East Texas
6	5-7/8	7x7x5	East Texas

Test 1. In the first test the drilling contractor was typically drilling the wells using two bits. In the upper section of the hole a PDC bit was used to drill soft shales at rates of 70 to 100 ft/hr, down to the cap rock, of the Mesa Verde formation, at approximately 6,000 to 7,000 ft (Figure 2.24). At this point the PDC bit would be pulled and replaced with a roller bit, because past experience had shown that drilling into the cap rock with the PDC bit would result in total failure of the cutters. Roller bits typically drilled this section at 10 to 30 ft/hr. The contractor wanted to make the entire run with a single bit. The production in this area is from sandstone layers in the Mesa Verde formation. The sandstone layers are separated by shale, however it is the sandstone that damages the PDC bit.

A 7-7/8 in. large cutter TSP bit was manufactured for this test to see if the TSP cutters could drill the hard abrasive sandstone in the Mesa Verde formation. The bit used 5 mm cube TSP cutters sharp set. This bit running on at 110 rpm on a Sperry Sun multilobe motor and a rotary table speed of 60 rpm drilled the hard sandstone cap rock (6904' to 6920') at 18 ft/hr. This is a good rate, however when the bit entered the shale below the cap the penetration rate decreased to 8.25 ft/hr and the bit was pulled. The bit did not drill the shale well because the small TSP cutters allowed the bit to ball up. This test showed that TSPs can drill hard abrasive formations, but in a typical diamond bit configuration the TSPs can not clean sticky formations. A new mounting method is needed to increase the exposer and open space between the bit and formation so that shale and other sticky formations can be drilled.

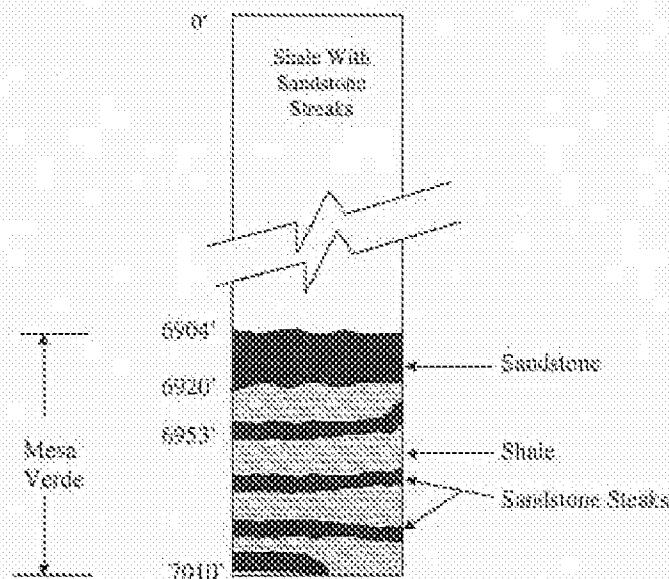


Figure 2.24. Wyoming Test Well Geology

Test 2. The second test was in hard abrasive sandstone in a horizontal well in California. PDC bits could not drill the formation because the sandstone caused excessive wear of the cutters. Prior to running TSP bits, natural diamond bits were used but these too suffered from slow penetration rates and excessive wear. The TSP bit increased

maximum drilling rates from 4.9 fph to 11.5 fph a 234% improvement. The average drilling rate increased from 3.0 fph to 4.5 fph a 150% increase. The TSP bottom hole assembly (BHA) with the TSP bit was pulled early due to differential sticking. The bit had minimal wear and was rerun on another well.

Test 3. This test compared large TSPs to small TSPs. The curved section of a horizontal well in Mississippi was drilled with a TSP bit made using 3mm cube cutters sharp set. The bit drilled 223 ft at 5.5 fph through an abrasive sandstone formation, and was completely used up. Concerned with slow penetration rates and high bit wear the operator wanted to try a different bit. A TSP manufactured with 5.3 mm round cutters was prepared for the job. During the BHA change a portion of the hole was lost a section of the curve had to be redrilled. In this section of the well there is a direct comparison between the large and small TSP outer bits. The large cutter bit drilled from 10,441 to 10,561, a total of 120 ft at 7.3 fph. The bit manufactured with 3 mm cutters drilled from 10,721 to 10,544, a distance of 223 ft at 5.8 fph. The bit with large cutters drilled 28% faster through the curved section of the well. The bit went on to drill a total 1215 ft at an average rate of 12.5 fph. This shows that large cutters drill faster and wear less than small cutters.

Test 4. This test consisted of 5 different bits. Four of the five were large cutter TSP bits manufactured using 5 mm cube cutters. The test results are summarized in Table 2.3. The first bit was run on junk so it is not included in calculations for penetration rate. The second bit was manufactured with 3 mm cubes and drilled 32 ft at 1.18 fph. The next 3 bit runs were made with bits using 5 mm round cutters. These bits drilled a total of 461 ft at rates of 2 to 4.67 fph.

Table 2.3 Test 4 Bit Run Summary

Bit Run	Bit S.N.	Type	No. of Runs	Total Footage	Average ROP	Formation	Mud Wt.	Flow	ROP Increase
1	9530	HT-250	1	23	9	Cement	10.5	100	NA
2	NA	HT-23	2	32	1.18	Marine Shale	10.5	100	-
3	9560	HT-250	5	318	2.87	Marine Shale & Tuscaloosa Sand	10.5	100 to 115	2.4
4	9557	HT-250	1	139	4.67	Tuscaloosa Sand	10.5	115	4.0
5	9561	HT-250	1	18	2.89	Tuscaloosa Sand	10.7	107	1.7

Offset data for straight wells in the same formation show that roller bits drill much faster than TSP bits in directional wells. However, the roller bits suffered severe wear and the directional drilling contractor felt that the TSP bits were needed to provide the

directional control to stay in the thin producing formation.

Test 5. This test is the best example of the benefits of large cutter TSP bits. A 5-7/8 in. bit manufactured with the largest (7mm x 7mm x 5 mm) TSP cutters was used to drill in the Bossier formation, a very hard shale in East Texas. Run on rotary this bit drilled 1600 ft at 10 to 12 fph. Replacing two natural diamond bits, this bit drill twice as far as an average diamond bit, and 600 more feet than the maximum (1000 ft) ever drilled by a natural diamond bit. Penetration rates were comparable for both bit types.

Test 6. This bit was identical to the bit used in test 5. However, this run was on a high speed motor. The bit performed well at the beginning of the run, but quickly slowed down, and was pulled after drilling only 400 ft. The bit was severely damaged with many cutters broken. The large cutters even though broken still presented a significant cutting structure so the bit was rerun on rotary in another well. In this well the damaged bit was able to drill an additional 600 ft at 10 fph. The total footage drilled was 1000 ft, equal to the best natural diamond bit run.

This test showed that large cutter TSP bits are very rugged and even damaged can drill long distances at high rates. The fracturing of the cutters during the motor run shows that TSP are very brittle and therefor need smooth running conditions and anti whirl protection. TSP bit designs should enhance the toughness of the cutters to achieve the best results.

Attempts were made to have the operator try this bit on a slow speed motor. However, hot hole conditions caused failures of multi lobe mud motors in previous attempts and the operator was unwilling to try these motors again so no further testing was done. The bits needed to be run on motors for directional control in this formation.

These tests showed that large cutter TSP bits can drill fast and have long life in hard abrasive formations. They also showed that in soft sticky formations the TSP bits tend to ball up, and due to their brittleness they can be fractured easily if exposed to bit whirl or impact loads.

These data prompted a design study to determine a way to get the benefits of PDC style bits and the wear resistance of TSPs. The ideal solution is to have a TSP that looks and mounts just like a PDC. This unfortunately can not be done because the TSP material can not be brazed with sufficient strength for drilling applications. Current research is underway to develop brazing techniques that will work with TSPs, but their commercial availability is still in the future. To overcome this road block the hybrid bit was designed. This bit uses both PDC and TSP cutters and has the attributes of each bit type. The development and field tests of the hybrid bit are described below.

2.5 Hybrid Bit Design

The hybrid bit is designed to capture the drilling qualities of both PDC and TSP bits. It starts out as a bladed PDC bit (Figure 2.25). This configuration allows the bit to drill many soft to medium formations at high rates. It includes four nozzles two replaceable and two fixed. The PDC can be either rotated or replaced to rebuild the bit after it has been run. The matrix body of the bit will resist erosion even from abrasive muds.

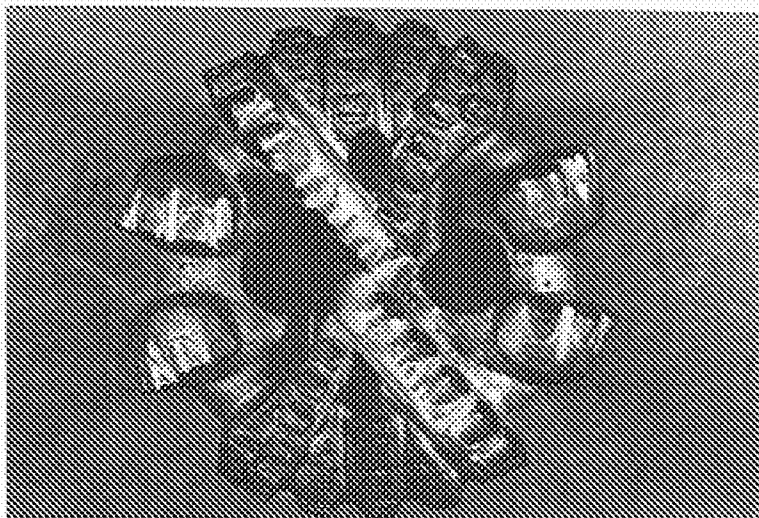


Figure 2.25. Hybrid Bit.

To enhance the bit's ability to drill harder formations, large TSP cutters have been set at the same height and behind the PDC cutters. Since the face of the bit must wear down evenly these TSP cutters protect the PDC cutters from damage (excessive wear).

Similar concepts to this have been used in the past. Natural diamond pads or carbide inserts have been placed behind PDC cutters on other bits to act as shock pads during drilling. The TSP cutters on the hybrid bit not only absorb shock but they also help drill the formation.

The nozzles on the bit are designed to provide cleaning even in sticky formations that may tend to ball the bit. The two adjustable nozzles can be selected to provide the jet impact force necessary to keep the bit face clean in any conditions.

The TSP cutters have been set up on pads. This has the effect of increasing their exposure to the formation for better cleaning and to provide maximum penetration rates.

2.6 Hybrid Bit Field Performances and Commercialization

A hybrid bit was used during the first shake down tests of the high power motor at the Catoosa test site. The bit performed well in many different drilling conditions. Most of the drilling during this first test was not taxing to the hybrid bit. However, one formation known as "The Wall" has a reputation for destroying PDC bits. Typically PDC bits hit this formation and quit drilling when many of the PDC become damaged. The hybrid bit was able to drill 40 ft into the "The Wall". The test was only stopped at this time because test monies had run out, not due to bit or motor failure.

Figure 2.26 shows the hybrid bit used in the first test. The PDC cutters show considerable wear, testimony to the hardness and abrasiveness of "The Wall". However, the bit was still in good condition and could have continued drilling. The TSP cutters on the bit showed minimal wear. This bit was rebuilt after the test and used again.



Figure 2.26. Hybrid Bit After Drilling "The Wall"

The hybrid bit has been successfully used in many commercial applications. Table 2.4 is a summary of these runs. Over 17,000 feet of hole has been drilled using the hybrid bit.

Table 2.4 Commercial Hybrid Bit Runs

Size	Formation	Footage	ROP
6-1/8	Sprayberry	897	35.5
6-1/8	Sprayberry	2275	38.4
6-1/8	Sprayberry	1830	22.5
6-1/8	Devonian Dolomite	1784	17.6
4-3/4	Red River Dolomite	1509	26
4-3/4	Cherry Canyon	1847	21.4
4-3/4	ABD Dolomite	366	8.5
4-3/4	Cherry Canyon	1331	29
4-3/4	Sprayberry	1511	58.5
4-3/4	Sand, Shale Limestone	830	50.8
4-3/4	Cherry Canyon	1557	15.2
4-3/4	Desert Creek	2098	15.3
Total		17,815	21.97

These data show that the hybrid bit can drill rapidly and have long life in a variety of formations. Three case histories given below show how the hybrid bit compares to other bit types.

Case 1

San Juan County, Utah; a 4-3/4 in. hybrid bit drill 2098 ft in hard limestone and shale formations in 137.25 hours for an average penetration rate of 15.28 fph. The bit drilled 2 horizontal legs and was only 1/3 worn. **Figure 2.27** shows the footage drilled for the hybrid bit and bits in two offset wells.

The hybrid bit was able to replace two rock bits and eliminate a trip and risk of lost cones in the hole. The bit was suitable for additional use and was more controllable in directional drilling making it much better and more cost effective than the roller bits in this application.

Footage Dilled

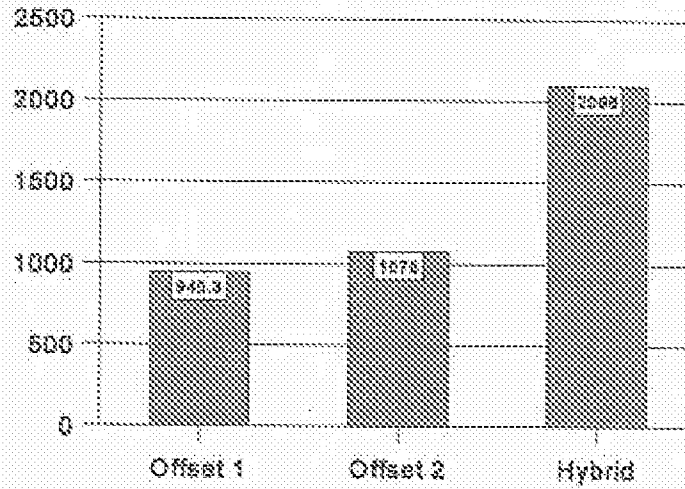


Figure 2.27. Comparison To Offset Wells.

Case 2

Borden County, Texas: A 6-1/8 in. hybrid bit was used to drill 3 horizontal legs in the Sprayberry formation. A total of 5002 ft were drilled in the three wells in 166.1 hours for an average penetration rate of 30.1 fph. Figures 2.28 and 2.29 show a comparison for rate of penetration and footage drilled between the hybrid bit and offset well data.

Average ROP

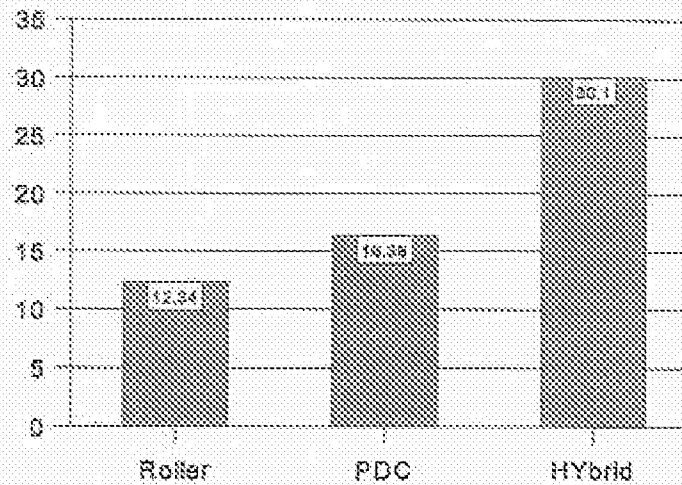


Figure 2.28. Comparison of ROP To Offset Wells

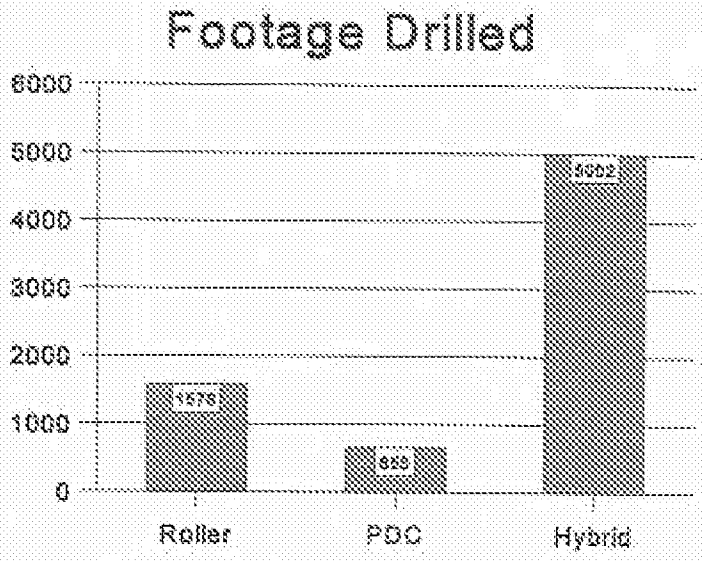


Figure 2.29. Comparison of Footage Drilled to Offset Wells.

The bit was able to replace several rock bits and was repairable and reusable at the conclusion of the run. It had higher penetration rates and longer life than the other bits. It eliminated several trips and was very controllable in directional drilling.

Case 3

Winkler County, Texas: A 4-3/4 in hybrid bit drilled 1331 ft of Cherry Canyon Sand in 45.75 hours at an average penetration rate of 29.09 fph. Figure 2.30 is a comparison

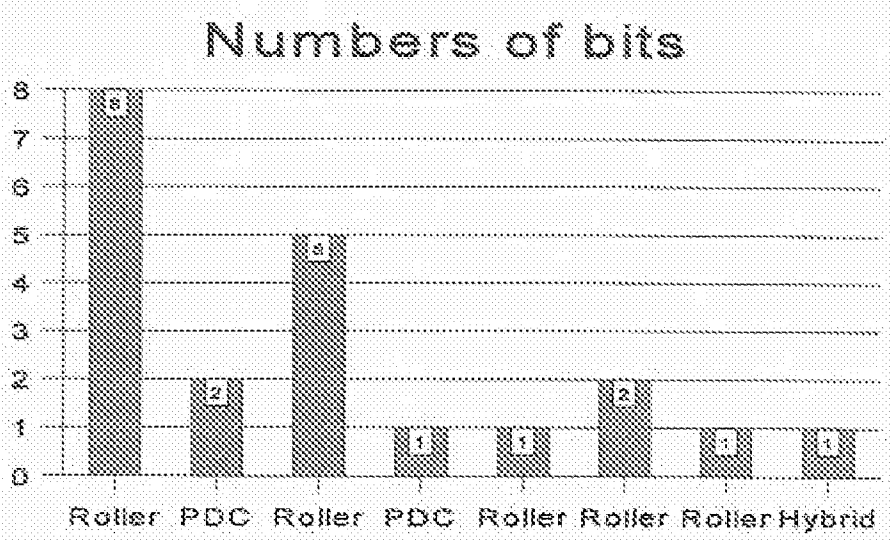


Figure 2.30. Comparison Of Numbers Of Bits.

of the number of bits used to drill offset wells. These data show that the hybrid bit replaced several roller bits and eliminated many trips.

Figure 2.31 shows a comparison of the average footage drilled for each bit. The hybrid was able to drill further than all but one PDC bit. It eliminated several trips and replaced many roller bits.

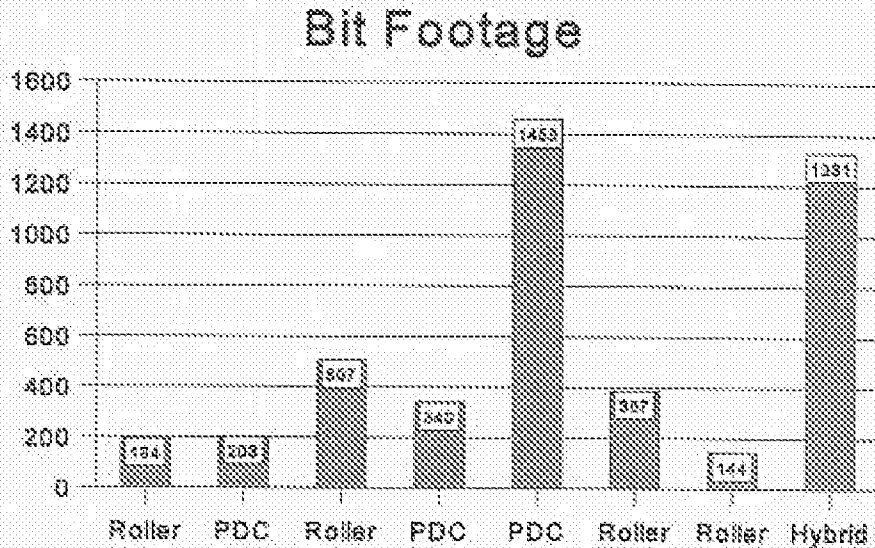


Figure 2.31. Bit Footage Drilled.

The hybrid bit was able to drill the formation faster than the other bits (Figure 2.32).

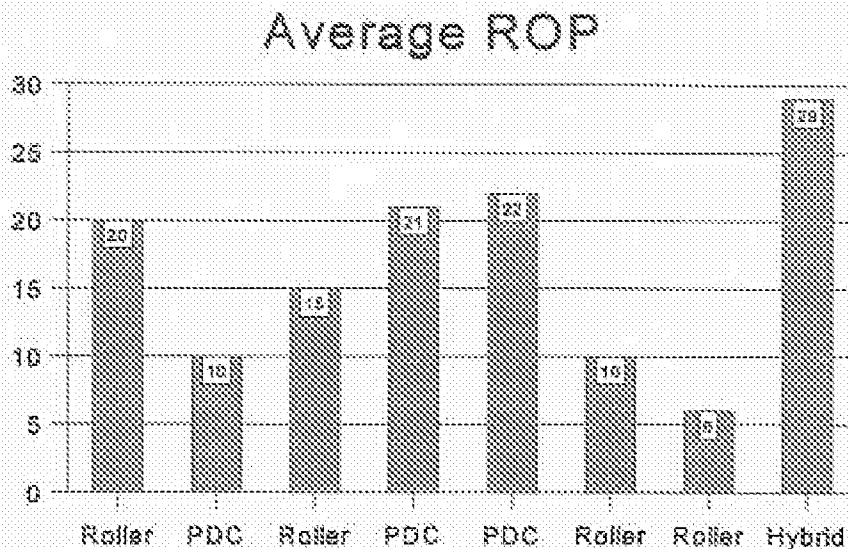


Figure 2.32. Average Bit ROP

The Hybrid bit was also able to reduce vibrations in this application. This saved costs by preventing damage to the steering tools and eliminating trips to replace the broken steering tools. This is a significant finding since these costs can be very high.

The Hybrid bit as shown in these case histories is an excellent design that combines many of the attributes of PDC and TSP bits into a single bit. The bit delivers high penetration rates while being able to drill through hard or abrasive formations or stringers. It reduces bit vibrations is very controllable making it an excellent bit for straight hole and directional jobs. The bits characteristics make a good selection when running under difficult conditions such as when used with high power or extended length motors.

Commercial Status

The hybrid bit was produced commercially by Phoenix Energy Systems. When Phoenix Energy was purchased by National Oil Well the bit division, Walker McDonald, was sold to Varel Manufacturing Co. They do not produce diamond bits so the hybrid is not currently available. MEI is trying to form a new bit company can manufacture the hybrid bit or transfer the technology to an existing bit company that can add the hybrid design to their current line.

3. HIGH POWER SLIM-HOLE MOTOR

3.1 Basic Motor Design

Down hole mud motors consist of three major subassemblies. These are the power section, flex coupling and the bearing pack (Figure 3.1). The power section converts a portion of the drilling fluid's hydraulic energy (in the form of pressure and flow rate) into mechanical energy (rotary speed and torque). The power section is based on pump designs developed by the French scientist Moineau. It is comprised of a steel rotor that turns inside of a rubber lined stator. As the rotor turns inside the stator, fluid packets progress from the top of the motor to the bottom. The Moineau power sections rotate eccentrically. The function of the flex coupling is to convert the eccentric rotation to pure rotation and couple this motion to the drive shaft/bearing pack assembly. The bearing packs absorb loads such as the hydraulic down thrust produced by the pressure differential across the tool and the loads generated at the bit while drilling.

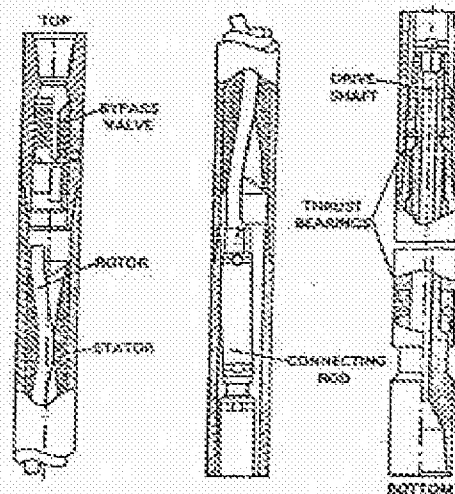


Figure 3.1. Basic Moineau Motor Design.

To produce a high-power slim-hole motor each of the major subassemblies must be improved. Specifically, the power sections must be modified to produce more power while the flex coupling and bearing pack must be redesigned to handle the increased power reliably.

3.2 Power Section Modifications

As previously stated, Moineau motor power sections convert hydraulic power to mechanical power. The hydraulic power is derived from the drilling fluid pumped down the

drill string and is proportional to the quantity of fluid being pumped and the pressure drop across the tool. Mathematically, hydraulic horsepower is

$$HP = \frac{P \times Q}{K} \tag{3.1}$$

where P is the pressure drop, Q is the flow rate and K is a constant. The mechanical power, represented by rotary motion is

$$HP = \frac{T \times N}{K} \tag{3.2}$$

where T is the torque, N is the rotary speed and K is a constant. These two equations show that the speed of rotation is proportional to the mud flow rate and that the torque is proportional to the pressure drop in the drilling mud. To increase the power output of a motor it is necessary to increase rotary speed and/or torque. This must be accompanied by an increase in the flow rate and/or the pressure drop.

$$\begin{aligned} N &\propto Q \\ T &\propto P \end{aligned} \tag{3.3}$$

There are many ways to alter the torque and speed of a Moineau motor. The rotor and stator cross sections are contoured. The stator contours have one more "lobe" than the rotor, as shown in Figure 3.2. As the number of lobes in a motor increases, the motor torque increases and the rotary speed decreases.

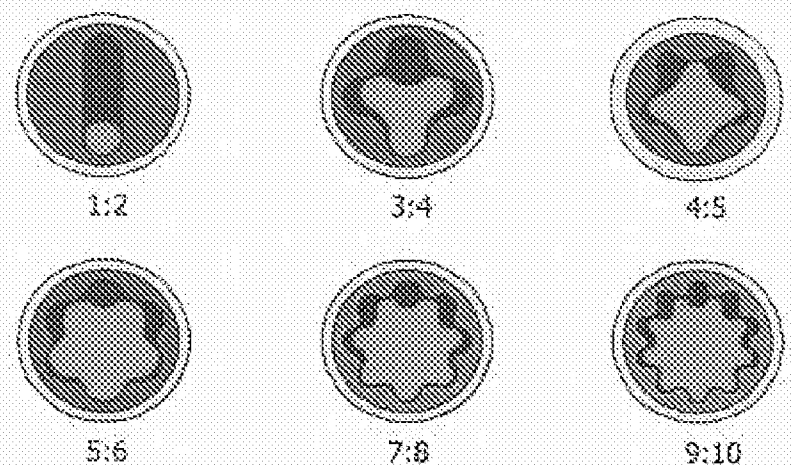
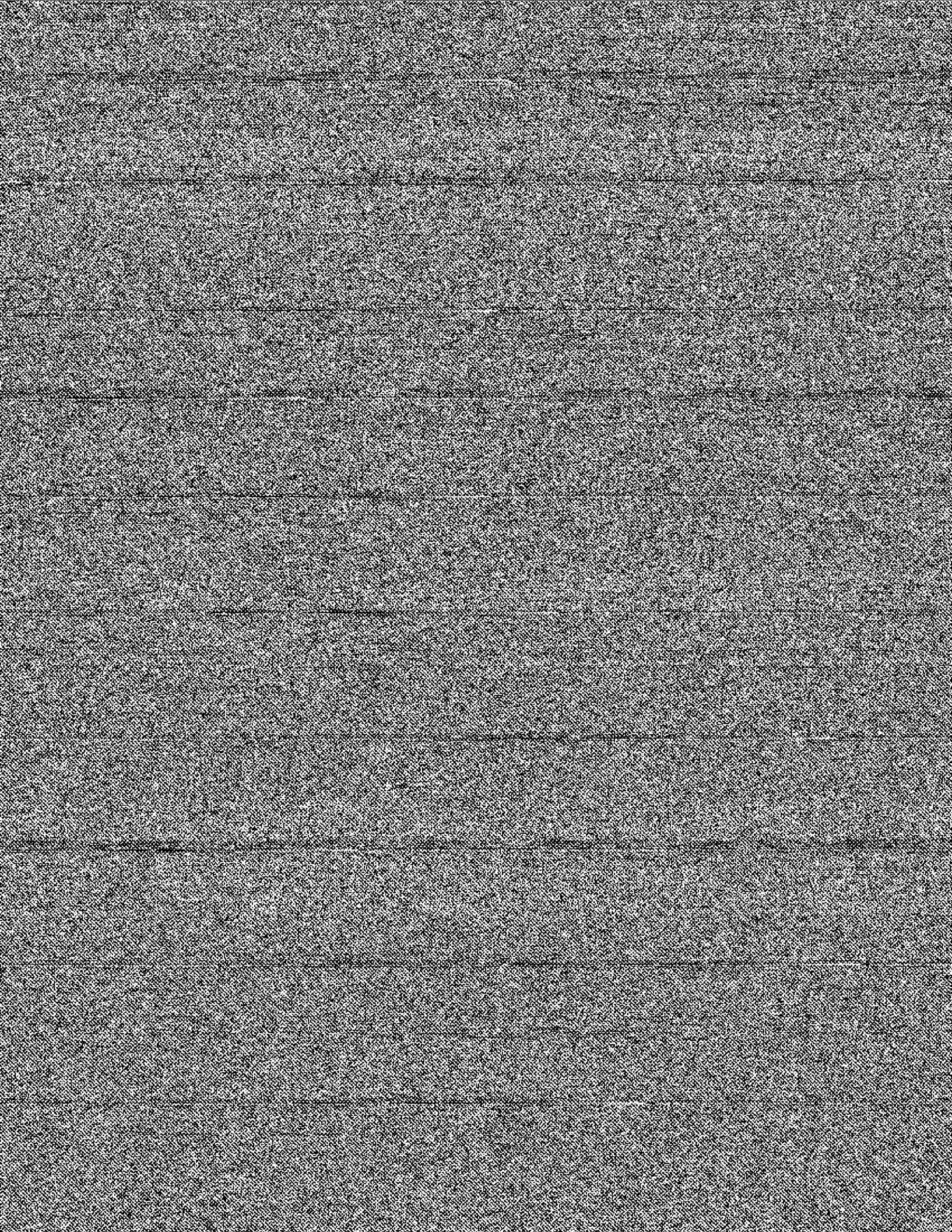


Figure 3.2. Different Lobe Configurations



can be accomplished by doubling the number of stages in a tool and thus doubling the pressure drop across the tool. In **Figure 3.4**, doubling the pressure drop from 900 psi to 1800 psi increases the torque from 75 to 150 ft-lbs.

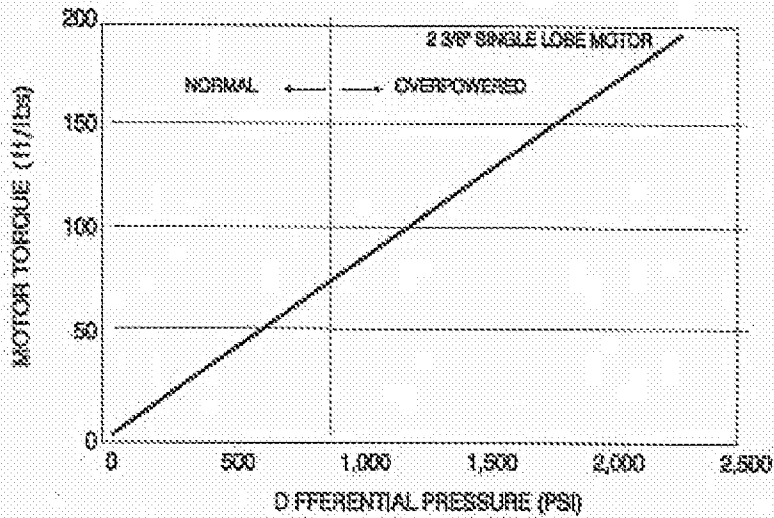


Figure 3.4. Torque for Normal And Overpowered Conditions.

Increasing the flow rate through the motor increases the rotary speed. This increases the power. **Figure 3.5** shows the speed vs. flow for a single lobe motor run in normal and over powered conditions, as the speed increases the power output increases linearly. However, this causes the rubber to flex more due to the increased speed. This flexing caused heat build up in the rubber that can eventually cause damage and failure. Therefore, increasing the flow rate through the motor is not a very good way to increase motor power.

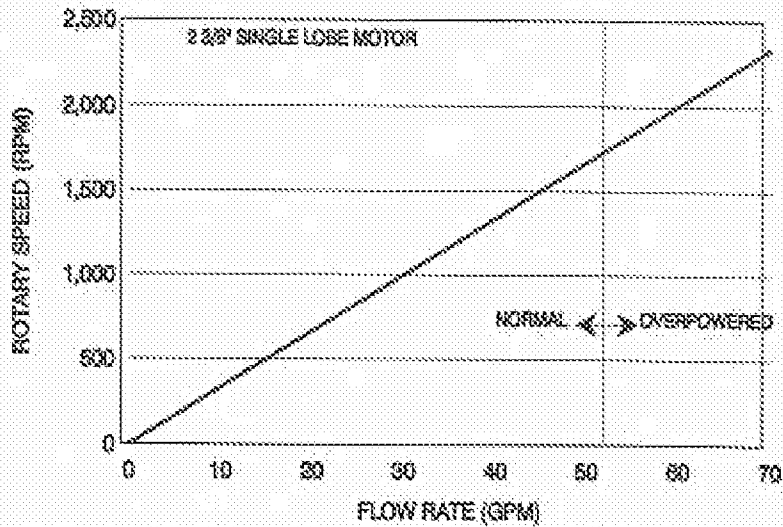


Figure 3.5. Motor Speed As A Function Of Flow Rate.

The high-power slim-hole DOE power section was manufactured from two R & M Energy System's 4:5 multilobe stators. These stators are welded together in a proprietary process that achieves a secure joint between the power sections without damaging the rubber in the stator. Figure 3.6 shows the standard performance curves for this power section while Table 3.1 lists the specifications.

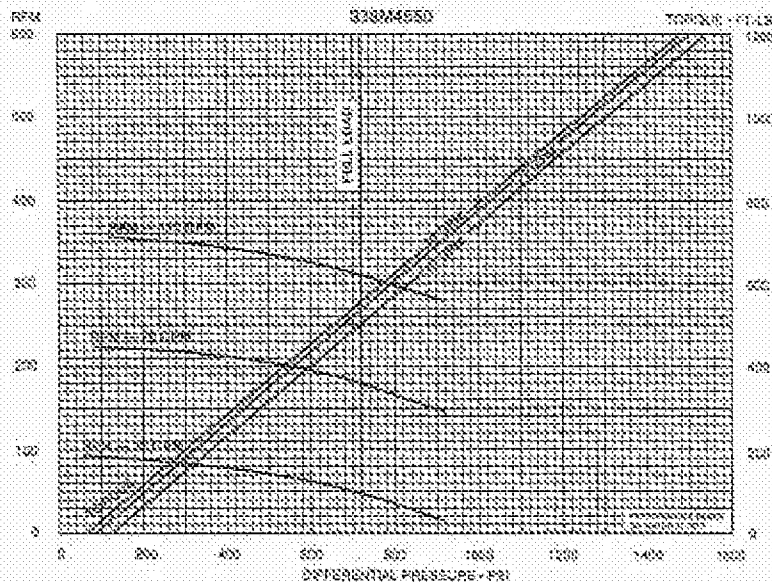


Figure 3.6. R & M 3-3/8 In. Performance Curves.

Table 3.1. Moyno™ Motor Specifications

ROTOR SPECIFICATIONS & DIMENSIONS		STATOR SPECIFICATIONS & DIMENSIONS	
Number of Lobes	4	Number of Lobes	5
Number of Stages	5.0	Nominal Tube OD	3.38 in.
Contour Length	107.0 in.	Nominal Tube ID	2.75 in.
Overall Length	111.0 in.	Overall Length	118.0 in.
Contour OD	1.940 in.	Length from End of	6.0 in. Each End
Head OD	1.75 in.	Contour OD	2.260 in.
Thread Form	1 $\frac{3}{4}$ -6 Stub Acme	Inside Diameter	1.600 in.
Eccentricity	0.165 in.	Material	4142 Heat Treated Hot Finished
Material	4140 Heat Treated Bar		Tubing with Nitride Insert
Weight	64 lbs	Weight	115 lbs

A special rotor was machined by R & M Energy Systems for use in the high-power motor. Its length is the maximum that R & M can manufacture on their rotor cutting machine. If necessary, two conventional rotors can be welded together to form a long rotor. Manufacturing limitations did not dictate maximum rotor length. The objective was to double the length so the power could be doubled.

Welded rotors work as well as single-piece rotors if care is taken to get a proper weld. The most significant problem is phasing the rotors correctly and then machining the weld to the final rotor form. Much of this work must be done by hand. Figure 3.7 shows the double length rotor and stator along with a conventional stator.

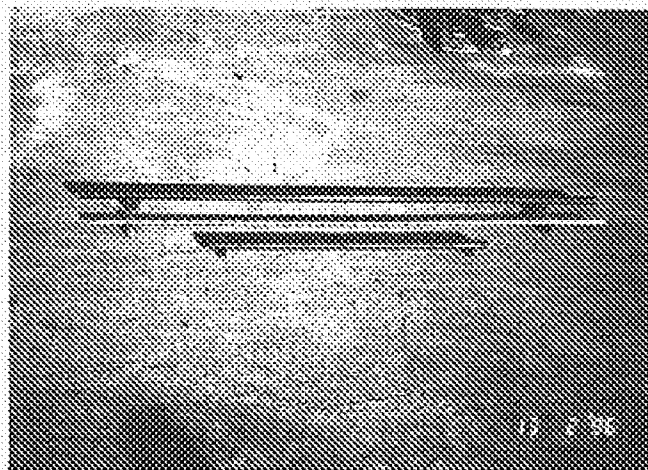


Figure 3.7. 3-3/8 In. R & M rotor and stators

3.3 Flex Coupling Design

The flex coupling is required because the power section does not rotate concentrically. The rotor orbits about a center offset from the stator's center line (Figure 3.8). The distance between the two centers is called the motor's eccentricity.

Moineau Principles

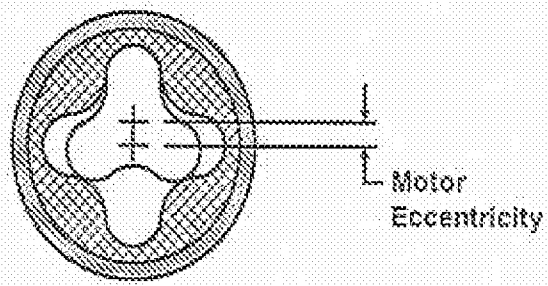


Figure 3.8. Multilobe Cross Section Showing Eccentricity

The flex coupling has always been a weak component in Moineau oil-field motors. The standard SlimDril motor uses a flame cut flex coupling. The flame-cutting operation damages the heat treatment of the steel, reducing its strength. To avoid this problem, a high-pressure water-jet cutting process (30,000 psi) was tried for the DOE motor. Some success has been achieved with this process in larger flex couplings, but the small size of the 3/8-in. coupling led to problems that could not be overcome. The small diameter of this coupling allowed the water jet to pass across the inside of the coupling and damage the inside diameter opposite the cut as shown in Figure 3.9.

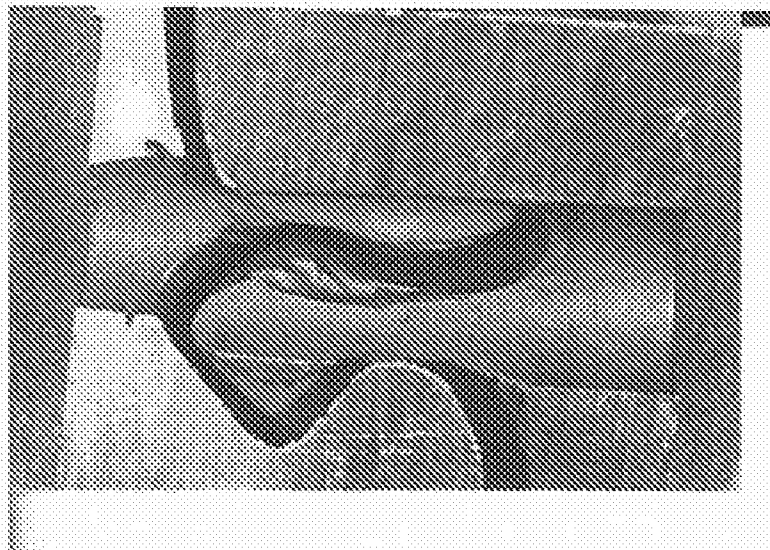


Figure 3.9. High-Pressure Jet Damage

Several different methods of cutting the flex coupling with the water jet were tested. These included varying pressure and placing a sacrificial bar inside the coupling to absorb the energy of the water jet before it could cut the opposite side of the coupling. However, cutting could not be accomplished without damage. Therefore, a conventional coupling was manufactured. The flame cut coupling was designed to maximize diameter while still allowing a bend in the motor of 2 to 2.5 degrees. Maximizing coupling diameter also maximizes coupling strength. This flex coupling failed under the high torques developed by the DOE motor during laboratory testing on the DRC dynamometer test stand (Figure 3.10). More details on these tests are presented later in this report.

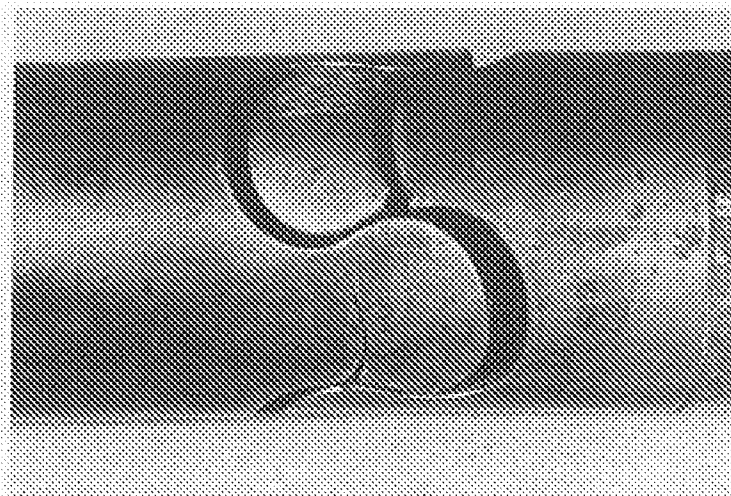


Figure 3.10. Broken Flex Coupling.

As an alternate to the conventional flex coupling, a titanium flex shaft was designed and fabricated that uses natural elasticity to accommodate the Moineau motor eccentricity. Figure 3.11 is a drawing of a flex shaft.

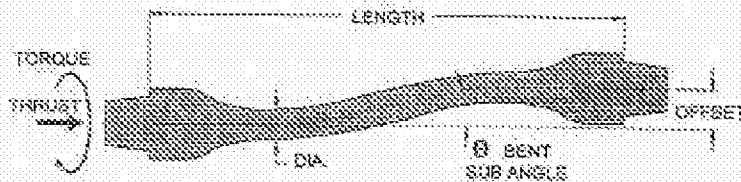


Figure 3.11. Flex Shaft

The stress in a flex shaft is a function of the material properties, length, diameter, and offset. A low modulus material like titanium or beryllium copper minimizes length. The flex shaft designed for the DOE motor is made with titanium, which has a modulus of 15×10^6 psi—half that of steel. Flex shafts have been used in Moineau pumps, but the increased length has made them unpopular for mud motors. Since the high-power motor is already double length, the slight increase in length for a flex shaft is insignificant.

R & M Energy Systems ran a finite element analysis to help design the DOE flex shaft. The flex shaft specifications (Table 3.2) were derived from data supplied in the R & M power section specification sheet, extrapolated data, and calculations.

TABLE 3.2. Flex Shaft Specifications

Motor Size:	3½, 4/5, High-Power Moineau
Eccentricity	0.165 in.
Max Torque	1500 ft-lbs
Max Down Thrust	5900 lbs
Coupling Length	
Min:	17.125 in.
Max:	36 in.
Coupling Diameter:	
OD:	2 in.
ID:	As required
Material:	Titanium, Beryllium Copper, Aluminum
Minimum Life:	1000 hrs.
Max Motor Bend:	2½°
Bit Sizes:	3½ to 6½ in.

The flex shaft must accommodate offsets from two sources: 1) rotor eccentricity and the 2) bent housing. The eccentricity is established by the power section design and is given on the R & M data sheet. The maximum bent housing the motor can use must be determined by layout drawings that show the clearance between the flex shaft and the flex shaft housing. **Figure 3.12 (A & B)** show a typical layout of this section.

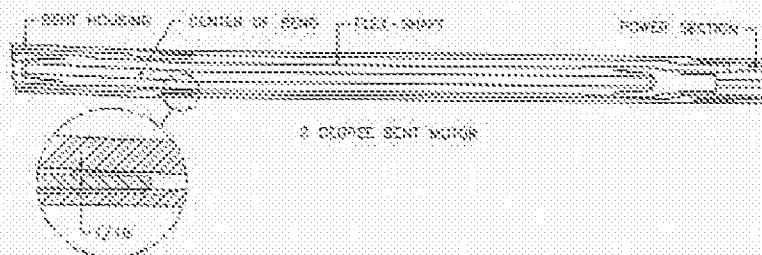


Figure 3.12A. Clearance with Bent Sub.

The designer must use judgement in determining the maximum bent sub that can

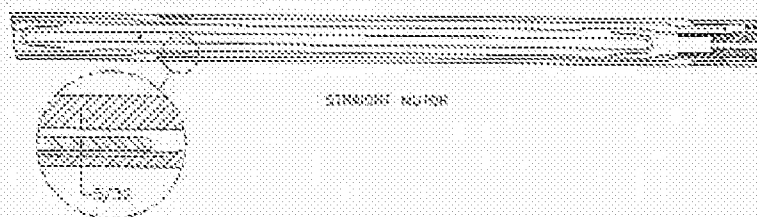


Figure 3.12B. Clearance in straight Motor.

be used. As the bend increases, the housing wall thickness must be decreased or the flex shaft diameter decreased. The optimum point is found through experience. The DOE high-power motor can support a 2.5" bent housing before the flex shaft begins to interfere with the housing.

The maximum torque for the flex shaft was calculated by doubling the operating torque listed in the R & M data for a standard motor and applying a safety factor of 1.5. In a similar manner, the down thrust was calculated by doubling the listed operating pressure drop and applying a safety factor of 1.4. This particular safety factor for down thrust was selected because it specified a load that could be safely carried by two thrust bearings.

The flex shaft length was selected to be equal to the conventional flex coupling length, up to a maximum of 36 in. Lengths over 36 in. were not considered due to concern that the coupling would become unstable and "whip" as it rotated. The final length was selected so that stress in the shaft will be kept below the fatigue endurance limit. The

maximum shaft OD was selected in the layout drawing shown in Figure 3.12 (A & B).

A flex shaft life of 1000 hours was selected so that it could replace 10 conventional flex couplings lasting 100 hrs each. The 100 hr life is a typical for a conventional coupling run in typical, but not severe, conditions.

Under this criteria, the flex shaft cost can be 10 times as much as the conventional coupling cost and still be at break-even. Table 3.3 gives the results of R & M's analysis while Table 3.4 shows results from an MEI analytical design program. Both analyses yielded similar results for the dimensions of the flex shaft. The stresses are below the 40,000 psi endurance limit for titanium. This means the shaft should not fatigue, regardless of the number of cycles. If these calculations prove to be correct, and there is no reason to believe otherwise, the life of the flex shaft will be determined by something other than fatigue. The shaft theoretically has infinite life with no maintenance required.

TABLE 3.3. Moyno Oil-Field Products Flex-Shaft Calculations

SHAFT LENGTH (INCH)	O.D (INCH)	I.D. (INCH)	MATERIAL	MAX STRESS (PSI)	VON MISES STRESS
30	1.5	0	STEEL	119,000	110,304
30	1.5	0.75	STEEL	130,000	115,000
30	1.5	0	TITANIUM	64,000	62,424
30	1.5	0.75	TITANIUM	72,000	62,114
36	1.5	0.75	STEEL	84,000	83,117
36	1.5	0.75	TITANIUM	48,000	46,039

TABLE 3.4. MEI Titanium Flex-Shaft Calculations

Flex Shaft Calculation		
Eccentricity	0.165 in.	
Shaft OD	2 in.	
Shaft ID	0 in.	
Motor bend	2.5 deg.	
Titanium (E=17500000 psi)		
Shaft length	Bending stress (psi)	
(in.)	Straight motor	Motor bend
17	59824	104253
25	27586	57438
36	13244	23447
Copper (E=15000000 psi)		
Shaft length	Bending stress (psi)	
(in.)	Straight motor	Motor bend
17	52160	89277
25	23636	49118
36	11334	26517
Aluminum (E=11000000 psi)		
Shaft length	Bending stress (psi)	
(in.)	Straight motor	Motor bend
17	37558	65311
25	17300	35802
36	8278	20605

During the first run of the high-power motor the lower sections of the stator was damaged. It was determined that the damage was caused because the flex shaft was too stiff. Further analysis was conducted on the shaft and the titanium material. It was determined that the endurance limit on the titanium selected could be increased from 40,000 psi to 60,000 psi. This allow the shaft diameter to be reduced to 1.5 in. while retaining the same infinite cycle fatigue life. This change was made and the motor with the new shaft retested. The smaller shaft worked and no subsequent damage to the stator has occurred.

3.4 Bearing Pack Design

The bearing pack reacts all internally and externally applied motor loads. There are

two types of bearing packs in use: 1) oil-filled sealed bearing packs and 2) mud-lubricated leaking bearing packs. Sealed bearing packs must be pressure compensated to respond to oil volume increases as they become heated. They are considerably more expensive than mud lubricated packs and have a very short life in the event the seals fall during operation.

Mud lubricated bearing packs are designed to divert a portion (approximately 10%) of the drilling fluid volume through the pack to cool and lubricate the bearings. The remainder of the fluid is routed through the center of the bearing pack shaft directly to the drill bit. Figure 3.13 shows a schematic of a mud lubricated pack. A flow restrictor is used to set the amount of flow across the bearings and to compensate for the pressure drop across the drill bit.

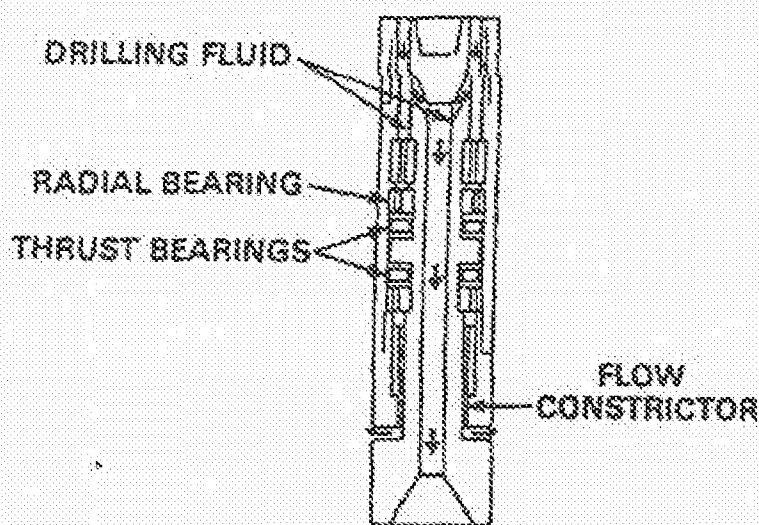


Figure 3.13 Leaking Bearing Pack

The thrust and radial bearings in mud lubricated bearing packs are expendable items and are often used up after a single run. There are two sources of thrust loads in a Moineau motor. The first is a result of the pressure drop across the power section, which pushes down on the rotor. Thrust bearings must absorb this down thrust load to keep the rotor in place. The other thrust loading comes from the bit load. This force pushes up on the bearing pack shaft counteracting the down thrust from the rotor. Bearings that absorb the down thrust are sometimes called "off bottom" bearings since these have maximum load when the bit is off bottom. When the bit weight exceeds the rotor down thrust then the "on bottom" bearings become loaded. Depending on the type of bearing pack and the bearings used, stacked bearings are often needed because of the high loads. When stacked bearings are used a load distribution system is needed to divide the load equally between the bearings. Failure of the load distribution system can cause bearings to fail prematurely.

Radial loads to motors come from normal drilling forces, purposeful side loads for directional drilling, and loads transferred through the flex coupling to the bearing pack. In mud lubricated bearing packs the radial bearings are often rubber marine bearings. These work well in the mud environment, but have low load limitations. Two radial bearings are typically used one at the top of the bearing pack and one at the bottom with the thrust bearings sandwiched between.

The small size of components in slim-hole motors make it challenging to develop a long life bearing pack. To handle the increased power, the thrust bearings and the load distribution system were modified to withstand higher thrust loads. Higher thrust loads come from two sources: 1) since the motor has twice the number of stages, the pressure drop and the down thrust are doubled, and 2) the increased torque of the high-power motor allows higher bit weights. In an ideal situation, the down thrust equals the bit thrust and the bearings carry no load. However, in reality, this is rarely achieved and the thrust bearings must carry substantial loads.

The down thrust on the bearing pack can be calculated by multiplying the operating pressure drop across the motor times the projected area of the rotor. This projected area can be calculated from the rotor contour outside diameter listed in **Table 3.1** (1.941 in.). At 1500 psi differential pressure, the down thrust for this DOE high-power motor will be 4400 lbs. This bearing pack has been constructed so that two bearings share the down thrust load and four bearings share the up-thrust or bit loads. If needed, additional bearings can be added to extend tool life.

Rubber radial marine bearings used in the conventional bearing packs have been replaced with metal-on-metal bearings in the high-power motor to increase the radial load capacity and life. The radial bearings are made using a proprietary process where a coating of tungsten carbide is fused to the surface of a steel sleeve. The powdered tungsten carbide is first made into a blanket as shown in **Figure 3.14**.



Figure 3.14. Powdered Tungsten Carbide Blanket.

This blanket material is then cut into a shape that matches the part to be covered. The blanket is glued into place with a layer of braze material between the blanket and part. The assembly is placed into a furnace to melt the braze and fuse the tungsten carbide to the part. The result is a final assembly that is very uniform and close to size. Final grinding finishes the part. The radial bearings are manufactured in two parts: 1) an inner and 2) outer sleeve as shown in Figure 3.15.

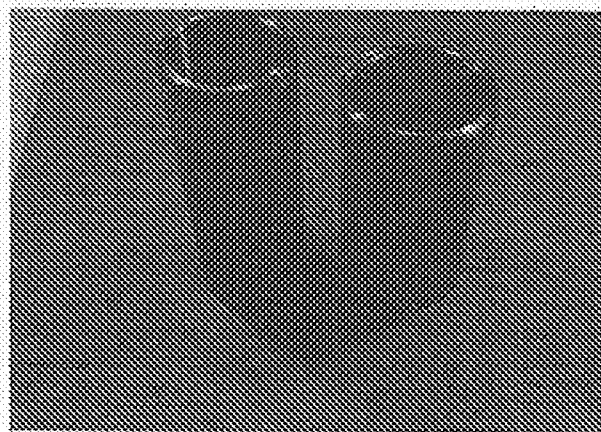


Figure 3.15 Metal On Metal Radial Bearings

These bearings wear well, because the surface is tungsten carbide, and are tough, because the core part is made from steel. They are becoming the industry standard because of their increased life and load carrying ability. The metal-on-metal bearings are also shorter than conventional rubber marine bearings, reducing bearing pack length. The metal-on-metal bearings are much more expensive than the marine bearings. Two sets (upper and lower) for the DOE high-power motor cost \$3500.

3.5 DOE High-Power Slim-Hole Motor

The above components are combined to form the slim-hole high-power motor. The specifications for this tool are shown in Table 3.5. Performance data used in the table comes from tests described in Chapter 4, Laboratory Testing.

**Table 3.5. DOE High-Power Motor
General Specifications**

	<u>ENGLISH</u>	<u>METRIC</u>
Outside Diameter	3½ Inch	85.7 mm
Overall Length	25.3 Ft	7716 mm
Weight	495 lb	225 kg
Top Connection	3½ API Reg	-
Make-Up Torque	3000 Ft-Lbs	4070 N-m
Bit Connection	2½ API Reg	-
Make-Up Torque	3000 Ft-Lbs	4070 N-m
Bit Size Range	4½ to 6 inches	-
Max WOB	19,000 Lbs	8620 kg
Max Bit Pressure Drop	500 psi	34.5 bar
Flow Rate	30 --- 110 gpm	114 --- 415 l/min
Free-Running Shaft Speed	125 --- 400 rpm	125 --- 400 rpm
Differential Pressure @ Max. Operating Torque	2000 psi	140 bar
Max Operating Torque	1100 Ft-Lbs	1490 N-m
Max Power Output	75 hp	56 kW
Max Stall Torque @ Max Flow Rate w/H ₂ O	1700 Ft-Lbs	2300 N-m
Max Allowable Overpull for Retracting Motor	22,500 Lbs	10,200 kg
Absolute Max Overpull	35,000 Lbs	15,875 kg
Configuration	4:5	4:5
Number of Stages	9.5	9.5

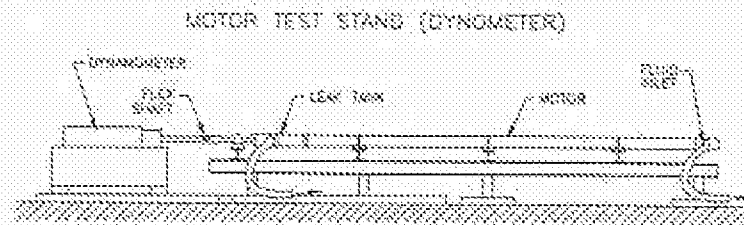
4. LABORATORY TESTING

4.1 Test Format and Objectives

The high-power, slim-hole motor was subjected to three types of laboratory tests. The first series of tests consisted of establishing the actual power output and efficiency of the motor for subsequent comparison to conventional motors. These tests were conducted on the Drilling Research Center dynamometer test stand (Figures 4.1 and 4.2). This test stand uses a water-cooled brake to apply torque resistance to the output of the motor. As torque is applied to the motor, a computer data acquisition system measures the following parameters:

1. Motor Input Pressure
2. Motor Output Pressure
3. Flow
4. Motor Speed
5. Motor Output Torque

During a performance test, the flow through the motor is fixed at a given rate and the torque on the dynamometer is gradually increased under computer control. As the torque



increases, so does the pressure drop across the motor. As torque is increased, the motor's speed decreases until the motor stalls.

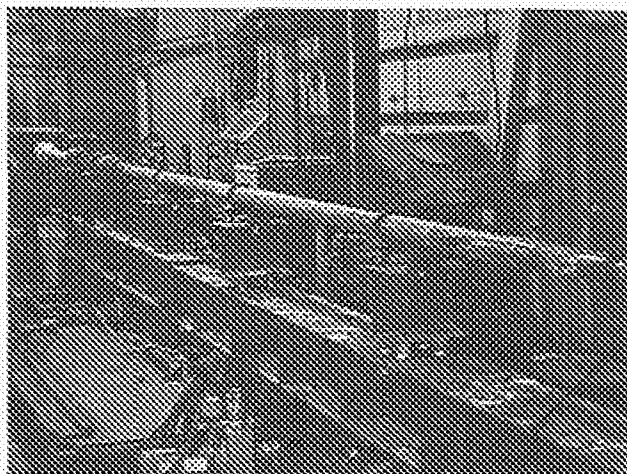


Figure 4.2. Motor in Dynamometer Stand.

The performance tests were run at 30, 70, and 110 gpm. These flow rates match the data published by R & M Energy Systems and allow direct performance comparisons with manufacturer's data. Appendix A contains the printed Data.

The second series of tests were focused on reliability and were specifically structured to identify any design weaknesses/high wear rate items which needed to be fixed prior to field testing. In reliability testing, the motor is run in a loaded condition for several hours while the computerized data acquisition system periodically monitors system parameters. The system parameters were monitored so that if they varied from the set conditions an alarm would sound to alert the operator to either make adjustments to the pump if input hydraulics were deviating from the desired settings or to examine the motor if its output speed or torque changed in any statistically significant way.

Two life tests were conducted; one for 20 hours and another for 10 hours. During these tests, conditions were held at a constant 70 gpm and 1200 psi motor differential pressure. The motor produced 770 to 790 ft-lbs of torque during the tests which represents a high loading condition.

The third form of testing was to conduct actual rock drilling tests to determine the increase in penetration rates made possible by the high power slim hole motor when combined with the high-power drag bits. These tests were conducted using Carthage marble, a hard, homogeneous rock (15,000 psi compressive strength).

4.2 Motor Performance Curves

Figures 4.3 A&B show speed and torque performance curves for the high-power

slim-hole 3½-in. DOE motor. Comparing these to the manufacturer's curves shows that the DOE motor operates at a higher rpm for the same flow rate. The difference between the laboratory measured speed and R & M's specification could result from several factors. The most logical explanation is that the longer stator of the high power motor has less slip and thus higher speed. Every motor has "slip" which is the fluid that leaks around the rotor and produces no work. A large amount of slip would reduce the speed of the motor. Increasing the number of stages reduces these losses - increasing motor speed and output horsepower.

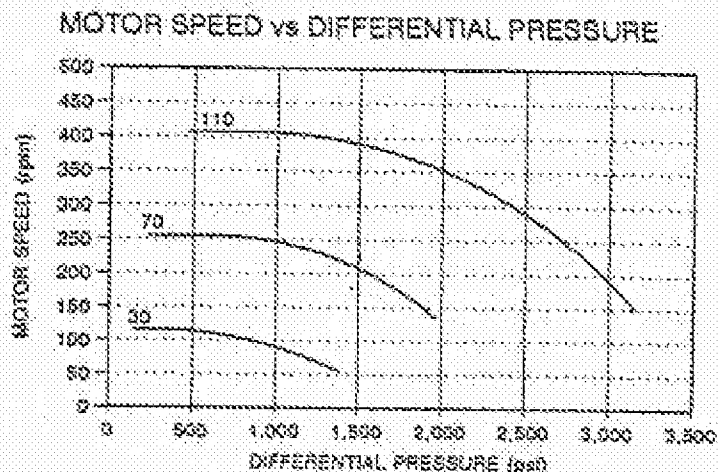


Figure 4.3A. Speed Curves

The torque output of a motor is a function of the pressure drop across the tool. Where the pressure drop is measured, can greatly affect the appearance of the torque curves and the motor efficiency. The data shown in **Figure 4.3B** were recorded using pressure transducers at the top and bottom of the motor. As a result, this pressure drop includes the losses through the bearing pack and provides the most realistic value for total motor efficiency. This can shift the torque curves from published data, resulting in a slightly lower torque at a given pressure drop. Most published data do not include pressure drop across the bearing pack - especially if the power section manufacturer, such as R&M Energy System, does not offer bearing packs for sale.

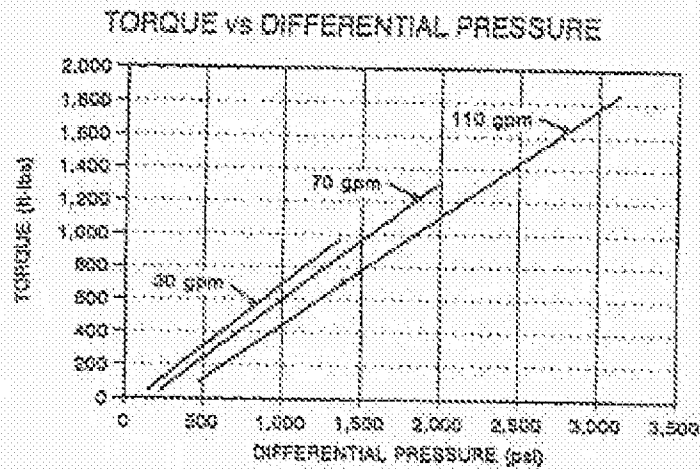


Figure 4.3B. Torque Curves.

An important source of lost energy is the pressure needed to overcome motor friction. The DOE tool has a higher startup pressure (150 to 250 psi) than conventional 3 $\frac{1}{2}$ -in. motors (50 to 100 psi) because of the longer power section. It takes more pressure to overcome the friction between the long rotor and stator. As a result, the DOE motor shows slightly less torque at a given pressure drop than the standard motor. However, the DOE motor can be operated at much higher differential pressures (2500 psi) and delivers twice the torque and horsepower of a conventional motor. (See Figure 4.4).

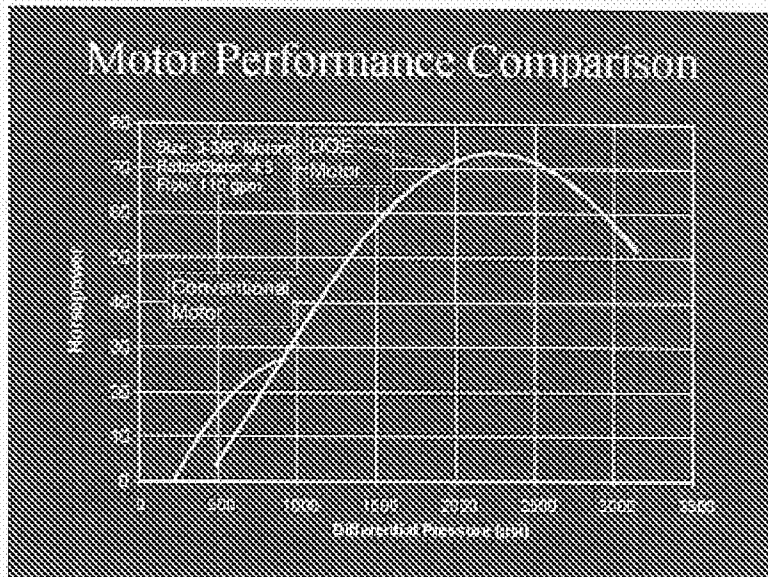


Figure 4.4. Power Curves

Motor torque is proportional to pressure drop. To take advantage of higher torques, the DOE motor must be operated at higher pressure drops. This requires rig pumps capable of producing the higher pressures at typical operating flow rates. This should not present a significant problem, as mud pumps are designed to operate at 5000 psi and most drillers operate their pump in the range of 2500 to 3000 psi.

Recently, extended-performance power sections have been introduced to the market. These new extended-length power sections were developed based on the same concepts that were used to design and build the DOE high-power motor. R & M Energy's extended-performance power sections are approximately 33% longer than their standard power sections, and therefore produce one-third more power. The DOE high-power motor is twice as long as standard, so it produces twice the power. This is two-thirds more power than commercial extended-performance power sections.

Maximum values for torque and pressure drop measured in typical laboratory tests are greater than typical field operating values. This is true because, in the laboratory, the torque load from the dynamometer is very uniform and is applied evenly, allowing the motor to perform up to maximum capability. In the field, the torque is produced from a bit drilling rock, a process that produces widely varying torque. If a motor is run too high on the performance curves (high pressure drop), spikes in the torque from the bit can stall the motor. To restart the motor, the driller must lift the bit off bottom, reestablish circulation and then slowly run back to bottom to start drilling again. This is a time-consuming process and slows overall drilling rates.

To avoid this problem, drillers normally operate motors in an area on the performance curves that allows the motor to continue drilling even when the bit torque spikes. This range is typically between 200 to 300 psi differential pressure for a standard motor. The high-power motor can easily be operated at 600 to 1000 psi differential pressure, providing twice the power. Because the high-power motor maintains rotary speed at higher pressure drops, it has the capability to continue rotating during larger torque spikes. This means that more weight on bit can be applied to increase penetration rate. This is how high-power motors achieve superior penetration rates when compared to conventional motors.

4.3 Reliability Test Results

During life testing on the dynamometer, several components suffered damage. This resulted in their redesign and retesting to validate the improvements to reliability. Specifically, the thrust bearings and load distribution system were damaged during the initial 20-hr life test as shown in **Figures 4.5 and 4.6**.

During dynamometer tests, the motor is run with no bit weight, which represents a worst-case operating situation since the "off-bottom" bearings are carrying the full hydraulic down thrust produced by the pressure drop across the motor. In normal operation, bit

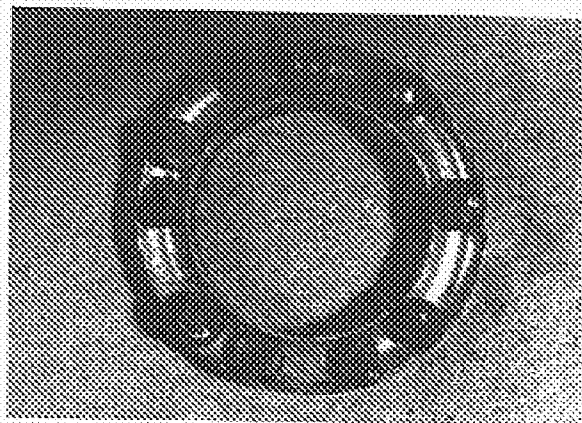


Figure 4.5. Damaged Thrust Bearing

weight offsets much of the down thrust, reducing the load on the off-bottom thrust bearings. Despite damaged thrust bearings and a broken flex coupling, the motor was still operating at full power at the end of the 20-hour endurance test.

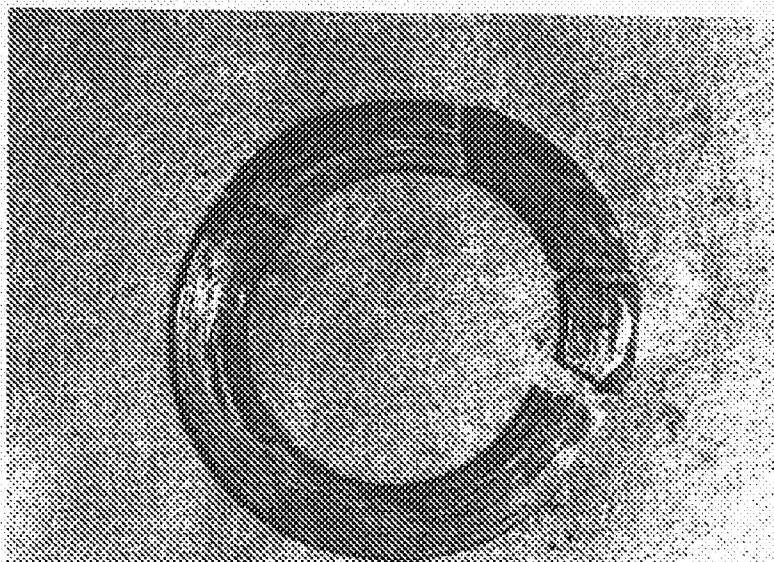


Figure 4.6. Damaged Belleville Spring.

Although bearing failure is not expected under normal drilling conditions, MEI strengthened the thrust bearings. The thickness was increased so that the bearings would flex less under load. MEI has used the same approach in the past and had excellent results. These modified thrust bearings performed well in field tests at the Catoosa test site in Oklahoma.

Belleville springs are used to distribute the load evenly between bearing sets. If these springs fail, the load can be distributed unevenly resulting in a premature bearing failure. Space constraints prevent significant design change on these components. One of the few changes that can be made is to limit the travel of the spring and thus limit the

stress in the spring. This is accomplished by machining the back of the ball race at the appropriate angle. After the dynamometer life test the stroke of the Belleville springs was reduced to reduce stress and prevent breakage. MEI has found that it is not uncommon for Belleville springs to develop a single crack and keep on functioning. When several cracks develop the shape and spring properties are lost causing incorrect load distribution.

The "baseball stitch" lobe on a flame-cut flex coupling failed during the dynamometer tests (Figure 4.7) due to the high torque and high thrust load produced by this high-power motor. This problem was anticipated prior to the dynamometer tests and resulted in the development of the titanium flex shaft previously described.

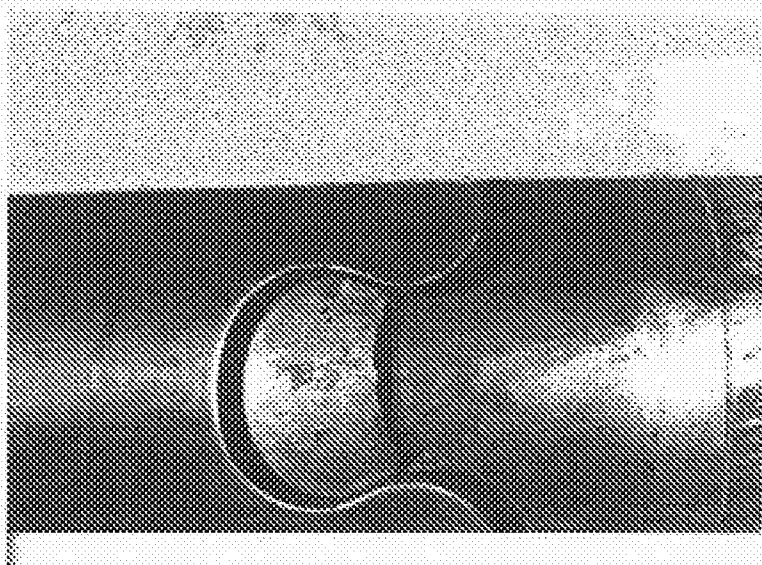


Figure 4.7. Broken Lobe On Flex Coupling.

The titanium flex shaft performed well in the second dynamometer test where the motor delivered the same power as with the conventional flame-cut flex coupling. Results confirmed that the titanium flex shaft efficiently transmitted the torque from the rotor to the drill bit. A 10-hr life test was completed with the titanium flex shaft.

4.4 Drilling Tests

The DOE high-power slim-hole drilling system consists of the high-power DOE motor and a high-power bit. Two advanced bits were manufactured for drilling tests with the high-power motor. The first, a large cutter TSP Bit (LC-TSP, Figure 4.8), was manufactured using the guidelines set out in Chapter 2 of this report. This bit has a large number of 5-mm round TSP cutters. As indicated previously, this bit design provides for the densest cutting structure possible in this size bit. This ensures cutter redundancy and

long bit life.

Previous R & D has shown that bits made with large 5- to 7-mm TSP cutters drill faster and last longer than conventional TSP bits with smaller 3-mm TSP cutters, and that rounding off the corners on the TSP cutters reduces breakage during drilling. The second DOE test bit is a hybrid design which uses both PDC and large TSP cutters (Figure 4.9). This bit utilizes 8-mm PDC cutters for drilling soft formations and 5-mm round TSP cutters for drilling hard formations. The PDC and TSP cutters are set at the same height so that they wear at the same rate. In the field, the hybrid design will allow the PDC cutters to drill soft formations at high rates yet drill through hard stringers with the TSPs. The TSPs main contribution is to prevent premature wear of the PDC cutters. This design has high drilling rates in nonhomogeneous formations that alternate between hard and soft rock.

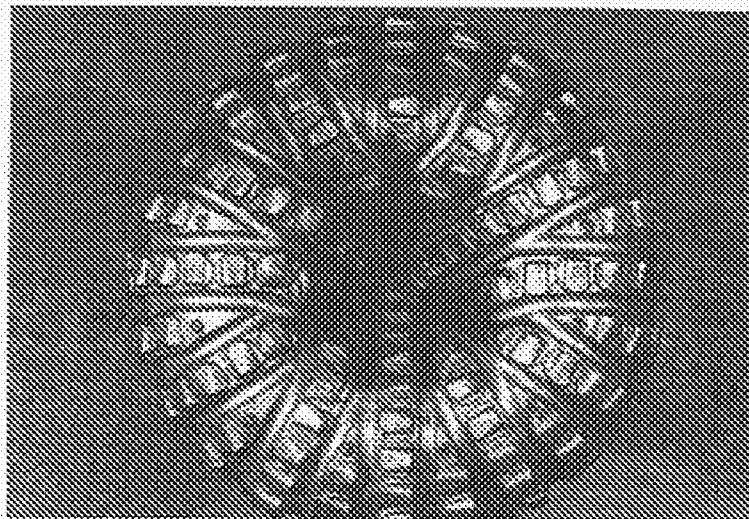


Figure 4.8. Large Cutter TSP Bit

Proper bit cleaning is critical in TSP and PDC bits because of their high drilling rates. Therefore, nozzles were added to the DOE TSP/PDC bit so that hydraulic horsepower used for cleaning the bit can be controlled and directed across the cutting faces.

Conventional diamond bit designs rely on small flow grooves and the narrow spaces between the bit body and rock face to aid in transporting the cuttings from under the bit. When drilling at high penetration rates, these small passages can become clogged with cuttings. This transfers some of the bit weight used to make the cutters penetrate the rock to the bit body, slowing penetration rates.

The design shown in **Figure 4.9** has large flow passages for removing the cuttings, and the nozzles increase the force and velocity of the fluid to move the cuttings more efficiently. Better cleaning increases penetration rates by eliminating energy wasted on re-grinding cuttings already removed from the rock faces.

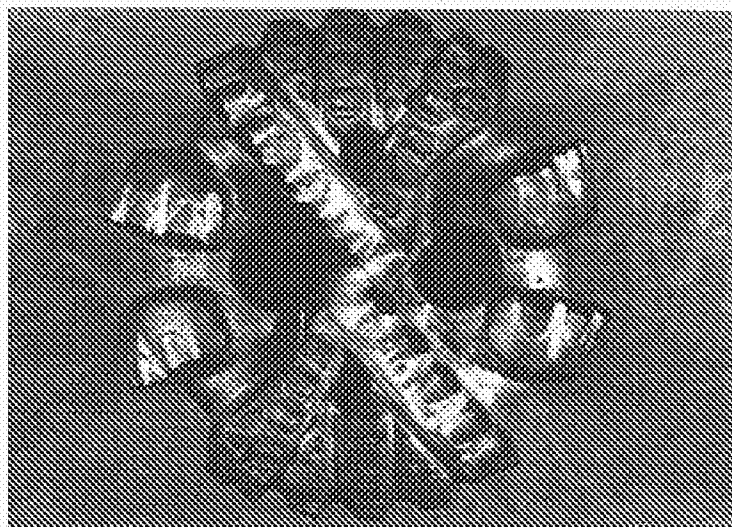


Figure 4.9. Hybrid TSP/PDC Bit.

The motor and bits were tested on the DRC motor test stand in Carthage marble. **Table 4.1** shows the conditions used for these tests.

TABLE 4.1. Motor Test Conditions

Motor:	3 $\frac{1}{2}$ -in. DOE motor
Flow rate:	110 gpm
Bit:	4 $\frac{3}{4}$ in. LC-TSP & Hybrid TSP/PDC
Bit weight:	2000 to 14,000 lbs

Figure 4.10 shows that the 5-mm round TSP bit and motor combination drilled Carthage marble at rates of 10 to 50 ft/hr as weight on bit (WOB) was increased from 4000 to 12,000 lbs. This bit is designed to drill harder rocks and is well matched to the motor. The input pressure to the motor determines the work the motor is performing. As the WOB

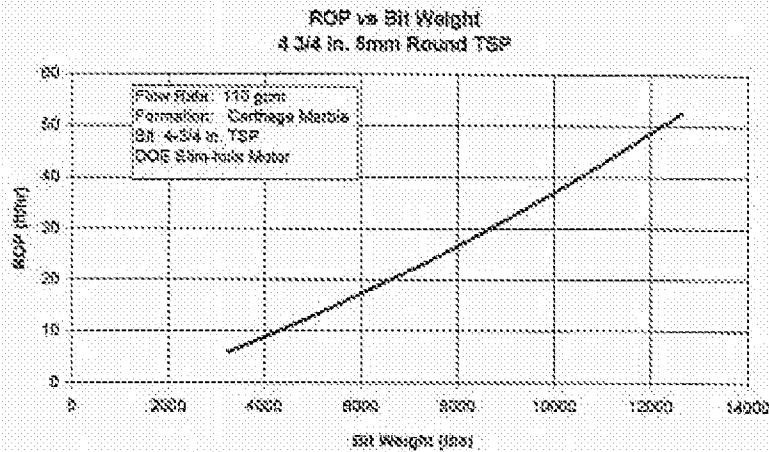


Figure 4.10. ROP For TSP Bit.

was increased from 4000 to 12,000 lbs, the pressure rose from 800 to 1400 psi (Figure 4.11).

This motor will operate well with a pressure drop of 1400 psi. These data show that, for hard rock, over 12,000 lbs weight on bit can be applied to the DOE slim-hole drilling system while remaining within operating parameters. A standard motor is designed to operate at a pressure drop of only 700 to 800 psi. This would correspond to a bit weight of less than 4000 lbs or only one-third that of the high-power slim-hole system.

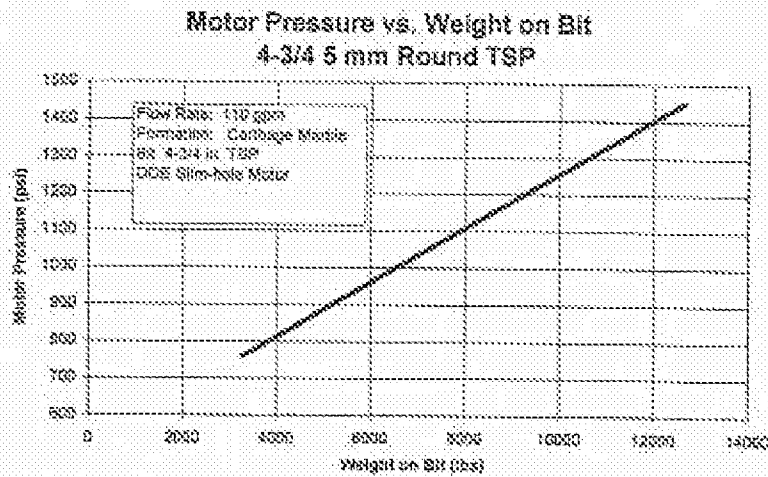


Figure 4.11. Motor Input Pressure As A Function Of bit Weight.

Figure 4.12 shows that the hybrid bit drilled Carthage marble at rates of 60 to 250 ft/hr, as weight on bit was increased from 4000 to 13,000 lbs. This is a high penetration rate for hard rock. The addition of PDC cutters and nozzles produced these very high penetration rates. Testing has shown that cleaning is very important, but it is unlikely that the high penetration rates obtained with this bit are solely due to improved cleaning.

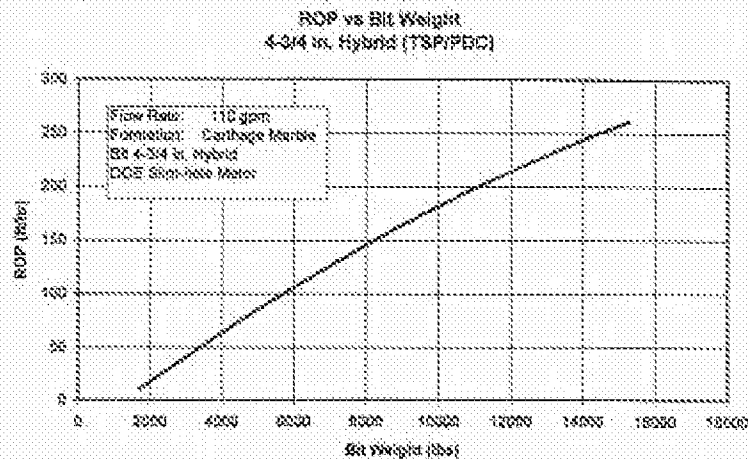


Figure 4.12. ROP For Hybrid PDC/TSP Bit.

As bit weight increased, more motor torque was required to rotate the bit. To increase motor torque output, the pressure drop across the DOE motor had to be increased. Figure 4.13 shows how the motor pressure drop increased as a function of bit weight. These data show that at 12,000 lbs WOB the motor pressure drop was 1500 psi, and that the motor could operate at pressure drops up to 1700 psi. These data show that

the high-power motor can drill at high bit weights with aggressive PDC bits designed for drilling softer formations.

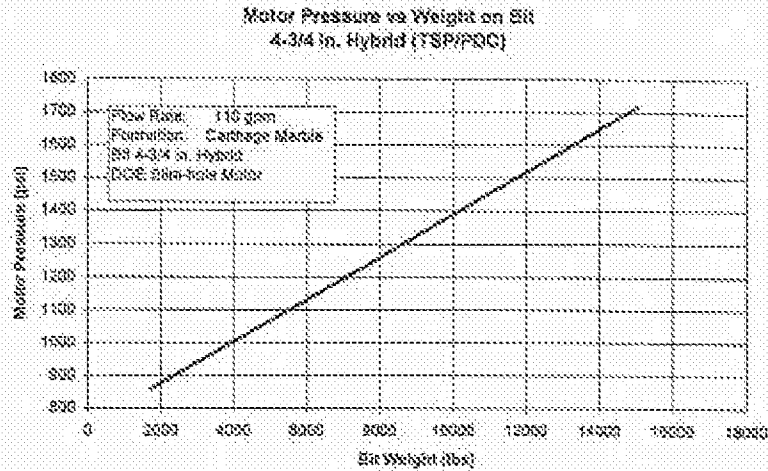


Figure 4.13. Motor Pressure & WOB for PDC/TSP Bit.

The PDC/TSP bit is designed to drill soft formations quickly, but if hard stringers of rock are encountered, the bit can continue drilling without damaging the PDCs. These tests demonstrated that both of these bits are good candidates for use with the high-power motor.

5. FIELD TESTING

5.1 Catoosa Test Site

Two field tests were conducted with the slim-hole high-power DOE motor at the Catoosa test facility in Oklahoma. This facility allows testing of oilfield down hole tools under actual well known field conditions. The site has numerous facilities for different types of testing including a large main drill rig that is instrumented so data can be gathered during the drilling process. **Figure 5.1** shows the Catoosa site large drilling rig.

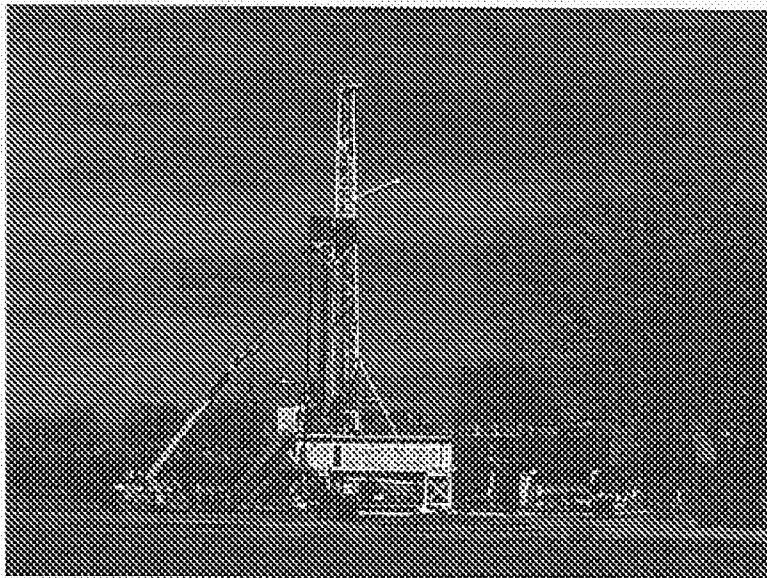


Figure 5.1. Instrumented Catoosa Drill Rig.

One of the unique features of Catoosa is the large number of formations that are encountered in a relatively shallow zone. **Figure 5.2** shows the lithology at Catoosa. The strength of the formations varies from very soft to vary hard. **Figure 5.3** is a plot of the rock strength, based on sonic logs, as a function of depth. The formations strengths vary from 5,000 to 30,000 psi compressive strength. At the top of the Mississippi Limestone at approximately 1350 feet is a formation know as "The Wall". The wall is a very hard section of rock that has historically proven to be difficult to drill. In fact, many drill bits that have been tested at Catoosa have failed to drill "The Wall". PDC bits are often severely damaged drilling this formation because of the hardness of the rock and the vibrations that it produces during drilling including bit whirl.

Drilling is conducted in 8 to 10 hour shifts during the day. At the end of the day the drill string is pulled to a safe level in the hole, usually to a point were all the bottom hole assembly components are inside cased hole. Since the formations are shallow this procedure does not excesssively disrupt the drilling process and allows fewer technical

personnel to monitor tests.

		Surface - 70 ft	Big Limestone
Pennsylvanian	Charlotte Group	70-277 ft	Peru Sandstone Zone
		277-304 ft	Oswego Limestone
		304-375 ft	Prue Sandstone Zone
		375-385 ft	Stanner Sandstone Zone
		385-595 ft	Stanner Sandstone Zone
		595-604 ft	Pink Limestone
		604-628 ft	Red Fork Sandstone Zone
		628-838 ft	India Limestone
		838-879 ft	Bartlesville Sandstone Zone
		879-1186 ft	Brook Sandstone Zone
Mississippian		1186-1218 ft	Burgess Sandstone
		1218-1252 ft	Fayetteville Shale
Devonian		1252-1549 ft	Missisquoi Lime
		1549-1578 ft	Woodford Shale
Cambro-Ordovician		1578-1605 ft	Missener Sandstone
		1605-2920 ft	Arbuckle Group

Figure 5.2. Catoosa Lithology

The first test conducted at Catoosa was a "shake out" test for the motor. It was intended

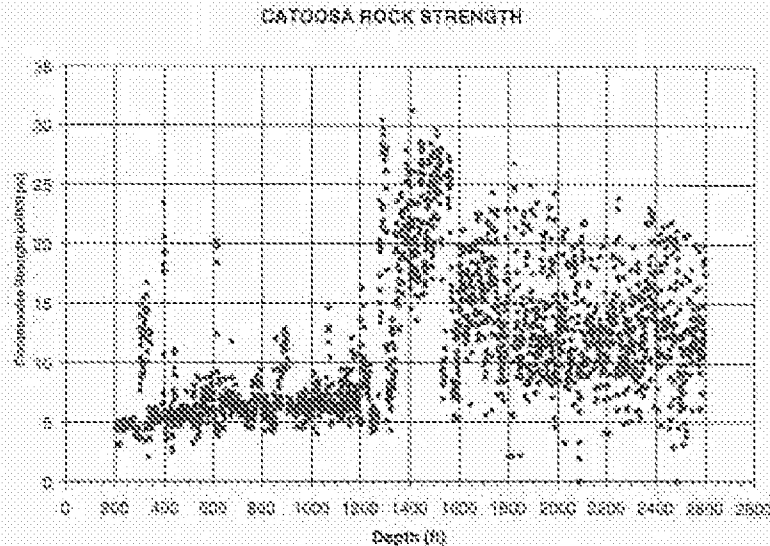


Figure 5.3. Catoosa Rock Strength.

only to find any obvious problems. The second test was conducted to compare the DOE drilling system against a conventional system.

5.2 First Field Test

The first test was conducted from February 22 to 27, 1996. During this test the DOE motor and a hybrid PDC/TSP bit were used to drill from 623 ft to 1450 ft. The drilling was conducted over three days. The majority of the first two days were through soft formations and the DOE system was able to drill at high rates. At the end of the second day, the bottom hole assembly entered "The Wall" at which time the penetration rates became considerably slower. Figure 5.4 shows the drilling rate for the three days as a function of depth. Appendix B contains data for this field test.

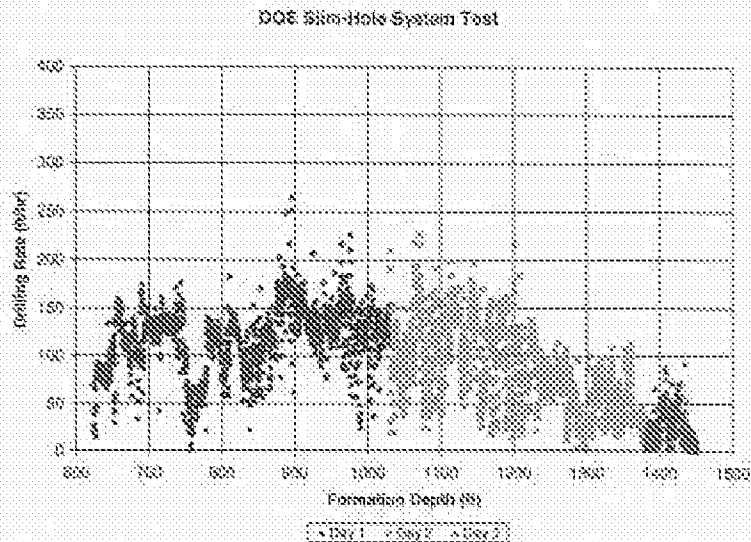


Figure 5.4. Drilling Rates Catoosa Shake Out Test.

Figure 5.4 shows that the drilling rate in the upper formations was averaging 100 to 175 feet per hour (fph). At the top of the Mississippi Limestone the average rate dropped to 50 to 75 fph. As the bit entered "The Wall" the rate dropped to less than 1 fph. The DOE system with hybrid bit drilled from 1380 to 1450 ft in this hard formation. Penetration rates varied in this section (1 to 12 fph), but the BHA continued to drill. The test was only terminated because time and test monies ran out, not because the system quit.

Bit weights were varied from 2,000 to 12,000 lbs, but averaged 8,000 to 10,000 lbs during the test. The motor performed well at different weights, but drilling rate was fairly independent of bit weight. This is because the upper portion of the hole is comprised of soft formations that do not require high bit weights to achieve maximum penetration rate. At "The Wall" higher weights are needed, but bit vibrations require that weight be reduced at some points in the drilling. Figure 5.5 shows the bit weights as a function of depth. The total drilling hours on the system in this test was 16.4 hours. This is not the total time below the rotary table but the actual drilling time.

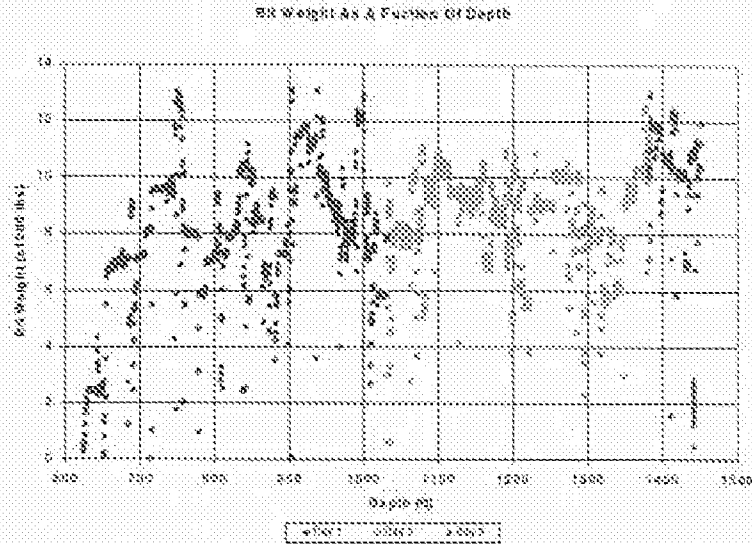


Figure 5.5. Bit Weight.

The motor and bit were still in excellent running condition at the completion of this test. Figure 5.6 shows the bit at the conclusion of the test. The PDC cutters do have a wear flat from drilling through "The Wall". However, none were broken as is common when drilling this formation with conventional PDC bits. This bit could have continued drilling or could have been rerun as it came from the well. For our testing purposes, the bit was rebuilt by rotating the worn cutters to new locations. The TSP cutters were still in excellent shape.

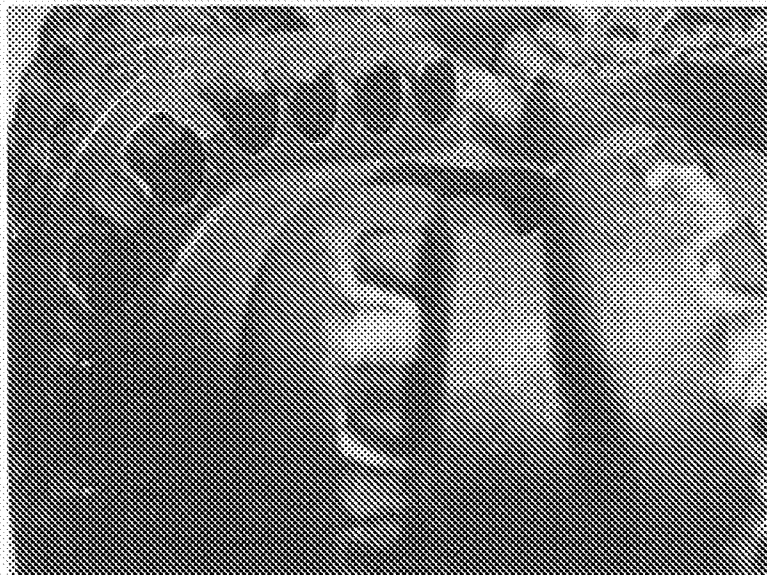


Figure 5.6. Hybrid Bit After Test No. 1.

The motor was returned to MEI's Drilling Research Center shop facility where it was disassembled and inspected. The bearing pack components were in excellent condition. The flex shaft showed no signs of wear. However, the bottom section of the stator showed some damage. This damage was in the form of "chunking" - pieces of rubber missing from the molded form. The stator was sent back to R & M Energy Systems for analysis. R & M did not have an explanation for the failure other than rubber fatigue. After further discussions between R & M engineers and MEI staff it was concluded that the titanium flex shaft was placing too high a load on the rubber. Further design analysis of the flex shaft and discussions with the titanium supplier concluded that too conservative a value for the endurance limit had been used in the initial design. The flex shaft was redesigned based upon a new, higher, value. The new design has a much smaller outside diameter making the shaft more flexible. The motor was repaired by relining the bottom section of the stator. The redesigned tool was then prepared for the second field test.

5.3 Second Field Test

The second field test compared the performance of the high-power slim-hole system against conventional motor drilling systems. To accomplish this comparison it is necessary to either have a uniform formation thick enough to justify running two bottom hole assemblies or significant offset well data where operating conditions are similar to the current well. This situation could not be found in actual wells so it was decided to test at Catoosa where BHAs could be changed out when necessary for test purposes. **Appendix C** contains printed data for each BHA.

The formation drilled during the test is the Arbuckle dolomite. (See **Figure 5.2**). It starts at 1805 ft and runs down to 2920 ft. This is the deepest formation drilled at the Catoosa site. The top 800 ft of the Arbuckle is very uniform and provides a location where the DOE drilling assembly performance could be compared to a conventional assembly.

The test plan was very simple. Three BHAs would be tested. The first and the third would use the high-power DOE motor with a conventional 3-3/8 motor run between these two in the second assembly. The hybrid bit was used on all assemblies so that drilling rates would not be affected by differences in bit performance. **Figure 5.7** shows a schematic of the test plan.

Both the DOE motor and the commercial 3-3/8 motor had a maximum rated flow rate of 110 gpm. This flow was used through out the test to simplify performance comparison between the different BHAs. Since flow rate is constant the power would be a function of the pressure drop across the motor. Since the DOE motor is twice as long, and has twice the number of stages, the pressure drop across the DOE motor will be much higher than across the commercial motor. Thus the DOE motor was able to produce more torque and drill faster, because more weight on bit could be applied without stalling the motor.

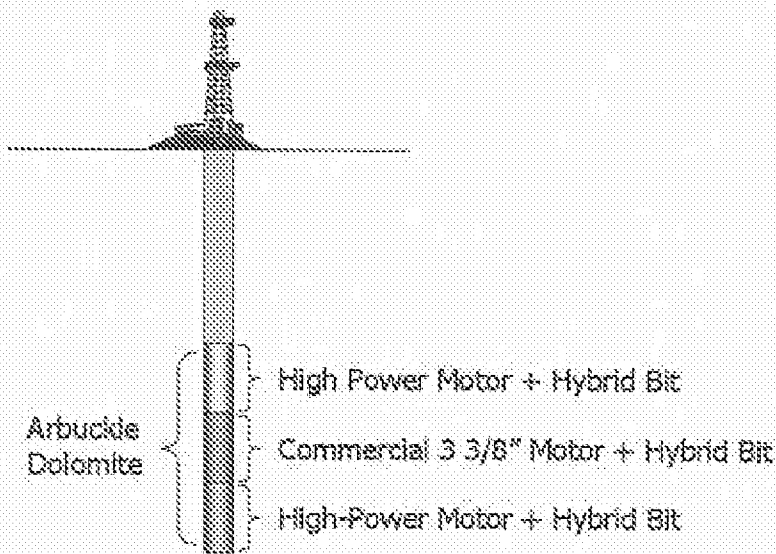


Figure 5.7. Field Test Plan Schematic.

The wells at Catoosa have not be drilled as slim holes so the upper portions of the well are completed with 13-3/8 in. casing. At 110 gpm and the velocity of the drilling fluid will not be fast enough to clean the hole. To avoid hole cleaning problems, two identical pumps (Figure 5.8) were used to drill the well. One pump provided drilling fluid to drill the well while the second pumped mud down a parasite string to increase the velocity in the upper section of the well. Figure 5.9 shows how the pumps were used.

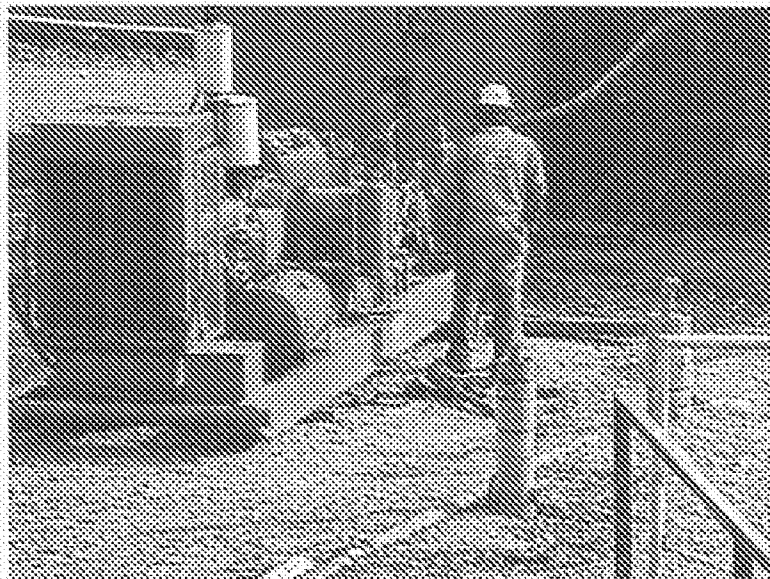


Figure 5.8. Haliburton Mud Pump Used For Test.

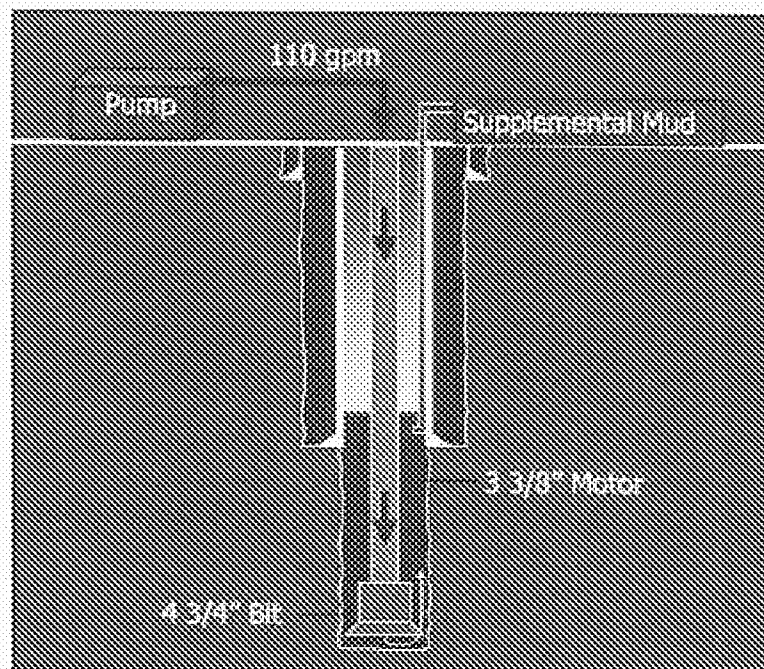


Figure 5.9. Main and Supplemental Mud Pumps.

Bottomhole Assembly #1

The first BHA consisted of the high-power motor and a new 4-3/4 in. hybrid bit. This assembly drilled a total of 98 feet in 4.7 hours for a penetration rate of 21 feet per hour. However, the first hour of drilling required several adjustments and repairs to the rig and mud pumps. Also, near the end of the run a very hard stringer of rock was encountered that slowed drilling. Since the other runs did not encounter these problems or similar hard stringers, a comparison can only be made if these sections are excluded. The average penetration rate for the middle section of drilling (1.5 to 3.5 hours) on BHA #1 is 29 feet per hour.

The testing of BHA No. 1 began on December 17, 1998. After rigging up the motor was surface tested. After confirming proper operation of the DOE motor, assembly was run into the hole and the bottom tagged. At this time, the rig tongs had to be repaired. Once the tongs were repaired the flow was increased to 76 gpm and the bit collared. Flow was then increased to 110 gpm and drilling begun. Problems with both the main pump and the supplemental pump caused further delays. After repairing the pumps, the BHA was brought up above the Bartlesville shale and operations concluded for the day. The Bartlesville shale can swell and sluff so this precaution was taken to prevent damage to the BHA.

Testing of BHA #1 resumed on December 15, 1998. The tool was run into the hole, the pumps were started and the driller washed to bottom. Flow rate on the pumps was set and drilling begun. The pump rate was set at 110 gpm. However the pump would speed

up on its own until it reached 118 gpm (Figure 5.10) were it would run consistently for long periods of time.

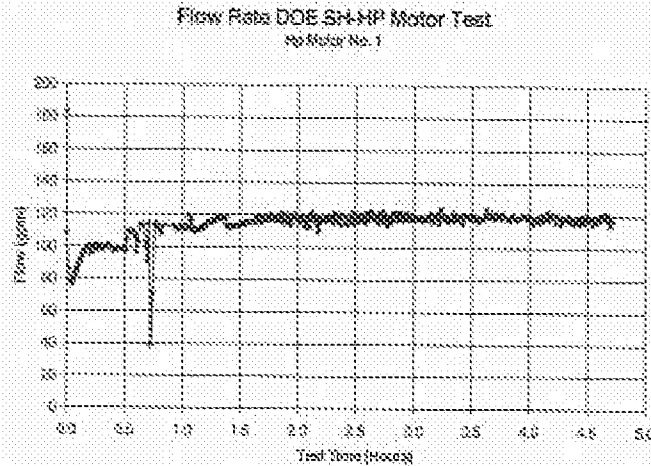


Figure 5.10. BHA No. 1 Flow Rate.

The bit weight was varied from 4,000 to 16,000 lbs during the test to find the optimum point. The optimum point is that bit weight that provides the highest penetration rate without stalling the motor. Figure 5.11 shows a plot of bit weight throughout the test. The

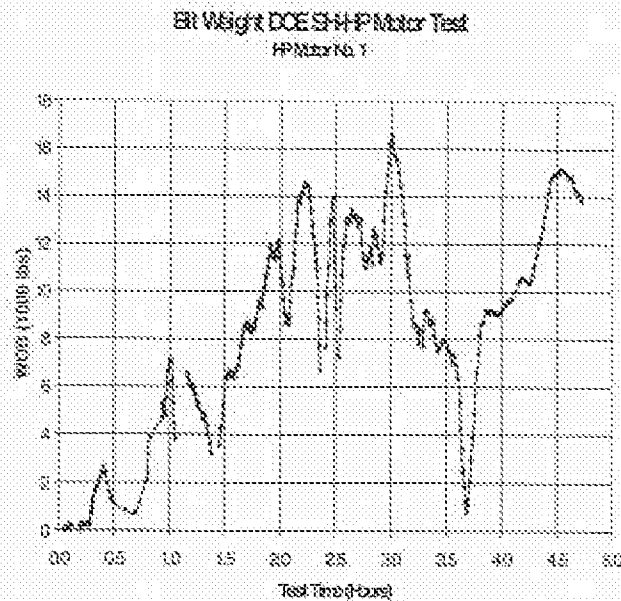


Figure 5.11. Bit Weight BHA No. 1.

BHA seemed to run best in the dolomite at a bit weight of approximately 12,000 lbs.

As bit weight was increased the torque to rotate the bit increased. The motor supplied the torque to rotate the bit and the pressure drop across the power section increased with the increased torque requirement. **Figure 5.12** shows the standpipe pressure. The increase in pressure corresponding to increased torque requirements can easily be seen. The off bottom or no load pressure was 1300 to 1400 psi. This makes the power section pressure drop 600 to 700 psi. This is very high for actual field conditions.

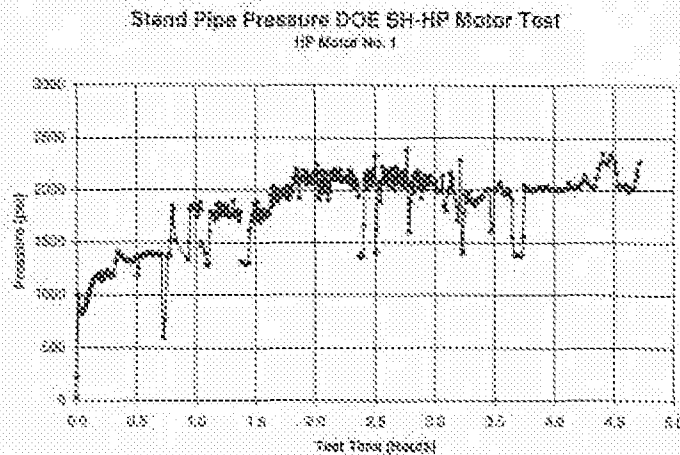


Figure 5.12. Stand Pipe Pressure BHA No. 1.

The penetration rate varied from under 1 fph through the hard stringer to over 70 fph. The majority of drilling was in the 20 to 40 fph range (**Figure 5.13**). When the BHA was pulled at the end of the run the bit was severely damaged. **Figure 5.14** shows how the bit was rung out. The manufacturer's designer examined the bit along with the bit used on the next two BHAs. He had seen this type of damage once before, and felt that one of the PDC inserts could have been pulled from the matrix because of the high drilling forces. The solution is to modify the design so that PDC inserts in this row are buried deeper into the matrix. This explanation has some supporting evidence from the field. When the drilling rate dropped off there were severe vibrations on the rig. These vibrations caused the whole rig to shake and the driller had to lift off bottom and run with light weight for several minutes before bit weight could be increased. It is possible that the vibrations were caused by the insert rolling under the bit, and this continued until the insert had been broken into small enough pieces that the mud could wash them away. Visual examination of the bit shows that some PDC cutters are missing from their braze pockets while others are still in place. If the formation were too hard for the bit all of the PDC cutters should be damaged. The TSP back up cutters are in good condition except for the wrung out area. This would be consistent with a lost PDC cutter rolling under the bit because it would have broken these TSP cutters. The drilling data do show that once through the hard stringer the ROP picked up again to over 20 fph despite the severe damage.

Penetration Rate DCE SH-P Motor Test
BHA No. 1

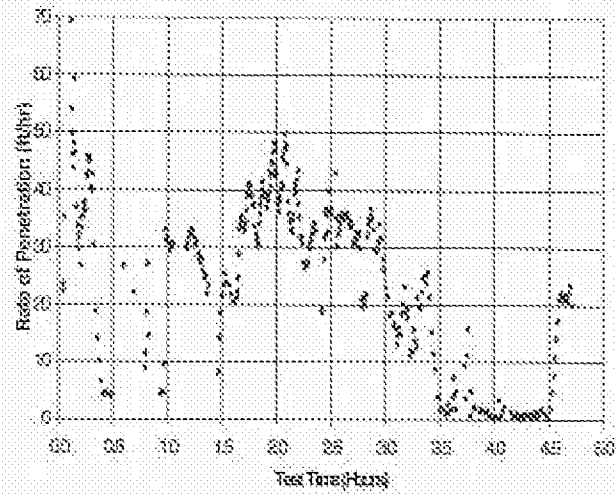


Figure 5.13. BHA No. 1 Penetration Rate.

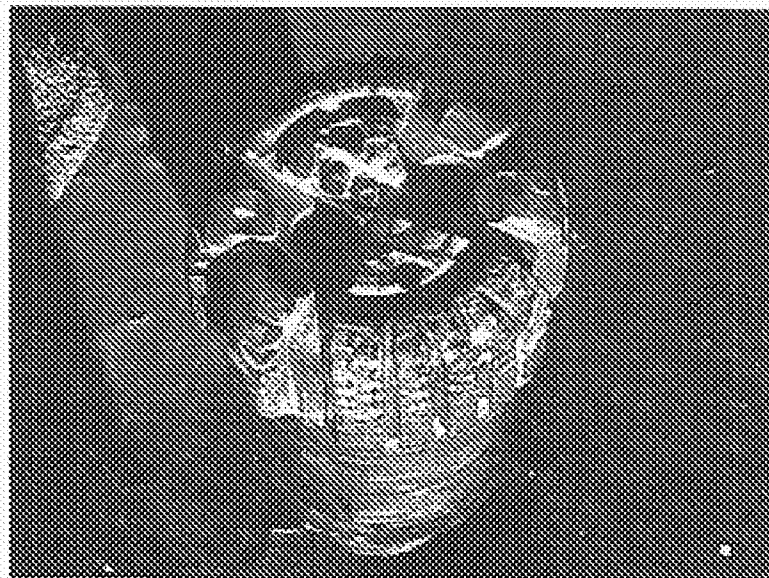


Figure 5.14. Damaged Hybrid Bit BHA No. 1.

Bottomhole Assembly #2

The second BHA used a commercial 3-3/8 in. mud motor. This tool was fitted with a new hybrid bit and run into the hole on December 16, 1998. After running to bottom and collaring the bit, drilling was begun. Recommended flow rate for this motor is 110 gpm. **Figure 5.15** shows the flow for BHA No. 2. During the first 1.25 hours of the test the flow was kept at this level. After a pump problem was repaired at 1.5 hours into the test, the flow was maintained at 120 gpm. As was previously stated, the pump had a "groove" at this flow rate.

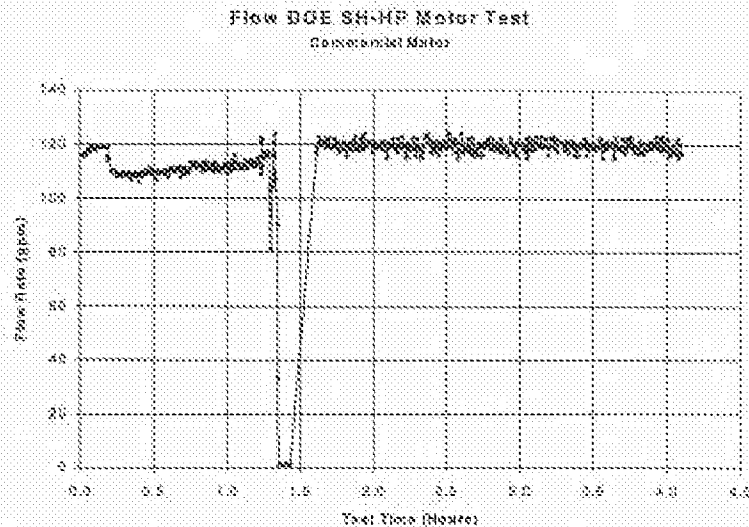


Figure 5.15. BHA No. 2 Flow Rate.

The driller applied bit weights that developed approximately 400 psi differential pressure on the motor. **Figure 5.16** shows the stand pipe pressure for this BHA. The driller commented that this tool stalled much easier than the high-power motor. Comparing **Figure 5.12 to 5.16** shows that the stand pipe pressure for the conventional motor was only 1600 psi while the high-power motor had a stand pipe pressure of 2000 psi. At 120 gpm, the DOE tool was generating 28 more horsepower than the conventional motor.

Pressure DOE SH-HP Motor Test
Commercial Motor

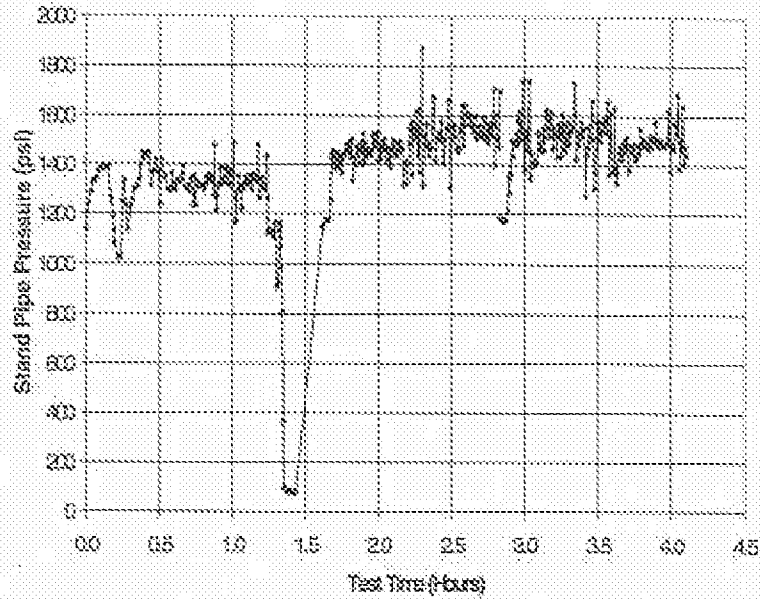


Figure 5.16. Stand Pipe Pressure BHA No. 2.

The bit weight for BHA # 2 (Figure 5.17) was a maximum of 6,800 lbs while the DOE motor ran at weights as high as 12,000 lbs. BHA # 2 drilled at approximately 20 fph with a flow rate of 110 gpm. Increasing the flow rate to 120 gpm helped and the rate increased to 25 fph (Figure 5.18).

Weight On Bit DOE SH-HP Motor Test
Commercial Motor

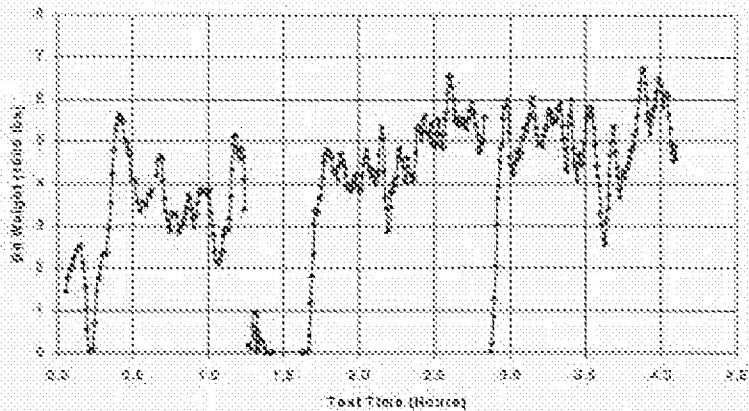


Figure 5.17. BHA No. 2 Bit Weight.

Penetration Rate DOE SH-HF Motor Test
 Downcomer Motor

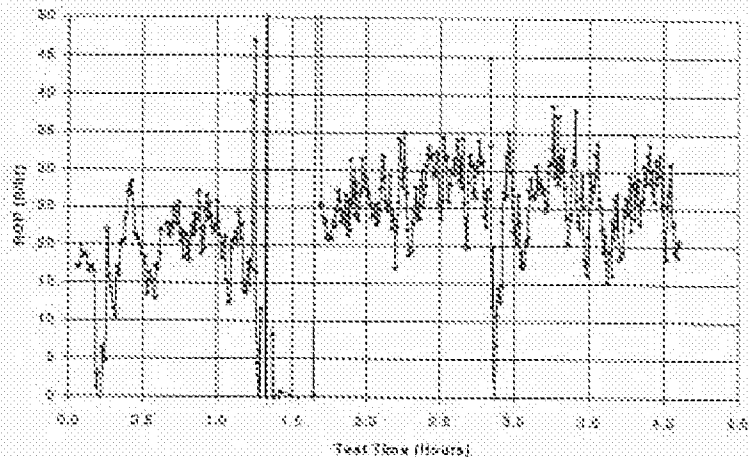


Figure 5.18. BHA, No. 2 Penetration Rate.

Although the penetration rates for BHA #2 are at times comparable to BHA #1, it must be noted that great efforts were made to obtain the best rates for BHA #2. The driller kept the motor as near to the stalling point as was possible. He was able to do this because the test lasted only a few hours and his attention on this test rig were not divided between other duties as they often are on an actual drilling operation.

At the conclusion of the run the motor and bit were pulled from the hole. The bit was in excellent condition so the decision was made to use it on BHA #3.

Bottomhole Assembly #3

BHA #3 reused the bit from BHA #2 and a new double length motor. The assembly was run into the hole on December 17, 1998. After tagging bottom and collaring the hole drilling began. Flow was set at 115 to a 120 gpm as shown in Figure 5.19. The purpose of the DOE high-power slim-hole drilling system is to double penetration rates in small holes so on this run the driller was instructed to keep high bit weights on the motor. Figure 5.20 shows the bit weight for BHA #3. Bit weight was held at 8,000 to 10,000 lbs, generating a standpipe pressure of 1,800 to 2,000 psi (Figure 5.21). This is a 800 to 800 psi motor differential pressure. This assembly obtained penetration rates of 40 to 80 fph with an overall average of 47 fph. This is double the rate for the conventional system. Figure 5.22 shows the penetration rate for BHA #3. This shows that doubling the length of a motor, and thus doubling the power, can more than double the penetration rate.

Flow Rate DOE SH-HP Motor Test
HP Motor No. 2

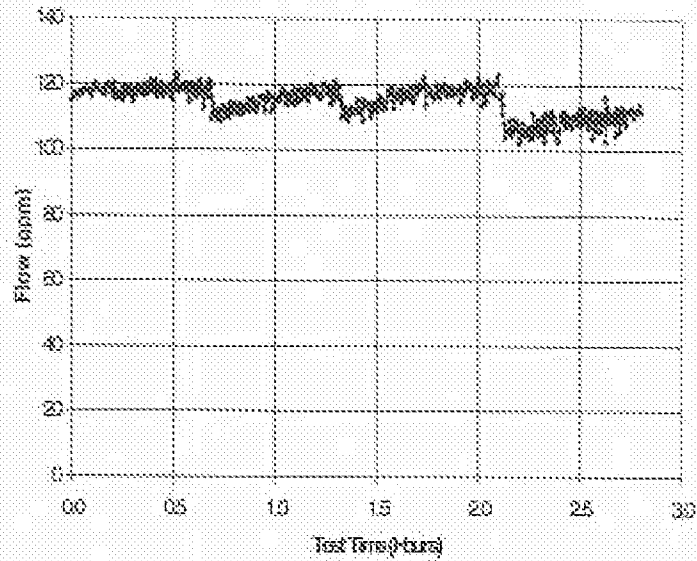


Figure 5.19. Flow Rate BHA No. 3.

Bit Weight DOE SH-HP Motor Test
HP Motor No. 2

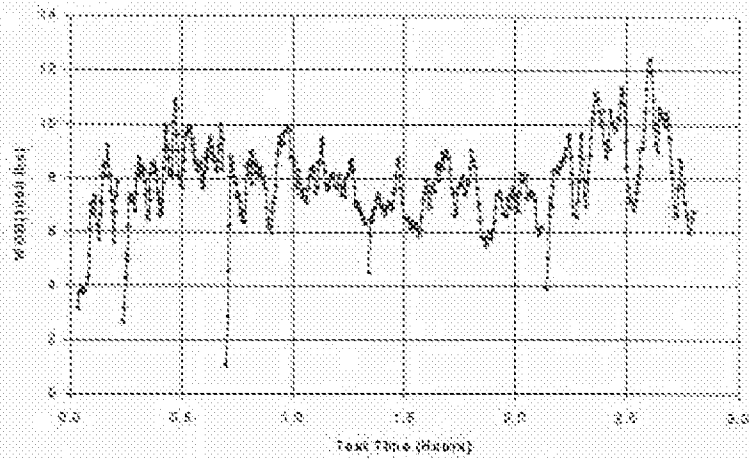


Figure 5.20. Bit Weight BHA No. 3.

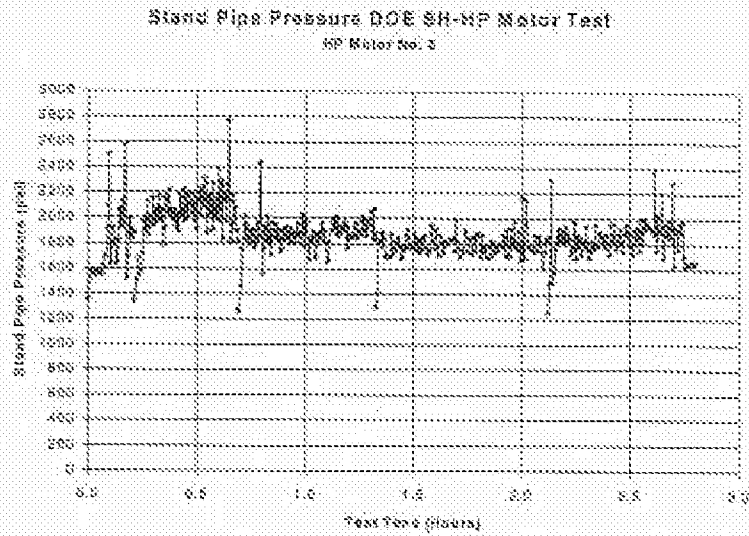


Figure 5.21. Standpipe Pressure BHA No. 3.

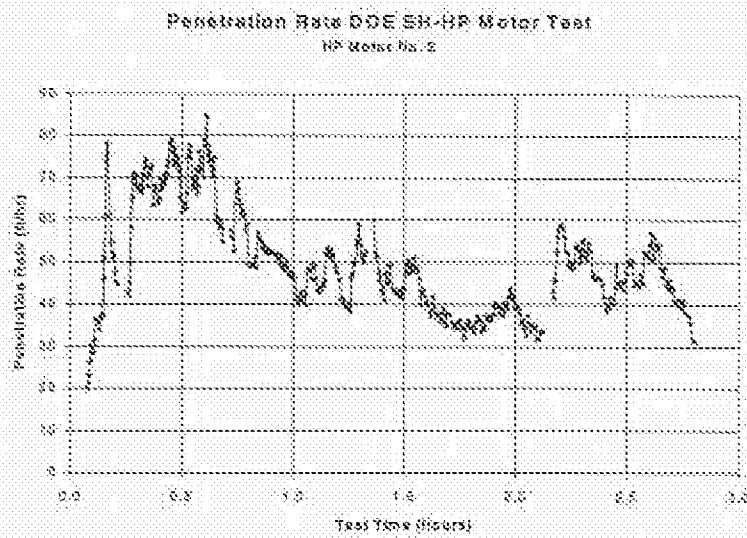


Figure 5.22. Penetration Rate BHA No. 3.

Figure 5.23 shows the penetration rates for the different BHAs. BHA #1 was only 17% faster than BHA #2 because as part of the first test we intentionally varied the drilling parameters

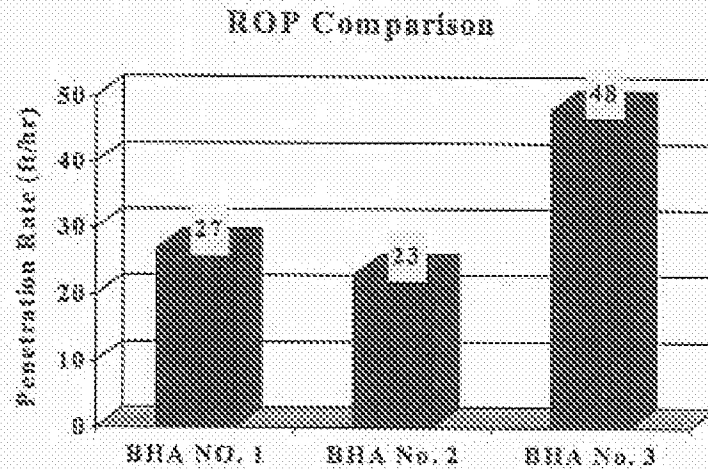


Figure 5.23. Penetration Rates For Different BHAs.

to see how the DOE motor responded. Also, even though the worst of the drilling through the hard streak was omitted from the average time, examination of the penetration rate curve for BHA #1 shows that the rate falling off even before the hard steak was contacted. If we compare the middle portion of the run, the rates are more in line with BHA #3, being from 35 to 45 fph.

6. CONCLUSIONS AND RECOMMENDATIONS

6.1 Conclusions

The work completed under this project has shown that a slim-hole drilling system comprise of a high-power mud motor and hybrid bit can be manufactured that has the ability to drill faster and have long life. This system overcomes many of the problems associated with slim-hole drilling particularly those areas that are most often sited, slow drilling rates and poor BHA life, as the reason slim-holes are not drilled more often. The following are major conclusion of the project.

1. A high-power slim-hole (HP SH) drilling system was developed that drills at double the rate of conventional systems.
2. The HP SH drilling system, when combined into a complete slim-hole drilling operation, will provide significant savings when drilling gas wells.
3. A high-power 3 $\frac{1}{2}$ -inch diameter drilling motor was developed that delivers twice the power of conventional drilling motors. This motor was made by welding two conventional stators together forming a single power section twice the length.
4. Doubling the torque output and thus the power of a mud motor increases the drilling rate when the proper bit is used.
5. Two conventional stators can be welded together to produce a single power section twice as long as a standard power section.
6. A double-length power section produces twice the torque and thus twice the power of a standard power section.
7. A flex shaft manufactured from titanium can transmit the high rotational torque from a mud motor rotor to the bearing pack shaft.
8. The flex shaft, if designed correctly does not damage the stator.
9. High strength ball thrust bearings and metal-on-metal radial bearings improved the performance of a conventional bearing pack.
10. Metal-on-metal radial bearings carry higher loads in a shorter package than elastomer marine bearings.
11. Improved bit performance can be achieved through the combined use of polycrystalline diamond compact (PDC) cutters and thermally stable product (TSP) cutters.
12. TSP cutters set behind and at the same level of PDC cutters can reduce wear of the PDC cutters when drilling mixed formations or through hard stringers in shale formations.

13. A hybrid bit can drill both soft and hard formations at high drilling rates.
14. The hybrid bit is a good bit to use with the high-power DOE motor.
15. Commercial application of the hybrid bit shows that it can replace multiple-roller or PDC bits.

6.2 Recommendations

The following recommendations are made as a result of the previous work.

1. Additional work should be done on the development of slim-hole drilling concepts and equipment.
2. Current slim-hole or reduce-hole-size projects should be reviewed to identify the areas needing development work, (i.e., identify the items which prevent slim-holes from being considered in the planning stages).
3. Continue field testing the high-power slim-hole drilling system developed in this project.
4. Identify and involve a commercial provider of mud motors in further work.
5. Integrate the DOE high-power slim-hole motor and bit into a complete slim-hole drilling operation.

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APPENDIX A

DOE High-Power Slim-Hole Motor Dynamometer data

- 30 gpm
- 70 gpm
- 110 gpm

Drilling Research Center

DOE 3-3/8 in. 4/5 multilobe motor-Flex Shaft

Test Time: 14:42:33.84

Test date: August 4, 1998

Pt. No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 30 gpm (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)
0	4	32.25	138	119	218	7	203	4	24	0.5	15%
1	5	32.25	110	102	208	9	197	3	20	0.4	11%
2	6	32.25	116	108	211	7	204	4	22	0.5	13%
3	7	32.25	116	108	209	7	201	4	22	0.5	13%
4	8	32.25	122	113	208	9	199	3	24	0.5	13%
5	9	32.25	126	116	208	9	199	3	24	0.5	13%
6	10	32.25	122	113	206	7	199	3	22	0.5	14%
7	11	32.25	122	113	208	9	199	3	20	0.4	13%
8	12	32.25	122	113	208	9	199	3	22	0.5	14%
9	13	32.25	122	113	211	7	204	4	22	0.5	13%
10	14	32.25	126	114	208	9	199	3	24	0.5	13%
11	15	33.13	126	113	202	7	195	3	22	0.5	14%
12	16	32.25	126	115	208	9	196	3	23	0.5	14%
13	17	32.25	116	108	204	9	196	3	22	0.5	13%
14	18	32.25	119	111	208	9	198	3	24	0.5	15%
15	19	32.25	122	113	208	9	198	3	24	0.5	15%
16	20	31.95	128	120	206	9	197	3	26	0.5	13%
17	21	34.01	128	113	206	9	197	3	24	0.5	15%
18	22	32.25	122	113	202	9	193	3	24	0.5	15%
19	23	32.25	118	111	211	9	202	4	22	0.5	13%
20	24	31.95	128	120	208	7	201	4	24	0.5	16%
21	25	32.25	113	105	208	9	199	3	22	0.4	13%
22	26	34.01	122	108	208	7	201	4	22	0.5	13%
23	27	32.25	126	116	202	7	195	3	26	0.4	13%
24	28	31.66	126	118	208	9	199	3	22	0.5	14%
25	29	31.07	122	118	204	9	195	3	22	0.5	14%
26	30	32.25	122	113	208	9	199	3	22	0.5	14%
27	31	32.25	136	118	208	9	199	3	34	0.6	16%
28	32	31.07	135	121	208	9	199	3	30	0.6	13%
29	33	31.07	126	121	208	9	199	3	34	0.6	16%
30	34	31.37	119	114	208	9	197	3	34	0.6	16%
31	35	32.25	113	105	208	11	197	3	24	0.5	14%
32	36	31.07	122	116	208	9	198	3	24	0.5	16%
33	37	31.07	122	118	208	9	198	3	24	0.5	16%
34	38	31.95	122	115	208	9	199	3	22	0.5	14%
35	39	33.13	116	105	208	9	199	3	22	0.4	13%
36	40	31.07	132	115	211	9	202	4	34	0.6	15%
37	41	31.07	113	108	208	9	197	3	34	0.5	14%
38	42	31.95	128	120	208	9	198	3	32	0.5	14%
39	43	32.25	122	113	208	11	195	3	32	0.5	14%
40	44	31.07	128	121	208	11	197	3	36	0.6	16%
41	45	31.66	128	121	208	9	197	3	24	0.5	16%
42	46	31.66	119	113	208	9	198	3	24	0.5	15%
43	47	31.66	122	116	208	9	198	3	26	0.6	16%
44	48	31.07	116	112	208	9	197	3	24	0.5	15%
45	49	31.07	122	118	208	7	201	4	22	0.5	14%
46	50	32.25	126	119	208	9	199	3	24	0.5	16%
47	51	31.66	122	115	211	11	200	4	24	0.5	15%
48	52	31.07	116	112	208	9	199	3	24	0.5	15%
49	53	31.07	119	115	208	9	199	3	32	0.5	14%
50	54	31.66	122	115	208	9	198	3	34	0.5	15%
51	55	32.25	119	111	208	9	198	3	24	0.5	15%
52	56	32.25	126	116	211	7	204	4	22	0.5	14%
53	57	32.25	131	124	208	7	201	4	24	0.6	16%

Milling Research Center
 DOE 3-3/8 in. 4/5 multi-lube motor--Flex Shaft
 Test Time: 14:42:30.64
 Test date: August 4, 1988

Pt. No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 30 gpm (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)
54	59	31.07	128	124	211	9	202	4	24	0.6	15%
55	59	31.07	119	115	208	9	199	3	22	0.6	14%
56	60	31.07	122	118	208	9	199	3	24	0.6	15%
57	61	31.07	129	121	210	9	201	9	26	0.6	17%
58	62	31.05	128	117	208	9	199	3	22	0.6	14%
59	63	31.07	122	118	211	9	202	4	24	0.6	15%
60	64	32.25	119	111	211	9	202	4	28	0.6	17%
61	65	33.13	119	108	211	11	200	4	28	0.6	15%
62	66	31.86	122	115	211	9	202	4	28	0.6	17%
63	67	31.86	122	115	211	11	200	4	28	0.6	16%
64	68	32.25	119	111	211	7	204	4	24	0.6	14%
65	69	32.25	128	115	211	9	202	4	26	0.6	16%
66	70	33.13	122	110	211	9	202	4	28	0.6	17%
67	71	34.01	119	105	211	7	204	4	28	0.6	16%
68	72	31.08	122	116	213	7	206	4	28	0.6	16%
69	73	32.25	113	106	211	11	200	4	28	0.6	16%
70	74	31.07	122	118	211	9	202	4	30	0.7	16%
71	75	31.07	128	124	215	9	208	4	30	0.7	20%
72	76	33.65	122	118	213	7	208	4	32	0.7	20%
73	77	31.07	119	115	217	9	208	4	30	0.7	18%
74	78	31.07	119	115	215	9	206	4	34	0.7	21%
75	79	31.07	116	112	221	9	212	4	40	0.9	23%
76	80	31.07	122	118	227	9	218	4	40	0.9	24%
77	81	31.07	125	121	233	9	224	4	43	1.0	25%
78	82	35.49	122	120	243	9	234	4	57	1.3	32%
79	83	31.07	128	124	254	9	245	4	71	1.7	39%
80	84	31.07	119	115	278	9	269	9	78	1.7	35%
81	85	30.2	116	115	288	9	279	9	92	2.0	41%
82	86	29.9	119	119	309	9	296	8	108	2.4	46%
83	87	30.2	116	115	321	12	308	8	119	2.6	48%
84	88	29.9	113	113	348	7	333	8	135	2.9	50%
85	89	30.2	116	115	362	9	343	6	144	3.2	53%
86	90	29.9	116	116	368	7	351	6	153	3.5	56%
87	91	30.49	116	114	375	9	366	6	164	3.6	58%
88	92	30.49	116	114	383	9	366	7	179	3.9	58%
89	93	29.9	116	116	403	7	396	7	181	4.2	61%
90	94	29.9	116	118	414	9	405	7	193	4.3	63%
91	95	29.32	119	122	420	11	409	7	196	4.3	63%
92	96	30.49	119	117	438	9	429	8	208	4.6	64%
93	97	32.25	119	111	438	9	429	8	218	4.6	64%
94	98	29.9	116	118	451	9	442	8	227	5.0	65%
95	99	30.2	119	118	453	7	446	8	226	5.1	65%
96	100	29.2	119	118	467	9	458	8	231	5.2	65%
97	101	30.49	116	114	465	9	458	9	237	5.2	65%
98	102	30.2	119	118	473	9	464	8	241	5.4	67%
99	103	32.25	113	105	475	9	466	8	247	4.9	64%
100	104	29.9	119	119	485	9	478	8	249	5.7	68%
101	105	30.49	119	117	489	11	478	8	247	5.6	68%
102	106	29.9	116	118	492	9	483	8	257	5.7	67%
103	107	30.2	119	118	498	9	487	9	262	5.9	68%
104	108	31.37	119	114	500	9	491	9	268	5.8	67%
105	109	30.2	119	119	512	11	501	9	272	6.1	70%
106	110	30.2	119	119	512	9	503	9	273	6.1	70%
107	111	30.2	119	118	515	9	507	9	272	6.1	69%

Grinding Research Center

DGE 3-3/8 in. 400 multistage motor-Plan Shear

Test Time: 14:42:30.84

Test date: August 4, 1985

Pt. No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 30 gpm (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (Hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)
108	112	34.01	119	105	514	9	505	9	284	5.7	64%
109	113	30.2	122	121	534	9	515	9	268	6.5	73%
110	114	30.2	119	118	518	9	509	9	287	6.5	73%
111	115	29.9	119	119	531	9	522	9	284	6.5	71%
112	116	30.2	118	115	535	9	526	9	286	6.3	68%
113	117	30.2	119	118	539	9	530	9	287	6.5	70%
114	118	30.2	116	115	541	9	532	9	301	6.6	71%
115	119	30.2	116	113	537	9	528	9	299	6.6	71%
116	120	29.9	116	115	555	7	548	10	301	6.7	70%
117	121	29.32	113	117	557	7	569	10	305	6.8	70%
118	122	29.32	113	116	572	7	585	10	311	6.8	69%
119	123	33.32	115	118	569	9	560	10	322	7.3	74%
120	124	29.32	116	119	572	11	561	10	321	7.3	75%
121	125	29.32	116	119	582	9	573	10	328	7.4	74%
122	126	29.02	113	117	582	7	575	10	330	7.3	73%
123	127	29.02	116	120	590	9	583	10	339	7.5	74%
124	128	29.32	115	119	590	9	581	10	332	7.5	74%
125	129	29.02	116	120	592	9	593	10	348	7.9	77%
126	130	29.32	115	119	600	9	591	10	355	8.0	77%
127	131	29.32	113	118	606	9	597	10	363	7.8	74%
128	132	29.32	113	118	615	7	608	11	353	7.8	73%
129	133	29.32	115	113	613	9	604	11	357	7.7	72%
130	134	29.32	110	113	633	7	626	11	363	7.8	71%
131	135	29.32	110	113	627	9	618	11	369	7.9	73%
132	136	29.32	110	113	623	9	614	11	377	8.1	75%
133	137	31.07	110	105	637	9	628	11	380	7.7	70%
134	138	29.02	116	129	633	12	631	11	390	8.7	80%
135	139	29.32	116	119	647	9	638	11	380	8.8	77%
136	140	29.02	113	117	648	12	636	11	384	8.8	77%
137	141	29.02	113	117	660	11	639	11	386	8.8	76%
138	142	29.9	116	118	664	9	655	11	392	8.7	75%
139	143	29.02	113	117	664	9	655	11	392	8.8	77%
140	144	29.32	113	118	670	9	661	12	400	8.9	78%
141	145	29.32	116	119	664	9	655	11	406	9.2	80%
142	146	29.32	116	119	683	9	673	12	413	9.3	79%
143	147	25.9	119	119	689	11	689	12	421	9.5	79%
144	148	29.61	116	118	695	9	696	12	423	9.5	79%
145	149	27.65	110	118	697	9	698	12	427	9.9	80%
146	150	25.09	105	121	701	9	692	12	431	9.9	82%
147	151	25.09	105	121	713	9	704	12	435	10.0	81%
148	152	25.8	105	122	719	11	730	12	442	10.3	83%
149	153	25.09	105	121	723	11	713	12	446	10.3	82%
150	154	26.35	99	113	739	9	721	13	446	9.5	76%
151	155	26.38	105	119	738	7	731	13	453	10.4	81%
152	156	27.26	108	119	746	11	735	13	458	10.4	81%
153	157	28.67	110	122	750	12	738	13	462	10.8	83%
154	158	27.26	108	119	764	9	745	13	466	10.5	81%
155	159	26.97	108	120	758	9	749	13	471	10.8	82%
156	160	25.68	105	118	762	9	753	13	471	10.6	80%
157	161	25.97	108	120	764	11	753	13	477	10.9	83%
158	162	26.97	105	117	769	9	760	13	481	10.7	80%
159	163	23.14	105	115	773	9	764	13	485	10.6	80%
160	164	27.35	110	118	779	9	770	13	489	11.1	83%
161	165	25.02	113	117	783	11	772	14	504	11.2	83%

Grinding Research Center

DCM 3-3/8 in. 4.5 mhp motor-Flex Shaft

Test Time: 14:42:30.64

Test Date: August 4, 1995

Pt. No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 20 gpm (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)
182	166	29.32	113	116	785	7	778	14	504	11.1	81%
183	167	29.32	116	118	789	9	780	14	504	11.4	83%
184	168	30.2	118	118	783	9	784	14	504	11.3	83%
186	168	29.9	119	119	783	11	782	14	495	11.3	82%
186	170	30.2	119	118	795	9	786	14	495	11.1	81%
187	171	32.25	119	111	795	11	784	14	497	10.9	78%
188	172	30.2	116	116	797	9	788	14	502	11.0	80%
189	173	31.37	113	109	795	13	784	14	508	10.8	77%
179	174	29.9	116	116	799	9	790	14	504	11.3	81%
171	175	30.2	118	118	805	9	798	14	508	11.7	86%
172	176	30.2	116	116	805	7	798	14	504	11.1	79%
173	177	31.66	116	110	805	9	793	14	518	11.8	78%
174	178	29.9	116	116	807	11	796	14	529	11.9	83%
175	179	29.9	116	116	814	8	805	14	524	11.8	82%
176	180	36.3	116	115	812	9	803	14	522	11.9	81%
177	181	35.49	116	114	816	9	807	14	518	11.2	79%
178	182	29.9	118	118	816	9	807	14	518	11.8	81%
179	183	29.9	118	113	824	9	815	14	524	11.3	79%
180	184	29.32	110	111	828	9	817	14	521	11.4	80%
181	185	29.32	110	114	834	11	823	14	547	11.8	82%
182	185	28.14	119	117	847	9	838	15	549	12.3	84%
183	187	27.36	118	126	863	11	852	15	557	13.4	86%
184	188	31.67	122	118	879	7	872	15	574	12.9	84%
185	189	35.18	133	113	892	11	881	15	578	12.3	80%
186	190	36.84	139	113	900	11	889	15	580	12.6	81%
187	191	38.11	139	109	904	7	897	15	583	12.1	77%
188	192	38.7	142	110	908	11	897	15	590	12.4	78%
189	193	38.11	138	107	910	9	901	15	586	11.8	76%
190	194	38.11	138	106	918	7	911	15	595	12.3	78%
191	195	38.11	138	107	920	9	911	15	592	12.1	76%
192	196	38.30	135	104	926	7	919	15	605	12.0	74%
193	197	38.11	138	109	929	9	925	15	601	12.5	78%
194	198	38.11	136	107	937	7	930	15	609	12.4	76%
195	199	38.34	139	113	941	7	934	15	611	13.1	80%
196	200	38.11	136	107	947	9	938	15	619	12.6	77%
197	201	37.23	136	110	951	11	940	15	619	12.9	79%
198	202	37.23	136	110	957	9	948	17	620	13.1	79%
199	203	38.34	133	108	961	9	952	17	624	13.8	77%
200	204	38.34	133	108	966	9	958	17	626	13.1	78%
201	205	46.16	139	104	973	11	961	17	632	12.5	74%
202	206	38.34	133	108	976	11	965	17	643	13.2	78%
203	207	38.34	130	106	984	9	975	17	644	12.9	76%
204	208	38.06	130	108	992	9	983	17	652	13.4	78%
205	209	38.35	133	110	1000	11	988	17	659	13.8	80%
206	210	37.23	133	107	1004	9	995	17	652	13.3	78%
207	211	38.11	133	105	1002	11	981	17	661	13.7	76%
208	212	38.34	130	106	1004	9	996	17	638	13.2	76%
209	213	38.35	125	103	1009	7	1002	18	663	13.0	74%
210	214	38.34	125	103	1015	9	1008	18	665	12.9	73%
211	215	34.89	122	105	1013	9	1004	18	663	13.2	75%
212	216	35.18	122	104	1011	9	1013	18	667	13.2	75%
213	217	36.35	128	106	1011	9	1013	18	671	13.5	77%
214	218	36.18	125	107	1017	9	998	17	663	13.5	77%
215	219	34.89	125	107	1004	11	991	17	659	13.5	78%

Drilling Research Center
DOE 3-3/8 in. 4/5 multi-cube motor-Flex Shaft
Test Time: 14:42:31.64
Test date: August 4, 1995

Pt. No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 30 gpm (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)
216	225	34.89	128	110	1004	7	997	17	665	13.8	50%
217	221	34.01	122	108	1007	8	999	17	668	13.6	78%
218	222	33.43	119	107	1007	7	1000	18	663	13.5	77%
219	223	34.89	122	105	1011	11	1000	18	659	13.2	75%
220	224	34.3	119	104	1011	8	1002	18	667	13.2	75%
221	225	33.13	119	103	1013	8	1004	18	671	13.8	79%
222	226	32.83	116	102	1019	9	1015	18	675	13.5	77%
223	227	33.13	113	102	1023	9	1014	18	677	13.2	74%
224	228	33.13	113	102	1029	9	1020	18	677	13.2	74%
225	229	33.13	113	102	1035	9	1026	18	675	13.2	74%
226	230	34.01	118	102	1039	9	1030	18	679	13.2	73%
227	231	32.42	113	101	1041	11	1030	18	684	13.2	73%
228	232	31.13	118	105	1045	11	1034	18	692	13.8	76%
229	233	34.01	118	103	1045	9	1036	18	696	13.6	75%
230	234	32.43	113	103	1048	9	1039	18	698	13.7	75%
231	235	32.35	110	103	1058	9	1049	18	706	13.8	76%
232	236	32.54	110	101	1069	11	1057	18	702	13.6	73%
233	237	32.83	110	101	1074	9	1065	19	704	13.8	73%
234	238	32.83	105	98	1079	7	1071	19	712	13.0	69%
235	239	31.07	105	101	1089	12	1077	19	721	13.8	74%
236	240	32.25	99	92	1101	11	1090	19	728	12.7	66%
237	241	32.54	105	87	1111	9	1102	19	727	13.4	69%
238	242	32.83	110	101	1113	9	1104	19	733	14.0	73%
239	243	38.35	113	93	1109	9	1100	19	733	13.8	69%
240	244	33.42	113	101	1107	9	1098	19	728	14.0	73%
241	245	33.13	113	102	1109	11	1088	19	729	14.2	74%
242	246	33.13	105	95	1113	11	1102	19	729	13.2	66%
243	247	29.9	83	83	1125	11	1114	19	743	13.2	66%
244	248	31.07	83	80	1148	9	1139	20	743	13.7	69%
245	249	31.07	89	85	1164	9	1155	20	752	13.7	68%
246	250	31.56	93	85	1179	9	1168	20	750	13.6	62%
247	251	31.13	93	85	1179	11	1168	20	750	13.0	64%
248	252	34.01	108	95	1175	12	1163	20	764	13.9	68%
249	253	33.13	99	90	1173	11	1162	20	760	13.0	64%
250	254	33.42	99	89	1175	11	1164	20	768	13.0	64%
251	255	31.37	88	84	1191	9	1182	21	768	12.3	60%
252	256	31.07	91	88	1206	11	1195	21	772	12.8	59%
253	257	33.13	89	90	1206	7	1189	21	775	13.2	63%
254	258	33.13	96	87	1210	11	1199	21	779	12.8	61%
255	259	36.54	113	82	1199	9	1190	21	783	13.7	66%
256	260	36.35	113	93	1179	11	1188	20	774	13.7	67%
257	261	36.35	119	96	1164	9	1155	20	764	13.9	69%
258	262	34.01	102	90	1158	11	1147	20	756	13.0	65%
259	263	31.37	93	89	1168	9	1156	20	762	12.9	64%
260	264	32.25	93	87	1177	9	1168	20	764	13.8	62%
261	265	33.13	91	82	1195	9	1185	21	772	12.1	58%
262	266	32.25	88	82	1203	9	1194	21	768	12.0	57%
263	267	33.83	99	90	1204	9	1182	21	783	13.5	65%
264	268	34.01	113	100	1193	9	1186	21	783	14.6	73%
265	269	36.35	118	95	1171	11	1160	20	772	14.1	69%
266	270	35.18	102	87	1167	11	1156	20	768	12.7	63%
267	271	32.35	93	87	1169	9	1160	20	766	12.6	62%
268	272	31.07	88	85	1185	12	1173	21	775	12.5	61%
269	273	26.14	71	76	1228	8	1219	21	803	11.6	54%

Grilling Research Center

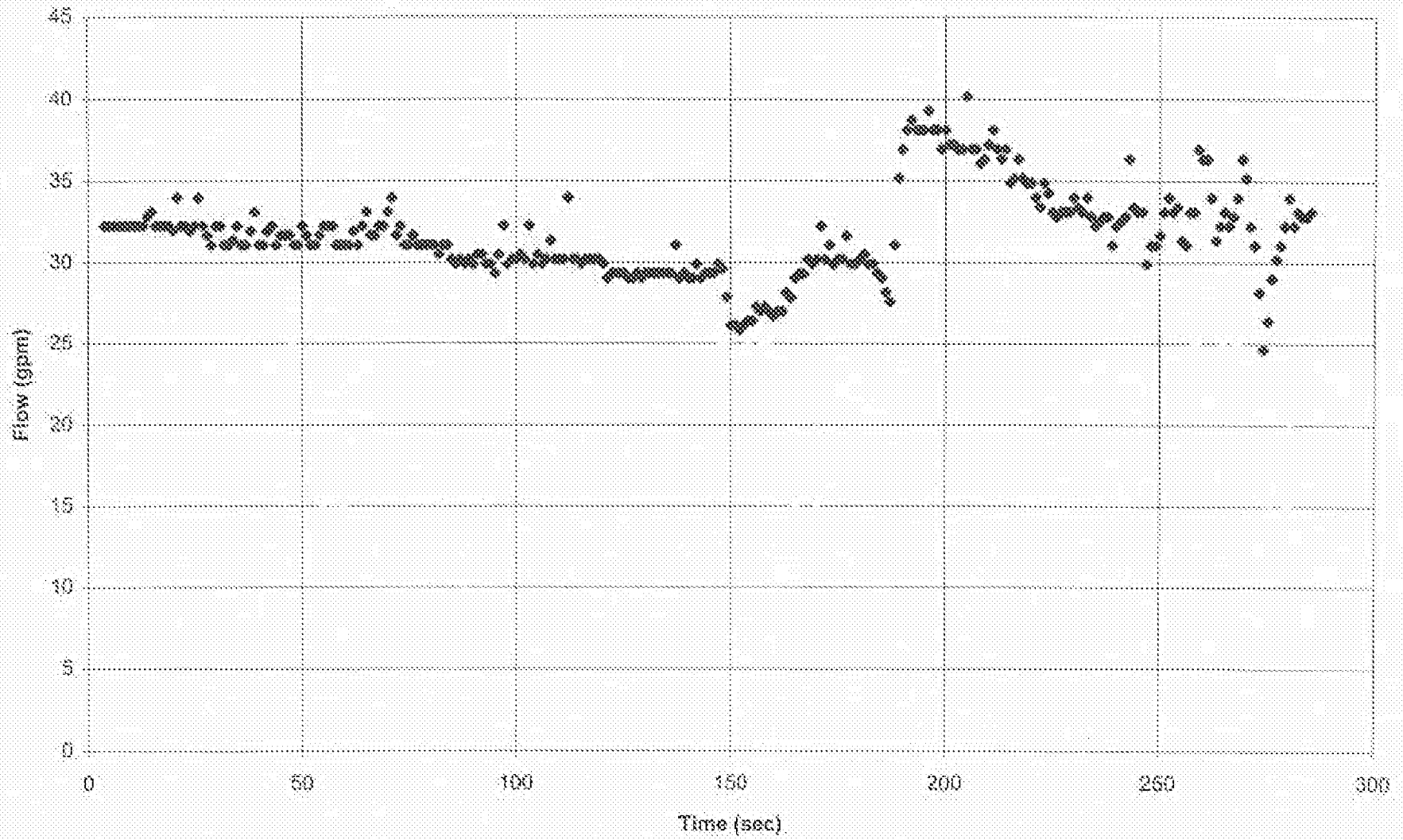
OCIE 3-3/8 in. 4/5 horsepower motor-Flex Shaft

Test Time: 14-42:30.64

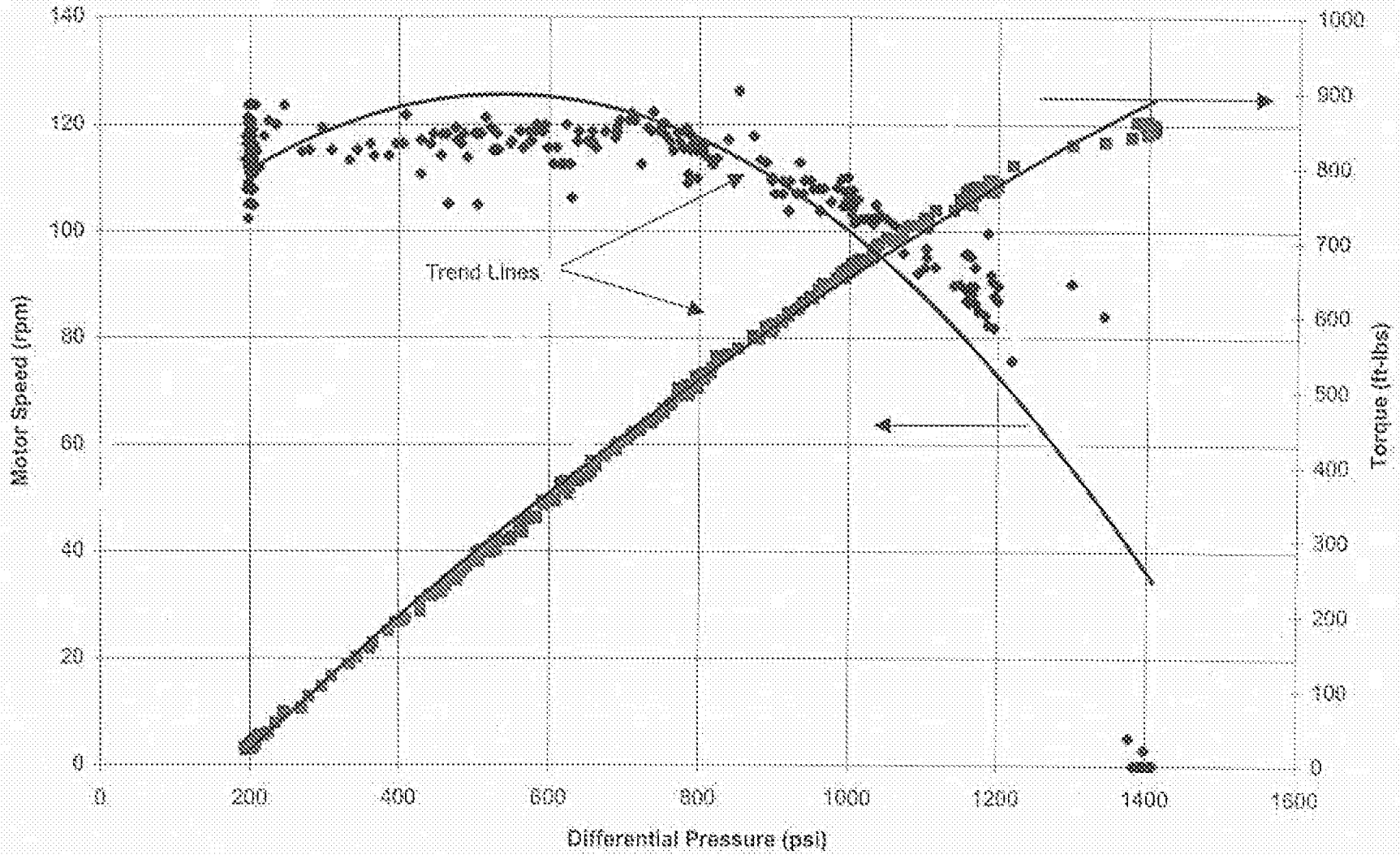
Test date: August 4, 1985

PL. No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 30 gpm (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)
270	274	24.83	74	50	1315	11	1299	23	830	13.2	63%
271	275	26.38	74	54	1351	9	1342	23	834	13.4	57%
272	276	28.02	5	5	1396	9	1377	24	841	13.8	3%
273	277	30.2	0	0	1435	7	1436	24	845	13.5	2%
274	278	31.07	0	0	1417	11	1406	25	848	13.9	0%
275	279	32.25	0	0	1419	11	1408	25	853	14.0	0%
276	280	34.03	0	0	1417	11	1406	25	857	14.0	0%
277	281	32.25	0	0	1415	11	1404	25	857	14.0	0%
278	282	33.13	0	0	1408	11	1398	24	861	14.0	0%
279	283	32.83	0	0	1404	9	1395	24	857	14.0	0%
280	284	32.83	0	0	1400	9	1321	24	861	14.0	0%
281	285	33.13	0	0	1396	12	1384	24	861	14.0	0%

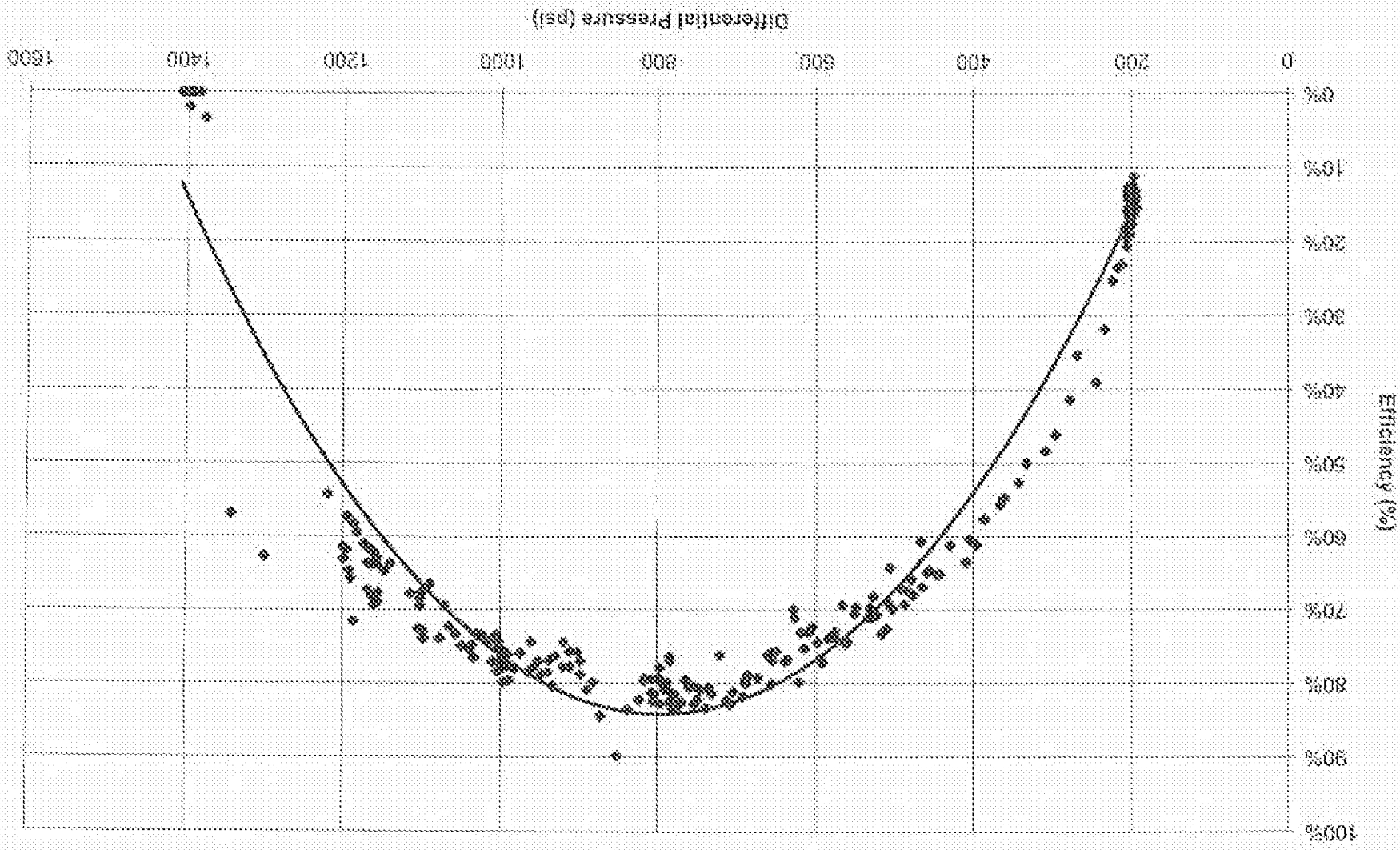
Mud Flow vs Time
30 gpm ~ Flex Shaft



Motor Speed and Torque vs Differential Pressure
30 gpm – Flex Shaft



Motor Efficiency vs Differential Pressure
30 gpm -- Flex Shaft



Drilling Research Center
 BDE J-311 in. 40 multistroke motor - Flex Shaft
 Test No.: 1628-18-58
 Test date: August 4, 1995

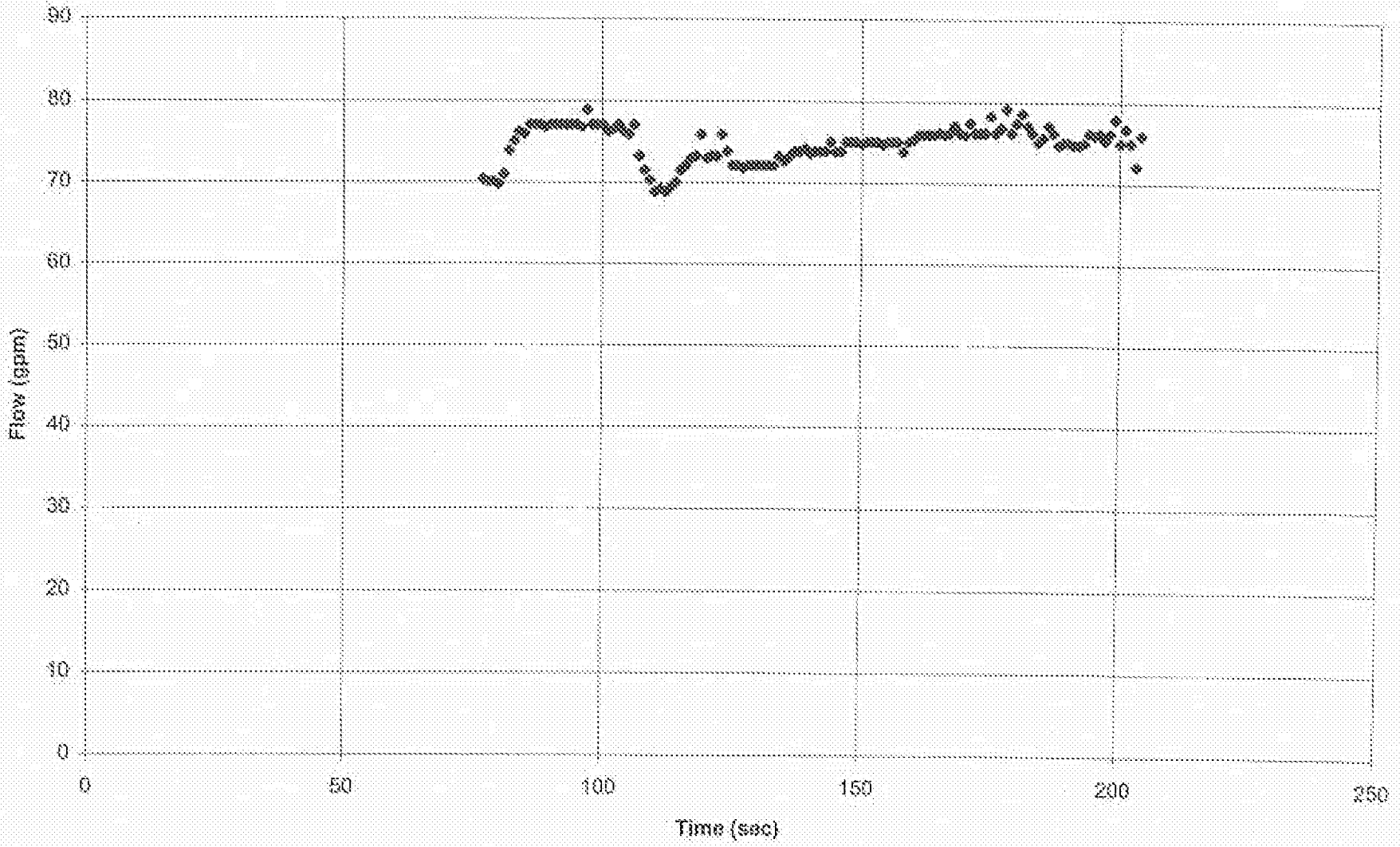
Pt. No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 70 gpm (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)
72	77	78.26	267	284	313	9	304	12	32	1.5	12%
73	78	70.67	255	253	313	9	304	12	34	1.8	13%
74	79	70.67	255	251	313	9	306	13	34	1.8	13%
75	80	69.77	255	255	313	9	304	12	38	1.8	14%
76	81	71.84	261	258	323	9	314	13	36	1.8	14%
77	82	73.88	287	283	327	7	320	13	38	1.7	13%
78	83	75.88	272	254	332	5	327	13	32	1.5	12%
79	84	76.29	275	290	332	7	325	13	39	1.4	13%
80	85	75.93	272	281	336	7	328	13	32	1.5	11%
81	86	77.1	278	272	338	6	331	14	34	1.8	12%
82	87	77.1	278	252	334	7	327	13	32	1.5	12%
83	88	77.1	278	252	334	9	325	13	34	1.6	12%
84	89	76.31	287	282	338	8	333	14	36	1.8	13%
85	90	77.1	278	252	340	9	331	14	40	1.8	14%
86	91	77.1	287	281	338	9	327	13	40	2.0	15%
87	92	77.1	278	252	338	9	330	13	38	1.8	14%
88	93	77.1	278	252	340	7	333	14	36	1.7	13%
89	94	77.1	278	252	344	7	337	14	42	2.1	15%
90	95	77.1	278	252	348	7	341	14	43	2.1	15%
91	96	76.81	281	268	350	9	343	14	47	2.3	16%
92	97	78.88	278	247	358	8	351	14	49	2.3	16%
93	98	77.1	278	252	358	8	353	14	50	2.6	18%
94	99	77.1	278	252	364	8	359	15	50	2.8	19%
95	100	77.1	281	285	379	4	379	15	71	3.4	23%
96	101	78.23	278	258	389	7	392	18	56	4.2	26%
97	102	79.51	272	245	412	9	403	16	58	4.6	28%
98	103	77.1	275	280	430	7	423	17	115	5.5	32%
99	104	76.32	275	283	457	8	453	15	133	6.4	35%
100	105	75.93	272	251	477	3	488	12	142	7.1	37%
101	106	77.1	278	252	482	9	483	20	103	7.3	36%
102	107	73.29	264	252	438	9	487	20	121	8.7	44%
103	108	71.53	255	250	506	7	501	20	150	9.4	46%
104	109	70.36	250	243	518	8	509	21	200	9.9	47%
105	110	69.69	251	257	531	7	524	21	215	10.7	50%
106	111	69.19	247	258	643	7	638	22	237	11.3	52%
107	112	68.89	244	243	658	7	652	23	245	11.8	51%
108	113	69.46	247	249	675	8	667	23	257	12.2	53%
109	114	70.07	253	259	694	7	687	24	268	12.9	54%
110	115	71.53	264	258	698	8	693	24	276	13.0	55%
111	116	72.12	261	252	621	7	614	25	282	13.5	54%
112	117	73	261	288	637	7	633	26	287	13.7	55%
113	118	73.29	261	249	648	7	641	26	299	14.2	54%
114	119	75.05	264	243	685	8	646	27	309	14.3	54%
115	120	78	267	258	670	8	661	27	322	15.7	58%
116	121	78.99	264	282	684	6	679	28	333	15.8	57%
117	122	73.29	261	248	638	6	664	28	348	16.1	57%
118	123	75.05	261	241	717	6	708	28	363	16.2	58%
119	124	73.89	258	249	726	5	723	30	369	17.2	60%
120	125	72.12	258	250	748	6	743	30	383	18.2	60%
121	126	72.12	255	248	771	8	762	31	402	18.6	61%
122	127	71.63	258	251	795	8	788	32	413	20.1	62%
123	128	72.12	261	253	812	7	805	33	425	21.0	62%
124	129	72.12	259	280	832	7	825	34	432	21.6	64%
125	130	72.12	258	248	855	9	846	35	470	22.1	64%
126	131	73.12	258	258	879	7	872	36	489	23.8	65%
127	132	72.12	258	252	892	7	895	37	502	24.2	66%
128	133	72.12	251	248	926	7	949	38	525	24.8	66%
129	134	73.39	258	248	951	7	944	38	543	25.5	68%

Drilling Research Center
 DCE 8-38 w/ 4.5 multi-bore motor-Flex Shank
 Test Time: 16:28:16.38
 Test date: August 4, 1995

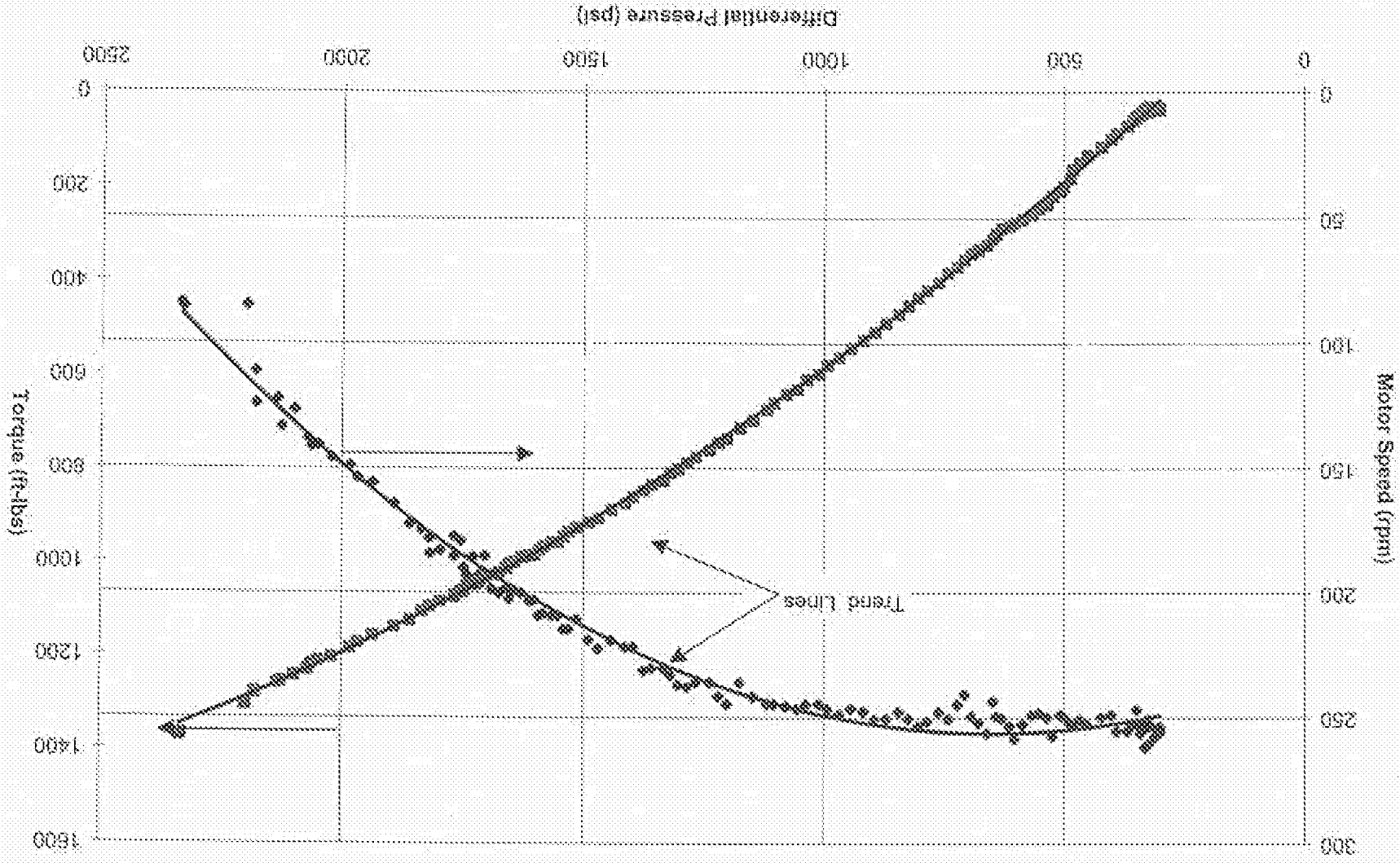
FR No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 70 gpm (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)
130	135	72.7	260	248	976	7	969	40	582	38.0	67%
131	136	73.29	260	248	1000	7	993	43	578	37.1	67%
132	137	73.88	259	244	1049	9	1040	43	597	37.6	67%
133	138	73.88	258	244	1043	7	1036	42	609	38.3	67%
134	139	74.37	251	246	1084	9	1075	43	608	38.3	68%
135	140	73.94	258	249	1088	9	1077	44	609	38.9	68%
136	141	73.88	258	244	1109	7	1102	46	609	38.7	68%
137	142	73.88	280	244	1125	9	1116	48	673	31.3	68%
138	143	73.88	265	249	1152	7	1145	47	688	32.0	68%
139	144	75.05	253	238	1179	7	1172	49	713	32.0	67%
140	145	73.88	258	244	1206	7	1199	49	739	34.3	70%
141	146	73.88	256	242	1234	7	1217	50	744	34.2	69%
142	147	75.05	250	236	1248	8	1239	58	708	34.1	68%
143	148	75.05	253	238	1273	8	1264	53	774	34.9	67%
144	149	75.05	259	238	1292	9	1283	53	787	35.6	69%
145	150	74.76	259	237	1308	7	1301	55	801	35.1	68%
146	151	75.05	250	233	1329	7	1317	54	808	35.9	67%
147	152	75.05	247	230	1341	9	1332	54	826	36.3	67%
148	153	75.05	247	230	1383	7	1358	55	834	36.6	68%
149	154	74.76	247	231	1389	9	1373	56	847	37.3	67%
150	155	75.05	228	222	1424	9	1385	57	864	36.4	64%
151	156	75.05	238	222	1431	9	1412	58	874	36.9	64%
152	157	75.05	238	219	1448	7	1441	58	889	37.1	62%
153	158	73.88	237	223	1476	9	1469	60	907	38.5	64%
154	159	75.05	237	219	1489	8	1480	61	915	38.2	63%
155	160	75.34	237	211	1529	9	1514	62	927	37.2	60%
156	161	75.05	233	215	1538	7	1531	63	936	38.3	61%
157	162	75.05	233	215	1550	8	1541	63	946	38.7	61%
158	163	75.33	227	209	1562	9	1559	63	958	38.2	60%
159	164	75.93	227	209	1575	8	1568	64	958	38.2	60%
160	165	76.22	227	209	1589	7	1582	65	967	38.4	60%
161	166	75.05	227	209	1601	9	1592	65	976	38.8	60%
162	167	75.22	221	209	1608	7	1601	65	985	38.1	60%
163	168	77.1	224	203	1620	9	1611	66	987	38.2	60%
164	169	76.22	218	200	1636	8	1627	66	990	37.7	60%
165	170	75.93	216	199	1646	7	1642	67	1000	37.6	60%
166	171	77.39	224	203	1656	7	1652	67	1004	38.7	60%
167	172	76.22	218	198	1664	7	1658	68	1014	38.3	60%
168	173	76.22	218	206	1679	7	1672	68	1023	38.8	60%
169	174	76.22	216	194	1684	7	1687	69	1029	38.9	60%
170	175	76.27	207	195	1710	9	1701	69	1035	38.5	60%
171	176	76.22	218	193	1722	9	1713	70	1043	38.3	60%
172	177	76.81	213	194	1739	8	1729	70	1047	38.7	60%
173	178	79.15	210	186	1733	7	1726	70	1056	37.1	60%
174	179	76.22	210	183	1747	9	1738	71	1056	38.6	64%
175	180	77.39	210	186	1753	7	1746	71	1062	38.8	64%
176	181	78.57	201	179	1756	7	1753	72	1066	38.3	61%
177	182	77.1	204	185	1774	8	1765	72	1072	37.8	62%
178	183	76.22	193	177	1773	7	1765	72	1076	38.2	60%
179	184	75.65	196	183	1803	8	1784	73	1086	37.8	62%
180	185	75.64	199	184	1805	7	1814	74	1095	38.4	62%
181	186	77.1	196	178	1823	6	1816	74	1097	37.2	60%
182	187	76.22	196	174	1839	7	1832	75	1107	38.6	60%
183	188	74.70	184	172	1846	9	1837	76	1126	39.9	60%
184	189	75.05	178	154	1857	7	1850	77	1140	38.4	60%
185	190	76.05	167	156	1854	9	1855	79	1159	34.4	60%
186	191	74.76	184	154	1875	9	1869	80	1174	35.3	60%
187	192	74.76	189	149	1881	9	1882	81	1186	38.6	62%
188	193	75.05	156	146	2030	8	2021	83	1206	31.9	60%
189	194	76.22	153	141	2037	7	2030	84	1213	32.6	60%

Drilling Research Center												
UDE 2-3/4 in. 475 multi-lobe motor - Flex Shaft												
Test Time: 18:26:18.88												
Test Date: August 2, 1995												
PI No	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 70 rpm (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)	
190	186	75.92	151	141	2071	7	2064	54	1221	32.8	38%	
191	199	78.22	156	148	2080	8	2071	55	1260	32.9	38%	
192	197	75.34	136	128	2105	8	2099	58	1214	29.9	35%	
193	198	75.22	145	133	2135	9	2128	57	1256	31.5	37%	
194	199	77.98	138	122	2143	9	2134	57	1250	29.3	34%	
195	200	78.05	119	111	2150	9	2141	55	1279	27.0	30%	
196	201	76.81	136	124	2158	7	2151	55	1284	34.2	34%	
197	202	75.86	91	85	2206	8	2200	50	1305	21.1	23%	
198	203	72.12	88	85	2240	8	2231	48	1308	22.2	23%	
199	204	75.93	91	84	2248	11	2235	45	1372	21.8	22%	

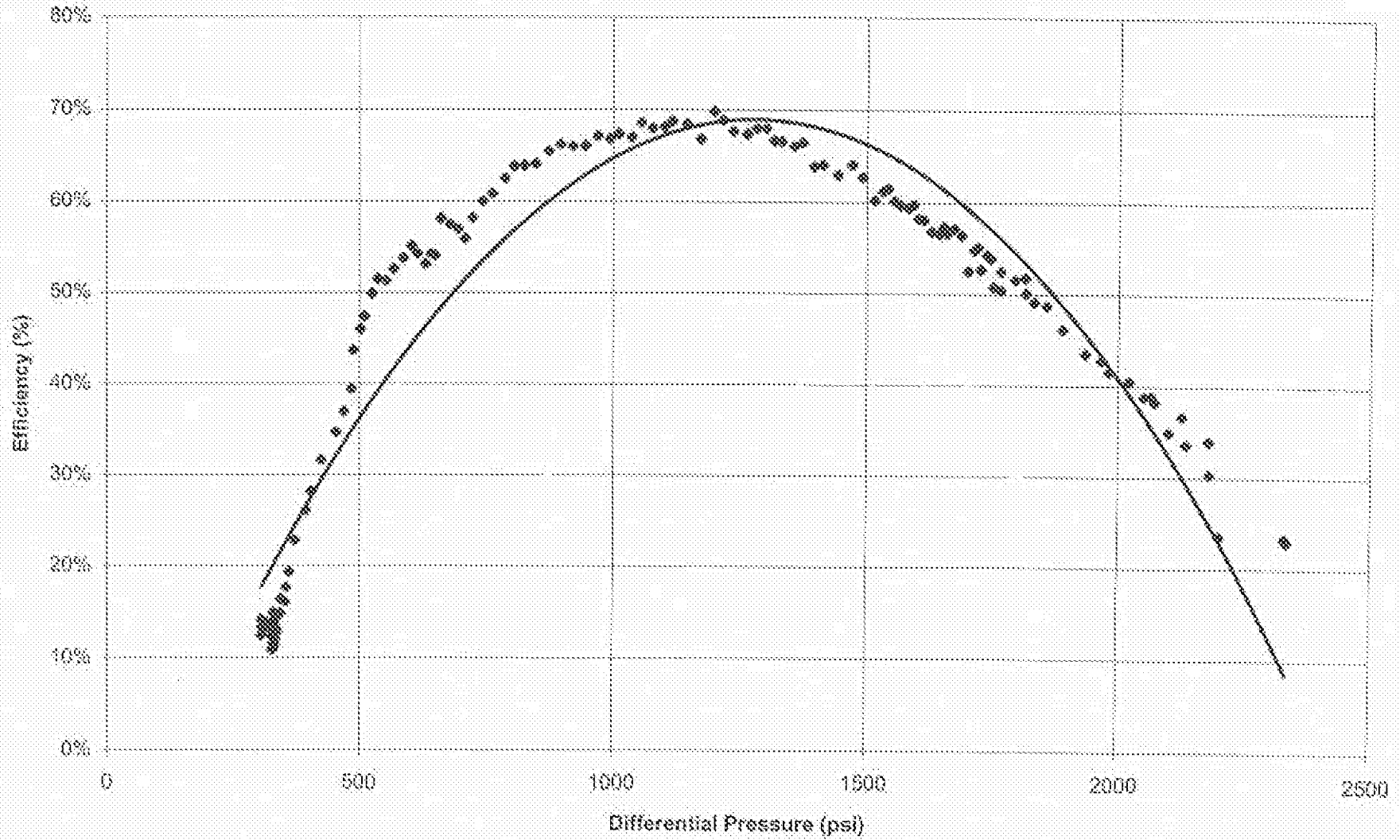
Mud Flow vs Time
70 gpm - Flex Shaft



Motor Speed and Torque vs Differential Pressure
70 gpm -- Flex Shaft



Motor Efficiency vs Differential Pressure
70 gpm -- Flex Shaft

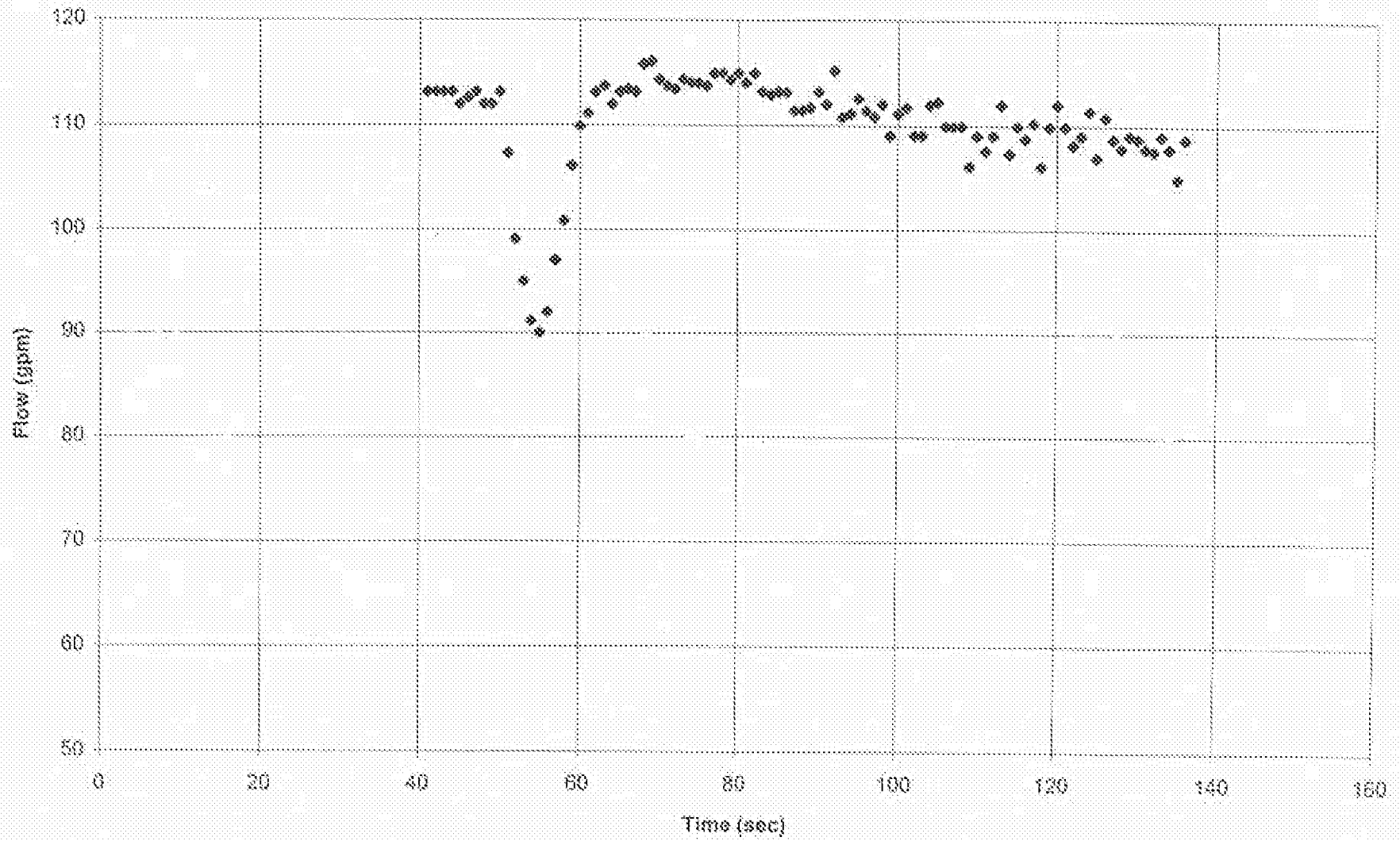


Drilling Research Center												
DOE 3-30 in. 4/5 multi-hole motor-Flex Shaft												
Test Time: 16:31:12.58												
Test date: August 4, 1995												
Pt. No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 110 (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)	
0	41	113.16	412	400	504	9	495	32	39	3.1	10%	
1	42	113.16	412	400	508	7	499	32	38	2.9	9%	
2	43	113.16	408	398	508	9	499	32	40	3.0	9%	
3	44	113.16	412	400	512	7	505	32	43	3.2	10%	
4	45	111.99	412	405	514	7	507	33	43	3.3	10%	
5	46	112.57	412	403	516	9	507	33	45	3.4	11%	
6	47	113.16	408	398	516	9	507	33	45	3.4	10%	
7	48	111.99	409	402	524	9	515	33	49	3.7	11%	
8	49	111.99	409	402	520	9	520	33	53	4.3	14%	
9	50	113.16	412	400	526	7	552	35	52	4.2	13%	
10	51	107.3	389	389	588	9	558	36	165	3.0	22%	
11	52	99.85	358	387	590	7	563	37	160	12.1	32%	
12	53	94.98	335	388	617	7	610	38	212	15.7	40%	
13	54	91.17	324	391	670	9	661	42	252	19.5	46%	
14	55	80	324	396	732	9	723	46	309	22.8	49%	
15	56	82.95	328	404	807	9	798	51	348	26.8	52%	
16	57	87.04	348	392	879	9	870	58	388	29.0	52%	
17	58	100.85	353	398	941	9	932	60	425	32.0	54%	
18	59	106.12	363	397	1007	9	998	64	446	33.7	53%	
19	60	109.03	392	392	1050	9	1041	67	479	35.3	53%	
20	61	111.11	400	396	1087	7	1080	69	497	37.5	54%	
21	62	112.16	400	390	1111	9	1102	71	520	38.5	54%	
22	63	113.75	400	387	1140	7	1133	73	539	39.7	55%	
23	64	111.99	397	399	1169	9	1160	74	556	41.2	55%	
24	65	113.16	403	392	1197	9	1188	76	578	43.1	57%	
25	66	113.45	403	391	1218	9	1209	75	595	44.3	57%	
26	67	113.16	400	389	1238	7	1231	78	609	45.1	57%	
27	68	115.3	400	380	1261	9	1252	80	624	45.1	58%	
28	69	116.09	403	392	1288	9	1273	82	642	46.7	57%	
29	70	114.33	400	385	1314	9	1305	84	663	48.5	58%	
30	71	113.75	400	390	1329	9	1320	85	679	50.4	59%	
31	72	113.45	400	388	1351	9	1342	86	690	51.0	59%	
32	73	114.33	400	385	1379	9	1361	87	708	51.9	59%	
33	74	114.94	400	386	1398	9	1386	85	729	53.8	59%	
34	75	114.94	400	386	1419	9	1410	86	739	54.3	60%	
35	76	113.75	400	387	1439	7	1428	92	752	55.4	61%	
36	77	114.92	397	380	1462	9	1453	93	772	55.9	60%	
37	78	114.92	395	378	1480	9	1471	94	787	55.7	60%	
38	79	114.33	392	377	1509	7	1502	96	808	58.0	60%	
39	80	114.92	392	378	1536	7	1531	98	820	58.5	60%	
40	81	114.94	395	381	1562	9	1553	100	837	60.7	61%	
41	82	114.92	396	369	1591	9	1582	102	865	63.5	60%	
42	83	113.16	386	375	1624	9	1615	104	890	63.9	61%	
43	84	112.87	380	370	1659	7	1638	106	911	64.2	61%	
44	85	113.16	380	369	1696	9	1667	108	930	65.4	60%	
45	86	113.16	368	356	1698	9	1669	106	958	64.9	60%	
46	87	111.4	375	370	1776	9	1767	113	973	68.6	60%	
47	88	111.4	365	358	1807	9	1798	115	1014	69.2	60%	
48	89	111.69	363	358	1854	9	1855	119	1035	70.5	59%	
49	90	113.16	345	336	1901	9	1892	121	1082	69.0	59%	
50	91	111.99	377	370	1932	9	1923	123	1092	74.2	60%	
51	92	115.21	338	323	1919	9	1919	123	1101	67.7	56%	
52	93	110.81	332	330	2024	9	2015	129	1140	71.5	55%	
53	94	111.11	335	332	2069	7	2067	132	1155	72.9	55%	

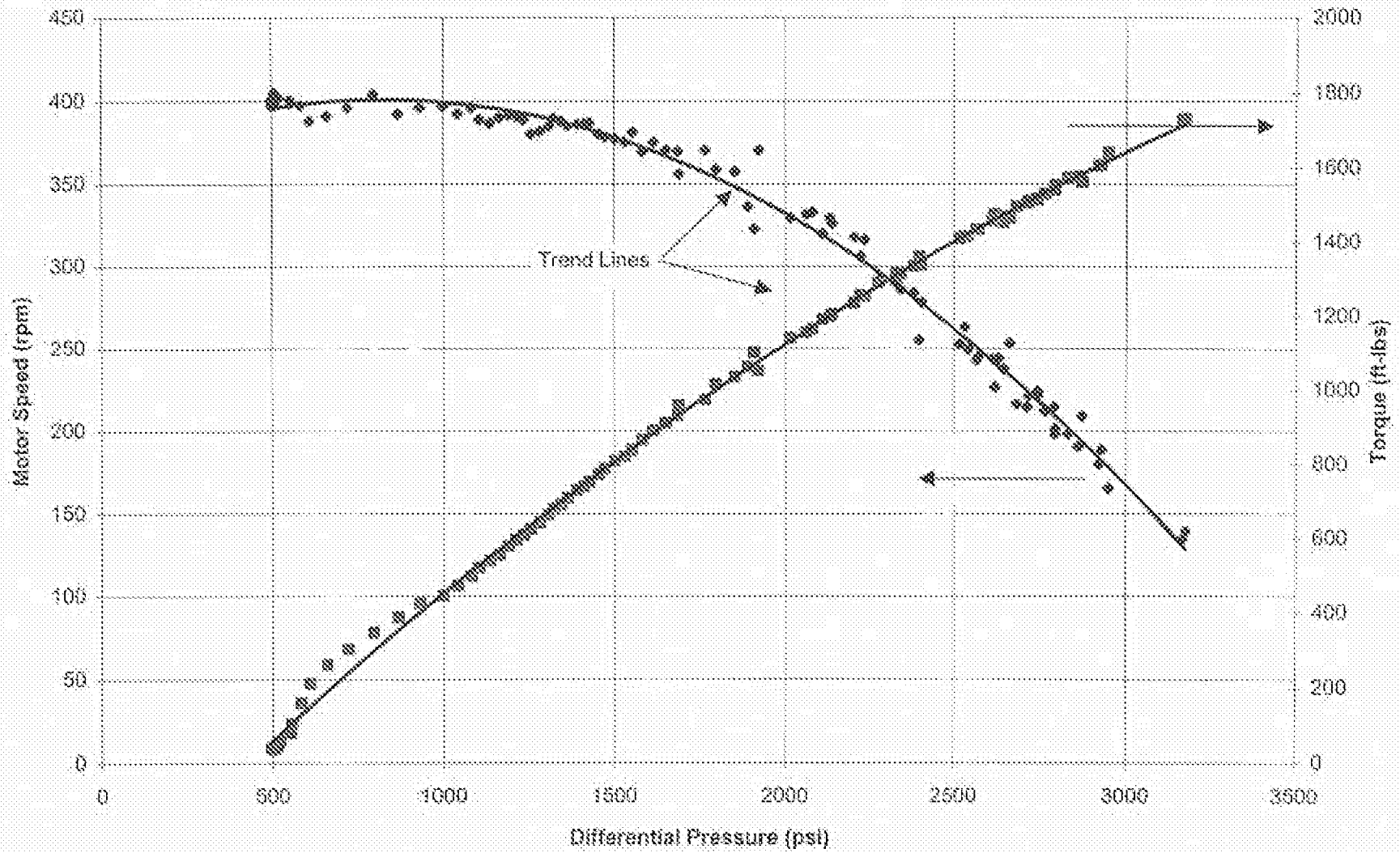
Oakley Research Center
 DOE 3-38 in 485 multiple motor-Fix Shaft
 Test Time: 16:31:12.88
 Test date: August 4, 1995

Pt. No.	Time (sec)	Flow (gpm)	Speed (rpm)	Speed Adjusted to 110 (rpm)	Input Pressure (psi)	Output Pressure (psi)	Differential Pressure (psi)	Hydraulic Horsepower (hp)	Torque (ft-lbs)	Mechanical Horsepower (hp)	Efficiency (%)
54	85	112.57	341	333	2091	9	2081	134	1165	73.9	50%
55	86	111.4	324	320	2119	9	2110	135	1190	72.5	54%
56	87	110.81	332	330	2143	11	2132	137	1188	73.2	55%
57	88	111.99	332	326	2147	9	2138	137	1205	74.8	55%
58	89	109.06	315	318	2213	9	2204	141	1236	74.8	53%
59	100	111.11	309	306	2233	11	2222	143	1256	73.2	51%
60	101	111.88	321	316	2244	9	2235	143	1262	75.4	53%
61	102	108.06	289	291	2287	11	2276	146	1291	71.7	49%
62	103	108.06	287	289	2338	9	2329	149	1314	72.4	48%
63	104	111.99	301	298	2358	7	2327	149	1286	73.0	48%
64	105	112.28	292	286	2358	11	2343	150	1314	71.8	48%
65	106	109.93	284	284	2389	11	2382	153	1335	72.2	47%
66	107	109.93	278	278	2412	9	2403	154	1337	70.8	46%
67	108	109.93	268	256	2408	11	2387	151	1300	58.1	43%
68	109	108.12	244	253	2520	11	2518	162	1408	67.9	42%
69	110	109.06	261	263	2541	9	2532	162	1415	70.9	44%
70	111	107.59	244	248	2553	11	2542	163	1415	67.2	41%
71	112	109.06	241	243	2578	9	2567	165	1434	68.4	40%
72	113	111.96	250	246	2584	11	2573	165	1434	67.0	41%
73	114	107.3	221	227	2634	11	2620	165	1475	63.8	38%
74	115	109.93	234	244	2642	11	2631	169	1493	68.3	40%
75	115	108.76	235	238	2654	9	2645	170	1483	63.8	38%
76	117	110.23	244	248	2623	9	2614	168	1459	67.8	40%
77	118	106.12	207	215	2724	11	2713	174	1508	61.5	35%
78	119	108.93	221	221	2736	12	2718	174	1511	63.5	36%
79	120	111.99	238	253	2674	11	2663	171	1465	70.7	41%
80	121	109.93	218	215	2693	11	2682	172	1495	61.3	36%
81	122	108.18	218	222	2752	9	2743	175	1517	64.5	38%
82	123	108.06	210	212	2777	11	2766	178	1531	61.7	35%
83	124	111.4	227	224	2755	11	2744	175	1515	64.7	37%
84	125	107	186	201	2806	11	2795	179	1542	59.2	33%
85	126	110.81	218	213	2804	11	2793	178	1542	63.0	36%
86	127	108.76	196	198	2806	11	2795	179	1554	58.7	33%
87	128	107.88	167	181	2873	12	2861	184	1577	57.3	31%
88	139	108.06	207	209	2884	12	2872	184	1582	62.1	34%
89	139	108.76	195	195	2939	7	2932	182	1573	59.4	31%
90	131	107.88	187	191	2873	11	2862	184	1577	57.3	31%
91	132	107.59	176	180	2931	11	2920	187	1606	55.0	29%
92	133	109.06	187	189	2935	12	2927	188	1608	57.7	31%
93	134	107.88	162	165	2950	12	2948	188	1641	51.8	27%
94	135	104.95	133	139	3165	11	3174	204	1732	46.0	23%
95	139	108.76	133	135	3177	12	3165	203	1728	44.3	22%

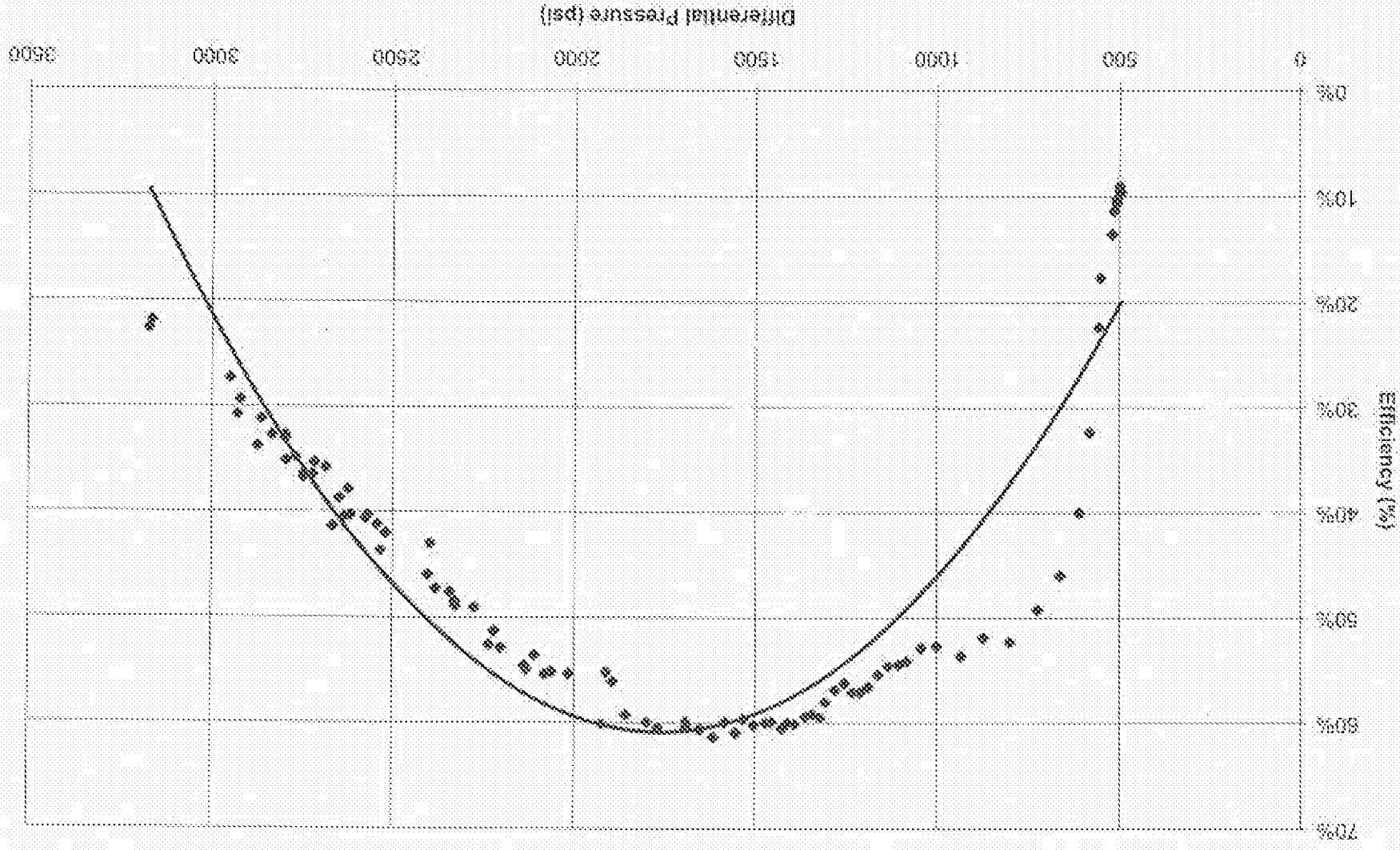
Mud Flow vs Time
110 gpm - Flex Shaft



Motor Speed and Torque vs Differential Pressure
110 gpm -- Flex Shaft



Motor Efficiency vs Differential Pressure
110 gpm -- Flex Shaft



APPENDIX B
DOE High-Power Slim-Hole System
Catoosa Field Test

- Day 1
- Day 2
- Day 3

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23		Date: 2/22/98																	
Starting Depth =	823.82	Bit Type =			Walker McDonald MP66H														
Ending Depth =	931.19	Bit Size =			4.75														
Total Depth Drilled	487.27	Bit Nozzles =			9, 9, 12, 12														
Hours On Bit =	4.09	Mud Type =			Water Based														
Average ROP =	89.58	Mud Weight (lbs/gal) =			9.09														
Drilling (ft) =	660.49	Pipe (ft) =			251.81		Casing (ft)			408.60									
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOUR	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours			
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	RRPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit			
11:35:23	823.82	105	727	381	739	757	36	17.25	1.77	0.12	0.30	1.29	1.46	89.06	3.99	0			
11:35:47	824.17	108	731	392	739	761	41	17.12	1.76	0.1	0.43	0.86	0.69	88.47	4.23	0.01			
11:36:08	824.43	107	738	389	749	761	41	17.09	1.75	0.09	0.46	0.74	0.57	42.56	4.47	0.02			
11:36:38	824.85	106	753	385	749	761	41	17.64	1.79	0.13	0.51	1.36	1.13	27.46	4.7	0.03			
11:37:08	824.83	109	753	395	742	761	36	18.68	1.75	0.08	0.57	0.91	1.01	20.83	4.88	0.03			
11:37:38	824.89	108	762	393	743	761	36	18.98	1.75	0.09	0.59	0.88	1.32	19.76	5.04	0.03			
11:38:03	825.14	106	776	386	742	761	36	18.67	1.77	0.11	0.58	1.01	0.79	17.60	5.19	0.05			
11:38:39	825.31	108	731	393	749	761	36	17	1.75	0.09	0.54	0.96	0.85	20.35	5.35	0.06			
11:38:59	825.5	108	737	392	749	761	41	17.63	1.75	0.09	0.51	0.79	0.59	23.28	5.56	0.07			
11:39:38	825.68	107	791	389	749	761	36	17.02	1.75	0.1	0.52	0.74	1.08	22.02	5.74	0.07			
11:40:09	825.85	108	737	394	741	757	32	17.03	1.75	0.09	0.52	0.77	0.67	19.81	5.9	0.08			
11:40:39	826.02	108	735	392	741	757	32	17.03	1.76	0.11	0.52	1.51	1.7	20.41	6.06	0.09			
11:41:09	826.13	108	730	393	741	761	36	17.02	1.75	0.1	0.52	0.74	0.45	14.08	6.19	0.1			
11:41:39	826.27	108	738	393	748	757	32	17.03	1.75	0.09	0.51	0.91	0.6	16.53	6.32	0.11			
11:42:08	826.4	109	730	385	742	757	32	17.04	1.75	0.09	0.51	1.51	1.22	15.58	6.48	0.11			
11:42:38	826.52	108	730	394	742	757	32	17.03	1.75	0.09	0.51	0.88	0.67	14.06	6.57	0.12			
11:43:09	826.77	107	844	391	743	761	45	18.67	1.78	0.14	0.87	1.94	1.59	40.85	6.54	0.13			
11:43:14	827.02	108	905	392	745	761	49	18.32	1.79	0.15	1.23	1.48	0.83	65.32	7.36	0.13			
11:43:28	827.27	106	881	385	748	765	32	15.91	1.8	0.16	1.64	2.11	0.86	76.42	7.31	0.13			
11:43:37	827.52	106	1062	387	748	765	36	15.07	2.7	1.67	2.38	3.97	3.09	83.79	7.57	0.14			
11:43:58	827.77	108	1094	393	742	777	88	15.8	2.72	2.14	1.64	4.5	5.07	46.45	7.51	0.14			
11:44:08	828.02	108	944	394	744	765	41	15.77	1.89	0.31	1.79	2.3	1.89	77.88	8.07	0.15			
11:44:18	828.27	108	966	392	742	761	36	15.86	1.81	0.19	2.06	2.75	1.1	89.55	8.33	0.15			
11:44:29	828.52	108	960	395	744	761	32	15.56	1.84	0.23	2.06	2.37	0.67	85.86	8.56	0.15			
11:44:38	828.77	110	953	401	745	765	36	15.56	1.81	0.22	2.09	2.25	0.5	92.11	8.84	0.16			
11:44:48	828.93	109	955	397	746	765	32	15.57	1.85	0.28	1.98	2.25	0.53	95.59	9.07	0.16			
11:44:59	829.28	108	953	393	746	765	32	15.58	1.89	0.24	1.98	2.25	0.98	88.23	9.33	0.16			
11:45:09	829.53	108	942	382	747	765	36	15.42	1.81	0.19	2.13	2.49	0.67	84.07	9.56	0.16			
11:45:20	829.78	110	958	400	747	765	32	15.13	1.81	0.19	2.42	2.88	0.55	82.97	9.85	0.17			
11:45:30	830.03	108	992	392	748	765	36	15.12	1.8	0.16	2.44	2.96	0.49	92.75	10.08	0.17			
11:45:41	830.28	108	973	393	748	765	36	15.1	1.82	0.23	2.45	2.73	0.5	83.55	10.33	0.17			
11:45:51	830.53	106	894	386	745	761	32	15.13	1.81	0.2	2.42	2.88	0.5	90.89	10.58	0.18			
11:46:01	830.78	110	873	399	746	761	36	15.08	1.82	0.22	2.68	3.54	1.32	96.96	10.93	0.18			
11:46:13	831.03	108	967	394	744	761	32	15.08	1.85	0.28	2.47	2.65	0.48	77.03	11.09	0.18			

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAR	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	%	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
11:48:23	831.28	107	969	360	744	761	36	15.1	1.81	0.19	2.46	2.66	0.65	80.67	11.33	0.19
11:48:34	831.53	106	968	366	744	765	35	15.09	1.83	0.24	2.45	3.35	2.21	81.68	11.68	0.19
11:48:45	831.78	108	980	393	744	765	41	15.11	1.88	0.28	2.44	3.49	1.7	82.82	11.84	0.19
11:48:56	832.00	106	985	368	743	761	30	15.09	1.81	0.23	2.46	3.33	1.13	83.62	12.08	0.19
11:47:08	832.26	105	971	382	742	761	36	15.08	1.8	0.19	2.47	2.75	0.53	74.83	12.33	0.2
11:47:19	832.53	106	985	388	744	763	32	15.08	1.84	0.23	2.47	2.73	0.45	81.82	12.5	0.2
11:47:30	832.78	110	981	401	744	765	41	15.08	1.8	0.18	2.48	2.85	0.82	78.26	12.82	0.2
11:47:41	833.03	108	982	392	743	761	36	15.08	1.83	0.23	2.47	2.7	0.5	79.22	13.07	0.21
11:47:52	833.28	108	982	393	743	761	36	15.09	1.85	0.26	2.46	2.7	0.53	81.53	13.55	0.21
11:48:04	833.54	108	984	392	743	765	41	15.09	1.85	0.31	2.46	2.75	0.72	77.13	13.6	0.21
11:48:15	833.79	108	981	394	743	761	36	15.09	1.86	0.25	2.46	2.75	0.57	81.56	13.84	0.22
11:48:27	834.04	107	986	388	743	761	36	15.11	1.83	0.27	2.44	2.75	0.62	80.05	14.08	0.22
11:48:38	834.29	107	987	390	744	765	41	15.1	1.87	0.3	2.44	2.75	0.62	81.36	14.33	0.22
11:48:48	834.54	106	985	384	743	761	38	15.1	1.84	0.28	2.45	2.78	0.67	82.97	14.59	0.23
11:48:01	834.78	109	986	397	743	761	45	15.1	1.85	0.37	2.46	2.79	0.62	74.54	14.84	0.23
11:49:11	835.04	110	982	399	743	761	38	15.1	1.83	0.23	2.45	2.78	0.77	85.00	15.08	0.23
11:49:23	835.28	108	978	384	741	765	41	15.1	1.81	0.19	2.45	2.68	0.53	74.58	15.35	0.24
11:49:34	835.54	108	979	363	742	761	38	15.09	1.82	0.21	2.45	2.68	0.5	80.98	15.61	0.24
11:49:45	835.79	105	979	395	742	761	39	15.11	1.85	0.22	2.44	2.78	0.62	82.54	15.86	0.24
11:49:56	836.04	108	966	354	743	761	36	15.07	1.81	0.2	2.47	2.76	0.57	78.97	16.08	0.24
11:50:06	836.29	107	975	350	743	761	36	15.13	1.81	0.22	2.41	2.73	0.6	80.78	16.35	0.25
11:50:19	836.54	108	973	392	743	761	36	15.1	1.82	0.21	2.44	2.75	0.57	75.79	16.59	0.25
11:50:30	836.79	108	977	384	744	761	38	15.1	1.82	0.21	2.44	2.7	0.55	81.81	16.84	0.25
11:50:40	837.04	107	982	383	742	761	36	15.13	1.81	0.19	2.42	2.68	0.53	88.85	17.1	0.25
11:50:51	837.29	107	988	389	742	761	36	15.13	1.81	0.19	2.41	2.7	0.56	79.78	17.34	0.25
11:51:02	837.54	110	981	401	743	761	36	15.1	1.83	0.16	2.45	2.75	0.62	82.19	17.59	0.25
11:51:14	837.79	106	979	387	744	761	36	15.09	1.83	0.21	2.45	2.76	0.65	78.15	17.85	0.27
11:51:26	838.04	105	978	383	744	761	32	15.00	1.81	0.19	2.47	2.73	0.55	77.60	18.08	0.27
11:51:36	838.29	107	983	390	744	765	41	15.1	1.81	0.19	2.44	2.75	0.6	83.87	18.34	0.27
11:51:48	838.55	109	987	398	742	761	35	15.11	1.81	0.2	2.43	2.7	0.53	77.91	18.59	0.28
11:51:59	838.8	108	981	395	744	761	32	15.12	1.8	0.19	2.42	2.69	0.53	85.20	18.85	0.28
11:52:10	839.05	106	973	386	743	761	35	15.08	1.81	0.21	2.46	2.73	0.65	77.23	19.09	0.28
11:52:22	839.3	108	981	394	742	761	36	15.11	1.81	0.19	2.43	2.7	0.53	76.82	19.34	0.29
11:52:34	839.55	107	980	389	742	765	41	15.09	1.81	0.19	2.45	2.75	0.56	76.78	19.56	0.29

Well No. 23 Date: 2/23/96

Starting Depth = 823.33 Bit Type = Walker McDonald MP68H
 Ending Depth = 1081.19 Bit Size = 4.75
 Total Depth Drilled Bit Nozzle = 9, 9, 12, 12
 Hours On Bit = 4.09 Mud Type = Water Based
 Average ROP = 98.58 Mud Weight (lbs/gal) = 9.00
 Driftstring (ft) = 663.43 Pipe (ft) = 251.81 Coker (ft) = 468.60

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
MM:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	GS	ft/s	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
11:52:45	638.8	111	984	405	742	781	41	15.1	1.82	0.23	2.44	2.78	0.6	71.77	19.85	0.29
11:52:57	640.08	112	981	405	744	781	38	15.08	1.8	0.18	2.45	2.73	0.53	82.88	30.12	0.29
11:53:06	640.3	108	981	388	743	765	41	15.31	1.81	0.19	2.43	2.75	0.57	76.38	20.34	0.3
11:53:21	640.88	107	989	388	740	767	39	15.08	1.8	0.17	2.46	2.73	0.53	75.44	20.6	0.3
11:53:33	640.8	109	976	392	741	761	38	15.1	1.81	0.19	2.44	2.7	0.53	78.34	20.88	0.3
11:53:44	641.08	108	979	393	743	761	36	15.11	1.81	0.19	2.43	2.68	0.48	77.78	21.11	0.31
11:53:55	641.3	106	978	398	742	781	38	15.08	1.84	0.23	2.45	2.8	0.62	82.30	21.34	0.31
11:54:08	641.58	109	936	392	743	781	36	15.03	1.8	0.18	2.51	2.82	0.62	68.18	21.6	0.31
11:54:22	641.8	108	936	392	743	765	41	15.61	1.81	0.18	2.58	2.82	0.6	68.18	21.87	0.32
11:54:35	642.08	108	933	394	742	781	35	15.81	1.83	0.18	2.59	2.82	0.55	68.18	22.13	0.32
11:54:48	642.3	109	944	396	742	781	41	15.06	1.81	0.19	2.48	2.78	0.57	69.05	22.36	0.32
11:55:00	642.55	108	926	394	742	781	38	14.99	1.81	0.17	2.54	3.14	0.63	76.45	22.58	0.32
11:55:12	642.81	108	952	393	743	757	32	14.11	1.81	0.19	3.43	4	1.2	78.22	22.88	0.32
11:55:24	643.08	116	947	399	743	781	35	13.6	1.81	0.19	3.98	4.6	1.32	78.73	23.11	0.33
11:55:34	643.31	106	1015	384	741	781	38	13.2	1.83	0.23	4.34	4.69	0.63	90.67	23.37	0.33
11:55:41	643.58	109	1083	383	740	767	35	13.73	1.81	0.2	3.83	4.25	1.35	133.37	23.61	0.33
11:55:53	643.81	108	978	397	741	737	32	14.28	1.8	0.19	3.28	3.71	0.66	96.17	23.88	0.33
11:56:01	644.08	108	985	394	741	737	32	14.1	1.8	0.17	3.44	3.75	0.67	75.35	24.1	0.33
11:56:11	644.31	109	971	398	740	737	32	14.16	1.81	0.19	3.17	3.69	0.69	81.22	24.38	0.33
11:56:21	644.58	108	1037	392	748	757	32	14.45	1.81	0.23	3.08	3.49	0.93	94.05	24.6	0.33
11:56:32	644.81	105	991	383	737	783	32	15.23	1.83	0.25	2.30	3.14	1.46	80.65	24.88	0.33
11:56:41	645.06	110	987	396	740	757	32	15.2	1.84	0.26	2.35	2.7	0.89	94.78	25.11	0.33
11:56:53	645.31	108	940	387	740	757	32	15.88	1.84	0.22	2.45	2.79	0.62	90.58	25.37	0.33
11:57:00	645.56	110	981	401	742	781	49	15.86	1.85	0.27	2.48	2.85	0.81	105.38	25.6	0.33
11:57:09	645.82	107	979	389	743	761	36	15.07	1.87	0.31	2.47	2.82	0.76	100.44	25.86	0.33
11:57:19	646.07	107	959	389	743	781	39	15.02	1.85	0.29	2.51	2.92	0.86	86.14	26.11	0.33
11:57:30	646.32	108	956	392	743	781	36	14.97	1.81	0.18	2.57	2.85	0.65	83.82	26.37	0.33
11:57:42	646.57	107	948	389	745	781	36	14.94	1.82	0.21	2.59	2.92	0.77	77.66	26.6	0.33
11:57:54	646.82	105	932	394	744	781	32	14.51	1.81	0.19	2.53	2.94	0.6	72.45	26.86	0.33
11:58:03	647.07	108	942	394	744	761	39	15.11	1.84	0.35	3.42	2.75	0.91	100.45	27.12	0.33
11:58:14	647.32	108	983	392	743	781	38	15.02	1.83	0.22	2.51	2.67	0.69	83.40	27.37	0.33
11:58:23	647.57	110	983	400	742	785	41	15.04	1.83	0.23	2.50	2.78	0.82	97.82	27.6	0.33
11:58:33	647.82	107	983	390	743	781	36	15.09	1.81	0.2	2.48	2.8	0.65	92.56	27.86	0.33
11:58:42	648.07	108	981	386	744	781	32	15.12	1.83	0.23	2.41	2.75	0.69	100.27	28.12	0.33

Well No. 23
 Starting Depth = 823.92
 Ending Depth = 1001.19
 Total Depth Drilled = 407.27
 Hours On Bit = 4.08
 Average ROP = 99.58
 Drillstring (ft) = 660.48

Bit Type = Walker McDonald MPFH
 Bit Size = 4.75
 Bit Nozzles = 9, 9, 32, 12
 Mud Type = Water Based
 Mud Weight (lb/gal) = 9.00
 Pipe (ft) = 251.81
 Coker (ft) = 488.89

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23	Date: 2/23/98																	
Starting Depth =	623.92	Bit Type =	Walker McDougal MP68H															
Ending Depth =	1031.19	Bit Size =	4.75															
Total Depth Drilled	407.27	Bit Sizes =	3, 9, 12, 12															
Hours On Bit =	4.06	Mud Type =	Water Based															
Average ROP =	90.56	Mud Weight (lb/gal) =	9.00															
Drillstring (ft) =	660.49	Pipe (ft) =	251.81	Collar (ft) =	408.68													

TIME HH:MM:SS	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELTA ft-lbs	HOOK		WOB KIPS	PEAK KIPS	DELTA KIPS	ROP FT/HR	Feet OnBit	Hours OnBit	
								LOAD KIPS	PEAK G's							
11:58:51	648.32	116	838	400	743	751	36	15.06	1.82	0.21	2.47	2.87	0.77	97.84	28.37	0.39
11:59:01	648.57	108	940	383	734	755	36	15.00	1.82	0.21	2.48	2.8	0.72	92.60	28.61	0.4
11:59:10	648.82	107	943	389	743	751	35	15.07	1.81	0.21	2.49	2.78	0.67	102.27	28.86	0.4
11:59:20	649.07	108	940	393	742	757	32	14.97	1.81	0.19	2.66	3.04	0.80	89.89	29.12	0.4
11:59:29	649.32	107	959	389	742	751	36	14.85	1.82	0.23	2.69	3.09	0.81	110.93	29.38	0.4
11:59:38	649.57	109	896	395	743	751	32	14.85	1.84	0.20	2.68	3.08	0.77	115.05	29.63	0.41
11:59:48	649.82	109	1008	395	743	757	38	14.81	1.83	0.24	2.72	3.09	0.74	101.96	29.88	0.41
11:59:58	650.07	110	1019	403	743	751	32	14.83	1.82	0.21	2.70	3.04	0.66	112.98	30.14	0.41
12:00:01	650.32	107	1008	391	743	751	35	14.85	1.83	0.22	2.68	3.05	0.79	114.95	30.39	0.41
12:00:09	650.57	107	1021	390	742	757	32	14.85	1.83	0.22	2.68	3.11	0.96	107.96	30.62	0.41
12:00:17	650.83	107	1019	390	743	751	32	14.81	1.83	0.21	2.71	3.04	0.69	113.88	30.8	0.42
12:00:26	651.08	106	1011	388	742	757	32	14.8	1.83	0.24	2.73	3.11	0.72	102.57	31.12	0.42
12:00:34	651.33	106	1019	387	742	757	32	14.81	1.81	0.2	2.73	3.09	0.74	108.01	31.4	0.42
12:00:43	651.58	109	1018	397	743	757	38	14.82	1.82	0.21	2.71	3.09	0.86	110.74	31.63	0.42
12:00:51	651.83	108	1024	394	742	757	32	14.79	1.82	0.22	2.74	3.14	0.72	100.12	31.89	0.43
12:01:00	652.08	105	1029	383	742	757	38	14.74	1.81	0.19	2.76	3.11	0.62	88.05	32.12	0.43
12:00:26	651.31	109	720	399	740	757	32	17.87	1.81	0.19	0.13	0.67	0.79	114.82	32.19	0.43
12:00:33	651.56	109	732	393	738	753	28	17.85	1.82	0.18	0.12	0.31	0.41	136.38	32.19	0.43
12:00:41	651.81	108	784	390	740	757	32	17.8	2.01	0.43	0.20	0.5	0.59	114.91	32.19	0.43
12:00:48	652.06	108	721	398	740	757	32	17.77	1.82	0.22	0.69	0.48	0.48	121.13	32.19	0.43
12:10:18	652.31	108	788	382	740	757	36	17.99	1.82	0.41	0.80	1.13	1.17	89.68	32.36	0.44
12:10:38	652.56	106	858	387	751	1016	252	16.88	2.02	0.66	1.32	5.22	5	42.79	32.6	0.45
12:11:01	652.81	109	692	388	743	834	109	16.85	1.89	0.30	1.54	2.49	2.87	41.27	32.85	0.45
12:11:18	653.06	108	1026	382	742	757	32	15.8	1.97	0.44	2.26	2.51	1.1	61.58	33.11	0.46
12:11:34	653.31	108	1083	392	742	751	36	15.76	1.85	0.44	2.22	2.48	0.58	57.18	33.36	0.46
12:11:51	653.56	109	1028	395	741	757	32	15.79	1.85	0.44	2.22	2.51	0.55	65.18	33.62	0.47
12:12:09	653.81	108	1039	391	739	757	36	15.82	1.83	0.42	2.18	2.47	0.62	57.84	33.88	0.47
12:12:22	654.06	107	1035	390	741	757	28	15.77	1.84	0.42	2.23	2.78	0.91	55.89	34.13	0.47
12:12:31	654.31	106	1141	390	740	757	32	14.42	1.98	0.57	3.50	4.98	2.44	91.86	34.38	0.48
12:12:38	654.56	106	1347	388	741	757	28	12.82	1.99	0.68	5.60	6.42	1.82	140.28	34.61	0.48
12:12:44	654.82	107	1444	390	741	757	32	11.55	2.08	0.68	6.47	7.11	1.17	149.13	34.87	0.48
12:12:51	655.07	103	1436	377	729	753	38	11.34	2.06	0.68	6.89	6.94	0.53	131.75	35.13	0.48
12:12:57	655.32	105	1498	381	741	757	36	11.34	2.05	0.64	6.09	7.11	0.74	146.31	35.38	0.48
12:13:03	655.57	106	1443	387	741	757	28	11.34	1.95	0.48	6.68	6.94	0.53	136.51	35.63	0.49

DOE High power mortar test Amaco Catoosa Test Site

TIME	DEPTH FEET	FLOW GPM	PRESS PSI	SPEED RPM	TORQUE N-BS	PEAK RPM	DELTA H-BS	LOAD NIPS	PEAK G/S	DELTA G/S	WOB KIPS	PEAK KIPS	DELTA RPM/S	ROP FT/HR	Feet Drift	Hours Cmpt
12:13:19	651.02	107	14560	386	742	757	32	11.34	2.01	0.64	6.68	7.01	0.33	155.83	35.92	0.49
12:13:15	656.07	104	14620	379	742	761	36	11.34	1.97	0.55	6.71	7.01	0.30	156.70	36.13	0.49
12:13:12	656.32	107	1446	369	742	757	32	11.32	2.08	0.56	6.70	7.04	0.34	158.14	36.13	0.49
12:13:08	656.57	108	1475	363	744	757	32	11.29	2.15	0.73	6.74	7.09	0.35	146.75	36.34	0.49
12:13:04	656.82	107	1479	368	742	757	32	11.31	2.01	0.82	6.73	7.01	0.28	142.03	36.89	0.49
12:13:40	657.07	104	1473	378	742	751	36	11.4	2.1	0.7	6.62	7.09	0.29	155.26	37.11	0.5
12:13:48	657.32	102	1459	373	744	757	32	11.37	2.09	0.71	6.83	7.22	1.01	159.36	37.38	0.5
12:13:32	657.57	106	1450	380	742	767	247	11.35	1.98	0.85	6.67	7.06	0.27	146.12	37.63	0.5
12:13:58	657.82	106	1466	367	743	751	32	11.26	1.93	0.86	6.79	7.16	0.34	145.66	37.91	0.5
12:14:05	658.07	104	1477	360	743	751	32	11.27	2.05	0.74	6.75	7.16	0.27	142.51	38.15	0.5
12:14:11	658.32	104	1472	360	742	751	33	11.25	2.06	0.69	6.72	7.06	0.57	135.21	38.39	0.5
12:14:18	658.58	103	1469	375	742	757	28	11.18	2.09	0.79	6.84	7.06	1.24	134.08	38.62	0.51
12:14:24	659.33	106	1453	387	742	757	28	11.28	1.94	0.87	6.69	7.01	0.77	139.75	38.86	0.51
12:14:31	659.08	107	1439	381	740	757	32	11.18	1.94	0.86	6.84	7.16	0.57	137.57	39.11	0.51
12:14:38	659.33	106	1440	384	740	757	32	11.22	1.96	0.88	6.86	7.16	0.55	137.71	39.35	0.51
12:14:44	659.58	106	1418	385	741	757	32	11.27	1.91	0.82	6.75	7.11	0.68	138.90	39.62	0.51
12:14:50	659.83	106	1415	385	741	757	32	11.26	2.05	0.84	6.73	7.11	0.6	145.54	39.8	0.52
12:14:56	660.08	108	1420	383	742	757	32	11.21	1.95	0.87	6.81	7.13	0.62	142.56	40.13	0.52
12:15:04	660.19	107	1437	385	742	757	32	11.22	1.89	0.89	6.80	7.05	0.8	141.83	40.38	0.52
12:15:14	660.58	106	1453	385	740	757	32	11.21	1.98	0.89	6.81	7.05	0.6	142.84	40.62	0.52
12:15:17	660.59	108	1451	385	741	761	38	11.27	1.98	0.5	6.75	7.01	0.85	140.95	40.9	0.52
12:15:21	661.08	107	1416	383	742	761	32	11.16	1.98	0.5	6.84	7.16	0.74	142.64	41.13	0.52
12:15:26	661.33	106	1459	383	743	757	28	11.24	1.93	0.5	6.78	7.13	0.74	138.98	41.36	0.53
12:15:30	661.58	106	1456	384	743	757	28	11.26	1.97	0.5	6.78	7.13	0.74	138.98	41.59	0.53
12:15:36	661.83	106	1456	384	743	757	28	11.26	1.97	0.5	6.78	7.13	0.74	138.98	41.82	0.53
12:15:42	662.08	105	1453	384	743	757	28	11.23	1.95	0.42	6.86	7.04	0.67	151.06	41.89	0.53
12:15:48	662.09	106	1453	382	743	757	28	11.25	1.97	0.46	6.77	7.04	0.53	146.01	41.95	0.53
12:15:54	662.34	105	1479	369	743	761	32	11.22	2.04	0.54	6.86	7.13	0.62	146.77	42.39	0.53
12:16:02	662.59	109	1394	384	743	761	32	11.06	1.68	0.54	6.88	7.23	0.28	132.50	42.84	0.54
12:16:08	662.84	108	1388	385	743	761	28	11.2	1.88	0.38	6.81	7.28	0.74	149.87	42.86	0.54
12:16:14	663.09	104	1386	380	743	757	24	11.3	1.86	0.57	6.71	7.06	0.55	150.77	43.13	0.54
12:16:21	663.34	105	1442	382	743	781	38	11.19	2.03	0.57	6.82	7.18	0.77	154.31	43.39	0.54
12:16:28	663.59	106	1446	380	743	781	32	11.18	1.62	0.41	6.86	7.25	0.74	149.75	43.65	0.54
12:16:35	663.84	104	1434	379	743	757	32	11.01	?	0.5	7.07	7.32	0.67	146.93	43.88	0.54
12:16:43	664.09	101	1662	389	742	757	24	11.12	1.91	0.44	6.90	7.18	0.57	142.36	44.14	0.54

Well No: 21 Date: 2/25/06
 Starting Depth = 621.92
 Ending Depth = 1031.19
 Total Depth Drilled = 409.27
 Hours On Site = 4.09
 Average ROP = 99.38
 Collected @ = 683.49

Bit Type = Washer Endomatic MFSBH
 Bit Size = 4.75
 Bit Nozzles = A 3/16 1/2
 Mud Type = Washer Slurcut
 Mud Weight (lb/gal) = 9.00
 Pipe ID = 261.61
 Casing ID = 408.60

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	CFM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	C's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBt
12:16:50	664.34	103	1506	375	742	757	32	11.06	1.98	0.81	6.97	7.3	0.57	109.20	44.39	0.56
12:16:58	664.58	103	1502	383	742	757	32	11.04	1.98	0.5	6.99	7.54	0.86	118.94	44.65	0.55
12:17:06	664.84	103	1531	376	742	757	28	11.01	1.93	0.46	7.01	7.3	0.85	118.03	44.86	0.55
12:17:14	665.09	100	1516	365	741	761	36	10.98	1.95	0.45	7.04	7.3	0.5	108.40	45.14	0.56
12:17:22	665.34	105	1535	382	742	757	28	10.95	1.97	0.48	7.06	7.39	0.57	113.17	45.39	0.56
12:17:31	665.58	103	1607	377	742	761	32	10.98	1.98	0.56	7.04	7.32	0.5	108.37	45.65	0.56
12:17:39	665.85	104	1606	380	741	757	32	10.99	1.96	0.45	7.03	7.71	0.68	111.71	45.89	0.56
12:17:48	666.1	103	1634	376	742	757	32	11.01	1.97	0.52	7.01	7.3	0.86	115.72	46.14	0.56
12:17:55	666.35	103	1664	377	741	761	36	11.03	2	0.58	6.98	7.3	0.57	108.58	46.41	0.57
12:18:02	666.6	106	1662	385	742	757	36	11	2.02	0.66	7.02	7.3	0.53	118.04	46.67	0.57
12:18:11	668.85	103	1630	376	741	757	32	10.97	1.96	0.5	7.04	7.35	0.62	108.03	46.92	0.57
12:18:18	667.1	105	1641	381	742	757	32	11.01	1.97	0.54	6.99	7.32	0.62	116.77	47.14	0.57
12:18:28	667.35	105	1653	382	742	781	32	11.06	2.04	0.61	6.95	7.3	0.62	123.15	47.41	0.58
12:18:33	667.6	107	1681	391	742	757	32	11.08	2.11	0.74	6.93	7.26	0.72	116.12	47.69	0.58
12:18:40	667.85	108	1664	388	742	761	32	11.13	2.03	0.89	6.89	7.18	0.62	122.93	47.94	0.58
12:18:47	668.1	103	1681	375	742	757	28	11.22	2.07	0.87	6.77	7.16	0.74	124.03	48.14	0.58
12:18:54	668.35	104	1677	378	741	757	32	11.15	2.01	0.58	6.85	7.21	0.89	132.93	48.3	0.58
12:19:01	668.6	103	1682	376	742	757	32	11.04	1.94	0.46	6.97	7.28	0.69	121.60	48.65	0.59
12:19:10	668.85	104	1641	378	740	757	32	10.99	1.98	0.51	7.02	7.3	0.5	105.38	48.91	0.59
12:19:17	669.1	103	1610	374	741	757	32	11	1.94	0.48	7.01	7.26	0.45	117.38	49.14	0.58
12:19:25	669.35	102	1626	372	742	757	28	11	1.95	0.48	7.01	7.26	0.55	113.24	49.4	0.59
12:19:33	669.6	101	1610	369	741	757	28	10.95	1.93	0.48	7.05	7.3	0.45	110.38	49.67	0.58
12:19:41	669.85	104	1623	381	742	757	32	10.98	1.99	0.5	7.03	7.23	0.41	114.65	49.91	0.58
12:19:50	670.1	104	1629	379	741	757	32	10.96	1.94	0.52	7.05	7.35	0.55	105.73	50.16	0.6
12:19:58	670.35	105	1626	381	742	757	32	10.92	1.93	0.48	7.09	7.35	0.3	108.77	50.42	0.6
12:20:06	670.6	105	1635	382	742	757	28	10.97	1.96	0.51	7.04	7.3	0.53	112.48	50.65	0.6
12:20:15	670.85	104	1635	379	742	761	32	10.99	1.95	0.52	7.02	7.3	0.57	104.33	50.91	0.61
12:20:23	671.1	106	1631	385	742	757	28	10.99	1.92	0.4	7.02	7.38	0.56	113.69	51.17	0.61
12:20:31	671.35	105	1630	384	741	757	32	10.99	1.99	0.52	7.02	7.32	0.57	105.63	51.43	0.61
12:20:39	671.6	105	1639	372	742	757	28	11.01	2.02	0.54	7.08	7.3	0.5	120.82	51.68	0.61
12:20:47	671.85	106	1633	382	743	757	28	10.99	1.98	0.5	7.03	7.39	0.62	114.86	51.94	0.61
12:20:54	672.1	105	1658	382	742	761	32	11.05	1.96	0.5	6.98	7.28	0.87	115.32	52.19	0.62
12:21:03	672.35	104	1627	378	743	757	36	10.94	1.95	0.45	7.07	7.37	0.55	111.04	52.4	0.62
12:21:12	672.6	103	1615	374	741	761	36	10.93	1.94	0.43	7.08	7.37	0.67	98.75	52.65	0.62

DOE high power motor test Amaco Catoosa Test Site

Well No. 23	Date: 2/22/98																	
Starting Depth =	623.92	Bit Type =	Walker McCannald MP68H															
Ending Depth =	1031.19	Bit Size =	4.75															
Total Depth Drilled	407.27	Bit Nozzles =	5, 8, 12, 12															
Hours On Bit =	4.09	Mud Type =	Water Based															
Average ROP =	99.58	Mud Weight (lb/gal) =	8.00															
Drilling (ft) =	680.49	Pipe (ft) =	351.61	Collar (ft) =	408.80													

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
12:21:30	673.96	107	1599	391	741	761	36	10.69	1.91	0.42	7.13	7.44	0.65	103.77	52.91	0.62
12:21:30	673.11	103	1592	377	741	761	36	10.63	1.94	0.44	7.18	7.62	0.6	92.74	53.17	0.62
12:21:40	673.36	106	1565	385	740	757	32	10.63	1.92	0.41	7.19	7.47	0.53	87.64	53.4	0.63
12:21:50	673.61	104	1602	380	741	757	32	10.84	1.95	0.44	7.17	7.49	0.57	98.39	53.68	0.63
12:22:00	673.86	106	1605	382	742	757	32	10.84	1.98	0.46	7.17	7.47	0.62	87.25	53.91	0.64
12:22:10	674.11	104	1591	380	741	761	36	10.81	1.94	0.43	7.20	7.47	0.59	90.61	54.17	0.64
12:22:22	674.36	105	1559	382	740	753	28	10.74	1.91	0.38	7.27	7.49	0.58	79.51	54.4	0.64
12:22:33	674.61	105	1543	388	740	757	33	10.7	1.94	0.38	7.28	7.89	0.65	79.45	54.66	0.64
12:22:46	674.86	104	1509	380	740	757	32	10.81	1.92	0.39	7.35	7.71	0.72	70.95	54.91	0.65
12:22:57	675.12	106	1651	385	740	757	32	10.70	1.95	0.4	7.21	7.64	0.79	80.05	55.18	0.65
12:23:06	675.37	106	1643	394	740	753	29	10.81	1.91	0.43	7.15	7.4	0.56	95.67	55.44	0.65
12:23:16	675.62	106	1632	385	740	757	32	10.78	1.93	0.4	7.18	7.42	0.53	89.95	55.68	0.66
12:23:27	675.87	103	1543	376	740	757	23	10.8	1.97	0.57	7.15	7.42	0.69	87.80	55.90	0.66
12:23:34	676.12	105	1597	384	738	753	28	10.96	2.06	0.68	7.01	7.66	0.74	114.91	56.19	0.66
12:23:50	676.37	105	1618	384	740	753	28	10.57	1.89	0.41	7.38	7.78	0.79	87.30	56.43	0.67
12:23:59	676.62	107	1634	388	738	753	28	10.89	2.04	0.64	7.07	7.59	1.03	104.05	56.68	0.67
12:24:06	676.87	103	1691	376	738	757	32	11.07	2.06	0.73	6.89	7.23	0.74	120.75	56.94	0.67
12:24:14	677.12	103	1788	377	740	757	29	11.01	2.13	0.84	6.85	7.37	0.86	118.56	57.19	0.67
12:24:21	677.37	103	1743	377	738	757	32	11.96	2.06	0.64	6.88	7.23	0.72	130.75	57.41	0.67
12:24:28	677.62	104	1754	380	739	753	28	11.98	2.13	0.87	6.88	7.3	0.89	117.67	57.67	0.68
12:24:35	677.87	101	1715	368	739	783	29	11.13	2.07	0.66	6.83	7.13	0.89	138.44	57.92	0.68
12:24:42	678.12	102	1794	373	740	757	32	11.12	2.01	0.66	6.84	7.65	0.74	136.55	58.18	0.68
12:24:49	678.37	105	1887	382	741	757	32	11.13	2.09	0.69	6.83	7.11	0.72	124.35	58.43	0.68
12:24:55	678.63	105	1880	380	741	757	32	11.89	2.14	0.71	6.87	7.18	0.89	134.77	58.67	0.68
12:25:03	678.88	103	1695	375	741	761	32	11.99	2.09	0.63	6.87	7.35	0.81	118.53	58.93	0.69
12:25:10	679.13	103	1677	376	741	761	35	11.59	2.13	0.74	6.87	7.23	0.74	133.89	59.18	0.69
12:25:17	679.38	104	1672	378	741	757	32	11.06	2.06	0.57	6.96	7.21	0.62	125.32	59.43	0.69
12:25:23	679.63	102	1689	372	741	757	30	11.07	2.09	0.67	6.88	7.13	0.62	121.35	59.67	0.69
12:25:31	679.88	104	1663	378	741	757	32	11.08	1.98	0.54	6.89	7.18	0.57	128.60	59.93	0.69
12:25:39	680.13	104	1669	379	741	757	32	11.05	2.09	0.65	6.90	7.21	0.67	121.15	60.2	0.7
12:25:46	680.38	104	1657	378	741	757	32	11.05	2	0.54	6.91	7.15	0.6	122.45	60.43	0.7
12:25:54	680.63	105	1640	383	741	757	32	11.01	2.11	0.65	6.95	7.23	0.57	119.59	60.68	0.7
12:26:02	680.88	105	1622	382	739	757	32	10.97	1.98	0.53	6.98	7.26	0.58	108.76	60.94	0.7
12:26:09	681.13	104	1819	378	738	757	38	10.97	2	0.52	6.99	7.23	0.57	121.69	61.19	0.7

DOE high power mortar test Amaco Callosa Test Site

TEST No. 33	DATE: 2/22/86	PIPE TYPE =	WALKER MACHINIST MFG/SH	PIPE SIZE =	4.75	9. A. 12. 12	Water Based	COILER (ft)	408.50							
Standing Depth =	622.82	RIE TYPE =		RIE SIZE =												
Striding Depth =	183.18															
Total Depth Drilled	460.27	RIE Strides =														
Hours On Shift =	4.09	RIE Type =														
Average ROPS =	39.58	RIE Weight (lb/str) =														
Collecting (ft) =	360.48	Pipe (ft) =	251.81													
TAKE	DEPTH	FLOW	PRESS	SPEED	TOPPOINT	FEAR	DEPT	LOAD	PEAK	DELTA	WOB	PEAK	DELTA	ROF	Feed	Hours
MIN/MIN	FEET	GPM	PSI	PPM	RPM	RPM	INCH	KPS	Q'S	Q'S	KPS	KPS	KPS	FT/HR	CHST	CHST
12-26.12	687.28	106	2687	385	739	757	32	10.03	1.96	0.28	7.60	7.39	0.57	106.37	67.43	3.73
12-28.25	687.63	107	2686	386	740	757	32	10.01	1.96	0.4	7.04	7.39	0.5	114.82	61.86	4.74
12-28.34	687.98	103	2597	376	737	753	32	10.6	1.81	0.38	7.06	7.32	0.6	160.89	61.93	6.71
12-28.44	687.13	107	2575	388	736	753	32	10.86	1.81	0.39	7.66	7.32	0.55	168.86	62.16	6.71
12-28.52	688.38	105	2582	392	738	751	28	10.39	1.81	0.37	7.08	7.35	0.58	112.19	62.44	6.72
12-27.00	688.63	107	2671	395	737	751	28	10.86	1.84	0.4	7.67	7.32	0.57	160.13	62.85	6.72
12-27.09	688.88	106	2684	397	736	752	32	10.85	1.9	0.39	7.10	7.37	0.57	166.58	62.55	6.72
12-27.18	688.14	106	2593	386	736	751	32	10.82	1.84	0.48	7.18	7.71	0.64	166.56	63.18	6.72
12-27.28	688.39	107	2594	399	737	751	28	10.82	1.85	0.37	7.18	7.42	0.52	169.31	63.41	6.72
12-27.37	688.64	106	2553	382	736	751	32	10.77	1.99	0.39	7.18	7.47	0.57	169.84	63.69	6.72
12-24.00	688.87	105	2618	364	733	757	32	10.87	1.79	0.38	7.55	7.48	1.63	129.96	64.11	6.74
12-24.17	684.32	104	2325	390	738	757	40	15.09	1.81	0.17	2.24	4.75	3.78	32.58	64.35	6.74
12-24.30	684.57	104	2493	378	734	757	45	12.86	1.8	0.18	4.92	8.19	6.27	73.25	64.63	6.76
12-24.43	684.82	106	2482	398	735	757	36	12.88	1.81	0.18	4.97	8.18	6.55	65.65	64.86	6.76
12-24.53	685.07	105	2489	382	734	753	28	12.88	1.81	0.18	4.92	8.17	6.53	88.83	65.11	6.76
12-25.02	685.32	105	2608	382	738	757	32	13.08	1.82	0.18	4.81	8.17	6.69	92.18	65.37	6.76
12-25.12	685.57	106	2538	383	737	757	26	13.06	1.84	0.24	4.76	8.06	6.5	97.05	65.63	6.76
12-25.20	685.82	104	2574	378	737	758	20	13.06	1.81	0.22	4.79	8.07	6.6	108.74	65.86	6.76
12-26.30	686.07	104	2585	379	737	747	35	13.08	1.83	0.28	4.77	8.07	6.62	68.34	66.12	6.76
12-26.38	686.32	103	2669	376	738	739	28	13.06	1.84	0.24	4.79	8.09	6.51	101.15	66.36	6.76
12-26.47	686.57	106	2518	385	738	757	36	13.06	1.82	0.21	4.76	8.03	6.52	66.45	66.63	6.77
12-26.56	686.82	107	2595	389	738	757	32	13.07	1.81	0.19	4.77	8	6.49	169.70	66.87	6.77
12-26.07	687.07	106	2484	389	738	753	32	12.94	1.81	0.19	4.91	8.1	6.49	68.21	67.12	6.77
12-26.24	687.32	105	2466	384	738	757	28	12.74	1.82	0.21	5.13	8.08	6.4	62.07	67.37	6.77
12-26.33	687.57	105	2539	383	739	755	28	12.73	1.83	0.21	7.32	8.19	6.4	96.18	67.62	6.78
12-26.42	687.82	102	2513	373	738	757	35	9.25	1.83	0.22	8.61	8.26	1.41	132.59	67.88	6.78
12-26.51	688.07	104	2516	373	737	753	35	8.71	1.86	0.29	8.16	8.65	1.1	149.35	68.13	6.79
12-26.58	688.32	104	2589	389	737	753	35	8.71	1.86	0.29	8.16	8.65	1.1	149.35	68.13	6.79
12-26.53	688.57	102	2518	373	738	753	32	8.67	1.83	0.27	8.85	8.17	0.53	184.03	68.37	6.79
12-26.58	688.82	106	2597	381	739	753	33	8.93	1.85	0.28	8.94	8.22	0.6	145.94	68.61	6.79
12-27.05	689.07	106	2704	381	738	753	28	8.91	1.84	0.28	8.98	8.22	0.63	181.64	68.85	6.79
12-27.10	689.32	102	2748	371	738	748	28	9.04	1.88	0.33	8.43	9.12	0.63	182.66	69.09	6.79
12-27.16	689.57	104	2655	380	745	748	28	8.99	1.88	0.33	8.59	9.17	0.56	164.90	69.38	6.79
12-27.21	689.82	107	2805	371	747	753	32	8.97	1.87	0.31	8.69	9.14	0.56	187.56	69.63	6.79
12-27.27	689.83	101	2895	385	738	753	32	8.93	1.98	0.34	8.84	9.18	0.6	181.84	69.89	6.79

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23	Date: 3/22/98																
Starting Depth =	623.92	BR Type =	Walker McDonald MP88H														
Ending Depth =	1031.19	BR Size =	4.75														
Total Depth Drilled	407.27	BR Nozzles =	9, 9, 12, 12														
Hours On Bit =	4.08	Mud Type =	Water Based														
Average ROP =	99.58	Mud Weight (lbs/gal) =	9.50														
Drillstring (ft) =	650.88	Pipe (ft) =	251.81	Collar (ft)	498.60												

TIME HH:MM:SS	BWT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELTA ft-lbs	HOOK		WOB KIPS	PEAK KIPS	DELTA KIPS	ROP FT/HR	Feet OnBit	Hours OnBit	
								LOAD KIPS	G%							
12:37:33	690.08	104	1827	376	734	748	28	8.84	1.85	0.3	8.32	8.19	0.53	173.64	70.12	0.8
12:37:39	690.33	102	1811	374	718	761	190	8.9	1.88	0.47	8.36	8.31	0.74	144.89	70.38	0.8
12:37:44	690.58	101	1854	384	661	769	289	8.84	1.85	0.41	8.03	8.91	1.84	157.91	70.64	0.8
12:37:50	690.83	104	2016	407	568	716	203	8.89	1.92	0.42	8.67	8.68	3.47	154.27	70.90	0.8
12:38:05	691.25	104	1380	375	737	753	32	10.89	1.89	0.2	2.48	3.33	2.68	81.34	71.29	0.81
12:38:45	691.5	104	1450	379	730	753	32	14.5	1.89	0.33	3.34	4.19	1.24	85.19	71.55	0.81
12:38:55	691.75	106	1519	385	737	753	32	13.63	1.89	0.27	4.21	4.48	0.85	92.67	71.79	0.82
12:39:05	692	105	1513	384	737	753	32	13.58	1.83	0.33	4.27	4.52	0.55	97.98	72.04	0.82
12:39:13	692.25	105	1581	384	738	753	36	13.01	1.83	0.27	4.83	5.33	1.2	104.90	72.30	0.82
12:39:21	692.5	103	1680	375	737	757	41	12.55	1.84	0.29	5.36	5.8	0.74	117.65	72.54	0.82
12:39:28	692.75	104	1629	377	737	753	32	12.52	1.89	0.28	5.35	5.83	0.8	124.53	72.8	0.83
12:39:36	693	105	1627	381	735	748	32	12.54	1.87	0.29	5.31	5.8	0.6	120.93	73.05	0.83
12:39:43	693.25	104	1614	379	735	748	38	12.68	1.81	0.32	5.35	5.65	0.62	121.03	73.31	0.83
12:39:51	693.5	107	1621	389	737	757	36	12.31	1.83	0.28	5.63	6.03	0.91	115.84	73.58	0.83
12:39:58	693.75	101	1641	389	738	757	45	11.88	1.86	0.29	5.89	6.3	0.72	131.23	73.79	0.83
12:40:04	694	103	1731	376	740	761	36	11.76	1.86	0.3	6.08	6.53	0.91	139.59	74.05	0.84
12:40:12	694.25	103	1688	377	738	757	32	11.89	1.84	0.27	6.16	6.42	0.65	184.03	74.32	0.84
12:40:18	694.5	104	1653	379	736	753	32	11.95	1.82	0.24	6.20	6.31	0.82	134.73	74.57	0.84
12:40:26	694.75	103	1673	376	739	757	36	11.63	1.84	0.27	6.22	6.49	0.57	123.61	74.81	0.84
12:40:33	695.01	103	1632	373	729	757	32	11.64	1.84	0.3	6.28	6.46	0.6	129.37	75.06	0.84
12:40:40	695.26	105	1631	385	738	753	38	11.01	1.83	0.25	6.23	6.53	0.57	121.79	75.32	0.85
12:40:47	695.51	105	1848	382	738	753	32	11.53	1.84	0.34	6.29	7.11	1.13	123.13	75.57	0.85
12:40:53	695.76	104	1708	378	738	757	36	10.75	1.87	0.3	7.09	7.42	0.88	130.22	75.8	0.85
12:41:00	696.01	101	1736	369	739	767	32	10.79	1.9	0.34	7.66	7.97	0.89	143.35	76.08	0.85
12:41:06	696.26	104	1718	379	739	757	32	10.74	1.84	0.31	7.11	7.42	0.65	143.15	76.31	0.85
12:41:12	696.51	106	1719	389	739	753	28	10.74	1.85	0.27	7.11	7.44	0.67	143.78	76.56	0.85
12:41:19	696.76	103	1726	374	739	753	28	10.72	1.84	0.26	7.13	7.52	0.72	134.21	76.8	0.86
12:41:25	697.01	104	1713	381	737	757	38	10.71	1.88	0.32	7.14	7.52	0.72	141.18	77.08	0.86
12:41:32	697.26	104	1665	375	738	753	28	10.69	1.82	0.28	7.15	7.55	0.89	129.21	77.31	0.86
12:41:39	697.51	104	1858	381	734	763	28	10.66	1.84	0.26	7.20	7.54	0.63	134.79	77.57	0.86
12:41:46	697.76	104	1589	381	738	753	25	10.63	1.88	0.27	7.23	7.48	0.53	129.83	77.8	0.86
12:41:53	698.01	107	1679	388	738	753	28	10.65	1.84	0.25	7.20	7.44	0.55	124.91	78.05	0.87
12:42:00	698.26	105	1708	384	738	753	28	10.65	1.85	0.3	7.19	7.49	0.65	139.28	78.11	0.87
12:42:07	698.51	105	1678	381	738	757	32	10.82	1.85	0.28	7.24	7.58	0.62	124.14	78.37	0.87

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	LOAD	Gr	Gr	KIPS	KIPS	KIPS	FT/HR	CMSt	CMSt
12:42:19	688.77	104	1670	380	737	757	38	10.67	1.83	0.28	7.18	7.4	0.53	139.20	78.82	0.87
12:42:20	688.02	104	1724	379	738	753	38	10.69	1.84	0.37	7.16	7.52	0.65	136.62	79.08	0.87
12:42:27	689.27	107	1693	391	739	753	38	10.66	1.84	0.28	7.19	7.46	0.57	127.13	78.32	0.88
12:42:34	689.52	105	1663	384	739	757	32	10.63	1.82	0.25	7.32	7.47	0.48	138.19	79.57	0.88
12:42:41	689.77	104	1694	380	739	753	28	10.66	1.85	0.28	7.39	7.54	0.53	134.11	80.68	0.88
12:42:47	700.02	105	1685	383	738	757	32	10.65	1.85	0.27	7.38	7.47	0.53	134.11	80.68	0.88
12:42:54	700.27	104	1683	378	738	753	38	10.64	1.85	0.29	7.30	7.49	0.57	140.53	80.13	0.88
12:43:03	700.52	105	1684	383	739	753	28	10.65	1.83	0.20	7.20	7.52	0.57	124.32	80.59	0.88
12:43:08	700.77	107	1697	381	739	757	32	10.65	1.88	0.34	7.39	7.44	0.35	137.04	80.81	0.89
12:43:15	701.02	105	1681	384	737	753	28	10.67	1.85	0.29	7.18	7.42	0.5	136.13	81.08	0.89
12:43:23	701.27	104	1655	379	738	753	28	10.62	1.87	0.32	7.22	7.54	0.6	128.17	81.32	0.89
12:43:28	701.52	104	1688	379	738	757	32	10.65	1.84	0.3	7.20	7.44	0.5	133.59	81.57	0.89
12:43:36	701.77	105	1684	381	738	753	28	10.61	1.88	0.31	7.24	7.56	0.62	123.36	81.85	0.89
12:43:43	702.03	106	1687	386	739	753	28	10.59	1.83	0.24	7.26	7.58	0.68	131.32	82.09	0.9
12:43:50	702.28	105	1680	383	739	753	38	10.66	1.83	0.27	7.16	7.48	0.6	128.04	82.32	0.9
12:43:57	702.53	105	1689	384	739	753	28	10.67	1.84	0.29	7.18	7.54	0.67	132.08	82.57	0.9
12:44:04	702.78	106	1682	386	738	753	28	10.64	1.84	0.25	7.21	7.44	0.57	132.08	82.83	0.9
12:44:11	703.03	106	1701	385	738	753	38	10.65	1.83	0.27	7.19	7.46	0.55	124.50	83.07	0.9
12:44:17	703.29	106	1688	386	738	753	28	10.62	1.83	0.26	7.22	7.52	0.6	133.96	83.32	0.91
12:44:25	703.53	104	1677	380	739	753	28	10.61	1.84	0.28	7.23	7.52	0.57	124.74	83.58	0.91
12:44:32	703.78	107	1683	389	739	753	28	10.53	1.83	0.24	7.24	7.71	0.67	120.34	83.83	0.91
12:44:39	704.03	106	1654	383	738	753	38	10.54	1.84	0.29	7.30	7.59	0.6	125.38	84.09	0.91
12:44:47	704.28	106	1647	385	738	753	28	10.58	1.82	0.26	7.25	7.52	0.57	118.55	84.32	0.91
12:44:54	704.53	105	1664	383	738	753	28	10.55	1.83	0.23	7.30	7.64	0.67	128.35	84.58	0.92
12:45:01	704.78	105	1657	383	738	753	28	10.58	1.84	0.29	7.26	7.54	0.57	123.95	84.85	0.92
12:45:08	705.04	108	1673	382	739	757	32	10.62	1.85	0.28	7.22	7.52	0.65	126.90	85.11	0.92
12:45:15	705.29	104	1679	378	738	753	28	10.61	1.84	0.27	7.23	7.48	0.6	134.47	85.32	0.92
12:45:23	705.54	104	1677	360	739	753	28	10.61	1.95	0.28	7.23	7.64	0.6	121.07	85.58	0.92
12:45:30	705.79	105	1683	383	738	753	28	10.59	1.85	0.23	7.28	7.66	0.57	127.15	85.83	0.93
12:45:39	706.04	109	1642	387	738	753	28	10.5	1.85	0.26	7.33	7.64	0.6	114.23	86.08	0.93
12:45:45	706.29	102	1654	373	738	753	28	10.58	1.84	0.26	7.28	7.64	0.69	120.67	86.34	0.93
12:45:52	706.54	104	1673	380	738	757	32	10.62	1.86	0.29	7.23	7.54	0.69	133.33	86.6	0.93
12:45:59	706.79	109	1660	381	738	757	32	10.55	1.85	0.31	7.29	7.64	0.74	112.53	86.83	0.93
12:46:07	707.04	105	1647	383	738	753	28	10.5	1.86	0.26	7.23	7.61	0.62	135.61	87.11	0.94

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOCK LOAD	PEAK	DELTA	RROP	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	ft/s	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
12:42:14	707.29	105	1677	381	737	748	32	9.93	1.84	0.3	8.01	8.4	1.34	125.77	87.34	0.84
12:42:28	707.54	103	1707	388	737	746	38	9.85	1.85	0.28	8.06	8.4	0.74	140.08	87.58	0.84
12:42:37	707.79	104	1702	379	736	753	28	9.81	1.88	0.31	8.04	8.35	0.87	134.14	87.88	0.84
12:42:34	708.05	105	1707	384	736	753	38	9.81	1.87	0.31	8.04	8.35	0.87	129.51	88.1	0.84
12:42:48	708.3	104	1723	380	736	753	38	9.85	1.88	0.31	7.98	8.26	0.87	148.59	88.34	0.85
12:42:57	708.55	105	1721	385	736	753	28	9.81	1.88	0.35	8.03	8.4	0.74	137.15	88.58	0.85
12:42:53	708.8	106	1712	386	739	753	38	9.81	1.86	0.3	8.03	8.31	0.85	134.54	88.88	0.85
12:47:00	709.05	105	1709	382	739	753	28	9.78	1.86	0.31	8.06	8.43	0.72	139.23	89.12	0.85
12:47:07	709.3	105	1699	387	739	753	28	9.71	1.85	0.29	8.14	8.52	0.72	122.87	89.34	0.85
12:47:14	709.55	105	1702	381	738	753	28	9.74	1.86	0.31	8.10	8.43	0.8	134.08	89.64	0.85
12:47:21	709.8	105	1704	382	737	753	28	9.75	1.83	0.27	8.09	8.35	0.8	128.78	89.85	0.85
12:47:38	710.05	106	1689	383	737	753	28	9.75	1.84	0.28	8.09	8.35	0.8	129.14	90.11	0.85
12:47:35	710.3	104	1684	378	738	753	28	9.7	1.84	0.28	8.14	8.43	0.68	127.78	90.34	0.85
12:47:42	710.55	105	1687	382	736	748	28	9.75	1.85	0.29	8.09	8.35	0.87	124.98	90.5	0.85
12:47:49	710.8	103	1694	377	737	753	32	9.74	1.87	0.3	8.11	8.4	0.83	134.47	90.85	0.85
12:47:58	711.05	105	1682	381	738	753	28	9.74	1.87	0.31	8.10	8.38	0.6	128.96	91.11	0.87
12:48:03	711.3	103	1678	377	738	753	28	9.68	1.85	0.28	8.15	8.45	0.6	122.27	91.36	0.87
12:48:18	711.55	105	1676	385	739	753	28	9.68	1.83	0.27	8.19	8.47	0.82	125.91	91.61	0.87
12:48:14	711.81	105	1683	382	738	753	28	9.72	1.87	0.31	8.12	8.4	0.89	118.58	91.85	0.87
12:48:24	712.05	105	1669	382	738	753	28	9.73	1.85	0.27	8.12	8.38	0.87	138.86	92.13	0.87
12:48:32	712.31	104	1683	379	735	748	29	9.64	1.83	0.25	8.16	8.45	0.87	122.18	92.38	0.88
12:48:38	712.56	105	1649	384	736	753	32	9.62	1.85	0.3	8.22	8.5	0.5	112.96	92.65	0.88
12:48:47	712.81	105	1647	382	738	753	38	9.63	1.84	0.25	8.19	8.5	0.85	124.87	92.88	0.88
12:48:55	713.06	105	1686	384	738	757	35	9.65	1.84	0.25	8.18	8.45	0.53	114.51	93.11	0.88
12:49:02	713.31	105	1686	387	738	751	36	9.65	1.85	0.28	8.20	8.4	0.48	120.57	93.38	0.88
12:49:16	713.56	103	1678	375	738	753	38	9.67	1.84	0.25	8.17	8.43	0.53	128.98	93.6	0.89
12:49:17	713.81	105	1681	386	738	753	32	9.67	1.84	0.26	8.18	8.43	0.6	118.08	93.86	0.89
12:49:24	714.06	104	1681	377	736	748	24	9.59	1.84	0.24	8.15	8.43	0.62	131.04	94.13	0.89
12:49:33	714.31	104	1674	378	738	753	28	9.66	1.84	0.26	8.17	8.43	0.55	115.28	94.38	0.89
12:49:39	714.56	105	1669	381	738	753	28	9.66	1.83	0.23	8.18	8.45	0.53	125.84	94.6	0.89
12:49:47	714.81	106	1684	385	738	753	28	9.68	1.86	0.28	8.15	8.47	0.67	118.48	94.88	0.89
12:49:54	715.06	105	1678	384	738	753	28	9.69	1.86	0.28	8.15	8.43	0.55	122.55	95.11	0.89
12:50:01	715.31	106	1678	385	738	753	28	9.71	1.85	0.27	8.13	8.4	0.6	123.64	95.38	0.89
12:50:52	715.31	54	-6	206	734	765	61	17.66	2.07	0.87	8.04	3.25	6.65	42.50	95.48	1.01

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23	Date: 2/22/96																	
Starting Depth =	523.52	Bit Type =	Walker McDougal's MP65H															
Ending Depth =	1031.19	Bit Size =	4.75															
Total Depth Drilled	497.27	Bit Increases =	9, 9, 10, 12															
Hours On Bit =	4.08	Mud Type =	Water Based															
Average ROP =	89.58	Mud Weight (lb/gal) =	9.09															
Drillstring (ft) =	863.99	Pipe (ft) =	251.83	Collar (ft)	409.80													

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK		PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
								LOAD	Gr's								
HR:MM:SS	FEET	GPM	PSI	RPM	N-lbs	N-lbs	N-lbs	KPS	Gr's	Gr's	Gr's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
12:57:26	715.07	107	1336	389	742	757	41	8.91	1.81	0.3	1.04	3.4	3.83	100.74	95.53	1.01	
12:57:35	715.73	103	1387	375	745	751	77	8.34	1.83	0.24	5.49	3.28	5.03	96.71	95.79	1.01	
12:57:42	715.98	103	1612	373	742	757	29	8.06	1.86	0.25	8.87	3.45	1.41	125.34	96.05	1.02	
12:57:48	716.23	103	1658	375	741	753	24	8.43	1.86	0.27	8.52	3.79	0.62	141.96	96.3	1.02	
12:57:55	716.48	103	1708	375	741	757	32	8.4	1.88	0.26	8.59	3.77	0.45	137.19	96.54	1.02	
12:58:01	716.73	103	1751	378	741	757	32	8.4	1.86	0.31	8.54	3.79	0.57	138.56	96.8	1.02	
12:58:07	716.98	103	1779	375	741	757	32	8.46	1.9	0.37	3.48	3.79	0.67	160.82	97.06	1.02	
12:58:13	717.23	104	1807	378	743	757	32	8.48	1.87	0.33	3.37	3.74	0.6	141.86	97.26	1.02	
12:58:20	717.48	104	1799	378	743	753	28	8.45	1.88	0.29	9.50	3.81	0.56	149.39	97.52	1.03	
12:58:25	717.73	103	1780	375	741	757	32	8.46	1.89	0.31	9.48	3.74	0.49	154.93	97.8	1.03	
12:58:32	717.98	104	1766	389	741	757	32	8.43	1.84	0.38	8.52	3.74	0.43	136.32	98.05	1.03	
12:58:38	718.23	106	1760	389	741	757	28	8.39	1.89	0.39	9.66	3.79	0.45	141.67	98.29	1.03	
12:58:45	718.48	105	1754	383	743	757	28	8.38	1.85	0.36	9.66	3.86	0.3	133.22	98.52	1.03	
12:58:52	718.73	103	1747	376	741	757	33	8.36	1.86	0.28	9.56	3.85	0.3	128.57	98.78	1.04	
12:58:58	718.98	104	1746	379	742	757	28	8.34	1.85	0.28	3.61	3.85	0.48	126.92	99.04	1.04	
12:59:05	719.24	103	1784	377	743	757	32	8.35	1.83	0.26	9.66	3.84	0.48	124.66	99.29	1.04	
12:59:12	719.49	104	1779	370	742	757	28	8.33	1.84	0.26	9.81	3.81	0.43	140.67	99.54	1.04	
12:59:19	719.74	103	1765	370	742	757	28	8.33	1.85	0.26	3.82	3.89	0.3	133.37	99.78	1.04	
12:59:26	719.99	104	1751	378	742	757	32	8.35	1.85	0.29	9.83	3.86	0.43	129.43	100.03	1.04	
12:59:33	720.24	105	1756	382	742	757	28	8.37	1.85	0.29	9.89	3.79	0.5	142.04	100.28	1.05	
12:59:39	720.49	108	1763	385	743	757	28	8.38	1.85	0.29	9.81	3.89	0.48	130.25	100.53	1.05	
12:59:46	720.74	103	1753	374	742	757	28	8.33	1.86	0.36	9.62	3.85	0.58	137.39	100.8	1.05	
12:59:53	720.99	105	1741	383	741	757	32	8.31	1.86	0.36	9.65	3.85	0.5	136.44	101.04	1.05	
13:00:00	721.24	103	1729	377	743	757	28	8.3	1.87	0.31	9.65	3.85	0.43	127.46	101.29	1.05	
13:00:07	721.5	105	1721	382	743	757	29	8.31	1.84	0.25	9.64	3.89	0.5	134.28	101.54	1.06	
13:00:14	721.75	103	1720	375	743	757	29	8.33	1.83	0.28	9.69	3.89	0.48	133.41	101.79	1.06	
13:00:21	722	103	1717	375	742	757	29	8.31	1.86	0.3	9.83	3.86	0.45	133.27	102.04	1.06	
13:00:28	722.25	104	1715	378	743	757	28	8.31	1.83	0.25	9.84	3.91	0.5	125.99	102.29	1.06	
13:00:35	722.5	104	1726	378	741	757	32	8.33	1.87	0.31	9.82	3.89	0.53	130.25	102.55	1.06	
13:00:42	722.75	103	1721	375	742	757	28	8.32	1.84	0.38	9.82	3.89	0.5	135.98	102.82	1.07	
13:00:49	723	104	1722	378	742	757	28	8.23	1.84	0.29	9.81	3.83	0.57	126.96	103.08	1.07	
13:00:55	723.25	101	1726	370	743	757	28	8.25	1.89	0.32	9.80	3.84	0.49	141.48	103.3	1.07	
13:01:02	723.5	105	1715	382	742	757	28	8.34	1.9	0.34	9.68	3.91	0.55	125.87	103.56	1.07	
13:01:09	723.75	105	1724	381	743	757	28	8.36	1.82	0.23	9.88	3.81	0.48	131.65	103.8	1.07	

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
MM:SS	FEET	CPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	RIPS	KIPS	KIPS	FT/HR	OnBr	OnBr
13:01:18	734	104	1721	378	740	753	28	8.34	1.85	0.28	9.91	9.88	0.48	136.18	104.04	1.08
13:01:23	724.25	103	1730	385	740	757	32	8.36	1.83	0.25	9.60	9.84	0.5	124.89	104.31	1.08
13:01:28	734.5	105	1749	382	741	753	24	8.38	1.83	0.25	9.56	9.84	0.5	144.07	104.56	1.08
13:01:38	724.75	104	1749	380	742	757	28	8.38	1.85	0.28	9.58	9.81	0.48	131.60	104.6	1.08
13:01:43	735	105	1748	375	742	757	28	8.37	1.85	0.28	9.58	9.88	0.48	133.63	105.06	1.08
13:01:48	728.25	103	1751	375	742	757	28	8.36	1.85	0.31	9.58	9.81	0.48	133.82	105.32	1.08
13:01:57	728.5	106	1743	385	741	757	28	8.36	1.84	0.28	9.59	9.84	0.53	122.45	105.65	1.08
13:01:57	725.75	105	1739	378	741	757	28	8.33	1.85	0.27	9.61	9.86	0.5	133.63	105.91	1.08
13:02:11	736	106	1741	387	742	757	28	8.36	1.84	0.27	9.66	9.84	0.48	127.58	106.04	1.08
13:02:17	726.26	108	1783	384	742	757	28	8.38	1.86	0.31	9.57	9.89	0.65	115.46	106.32	1.08
13:02:24	726.5	103	1768	377	742	753	24	8.35	1.88	0.33	9.89	9.91	0.57	134.63	106.57	1.08
13:02:29	726.76	103	1784	377	741	753	24	8.38	1.87	0.33	9.55	9.96	0.58	137.68	106.83	1.1
13:02:37	727.01	103	1789	376	742	757	32	8.39	1.88	0.33	9.85	9.84	0.62	144.19	107.08	1.1
13:02:44	727.26	103	1771	378	742	757	28	8.41	1.87	0.31	9.83	9.84	0.65	138.31	107.3	1.1
13:02:50	727.51	106	1769	384	743	757	28	8.39	1.86	0.31	9.56	9.84	0.6	137.35	107.57	1.1
13:02:57	727.76	105	1747	382	743	757	24	8.35	1.88	0.32	9.58	9.91	0.57	137.27	107.81	1.1
13:03:04	728.01	104	1769	378	742	757	28	8.3	1.88	0.33	9.64	9.91	0.72	131.78	108.07	1.1
13:03:10	728.26	106	1757	383	741	757	28	8.39	1.89	0.33	9.55	9.86	0.6	143.77	108.3	1.1
13:03:17	728.51	106	1739	384	743	757	28	8.46	1.86	0.35	9.56	9.85	0.63	131.28	108.56	1.1
13:03:24	728.76	104	1738	383	743	757	28	8.36	1.87	0.31	9.58	9.84	0.57	132.47	108.81	1.1
13:03:30	729.01	105	1742	383	743	757	28	8.36	1.8	0.38	9.58	9.81	0.55	140.07	109.06	1.1
13:03:37	729.26	103	1787	377	743	757	24	8.44	1.88	0.33	9.49	9.77	0.5	135.08	109.31	1.1
13:03:43	729.51	106	1777	388	741	753	24	8.4	1.91	0.38	9.54	9.81	0.55	142.74	109.56	1.1
13:03:50	729.76	104	1751	386	742	757	28	8.31	1.91	0.39	9.63	9.88	0.72	128.63	109.81	1.1
13:03:57	730.01	106	1747	382	742	757	28	8.31	1.88	0.37	9.63	9.91	0.57	138.13	110.07	1.1
13:04:04	730.26	108	1756	385	742	757	28	8.33	1.91	0.39	9.82	9.96	0.62	134.21	110.32	1.1
13:04:11	730.52	106	1790	385	741	757	28	8.4	1.9	0.35	9.54	9.81	0.57	130.25	110.56	1.1
13:04:17	730.77	104	1787	386	741	757	28	8.38	1.88	0.33	9.58	9.95	0.6	138.12	110.81	1.1
13:04:24	731.02	107	1756	389	742	757	28	8.39	1.86	0.3	9.34	9.79	0.48	134.34	111.06	1.1
13:04:31	731.27	104	1721	377	743	757	24	8.31	1.86	0.29	9.63	9.91	0.53	129.71	111.31	1.1
13:04:38	731.52	104	1725	378	744	757	24	8.28	1.85	0.28	9.68	9.96	0.57	126.02	111.56	1.1
13:04:46	731.77	105	1743	383	743	757	28	8.33	1.85	0.28	9.62	9.88	0.6	121.69	111.81	1.1
13:04:53	732.02	104	1717	373	743	757	24	8.3	1.83	0.29	9.63	9.85	0.48	128.13	112.07	1.1
13:05:00	732.27	105	1735	384	743	757	24	8.35	1.85	0.28	9.69	9.84	0.53	131.05	112.31	1.1

DOE high power mortar test Amaco Catoosa Test Site

Well No. 33	Date: 2/22/98																
Starting Depth =	823.62	Bit Type =	Walker McDougal 6P65H														
Ending Depth =	1631.18	Bit Size =	4.75														
Total Depth Drilled	407.27	Bit Nozzles =	9, 9, 12, 12														
Hours On Bit =	4.09	Mud Type =	Water Based														
Average ROP =	99.58	Mud Weight (lbs/gal) =	9.8														
Casing (ft) =	666.49	Pipe (ft) =	351.91					Collar (ft)	408.69								

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HR:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
13:05:07	732.53	109	1725	383	743	757	24	8.35	1.85	0.38	9.58	9.91	0.52	132.39	112.36	1.14
13:05:13	732.77	106	1735	384	744	757	28	8.36	1.83	0.34	9.58	9.89	0.6	137.54	112.83	1.14
13:05:20	733.02	105	1745	381	744	757	24	8.37	1.84	0.27	9.57	9.84	0.53	121.46	113.37	1.14
13:05:27	733.27	104	1721	379	744	761	28	8.34	1.86	0.39	9.60	9.89	0.5	132.89	113.31	1.15
13:05:34	733.52	106	1724	385	744	761	28	8.34	1.83	0.24	9.59	9.91	0.57	133.82	113.88	1.15
13:05:41	733.77	105	1721	383	744	757	24	8.35	1.85	0.25	9.61	9.86	0.5	124.15	113.82	1.15
13:05:48	734.02	106	1685	387	744	757	24	8.28	1.82	0.38	9.64	9.94	0.48	128.92	114.08	1.15
13:05:56	734.28	105	1675	383	743	757	28	8.28	1.85	0.25	9.66	9.96	0.53	116.26	114.33	1.15
13:06:03	734.53	108	1675	392	743	757	24	8.3	1.82	0.39	9.64	9.86	0.5	130.01	114.38	1.15
13:06:10	734.78	104	1639	379	744	757	28	8.24	1.82	0.21	9.69	10.03	0.55	124.24	114.92	1.16
13:06:17	735.03	103	1742	372	742	757	28	8.35	1.83	0.26	9.58	9.84	0.5	124.16	115.08	1.16
13:06:24	735.28	104	1631	391	742	757	24	8.38	1.81	0.21	9.56	9.84	0.6	140.88	115.35	1.16
13:06:31	735.53	108	1629	383	741	753	24	8.38	1.81	0.21	9.58	9.91	0.6	133.91	115.60	1.16
13:06:37	735.78	108	1628	383	743	757	24	8.38	1.83	0.21	9.55	9.85	0.57	138.53	115.84	1.16
13:06:44	736.03	109	1632	387	744	757	28	8.35	1.84	0.24	9.57	9.84	0.6	134.57	116.06	1.17
13:06:51	736.28	106	1614	387	744	757	24	8.28	1.83	0.21	9.65	9.86	0.62	132.70	116.33	1.17
13:06:58	736.53	105	1615	381	744	757	24	8.27	1.81	0.19	9.65	9.86	0.57	128.00	116.67	1.17
13:07:04	736.78	104	1666	380	744	757	28	8.78	1.84	0.25	9.14	9.77	1.01	170.89	116.83	1.17
13:07:10	737.03	108	1654	382	744	757	24	8.54	1.87	0.3	9.39	9.74	0.67	154.72	117.1	1.17
13:07:16	737.28	108	1649	387	744	757	24	8.49	1.85	0.26	9.48	9.74	0.5	145.83	117.33	1.18
13:07:22	737.53	108	1613	391	743	757	28	8.41	1.85	0.26	9.52	9.84	0.6	135.54	117.59	1.18
13:07:28	737.79	107	1691	388	743	757	28	8.45	1.82	0.39	9.48	9.72	0.55	162.98	117.83	1.18
13:07:36	738.04	107	1613	390	744	757	24	8.43	1.84	0.27	9.51	9.81	0.79	151.69	118.1	1.18
13:07:42	738.29	108	1646	385	743	757	28	8.21	1.84	0.25	9.62	9.81	0.62	124.80	118.34	1.18
13:07:49	738.54	109	1669	386	743	757	28	8.35	1.85	0.27	9.55	9.91	0.65	137.35	118.59	1.18
13:07:57	738.79	108	1638	385	744	757	28	8.18	1.84	0.29	9.77	10.2	0.93	187.08	118.84	1.19
13:08:06	739.04	105	1668	384	744	761	28	8.93	1.84	0.28	9.81	10.36	1.05	203.98	119.1	1.19
13:08:15	739.29	105	1637	382	744	757	28	8.1	1.83	0.27	9.83	10.2	0.89	98.68	119.34	1.19
13:08:23	739.54	107	1649	389	743	757	24	8.16	1.85	0.28	9.77	10.08	0.67	119.47	119.61	1.19
13:08:30	739.79	104	1633	375	744	757	24	8.25	1.85	0.27	9.68	10.05	0.88	158.41	119.85	1.2
13:08:38	740.04	103	1657	375	744	757	24	8.19	1.85	0.25	9.74	10.05	0.77	112.77	120.09	1.2
13:08:45	740.29	106	1637	385	744	767	24	8.32	1.88	0.3	9.81	9.93	0.86	138.71	120.34	1.2
13:08:52	740.54	101	1678	368	744	757	24	8.43	1.88	0.35	9.50	9.84	0.72	153.24	120.62	1.2
13:09:00	740.8	102	1637	372	743	757	28	8.49	1.88	0.29	9.44	9.84	0.79	151.77	120.85	1.2

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23		Date: 2/22/96		Well Type =		Walker McDonald MP68K		Well Size =		4.75		Well No. =		9, 9, 12, 12		Mud Type =		Water Based		Mud Weight (lb/gal) =		9.00		Pipe (I) =		351.81		Casing (II) =		305.60	
Starting Depth =		623.62		Ending Depth =		1031.19		Total Depth Drilled		407.27		Hours On Bit =		4.09		Average ROP =		59.58		Drillstring (II) =		580.48									
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	FEAR	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours															
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit															
13:08:04	741.05	107	1839	388	742	757	28	8.47	1.81	0.18	9.48	9.64	0.77	151.33	121.1	1.21															
13:08:10	741.3	108	1789	384	744	757	24	8.53	1.83	0.19	9.43	9.77	0.69	149.70	121.35	1.21															
13:08:15	741.55	109	1739	395	744	757	24	8.58	1.81	0.15	9.37	9.72	0.66	153.72	121.6	1.21															
13:08:21	741.8	107	1690	388	744	757	24	8.56	1.8	0.14	9.38	9.74	0.81	147.51	121.85	1.21															
13:08:28	742.05	105	1693	381	744	757	28	8.33	1.8	0.15	9.60	10.08	0.93	136.95	122.12	1.21															
13:08:34	742.3	107	1653	388	743	757	28	7.93	1.79	0.12	10.01	10.29	0.72	122.97	122.34	1.22															
13:08:40	742.55	106	1690	387	744	757	28	8.12	1.81	0.17	9.81	10.29	1.01	100.74	122.52	1.22															
13:08:46	742.8	104	1728	377	742	757	28	8.48	1.8	0.16	9.45	9.84	0.77	151.14	122.85	1.22															
13:10:01	743.05	107	1699	388	744	757	24	8.39	1.81	0.15	9.54	9.89	0.66	128.58	123.11	1.22															
13:10:07	743.3	107	1673	388	744	757	24	8.47	1.81	0.15	9.48	9.79	0.81	148.79	123.34	1.22															
13:10:13	743.55	104	1788	379	744	757	24	8.3	1.81	0.16	9.53	9.89	0.81	136.99	123.62	1.22															
13:10:20	743.8	102	1840	372	744	757	24	8.51	1.82	0.19	9.43	9.77	0.69	149.63	123.87	1.23															
13:10:26	744.05	103	1829	375	743	757	28	8.59	1.81	0.16	9.28	9.87	0.74	179.78	124.13	1.23															
13:10:33	744.3	108	1702	388	743	757	28	8.28	1.8	0.13	9.54	10.17	1.24	114.74	124.34	1.23															
13:10:42	744.55	108	1698	378	743	757	24	8.08	1.8	0.14	9.85	10.22	0.96	100.25	124.8	1.23															
13:10:49	744.8	104	1704	378	744	757	28	8.16	1.79	0.12	9.78	10.1	0.69	114.95	124.85	1.23															
13:10:55	745.05	108	1793	387	743	757	24	8.32	1.8	0.14	9.41	9.84	0.81	138.46	125.09	1.24															
13:11:02	745.3	104	1759	380	743	757	24	8.32	1.81	0.17	9.40	9.77	0.79	154.34	125.35	1.24															
13:11:08	745.55	106	1696	368	745	757	28	8.19	1.79	0.13	9.45	9.74	0.69	140.38	125.6	1.24															
13:11:14	745.81	103	1679	375	743	757	24	8.34	1.8	0.14	9.39	9.74	0.74	157.63	125.86	1.24															
13:11:21	746.05	105	1658	384	743	757	24	8.3	1.79	0.12	9.48	9.77	0.67	149.20	126.11	1.24															
13:11:27	746.31	105	1691	381	742	758	24	8.42	1.8	0.14	9.51	9.81	0.78	132.03	126.35	1.25															
13:11:33	746.55	106	1656	388	742	753	24	8.44	1.8	0.13	9.48	9.79	0.65	145.14	126.6	1.25															
13:18:24	747.08	69	808	257	743	781	49	13.98	1.87	0.31	4.35	10.17	9.07	38.34	127.15	1.26															
13:19:35	747.33	64	1144	230	744	757	24	5.49	2.06	0.54	11.84	13.89	3.9	88.67	127.39	1.26															
13:19:43	747.58	64	1144	239	744	757	24	5.67	1.85	0.44	12.57	14.05	2.42	110.63	127.64	1.26															
13:19:50	747.83	60	1213	225	745	781	28	5.89	1.97	0.49	11.74	12.89	0.3	132.18	127.88	1.26															
13:19:56	748.08	60	1387	223	749	789	48	6.84	4.05	4.03	11.49	12.83	8.74	138.83	128.13	1.27															
13:20:21	748.33	68	775	253	743	789	69	16.5	2.09	0.64	1.78	7.35	8.82	36.48	128.37	1.27															
13:20:32	748.58	65	870	241	745	781	28	8.44	1.84	0.22	8.67	11.13	6.15	82.80	128.54	1.27															
13:21:09	748.83	58	1632	206	744	757	28	6.6	1.98	0.49	11.72	14	10.58	37.45	128.58	1.28															
13:21:14	749.08	67	891	251	743	757	38	12.42	1.88	0.29	8.85	7.97	3.78	67.80	129.12	1.28															
13:21:23	749.33	64	1095	241	742	753	34	6.2	1.83	0.22	10.11	11.98	4.07	82.77	129.37	1.29															
13:21:33	749.58	60	1257	228	742	757	28	5.99	1.87	0.3	12.74	13.5	1.75	80.95	129.61	1.29															

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HDOR	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	%	%	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
13:21:44	748.83	58	1399	218	743	757	28	5.27	1.89	0.35	13.08	14.31	1.82	81.68	129.89	1.29
13:21:53	753.99	52	1388	232	741	757	28	5.78	1.9	0.32	12.54	13.02	0.77	103.89	130.13	1.3
13:22:03	758.34	53	1292	234	743	757	28	5.75	1.82	0.37	12.57	13	0.69	99.29	130.38	1.3
13:22:13	758.99	59	1252	229	743	757	28	5.81	1.89	0.38	12.53	13.81	0.55	108.10	130.56	1.3
13:22:23	759.54	52	1235	231	743	757	28	5.71	1.94	0.37	12.62	12.93	0.62	90.95	130.89	1.3
13:22:31	751.09	58	1286	217	743	757	28	5.74	1.89	0.31	12.59	12.88	0.65	95.44	131.13	1.31
13:22:41	751.34	52	1177	236	743	757	28	5.82	1.87	0.27	12.71	12.97	0.53	88.15	131.38	1.31
13:22:55	751.58	53	1191	238	743	757	28	5.83	1.89	0.28	12.88	13.07	0.53	88.38	131.64	1.31
13:23:07	751.84	53	1189	217	743	761	28	5.51	1.87	0.25	12.82	13.14	0.58	79.49	131.89	1.32
13:23:25	752.89	51	1235	228	743	757	28	5.43	1.92	0.37	12.89	13.38	0.56	59.35	132.12	1.32
13:23:38	752.34	53	1212	234	741	753	28	5.88	1.86	0.31	12.75	13.12	0.65	73.75	132.4	1.32
13:23:51	752.89	54	1182	237	742	757	28	5.84	1.88	0.3	12.78	13.09	0.62	79.42	132.66	1.32
13:24:06	752.84	53	1185	238	743	757	28	5.44	1.88	0.25	12.68	13.24	0.72	59.53	132.89	1.32
13:24:26	753.09	53	1185	234	743	757	28	5.33	1.89	0.27	12.89	13.35	0.85	45.29	133.13	1.34
13:24:42	753.34	53	1217	237	743	757	28	5.47	1.9	0.3	12.89	13.17	0.6	58.91	133.38	1.34
13:24:58	753.89	59	1273	225	743	757	28	5.45	1.91	0.31	12.87	13.31	0.77	52.98	133.64	1.35
13:25:11	753.84	59	1384	228	743	757	28	5.48	1.91	0.31	12.85	13.45	0.98	80.93	133.89	1.35
13:25:28	754.09	52	1292	238	743	757	28	5.48	1.9	0.33	13.85	13.4	0.56	65.67	134.15	1.35
13:25:38	754.26	59	1382	229	743	761	41	8.24	2.12	0.55	10.07	13.69	0.46	20.44	134.32	1.35
13:26:23	754.21	54	1051	239	744	757	28	11.39	1.89	0.41	6.98	13.29	14.37	18.35	134.45	1.37
13:26:53	754.89	54	1141	238	743	757	28	6.52	1.92	0.32	11.79	12.78	5.39	31.98	134.72	1.38
13:27:14	754.81	54	1111	246	743	757	28	5.97	1.9	0.3	12.35	12.71	0.82	43.51	134.95	1.38
13:27:44	755.15	56	1044	246	746	757	32	5.9	1.89	0.24	12.42	12.73	0.97	27.56	135.19	1.38
13:28:14	755.37	56	1018	246	741	757	28	5.85	1.84	0.23	12.46	12.78	0.85	28.58	135.41	1.38
13:28:39	755.85	55	1070	242	739	753	24	5.85	1.84	0.24	12.37	12.89	0.6	41.09	135.67	1.41
13:28:59	755.87	55	1093	243	748	753	23	5.97	1.89	0.19	12.34	12.59	0.87	39.08	135.92	1.41
13:29:21	756.19	55	1082	241	749	757	32	5.7	1.89	0.21	12.81	13.45	1.29	40.08	136.16	1.42
13:29:48	758.37	51	1230	228	741	757	32	6.95	1.94	0.35	11.98	13.61	6.97	32.67	136.41	1.43
13:30:15	758.62	53	1149	335	743	757	28	5.94	1.9	0.3	12.95	12.78	0.61	39.90	136.67	1.43
13:30:48	758.8	52	1270	332	749	757	32	6.17	1.87	0.34	12.14	13.09	1.3	21.01	136.85	1.44
13:31:15	758.88	55	909	244	741	759	35	16.23	2.1	0.67	3.03	9.48	10.27	6.34	136.9	1.45
13:31:48	757.08	56	944	245	741	757	32	6.34	1.85	0.32	8.95	10.7	5.46	24.78	137.1	1.46
13:32:07	757.34	52	1089	232	742	759	32	7.88	1.88	0.27	11.42	10.1	0.87	43.86	137.36	1.46
13:32:37	757.49	55	999	243	742	757	32	7.72	1.85	0.33	10.67	10.98	0.84	21.91	137.54	1.47

DOE High power motor test Amaco Catrosa Test Site

TIME	DEPTH (FEET)	FLOW (GPM)	PRESS (PSI)	SPEED (RPM)	TORQUE (LBS)	PEAK (LBS)	DRIFT (IN)	LOAD (KIPS)	PEAK (KIPS)	TELLTA (IN)	WOS (KIPS)	PEAK (KIPS)	DELTA (KIPS)	POP (KIPS)	FEET (IN)	HOURS (HRS)
13:33:02	757.54	65	632	234	741	757	32	7.71	1.68	0.23	10.58	10.92	0.3	17.65	137.59	1.48
13:33:37	757.94	60	1152	227	742	761	32	9.45	2.03	0.34	8.84	11.08	2.24	4.25	137.59	1.49
13:33:51	757.09	63	718	255	743	757	28	46.19	1.8	0.15	2.07	5.39	3.59	63.43	137.94	1.49
13:34:21	758.08	65	605	246	743	757	28	9.22	1.85	0.22	9.05	19.85	10.8	24.18	138.54	1.5
13:34:51	758.32	63	1063	250	744	757	28	9.1	1.85	0.28	9.18	16.6	7.41	27.05	138.56	1.51
13:35:19	758.57	64	1183	238	744	761	25	18.14	1.87	0.32	8.14	8.52	1.34	32.05	138.57	1.52
13:35:38	758.43	67	1220	248	743	757	28	19.18	1.85	0.33	8.16	8.4	0.25	34.48	138.86	1.52
13:35:56	759.07	65	1219	241	743	757	26	19.24	1.91	0.35	8.04	8.35	0.3	60.55	139.15	1.53
13:36:06	759.07	65	1231	240	741	757	41	10	1.86	0.28	8.29	9.55	1.25	59.47	139.37	1.53
13:36:21	759.57	65	1384	237	736	753	26	8.35	1.89	0.34	10.14	10.77	0.63	50.58	139.62	1.53
13:36:51	759.71	65	1600	234	741	823	97	12.8	1.53	0.58	8.49	11.01	2.52	12.72	139.76	1.54
13:37:17	759.97	66	984	267	745	763	36	43.69	1.56	0.2	8.57	8.27	0.27	33.62	140.01	1.55
13:37:34	760.22	67	1123	250	748	757	32	18.84	1.87	0.29	7.81	8.31	0.5	40.41	140.26	1.55
13:37:52	760.47	66	1232	245	748	757	32	18.33	1.87	0.27	7.96	8.25	0.3	67.87	140.52	1.56
13:38:07	760.72	67	1235	248	748	757	32	18.34	1.83	0.25	7.94	8.19	0.15	64.29	140.75	1.56
13:38:26	760.57	68	1151	252	738	757	32	18.22	1.83	0.21	8.05	8.35	0.35	67.95	141.01	1.57
13:38:40	761.22	67	1182	261	739	757	32	18.22	1.82	0.25	8.01	8.28	0.27	67.95	141.27	1.57
13:38:54	761.47	68	1123	246	739	753	29	18.34	1.98	0.28	7.83	8.39	0.56	53.56	141.52	1.58
13:39:09	761.72	68	1215	252	739	753	28	18.34	1.87	0.24	7.95	8.21	0.26	68.34	141.76	1.58
13:39:22	761.97	68	1303	246	739	757	32	18.32	1.84	0.23	7.93	8.21	0.28	64.58	142.01	1.59
13:39:37	762.22	68	1210	258	738	738	28	18.32	1.98	0.28	7.95	8.19	0.25	60.19	142.27	1.59
13:39:56	762.47	68	1312	245	738	738	28	18.33	1.85	0.22	7.85	8.19	0.35	68.17	142.52	1.59
13:40:05	762.72	68	1300	244	738	757	32	18.3	1.88	0.28	7.88	8.31	0.43	60.09	142.78	1.6
13:40:24	762.97	68	1160	253	739	751	32	18.31	1.82	0.21	7.86	8.16	0.31	63.17	143.03	1.6
13:40:44	763.22	68	1175	249	739	751	32	18.33	1.82	0.19	7.93	8.23	0.3	64.18	143.27	1.6
13:40:54	763.47	67	1175	249	739	751	32	18.33	1.85	0.22	7.94	8.19	0.21	64.18	143.52	1.6
13:41:08	763.72	68	1185	253	739	751	28	18.29	1.88	0.25	7.92	8.19	0.21	64.18	143.76	1.61
13:41:17	763.97	69	1186	257	739	753	28	18.33	1.95	0.29	7.95	8.25	0.3	61.26	144.01	1.61
13:41:32	764.22	67	1228	248	740	757	32	18.3	1.85	0.22	7.98	8.25	0.27	63.79	144.27	1.62
13:41:46	764.47	68	1185	255	740	753	26	18.34	1.85	0.21	7.93	8.21	0.21	64.24	144.52	1.62
13:42:05	764.72	67	1215	280	740	753	32	18.3	1.83	0.18	7.93	8.17	0.02	64.24	144.77	1.63
13:42:29	764.97	68	1226	282	749	753	28	18.27	1.85	0.23	8.03	8.33	0.3	47.85	144.78	1.63
13:42:35	765.22	67	1210	249	741	757	32	18.26	1.85	0.23	7.92	8.38	0.46	44.5	145.03	1.63
13:43:02	765.47	66	1688	257	741	757	32	18.09	1.82	0.17	8.18	8.47	0.29	59.85	145.28	1.64

Steel No. 33
 Starting Depth = 628.92
 Ending Depth = 1031.18
 Total Depth Gained = 402.27
 Hours On ER = 4.09
 Average POP = 55.28
 Discharge (G) = 850.45

Air Type = Washer Mechanism Fresh
 Air Size = 4.75
 Air Nozzle = 5, 8, 12, 15
 Hand Type = Washer Based
 Hand Weight (lbs) = 9.50
 Pipe (in) = 2.51 (1)

Motor (HP) = 408.60

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23	Date: 2/22/98																	
Starting Depth =	633.81					Bit Type =	Walker McGowan MP68H											
Ending Depth =	1031.18					Bit Size =	4.75											
Total Depth Drilled	407.27					Bit Nozzles =	8, 9, 12, 12											
Hours On Bit =	4.69					Mud Type =	Water Based											
Average ROP =	90.68					Mud Weight (lbs/gal) =	9.00											
Drilling (ft) =	669.49					Pipe (ft) =	251.81			Collar (ft)	408.69							

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	LOAD	Gr's	Gr's	KIPS	KIPS	KIPS	FT/HR	OnSh	OnSh
13:43:25	765.73	59	1147	257	741	757	28	10.12	1.85	0.31	8.14	8.45	0.74	38.20	145.76	1.65
13:43:45	765.98	58	1175	254	741	758	28	10.19	1.85	0.21	8.08	8.4	0.72	46.20	146.01	1.68
13:43:58	766.23	57	1162	250	740	757	32	10.13	1.84	0.23	8.13	8.43	0.68	36.72	146.37	1.68
13:44:27	766.48	58	1179	252	740	757	32	10.18	1.83	0.23	8.08	8.38	0.6	47.30	146.62	1.67
13:44:44	766.73	58	1170	253	740	757	32	10.21	1.83	0.18	8.06	8.31	0.5	51.85	146.76	1.67
13:45:03	766.98	59	1102	255	740	753	28	10.21	1.84	0.2	8.05	8.35	0.6	51.24	147.02	1.68
13:45:18	767.23	57	1133	256	738	753	28	10.25	1.84	0.19	8.02	8.28	0.58	53.68	147.27	1.68
13:45:35	767.48	59	1096	255	740	753	28	10.21	1.83	0.23	8.05	8.33	0.57	52.94	147.53	1.68
13:45:49	767.73	57	1184	248	739	753	28	10.38	1.85	0.23	7.91	8.19	0.55	67.27	147.78	1.69
13:46:03	767.98	58	1182	265	738	753	28	10.3	1.83	0.21	7.97	8.25	0.6	60.88	148.02	1.69
13:46:17	768.23	59	1124	255	738	753	28	10.31	1.84	0.22	7.98	8.21	0.53	64.67	148.28	1.7
13:46:35	768.48	57	1162	250	738	753	28	10.33	1.84	0.2	7.94	8.21	0.59	63.17	148.63	1.7
13:46:45	768.73	57	1264	246	738	753	28	10.31	1.84	0.21	7.96	8.23	0.55	57.32	148.78	1.71
13:47:00	768.98	58	1185	245	739	753	28	10.29	1.85	0.22	7.97	8.31	0.6	61.25	149.02	1.71
13:47:14	769.23	70	1150	259	739	753	28	10.3	1.82	0.18	7.96	8.28	0.6	61.21	149.28	1.71
13:47:30	769.48	57	1192	249	738	753	28	10.25	1.83	0.19	8.01	8.31	0.6	59.87	149.53	1.72
13:47:46	769.73	58	1225	250	739	753	28	10.37	1.84	0.22	7.99	8.33	0.67	55.47	149.79	1.72
13:48:01	769.98	58	1210	248	739	753	28	10.35	1.83	0.2	8.02	8.35	0.62	60.91	150.02	1.73
13:48:15	770.23	58	1201	252	739	757	32	10.38	1.85	0.24	7.98	8.33	0.65	60.06	150.28	1.73
13:48:29	770.48	57	1253	251	737	753	32	10.35	1.84	0.24	7.93	8.26	0.6	67.88	150.53	1.73
13:48:42	770.73	57	1179	250	738	753	28	10.36	1.84	0.23	7.90	8.19	0.62	71.16	150.77	1.74
13:48:58	770.98	57	1166	246	737	753	28	10.28	1.85	0.21	7.99	8.31	0.65	65.82	151.02	1.74
13:49:15	771.23	57	1168	250	736	753	28	10.33	1.82	0.19	7.93	8.23	0.6	73.81	151.26	1.75
13:49:25	771.48	59	1150	255	739	753	28	10.25	1.84	0.19	8.01	8.26	0.6	59.88	151.53	1.75
13:49:45	771.73	57	1228	248	738	755	25	10.18	1.86	0.21	8.09	8.35	0.69	47.87	151.79	1.75
13:49:58	771.98	57	1231	249	739	753	28	10.27	1.85	0.24	8.10	8.33	0.74	63.20	152.03	1.75
13:50:17	772.23	59	1213	246	739	753	28	10.21	1.83	0.2	8.05	8.35	0.65	50.44	152.28	1.75
13:50:33	772.48	57	1199	249	738	753	28	10.21	1.83	0.2	8.03	8.43	0.78	55.03	152.54	1.77
13:50:48	772.73	57	1165	251	739	753	38	10.27	1.83	0.19	7.93	8.33	0.65	50.79	152.79	1.77
13:51:03	772.98	57	1148	249	738	753	38	10.27	1.84	0.2	7.99	8.39	0.5	61.96	153.03	1.78
13:51:18	773.24	58	1198	247	738	757	32	10.27	1.85	0.2	7.95	8.26	0.57	61.22	153.28	1.78
13:51:33	773.49	57	1169	248	739	753	28	10.29	1.81	0.18	7.98	8.21	0.48	58.82	153.54	1.78
13:51:47	773.74	59	1207	248	738	753	28	10.26	1.82	0.18	8.00	8.26	0.57	65.29	153.79	1.79
13:52:01	773.99	59	1154	258	738	753	32	10.27	1.83	0.17	7.98	8.23	0.57	63.37	154.05	1.79

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRESS	SPEED	TORQUE	PEAK	DELTA	LOAD	PEAK	DELTA	WOB	PEAR	DELTA	ROP	Feed	Hours
HEIGHTS	FEET	QPM	PSI	FEET	FT/LBS	FT/LBS	FT/LBS	KIPS	QZ	QZ	KIPS	KIPS	KIPG	FT/HR	DMR	OPER
14:01:37	762.55	186	1777	382	741	753	26	12.53	2.12	0.55	5.92	6.1	0.6	128.89	162.63	1.9
14:03:45	762.84	181	1805	379	740	757	28	12.46	1.99	0.53	5.89	6.3	0.77	128.63	162.88	1.9
14:03:52	763.05	183	1808	375	741	751	24	12.46	2.03	0.57	5.86	6.13	0.53	134.75	163.14	1.9
14:03:59	763.34	185	1775	386	740	755	28	12.53	1.98	0.56	5.92	6.13	0.5	134.18	163.38	1.9
14:04:06	763.55	185	1742	381	740	755	28	12.46	1.88	0.49	5.88	5.18	0.5	113.88	163.55	1.9
14:04:14	763.84	188	1715	385	740	755	33	12.43	1.84	0.44	5.85	5.27	0.69	118.74	163.85	1.91
14:04:21	764.15	197	1714	391	741	757	38	12.45	1.97	0.48	5.90	5.18	0.6	128.53	164.14	1.93
14:04:29	764.36	198	1713	385	740	757	38	12.47	1.95	0.47	5.87	5.18	0.55	134.51	164.38	1.93
14:04:36	764.59	195	1748	383	741	755	24	12.5	2.03	0.54	5.84	5.13	0.62	139.41	164.62	1.93
14:04:43	764.81	192	1755	390	743	757	28	12.53	1.99	0.51	5.85	5.13	0.58	121.58	164.91	1.93
14:04:51	765.09	197	1742	386	740	757	32	12.53	2.02	0.5	5.81	5.09	0.5	128.14	165.15	1.93
14:04:57	765.34	193	1759	393	741	757	28	12.52	1.99	0.46	5.82	5.12	0.5	133.02	165.38	1.93
14:05:05	765.59	198	1755	385	742	757	24	12.52	1.97	0.46	5.82	5.1	0.67	139.15	165.65	1.92
14:05:12	765.84	195	1744	382	741	753	24	12.5	2.01	0.51	5.84	5.1	0.58	139.15	165.89	1.92
14:05:19	766.08	196	1740	384	741	757	28	12.5	1.94	0.41	5.88	5.1	0.58	139.17	166.14	1.93
14:05:27	766.34	196	1735	385	738	757	32	12.47	1.96	0.46	5.87	5.15	0.58	139.17	166.4	1.93
14:05:34	766.59	197	1722	390	741	757	28	12.44	1.95	0.41	5.90	5.22	0.55	128.70	166.69	1.93
14:05:42	766.84	197	1723	383	741	753	24	12.42	1.88	0.42	5.88	5.15	0.53	110.48	166.92	1.93
14:05:49	767.08	196	1791	385	741	753	24	12.41	1.94	0.42	5.93	5.25	0.65	131.02	167.18	1.93
14:05:56	767.34	196	1692	387	740	757	26	12.17	1.94	0.4	5.97	5.22	0.61	108.36	167.42	1.94
14:06:03	767.59	187	1634	385	741	757	28	12.31	1.89	0.31	6.03	5.32	0.53	108.36	167.65	1.94
14:06:10	767.85	187	1634	385	741	757	28	12.31	1.85	0.42	6.03	5.32	0.53	108.36	167.89	1.94
14:06:17	768.1	196	1693	385	740	753	24	12.31	1.9	0.42	6.03	5.3	0.53	114.12	168.14	1.94
14:06:24	768.36	196	1643	387	740	753	24	12.21	1.9	0.42	6.13	5.3	0.53	97.17	168.38	1.94
14:06:31	768.61	197	1676	389	740	753	24	11.86	1.91	0.31	6.09	5.1	0.89	125.73	168.62	1.95
14:06:38	768.86	197	1674	388	740	753	24	11.27	1.9	0.36	6.07	5.1	0.89	115.40	168.86	1.95
14:06:45	769.11	198	1674	388	740	753	24	11.27	1.9	0.36	6.07	5.1	0.89	115.40	169.1	1.95
14:06:52	769.36	198	1669	382	741	753	24	11.26	1.86	0.35	6.05	5.1	0.89	115.40	169.34	1.95
14:06:59	769.61	198	1669	382	741	753	24	11.26	1.86	0.35	6.05	5.1	0.89	115.40	169.58	1.95
14:07:06	769.86	198	1646	386	740	753	20	11.27	1.83	0.37	6.07	5.1	0.89	112.1	169.82	1.95
14:07:13	770.11	197	1638	390	740	753	20	11.27	1.83	0.36	6.11	5.1	0.89	128.73	170.06	1.95
14:07:20	770.36	198	1755	385	741	753	24	11.31	1.89	0.45	6.08	5.1	0.85	127.61	170.31	1.95
14:07:27	770.61	197	1663	390	740	753	24	11.29	1.88	0.35	6.05	5.1	0.85	130.87	170.55	1.95
14:07:34	770.86	196	1728	385	740	753	24	11.28	1.94	0.4	6.07	5.1	0.8	114.17	170.85	1.95
14:07:41	771.11	196	1728	385	740	753	24	11.28	1.94	0.41	6.15	5.1	0.65	128.42	171.09	1.97

Well No: 23 Date: 2/27/98
 Starting Depth = 625.52
 Ending Depth = 631.16
 Total Counts Deleted = 407.27
 State Of Bit = 4.09
 Average ROP = 39.28
 Logging ID = 00049
 Bit Type = Water Molarious APRESH
 Bit Size = 4.75
 Bit Record = 9.9.12.13
 Mud Type = Water Based
 Mud Weight (lb/gal) =
 Pipe ID = 251.83
 Collar ID = 400.30

DOE high power mortar test Amaco Catonsa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOCK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	%	G's	KIPS	KIPS	KIPS	FT/MIN	OnBit	OnBit
14:07:54	781.1	196	1723	495	740	753	24	11.25	1.94	0.44	7.08	7.42	0.77	115.13	171.18	1.97
14:08:02	791.35	195	1713	382	740	753	25	11.29	2	0.58	7.08	7.42	0.69	117.30	171.4	1.97
14:08:08	791.5	196	1705	387	740	753	24	11.3	1.93	0.4	7.04	7.37	0.67	127.21	171.55	1.97
14:08:17	791.85	197	1696	390	738	753	28	11.29	1.91	0.38	7.07	7.37	0.6	105.96	171.9	1.98
14:08:25	792.1	196	1717	387	738	753	28	11.27	1.94	0.4	7.07	7.47	0.74	126.72	172.18	1.98
14:08:33	792.35	195	1724	393	740	753	28	11.31	1.94	0.34	7.03	7.4	0.69	118.84	172.4	1.98
14:08:40	792.61	197	1710	390	741	753	24	11.29	1.94	0.44	7.05	7.42	0.72	118.12	172.65	1.98
14:08:47	792.85	196	1711	385	739	753	24	11.3	1.94	0.45	7.04	7.47	0.86	124.47	172.9	1.98
14:08:55	793.11	198	1723	379	741	757	28	11.29	1.99	0.52	7.05	7.42	0.74	114.31	173.18	1.99
14:09:03	793.36	197	1733	389	740	753	24	11.29	1.93	0.4	7.05	7.37	0.67	128.84	173.4	1.99
14:09:10	793.61	197	1746	398	741	753	24	11.32	2.03	0.55	7.02	7.32	0.65	118.25	173.55	1.99
14:09:18	793.85	197	1694	390	739	753	28	11.32	1.95	0.42	7.02	7.35	0.65	122.33	173.92	1.99
14:09:25	794.11	199	1722	387	740	753	24	11.31	1.94	0.42	7.03	7.4	0.79	128.84	174.16	1.99
14:09:33	794.36	195	1715	382	740	757	32	11.32	1.95	0.44	7.01	7.3	0.74	112.94	174.32	2
14:09:39	794.61	197	1711	388	741	791	35	11.31	1.94	0.43	7.04	7.4	0.65	139.05	174.55	2
14:09:47	794.85	198	1708	388	741	757	28	11.3	1.96	0.53	7.04	7.42	0.59	120.69	174.91	2
14:09:54	795.11	199	1708	385	740	787	32	11.3	1.94	0.44	7.04	7.37	0.67	116.36	175.15	2
14:10:02	795.36	195	1679	383	740	733	24	11.29	1.96	0.44	7.07	7.44	0.72	120.68	175.4	2
14:10:10	795.61	197	1659	390	740	733	25	11.24	1.91	0.38	7.08	7.37	0.6	116.51	175.65	2.01
14:10:17	795.85	196	1698	383	740	733	24	11.27	1.94	0.44	7.07	7.32	0.57	122.81	175.91	2.01
14:10:25	796.11	197	1694	389	740	753	23	11.27	1.95	0.44	7.07	7.37	0.56	118.95	176.17	2.01
14:10:33	796.36	198	1657	395	740	753	34	11.25	1.95	0.41	7.08	7.37	0.57	114.31	176.4	2.01
14:10:40	796.61	197	1680	390	741	757	28	11.28	2	0.5	7.05	7.37	0.67	129.46	176.66	2.01
14:10:48	796.85	197	1654	390	739	782	24	11.24	1.93	0.4	7.08	7.37	0.6	109.74	176.91	2.02
14:10:56	797.11	197	1645	388	739	757	28	11.21	1.92	0.44	7.12	7.56	0.73	114.06	177.16	2.02
14:11:04	797.37	197	1648	389	735	753	24	11.19	1.9	0.38	7.14	7.42	0.57	107.85	177.4	2.02
14:11:13	797.62	197	1639	388	740	753	24	11.15	1.94	0.48	7.17	7.53	0.65	101.09	177.66	2.02
14:11:21	797.87	198	1661	393	739	753	28	11.17	1.93	0.42	7.16	7.44	0.62	111.89	177.91	2.03
14:11:30	798.12	197	1650	388	739	753	28	11.18	1.94	0.44	7.15	7.54	0.72	103.03	178.17	2.03
14:11:38	798.37	198	1629	382	737	753	32	11.13	1.9	0.34	7.21	7.51	0.72	101.19	178.44	2.03
14:11:46	798.62	197	1655	388	738	753	28	11.16	1.93	0.51	7.17	7.58	0.81	100.41	178.66	2.03
14:11:57	798.87	197	1654	388	739	753	28	11.15	1.93	0.39	7.18	7.54	0.74	101.51	178.91	2.04
14:12:05	799.12	198	1667	393	739	753	24	11.17	1.94	0.4	7.17	7.54	0.72	111.42	179.17	2.04
14:12:14	799.37	197	1665	389	739	753	24	11.14	1.94	0.38	7.21	7.61	0.61	95.14	179.43	2.04

DOE high power mortar test Amaco Catoosa Test Site

TIME	SIT	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GRM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	RPS	%	%	%	RIPS	RIPS	RIPS	FT/HR	OnBit	OnBit
14:12:34	798.92	308	1509	394	739	753	28	11.08	1.92	0.43	7.25	7.68	0.74	84.21	179.66	2.04	
14:12:34	798.92	307	1509	388	738	753	28	11.08	1.92	0.33	7.29	7.73	0.79	81.36	179.94	2.05	
14:12:45	800.12	308	1504	387	738	753	24	11.02	1.91	0.36	7.32	7.65	0.74	81.43	180.17	2.05	
14:12:56	800.92	308	1573	392	739	753	28	10.94	1.88	0.32	7.38	7.73	0.67	78.26	180.42	2.05	
14:13:08	800.82	307	1580	391	740	753	28	10.99	1.8	0.36	7.34	7.71	0.67	79.62	180.66	2.05	
14:13:20	800.92	308	1579	389	738	753	28	10.91	1.89	0.31	7.42	7.85	0.79	74.86	180.91	2.06	
14:13:31	801.12	308	1638	386	738	753	24	10.98	1.89	0.32	7.35	7.83	0.98	78.95	181.17	2.06	
14:13:43	801.37	305	1518	384	738	753	28	11	1.94	0.37	7.39	7.68	0.72	79.78	181.43	2.07	
14:13:54	801.62	308	1557	389	739	753	28	10.92	1.87	0.36	7.40	7.68	0.65	77.94	181.68	2.07	
14:14:10	801.97	308	1630	393	739	757	32	10.95	1.88	0.37	7.48	7.85	0.78	88.97	181.92	2.07	
14:14:25	802.12	307	1573	390	740	753	28	10.96	1.9	0.3	7.77	8.26	2.13	89.83	182.17	2.08	
14:14:37	802.92	307	1672	390	736	753	28	8.99	1.89	0.34	8.39	8.81	1.32	78.43	182.43	2.08	
14:14:48	802.62	306	1714	389	740	753	24	9.15	1.91	0.31	8.19	8.72	1.22	102.99	182.67	2.08	
14:14:54	802.89	306	1664	388	738	753	28	9.15	1.87	0.3	8.29	8.6	0.84	113.77	182.93	2.08	
14:15:04	803.13	307	1542	389	738	753	29	9.11	1.89	0.36	8.23	8.69	1.06	88.06	183.17	2.08	
14:15:13	803.38	307	1582	389	738	753	28	9.02	1.8	0.33	8.31	8.69	0.81	93.94	183.42	2.09	
14:15:24	803.63	308	1585	394	739	753	28	8.99	1.88	0.31	8.34	8.61	0.96	84.81	183.68	2.09	
14:15:35	803.88	307	1585	391	738	753	28	8.96	1.88	0.27	8.38	8.61	1.05	79.25	183.93	2.1	
14:15:47	804.19	306	1564	387	739	753	28	8.9	1.87	0.28	8.43	8.61	1.05	79.44	184.19	2.1	
14:15:58	804.38	308	1593	387	738	753	28	8.96	1.88	0.28	8.35	8.61	1.05	80.99	184.42	2.1	
14:16:10	804.63	309	1585	393	739	753	28	8.9	1.88	0.28	8.43	8.89	0.86	75.19	184.68	2.11	
14:16:19	804.98	309	1599	387	738	753	28	9.06	1.8	0.3	8.26	8.61	1.01	84.24	184.92	2.11	
14:16:27	805.13	305	1720	383	736	753	28	9.28	1.93	0.38	8.07	8.65	0.83	113.09	185.17	2.11	
14:16:36	805.38	305	1393	384	738	753	28	11.27	1.84	0.25	7.69	8.43	4.45	102.34	185.43	2.11	
14:16:47	805.63	306	1577	387	737	753	28	10.99	1.91	0.31	7.33	7.9	1.96	85.23	185.68	2.12	
14:16:54	805.88	308	1534	393	738	753	28	10.7	1.91	0.32	7.62	8.29	1.24	139.88	185.94	2.12	
14:17:02	806.13	308	1547	391	738	753	24	10.13	1.91	0.34	8.19	8.67	0.93	135.38	186.17	2.12	
14:17:10	806.38	307	1542	393	738	753	24	10.11	1.9	0.29	8.21	8.67	0.86	133.51	186.44	2.12	
14:17:17	806.63	307	1543	391	738	753	24	10.14	1.91	0.33	8.20	8.67	1.1	127.74	186.68	2.13	
14:17:25	806.88	307	1643	388	738	753	28	10.04	1.92	0.8	8.36	8.71	0.88	103.50	186.93	2.13	
14:17:33	807.13	306	1727	382	738	753	28	10.19	1.89	0.33	8.14	8.59	0.89	128.13	187.18	2.13	
14:17:40	807.38	306	1703	383	736	753	24	10.19	1.8	0.31	8.13	8.58	0.98	127.99	187.43	2.13	
14:17:47	807.63	304	1838	378	736	753	24	10.35	1.95	0.49	8.08	8.57	1.08	125.50	187.68	2.13	
14:17:53	807.88	304	1840	380	736	753	28	10.34	1.96	0.44	7.66	8.5	0.98	150.51	187.94	2.14	

DOE high power mortar test Amaco Catoosa Test Site

TIME	BRT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK LOAD	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HR:MM:SS	FEET	GPM	PSI	RPM	FT-LBS	FT-LBS	FT-LBS	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnSH	OnBR
14:18:01	808.13	103	2118	393	661	766	397	10.16	3.1	0.58	8.17	9.91	4.5	107.00	188.18	2.14
14:18:16	808.30	108	1530	394	738	753	49	15.6	1.67	0.29	2.80	5.41	4.20	59.75	188.43	2.14
14:18:30	808.54	107	1451	389	739	753	28	16.25	1.88	0.21	3.05	3.3	0.62	68.47	188.68	2.15
14:18:48	808.89	108	1440	393	739	753	36	15	1.9	0.29	3.30	5.27	3.44	68.53	188.93	2.15
14:18:54	809.14	105	1584	384	739	753	24	13.38	1.94	0.36	5.03	5.36	0.65	103.56	189.19	2.15
14:19:03	809.39	106	1600	383	738	753	28	13.26	1.95	0.34	5.05	5.38	0.62	95.86	189.42	2.16
14:19:13	809.64	106	1582	385	738	753	24	13.33	1.94	0.33	5.09	5.38	0.55	90.88	189.68	2.16
14:19:23	809.89	107	1551	391	738	753	32	13.24	1.91	0.33	5.07	5.38	0.66	98.19	189.93	2.16
14:19:36	810.08	106	1258	387	740	753	24	16.17	1.82	0.15	2.83	4.48	4.68	182.43	190.13	2.16
14:19:48	810.33	105	1489	384	740	753	24	15.76	1.81	0.12	4.97	5.8	1.46	81.47	190.37	2.16
14:19:56	810.58	104	1586	379	741	757	28	12.69	1.83	0.16	6.94	8.61	1.2	112.75	190.64	2.17
14:20:04	810.83	104	1856	380	741	757	28	11.85	1.84	0.15	6.88	7.37	1.11	113.13	190.89	2.17
14:20:11	811.08	105	1679	384	741	753	24	11.43	1.83	0.16	7.31	7.54	0.5	127.78	191.14	2.17
14:20:18	811.33	105	1884	381	741	753	24	11.38	1.83	0.15	7.38	7.56	0.43	121.13	191.37	2.17
14:20:26	811.58	105	1701	383	740	753	24	11.39	1.84	0.18	7.34	7.58	0.43	122.51	191.65	2.17
14:20:32	811.84	105	1733	385	741	753	24	11.4	1.85	0.21	7.34	7.68	0.43	135.32	191.9	2.18
14:20:39	812.09	105	1805	382	740	753	24	11.46	1.84	0.21	7.37	7.62	0.55	130.97	192.14	2.18
14:20:45	812.34	104	1822	378	741	753	24	11.5	1.9	0.24	7.34	7.49	0.57	145.87	192.37	2.18
14:20:52	812.59	107	1920	388	741	753	24	11.48	1.87	0.23	7.35	7.62	0.57	134.43	192.63	2.18
14:20:59	812.84	105	1824	383	741	757	28	11.48	1.87	0.25	7.34	7.54	0.57	124.86	192.88	2.18
14:21:06	813.09	104	1982	378	741	753	24	11.49	1.88	0.25	7.34	7.59	0.67	135.56	193.14	2.19
14:21:13	813.34	104	1905	375	740	753	24	11.6	1.88	0.25	7.34	7.59	0.67	130.94	193.39	2.19
14:21:20	813.59	104	1916	379	739	753	28	11.48	1.88	0.31	7.28	7.64	0.72	135.88	193.63	2.19
14:21:28	813.84	105	1888	382	740	753	24	11.51	1.88	0.23	7.22	7.47	0.57	139.96	193.88	2.19
14:21:33	814.09	104	1909	381	740	753	24	11.57	1.87	0.22	7.17	7.47	0.6	128.67	194.16	2.19
14:21:40	814.34	105	1572	383	740	753	24	11.51	1.86	0.25	7.22	7.52	0.57	130.85	194.4	2.2
14:21:46	814.59	104	1677	378	740	753	24	11.54	1.9	0.28	7.20	7.54	0.72	148.12	194.63	2.2
14:21:52	814.84	105	1657	383	736	753	30	11.51	1.84	0.19	7.22	7.49	0.8	139.29	194.88	2.2
14:21:59	815.09	105	1937	381	740	753	38	11.52	1.85	0.2	7.21	7.44	0.85	138.26	195.14	2.2
14:22:06	815.34	106	1931	385	740	753	24	11.47	1.82	0.18	7.25	7.49	0.49	130.58	195.4	2.2
14:22:12	815.58	104	1816	378	740	753	24	11.64	1.83	0.17	7.29	7.52	0.6	158.60	195.63	2.2
14:22:19	815.84	106	1910	388	740	753	24	11.45	1.84	0.3	7.28	7.44	0.9	126.51	195.89	2.2
14:22:25	816.09	106	1814	385	740	753	25	11.45	1.82	0.15	7.28	7.49	0.45	134.86	196.15	2.2
14:22:33	816.34	105	1792	385	740	753	24	11.32	1.89	0.24	7.41	8.11	1.13	128.56	196.38	2.2

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	ISPM	PSI	RP&M	ft-lbs	ft-lbs	ft-lbs	LOAD	G's	G's	KIPS	KIPS	KIPS	FT/HR	Onset	OnBr
14:27:40	816.59	109	1807	383	740	753	24	10.76	1.86	0.21	7.98	8.38	0.74	124.58	196.65	2.21
14:27:47	816.84	107	1775	380	740	753	28	10.88	1.82	0.17	7.85	8.07	0.5	135.95	196.88	2.21
14:27:54	817.08	105	1782	383	738	753	24	10.82	1.85	0.23	7.83	8.02	0.43	138.18	197.14	2.22
14:28:00	817.34	103	1792	375	738	753	24	10.82	1.83	0.19	7.81	8.02	0.45	142.98	197.4	2.22
14:28:07	817.58	106	1787	385	740	753	24	10.88	1.83	0.16	7.85	8.08	0.43	138.24	197.65	2.22
14:28:15	817.86	105	1733	383	738	753	24	10.85	1.81	0.14	7.88	8.07	0.41	134.20	197.91	2.23
14:28:21	818.1	108	1754	385	740	757	28	10.86	1.81	0.13	7.87	8.11	0.33	136.38	198.14	2.23
14:28:29	818.35	106	1749	387	739	753	28	10.84	1.87	0.18	7.89	8.08	0.41	133.12	198.36	2.23
14:28:36	818.6	108	1739	387	739	753	24	10.85	1.83	0.17	7.89	8.11	0.45	128.50	198.67	2.23
14:28:43	818.85	108	1730	389	740	753	24	10.88	1.82	0.14	7.85	8.09	0.43	125.48	198.93	2.23
14:28:50	819.1	108	1745	389	740	753	24	10.88	1.82	0.16	7.85	8.09	0.53	125.28	199.14	2.23
14:28:57	819.35	108	1753	386	739	753	28	10.86	1.81	0.13	7.87	8.11	0.48	127.32	199.4	2.23
14:29:04	819.6	108	1787	383	740	753	28	10.86	1.82	0.16	7.87	8.09	0.5	122.05	199.65	2.24
14:29:11	819.85	107	1783	388	738	753	28	10.87	1.81	0.14	7.85	8.09	0.45	131.63	199.89	2.24
14:29:18	820.1	108	1799	391	738	753	24	10.82	1.85	0.16	7.81	8.14	0.53	126.93	200.14	2.24
14:29:25	820.35	108	1777	392	740	753	28	10.86	1.83	0.16	7.87	8.16	0.53	121.61	200.42	2.24
14:29:32	820.6	105	1780	383	739	753	28	10.84	1.82	0.13	7.89	8.15	0.53	130.83	200.66	2.24
14:29:40	820.85	105	1745	387	739	753	24	10.82	1.86	0.19	7.93	8.23	0.55	119.17	200.89	2.25
14:29:47	821.1	107	1740	389	740	753	28	10.83	1.82	0.14	7.90	8.13	0.48	128.75	201.14	2.25
14:29:54	821.35	107	1758	390	739	753	24	10.87	1.82	0.15	7.85	8.18	0.69	127.44	201.43	2.25
14:29:01	821.6	107	1743	389	738	753	28	10.84	1.85	0.18	7.88	8.14	0.48	119.58	201.67	2.26
14:29:08	821.85	106	1732	394	740	753	28	10.83	1.82	0.16	7.92	8.19	0.5	127.66	201.91	2.26
14:29:15	822.1	106	1763	393	740	753	24	10.88	1.83	0.16	7.88	8.15	0.5	121.58	202.17	2.26
14:29:23	822.35	107	1742	389	738	753	28	10.87	1.83	0.17	7.86	8.13	0.3	128.78	202.4	2.26
14:29:30	822.6	108	1739	391	737	753	28	10.83	1.84	0.18	7.88	8.23	0.65	125.59	202.66	2.26
14:29:38	822.85	105	1723	393	738	753	28	10.8	1.83	0.17	7.93	8.21	0.57	115.07	202.91	2.26
14:29:45	823.1	107	1725	399	739	748	20	10.79	1.84	0.18	7.94	8.30	0.48	125.95	203.18	2.26
14:29:53	823.35	109	1737	396	740	753	28	10.78	1.82	0.14	7.95	8.23	0.4	118.35	203.4	2.27
14:31:01	823.61	106	1730	385	740	753	24	10.75	1.83	0.17	7.96	8.33	0.79	113.58	203.66	2.27
14:31:08	823.85	105	1709	385	740	753	24	10.8	1.88	0.19	7.92	8.21	0.33	120.50	203.91	2.27
14:31:16	824.11	108	1717	386	740	753	39	10.6	1.84	0.19	7.93	8.29	0.3	115.92	204.17	2.27
14:31:24	824.36	105	1729	384	740	753	28	10.73	1.84	0.19	7.96	8.31	0.65	115.75	204.42	2.27
14:31:32	824.61	108	1707	385	740	753	24	10.69	1.88	0.2	8.04	8.35	0.72	107.80	204.66	2.28
14:31:40	824.86	107	1744	388	740	757	28	10.77	1.86	0.2	7.95	8.26	0.65	112.80	204.91	2.28

DOE high power mortar test Amaco Catoosa Test Site

TIME	BHT DEPTH	FLOW	PRES.	SPEED	TORQUE	PEAK	DELTA	HCOCK LOAD	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HR:MM:SS	FEET	ISPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	RPS	%	%	KIPS	KIPS	KIPS	FT/HR	OnBr	OnBd
14:31:48	825.14	106	1768	387	740	753	24	10.75	1.87	0.23	7.98	8.28	0.62	112.50	205.15	2.28
14:31:57	825.36	106	1741	385	740	753	24	10.73	1.84	0.2	8.00	8.28	0.62	108.85	205.4	2.28
14:32:08	825.61	108	1729	392	740	753	24	10.61	1.84	0.21	8.12	8.5	0.74	98.37	205.66	2.28
14:32:15	825.86	106	1747	385	740	753	24	10.7	1.87	0.23	8.03	8.58	0.65	104.53	205.92	2.28
14:32:23	826.11	107	1711	384	740	753	24	10.7	1.83	0.17	8.03	8.51	0.66	104.35	206.19	2.28
14:32:32	826.36	108	1695	392	740	753	28	10.63	1.88	0.18	8.09	8.5	0.72	98.55	206.4	2.28
14:32:42	826.62	108	1732	382	740	757	32	10.68	1.83	0.17	8.05	8.38	0.69	98.18	206.66	2.28
14:32:51	826.87	108	1703	388	738	753	28	10.61	1.82	0.16	8.11	8.38	0.57	98.31	206.94	2.28
14:33:02	827.12	107	1648	390	740	753	24	10.48	1.85	0.16	8.25	8.57	0.67	78.41	207.17	2.28
14:33:12	827.37	109	1652	386	740	753	24	10.58	1.84	0.17	8.14	8.45	0.62	90.75	207.4	2.28
14:33:21	827.62	108	1685	392	740	753	24	10.64	1.86	0.18	8.09	8.35	0.5	103.33	207.68	2.28
14:33:31	827.87	108	1681	395	740	753	24	10.63	1.85	0.18	8.15	8.52	0.72	84.85	207.92	2.28
14:33:40	828.12	107	1689	389	740	753	24	10.62	1.84	0.18	8.18	8.4	0.6	91.77	208.17	2.28
14:33:50	828.37	107	1644	388	738	748	24	10.53	1.85	0.17	8.18	8.62	0.79	85.34	208.41	2.28
14:34:01	828.62	108	1638	384	738	753	28	10.5	1.81	0.13	8.32	8.5	0.8	80.07	208.66	2.28
14:34:13	828.87	106	1638	387	740	753	28	10.48	1.83	0.16	8.24	8.62	0.89	79.78	208.91	2.28
14:34:26	829.12	109	1579	395	740	757	32	10.32	1.82	0.13	8.41	8.67	0.95	53.24	209.17	2.28
14:34:42	829.37	108	1602	393	738	753	28	10.42	1.85	0.18	8.30	8.74	0.79	74.39	209.43	2.28
14:34:52	829.62	107	1660	389	738	753	28	10.51	1.85	0.18	8.21	8.47	0.55	84.73	209.68	2.28
14:35:03	829.87	107	1713	390	737	753	28	10.54	1.83	0.17	8.19	8.45	0.55	84.36	209.94	2.28
14:35:16	830.12	130	1699	393	740	757	28	10.43	1.82	0.15	8.29	8.69	0.81	75.52	210.17	2.28
14:35:28	830.37	108	1690	392	740	753	24	10.44	1.83	0.18	8.28	8.55	0.62	83.33	210.43	2.28
14:35:38	830.62	107	1726	390	740	753	28	10.51	1.83	0.18	8.21	8.62	0.69	83.25	210.68	2.28
14:35:48	830.87	107	1742	390	738	757	32	10.55	1.83	0.17	8.17	8.4	0.5	90.83	210.92	2.28
14:35:58	831.12	108	1710	395	738	753	28	10.4	1.83	0.18	8.33	8.59	0.65	85.73	211.17	2.28
14:36:14	831.37	108	1727	392	740	757	28	10.44	1.83	0.18	8.28	8.52	0.62	75.32	211.43	2.28
14:36:26	831.62	108	1713	392	740	753	28	10.46	1.82	0.14	8.27	8.55	0.57	71.35	211.67	2.28
14:36:40	831.87	109	1681	395	740	753	24	10.38	1.83	0.18	8.34	8.62	0.72	67.87	211.92	2.28
14:36:53	832.12	109	1707	396	740	753	24	9.97	1.84	0.16	8.75	9.34	1.17	89.79	212.16	2.28
14:37:01	832.38	107	1775	391	738	753	41	9.85	1.84	0.18	8.68	9.22	0.78	107.10	212.42	2.28
14:37:12	832.63	109	1873	386	738	753	32	9.64	1.82	0.16	9.08	9.36	0.79	85.60	212.68	2.28
14:37:23	832.88	130	1857	388	740	753	28	9.85	1.84	0.17	9.07	9.38	0.6	78.68	212.93	2.28
14:37:34	833.13	109	1831	387	740	753	24	9.69	1.81	0.15	9.10	9.36	0.53	82.89	213.19	2.28
14:37:43	833.38	109	1864	386	740	753	28	9.42	1.83	0.15	9.31	10.21	1.51	95.73	213.43	2.28

DOE high power mortar test Amaco Cataosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	BELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	RDP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
13:37:51	833.63	107	1707	388	739	753	24	8.58	1.84	0.2	10.14	10.91	0.84	114.54	213.68	2.38
13:38:08	833.28	106	1674	387	740	753	24	8.49	1.85	0.18	10.25	10.51	0.82	100.82	213.92	2.38
13:38:18	834.43	106	1718	385	739	753	24	8.49	1.84	0.2	10.23	10.88	0.89	94.98	214.18	2.39
13:38:17	834.38	105	1784	381	739	753	28	9.84	1.85	0.19	10.09	10.41	0.74	128.28	214.48	2.39
13:38:24	834.63	105	1778	384	741	753	24	8.63	1.85	0.19	10.10	10.44	0.74	119.32	214.87	2.39
13:38:38	834.88	108	1771	384	741	753	24	8.59	1.84	0.18	10.34	10.6	0.69	88.37	214.82	2.39
13:38:43	835.13	108	1788	388	740	753	24	8.44	1.85	0.18	10.28	10.88	0.68	101.12	215.18	2.4
13:38:54	835.38	107	1778	388	740	753	24	8.36	1.84	0.17	10.37	10.83	0.62	82.57	215.43	2.4
13:39:04	835.63	108	1788	385	738	753	24	8.39	1.82	0.14	10.34	10.6	0.58	98.96	215.89	2.4
13:39:15	835.88	108	1788	388	740	753	24	8.34	1.84	0.16	10.38	10.65	0.6	81.94	215.92	2.4
13:39:25	836.13	107	1773	389	739	753	24	8.36	1.85	0.17	10.33	10.63	0.81	88.31	216.18	2.41
13:39:36	836.38	108	1771	386	739	753	28	8.36	1.82	0.14	10.37	10.7	0.91	87.10	216.43	2.41
13:39:58	836.63	105	1688	388	740	753	24	8.24	1.82	0.13	10.48	10.72	0.6	63.86	216.88	2.41
13:40:01	836.88	108	1734	387	740	753	24	8.28	1.85	0.16	10.45	10.8	0.74	76.80	216.92	2.42
13:40:11	837.13	107	1739	388	739	753	28	8.41	1.82	0.13	10.33	10.88	0.53	81.72	217.18	2.42
13:40:31	837.38	108	1718	387	739	753	24	8.36	1.82	0.15	10.38	10.85	0.6	87.13	217.43	2.42
13:40:33	837.63	107	1684	390	740	753	28	8.24	1.81	0.12	10.48	10.7	0.5	73.84	217.68	2.43
13:40:47	837.88	107	1683	381	739	753	28	8.28	1.81	0.12	10.47	10.77	0.6	84.78	217.94	2.43
13:40:56	838.14	107	1636	388	738	753	28	8.51	1.87	0.22	10.22	10.58	1.17	197.83	218.2	2.43
13:41:06	838.38	107	1588	386	732	1688	1807	16.21	1.98	0.47	2.48	11.40	12.02	22.24	218.42	2.44
13:41:45	838.57	108	1582	398	1078	1781	1853	16.26	1.82	0.11	2.44	5.84	8.8	48.88	218.81	2.45
13:42:02	838.82	107	1498	389	740	753	24	12.21	1.83	0.13	6.49	8.8	7.1	53.21	218.88	2.45
13:42:11	839.07	104	1800	380	740	753	24	12.54	1.88	0.13	6.16	6.48	0.85	85.89	219.12	2.45
13:42:20	839.32	105	1804	383	740	753	20	12.8	1.82	0.14	6.11	6.42	0.8	104.78	219.37	2.46
13:42:29	839.57	108	1573	387	741	753	24	13.48	1.81	0.12	6.23	6.38	0.57	102.88	219.51	2.46
13:42:39	839.82	107	1567	388	740	753	28	12.47	1.83	0.15	6.24	6.51	0.80	86.03	219.86	2.46
13:42:49	840.07	108	1544	381	740	753	24	11.84	1.82	0.14	6.88	6.28	2.20	88.26	220.12	2.46
13:42:58	840.32	108	1594	383	739	753	28	10.81	1.81	0.12	7.60	8.23	0.69	93.66	220.38	2.47
13:43:11	840.58	107	1619	380	741	753	24	10.77	1.82	0.12	7.84	8.21	0.58	76.82	220.63	2.47
13:43:21	840.83	108	1621	385	741	757	28	10.78	1.84	0.13	7.93	8.28	0.67	83.88	220.88	2.47
13:43:31	841.08	107	1588	388	739	753	28	10.93	1.81	0.14	7.78	8.08	0.62	92.14	221.12	2.48
13:43:38	841.33	107	1614	389	739	748	20	11.13	1.82	0.14	7.57	7.60	0.88	128.89	221.38	2.48
13:49:08	841.77	107	1284	389	740	753	24	16.87	1.68	0.23	2.83	2.78	1.84	58.07	221.81	2.48
13:49:17	842.02	108	1372	384	740	753	28	14.48	1.94	0.37	4.73	7.78	5.48	76.13	222.66	2.49

DOE high power motor test Amaco Catoosa Test Site

Well No. 23	Date: 2/22/95																	
Starting Depth =	823.82	Bit Type =	Walker McDonald MPC8H															
Ending Depth =	1831.18	Bit Size =	4.75															
Total Depth Drilled	407.27	Bit Nozzles =	9, 9, 12, 12															
Hours On Bit =	4.09	Mod Type =	Water Based															
Average ROP =	99.58	Mod Weight (lb/gal) =	9.88															
Drillstring (ft) =	980.49	Pipe (ft) =	254.84	Collar (ft) =	469.60													

TIME HH:MM:SS	DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELT ft-lbs	HOOK LOAD KIPS	PEAK G's	DELTA G's	WOB KIPS	PEAK KIPS	DELTA KIPS	ROP FT/HR	Feet OnBit	Hours OnBit
14:49:26	842.27	106	1569	392	739	753	24	10.71	1.93	0.38	8.53	8.85	2.49	109.77	222.31	2.49
14:49:34	842.52	107	1604	389	739	753	24	9.88	1.8	0.27	8.36	8.86	0.86	101.48	222.56	2.49
14:49:40	842.77	105	1688	384	738	748	20	9.29	1.64	0.37	10.61	10.36	0.96	182.96	222.83	2.5
14:49:48	843.02	108	1704	386	738	748	20	8.87	1.62	0.3	10.37	10.65	0.93	113.16	223.08	2.5
14:49:56	843.27	106	1712	388	739	753	20	8.88	1.9	0.32	10.36	10.65	0.67	123.13	223.34	2.5
14:50:04	843.52	108	1678	388	740	753	24	8.89	1.91	0.31	10.55	10.87	0.69	187.58	223.57	2.5
14:50:13	843.77	107	1635	388	740	753	24	8.64	1.91	0.31	10.59	10.92	0.93	87.65	223.83	2.51
14:50:22	844.02	105	1645	382	740	753	24	8.88	1.95	0.36	10.56	10.94	0.98	105.83	224.06	2.51
14:50:32	844.27	107	1649	389	740	753	24	8.99	1.93	0.35	10.55	10.87	0.79	90.73	224.32	2.51
14:50:39	844.52	105	1684	384	741	753	24	8.95	1.93	0.34	10.27	10.93	0.91	132.83	224.58	2.51
14:50:47	844.77	102	1629	381	739	753	24	8.36	1.92	0.33	10.88	11.39	1.2	102.15	224.83	2.51
14:50:55	845.02	104	1792	373	738	753	24	8.08	1.96	0.4	11.36	11.37	0.5	137.52	225.08	2.52
14:51:12	845.27	106	2079	388	819	871	847	12.03	2.18	0.91	7.18	12.89	9.57	82.56	225.31	2.52
14:51:27	845.52	107	1684	399	740	753	43	13.48	2	0.44	5.76	6.2	1.17	59.53	225.58	2.53
14:51:38	845.77	105	1748	381	740	753	24	13.44	2.01	0.49	5.74	6.1	0.77	81.49	225.81	2.53
14:51:46	846.02	104	1713	376	740	757	26	13.67	1.93	0.38	5.89	5.64	0.62	109.59	226.07	2.53
14:51:55	846.27	105	1717	383	739	753	28	13.51	2.02	0.5	5.86	5.84	0.53	95.78	226.34	2.53
14:52:04	846.52	105	1735	382	741	753	24	11.5	1.99	0.4	5.88	5.84	0.57	106.78	226.58	2.54
14:52:14	846.77	106	1671	386	740	753	28	11.49	1.9	0.32	5.89	5.84	0.3	93.95	226.85	2.54
14:52:24	847.02	107	1656	388	739	753	24	13.48	1.93	0.36	5.79	6.01	0.66	88.92	227.07	2.54
14:52:33	847.28	108	1541	384	740	753	24	13.47	1.9	0.27	5.76	5.96	0.55	100.12	227.33	2.54
14:52:43	847.53	108	1549	394	741	758	24	13.43	1.89	0.25	5.78	7.09	1.7	59.63	227.57	2.55
14:52:50	847.78	106	1618	382	740	753	24	10.83	1.92	0.31	8.38	10.01	3.11	119.97	227.82	2.55
14:53:08	848.03	106	1696	387	740	758	26	9.36	1.94	0.31	8.89	10.58	0.5	119.56	228.07	2.55
14:53:11	848.28	107	1795	388	741	753	24	8.5	1.93	0.34	10.29	10.75	1.03	85.41	228.33	2.55
14:53:20	848.53	106	1829	384	740	753	29	9.16	1.95	0.38	10.04	10.91	0.77	103.83	228.58	2.56
14:53:32	848.78	106	1787	385	740	753	24	8.53	1.86	0.4	10.15	10.56	0.84	77.95	228.84	2.56
14:53:44	849.03	107	1790	390	740	753	29	8.33	1.95	0.41	10.26	10.66	0.72	79.12	229.07	2.56
14:54:00	849.28	105	1747	382	740	753	24	8.99	1.98	0.42	10.38	10.75	0.68	58.21	229.33	2.57
14:54:11	849.53	108	1786	386	740	753	36	9.02	2	0.47	10.17	10.81	0.77	77.72	229.58	2.57
14:54:23	849.78	108	1737	386	741	753	24	9.11	1.98	0.44	10.09	10.36	0.72	94.38	229.84	2.57
14:54:36	850.03	106	1843	381	739	753	24	9.25	2.04	0.53	9.94	10.33	0.73	109.84	230.05	2.58
14:54:38	850.28	104	1912	385	740	753	24	9.44	2.08	0.66	9.74	10.34	1.05	136.18	230.34	2.58
14:54:47	850.53	105	1828	396	740	753	28	9.13	1.98	0.38	10.05	10.41	0.98	85.82	230.61	2.58

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	LOAD	Gr	%	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
14:54:56	850.78	107	1774	388	740	783	24	9.18	1.94	0.38	10.01	10.41	0.74	84.07	235.83	2.58
14:55:08	851.03	106	1718	386	740	787	26	8.99	1.96	0.41	10.20	10.63	1.05	75.80	231.68	2.59
14:55:23	851.28	107	1716	388	740	783	24	8.94	1.98	0.44	10.24	10.65	1.03	81.26	231.34	2.59
14:55:34	851.54	107	1710	380	741	789	24	9.04	2.08	0.65	10.14	10.63	0.91	84.67	231.81	2.59
14:55:43	851.79	107	1719	388	740	783	24	9.13	1.93	0.38	10.05	10.48	0.91	81.47	231.88	2.6
14:55:52	852.04	105	1511	388	738	783	26	9.39	2.34	0.69	9.79	10.37	1.72	111.30	232.00	2.6
14:56:01	852.29	106	1815	386	738	783	26	10.41	1.87	0.44	8.77	9.19	0.79	88.34	232.33	2.6
14:56:08	852.54	106	1779	383	740	783	24	10.68	1.93	0.43	8.52	8.83	0.87	111.30	232.59	2.6
14:56:16	852.79	106	1844	382	740	783	24	10.88	1.98	0.44	8.51	8.9	0.88	128.17	232.83	2.61
14:56:23	853.04	107	1694	390	740	783	24	10.88	1.95	0.37	8.30	8.76	0.88	131.74	233.1	2.61
14:56:28	853.29	107	1738	390	739	783	24	11.13	1.98	0.46	8.54	8.83	1.48	170.05	233.34	2.61
14:56:35	853.54	108	1802	386	740	783	24	10.9	1.94	0.39	8.58	8.95	0.77	121.08	233.59	2.61
14:56:44	853.79	108	1853	384	740	783	24	10.53	1.99	0.38	8.59	8.93	0.91	107.88	233.84	2.61
14:56:53	854.04	108	1908	375	741	783	24	10.47	2.01	0.8	8.71	9.14	0.77	106.92	234.08	2.62
14:57:01	854.29	104	2006	378	740	787	28	10.47	2.03	0.54	8.71	9.05	0.79	98.05	234.34	2.62
14:57:11	854.54	103	1999	377	739	783	28	10.47	2.1	0.65	8.71	9.05	0.69	98.07	234.59	2.62
14:57:19	854.79	105	2010	381	740	783	24	10.47	2.1	0.5	8.71	9.07	0.72	104.25	234.85	2.62
14:57:27	855.04	103	1822	375	740	787	28	10.66	2.07	0.65	8.82	9.38	0.91	115.25	235.08	2.62
14:57:35	855.29	107	1736	388	740	783	24	10.56	1.97	0.45	8.83	9	0.74	112.64	235.34	2.62
14:57:42	855.54	106	1734	387	740	783	24	10.73	1.98	0.43	8.44	8.81	0.74	128.99	235.58	2.63
14:57:58	855.79	107	1728	390	740	783	24	10.21	1.93	0.47	8.98	9.40	1.24	85.04	235.85	2.63
14:58:12	856.05	107	1748	388	739	783	24	10.13	1.99	0.45	9.05	9.38	0.77	58.21	236.1	2.64
14:58:28	856.3	108	1760	393	739	787	32	10.2	2.03	0.48	8.88	9.29	0.77	58.83	236.34	2.64
14:58:36	856.55	107	1733	380	738	783	26	10.3	2	0.48	8.87	9.17	0.67	81.82	236.59	2.64
14:58:48	856.8	107	1764	388	740	783	24	10.44	2.05	0.58	8.74	9.1	0.72	94.75	236.85	2.65
14:58:56	857.05	105	1817	381	738	783	24	10.57	1.97	0.42	8.60	8.9	0.67	106.22	237.09	2.65
14:59:14	857.3	105	1786	384	738	783	24	10.59	1.96	0.46	8.60	8.95	0.69	120.67	237.35	2.65
14:59:12	857.35	107	1756	388	739	783	24	10.57	2.01	0.44	8.60	8.95	0.79	104.35	237.8	2.65
14:59:19	857.8	108	1788	393	738	783	24	10.53	2.01	0.48	8.55	8.88	0.79	130.06	237.85	2.66
14:59:27	858.05	108	1768	393	738	783	24	10.71	2.04	0.47	8.47	8.81	0.69	125.25	238.11	2.66
14:59:34	858.3	108	1783	381	739	783	28	10.97	1.98	0.44	8.58	8.88	0.74	118.60	238.34	2.66
14:59:41	858.55	107	1771	388	740	783	24	10.61	2.01	0.51	8.57	8.93	0.77	121.38	238.6	2.66
14:59:49	858.8	108	1868	385	740	783	24	10.73	2	0.5	8.44	8.88	0.84	125.07	238.86	2.67
14:59:56	859.05	103	1846	377	739	783	24	10.69	2.07	0.58	8.48	8.9	0.78	132.87	239.09	2.67

DOE high power motor test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HR:MM:SS	FEET	GPM	PSI	RPM	R-lbs	R-lbs	R-lbs	LOAD	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
15:00:00	859.3	104	1874	380	738	763	24	10.82	2.02	0.48	8.55	8.88	0.72	120.35	239.38	2.67
15:00:11	858.85	105	1794	381	738	753	28	10.65	1.98	0.52	8.52	8.9	0.81	117.87	239.5	2.67
15:00:16	859.8	107	1790	380	739	753	28	10.63	2.01	0.47	8.55	8.9	0.81	120.04	239.88	2.67
15:00:26	860.05	105	1810	387	739	763	24	10.67	1.98	0.48	8.50	8.9	0.84	117.28	240.11	2.68
15:00:33	860.3	106	1788	388	739	763	28	10.63	1.98	0.44	8.54	8.93	0.84	126.60	240.38	2.68
15:00:41	860.58	105	1783	385	740	763	32	10.64	1.98	0.44	8.54	8.88	0.69	124.84	240.6	2.68
15:00:48	860.81	107	1769	391	739	767	28	10.61	1.98	0.44	8.58	8.88	0.72	118.87	240.85	2.68
15:00:58	861.06	106	1778	388	739	753	28	10.6	1.98	0.42	8.57	8.9	0.69	128.51	241.13	2.68
15:01:04	861.31	107	1789	388	737	758	24	10.61	1.98	0.44	8.58	8.9	0.69	121.77	241.37	2.68
15:01:11	861.56	105	1791	383	738	763	28	10.61	1.98	0.48	8.58	8.88	0.77	120.96	241.6	2.69
15:01:12	861.81	108	1813	387	740	757	28	10.66	2	0.5	8.59	8.88	0.74	118.06	241.86	2.69
15:01:28	862.06	107	1883	388	746	753	24	10.73	2.06	0.63	8.44	8.81	0.74	129.41	242.1	2.69
15:01:33	862.31	103	1824	378	746	753	28	10.61	2.04	0.58	8.58	8.88	0.69	120.58	242.37	2.69
15:01:40	862.56	105	1858	382	739	753	28	10.68	2	0.5	8.49	8.9	0.86	128.88	242.61	2.7
15:01:47	862.81	106	1840	386	739	753	24	10.73	1.98	0.53	8.43	8.79	0.78	133.58	242.88	2.7
15:01:54	863.06	109	1991	385	738	763	28	10.77	2.07	0.82	8.49	8.61	0.89	132.87	243.1	2.7
15:02:01	863.31	109	1899	382	738	753	24	10.76	2.08	0.51	8.49	8.93	0.96	128.68	243.37	2.7
15:02:07	863.56	105	1868	381	738	753	28	10.78	2.02	0.59	8.59	8.83	0.91	144.07	243.63	2.7
15:02:14	863.81	107	1837	389	739	753	24	10.75	1.98	0.52	8.42	8.79	0.79	137.91	243.88	2.71
15:02:21	864.06	104	1821	379	740	763	24	10.71	2.01	0.58	8.48	8.79	0.72	136.72	244.1	2.71
15:02:28	864.31	105	1837	381	739	753	24	10.76	2.03	0.53	8.41	8.88	0.89	130.11	244.36	2.71
15:02:35	864.56	107	1852	390	739	763	24	10.7	1.98	0.41	8.47	8.83	0.66	122.57	244.61	2.71
15:02:49	864.81	104	2109	380	827	1364	836	12.99	2.66	0.61	6.16	18.01	8.34	69.14	244.88	2.72
15:03:00	865.06	107	1386	390	738	753	23	14.27	1.94	0.34	4.87	5.34	3.21	78.87	245.12	2.72
15:03:09	865.31	107	1685	391	739	763	28	12.49	2.01	0.55	6.28	7.04	0.72	108.87	245.37	2.72
15:03:17	865.56	107	1791	388	738	753	28	12.51	1.94	0.37	6.25	6.94	0.67	108.86	245.64	2.72
15:03:28	865.82	107	1715	389	738	753	28	12.52	1.98	0.42	5.64	6.86	0.72	104.68	245.89	2.72
15:03:33	866.07	114	1856	414	738	753	29	12.54	2.01	0.47	6.62	7.04	0.81	121.37	246.12	2.73
15:03:43	866.32	114	1907	413	737	763	32	12.55	2.06	0.55	6.81	7.28	1.15	87.58	246.38	2.73
15:03:57	866.57	114	1869	415	737	748	24	12.55	1.97	0.45	6.98	7.37	1.05	88.18	246.63	2.73
15:04:09	866.83	116	1884	419	737	748	24	12.27	2.05	0.56	6.89	7.3	1.03	79.69	246.87	2.74
15:04:26	867.07	114	1872	414	738	753	28	12.29	2.21	0.64	6.87	7.29	1.08	78.36	247.12	2.74
15:04:29	867.32	114	1836	416	739	748	24	12.39	2.03	0.56	6.77	7.3	1.2	87.94	247.38	2.74
15:04:41	867.57	116	1848	420	737	748	24	12.28	2.05	0.56	6.87	7.32	1.1	75.61	247.64	2.75

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE H-lbs	PEAK H-lbs	DELT H-lbs	HOOK LOAD KIPS	PEAK G's	DELTA G's	WOB KIPS	PSAK KIPS	DELTA KIPS	ROP FT/Hr	Feet OnBit	Hours OnBit
Well No. 23	Date: 2/22/98															
Starting Depth =	823.82															
Ending Depth =	1931.19															
Total Depth Drilled	407.27															
Losses On Bit =	4.09															
Average ROP =	99.59															
Coring (ft) =	580.49															
								Collar (ft)	408.60							

TIME	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE H-lbs	PEAK H-lbs	DELT H-lbs	HOOK LOAD KIPS	PEAK G's	DELTA G's	WOB KIPS	PSAK KIPS	DELTA KIPS	ROP FT/Hr	Feet OnBit	Hours OnBit
15-04-46	857.82	113	1642	413	737	758	28	12.71	1.89	0.6	6.45	6.85	0.89	135.92	247.86	2.78
15-04-59	858.07	113	1608	410	737	748	24	12.66	1.87	0.43	6.49	6.90	0.91	128.56	248.11	2.78
15-05-05	858.32	114	1650	413	737	748	24	12.77	1.88	0.43	6.39	6.82	1.1	130.39	248.37	2.78
15-05-16	858.57	115	1630	416	736	759	28	12.76	1.89	0.43	6.40	6.77	1.09	150.11	248.62	2.78
15-05-26	858.82	116	1708	422	737	759	28	12.8	1.92	0.36	6.55	6.97	0.89	118.99	248.87	2.78
15-05-33	859.07	115	1786	417	737	759	28	12.85	1.9	0.31	6.60	6.94	0.74	118.12	249.11	2.78
15-05-31	859.32	114	1767	416	737	759	28	12.86	1.9	0.31	6.60	6.90	0.72	118.67	249.36	2.78
15-05-39	859.57	115	1791	421	737	758	25	12.88	1.92	0.39	6.57	6.89	0.74	112.61	249.64	2.78
15-05-45	859.82	115	1791	419	738	759	24	12.86	1.92	0.51	6.58	6.94	0.74	121.49	249.88	2.78
15-05-54	870.07	116	1794	421	737	748	24	12.87	1.94	0.31	6.54	6.92	0.72	114.17	250.13	2.77
15-06-03	870.33	116	1793	419	737	759	25	12.86	1.9	0.22	6.58	6.97	0.81	116.47	250.37	2.77
15-06-10	870.58	115	1791	415	738	758	26	12.88	1.9	0.22	6.60	6.94	0.67	116.39	250.62	2.77
15-06-18	870.83	116	1798	420	738	759	26	12.88	1.93	0.41	6.58	6.94	0.68	110.41	250.8	2.77
15-06-25	871.08	115	1802	427	737	748	24	12.88	1.92	0.31	6.58	6.94	0.74	122.27	251.13	2.78
15-08-35	871.33	117	1805	423	736	748	24	12.87	1.98	0.37	6.58	6.94	0.84	117.24	251.36	2.78
15-08-41	871.58	115	1805	436	737	759	30	12.88	1.94	0.31	6.58	6.94	0.72	114.51	251.62	2.78
15-08-49	871.83	117	1807	424	737	748	23	12.88	1.91	0.34	6.58	6.98	0.67	116.12	251.88	2.78
15-08-57	872.08	115	1811	438	737	753	28	12.88	1.92	0.3	6.59	6.97	0.69	110.21	252.13	2.78
15-07-04	872.33	118	1810	432	737	759	30	12.88	1.95	0.34	6.62	6.97	0.69	122.60	252.39	2.79
15-07-12	872.58	116	1809	426	738	753	28	12.88	1.95	0.38	6.60	6.94	0.74	113.58	252.63	2.79
15-07-20	872.83	118	1810	438	738	748	30	12.88	1.92	0.3	6.60	6.94	0.82	115.18	252.88	2.79
15-07-27	873.08	109	1743	366	736	750	45	12.88	1.93	0.42	6.58	6.89	1.27	120.15	253.14	2.79
15-12-52	873.33	115	1847	438	741	757	28	14.68	1.93	0.33	4.59	4.98	2.35	180.84	253.4	2.79
15-13-01	873.58	116	1759	429	965	1579	851	14.49	1.93	0.34	4.66	4.91	0.89	88.80	253.66	2.79
15-13-09	873.83	118	1759	427	743	757	24	14.5	1.84	0.34	4.58	4.86	0.67	115.42	253.91	2.8
15-13-17	874.08	116	1830	429	743	757	20	13.84	1.93	0.3	5.45	6.37	1.99	108.66	254.16	2.8
15-13-32	874.33	119	1846	417	749	757	20	12.89	1.95	0.35	6.36	6.53	0.57	144.88	254.4	2.8
15-13-30	874.58	119	1852	417	749	757	24	12.21	1.96	0.35	6.89	7.73	1.6	134.57	254.65	2.8
15-13-36	874.83	112	1904	405	743	757	28	10.87	1.98	0.37	6.34	6.74	1.44	150.90	254.92	2.8
15-13-41	875.08	113	1961	410	743	757	24	10.7	1.98	0.44	6.40	6.82	0.45	171.30	255.18	2.81
15-13-47	875.33	113	1960	409	743	757	24	10.71	2.03	0.42	6.39	6.87	0.57	164.34	255.43	2.81
15-13-53	875.58	113	1936	411	742	757	28	10.7	1.97	0.4	6.40	6.82	0.43	172.27	255.69	2.81
15-13-58	875.83	113	1941	416	744	757	24	10.52	1.99	0.4	6.45	6.81	0.57	159.87	255.92	2.81
15-14-04	876.08	113	1938	409	744	757	24	10.09	1.99	0.4	6.01	6.57	1.08	180.58	256.18	2.81

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	R-lbs	R-lbs	R-lbs	LOAD	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBt	OnBt
Well No. 23	Date: 2/22/96															
Starting Depth =	833.83							Bit Type =	Walker McDonald MF58H							
Ending Depth =	1831.15							Bit Size =	3.75							
Total Depth Drilled	407.27							Bit Nozzles =	9, 8, 12, 12							
Hours On Bit =	4.05							Mud Type =	Water Based							
Average ROP =	99.58							Mud Weight (lbs/gal) =	9.00							
Drillstring (ft) =	550.48							Pipe (ft) =	251.81		Collar (ft) =	40R 50				
15:14:08	875.38	113	1969	411	744	757	24	9.75	1.99	0.45	9.32	9.53	9.43	176.98	238.42	2.81
15:14:14	876.81	111	2011	403	744	757	24	9.79	1.96	0.37	9.32	9.6	9.57	161.82	258.56	2.82
15:14:20	878.28	113	2012	411	744	757	24	9.84	1.97	0.43	9.27	9.5	9.57	173.84	256.91	2.82
15:14:25	877.11	115	1969	417	743	757	28	9.86	1.94	0.37	9.28	9.65	9.61	167.17	257.16	2.82
15:14:21	877.36	110	1917	416	741	753	24	9.5	1.96	0.44	9.51	9.84	9.67	148.62	257.4	2.82
15:14:36	877.61	114	2003	412	742	757	24	9.55	2.02	0.5	9.55	9.86	9.67	148.07	257.65	2.82
15:14:44	877.86	114	2053	413	742	753	24	9.66	1.96	0.41	9.44	9.76	9.69	150.46	257.91	2.82
15:14:48	878.11	113	1981	416	742	753	24	9.84	1.94	0.38	9.38	9.65	9.53	172.84	258.18	2.82
15:14:54	878.36	113	2022	412	741	757	28	9.78	2.07	0.59	9.32	9.72	9.74	162.88	258.4	2.83
15:15:00	878.61	115	1970	417	741	753	24	9.69	1.94	0.39	9.41	9.67	9.55	152.38	258.67	2.83
15:15:07	878.86	114	1978	415	873	3041	1313	9.72	1.95	0.43	9.39	9.62	9.53	132.28	258.94	2.83
15:15:12	879.11	113	1984	418	844	1425	693	9.72	1.93	0.43	9.38	9.74	9.67	302.57	259.18	2.83
15:15:17	879.36	113	1947	418	742	757	24	9.7	1.94	0.41	9.41	9.79	9.69	159.39	259.42	2.83
15:15:23	879.61	115	1865	417	742	757	28	9.74	1.97	0.43	9.37	9.65	9.57	162.18	259.65	2.83
15:15:28	879.87	116	1981	422	742	757	24	9.71	1.88	0.43	9.39	9.69	9.62	161.05	259.89	2.84
15:15:34	880.12	115	2027	417	741	753	24	9.71	2.03	0.57	9.39	9.72	9.67	161.81	260.19	2.84
15:15:40	880.37	114	2041	416	739	753	24	9.75	2.03	0.54	9.38	9.72	9.59	158.38	260.42	2.84
15:15:46	880.62	117	2131	408	831	1170	442	9.7	2.1	0.74	9.38	10.05	1.15	174.18	260.66	2.84
15:15:50	880.87	117	2235	404	716	753	25	9.78	2.26	0.97	9.28	9.91	1.15	167.85	260.93	2.84
15:15:53	881.12	114	2447	414	829	1628	899	13.18	2.38	1.3	9.89	11.06	9.02	77.28	261.18	2.85
15:15:11	881.37	119	1759	431	740	753	25	16.51	1.88	0.28	3.53	4.55	2.03	93.44	261.41	2.85
15:15:19	881.62	116	1834	431	740	753	24	14.78	1.98	0.38	4.27	4.62	0.62	115.88	261.69	2.85
15:15:28	881.87	114	1875	433	737	748	24	14.54	1.91	0.45	4.59	5.22	1.1	132.60	261.92	2.85
15:15:31	882.12	113	1903	431	740	753	24	14.19	2.02	0.54	4.38	5.19	0.65	157.47	262.17	2.85
15:15:38	882.37	113	1921	408	736	753	28	13.53	2.06	0.54	5.51	5.84	0.96	141.97	262.42	2.85
15:15:43	882.62	114	1916	434	736	753	28	13.44	1.94	0.42	5.65	5.91	0.81	160.99	262.67	2.86
15:15:49	882.87	114	1902	434	736	748	24	13.43	2	0.44	5.81	5.91	0.68	146.23	262.91	2.86
15:15:56	883.12	114	1937	433	737	748	48	13.43	2.05	0.48	5.52	5.69	0.59	143.62	263.17	2.86
15:17:02	883.37	115	1989	417	1311	2318	1616	13.5	1.99	0.42	5.58	5.89	0.85	135.53	263.42	2.86
15:17:07	883.62	113	1996	418	822	1189	882	13.5	2	0.5	5.54	5.91	0.79	193.44	263.67	2.86
15:17:13	883.87	113	1998	408	739	753	24	13.54	2	0.64	5.51	5.79	0.66	155.78	263.91	2.86
15:17:18	884.12	115	1987	417	739	753	28	13.48	2.08	0.56	5.55	5.91	0.72	153.47	264.17	2.87
15:17:24	884.38	113	1973	411	736	753	28	13.23	2.05	0.54	5.81	7.04	1.54	157.72	264.43	2.87
15:17:29	884.63	113	2105	430	737	753	28	12.26	2.17	0.7	6.77	7.16	0.64	172.56	264.7	2.87

DOE high power mortar test Amaco Catoosa Test Site

Well No. 33	Comp. 2/22/88																	
Starting Depth =	823.92	Bit Type =	Walker McDonald MP68H															
Ending Depth =	1021.19	Bit Size =	4.75															
Total Depth Drilled	407.27	Bit Nozzles =	5, 3, 12, 12															
Hours On Bit =	4.99	Mod Type =	Water Based															
Average ROP =	88.58	Mod Weight (Nbs/gal) =	9.00															
Driftang (%) =	860.49	Pipe (N) =	251.81	Collar (ft)	406.50													

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	N-lbs	N-lbs	N-lbs	KIPS	G%	G%	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
15-17:35	884.88	113	2104	412	738	748	24	32.40	2.14	0.71	6.58	6.94	0.77	181.74	264.92	2.87
15-17:40	885.13	112	2116	408	836	1178	454	32.36	2.03	0.58	6.68	7.37	1.24	174.82	305.19	2.87
15-17:45	885.38	114	2083	413	738	753	25	32.11	2.11	0.58	6.83	7.54	1.1	167.09	305.44	2.87
15-17:51	885.63	114	2172	413	738	748	24	31.72	2.12	0.8	7.32	7.68	0.79	174.81	265.68	2.88
15-17:58	885.88	112	2179	408	738	748	23	31.71	2.2	0.87	7.33	7.73	0.77	173.76	265.93	2.88
15-18:01	886.13	112	2191	406	738	748	23	31.75	2.25	0.98	7.29	7.85	1.32	158.05	266.18	2.88
15-18:06	886.38	112	2163	409	737	753	25	31.75	2.31	0.84	7.36	7.85	1.1	184.75	266.44	2.88
15-18:11	886.63	112	2161	407	737	748	23	31.75	2.23	0.93	7.31	7.88	0.98	171.72	266.67	2.89
15-18:17	886.88	114	2165	415	737	748	23	31.75	2.05	0.66	7.29	7.88	0.84	164.75	266.93	2.88
15-18:22	887.13	114	2179	415	737	748	24	31.78	2.07	0.74	7.28	7.73	0.89	177.86	267.18	2.88
15-18:27	887.38	112	2183	406	736	748	24	31.76	2.11	0.8	7.28	7.86	0.81	160.13	267.44	2.88
15-18:32	887.64	113	2153	410	737	753	25	31.78	2.15	0.81	7.27	7.73	0.86	180.40	267.67	2.88
15-18:40	887.88	114	2108	418	1518	2523	1819	31.72	2.16	0.78	7.37	7.83	1.05	124.38	267.87	2.89
15-18:45	888.14	114	2062	413	1617	2357	1888	31.8	2.18	0.79	7.29	7.68	0.86	175.92	268.21	2.89
15-18:48	888.38	113	2177	410	815	1236	602	31.77	2.19	0.84	7.28	7.78	0.91	248.46	268.46	2.89
15-18:54	888.54	115	2157	418	738	753	26	31.78	2.13	0.72	7.28	7.61	0.84	182.02	268.7	2.89
15-18:59	888.85	115	2154	416	736	746	24	31.78	2.11	0.71	7.28	7.68	0.79	181.01	268.93	2.89
15-19:04	889.14	113	2154	410	737	748	23	31.75	2.31	0.83	7.36	7.59	0.6	170.01	269.18	2.9
15-19:18	889.38	114	2158	415	737	753	26	31.73	2.13	0.7	7.32	7.88	0.79	168.39	269.44	2.9
15-19:18	889.64	113	2161	410	737	748	24	31.74	2.06	0.65	7.31	7.73	0.79	178.54	269.72	2.9
15-19:23	889.9	113	2170	411	738	748	24	31.77	2.04	0.67	7.28	7.54	0.69	183.20	269.96	2.9
15-19:25	890.16	112	2170	408	736	753	28	31.77	2.05	0.68	7.28	7.68	0.77	182.39	270.18	2.9
15-19:30	890.4	114	2169	416	738	753	29	31.77	2.08	0.63	7.27	7.81	0.77	172.10	270.44	2.9
15-19:36	890.65	114	2163	414	738	748	24	31.78	2.1	0.61	7.27	7.58	0.75	173.37	270.7	2.9
15-19:41	890.9	113	2150	411	738	753	28	31.74	2.03	0.44	7.39	7.84	0.86	178.02	270.94	2.91
15-19:46	891.15	112	2149	408	736	748	24	31.77	2.02	0.57	7.28	7.71	0.89	168.23	271.2	2.91
15-19:51	891.4	115	2138	418	738	753	28	31.74	2	0.49	7.36	7.71	0.84	175.21	271.46	2.91
15-19:56	891.65	114	2138	414	738	753	28	31.74	2.04	0.56	7.30	7.78	0.91	176.43	271.7	2.91
15-20:02	891.9	113	2123	411	737	748	41	31.78	2.03	0.58	7.27	7.64	0.81	161.48	271.99	2.91
15-20:08	892.15	115	2123	417	1703	2616	1884	31.8	2.06	0.56	7.38	7.84	0.74	145.82	272.22	2.91
15-20:13	892.4	113	2116	411	920	1384	602	31.78	2.07	0.67	7.39	7.64	0.72	216.50	272.46	2.91
15-20:17	892.65	114	2105	415	738	753	24	31.73	2.2	0.89	7.31	7.73	0.61	178.11	272.72	2.92
15-20:23	892.9	114	2110	414	738	753	28	31.74	2.08	0.69	7.31	7.63	0.66	170.86	272.94	2.93
15-20:28	893.15	114	2114	414	738	753	26	31.71	2.1	0.7	7.33	7.71	0.79	160.55	273.21	2.93

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK LOAD	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	lbs	lbs	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
15:20:33	893.41	113	2108	410	737	748	24	11.89	2.1	0.71	7.34	7.71	0.72	176.43	273.47	2.92
15:20:36	893.86	113	2110	412	738	748	24	11.88	2.05	0.68	7.36	7.78	0.66	182.98	273.7	2.92
15:20:44	893.84	113	2148	411	737	748	24	11.79	2.12	0.78	7.25	7.71	1.03	181.50	273.96	2.92
15:20:48	894.16	115	2161	418	738	748	24	11.81	2.12	0.8	7.24	7.66	1.05	178.53	274.2	2.92
15:20:55	894.43	113	2138	412	735	748	24	11.73	2.04	0.65	7.31	7.73	0.88	161.07	274.47	2.93
15:21:02	894.66	113	2064	409	738	748	24	11.34	2.03	0.62	7.78	8.21	1.27	181.85	274.7	2.93
15:21:10	894.93	115	2018	420	737	748	28	11.28	1.97	0.55	7.78	8.16	0.83	115.71	274.98	2.93
15:21:16	895.15	115	2083	417	738	748	24	11.42	1.97	0.45	7.51	7.87	0.81	142.89	275.21	2.93
15:21:23	895.43	118	2052	420	738	748	24	11.34	2.01	0.52	7.59	8.09	0.84	130.93	275.48	2.93
15:21:32	895.68	114	2052	415	1258	2219	1515	11.35	2	0.53	7.72	8.19	1.2	81.59	275.73	2.94
15:21:36	895.91	114	2137	415	1071	1581	851	11.75	2.06	0.56	7.36	7.71	0.88	364.82	275.66	2.94
15:21:43	896.17	113	2141	411	1658	2857	1648	11.77	1.99	0.58	7.38	7.83	1.13	127.80	278.22	2.94
15:21:47	896.43	113	2132	411	644	1372	840	11.76	2.04	0.61	7.27	7.71	0.98	251.21	278.47	2.94
15:21:52	896.67	112	2118	407	737	748	24	11.73	2.07	0.63	7.32	7.8	0.91	155.48	278.73	2.94
15:21:58	898.92	114	2119	413	736	753	28	11.67	1.98	0.44	7.36	7.78	0.93	152.66	278.98	2.94
15:22:04	897.17	115	2118	417	736	748	24	11.69	2	0.46	7.35	7.65	0.98	170.88	277.22	2.95
15:22:09	897.43	114	2129	415	736	748	28	11.74	2.01	0.54	7.31	7.78	1.03	155.01	277.46	2.95
15:22:15	897.67	114	2127	414	736	748	24	11.69	1.97	0.45	7.35	7.78	0.98	170.05	277.71	2.95
15:22:20	897.92	114	2133	415	736	746	24	11.69	2.03	0.49	7.35	7.8	0.98	167.41	277.98	2.95
15:22:26	898.17	113	2149	410	735	748	24	11.74	2.03	0.53	7.35	7.71	0.89	163.64	278.22	2.95
15:22:30	898.42	114	2178	419	736	753	28	10.74	2.15	0.8	8.33	8.19	2.42	189.76	278.48	2.95
15:22:45	898.67	114	2157	415	851	1575	859	14.82	2.15	0.7	8.10	10.7	11.49	62.37	278.72	2.96
15:22:51	898.92	118	1926	427	738	753	28	13.43	2	0.59	8.60	6.34	2.68	144.94	278.98	2.96
15:22:57	899.17	115	2055	422	1325	2365	1873	13.05	2.04	0.51	8.62	6.48	0.98	157.71	279.25	2.96
15:23:02	899.42	117	2070	424	746	808	109	13.03	2.08	0.81	6.08	6.51	1.01	156.98	279.47	2.96
15:23:07	899.67	117	2078	424	811	1059	512	13.02	1.97	0.54	6.03	6.48	0.96	177.34	279.74	2.96
15:23:13	899.92	115	2061	418	736	753	28	13.01	2.02	0.56	6.02	6.51	1.03	169.18	279.98	2.96
15:23:18	900.18	115	2048	415	738	753	28	13.01	1.89	0.44	6.01	6.44	0.98	171.30	280.23	2.97
15:23:24	900.43	115	2021	417	738	753	28	13	1.88	0.49	6.03	6.49	0.93	165.21	280.48	2.97
15:23:30	900.68	116	1985	416	738	748	28	12.93	2	0.52	6.11	6.51	1.03	152.95	280.73	2.97
15:23:36	900.93	117	1835	426	738	753	28	11.89	1.93	0.33	7.08	8	2.08	134.31	280.98	2.97
15:23:44	901.18	115	1843	418	737	753	28	11.82	2.02	0.48	6.02	6.48	2.18	122.57	281.24	2.97
15:23:49	901.43	115	1901	417	737	748	24	8.51	1.95	0.42	9.54	10.58	1.65	161.48	281.48	2.97
15:23:55	901.68	115	1955	416	737	753	28	8.51	2.01	0.52	10.21	10.53	0.67	154.85	281.73	2.98

DOE high power mortar test Amaco Catoosa Test Site

TIME HH:MM:SS	DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELTA ft-lbs	ROCK LOAD KIPS	PEAK G's	DELTA G's	WOB KIPS	PEAK KIPS	DELTA KIPS	ROP FT/HR	Feet OnBit	Hours OnBit
15:24:01	901.93	115	1887	438	738	748	34	8.37	2.84	0.54	10.15	19.58	0.78	190.86	281.97	2.98
15:24:06	902.16	114	2005	412	738	753	34	8.83	2.93	0.53	10.16	19.48	0.68	185.58	282.23	2.98
15:24:13	902.43	114	1899	438	738	753	36	8.81	1.98	0.5	10.23	19.58	0.68	134.89	282.46	2.98
15:24:19	902.68	115	1832	418	738	753	36	8.12	1.84	0.58	10.93	12.33	2.32	136.81	282.75	2.98
15:24:25	902.83	114	2059	412	738	753	39	8.85	1.99	0.43	12.70	13.67	1.84	181.82	282.98	2.98
15:24:30	903.18	113	2081	412	738	753	38	8.95	1.88	0.49	13.16	13.48	0.64	185.05	283.23	2.98
15:24:36	903.43	115	2059	418	738	753	34	8.82	2.01	0.43	13.14	13.49	0.67	166.80	283.48	2.98
15:24:41	903.89	114	2143	414	737	757	32	8.99	2.05	0.45	13.08	13.95	0.87	163.43	283.76	2.98
15:24:46	903.94	113	2103	411	738	748	30	8	1.88	0.55	13.08	13.33	0.62	183.89	283.98	2.98
15:24:51	904.19	112	2182	409	738	753	34	8.88	1.86	0.41	13.02	13.36	0.37	172.06	284.23	2.98
15:24:57	904.44	112	2308	408	738	753	39	8.64	1.84	0.32	13.08	13.31	0.66	171.33	284.51	2.98
15:25:03	904.69	115	1975	418	738	757	41	10.58	1.82	0.29	8.47	13.17	8.24	133.46	284.74	2.98
15:31:38	903.43	118	1323	421	738	753	24	12.34	1.9	0.33	9.06	8.53	0.93	158.58	284.75	3
15:31:44	903.7	115	1354	417	738	753	24	12.32	1.88	0.34	8.09	8.5	0.81	183.72	284.76	3
15:32:03	904.96	115	1781	418	737	748	24	11.79	1.84	0.4	7.64	8.34	0.81	122.69	285	3
15:32:09	905.21	115	1893	417	738	753	24	10.3	2.01	0.5	8.14	8.57	1.01	141.11	285.25	3
15:32:15	905.46	114	1911	416	746	753	24	11.21	2	0.54	8.14	8.55	0.81	151.04	285.51	3.01
15:32:22	905.71	115	1905	419	739	793	28	13.32	1.89	0.45	8.12	8.57	0.84	127.15	285.78	3.01
15:32:28	905.96	115	1823	419	749	753	24	13.29	1.94	0.41	8.15	8.48	0.77	156.84	286.02	3.01
15:32:35	906.21	116	1911	422	739	753	24	15.26	2.03	0.47	8.15	8.53	0.64	134.85	286.28	3.01
15:32:42	906.46	115	1901	419	739	753	28	10.27	1.95	0.39	8.16	8.6	0.86	138.58	286.51	3.01
15:32:48	906.71	117	1927	424	739	753	24	10.34	1.84	0.37	8.99	8.5	0.81	150.07	286.75	3.02
15:32:54	906.96	116	1951	421	739	783	24	10.57	2.03	0.48	8.07	8.46	0.81	139.77	287.01	3.02
15:33:00	907.21	115	1991	419	740	753	24	10.39	2.03	0.54	8.05	8.46	0.84	155.68	287.28	3.02
15:33:06	907.46	117	1929	422	738	753	28	10.17	1.99	0.46	8.05	8.55	0.81	144.83	287.53	3.02
15:33:13	907.71	115	1909	418	739	753	28	10.23	1.98	0.49	8.21	8.74	0.95	133.50	287.76	3.02
15:33:19	907.96	115	1828	418	739	753	24	8.55	1.94	0.4	8.46	8.64	0.88	158.88	288.02	3.02
15:33:25	908.21	114	1806	415	735	753	28	8.88	1.88	0.44	8.58	8.93	0.74	133.31	288.27	3.03
15:33:32	908.46	115	1900	422	739	753	28	8.75	1.99	0.47	8.68	10.56	1.29	140.23	288.52	3.03
15:33:38	908.71	114	1952	415	739	753	28	8.28	2	0.39	11.16	11.68	1.98	148.25	288.78	3.03
15:33:43	908.97	114	2054	413	739	753	24	7.98	1.94	0.33	11.46	11.75	0.65	164.67	289.01	3.03
15:33:49	909.22	113	2068	419	739	753	24	8	1.85	0.38	11.43	11.73	0.57	169.47	289.27	3.03
15:33:54	909.47	113	2073	412	739	753	28	8.01	2.03	0.59	11.43	11.71	0.65	159.23	289.52	3.03
15:34:00	909.72	114	2077	413	739	753	24	8.93	1.84	0.4	11.41	11.71	0.6	174.65	289.75	3.04

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23 Date: 2/22/88

Starting Depth = 523.53 Bit Type = Walker McGovern's MFESH
 Ending Depth = 1021.19 Bit Size = 4.75
 Total Depth Cried = 497.27 Bit Nozzles = 9, 9, 12, 12
 Hours On Bit = 4.09 Mud Type = Water Based
 Average ROP = 69.58 Mud Weight (lb/gal) = 9.00
 Delisting (%) = 860.49 Pipe (ft) = 251.51 Collar (ft) = 408.80

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
15:34:05	909.97	113	2057	409	740	753	24	8.02	1.93	0.36	11.42	11.68	0.55	162.45	290.01	3.04
15:34:11	910.22	113	2053	412	739	757	29	8.01	1.97	0.47	11.43	11.78	0.69	155.33	290.27	3.04
15:34:16	910.47	114	2048	413	740	753	24	7.98	1.98	0.42	11.47	11.78	0.72	165.66	290.52	3.04
15:34:23	910.72	113	2026	411	739	755	24	7.8	1.95	0.45	11.53	11.9	0.6	141.96	290.8	3.04
15:34:28	910.97	114	2059	414	739	753	24	7.99	1.99	0.45	11.48	11.92	0.75	163.75	291.03	3.04
15:34:34	911.22	113	2037	412	735	753	41	7.83	1.94	0.49	11.50	11.87	0.67	157.84	291.29	3.04
15:34:40	911.48	114	2034	414	735	748	24	7.92	2	0.44	11.59	11.85	0.89	159.35	291.52	3.05
15:34:45	911.73	113	2039	410	735	748	24	7.91	2.02	0.56	11.59	11.9	0.89	156.54	291.79	3.05
15:34:51	911.98	114	2045	415	735	748	28	7.92	2	0.59	11.49	11.9	0.89	155.36	292.02	3.05
15:34:57	912.23	112	2041	408	735	748	24	7.89	2.06	0.46	11.51	11.85	0.72	163.72	292.29	3.05
15:35:02	912.48	114	2053	413	736	748	24	7.8	2.01	0.36	11.50	11.9	0.81	157.36	292.53	3.05
15:35:08	912.73	114	2090	415	736	748	24	7.85	2.01	0.52	11.45	11.9	0.69	154.83	292.8	3.05
15:35:13	912.98	113	2042	409	736	753	28	7.93	1.94	0.42	11.47	11.8	0.77	175.74	293.02	3.06
15:35:20	913.23	114	2024	414	736	753	28	7.85	2.04	0.36	11.54	11.94	0.84	141.04	293.27	3.06
15:35:26	913.48	115	2034	416	737	748	34	7.85	1.97	0.42	11.55	11.87	0.84	158.94	293.52	3.06
15:35:32	913.73	114	2037	416	736	748	24	7.89	1.99	0.47	11.53	11.92	0.77	146.73	293.78	3.06
15:35:38	913.98	114	2031	415	737	748	24	7.87	2.01	0.54	11.53	11.87	0.91	146.97	294.02	3.06
15:35:43	914.23	112	2053	406	737	748	24	7.87	1.96	0.44	11.53	11.87	0.54	166.84	294.27	3.06
15:35:49	914.48	115	2047	419	736	753	38	7.85	1.97	0.44	11.53	11.84	0.81	146.88	294.53	3.07
15:35:55	914.73	113	2046	411	736	748	24	7.79	1.97	0.48	11.61	12.06	0.91	133.53	294.78	3.07
15:36:02	914.98	114	2041	412	738	753	28	7.79	2.01	0.45	11.61	12.02	0.81	142.96	295.04	3.07
15:36:08	915.23	115	1966	415	735	748	34	7.74	2	0.46	11.66	12.05	0.89	132.12	295.3	3.07
15:36:15	915.48	114	2012	415	735	748	34	7.8	1.98	0.44	11.60	11.97	0.77	148.91	295.53	3.07
15:36:21	915.73	115	2049	415	737	748	34	7.94	1.98	0.46	11.46	11.92	1.48	141.35	295.78	3.07
15:36:27	915.98	115	1996	418	736	748	34	9	1.85	0.44	12.40	11.95	2.61	138.53	296.02	3.08
15:36:34	916.23	115	2023	417	736	748	34	7.75	2.02	0.46	11.66	12.09	0.89	146.02	296.28	3.08
15:36:41	916.48	115	2015	417	738	748	24	7.69	1.84	0.4	11.72	12.05	0.72	128.26	296.53	3.08
15:36:47	916.74	113	2043	411	738	745	24	7.71	2.05	0.5	11.70	12.14	0.89	160.91	296.78	3.08
15:36:53	916.99	113	2030	410	738	746	24	7.88	2.02	0.53	11.71	12.05	0.74	132.58	297.06	3.08
15:37:00	917.24	115	2020	419	735	748	24	7.68	2.01	0.44	11.73	12.05	0.73	138.17	297.27	3.08
15:37:07	917.49	114	2017	414	738	748	24	7.67	1.95	0.41	11.73	12.11	0.79	133.79	297.53	3.08
15:37:14	917.74	116	1996	439	735	748	24	7.64	1.98	0.42	11.76	12.18	0.84	123.15	297.78	3.09
15:37:21	917.99	114	2001	413	735	745	28	7.62	1.88	0.42	11.75	12.14	0.81	134.58	298.04	3.09
15:37:28	918.24	114	2006	413	735	748	28	7.66	1.88	0.41	11.73	12.09	0.72	125.84	298.32	3.09

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	NOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	LOAD	G%	G%	KIPS	KIPS	KIPS	FT/HR	OnM	OnM
15:37:35	918.40	113	2030	410	735	748	24	7.89	1.94	0.39	11.70	12.06	0.72	130.41	298.54	3.1
15:37:41	918.74	114	2044	413	735	748	25	7.74	1.98	0.41	11.67	12.09	0.84	136.44	298.79	3.1
15:37:48	918.99	114	2043	414	734	748	25	7.75	1.97	0.4	11.63	12.02	0.78	133.24	299.04	3.1
15:37:54	919.25	114	2022	413	735	748	24	7.65	1.94	0.36	11.74	12.02	0.62	144.48	299.3	3.1
15:38:01	919.5	114	2054	413	736	748	24	7.68	1.96	0.44	11.72	12.06	0.77	128.68	299.55	3.1
15:38:08	919.75	115	2074	418	735	748	24	7.7	1.94	0.41	11.70	12.08	0.72	137.35	299.79	3.1
15:38:14	920	115	2088	419	735	748	24	7.68	1.97	0.38	11.72	12.02	0.65	155.25	300.04	3.11
15:38:21	920.25	117	2071	424	735	748	24	7.72	1.98	0.42	11.68	12.06	0.74	135.03	300.3	3.11
15:38:28	920.5	115	2083	419	735	748	24	7.67	2	0.43	11.73	12.09	0.79	140.12	300.55	3.11
15:38:35	920.75	115	2022	419	735	748	28	7.62	1.95	0.41	11.78	12.11	0.74	128.18	300.81	3.11
15:38:42	921	113	2011	414	734	753	32	7.97	1.94	0.32	11.82	12.16	0.79	126.83	301.06	3.11
15:38:49	921.25	115	2093	417	735	748	28	7.57	1.95	0.42	11.83	12.23	0.84	123.02	301.3	3.12
15:38:57	921.5	115	2039	417	735	748	24	7.58	1.98	0.43	11.81	12.21	0.74	117.24	301.56	3.12
15:39:04	921.75	115	2091	419	733	744	24	7.82	1.94	0.37	11.77	12.16	0.86	133.78	301.81	3.12
15:39:11	922	115	1969	416	736	748	28	7.98	1.95	0.31	11.83	12.16	0.74	117.34	302.05	3.12
15:39:18	922.25	118	1943	419	735	744	28	7.88	1.94	0.34	11.71	12.06	0.74	134.87	302.3	3.12
15:39:25	922.5	115	1987	418	735	748	26	7.55	2.01	0.44	11.83	12.21	0.86	124.72	302.56	3.13
15:39:32	922.75	115	2037	416	735	748	24	7.69	1.97	0.35	11.73	12.04	0.69	127.56	302.79	3.13
15:39:39	923	114	2036	413	735	748	24	7.65	1.94	0.37	11.74	12.09	0.67	139.46	303.05	3.13
15:39:47	923.25	115	1980	419	734	746	28	7.54	1.92	0.33	11.89	12.26	0.81	112.94	303.3	3.13
15:39:54	923.51	114	2094	413	733	744	29	7.81	1.94	0.41	11.78	12.23	0.93	128.52	303.56	3.13
15:40:01	923.78	115	1993	418	734	744	29	7.54	1.94	0.41	11.86	12.23	0.74	119.77	303.81	3.14
15:40:09	924.01	114	2015	412	735	748	24	7.58	1.93	0.41	11.81	12.23	0.86	116.52	304.05	3.14
15:40:18	924.25	115	2016	418	734	744	24	7.61	1.96	0.38	11.79	12.14	0.89	127.32	304.3	3.14
15:40:22	924.51	114	2196	405	734	748	28	7.89	2.33	1.04	11.58	12.18	1.58	148.58	304.55	3.14
15:40:29	924.76	114	2004	416	734	748	24	8.26	2	0.48	11.61	11.44	0.91	127.33	304.8	3.14
15:40:36	925.01	116	1939	420	735	748	24	8.37	2.32	0.48	11.62	11.39	0.93	128.38	305.05	3.15
15:40:42	925.26	113	2008	412	734	744	34	8.48	2.81	0.49	11.66	11.38	0.86	148.26	305.32	3.15
15:40:47	925.51	115	2029	418	734	744	29	8.83	1.93	0.4	11.55	11.08	1.15	206.97	305.58	3.15
15:40:54	925.76	116	2010	420	735	748	24	8.34	3.08	0.59	11.15	11.06	1.29	124.78	305.8	3.15
15:41:02	926.01	118	2054	418	734	748	28	8.09	3.08	0.39	11.29	11.03	0.73	115.81	306.06	3.15
15:41:10	926.26	115	2036	418	735	748	28	8.1	3.05	0.63	11.28	11.8	1.01	114.29	306.32	3.15
15:41:16	926.51	113	2065	409	735	748	24	8.42	2.99	0.58	10.97	11.42	0.91	140.47	306.55	3.15
15:41:22	926.76	115	2041	415	735	748	24	8.35	1.98	0.36	11.64	11.42	0.64	154.56	306.81	3.15

Well No. 23
 Date: 3/22/05
 Starting Depth = 823.92
 Ending Depth = 1831.19
 Total Depth Drilled = 407.27
 Hours On Bit = 4.09
 Average ROP = 99.56
 Drillstring (ft) = 660.49

Bit Type = Walker McDermold MP66F+
 Bit Size = 4.75
 Bit Number = 2, 9, 12, 12
 Mud Type = Water Based
 Mud Weight (lbs/gal) = 9.80
 Pipe (ft) = 251.91
 Collar (ft) = 408.60

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
15:41:28	927.02	114	2069	414	733	744	24	8.4	2.08	0.58	11.89	11.42	0.91	141.11	307.88	3.18
15:41:35	927.27	113	2059	409	734	744	24	8.26	2.04	0.6	11.13	11.98	0.61	136.81	307.32	3.18
15:41:43	927.52	114	2054	414	734	748	25	8.19	2.02	0.5	11.20	11.59	0.79	131.38	307.57	3.18
15:41:51	927.77	115	2026	418	733	748	26	8.01	1.98	0.39	11.38	11.71	0.74	101.71	307.83	3.17
15:41:58	928.02	113	2057	409	733	748	26	8.06	1.94	0.39	11.34	11.71	0.86	111.34	308.06	3.17
15:42:08	928.27	115	2038	418	734	748	24	8.08	1.95	0.39	11.32	11.73	0.86	106.69	308.32	3.17
15:42:14	928.52	114	2035	415	735	748	24	8.33	1.96	0.4	11.06	11.44	0.79	142.58	308.58	3.17
15:42:22	928.77	113	2039	411	735	748	26	8.19	2.03	0.48	11.20	11.54	0.69	120.78	308.82	3.17
15:42:29	929.02	114	2034	413	735	744	26	8.35	2.03	0.56	11.03	11.51	1.08	132.82	308.07	3.18
15:42:34	929.27	115	2045	416	735	748	26	8.42	1.99	0.45	10.96	11.32	0.84	106.56	308.32	3.18
15:42:40	929.52	113	2069	413	735	744	26	8.35	2.04	0.5	11.03	11.44	0.81	140.75	308.58	3.18
15:42:47	929.77	115	2080	416	735	744	24	8.39	1.99	0.47	11.03	11.44	0.78	143.72	308.83	3.18
15:42:53	930.02	114	2070	414	734	746	26	8.32	1.98	0.4	11.07	11.42	0.77	141.76	310.07	3.18
15:43:06	930.27	113	2103	410	734	744	24	8.34	1.98	0.43	11.05	11.51	0.88	134.66	310.32	3.19
15:43:06	930.52	114	2087	415	734	748	26	8.26	1.97	0.46	11.12	11.54	0.89	142.53	310.57	3.19
15:43:13	930.77	114	2053	414	735	750	26	8.33	1.96	0.42	11.05	11.38	0.79	137.54	310.81	3.19
15:43:16	931.02	116	2042	422	736	750	26	8.34	1.95	0.38	11.05	11.38	0.78	130.95	311.27	3.19
15:43:26	931.27	115	2062	416	735	748	26	8.28	1.94	0.49	11.11	11.54	0.69	136.21	311.34	3.19
15:43:33	931.53	115	2024	417	734	748	24	8.36	2.04	0.62	11.03	11.42	0.66	132.05	311.58	3.19
15:43:39	931.78	114	2011	415	734	749	26	8.24	1.95	0.37	11.15	11.59	0.54	142.06	311.83	3.2
15:43:48	932.03	115	2016	416	735	748	26	8.21	1.94	0.42	11.18	11.54	0.72	125.52	312.07	3.2
15:43:53	932.28	114	2022	413	735	750	26	8.28	1.93	0.38	11.11	11.51	0.84	134.86	312.32	3.2
15:43:59	932.53	115	2022	418	735	748	24	8.28	1.96	0.37	11.11	11.49	0.66	141.42	312.38	3.2
15:44:07	932.78	116	2015	422	736	744	26	8.28	1.92	0.35	11.10	11.42	0.69	138.65	312.63	3.2
15:44:13	933.03	115	2015	417	736	748	24	8.28	1.92	0.4	11.10	11.47	0.69	143.67	313.07	3.21
15:44:20	933.28	116	2001	422	735	748	24	8.28	1.91	0.33	11.11	11.51	0.79	134.15	313.33	3.21
15:44:27	933.53	119	1987	421	735	748	24	8.21	1.93	0.31	11.18	11.54	0.72	123.31	313.6	3.21
15:44:34	933.78	119	1997	433	733	748	26	8.21	1.94	0.32	11.18	11.49	0.65	138.26	313.84	3.21
15:44:42	934.03	118	1979	427	735	748	24	8.17	1.93	0.33	11.21	11.59	0.84	117.34	314.09	3.21
15:44:49	934.28	118	1985	427	734	748	24	8.2	1.95	0.38	11.19	11.54	0.69	128.38	314.33	3.22
15:44:56	934.53	117	1991	426	735	748	24	8.15	2.01	0.47	11.23	11.54	0.74	124.03	314.58	3.22
15:45:04	934.79	114	1992	412	734	748	26	8.1	1.93	0.32	11.26	11.75	0.69	110.12	314.94	3.22
15:45:12	935.04	116	1921	419	735	748	24	8.04	1.91	0.26	11.34	11.58	0.6	132.75	315.07	3.23
15:45:22	935.29	116	1998	420	733	744	24	7.97	1.93	0.3	11.41	11.68	0.69	83.65	315.34	3.23

Well No. 23
 Date: 2/22/98
 Starting Depth = 623.32
 Ending Depth = 1031.19
 Total Depth Drilled = 407.27
 Hours On Bit = 4.39
 Average RCP = 96.58
 Drillstring (ft) = 650.49

Bit Type = Walker McQuay Coenals MP66H
 Bit Size = 4.75
 Bit Nozzles = 9, 9, 12, 12
 Mud Type = Water Based
 Mud Weight (lbs/gal) = 9.00
 Pipe (ft) = 251.81
 Collar (ft) = 498.60

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	ft-lbs	ft-lbs	ft-lbs	KIPS	KIPS	KIPS	FT/HR	OnBR	OnBR
15:48:31	935.94	116	1875	419	736	748	24	7.9	1.91	0.29	11.46	11.8	0.65	84.90	315.5	3.23
15:48:41	935.79	117	1875	423	733	744	24	7.92	1.91	0.3	11.46	11.73	0.57	85.64	315.84	3.23
15:48:51	936.04	116	1876	422	734	748	28	7.9	2.01	0.47	11.47	11.71	0.57	86.23	316.06	3.23
15:48:00	936.29	116	1897	420	734	744	20	7.95	2.02	0.5	11.42	11.78	0.72	88.99	316.33	3.23
15:51:00	936.57	116	1439	420	738	753	24	8.22	1.89	0.23	3.61	6.37	0.53	121.03	316.62	3.24
15:51:09	936.82	114	1700	415	738	753	28	8.48	1.64	0.31	3.37	11.32	4.52	102.72	316.85	3.23
15:51:15	937.07	113	1860	411	738	753	28	7.7	1.66	0.36	12.17	13.17	2.27	139.77	317.11	3.26
15:51:24	937.32	114	1926	412	739	753	28	8.78	1.67	0.38	13.09	13.52	0.79	105.73	317.38	3.26
15:51:34	937.57	115	1910	416	739	753	28	8.76	1.66	0.32	13.32	13.48	0.72	116.38	317.53	3.26
15:51:40	937.82	115	1918	416	739	753	28	8.76	1.64	0.34	13.31	13.4	0.56	104.40	317.67	3.26
15:51:45	938.07	115	1968	418	738	757	32	8.82	1.64	0.33	13.06	13.36	0.85	114.85	318.13	3.26
16:01:31	939.9	113	1847	410	737	748	24	8.65	1.56	0.47	10.71	11.87	6.51	132.46	319.54	3.29
16:01:36	940.15	113	2001	413	736	748	24	9.23	2.07	0.56	10.32	11.86	1.51	176.03	320.19	3.29
16:01:42	940.4	115	2010	416	734	748	28	9.33	2.03	0.53	10.29	10.72	1.22	151.82	320.44	3.29
16:01:46	940.65	115	1873	417	736	753	28	8.48	1.99	0.4	10.08	10.53	0.86	151.69	320.69	3.29
16:01:53	940.9	113	2024	412	736	748	24	9.46	2.06	0.53	10.10	10.53	0.84	164.40	320.94	3.29
16:02:00	941.15	116	1893	420	736	748	24	9.43	1.96	0.44	10.12	10.98	0.86	138.33	321.22	3.3
16:02:07	941.4	115	1914	418	736	748	24	9.45	2.03	0.51	10.10	10.69	1.1	143.77	321.47	3.3
16:02:13	941.65	113	2025	419	734	748	26	9.22	2.06	0.57	10.33	10.8	0.89	150.99	321.71	3.3
16:02:19	941.9	114	2005	414	739	748	24	9.2	2.08	0.52	10.36	10.8	0.86	146.41	321.96	3.3
16:02:25	942.15	115	2028	417	739	748	24	9.18	2.02	0.49	10.38	10.67	0.96	153.21	322.2	3.3
16:02:32	942.4	115	1995	418	739	748	24	9.27	1.99	0.45	10.29	10.7	0.81	137.49	322.46	3.31
16:02:38	942.65	115	1993	419	734	748	26	9.23	2.09	0.61	10.33	10.8	0.89	143.78	322.72	3.31
16:02:45	942.91	113	1997	416	736	748	24	9.27	2.03	0.51	10.29	10.82	0.98	133.52	322.95	3.31
16:02:51	943.16	115	1994	417	738	748	28	9.24	2.05	0.52	10.11	10.72	0.84	136.55	323.2	3.31
16:02:58	943.41	114	1976	413	736	748	24	9.22	1.99	0.43	10.34	10.72	0.84	142.67	323.46	3.31
16:03:10	943.66	115	1856	416	736	748	28	9.78	2	0.44	10.79	11.2	1.03	76.34	323.71	3.32
16:03:19	943.91	113	1857	412	735	748	28	8.11	2	0.39	11.44	12.16	1.59	96.44	323.95	3.32
16:03:28	944.16	114	1917	413	735	748	24	7.61	1.99	0.41	11.96	12.38	0.81	97.11	324.2	3.32
16:03:40	944.41	115	1872	419	735	750	28	7.47	1.93	0.35	13.09	12.83	0.93	78.78	324.46	3.32
16:03:46	944.66	114	2021	412	735	748	24	7.6	2.12	0.63	11.65	12.16	1.89	136.61	324.7	3.32
16:03:52	944.91	114	2008	414	734	744	24	10.82	1.99	0.46	9.02	10.17	1.89	149.30	324.97	3.33
16:03:59	945.16	115	1900	417	734	744	24	9.33	1.94	0.34	10.03	10.8	1.75	140.73	325.2	3.33
16:04:05	945.41	113	2012	414	734	748	24	9.36	2.12	0.74	10.19	10.64	1.8	146.61	325.45	3.33

DOE high power mortar test Amaco Catoosa Test Site

Well No. 33	Date: 2/22/98																		
Starting Depth =	533.92	Bit Type =	Walker McDermold MH60H																
Ending Depth =	1031.19	Bit Size =	4.75																
Total Depth Drilled	497.27	Bit Nozzles =	9, 9, 12, 12																
Hours On Bit =	4.99	Mud Type =	Water Based																
Average ROP =	99.58	Mud Weight (lbs/gal) =	8.00																
Drilling (%) =	660.49	Pipe (ft) =	251.61	Order (ft)	408.58														

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	GELT	MODK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	Q's	Q's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
16:04:11	845.68	115	1984	419	734	748	24	1.66	0.35	9.85	10.17	1.2	148.41	328.7	3.33	
16:04:17	845.91	115	1949	418	730	748	24	1.66	0.35	9.89	10.27	0.79	145.44	328.66	3.33	
16:04:25	846.16	115	1963	416	734	748	24	1.59	0.38	9.86	10.36	0.86	122.30	328.23	3.34	
16:04:31	846.41	115	1973	416	734	744	24	1.60	0.35	9.93	10.41	0.81	139.51	328.47	3.34	
16:04:38	846.67	115	1943	417	734	748	24	1.66	1.96	9.99	10.34	0.77	124.38	328.71	3.34	
16:04:46	846.92	113	1942	411	734	748	24	1.61	1.93	9.95	10.34	0.84	128.70	328.68	3.34	
16:04:52	847.17	115	1955	418	738	748	24	1.64	1.94	9.91	10.32	0.86	140.33	327.22	3.34	
16:04:59	847.42	115	1934	419	738	748	24	1.68	1.96	9.96	10.32	0.81	121.06	327.47	3.34	
16:05:06	847.67	115	1926	417	738	748	24	1.61	1.93	9.94	10.38	0.93	134.38	327.71	3.35	
16:05:13	847.92	115	1935	419	736	748	24	1.62	1.94	9.94	10.34	0.84	130.48	327.96	3.35	
16:05:19	848.17	114	2017	413	734	748	26	1.87	2.09	9.88	10.22	1.15	151.85	328.26	3.35	
16:05:26	848.42	114	1938	419	738	748	28	1.7	1.96	9.85	10.25	1.03	150.11	328.49	3.35	
16:05:33	848.67	116	1923	420	733	744	24	1.68	2	9.86	10.48	0.88	117.17	328.75	3.36	
16:05:40	848.92	116	1921	421	734	748	24	1.59	1.96	9.97	10.03	0.81	127.49	328.96	3.36	
16:05:47	849.17	115	1932	417	734	748	26	1.55	1.96	9.41	10.01	0.94	124.98	329.21	3.36	
16:05:56	849.42	118	1911	422	735	748	24	1.46	1.95	9.46	10.08	0.79	108.58	329.46	3.36	
16:06:03	849.67	117	1922	424	735	750	32	1.41	1.94	9.35	10.14	0.74	115.54	329.73	3.36	
16:06:11	849.92	114	1987	414	733	748	26	1.92	2.03	9.5	10.02	0.96	113.02	329.98	3.37	
16:06:18	850.18	114	1960	414	734	744	24	1.55	1.97	9.46	10.09	1.01	127.98	330.22	3.37	
16:06:25	850.43	114	1998	413	738	748	24	1.64	1.96	9.42	9.91	1.04	133.14	330.47	3.37	
16:06:31	850.68	113	2046	411	735	744	26	1.79	2.04	9.49	9.78	1.06	138.56	330.72	3.37	
16:06:38	850.93	116	1903	420	735	748	24	1.18	1.98	9.36	9.86	1.2	148.75	331	3.37	
16:06:45	851.18	115	1882	419	736	748	24	1.6	1.92	9.58	10.05	1.01	118.08	331.25	3.38	
16:06:53	851.43	114	1905	415	735	748	24	1.9	1.94	9.64	10.01	0.84	117.32	331.5	3.38	
16:06:59	851.68	113	2009	412	734	748	24	1.33	2.06	9.55	9.25	1.27	159.47	331.75	3.38	
16:07:05	851.93	114	1958	412	734	744	26	1.2	1.95	9.34	9.84	1.03	118.60	331.98	3.38	
16:07:12	852.18	116	1924	408	734	748	24	1.08	1.94	9.37	9.64	0.84	119.26	332.23	3.38	
16:07:19	852.43	117	1917	424	735	748	24	1.07	1.94	9.48	10.01	1.01	123.07	332.48	3.39	
16:07:26	852.68	115	1917	417	735	748	24	1.07	1.95	9.47	9.85	0.89	138.56	332.72	3.39	
16:07:32	852.93	114	1928	415	736	753	28	1.12	1.94	9.42	9.82	0.89	136.48	332.98	3.39	
16:07:39	853.18	115	1903	419	735	745	24	1.09	1.95	9.45	9.88	0.86	125.83	333.23	3.39	
16:07:46	853.43	113	1918	417	735	748	24	1.05	1.95	9.48	9.89	0.89	136.09	333.48	3.39	
16:07:53	853.68	119	1932	417	734	746	24	1.07	1.95	9.47	9.89	0.93	125.44	333.73	3.39	
16:08:00	853.93	114	1925	415	735	744	24	1.09	1.94	9.45	9.84	0.84	137.16	333.97	3.4	

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	LOAD	G's	G's	KIP's	KIP's	KIP's	FT/HR	OnBit	OnBit
16:06:05	954.18	115	1963	419	733	744	24	10.15	1.94	0.23	9.39	9.91	1.08	141.31	334.23	3.4
16:06:15	954.44	115	1941	419	734	744	24	10.17	1.92	0.47	9.37	9.64	1.2	133.08	334.46	3.4
16:06:16	954.69	114	2061	414	733	748	28	10.31	2.11	0.62	9.03	9.57	1.27	186.20	334.74	3.4
16:06:24	954.94	115	1975	418	734	749	24	10.48	1.92	0.45	9.05	9.62	1.38	133.95	335	3.4
16:06:31	955.19	117	1919	424	736	748	24	10.48	1.93	0.31	9.06	9.48	0.91	129.86	335.26	3.41
16:06:36	955.43	115	1924	417	735	748	25	10.48	1.94	0.44	9.06	9.48	0.96	127.77	335.49	3.41
16:06:46	955.69	115	1880	417	733	748	26	10.48	1.94	0.35	9.06	9.48	0.89	129.18	335.73	3.41
16:06:52	955.94	115	1971	422	734	749	24	10.55	1.94	0.47	9.06	9.5	1.1	149.56	335.99	3.41
16:06:56	956.19	114	1942	415	736	748	24	10.54	1.94	0.34	9.05	9.43	0.93	133.02	336.26	3.41
16:07:05	956.44	114	1973	413	736	748	24	10.59	1.94	0.41	9.01	9.46	1.05	136.28	336.48	3.41
16:07:12	956.69	117	2005	423	736	748	24	10.57	1.96	0.42	8.97	9.43	1.03	136.35	336.73	3.42
16:07:19	956.94	115	1967	421	736	748	24	10.52	1.95	0.35	9.01	9.41	0.93	126.53	336.99	3.42
16:07:25	957.19	114	1961	415	736	748	24	10.59	1.94	0.33	8.99	9.46	1.17	147.05	337.26	3.42
16:07:32	957.44	114	1923	415	736	748	24	10.56	1.94	0.43	8.99	9.43	1.03	128.08	337.5	3.42
16:07:40	957.69	115	1868	422	735	763	28	10.38	1.93	0.33	9.16	9.62	0.96	115.36	337.75	3.42
16:07:47	957.94	115	1959	418	736	748	24	10.51	1.93	0.48	8.92	9.57	1.08	129.55	338.01	3.42
16:07:54	958.19	114	2024	413	736	748	24	10.68	2	0.47	8.96	9.36	1.1	141.14	338.24	3.42
16:08:03	958.44	113	1984	409	736	748	24	10.67	1.96	0.41	8.97	9.38	1.1	159.57	338.6	3.42
16:10:07	958.7	117	1903	421	736	748	24	10.46	1.96	0.35	9.08	9.5	0.93	139.54	338.75	3.42
16:10:14	958.95	115	1977	416	736	748	24	10.53	2	0.56	9.09	9.66	1.26	137.92	339.01	3.42
16:10:21	959.2	113	1988	409	738	748	24	10.81	1.95	0.43	9.02	9.59	1.15	125.89	339.24	3.42
16:10:29	959.45	115	1905	419	736	748	26	10.56	1.97	0.42	9.15	9.68	1.06	159.25	339.52	3.42
16:10:36	959.7	116	1978	420	736	748	24	10.45	1.95	0.5	9.08	9.82	1.17	134.85	339.74	3.42
16:10:43	959.95	115	1850	417	736	733	32	10.5	1.94	0.35	9.04	9.5	1.05	135.21	340.01	3.42
16:10:50	960.2	114	1844	416	736	748	24	10.59	1.97	0.41	8.95	9.35	0.91	137.87	340.27	3.42
16:10:56	960.45	115	1880	418	738	748	24	10.78	1.99	0.46	8.75	9.24	1.08	168.53	340.49	3.42
16:11:02	960.7	115	2031	410	736	748	24	10.76	2.02	0.46	8.77	9.24	1.13	148.13	340.74	3.42
16:11:07	960.95	113	2016	412	736	748	34	10.97	2.03	0.44	8.56	9.14	1.22	168.99	341	3.42
16:11:13	961.2	114	1993	413	736	748	24	11.06	1.97	0.41	8.47	8.82	1.05	152.29	341.24	3.42
16:11:19	961.45	116	1932	419	735	748	24	11	1.95	0.44	8.53	8.95	0.93	147.76	341.51	3.42
16:11:25	961.7	114	1946	416	735	744	20	10.99	1.95	0.35	8.53	8.95	1.06	147.76	341.74	3.42
16:11:32	961.95	118	1931	420	734	748	28	10.99	1.96	0.36	8.55	9	1.01	136.81	342	3.42
16:11:38	962.21	115	1950	418	734	744	24	10.96	1.94	0.37	8.96	9.02	1.01	156.26	342.25	3.42
16:11:44	962.46	117	1934	423	736	753	26	10.97	1.94	0.34	8.97	9.02	1.05	138.87	342.51	3.42

Well No. 23 Date: 2/22/88
 Starting Depth = 623.52
 Ending Depth = 1031.19
 Total Depth Drilled = 407.27
 Hours On Bit = 4.05
 Average ROP = 99.56
 Drilling (ft) = 660.46

Bit Type = Walker McDonalds MP68H
 Bit Size = 4.75
 Bit Nozzles = 8, 9, 12, 13
 Mud Type = Water Based
 Mud Weight (lb/gal) = 9.00
 Pipe (B) = 351.21
 Casing (ft) = 408.60

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HOURS:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
16:11:50	962.71	116	1917	421	734	744	24	10.94	1.98	0.33	8.59	9.07	1.01	144.89	342.75	3.46
16:11:52	962.95	114	1924	416	734	744	24	10.96	1.95	0.44	8.57	9.02	0.93	143.65	343.01	3.46
16:12:03	963.21	116	1969	419	734	744	20	10.98	1.98	0.45	8.55	9.02	0.98	134.95	343.28	3.46
16:12:09	963.45	115	1983	416	738	748	24	10.98	2.01	0.44	8.55	9.06	1.03	151.75	343.51	3.47
16:12:15	963.71	113	1983	412	738	748	24	11.04	1.92	0.36	8.48	8.95	0.96	159.65	343.77	3.47
16:12:31	963.96	114	1938	415	735	744	20	10.99	1.94	0.34	8.55	9.02	0.98	157.43	344.01	3.47
16:12:37	964.21	114	1929	414	738	748	24	10.99	1.95	0.38	8.54	9.02	0.98	151.07	344.26	3.47
16:12:38	964.47	112	1984	408	734	748	20	11.18	2.02	0.43	8.35	8.9	1.35	158.63	344.54	3.47
16:12:37	964.72	115	1951	417	734	744	20	11.51	2	0.49	8.03	8.62	1.15	216.37	344.76	3.47
16:12:42	964.97	113	1937	411	734	748	24	11.34	2.03	0.45	8.19	8.76	1.29	182.34	345.01	3.47
16:12:46	965.23	115	1973	416	734	748	24	11.43	1.94	0.41	8.13	8.62	1.2	197.53	345.26	3.48
16:12:52	965.47	115	1977	417	734	744	20	11.21	1.98	0.43	8.33	8.83	1.15	175.91	345.52	3.48
16:12:58	965.72	115	1945	418	738	748	24	10.92	1.93	0.34	8.61	8.19	1.25	181.10	345.76	3.48
16:13:07	965.97	113	2009	412	738	748	28	10.6	1.93	0.31	8.93	8.36	0.98	119.40	346.02	3.48
16:13:17	966.22	114	1982	414	738	748	24	10.45	1.99	0.44	9.08	8.55	1.15	84.23	346.30	3.48
16:13:27	966.47	116	1990	420	735	744	24	10.5	1.95	0.34	9.03	8.38	1.01	90.45	346.51	3.48
16:13:36	966.72	115	1994	426	735	748	28	10.55	1.98	0.35	8.98	8.46	1.1	58.46	346.77	3.48
16:13:44	966.97	115	1995	421	735	748	28	10.78	1.94	0.35	8.78	8.34	1.17	112.07	347.01	3.49
16:13:58	967.22	115	2015	421	735	748	24	10.89	1.97	0.43	8.64	8.31	1.24	147.10	347.27	3.49
16:13:58	967.47	114	2054	413	735	744	20	11.01	1.98	0.45	8.52	9.02	1.05	143.37	347.52	3.5
16:14:02	967.72	115	2083	417	734	744	20	11.05	2.03	0.62	8.45	8.93	1.05	154.35	347.8	3.5
16:14:08	967.98	114	2030	415	734	748	28	11.17	2	0.35	8.35	8.85	1.91	165.34	348.03	3.5
16:18:03	968.25	113	1905	417	742	753	24	15.97	1.93	0.32	4.03	6.17	4.91	115.69	348.26	3.51
16:18:08	968.5	114	1896	413	742	753	24	18.41	1.99	0.38	6.61	7.01	0.89	142.69	348.54	3.51
16:18:15	968.75	115	1949	418	741	757	28	12.91	2.08	0.56	7.11	7.56	1.1	133.76	348.8	3.52
16:18:22	969	112	1953	408	740	753	28	12.83	2.03	0.34	7.19	7.58	0.96	145.07	349.07	3.52
16:18:37	969.25	114	1922	414	738	753	41	12.9	1.98	0.45	7.11	7.56	0.93	177.33	349.3	3.52
16:18:34	969.5	115	1897	418	737	753	38	12.75	2.02	0.41	7.24	7.66	0.98	140.61	349.56	3.52
16:18:40	969.75	114	1940	414	737	758	24	12.44	2.11	0.62	7.94	7.82	0.61	143.66	349.81	3.52
16:18:46	970	113	2072	409	738	753	28	12.44	2.06	0.62	7.94	7.88	0.65	150.11	350.08	3.52
16:18:52	970.25	113	2036	419	738	753	28	12.99	2.05	0.87	7.41	7.78	1.01	148.00	350.31	3.52
16:18:58	970.5	115	1919	421	737	753	28	12.71	1.99	0.44	7.27	8.11	1.48	154.15	350.56	3.52
16:19:08	970.75	115	1876	418	735	748	24	11.41	1.97	0.38	8.57	9.15	1.46	86.97	350.79	3.52
16:19:17	971	114	1919	415	738	753	28	10.29	2	0.4	9.79	10.48	1.52	110.82	351.05	3.52

DOE high power mortar test Amaco Caloosa Test Site

TIME HH:MM:SS	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELT ft-lbs	RQCK LOAD PPS	PEAK IS's	DELTA OS's	WOB KIPS	PEAK KIPS	DELTA KIPS	ROP FTHR	Fast CMBR	Hours CMBR
Well No. 23	Date: 2/23/95															
Starting Depth =	623.92	Bit Type = Walker McDougald 44P68H														
Ending Depth =	1031.19	Bit Size = 4.75														
Total Depth Drilled	407.27	Bit Nozzles => 9, 9, 12, 12														
Hours On Bit =	4.89	Mud Type = Water Based														
Average ROP =	96.58	Mud Weight (lb/gal) = 9.00														
Drilling (ft) =	680.49	Pipe (ft) = 251.81 Coffer (ft) = 408.60														
18:19:25	871.25	114	1940	434	738	753	28	9.65	1.95	0.36	8.33	8.77	0.44	193.08	351.3	3.54
18:19:32	871.5	113	1939	432	738	748	24	10.52	2.08	0.47	9.97	10.49	1.03	132.31	351.54	3.54
18:19:37	871.75	113	1998	430	737	748	24	10.5	1.97	0.48	9.98	10.38	0.88	131.36	351.62	3.54
18:19:43	872.01	115	2070	436	738	753	25	10.26	1.88	0.48	9.73	10.03	0.67	158.01	352.96	3.54
18:19:49	872.26	113	2092	408	739	753	24	10.26	2.04	0.53	9.72	10.13	0.75	158.44	352.31	3.54
18:19:54	872.51	113	2058	407	738	753	28	11.53	2.01	0.44	8.45	9.88	2.13	167.93	352.57	3.54
18:20:00	872.76	115	2041	416	738	753	28	11.56	2	0.44	8.43	8.88	0.89	151.03	352.82	3.55
18:20:06	873.01	114	2042	412	738	753	28	11.63	1.98	0.37	8.25	8.71	0.74	178.26	353.08	3.55
18:20:11	873.26	114	2073	412	738	753	28	11.75	1.98	0.44	8.20	8.64	0.64	159.36	353.31	3.55
18:20:17	873.51	114	2049	414	738	753	28	12	1.92	0.36	7.88	8.43	0.91	148.98	353.56	3.55
18:20:22	873.76	113	2056	412	738	753	28	12.14	1.98	0.46	7.93	8.14	0.69	162.17	353.83	3.55
18:20:29	874.01	114	2018	414	738	748	30	12.23	1.98	0.39	7.69	8.07	0.77	147.87	354.07	3.55
18:20:36	874.26	115	2004	419	738	748	30	12.25	1.98	0.47	7.73	8.11	0.79	152.82	354.31	3.55
18:20:41	874.51	115	2039	416	739	763	34	12.27	2.04	0.44	7.70	8.07	0.74	159.10	354.56	3.56
18:20:47	874.77	118	1987	419	787	763	28	12.18	1.93	0.37	7.99	8.23	0.96	135.48	354.83	3.56
18:20:58	875.02	117	1879	424	797	753	28	11.91	1.93	0.34	8.08	8.33	0.58	116.77	355.08	3.56
18:21:04	875.27	118	1901	422	796	753	28	11.86	1.94	0.36	8.12	8.5	0.67	104.38	355.33	3.56
18:21:18	875.82	115	1952	417	788	753	28	11.8	2.05	0.47	8.38	8.98	0.98	77.77	355.56	3.57
18:21:24	876.07	118	1929	420	799	753	28	12.13	1.96	0.43	7.84	8.8	1.53	138.23	355.82	3.57
18:21:27	876.02	118	1896	423	799	753	24	12.62	2.03	0.52	7.36	7.98	0.88	183.37	356.06	3.57
18:21:31	876.07	113	1889	413	738	748	24	12.87	1.95	0.38	7.30	7.71	0.79	208.89	356.31	3.57
18:21:36	876.32	115	1983	417	738	753	24	12.72	1.96	0.39	7.24	7.61	0.77	197.58	356.58	3.57
18:21:40	876.77	116	1898	419	738	753	28	12.89	1.98	0.35	7.09	7.44	0.74	228.33	356.81	3.57
18:21:45	877.02	116	1834	422	738	753	24	12.95	1.99	0.39	7.61	8.25	1.41	162.88	357.07	3.57
18:21:55	877.27	119	1924	417	739	753	28	11.78	2.04	0.48	8.16	8.53	0.81	92.58	357.32	3.58
18:22:03	877.52	116	1891	423	739	753	24	11.86	1.97	0.5	8.11	8.78	0.67	68.97	357.58	3.58
18:22:23	877.77	116	1919	415	738	753	28	11.34	1.98	0.39	8.43	8.76	0.78	58.82	357.81	3.59
18:22:32	878.02	116	1982	420	738	753	28	11.8	2	0.51	8.18	8.99	1.3	161.23	358.06	3.59
18:22:41	878.27	116	2030	421	738	748	24	11.85	2.04	0.51	8.19	8.52	0.69	101.76	358.34	3.59
18:22:46	878.52	114	2100	415	737	753	28	12.11	2.08	0.56	7.97	8.21	0.77	128.03	358.59	3.59
18:22:54	878.77	117	2014	424	737	753	28	12.35	2.08	0.56	7.82	8	0.69	163.40	358.84	3.59
18:22:59	879.03	116	2022	422	735	748	24	12.38	2.11	0.58	7.59	7.97	0.77	154.37	359.07	3.6
18:23:05	879.28	116	2018	423	735	748	30	12.38	1.94	0.37	7.62	7.96	0.74	156.32	359.33	3.6
18:23:11	879.53	117	2011	423	736	748	36	12.37	2.05	0.47	7.69	7.95	0.89	187.68	359.57	3.6

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23																	Date: 3/22/05																																																																																																																																																																																																																																																																															
Starting Depth =																	523.93																	Bit Type =																	Walker McCaonald MP5BH																																																																																																																																																																																																																																													
Ending Depth =																	1031.15																	Bit Size =																	4.75																																																																																																																																																																																																																																													
Total Depth Drilled																	497.27																	Bit Nozzles =																	8, 9, 12, 12																																																																																																																																																																																																																																													
Hours On Bit =																	4.05																	Mud Type =																	Water Based																																																																																																																																																																																																																																													
Average ROP =																	99.99																	Mud Weight (lb/cc) =																	9.00																																																																																																																																																																																																																																													
Gridding (ft) =																	550.00																	Pile (ft) =																	251.84																	Color (R)																	498.50																																																																																																																																																																																																											
																	BIT																																		HOOK																																																																																																																																																																																																																																													
TIME																	DEPTH																	FLOW																	PRES																	SPEED																	TORQUE																	PEAK																	DELTA																	LOAD																	PEAK																	DELTA																	WGS																	PEAK																	DELTA																	ROP																	Feet																	Hours																
HH:MM:SS																	FEET																	GPM																	PSI																	RPM																	R-lbs																	R-lbs																	R-lbs																	KIPS																	G's																	G's																	KIPS																	KIPS																	KIPS																	FT/MR																	OnBit																	OnBit																
18:23:17																	979.79																	115																	2011																	430																	739																	753																	28																	12.52																	1.94																	0.34																	7.64																	8.04																	0.79																	147.45																	359.82																	3.5																
18:23:23																	980.03																	115																	1950																	422																	738																	753																	28																	12.2																	1.92																	0.37																	7.76																	8.14																	0.83																	145.71																	360.08																	3.5																
18:23:31																	980.28																	115																	1881																	428																	737																	753																	28																	12.07																	1.94																	0.31																	7.60																	8.25																	0.77																	119.94																	360.33																	3.5																
18:23:38																	980.53																	117																	1883																	425																	737																	748																	30																	13.06																	2.02																	0.52																	7.87																	8.28																	0.77																	129.55																	360.58																	3.51																
18:23:45																	980.78																	118																	1846																	422																	737																	753																	28																	12.63																	1.94																	0.33																	7.95																	8.31																	0.74																	121.16																	360.82																	3.51																
18:23:54																	981.03																	118																	1817																	421																	737																	753																	28																	11.98																	1.94																	0.28																	7.89																	8.38																	0.74																	119.48																	361.07																	3.51																
18:24:00																	981.28																	113																	1868																	412																	737																	748																	30																	12.18																	2.02																	0.47																	7.73																	8.26																	0.85																	144.25																	361.35																	3.51																
18:24:07																	981.53																	115																	1887																	416																	737																	753																	28																	12.68																	1.93																	0.31																	7.91																	8.23																	0.81																	121.58																	361.60																	3.51																
18:24:16																	981.78																	115																	1853																	417																	736																	749																	24																	11.91																	1.95																	0.35																	8.05																	8.5																	0.93																	107.55																	361.84																	3.52																
18:24:24																	982.03																	115																	1871																	419																	737																	753																	28																	11.87																	1.97																	0.42																	8.09																	8.5																	0.93																	104.53																	362.07																	3.52																
18:24:30																	982.28																	118																	1842																	429																	738																	753																	28																	11.73																	1.92																	0.3																	8.24																	8.67																	0.84																	70.14																	362.31																	3.52																
18:24:43																	982.53																	114																	1880																	414																	738																	748																	24																	11.56																	1.94																	0.33																	8.02																	8.35																	0.77																	118.73																	362.55																	3.52																
18:24:51																	982.78																	119																	1873																	417																	737																	739																	28																	12.57																	1.94																	0.33																	7.95																	8.28																	0.79																	120.73																	362.83																	3.63																
18:24:58																	983.03																	119																	1890																	417																	737																	748																	24																	12.1																	1.97																	0.38																	7.88																	8.28																	0.77																	131.32																	363.08																	3.63																
18:25:04																	983.28																	115																	1890																	418																	738																	738																	24																	12.04																	1.95																	0.37																	7.88																	8.28																	0.88																	131.63																	363.33																	3.63																
18:25:13																	983.54																	115																	1890																	419																	737																	738																	28																	12																	1.92																	0.38																	7.97																	8.35																	0.84																	111.57																	363.59																	3.63																
18:25:20																	983.79																	114																	1892																	415																	737																	748																	24																	11.97																	1.93																	0.34																	8.05																	8.35																	0.77																	119.92																	363.83																	3.63																
18:25:30																	984.04																	119																	1882																	422																	737																	753																	28																	11.78																	1.95																	0.37																	8.19																	8.64																	1.05																	97.40																	364.08																	3.64																
18:25:46																	984.29																	115																	1836																	419																	737																	748																	24																	11.53																	1.97																	0.4																	8.44																	8.76																	0.77																	56.86																	364.33																	3.64																
18:25:55																	984.54																	114																	1890																	416																	737																	748																	24																	11.67																	1.98																	0.38																	8.09																	8.62																	1.08																	104.32																	364.61																	3.64																
18:26:03																	984.79																	115																	1935																	419																	735																	753																	28																	12																	1.95																	0.35																	7.99																	8.38																	0.88																	113.31																	364.87																	3.65																
18:26:11																	985.04																	115																	1906																	419																	737																	753																	28																	11.94																	2.02																	0.51																	8.03																	8.35																	0.77																	118.03																	365.08																	3.65																
18:26:23																	985.29																	116																	1854																	419																	737																	733																	28																	11.65																	1.95																	0.4																	8.32																	8.71																	1.01																	72.29																	365.34																	3.65																
18:26:32																	985.54																	115																	1878																	416																	737																	733																	28																	11.76																	1.94																	0.39																	8.20																	8.89																	1.25																	89.15																	365.59																	3.65																
18:26:40																	985.79																	115																	1817																	412																	737																	748																	24																	12.03																	2.04																	0.58																	7.94																	8.31																	0.81																	125.47																	365.85																	3.66																
18:26:48																	986.04																	114																	1918																	415																	737																	748																	20																	12.02																	1.94																	0.35																	7.94																	8.33																	0.99																	118.28																	366.08																	3.66																
18:26:54																	986.29																	114																	1949																	416																	737																	748																	24																	12.19																	1.94																	0.4																	7.78																	8.14																	0.77																	147.48																	366.34																	3.66																
18:27:01																	986.54																	112																	2011																	406																	737																	748																	24																	12.1																	2.01																	0.51																	7.66																	8.21																	0.91																	128.65																	366.59																	3.66																
18:27:07																	986.8																	114																	1899																	414																	737																	753																	28																	12.28																	2.01																	0.48																	7.67																	8.99																	0.91																	150.44																	366.85																	3.66																
18:27:15																	987.05																	115																	1926																	412																	737																	753																	28																	11.93																	1.95																	0.42																	8.03																	8.87																	1.15																	112.59																	367.1																	3.67																
18:27:23																	987.3																	119																	1938																	419																	737																	753																	28																	12.08																	1.98																	0.43																	7.87																	8.49																	1.01																	121.35																	367.34																	3.67																
18:27:29																	987.55																	115																	1937																	416																	737																	753																	28																	12.11																	2																	0.43																	7.89																	8.28																	0.89																	136.41																	367.58																	3.67																
18:27:35																	987.8																	119																	1900																	418																	737																	753																	32																	11.82																	1.97																	0.38																	8.15																	8.55																	0.63																	99.26																	367.82																	3.67																
18:27:41																	988.05																	116																	1897																	420																	737																	753																	28																	11.64																	1.91																	0.31																	8.32																	8.67																	0.69																	72.56																	368.1																	3.68																

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	RIPS	G's	G's	KIPS	KIPS	KIPS	FT/MIN	OnBR	OnBR
15:25:00	988.3	116	1918	421	736	753	28	11.56	1.96	0.44	8.68	8.59	1.13	104.83	388.34	3.68
15:25:19	989.55	116	1821	422	737	753	28	11.47	1.89	0.26	8.49	8.8	1.17	48.45	388.63	3.68
15:25:42	990.5	117	1758	424	737	753	28	11.26	1.94	0.31	8.70	9.74	1.44	36.23	388.85	3.69
15:26:09	989.05	116	1807	421	737	753	28	9.4	1.91	0.3	10.56	11.44	2.01	51.58	389.1	3.7
15:26:33	988.3	116	1839	427	736	748	28	9.03	1.91	0.3	10.93	11.95	1.27	37.56	389.26	3.7
15:26:40	989.55	116	2082	420	737	748	24	9.58	2.64	0.9	10.39	11.01	1.39	121.01	389.62	3.71
15:26:47	989.8	113	2161	408	737	748	24	10.78	2.98	0.54	9.18	10.48	3.78	148.44	389.87	3.71
15:26:53	990.05	116	1994	420	738	748	24	13.26	1.94	0.32	6.89	7.09	0.81	148.45	379.11	3.71
15:26:59	990.31	118	1909	428	736	748	28	13.25	1.93	0.33	6.70	7.16	1.85	133.21	379.36	3.71
15:26:59	990.58	118	1758	427	737	753	29	12.41	1.89	0.28	7.84	7.88	1.34	30.51	379.64	3.72
15:27:09	990.75	117	1704	428	737	753	29	12.35	1.9	0.28	7.99	7.9	0.66	23.75	379.81	3.73
15:27:21	991.01	115	1743	418	737	753	28	10.96	1.94	0.41	8.00	12.5	5.32	48.22	371.05	3.73
15:27:39	991.26	113	1972	408	738	748	24	7.76	1.97	0.37	12.21	12.84	0.87	115.22	371.1	3.74
15:27:37	991.51	112	2029	406	739	753	28	7.82	1.98	0.41	12.15	12.84	0.78	113.15	371.55	3.74
15:27:45	991.76	113	2036	412	738	748	24	7.81	1.82	0.36	12.37	12.83	0.91	113.73	371.83	3.74
15:27:52	992.01	111	2104	406	738	748	24	7.91	1.95	0.38	12.84	12.82	1.01	143.44	372.06	3.74
15:28:00	992.26	113	2053	412	738	750	28	7.8	1.94	0.36	12.14	12.89	0.77	111.56	372.31	3.75
15:28:07	992.51	113	2075	409	738	750	28	7.7	1.93	0.32	12.27	12.84	0.89	116.64	372.56	3.75
15:28:15	992.76	113	2106	409	738	753	28	7.77	1.94	0.38	12.20	12.84	1.08	118.81	372.81	3.75
15:28:21	993.01	113	2132	411	737	748	28	8.11	1.94	0.37	11.87	12.26	0.86	155.81	373.08	3.75
15:28:27	993.26	113	2070	419	737	753	28	8.01	1.93	0.32	11.96	12.38	0.91	147.05	373.32	3.75
15:28:34	993.51	114	2004	414	738	748	24	7.89	1.92	0.34	12.15	12.5	0.79	119.97	373.55	3.75
15:28:41	993.76	115	1996	417	738	753	28	7.83	1.91	0.3	12.15	12.47	0.72	135.82	373.82	3.76
15:28:49	994.01	115	1984	419	738	753	28	7.79	1.84	0.32	13.18	12.59	0.99	122.85	374.08	3.76
15:28:56	994.26	114	1971	418	738	748	24	7.75	1.9	0.29	13.25	12.59	0.79	115.34	374.31	3.76
15:29:04	994.51	115	1977	419	738	753	28	7.74	1.83	0.32	12.23	12.57	0.89	116.47	374.56	3.76
15:29:13	994.76	114	1970	416	738	753	28	7.74	1.85	0.32	12.23	12.85	0.51	105.60	374.84	3.77
15:29:20	995.02	116	1987	416	738	748	28	7.78	1.91	0.3	12.20	13.52	0.72	128.08	375.06	3.77
15:29:27	995.27	116	2008	420	738	753	24	7.82	1.88	0.41	12.15	12.54	0.77	184.79	375.31	3.77
15:29:34	995.52	116	1984	420	737	748	24	7.77	1.84	0.31	12.19	12.52	0.89	120.93	375.57	3.77
15:29:41	995.77	114	2029	414	738	748	28	7.88	1.91	0.3	12.08	12.45	0.86	133.94	375.82	3.77
15:29:49	996.02	115	1979	412	738	753	28	7.78	1.85	0.33	12.31	12.6	0.82	110.77	376.06	3.78
15:29:56	996.27	115	1984	416	738	753	28	7.73	1.94	0.33	12.23	12.54	0.65	134.35	376.33	3.78
15:30:04	996.52	114	1986	414	738	753	24	7.71	1.91	0.31	12.27	12.84	0.79	118.11	376.57	3.78

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23 Date: 3/22/98

Starting Depth = 823.82
 Ending Depth = 1031.19
 Total Depth Drilled = 407.27
 Hours On Bit = 4.09
 Average ROP = 99.58
 Circulating (ft) = 688.49

Bit Type = Walker McDoanold MFG8H
 Bit Size = 4.75
 Bit Number = 9, 9, 12, 12
 Mud Type = Water Based
 Mud Weight (lbs/gal) = 9.00
 Pipe (ft) = 251.93
 Casing (ft) = 408.50

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
16:48:03	1068.38	113	2048	413	743	757	24	11.22	2.02	0.6	8.91	9.84	2.73	120.51	388.43	3.88
16:48:08	1068.63	114	1947	413	744	757	24	13.02	1.99	0.44	7.09	7.49	0.99	130.11	386.67	3.88
16:48:14	1068.88	114	1879	414	744	757	24	12.98	2.08	0.52	7.14	7.81	1.1	147.83	386.92	3.88
16:48:20	1067.13	115	1874	419	744	751	28	12.5	2.01	0.46	7.25	7.81	0.66	162.54	387.2	3.88
16:48:26	1067.38	114	1864	419	743	757	24	12.94	1.99	0.4	7.18	7.81	0.91	158.49	387.42	3.88
16:48:31	1067.63	114	1840	413	743	757	24	12.63	2.01	0.47	7.19	7.59	0.84	146.08	387.67	3.89
16:48:37	1067.88	112	2028	408	744	757	24	12.98	2.1	0.61	7.14	7.59	0.88	169.70	387.93	3.89
16:48:43	1068.13	114	2000	413	743	757	28	12.76	2.12	0.69	7.36	7.95	1.34	105.83	388.18	3.89
16:48:48	1068.38	116	1893	421	744	757	24	12.71	2.15	0.73	7.41	7.78	0.77	69.83	388.46	3.9
16:48:51	1068.63	115	1881	418	744	761	28	12.63	2.12	0.76	7.43	7.78	1.15	71.08	388.58	3.9
16:48:55	1068.88	115	1924	418	858	1773	1041	17.1	2.25	0.93	2.89	8.09	9.34	37.10	388.92	3.91
16:48:45	1069.13	115	1724	415	745	761	33	15.76	2	0.45	3.34	3.93	1.58	89.18	389.18	3.91
16:48:53	1069.38	114	1840	415	745	761	28	15.99	2.09	0.63	4.12	4.8	0.98	117.56	389.45	3.91
16:50:01	1069.63	116	1854	420	748	761	28	15.94	2.01	0.48	4.16	4.62	0.72	117.55	389.68	3.91
16:50:08	1069.88	115	1858	417	748	757	24	15.29	1.97	0.43	4.62	5.31	1.32	138.08	389.92	3.92
16:50:15	1070.14	115	1889	417	745	761	28	15.21	2.01	0.51	4.89	5.29	0.98	131.27	390.18	3.92
16:50:23	1070.39	115	1829	419	745	761	28	15.1	1.86	0.38	5.00	5.48	0.98	118.15	390.43	3.92
16:50:33	1070.64	116	1795	422	748	761	24	14.92	1.95	0.41	5.18	5.65	1.1	90.95	390.69	3.92
16:50:40	1070.89	116	1807	422	748	761	28	15.18	1.84	0.33	4.92	5.29	0.84	133.54	390.96	3.92
16:50:47	1071.14	116	1812	420	748	761	28	15.17	1.96	0.37	4.93	5.34	0.81	135.76	391.2	3.93
16:50:55	1071.39	117	1895	423	747	761	24	15.17	1.95	0.34	4.93	5.26	0.79	117.28	391.44	3.93
16:51:02	1071.64	116	1832	419	747	761	28	14.48	1.86	0.38	5.82	6.53	1.95	139.33	391.68	3.93
16:51:09	1071.89	115	1895	416	747	761	24	14	1.99	0.42	6.11	6.81	0.91	141.48	391.96	3.93
16:51:15	1072.14	113	1893	412	747	761	28	13.85	2.06	0.56	6.15	6.81	0.98	133.24	392.18	3.93
16:51:21	1072.39	114	1808	413	746	737	24	14.01	1.99	0.51	6.10	6.49	0.69	148.05	392.44	3.94
16:51:28	1072.64	115	1924	418	747	761	24	13.98	2.02	0.51	6.15	6.68	1.2	138.32	392.69	3.94
16:51:35	1072.89	115	1821	417	746	761	28	13.96	2.09	0.52	6.15	6.68	0.99	141.42	392.93	3.94
16:51:41	1073.14	116	1870	420	747	761	24	13.94	1.94	0.37	6.18	6.61	0.94	102.73	393.18	3.94
16:51:49	1073.39	115	1848	420	747	781	38	13.9	1.94	0.34	6.21	6.58	0.64	125.45	393.44	3.94
16:51:55	1073.64	115	1891	417	747	761	24	12.74	1.95	0.35	7.38	7.95	2.06	136.82	393.69	3.95
16:52:02	1073.89	115	1921	415	747	761	24	12.98	1.98	0.38	7.53	7.97	0.92	128.11	393.95	3.95
16:52:09	1074.14	114	1948	414	747	761	28	12.93	1.93	0.31	7.55	8.07	0.98	138.87	394.19	3.95
16:52:16	1074.39	114	1927	415	747	761	24	12.45	1.94	0.31	7.66	8.09	0.99	120.50	394.44	3.95
16:52:25	1074.65	115	1892	418	748	761	24	11.93	1.97	0.36	8.18	8.81	1.56	180.62	394.69	3.95

DOE high power mortar test Amaco Caloosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
16:52:34	1014.9	114	1932	414	747	765	32	11.51	2.07	0.49	8.50	8.98	1.13	87.79	384.98	3.96
16:52:42	1015.15	114	1957	414	747	761	24	11.2	1.98	0.4	8.32	8.69	0.84	112.64	383.21	3.96
16:52:49	1015.4	113	2019	412	747	761	24	11.95	3.03	0.62	8.17	8.62	0.95	131.35	383.44	3.96
16:52:55	1015.65	114	2039	413	746	761	24	12.07	3.09	0.8	8.05	8.52	0.91	148.34	383.69	3.96
16:53:03	1015.9	115	1971	417	747	761	24	11.71	1.95	0.33	8.40	8.93	1.15	105.09	383.94	3.96
16:53:17	1016.15	116	1869	422	746	759	34	11.37	1.91	0.3	8.73	9.05	0.74	64.82	384.19	3.97
16:53:26	1016.4	115	1924	419	748	761	24	11.78	2.04	0.5	8.35	8.93	1.46	105.94	384.43	3.97
16:53:32	1016.65	115	1970	418	748	761	34	11.98	3.01	0.44	8.14	8.66	1.51	137.58	384.7	3.97
16:53:41	1016.9	115	1983	418	748	761	34	11.93	1.98	0.47	8.48	8.96	0.86	98.74	384.94	3.97
16:53:50	1017.15	115	2087	419	749	761	24	11.75	2.01	0.47	8.36	8.98	1.29	111.09	385.2	3.98
16:53:56	1017.4	115	2063	417	749	761	34	11.80	1.98	0.43	8.22	8.84	0.89	138.05	385.45	3.98
16:54:03	1017.65	114	1988	413	748	765	38	12	2.07	0.81	8.12	8.99	0.93	153.31	385.72	3.98
16:54:09	1017.9	113	2016	419	749	761	34	11.99	2.07	0.48	8.12	8.52	0.91	145.78	385.95	3.98
16:54:16	1018.15	113	2083	413	748	761	38	13.9	3.19	0.71	8.21	8.71	1.1	130.67	386.2	3.98
16:54:23	1018.41	114	2035	414	748	761	23	14.28	2.06	0.56	8.82	8.4	3.59	122.81	386.45	3.98
16:54:30	1018.66	116	1946	421	747	761	33	14.6	1.99	0.58	8.49	8.18	1.38	122.88	386.71	3.99
16:54:38	1018.91	115	1916	419	749	761	24	14.32	2.01	0.61	8.79	8.22	0.95	124.99	386.96	3.99
16:54:45	1019.16	116	1933	422	749	759	28	14.27	2.01	0.48	8.83	8.22	0.89	130.38	387.2	3.99
16:54:51	1019.41	115	1944	416	748	761	24	14.31	1.98	0.44	8.79	8.3	0.89	134.41	387.45	3.99
16:54:59	1019.66	116	1928	420	748	761	24	14.38	2	0.54	8.82	8.27	0.86	126.31	387.7	4
16:55:06	1019.91	119	1929	416	748	761	28	14.29	2.01	0.47	8.81	8.22	0.93	131.77	387.97	4
16:55:13	1020.16	116	1948	417	746	761	26	14.29	2.04	0.45	8.81	8.25	0.88	118.26	388.21	4
16:55:20	1020.41	115	1949	419	747	761	26	14.29	2.02	0.43	8.81	8.3	0.91	132.21	388.45	4
16:55:27	1020.66	114	1963	415	748	761	24	14.5	2.03	0.54	8.79	8.22	0.61	131.52	388.72	4
16:55:34	1020.91	114	1977	413	748	765	28	14.3	2.06	0.57	8.79	8.22	0.89	128.83	389.97	4.01
16:55:41	1021.16	114	1954	413	747	761	26	14.32	2.04	0.55	8.77	8.22	0.91	136.81	401.22	4.01
16:55:48	1021.41	115	1948	417	747	761	24	14.29	2.01	0.54	8.81	8.22	0.89	122.69	401.45	4.01
16:55:55	1021.67	116	1929	420	747	761	24	14.26	2.06	0.56	8.84	8.32	0.91	128.15	401.71	4.01
16:56:02	1021.92	114	1974	414	745	761	26	14.26	2.03	0.49	8.84	8.38	1.01	127.53	401.97	4.01
16:56:10	1022.17	115	1940	418	748	761	24	14.34	2.02	0.46	8.78	8.3	0.95	135.84	402.22	4.02
16:56:17	1022.42	115	1946	418	747	761	24	14.16	2.11	0.62	8.83	8.93	1.24	116.72	402.48	4.02
16:56:26	1022.67	114	1982	415	747	761	24	14.19	2.02	0.56	8.96	8.34	0.91	108.14	402.73	4.02
16:56:34	1022.92	114	1957	413	747	761	24	14.1	2.12	0.67	8.96	8.48	0.93	108.85	402.97	4.02
16:56:41	1023.17	114	1972	413	747	761	28	14.24	2.09	0.59	8.96	8.27	0.98	124.14	403.23	4.02

DOE high power mortar test Amaco Catoosa Test Site

Well No. 25	Date: 2/22/96																
Starting Depth =	623.92	Bit Type =	Walker McCosnald MP68H														
Ending Depth =	1031.19	Bit Size =	475														
Total Depth Drilled	407.27	Bit Nozzles =	9, 9, 12, 12														
Hours On Bit =	4.09	Mud Type =	Water Based														
Average ROP =	99.56	Mud Weight (lb/gal) =	9.00														
Collaring (ft) =	666.49	Pipe (ft) =	251.61	Collar (ft)	408.86												

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	GELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
16:56:46	1023.42	115	1948	410	747	781	24	14.32	1.98	0.48	5.75	6.25	1.08	127.70	403.48	4.03
16:56:55	1023.67	115	1957	419	747	781	28	14.35	1.98	0.44	5.75	6.15	0.99	125.98	403.71	4.03
16:57:03	1023.93	114	1976	419	747	781	28	14.27	2	0.51	5.82	6.22	0.91	119.34	403.97	4.03
16:57:09	1024.17	115	1991	417	748	781	24	14.33	2.11	0.56	5.77	6.2	0.89	131.52	404.25	4.03
16:57:16	1024.42	115	1977	417	747	781	24	14.31	1.94	0.42	5.79	6.22	0.93	138.60	404.47	4.03
16:57:23	1024.67	115	1974	417	747	781	28	14.27	2.02	0.52	5.83	6.3	0.98	124.67	404.74	4.04
16:57:30	1024.92	113	1986	412	748	781	28	14.32	2.05	0.56	5.78	6.3	0.93	136.53	404.98	4.04
16:57:37	1025.17	114	1968	414	748	781	24	14.32	1.99	0.47	5.78	6.3	0.84	125.93	405.29	4.04
16:57:43	1025.42	115	1962	417	748	781	24	14.32	1.96	0.4	5.77	6.22	0.93	135.16	405.72	4.04
16:57:50	1025.67	114	1952	414	748	781	24	14.32	1.96	0.4	5.78	6.27	1.02	139.76	405.72	4.04
16:57:57	1025.93	116	1950	420	748	781	24	14.34	1.98	0.4	5.75	6.15	0.86	129.01	405.98	4.05
16:58:03	1026.18	115	1948	420	748	781	24	14.35	1.99	0.44	5.74	6.18	0.96	141.87	406.22	4.05
16:58:11	1026.43	114	1940	415	748	785	28	14.34	1.95	0.38	5.75	6.15	0.79	128.55	406.46	4.05
16:58:17	1026.68	115	1921	417	748	781	24	14.29	1.94	0.34	5.81	6.18	0.84	133.11	406.72	4.05
16:58:24	1026.93	115	1944	418	747	781	24	14.23	1.99	0.4	5.75	6.15	0.86	138.75	406.98	4.05
16:58:31	1027.18	115	1939	416	747	781	24	14.33	1.95	0.35	5.76	6.2	0.93	129.80	407.23	4.06
16:58:38	1027.43	115	1912	418	747	781	28	14.4	1.95	0.37	5.88	6.2	0.86	133.95	407.47	4.06
16:58:45	1027.68	116	1912	419	747	781	28	14.31	1.97	0.39	5.79	6.15	0.81	126.38	407.74	4.06
16:58:51	1027.93	115	1885	416	747	781	24	14.31	1.93	0.31	5.77	6.15	0.79	134.08	407.98	4.06
16:58:59	1028.18	119	1905	422	747	781	24	14.32	1.87	0.34	5.77	6.15	0.81	137.15	408.22	4.06
16:59:05	1028.43	115	1909	419	747	781	24	14.31	2.02	0.44	5.76	6.18	0.84	121.74	408.47	4.06
16:59:12	1028.68	115	1907	417	747	781	24	14.33	1.99	0.32	5.76	6.13	0.85	141.96	408.73	4.07
16:59:19	1028.93	116	1899	422	748	785	26	14.31	2.09	0.54	5.77	6.14	1.13	120.13	408.98	4.07
16:59:26	1029.18	116	1828	428	747	781	25	14.31	1.94	0.3	5.78	6.25	0.93	135.70	409.23	4.07
16:59:33	1029.43	117	1815	429	747	781	24	14.21	1.91	0.27	5.88	6.3	0.91	124.03	409.49	4.07
16:59:41	1029.68	117	1850	423	748	781	39	14.2	1.92	0.26	5.89	6.27	0.96	112.38	409.72	4.07
16:59:48	1029.93	117	1894	423	746	781	38	14.25	1.93	0.26	5.85	6.2	0.74	129.82	409.98	4.08
16:59:56	1030.18	117	1881	424	745	781	38	14.24	1.95	0.32	5.83	6.22	0.89	118.76	410.21	4.08
17:00:02	1030.44	117	1857	424	746	781	28	12.3	1.93	0.31	7.90	8.18	2.78	139.07	410.48	4.08
17:00:08	1030.69	117	2024	423	747	781	28	12.23	1.95	0.38	7.87	8.26	0.81	153.49	410.73	4.08
17:00:15	1030.94	117	2031	426	747	781	28	12.26	1.93	0.31	7.83	8.31	0.93	145.87	411.01	4.08
17:00:21	1031.19	116	1987	421	748	781	24	12.17	1.84	0.34	7.92	8.38	0.86	142.41	411.24	4.08

DOE high power motor test Amaco Catoosa Test Site

Well No. 23		Date: 02/28/98		Bit Type = Warner M Donald MF08H		Bit Size = 4 7/8		Bit Nozzles = 8, 9, 12, 12		Mud Type = Water Based		Mud Weight (lb/gal) = 8.50		Collar (ft) = 400.00		
Starting Depth =	1031.27	Flow	Press	Speed	Torque	Peak	Delta	Rock	Peak	Delta	WOB	Peak	Delta	ROP	Feet	Hours
Ending Depth =	1032.14	ISPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	RIPE	ft-lbs	ft-lbs	lbs	RIPE	RIPE	FT/HR	Chart	OnBit
Total Depth (Drill) =	380.87															
Hours On Bit =	0.58															
Average ROP =	63.72															
Drilling (ft) =	1071.36															
8:19:15	1031.27	108	673	924	-39	-39	21	19.66	1.81	0.23	0.99	0.34	0.58	189.94	411.76	4.1534
8:19:14	1031.33	112	667	406	-40	-29	20	19.60	1.82	0.24	0.12	0.38	1.05	299.43	411.76	4.1534
8:19:23	1031.74	108	1029	392	-37	-29	20	16.21	1.64	0.28	0.05	1.20	1.54	57.69	411.63	4.1562
8:19:30	1032.03	107	1160	359	-39	-25	21	16.25	1.80	0.26	1.02	0.65	0.64	81.44	413.00	4.1510
8:20:23	1032.18	107	1214	389	-38	-35	24	14.17	1.87	0.23	0.41	0.7	0.67	18.93	412.29	4.1215
8:20:38	1032.40	107	1397	386	-38	-29	20	12.47	1.87	0.34	1.14	0.88	4.01	61.31	412.47	4.1256
8:20:58	1032.68	107	1637	389	-41	-28	20	8.82	1.98	0.31	0.78	10.64	1.08	78.45	412.75	4.1288
8:20:58	1032.94	104	1775	378	-40	-29	24	18.87	2.63	0.64	0.94	0.34	1.03	138.14	413.88	4.1313
8:21:04	1033.18	106	1853	380	-39	-30	16	10.86	3	0.35	0.95	0.05	0.31	148.3	415.23	4.133
8:21:16	1033.44	106	1547	380	-39	-20	20	10.9	1.84	0.31	0.71	0.07	0.54	148.84	415.48	4.1347
8:21:17	1033.69	107	1935	389	-41	-25	13	10.48	2.03	0.4	0.75	0.28	0.44	130.54	415.73	4.1367
8:21:23	1033.94	103	1644	378	-39	-21	40	10.93	1.92	0.36	0.67	0.07	0.44	132.08	415.99	4.1361
8:21:31	1034.19	106	1629	385	-41	-25	53	10.74	1.98	0.45	0.87	0.23	0.31	116.4	414.25	4.1404
8:21:38	1034.44	109	1970	384	-40	-21	53	10.75	3	0.59	0.82	0.19	0.84	120.58	414.5	4.1434
8:21:45	1034.69	109	1932	382	-37	-25	48	10.79	1.95	0.47	0.85	0.19	0.74	127.01	414.76	4.1444
8:21:53	1034.94	106	1908	387	-37	-25	48	10.88	1.94	0.46	0.94	0.34	0.78	107.83	414.89	4.1465
8:22:04	1035.19	103	1674	375	-42	-25	39	10.48	1.90	0.38	0.18	0.5	0.74	88.33	415.05	4.1468
8:22:18	1035.45	103	2248	381	-31	-21	368	10.47	3.66	0.61	0.19	10.46	1.21	58.76	416.5	4.1524
8:22:45	1035.6	109	1456	360	-32	-25	83	13.97	2.18	1.26	0.4	0.62	15.63	18.88	416.65	4.163
8:22:54	1035.85	107	1761	399	-38	-25	24	16.36	1.86	0.31	3.32	4.4	2.06	65.19	416.81	4.1576
8:23:12	1036.1	108	1671	388	-39	-29	20	15.06	1.95	0.33	4.5	4.44	0.88	26.22	418.15	4.1627
8:23:38	1036.35	103	1674	389	-41	-29	24	14.67	1.87	0.32	4.81	4.95	0.67	37.36	416.36	4.1603
8:24:05	1036.6	107	1658	391	-40	-29	20	14.59	1.87	0.34	3.02	6.77	2.72	38.29	416.85	4.1702
8:24:13	1036.85	107	1781	389	-40	-29	20	12.87	1.86	0.32	0.73	1.09	0.84	84	418.0	4.1731
8:24:21	1037.1	107	1778	388	-39	-29	20	12.78	1.87	0.33	0.8	1.08	0.83	84	418.0	4.1731
8:24:32	1037.35	106	1801	393	-39	-29	20	12.8	1.87	0.33	0.76	1.08	0.87	80.23	417.41	4.1688
8:24:42	1037.6	103	1804	377	-39	-29	20	12.8	1.9	0.38	0.78	1.06	0.57	80.88	417.66	4.1677
8:24:53	1037.85	108	1788	381	-39	-29	24	12.77	1.92	0.48	0.83	1.08	0.58	84.79	417.9	4.1625
8:25:04	1038.1	109	1794	384	-38	-29	20	12.75	1.87	0.38	1.07	1.47	0.91	80.22	418.11	4.1683
8:25:23	1038.35	107	1732	389	-39	-30	16	12.62	1.89	0.38	0.89	1.38	0.88	78.26	418.65	4.202
8:25:34	1038.6	107	1793	389	-39	-30	16	12.75	1.89	0.38	0.89	1.38	0.88	78.26	418.65	4.202
8:25:41	1038.85	105	1899	382	-41	-30	18	12.42	1.88	0.31	1.17	1.95	1.58	119.17	418.31	4.2043
8:25:48	1039.1	104	1861	379	-38	-29	13	11.88	1.85	0.31	1.77	0.14	0.67	130.21	418.17	4.2006
8:25:55	1039.35	103	1884	372	-37	-25	26	11.89	1.86	0.36	1.71	0.92	0.85	128.27	418.42	4.2038
8:26:02	1039.6	100	1871	381	-29	-20	20	11.84	1.94	0.40	1.76	0.14	0.89	132.13	418.85	4.21
8:26:09	1039.85	106	1834	385	-39	-34	16	11.95	1.88	0.39	1.84	1.3	0.8	135.38	419.69	4.2117
8:26:16	1040.11	102	1834	383	-39	-38	16	11.88	1.87	0.35	1.71	0.67	0.67	133.68	420.15	4.2136

DOE high power mortar test Amaco Cataosa Test Site

Well No. 25		Date: 2/26/98															
Starting Depth = 1031.97		Bit Type = Walker McDanahay MP68H															
Ending Depth = 1382.14		Bit Size = 4.75															
Total Depth Drilled = 350.17		Bit Nozzles = 8, 8, 12, 12															
Mounts On Bit = 8.53		Mud Type = Water Based															
Average ROP = 53.73		Mud Weight (lb/gal) = 9.00															
Circulating It = 1071.36		Pipe ID = 663.62												Casing ID = 408.65			
TIME	BIT	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	NOOR	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours	
HH:MM:SS	FEET	GPM	PSI	RPM	LB-FT	LB-FT	LB-FT	KIPS	Qz	SPs	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit	
8:28:28	1040.30	104	1818	379	-39	-38	30	11.72	1.68	0.34	7.87	8.14	0.68	115.02	430.4	4.218	
8:28:30	1040.61	106	1875	384	-40	-28	20	11.62	1.81	0.41	7.97	8.30	0.78	94.83	429.67	4.2186	
8:28:33	1040.88	109	1884	388	-40	-25	24	11.54	1.69	0.38	8.09	8.51	0.67	83.82	429.82	4.2192	
8:28:34	1041.11	106	1899	393	-40	-29	29	11.48	1.66	0.34	8.13	8.45	0.57	76.75	424.98	4.2244	
8:27:38	1041.38	107	1908	388	-40	-30	30	11.48	1.67	0.38	8.1	8.38	0.57	85.2	421.4	4.2278	
8:27:14	1041.61	106	1885	384	-40	-33	29	11.58	1.67	0.31	8.01	8.28	0.8	67.77	421.69	4.2301	
8:27:35	1041.88	108	1875	384	-38	-29	30	11.54	1.68	0.34	8.05	8.31	0.62	85.35	421.81	4.2308	
8:27:34	1042.11	107	1902	387	-40	-29	29	11.58	1.65	0.33	8.02	8.35	0.65	100.84	423.18	4.2352	
8:27:44	1042.38	107	1897	381	-40	-30	30	11.58	1.67	0.32	8.04	8.28	0.53	88.82	422.42	4.2361	
8:27:53	1042.61	106	1902	387	-40	-29	29	11.58	1.68	0.36	8.02	8.31	0.6	94.83	422.68	4.2407	
8:28:04	1042.88	108	1885	394	-40	-38	16	11.61	1.65	0.31	8.08	8.38	0.67	84.67	422.91	4.2426	
8:28:17	1043.11	107	1842	388	-41	-29	27	11.43	1.84	0.32	8.15	8.45	0.57	88.28	423.18	4.2473	
8:28:30	1043.38	107	1894	391	-40	-31	28	11.38	1.88	0.34	8.23	8.52	0.77	89.37	423.42	4.2513	
8:28:39	1043.61	103	1845	374	-40	-33	16	11.67	1.89	0.38	7.92	8.19	0.59	101.54	423.68	4.2538	
8:28:47	1043.88	108	1829	385	-40	-38	38	11.68	1.89	0.37	7.93	8.23	0.67	105.1	423.91	4.2569	
8:28:58	1044.11	105	1812	381	-40	-33	18	11.66	1.91	0.43	7.93	8.23	0.57	108.32	424.18	4.2582	
8:29:08	1044.38	105	1820	381	-40	-33	18	11.67	1.87	0.25	7.92	8.18	0.62	102.88	424.43	4.2607	
8:29:14	1044.61	105	1874	384	-39	-29	18	11.54	1.84	0.21	8.05	8.4	0.74	84.3	424.68	4.2638	
8:29:25	1044.87	107	1789	391	-40	-26	29	11.58	1.89	0.18	8.21	8.47	0.63	84.83	424.94	4.2678	
8:29:47	1045.12	107	1750	389	-40	-33	19	11.24	1.89	0.17	8.34	8.64	0.73	47.52	425.19	4.2723	
8:30:02	1045.37	107	1776	386	-40	-38	18	11.33	1.3	0.15	8.23	8.8	0.58	69.43	425.42	4.2763	
8:30:19	1045.62	107	1771	394	-42	-33	20	11.3	1.89	0.13	8.28	8.55	0.6	92.34	425.65	4.2814	
8:30:30	1045.87	107	1748	389	-41	-33	18	11.26	1.85	0.25	8.31	8.82	0.6	84.83	425.93	4.286	
8:30:40	1046.12	108	1732	382	-40	-33	16	11.27	1.81	0.14	8.31	8.68	0.53	88	426.18	4.2908	
8:31:07	1046.37	107	1788	380	-40	-28	20	11.39	1.89	0.3	8.18	8.55	0.79	68.38	426.42	4.2946	
8:31:23	1046.62	108	1786	382	-42	-38	20	11.29	1.84	0.28	8.3	8.53	0.58	55.82	426.88	4.2981	
8:31:39	1046.87	108	1751	387	-41	-29	20	11.32	1.83	0.29	8.27	8.6	0.6	54.85	426.91	4.3037	
8:31:54	1047.12	108	1750	394	-41	-33	16	11.31	1.82	0.26	8.27	8.67	0.57	60.68	427.17	4.3073	
8:32:08	1047.37	107	1790	389	-42	-29	24	11.43	1.83	0.3	8.15	8.45	0.69	72.14	427.41	4.3113	
8:32:25	1047.62	108	1747	392	-42	-33	20	11.24	1.81	0.23	8.34	8.52	0.59	47.84	427.86	4.3168	
8:32:41	1047.87	107	1788	391	-41	-23	18	11.32	1.83	0.28	8.28	8.47	0.6	88.25	427.91	4.3206	
8:33:01	1048.13	108	1754	391	-42	-33	20	11.34	1.82	0.25	8.35	8.55	0.43	43.77	428.17	4.3264	
8:33:18	1048.37	103	1774	384	-42	-33	38	11.33	1.85	0.3	8.28	8.47	0.48	62.57	428.43	4.3304	
8:33:38	1048.62	108	1753	387	-41	-33	38	11.38	1.85	0.3	8.22	8.45	0.53	62.88	428.68	4.3344	
8:33:41	1048.87	107	1774	380	-42	-33	23	11.48	1.83	0.35	8.1	8.35	0.67	60.34	428.93	4.3373	
8:34:02	1049.12	109	1745	398	-41	-33	18	11.59	1.81	0.24	8.28	8.67	0.81	42.99	429.17	4.3433	
8:34:28	1049.37	107	1742	391	-42	-33	18	11.18	1.87	0.37	8.4	8.74	0.91	57.75	429.43	4.3488	

DOE high power mortar test Amaco Catoosa Test Site

TIME MM:SS	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELT ft-lbs	HOCR LOAD KIPS	PEAK G's	DELTA G's	WOB KIPS	PEAK KIPS	DELTA KIPS	RCP FT/HR	Fast DRHR	Hours DRHR
8:33:28	1048.62	105	1874	382	-41	-33	16	11.84	1.86	0.58	8.04	8.43	1.05	89.47	439.66	4.3537
8:34:42	1048.67	108	1881	385	-41	-33	16	11.01	1.86	0.59	7.87	7.92	0.72	139.05	429.33	4.3544
8:34:51	1050.12	108	1877	388	-41	-33	16	11.72	1.86	0.29	7.85	8.23	0.80	108.67	430.2	4.3587
8:35:09	1050.37	108	1824	387	-41	-33	16	11.58	1.87	0.31	8	8.33	0.82	98.41	430.41	4.3593
8:35:18	1050.62	108	1823	380	-42	-33	20	11.53	1.84	0.31	8.05	8.35	0.85	80.27	430.67	4.3598
8:35:27	1050.67	108	1855	385	-42	-33	20	11.55	1.85	0.31	8.03	8.43	0.38	84.83	430.82	4.3599
8:35:36	1051.12	108	1820	388	-41	-33	16	11.73	1.87	0.36	7.85	8.23	0.79	114.96	431.18	4.3605
8:35:39	1051.37	107	1838	389	-41	-33	16	11.83	1.86	0.34	8.04	8.31	0.6	84.71	431.48	4.3602
8:35:49	1051.69	108	1835	385	-42	-33	16	11.51	1.84	0.31	8.06	8.35	0.66	61.93	431.88	4.3701
8:35:59	1051.85	105	1851	384	-41	-33	20	11.80	1.88	0.35	8.02	8.31	0.81	88.4	431.88	4.3702
8:36:07	1052.13	107	1862	389	-41	-33	16	11.76	1.85	0.31	7.21	8.19	0.84	121.74	432.17	4.3753
8:36:18	1052.38	108	1815	395	-41	-33	20	11.48	1.83	0.25	8.03	8.38	0.57	89.58	432.42	4.3811
8:36:28	1052.63	108	1856	394	-48	-37	16	11.57	1.85	0.28	8.31	8.35	0.67	68.98	432.97	4.3836
8:36:37	1052.88	105	1862	390	-41	-33	16	11.3	1.84	0.28	7.87	8.26	0.82	101.81	432.98	4.3862
8:36:46	1053.13	105	1892	382	-42	-33	16	11.86	1.84	0.25	7.81	8.21	0.65	89.48	433.17	4.3868
8:36:55	1053.38	108	1832	385	-42	-33	16	11.84	1.84	0.28	7.83	8.28	0.77	104.78	433.48	4.3914
8:37:04	1053.63	108	1858	384	-43	-33	16	11.81	1.84	0.28	7.88	8.25	0.98	88.75	433.87	4.3937
8:37:12	1053.88	105	1884	384	-42	-33	16	11.88	1.84	0.28	7.83	8.26	0.79	104.98	433.93	4.3962
8:37:21	1054.13	108	1877	382	-42	-33	16	11.53	1.85	0.25	7.94	8.28	0.6	100.59	434.18	4.3988
8:37:30	1054.38	105	1908	384	-42	-33	16	11.89	1.85	0.37	7.82	8.28	0.74	88.28	434.58	4.4011
8:37:39	1054.63	106	1871	387	-42	-33	16	11.62	1.81	0.29	7.88	8.26	0.77	104.81	434.87	4.4034
8:37:48	1054.88	108	1752	388	-42	-33	20	11.37	1.84	0.25	8.3	8.57	0.79	84.37	434.87	4.408
8:38:08	1055.13	108	1795	385	-44	-33	20	11.4	1.81	0.25	8.17	8.4	0.83	88.12	435.2	4.4117
8:38:17	1055.38	104	1894	385	-43	-33	16	11.54	1.83	0.31	7.93	8.33	0.89	108.88	435.42	4.414
8:38:29	1055.63	107	1818	381	-42	-33	16	11.48	1.85	0.3	8.1	8.45	0.74	78.89	435.58	4.4178
8:38:41	1055.88	109	1754	385	-42	-33	20	11.37	1.85	0.22	8.2	8.57	0.88	70.78	435.98	4.4209
8:38:54	1056.13	108	1792	382	-38	-29	20	11.42	1.85	0.21	8.18	8.43	0.88	78.85	436.18	4.4243
8:39:12	1056.38	107	1770	389	-42	-33	20	11.26	1.83	0.23	8.31	8.64	0.76	81.68	436.34	4.4282
8:39:19	1056.63	108	1872	384	-42	-28	20	11.7	1.83	0.27	7.87	8.19	0.52	114.67	436.68	4.4318
8:39:31	1056.88	105	1738	382	-42	-33	20	11.47	1.86	0.31	8.3	8.43	0.93	73.58	436.88	4.4347
8:39:43	1057.13	107	1785	385	-42	-33	20	11.41	1.83	0.24	8.15	8.68	1.01	75	437.18	4.4381
8:39:56	1057.38	107	1798	388	-40	-28	20	11.41	1.88	0.33	8.18	8.67	1.23	72.31	437.44	4.4416
8:40:07	1057.64	108	1811	383	-40	-28	20	11.48	1.85	0.25	8.08	8.38	0.81	78.82	437.7	4.4447
8:40:13	1057.89	108	1848	382	-43	-33	16	11.87	1.86	0.3	7.8	7.95	0.72	148.51	437.98	4.4484
8:40:20	1058.14	108	1822	387	-43	-33	20	11.88	1.85	0.32	7.86	7.95	0.76	133.31	438.18	4.4514
8:40:27	1058.39	107	1857	389	-44	-33	20	11.66	1.81	0.34	7.73	8.04	0.78	125.38	438.43	4.4559
8:40:35	1058.64	105	1837	381	-43	-33	16	11.77	1.81	0.21	7.79	8.14	0.66	121.84	438.88	4.4624

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	MIN	R-Rate	LOAD	IPS	CS	KIPS	KIPS	KIPS	FT/HR	Depth	Cost
8:35:43	1059.88	107	1819	350	-41	-39	24	11.74	1.81	0.32	7.82	8.17	0.63	110.33	439.94	4.4547
8:36:20	1059.14	107	1810	351	-42	-39	16	11.72	1.82	0.28	7.85	8.14	0.65	118.53	439.19	4.4567
8:36:59	1058.39	107	1820	348	-43	-39	16	11.72	1.82	0.24	7.89	8.11	0.57	105.90	438.43	4.4588
8:37:27	1058.64	109	1795	337	-42	-39	20	11.64	1.83	0.34	7.92	8.24	0.74	167.52	437.69	4.4613
8:37:58	1059.89	108	1787	338	-42	-39	20	11.42	1.83	0.25	8.15	8.6	0.77	74.83	436.94	4.4637
8:38:21	1060.14	108	1766	337	-42	-39	20	11.48	1.85	0.31	8.08	8.38	0.66	76.42	440.19	4.4682
8:38:43	1060.39	107	1784	340	-43	-39	20	11.60	1.87	0.31	8.09	8.39	0.5	89.5	438.43	4.4711
8:38:50	1060.64	108	1803	333	-42	-38	20	11.78	1.88	0.42	7.82	8.24	0.66	105.6	440.69	4.4733
8:39:06	1060.89	107	1831	329	-42	-39	18	12	1.88	0.34	7.96	7.9	0.67	183.39	440.95	4.4753
8:39:23	1061.14	105	1837	333	-42	-39	16	11.93	1.87	0.35	7.84	8.02	0.74	138.0	441.2	4.4788
8:39:38	1061.39	104	1833	330	-41	-39	16	11.84	1.88	0.42	7.73	8.18	0.66	117.42	441.45	4.4795
8:39:57	1061.64	105	1848	334	-41	-38	16	11.81	1.88	0.38	7.76	8.23	0.64	122.52	441.69	4.4811
8:40:09	1061.89	109	1853	337	-42	-39	20	11.76	1.89	0.28	7.81	8.11	0.73	110.88	441.94	4.4831
8:40:24	1062.14	108	1845	332	-43	-39	20	11.8	1.84	0.34	7.96	8.28	0.66	102.66	442.19	4.4857
8:40:40	1062.39	108	1810	332	-43	-39	16	11.44	1.82	0.38	8.13	8.36	0.53	85.23	442.43	4.4888
8:40:58	1062.64	103	1849	338	-41	-39	30	11.86	1.84	0.28	8.1	8.38	0.57	78.97	442.69	4.4923
8:41:08	1062.89	108	1839	337	-41	-38	20	11.88	1.85	0.27	8.07	8.31	0.53	86.83	441.94	4.4931
8:41:23	1063.14	108	1808	443	779	282	361	18.38	1.85	0.51	8.8	8.81	0.21	31.83	443.96	4.5034
8:41:52	1063.47	109	1860	438	908	1117	253	14.94	2.01	0.56	8.24	8.32	0.89	97.51	443.53	4.506
8:42:08	1063.72	109	1899	442	1064	1157	401	11.34	2	0.4	8.48	10.38	1.72	131.64	443.78	4.5174
8:42:44	1063.97	104	1895	434	1084	1174	203	11.07	1.89	0.53	10.12	10.36	1.05	165.23	444	4.5282
8:43:00	1064.22	107	1877	443	1016	1199	374	11.4	1.99	0.53	8.89	10.40	1.41	193.39	444.31	4.5398
8:43:52	1064.47	107	1828	443	1044	1133	302	11.06	1.96	0.51	8.53	10.01	1.1	217.34	444.22	4.5477
8:44:07	1064.72	107	1862	444	981	1159	380	11.39	2.01	0.63	8.88	10.31	1.31	188.38	444.77	4.5539
8:44:02	1064.97	104	1923	436	1045	1179	289	11.16	2.08	0.62	10.33	10.34	1.15	172.36	445.01	4.5543
8:44:08	1065.22	108	1877	451	981	1154	247	11.22	1.98	0.54	8.84	10.33	0.83	173.48	445.26	4.5558
8:44:13	1065.47	106	1889	448	893	1134	247	11.24	2.04	0.6	8.95	10.44	0.94	187.83	445.53	4.5579
8:44:18	1065.72	107	1825	446	957	1267	359	11.14	2.08	0.6	10.06	10.51	0.96	160.29	445.96	4.5586
8:44:24	1065.97	108	1859	442	984	1121	280	11.12	1.86	0.52	10.57	10.83	1.06	188.17	446.03	4.5623
8:44:28	1066.22	103	1901	429	1026	1081	123	11.38	2.02	0.65	8.38	10.44	1.01	173.47	446.27	4.5628
8:44:33	1066.47	104	1932	438	1073	1174	174	11.18	2.02	0.64	10.31	10.53	1.1	163.68	446.52	4.5633
8:44:40	1066.72	104	2001	433	1141	1201	257	11.54	2.02	0.63	10.44	10.53	0.86	178.78	446.78	4.5646
8:44:48	1066.97	104	1998	435	1100	1154	188	11.13	2.14	0.69	10.38	10.51	0.88	150	447.04	4.5664
8:44:51	1067.22	104	1978	434	1102	1134	190	11.1	2.14	0.61	10.08	10.53	0.84	166.87	447.27	4.5681
8:44:57	1067.46	108	2000	448	1138	1267	219	11.09	2.08	0.63	10.1	10.56	0.98	167.75	447.52	4.5695
8:45:02	1067.71	103	2048	431	1176	1349	228	11.52	2.15	0.68	8.87	10.46	1.18	177.8	447.78	4.5708
8:45:07	1067.96	104	2057	434	1202	1279	180	11.29	2.27	0.7	8.98	10.53	1.30	182.62	448.02	4.5724

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOR	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Pres	Hum
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	Gs	Gs	KIPS	KIPS	KIPS	FT/HR	OnSu	OnSu
8:50:12	1068.23	103	2118	432	1248	1384	340	11.23	2.31	1.09	8.05	10.53	1.22	187.4	448.27	4.5030
8:50:17	1068.48	105	2191	437	1225	1358	235	11.21	2.22	1.03	8.07	10.58	1.20	186.29	448.50	4.5052
8:50:23	1068.73	104	2145	434	1233	1405	344	11.18	2.3	0.99	10.04	10.53	1.03	171.47	448.82	4.5087
8:50:29	1068.98	104	2115	430	1193	1352	312	11.04	2.31	0.96	10.16	10.85	1.1	144.7	448.05	4.5094
8:50:36	1069.23	102	2156	426	1241	1377	798	11.1	2.29	1.08	10.00	10.92	1.53	103.12	448.27	4.5091
8:50:40	1069.48	103	2123	430	1181	1372	478	11.14	2.33	1.11	10.05	10.88	1.38	185.28	448.96	4.5115
8:50:47	1069.73	105	2050	428	1124	1318	389	10.87	2.20	1.07	10.32	10.84	1.1	130.04	448.78	4.5135
8:50:54	1069.98	108	2102	438	1203	2732	2131	10.84	2.31	0.93	10.34	11.9	2.91	131.75	450.95	4.5136
8:51:01	1070.24	104	2030	432	1498	2738	2301	12.37	2.25	1.14	8.8	11.87	5.62	141.8	450.28	4.5173
8:51:03	1070.49	108	1792	444	257	1267	802	16.1	2.25	1.01	5.08	6.58	3.47	117.22	450.84	4.5186
8:51:14	1070.74	105	1913	439	1029	1344	620	14.49	2.27	1.06	6.7	6.33	3.21	103.57	450.61	4.521
8:51:21	1070.99	104	1831	442	1044	1287	488	13.87	2.31	1.18	7.31	6.57	1.75	140.41	451.03	4.5237
8:51:25	1071.24	105	2072	437	1073	1308	314	13.78	2.32	1.2	7.4	8.23	3.06	225.88	451.3	4.5238
8:51:30	1071.49	105	2086	439	1162	2539	1849	13.76	2.3	1.09	7.42	8.56	3.98	173.1	451.58	4.5255
8:51:36	1071.75	109	2157	451	1388	2571	1855	13.48	2.29	1.16	7.72	8.62	3.88	183.52	451.83	4.5267
8:51:38	1072	103	1856	440	752	1320	779	17.46	2.11	0.76	3.63	7.37	3.27	218.42	452.04	4.5278
8:51:49	1072.25	108	1750	448	913	1261	867	15.27	2.28	1.03	5.9	7.83	4.28	88.96	452.3	4.5297
8:51:55	1072.5	107	1848	444	913	1188	881	13.73	2.13	0.89	7.45	8.16	1.24	170.19	452.56	4.5323
8:52:02	1072.75	106	1914	442	920	1552	359	13.2	2.07	0.78	7.96	8.43	1.93	121.47	452.81	4.5345
8:52:08	1073	108	1912	442	916	1543	232	13.06	2.14	0.97	8.12	8.86	1.27	123.68	453.04	4.5383
8:52:30	1073.25	107	1829	445	931	2101	1288	12.73	2.20	1.03	8.49	9.62	3.23	71.89	453.3	4.5404
8:52:39	1073.5	106	1830	442	1004	1336	593	13.17	2.24	1.49	9.15	9.34	1.48	128.82	453.54	4.5419
8:52:34	1073.75	108	1800	452	954	1044	388	13.41	2.08	0.73	7.76	8.38	0.69	167.93	453.81	4.5438
8:52:41	1074	109	1783	452	833	649	580	13.29	2.08	0.63	7.89	8.25	0.93	148.34	454.08	4.5454
8:52:47	1074.25	106	1749	441	833	829	164	13.16	2.01	0.61	5.01	8.45	0.86	134.54	454.31	4.5468
8:52:54	1074.5	108	1783	446	890	893	288	13.21	2.02	0.66	7.98	8.40	0.96	129.22	454.58	4.5488
8:53:01	1074.75	107	1797	447	884	883	199	13.20	1.99	0.63	7.91	8.4	0.93	137.71	454.81	4.5505
8:53:07	1075	109	1851	440	904	1044	150	13.29	2.01	0.6	7.88	8.35	1.01	147.97	455.06	4.5522
8:53:13	1075.25	104	1883	442	970	1049	189	13.29	2.13	0.84	7.63	8.35	0.83	136.64	455.31	4.5543
8:53:16	1075.51	105	1836	439	991	971	166	13.29	1.88	0.81	7.9	8.4	0.88	106.34	455.56	4.5573
8:53:24	1075.76	111	1774	480	884	1077	384	13.03	2.06	0.73	8.14	8.82	1.24	101.62	455.8	4.5602
8:53:34	1076.01	108	1886	437	820	1036	211	13.38	2.09	0.69	7.81	8.26	1.01	103.28	456.03	4.5617
8:53:42	1076.26	107	1800	438	880	1016	255	12.98	2.08	0.74	8.21	8.64	0.86	107.88	456.1	4.5623
8:53:50	1076.51	108	1798	443	859	1025	450	12.81	2.05	0.71	8.38	9	1.08	93.78	456.56	4.5668
8:54:21	1078.76	105	1725	449	749	1020	446	12.49	2.06	0.69	8.07	8.63	0.83	40.84	457.8	4.6028
8:54:31	1078.96	105	1843	440	699	942	429	12.41	2.03	0.69	8.78	9.1	0.67	24.82	457	4.6112
8:55:15	1077.21	109	1883	449	787	971	448	12.53	2.08	0.72	8.65	9.12	0.64	37.87	457.28	4.6177

DOE high power mortar test Amaco Catonsa Test Site

TIME	BIT DEPTH FEET	FLOW GPM	PRESS PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELT ft-lbs	HOOK LOAD KIPS	PEAK G's	DELTA G's	WOB KIPS	PEAK RPIE	DELTA RPIE	RCP FT/HR	Feet Drift	Hours OnBit
8:59:25	1077.40	306	1755	543	939	1379	739	12.24	2.68	3.29	6.93	10.29	2.44	61.05	467.91	4.522
8:59:48	1077.71	306	1764	480	802	1085	480	10.6	2.08	0.89	13.55	11.56	2.13	64.68	467.75	4.6386
8:59:54	1077.96	305	1872	429	821	1060	366	10.29	2.08	0.71	10.85	11.32	0.54	118.67	468	4.6386
8:59:54	1078.31	306	1834	449	880	1032	235	10.27	2.1	0.74	10.87	11.35	0.93	91.41	459.27	4.6310
8:59:15	1078.46	305	1824	437	870	887	275	10.86	2.09	0.77	10.92	11.97	1.01	97.16	458.91	4.6341
8:59:22	1078.71	308	1807	486	941	1101	442	10.2	2.11	0.73	10.88	11.47	1.05	98.44	458.75	4.6387
8:59:34	1078.96	307	1790	444	838	1036	340	10.14	3.11	0.78	11.05	11.48	0.93	78.23	458.88	4.6388
8:59:42	1079.22	308	1864	451	840	1121	365	10.31	2.08	0.78	10.87	11.3	1.03	106.33	458.28	4.6429
8:59:48	1079.47	304	2001	438	1183	3118	349	10.84	2.05	1.85	10.84	11.15	1.36	123.33	458.51	4.6443
8:59:55	1079.73	308	2116	442	1014	1312	872	12.87	3.28	3.05	8.28	12.05	7.70	159.28	458.78	4.6455
8:59:58	1079.97	308	1790	438	775	874	236	15.87	2.34	0.93	5.18	5.87	1.13	81.9	460.02	4.6467
8:59:14	1080.22	305	1728	449	701	862	293	16.05	2.11	0.72	5.1	5.83	1.03	101.15	460.38	4.651
8:59:30	1080.47	310	1879	385	714	838	288	15.76	2.11	0.73	5.28	5.77	0.88	58.17	460.51	4.6503
8:59:43	1080.72	313	1693	459	645	855	284	15.78	2.03	0.8	5.38	5.79	1.03	88.77	460.77	4.655
8:59:58	1080.97	313	1880	458	821	773	384	18.74	1.96	0.55	6.48	5.91	1.37	57.11	461.01	4.6612
8:59:18	1081.22	316	1582	456	511	777	292	15.86	2.01	0.83	5.48	5.94	1.09	45.39	461.06	4.6681
8:59:31	1081.47	308	1579	446	526	740	199	15.83	2.01	0.95	5.32	5.85	0.85	73.28	461.5	4.6722
8:59:31	1081.72	306	1575	489	516	745	348	15.85	2.08	0.87	5.42	5.84	0.98	44.67	461.77	4.6775
8:59:37	1081.97	306	1583	453	618	704	279	16.7	2.06	0.75	5.44	5.94	0.91	64.05	461.99	4.6805
8:59:37	1082.18	308	1512	452	959	749	349	15.35	2.05	0.84	5.01	5.04	2.98	58.12	462.24	4.6806
8:59:03	1082.41	308	1894	449	846	781	287	11.53	1.89	0.82	6.64	15.41	2.55	35.75	462.48	4.6872
8:59:22	1082.68	307	1838	445	876	777	238	11.21	2.62	0.83	6.68	10.39	0.86	48.88	462.68	4.6912
8:59:38	1082.91	307	1889	443	731	871	454	11.23	3.38	0.73	6.93	10.38	0.93	48.43	462.99	4.7083
8:59:53	1083.18	307	1784	445	821	1088	543	11.42	2.82	0.88	6.75	10.32	1.46	88.7	463.29	4.712
8:59:04	1083.41	302	1931	428	889	1648	328	12.82	2.98	0.71	6.15	5.69	1.23	139.35	463.49	4.7187
8:01:08	1083.67	300	1874	441	876	1030	243	11.88	2	0.59	9.28	9.88	1.43	145.07	463.75	4.7187
8:01:17	1083.82	307	1833	444	856	879	271	11.51	2.58	0.73	6.28	10.13	1.1	86.01	463.96	4.7183
8:01:24	1084.17	309	1816	442	803	881	367	11.7	2.64	0.64	5.48	8.93	1.1	117.48	464.21	4.7256
8:01:39	1084.42	308	1795	441	742	967	488	11.3	2.65	0.7	6.88	10.98	1.15	62.51	464.45	4.7245
8:01:48	1084.67	309	1781	442	818	838	258	11.81	2.65	0.77	6.88	9.86	0.89	98.19	464.72	4.7273
8:01:53	1084.92	308	1837	439	838	875	243	11.72	2.1	0.7	6.44	8.88	0.89	128.08	464.97	4.7283
8:02:12	1085.17	306	1787	443	794	843	236	11.28	3.05	0.73	6.94	10.32	0.98	83.12	465.21	4.7336
8:02:38	1085.43	303	1778	438	788	1020	388	11.2	2.16	0.86	6.96	10.34	1.04	80.3	465.47	4.7389
8:02:52	1085.67	307	1877	448	887	773	134	11.18	8.07	0.78	10.03	10.39	0.77	41.84	465.73	4.7439
8:03:08	1085.92	305	1771	442	838	1218	693	11.41	2.88	0.7	6.74	10.34	1.04	63.5	465.98	4.7489
8:03:12	1086.17	308	2061	441	980	1037	186	12.01	3.13	0.88	6.15	6.05	1.22	181.54	466.22	4.7534
8:03:18	1086.42	305	1875	438	875	1085	389	11.89	2.79	0.71	9.17	8.62	0.85	148.95	466.48	4.7581

Well No. 23
 Date: 2/26/86
 Starting Depth = 1081.27
 Ending Depth = 1082.14
 Total Depth Crated = 350.87
 Hours On Bit = 6.83
 Average ROP = 53.72
 Cratering (ft) = 1071.36

Bit Type = Wacker McDowell MP58H
 Bit Size = 4.75
 Bit Grades = 8, 9, 12, 12
 Mud Type = Water Based
 Mud Weight (lb/gal) = 9.00
 Pipe (in) = 603.88
 Collar (in) = 406.88

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23		Date: 2/26/98		Bit Type = Weather McComboid MP58H		Bit Size = 4.75		Bit Nozzles = 3, 9, 12, 12		Mud Type = Water Based		Mud Weight (lbs/gal) = 8.55		Pump (ft) = 302.58		Coke (ft) = 408.68	
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	RQP	Feet	Hours	
HR:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	RPM	ft-lbs	%	RPM	RPM	RPM	FT/HR	OnBR	OnBR	
9:03:38	1095.67	104	1970	425	548	1239	630	11.72	2.07	0.71	9.44	10.13	1.43	170.59	488.74	2.7542	
9:03:23	1095.83	106	1982	423	643	1182	381	11.88	2.08	0.75	9.5	9.91	1.01	135.91	486.87	2.7568	
9:03:47	1097.18	106	1918	443	915	1020	339	11.79	2.08	0.7	9.36	9.84	1.01	118.07	487.25	2.7587	
9:03:47	1097.42	104	2013	435	1040	1137	297	11.58	2.17	0.59	9.18	9.67	1.08	147.85	487.47	2.7601	
9:03:54	1097.69	107	2019	443	1021	1137	293	11.8	2.49	0.81	9.28	9.98	1.37	138.69	487.73	2.7621	
9:04:07	1097.29	106	1983	440	658	1077	288	11.88	2.11	0.66	9.5	10.2	1.2	122.45	487.39	2.7643	
9:04:29	1098.18	106	1983	441	978	1151	280	11.73	2.08	0.65	9.43	9.99	0.88	126.82	488.22	2.7661	
9:04:19	1098.42	107	1917	447	892	1222	336	11.35	2.04	0.64	9.71	10.17	1.29	83.98	488.47	2.7683	
9:04:30	1098.69	107	1898	446	803	1186	690	11.18	2.19	0.88	10	10.44	1.03	44.23	488.74	2.7707	
9:04:30	1098.89	107	1894	444	638	1202	679	11.48	2.09	0.66	9.71	10.1	0.89	85.04	488.97	2.7728	
9:05:00	1099.18	109	1859	453	834	1016	306	11.48	2.09	0.73	9.67	10.03	0.79	81.07	489.23	2.7800	
9:05:10	1099.43	108	1800	442	802	825	170	11.47	2.09	0.72	9.88	10.1	0.86	80.03	489.48	2.7823	
9:05:27	1099.86	106	1828	442	836	1271	636	11.28	2.09	0.69	9.88	10.41	1.15	65.43	489.73	2.7879	
9:05:27	1099.83	106	1881	443	823	1229	651	11.41	2.09	0.69	9.79	10.2	0.90	67.03	489.86	2.7908	
9:05:48	1099.18	109	1809	442	798	979	390	11.37	2.08	0.66	9.78	10.25	0.89	73.58	490.23	2.7942	
9:05:59	1099.43	108	1783	450	778	635	233	11.48	2.09	0.63	9.88	10.61	0.79	68.79	490.5	2.7968	
9:06:09	1099.89	108	1772	449	780	888	194	11.53	2.04	0.64	9.63	9.98	0.81	97.39	490.78	2.7983	
9:06:19	1099.93	108	1781	449	814	1048	332	11.63	2.17	0.80	9.69	10.06	1.17	93.21	491	2.8023	
9:06:29	1099.18	109	1871	440	879	978	180	11.53	2.08	0.73	9.39	9.65	0.88	148.93	491.28	2.8038	
9:06:30	1099.44	107	1905	438	811	978	148	12.03	2.04	0.69	9.12	9.56	0.81	155.46	491.46	2.8054	
9:06:56	1099.19	109	1899	439	880	979	196	12.08	2	0.81	9.08	9.55	0.85	155.83	491.74	2.8077	
9:06:41	1099.94	106	1867	441	844	823	134	12.07	2.11	0.71	9.08	9.63	1.09	167.43	492	2.8088	
9:06:48	1099.18	106	1803	440	827	927	154	11.38	2.01	0.8	9.19	9.85	0.88	135.28	492.24	2.8105	
9:06:36	1099.44	106	1810	441	809	896	85	11.68	2.08	0.84	9.3	9.72	0.86	134.68	492.59	2.8123	
9:07:02	1099.89	108	1791	442	785	888	188	11.68	1.96	0.85	9.49	10.01	1.1	116.71	492.74	2.8148	
9:07:12	1099.94	108	1786	440	782	854	138	11.58	2.03	0.86	9.58	9.98	0.84	90.81	492.86	2.8171	
9:07:24	1099.18	106	1812	443	798	1008	426	11.38	2.02	0.8	9.77	10.22	1.03	70.51	493.23	2.8203	
9:07:36	1099.44	106	1882	443	910	8086	1515	11.51	2.20	1.13	9.64	10.53	2.01	70.45	493.55	2.8237	
9:07:40	1099.89	104	1983	435	844	1340	812	12.17	2	0.81	9.99	9.62	1.34	190.65	493.73	2.8268	
9:07:48	1099.94	107	1784	445	707	947	336	12.11	1.92	0.4	9.04	9.69	1.15	188.63	493.89	2.8274	
9:08:08	1099.19	107	1874	446	882	802	373	11.87	1.99	0.8	9.27	9.72	0.96	54.96	494.24	2.8338	
9:08:20	1099.44	109	1789	448	898	856	209	11.78	1.99	0.82	9.4	9.85	1.1	48.44	494.51	2.8376	
9:08:21	1099.54	107	1838	443	781	827	371	12.09	1.94	0.84	9.2	10.08	0.83	102.86	494.89	2.8437	
9:08:26	1099.58	108	1821	430	1031	1190	316	11.57	2.04	0.86	10.14	10.58	1.15	123.21	495.19	2.8457	
9:08:34	1099.34	108	2078	431	1195	1214	283	11.71	1.99	0.86	10.01	10.81	1.1	156.0	495.30	2.8474	
9:08:40	1099.0	102	2093	424	1048	1170	218	11.75	1.98	0.48	9.96	10.48	1.03	181.41	495.64	2.8483	
9:08:46	1099.86	104	1918	432	879	1028	243	11.64	1.89	0.81	10.08	10.58	0.98	166.26	495.92	2.8505	

DOE high power mortar test Amaco Catonsa Test Site

Test No. 23	Date: 2/28/98																	
Starting Depth *	1021.27	Bit Type *	Walker McCornard MPRH															
Ending Depth *	1082.14	Bit Size *	4.75															
Total Depth Corred *	350.87	Bit Nozzles *	9, 9, 12, 12															
Hours On Bit *	6.88	Mud Type *	Water Based															
Average ROP *	50.72	Mud Weight (lb/gal)	9.00															
Drilling (ft) *	1071.85	Pipe (ft) *	870.68	Collar (ft) *	408.89													

TIME HH:MM:SS	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELTA ft-lbs	ROP		DELTA ft/s	WOB KIPS	PEAK KIPS	DELTA KIPS	ROP FT/HR	Feet OnBit	Hours OnBit
								LOAD KIPS	%							
8:12:54	1026.1	108	1871	428	873	1918	280	11.41	1.82	0.87	10.21	10.25	0.86	110.95	476.14	4.8528
8:14:02	1028.95	104	1854	430	851	896	342	11.43	1.85	0.3	10.28	10.27	0.88	111.01	476.4	4.8552
8:14:08	1030.6	107	1824	442	820	874	84	11.54	1.88	0.28	10.17	10.26	0.77	137.87	476.66	4.8568
8:14:17	1032.35	109	1796	446	795	927	307	11.45	1.91	0.34	10.27	10.5	0.85	110.75	476.91	4.8592
8:14:23	1034.1	108	1806	446	798	870	100	11.38	1.89	0.29	10.23	10.63	0.86	101.38	477.17	4.8612
8:14:31	1037.35	108	1763	440	789	846	117	11.42	1.87	0.31	10.28	10.7	0.88	113.5	477.39	4.8632
8:14:39	1037.6	107	1799	440	790	880	151	11.48	1.87	0.33	10.28	10.88	0.89	114.78	477.63	4.8652
8:14:48	1037.95	110	1748	454	788	878	195	11.38	1.86	0.28	10.46	10.8	0.89	107.85	477.92	4.868
8:15:02	1038.1	107	1752	443	781	880	235	11.07	1.92	0.33	10.84	11.94	0.93	88.98	478.14	4.8718
8:15:15	1038.35	108	1728	448	730	830	336	10.82	1.85	0.29	10.79	11.01	0.93	98.27	478.39	4.8761
8:15:34	1038.6	107	1711	442	728	815	316	10.86	1.84	0.29	10.77	11.09	0.73	89.56	478.66	4.8807
8:15:53	1038.85	108	1688	439	715	882	300	10.9	1.83	0.29	10.81	11.13	0.89	48.39	478.9	4.8858
8:16:07	1039.1	106	1807	437	681	881	247	10.60	1.84	0.25	10.74	11.11	0.74	62.53	479.18	4.8888
8:16:20	1039.35	108	1853	448	685	757	196	11.1	1.86	0.3	10.81	10.85	0.65	76.88	479.4	4.8938
8:16:36	1039.6	108	1728	447	750	831	361	10.83	1.87	0.32	10.77	11.15	0.93	65.33	478.85	4.8976
8:17:01	1039.85	107	1804	442	729	851	366	10.84	1.86	0.32	10.88	11.25	0.77	36.81	479.81	4.9047
8:17:20	1100.1	108	1751	437	787	1038	489	10.82	1.83	0.35	10.38	11.16	0.68	47.82	480.18	4.9102
8:17:29	1100.48	108	1800	437	858	1051	494	11.88	2.07	0.84	10.42	10.80	1.17	87.73	480.4	4.9128
8:17:39	1100.6	109	1878	438	889	1089	327	11.88	1.98	0.47	10.84	10.48	0.98	134.7	480.65	4.9142
8:17:42	1100.85	104	1943	403	830	1080	316	11.81	1.94	0.41	10.86	10.39	1.01	155.78	480.9	4.9162
8:17:58	1101.11	106	1754	440	757	915	350	11.05	1.86	0.34	10.85	11.11	1.03	63.85	481.17	4.9188
8:18:19	1101.36	108	1725	440	719	847	373	10.87	1.87	0.32	10.83	11.19	0.69	98.71	481.4	4.9208
8:18:40	1101.61	107	1704	444	759	878	364	10.86	1.83	0.34	10.84	11.18	0.67	42.58	481.85	4.9238
8:18:56	1101.86	107	1703	442	719	829	238	10.99	1.87	0.31	10.71	11.34	0.89	58.98	481.9	4.9268
8:19:06	1102.11	106	1857	438	712	823	188	11.84	1.88	0.27	10.87	10.92	0.83	71.88	482.16	4.9283
8:19:21	1102.36	109	1804	438	700	817	227	11.07	1.89	0.37	10.63	10.96	0.81	70.79	482.4	4.9344
8:19:34	1102.61	107	1736	441	747	879	230	11.11	1.89	0.31	10.58	10.83	0.87	73.84	482.65	4.9371
8:19:44	1102.86	107	1738	440	744	821	174	11.18	1.87	0.33	10.55	10.84	0.85	88.3	482.8	4.938
8:19:50	1103.11	107	1727	440	730	815	194	11.13	1.86	0.33	10.57	10.87	0.93	77.31	483.16	4.9384
8:20:07	1103.36	107	1708	444	714	825	286	11.11	1.87	0.28	10.60	10.84	0.86	76.29	483.41	4.9388
8:20:17	1103.61	107	1830	442	808	1121	448	11.37	2.08	0.88	10.54	10.87	1.13	98.34	483.65	4.9393
8:20:24	1103.86	105	1883	439	867	1184	538	11.88	1.95	0.46	10.15	10.78	1.1	124.68	483.84	4.9412
8:20:30	1104.11	105	1948	436	872	1077	393	11.51	1.88	0.34	10.19	10.69	0.46	104.85	484.18	4.9428
8:20:45	1104.36	105	1895	436	867	1044	385	11.28	1.88	0.51	10.48	10.89	1.01	80.84	484.41	4.9453
8:20:58	1104.61	107	1970	440	880	1145	528	11.54	2.03	0.61	10.18	10.77	1.27	134.7	484.66	4.9475
8:20:59	1104.86	104	1961	431	887	1109	263	11.63	2.02	0.8	10.07	10.51	1.03	138.85	484.91	4.9492
8:20:59	1105.11	104	2029	432	1054	1120	327	11.63	1.87	0.56	10.07	10.51	0.96	143	485.16	4.9518

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	LOAD	Q%	Q%	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
8:21:08	1085.30	107	1986	444	944	1048	374	11.28	1.92	0.38	10.92	10.44	0.84	482.79	486.47	4.9736
8:21:12	1085.81	107	1948	441	928	1044	249	11.6	1.91	0.41	10.11	10.53	0.91	481.42	486.66	4.9746
8:21:16	1086.32	106	1940	439	908	1039	352	11.45	1.95	0.46	10.25	10.75	1.03	483.13	485.82	4.9766
8:21:20	1086.83	105	1925	436	874	1034	482	11.54	1.99	0.61	10.16	10.86	1.13	482.51	486.17	4.9786
8:21:24	1087.34	103	1979	429	963	1050	399	11.56	1.97	0.45	10.15	10.69	1.05	480.87	486.43	4.9804
8:21:28	1087.85	103	1974	424	900	1012	297	11.41	1.88	0.35	10.38	10.7	0.98	482.27	486.67	4.9824
8:21:32	1088.37	108	1924	430	932	1084	275	11.42	1.92	0.44	10.26	10.7	1.03	487.18	488.91	4.9841
8:21:36	1088.88	107	1905	441	889	1073	417	11.22	1.81	0.4	10.48	10.89	0.98	488.55	487.17	4.9872
8:21:40	1089.39	103	1975	435	974	1088	604	11.09	1.93	0.44	10.81	11.84	0.98	488.48	487.41	4.9901
8:21:44	1089.90	103	2043	435	1037	1275	872	11.34	2.07	0.84	10.16	10.82	0.99	487.42	487.69	4.993
8:21:48	1090.41	103	2014	428	973	1184	374	11.67	1.84	0.45	10.62	10.48	1.1	482.86	487.92	4.9944
8:21:52	1090.92	108	1975	440	882	1082	176	11.36	1.92	0.35	10.12	10.98	0.98	480.31	488.19	4.9963
8:21:56	1091.43	106	1977	439	976	1101	235	11.55	1.93	0.43	10.14	10.82	0.98	483.39	488.43	4.9981
8:22:00	1091.94	105	1972	434	944	1083	239	11.5	1.99	0.46	10.2	10.7	1.03	482.53	488.07	5.0001
8:22:04	1092.45	108	1981	436	998	1219	417	11.35	1.84	0.44	10.32	10.72	0.99	480.36	488.82	5.0027
8:22:08	1092.96	106	1975	439	943	1094	292	11.36	1.81	0.32	10.14	10.53	0.89	487.3	488.17	5.0044
8:22:12	1093.47	105	1981	435	948	1091	286	11.54	1.94	0.45	10.16	10.53	0.86	487.05	488.42	5.0064
8:22:16	1093.98	105	1988	434	989	1185	392	11.48	1.92	0.47	10.21	10.7	1.04	487.12	489.67	5.0084
8:22:20	1094.49	107	1948	441	964	1069	323	11.62	1.88	0.44	10.17	10.9	0.99	483.46	489.85	5.0102
8:22:24	1095.00	103	1982	429	967	1109	280	11.91	1.89	0.35	10.19	10.63	1.01	480.89	490.43	5.0142
8:22:28	1095.51	106	1913	438	889	893	182	11.42	1.93	0.42	10.38	10.89	0.79	481.31	490.67	5.0185
8:22:32	1096.02	107	1944	441	932	883	307	11.40	1.92	0.41	10.27	10.69	0.89	487.36	490.93	5.0192
8:22:36	1096.53	106	1930	439	873	1052	355	11.36	1.88	0.37	10.3	10.72	0.91	487.78	491.18	5.0208
8:22:40	1097.04	107	1843	442	915	1108	330	11.46	2.04	0.64	10.34	10.63	0.66	480.67	491.44	5.0238
8:22:44	1097.55	109	1917	428	988	1108	291	11.37	1.8	0.35	10.39	10.77	0.89	488.15	491.67	5.0291
8:22:48	1098.06	106	1917	440	880	1038	287	11.34	1.92	0.38	10.38	10.77	0.79	489.22	491.92	5.0373
8:22:52	1098.57	106	1930	439	884	997	196	11.38	1.94	0.44	10.35	10.8	0.96	488.69	492.18	5.0396
8:22:56	1099.08	108	1885	445	845	1032	352	11.21	1.97	0.36	10.46	10.96	1.13	483.87	492.44	5.0323
8:23:00	1099.59	107	1895	441	875	1052	328	11.35	1.89	0.4	10.34	10.79	0.89	485.86	492.7	5.0348
8:23:04	1099.99	109	1936	440	878	965	199	11.38	1.88	0.4	10.3	10.89	0.91	480.79	492.93	5.0388
8:23:08	1100.40	108	1897	427	895	931	180	11.41	1.88	0.37	10.38	10.9	0.81	482.89	493.18	5.0391
8:23:12	1100.81	108	1844	434	850	980	299	11.38	1.87	0.35	10.23	10.75	0.89	484.27	493.43	5.0411
8:23:16	1101.22	107	1844	442	790	940	395	11.21	1.9	0.4	10.48	11.04	1.27	488.28	493.63	5.0437
8:23:20	1101.63	107	1801	444	780	938	324	11.38	1.9	0.39	10.33	10.98	1.88	487.71	493.93	5.0455
8:23:24	1102.04	106	1897	439	879	843	105	12.04	1.84	0.42	9.66	10.2	1.15	487.77	494.22	5.0477
8:23:28	1102.45	106	1829	436	878	983	188	12.04	1.82	0.44	9.63	10.27	1.39	483.89	494.45	5.0491

Well No: 23
 Date: 2/26/86
 Starting Depth = 1081.27
 Ending Depth = 1082.14
 Total Depth Drilled = 1080.87
 Hours On Bit = 6.53
 Average ROP = 53.72
 Drilling (ft) = 1071.36

Bit Type = Walker McDougald MP68H
 Bit Size = A 75
 Bit Nozzles = 9, 9, 12, 12
 Mud Type = Water Based
 Mud Weight (lb/gal) = 8.34
 Pipe In = 402.08

Corer (ft) = 403.88

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	ft-lbs	ft-lbs	KIPS	KIPS	KIPS	FT/HR	Orbit	Orbit
8:25:28	1114.64	100	2037	435	1041	1233	324	11.84	2.31	0.87	10.05	10.05	1.15	141.99	494.92	5.0568
8:25:53	1114.69	104	2050	432	1021	1124	364	11.08	1.37	0.48	10.03	10.44	0.03	141.15	494.36	5.0569
8:26:09	1115.14	105	2072	438	1054	1149	227	11.88	2.02	0.36	9.71	10.44	1.53	139.38	495.18	5.0573
8:26:34	1115.30	103	2054	427	1018	1117	165	12.32	1.98	0.45	9.37	9.24	1.1	138.28	495.43	5.0577
8:26:10	1115.64	108	2018	434	981	1092	186	12.28	1.64	0.44	9.4	9.05	1.06	148.33	495.68	5.0578
8:26:18	1115.68	104	1990	432	956	1000	105	12.18	1.81	0.38	9.51	10.01	0.98	148.24	495.08	5.0581
8:26:22	1116.14	107	1982	442	940	1023	140	12.28	1.85	0.30	9.43	9.86	0.30	139.57	496.18	5.0586
8:26:28	1116.36	106	1995	439	955	1040	130	12.28	1.93	0.36	9.43	9.36	0.36	142.7	496.47	5.0588
8:26:34	1116.64	107	1992	444	938	1044	219	12.24	1.8	0.28	9.35	9.39	0.36	140.69	496.72	5.0589
8:26:40	1116.68	106	1998	446	929	1058	211	12.28	1.67	0.34	9.32	9.89	0.51	148.94	496.93	5.0592
8:26:48	1117.14	100	1990	436	968	1048	178	12.28	1.54	0.42	9.43	9.89	0.91	158.46	497.18	5.0597
8:26:51	1117.36	105	1984	434	949	1020	138	12.3	1.54	0.37	9.4	9.84	0.91	157.89	497.44	5.0599
8:26:57	1117.64	104	1985	433	948	1026	150	12.3	1.86	0.35	9.39	9.84	1.01	153.98	497.7	5.0600
8:27:03	1117.8	103	1987	427	936	1018	138	12.31	1.94	0.4	9.38	9.79	0.96	159.51	497.96	5.0601
8:27:08	1118.15	109	1958	434	912	988	174	12.31	1.92	0.36	9.38	9.79	0.98	152.58	498.2	5.0602
8:27:14	1118.4	108	1910	448	981	971	132	12.31	1.88	0.38	9.34	9.36	0.96	163.81	498.44	5.0603
8:27:20	1118.66	105	1829	437	903	1040	211	12.26	1.9	0.39	9.33	9.86	0.98	153.19	498.72	5.0604
8:27:27	1118.8	107	1957	442	949	1018	170	12.22	1.88	0.38	9.47	9.89	1.01	138.98	498.94	5.0606
8:27:32	1119.18	104	1977	432	945	1004	219	12.24	1.84	0.42	9.40	9.89	0.93	161.78	499.2	5.0607
8:27:38	1119.4	108	1943	436	917	993	134	12.18	1.88	0.37	9.33	9.83	0.86	135.48	499.44	5.0608
8:27:48	1119.66	104	1987	431	927	1018	190	12.17	1.93	0.4	9.52	9.91	0.88	163.11	499.68	5.0609
8:27:51	1119.8	108	1980	439	935	1024	238	12.16	1.87	0.38	9.53	10.17	1.02	143.29	499.94	5.0613
8:27:58	1120.15	105	1950	437	904	1034	162	12.18	1.87	0.38	9.53	9.96	0.91	135.81	500.21	5.0615
8:28:04	1120.4	107	1954	441	917	993	122	12.18	1.89	0.33	9.34	9.93	0.84	148.88	500.46	5.0616
8:28:11	1120.68	108	1941	440	894	1020	207	12.13	1.89	0.37	9.58	9.88	0.89	131.68	500.7	5.0618
8:28:17	1120.8	107	1940	441	934	1022	207	12.13	1.9	0.38	9.55	9.66	0.81	138.14	500.96	5.0621
8:28:24	1121.15	106	2030	436	1012	1117	237	12.21	1.92	0.43	9.48	10.19	1.09	140.74	501.2	5.0624
8:28:30	1121.41	104	2059	431	1035	1101	146	12.18	1.94	0.43	9.53	9.92	0.93	135.18	501.46	5.0624
8:28:38	1121.66	104	2079	432	1044	1101	110	12.16	1.91	0.37	9.53	10.03	1.08	151.71	501.7	5.0624
8:28:43	1121.81	106	2076	435	1044	1113	140	12.14	1.84	0.41	9.54	9.89	0.88	133.53	501.96	5.0628
8:28:50	1122.16	104	2073	431	1048	1121	182	12.12	1.82	0.44	9.57	10.08	0.88	137.87	502.2	5.0618
8:28:58	1122.41	104	2081	431	1032	1104	189	12.13	1.84	0.43	9.88	10.03	1.05	143.64	502.46	5.0623
8:29:05	1122.66	104	2052	431	1022	1104	148	12.13	1.8	0.36	9.34	10.03	0.85	131.1	502.7	5.0623
8:29:09	1122.91	103	2022	427	995	1084	203	12.12	1.91	0.37	9.36	9.86	0.81	138.83	502.96	5.0617
8:29:18	1123.18	106	2019	436	988	1088	182	12.18	1.89	0.38	9.57	9.91	0.81	134.83	503.21	5.0619
8:29:22	1123.41	104	2060	430	1029	1109	170	12.1	1.83	0.43	9.59	10.03	0.99	135.88	503.47	5.0617
8:29:29	1123.68	106	2045	435	1023	1141	225	12.14	1.89	0.37	9.59	9.98	0.89	137.84	503.73	5.0617

DOE high power mortar test Amaco Caloosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOR	PEAK	DELT	WOB	PEAK	DELT	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lb	ft-lb	ft-lb	KIPS	ft-lb	ft-lb	KIPS	KIPS	KIPS	FT/HR	CrBit	CrBit
9:29:30	1120.91	106	1933	442	953	1085	188	12.17	1.65	0.48	9.81	10.65	1.60	127.53	501.95	5:1134
9:29:42	1124.31	106	1934	439	983	1086	231	12.14	1.67	0.31	9.54	9.91	0.84	143.53	504.33	5:1161
9:29:48	1124.41	106	1931	438	952	1075	263	12.11	1.65	0.32	9.37	9.59	0.89	139.89	504.47	5:1182
9:29:55	1124.58	105	1932	437	952	1056	211	12.14	1.65	0.20	9.54	9.91	0.84	142.29	504.7	5:1199
9:30:01	1124.51	108	1971	445	939	956	138	12.15	1.8	0.24	9.51	9.83	0.69	147.08	504.36	5:1218
9:30:07	1125.36	107	1938	443	949	1050	139	12.2	1.67	0.17	9.48	9.91	0.80	133.27	505.2	5:1230
9:30:13	1125.41	106	1938	448	937	1056	319	12.18	1.67	0.31	9.5	9.86	0.85	130.17	505.47	5:125
9:30:20	1125.58	107	1977	443	903	959	134	12.17	1.69	0.3	9.51	9.91	0.86	142.75	505.32	5:1267
9:30:28	1125.93	106	1997	436	961	1129	338	12.18	1.69	0.35	9.56	9.91	0.91	138.14	505.68	5:1283
9:30:35	1126.37	106	2022	438	983	1143	276	12.37	1.65	0.31	9.31	9.96	2.17	142.84	506.21	5:1302
9:30:46	1126.54	106	1969	433	744	1085	749	17.01	1.64	0.25	9.19	9.44	0.22	162.62	506.5	5:132
9:30:53	1126.72	106	1937	432	983	1063	152	12.57	1.57	0.31	9.66	9.07	0.75	146.95	506.85	5:1337
9:30:58	1127.08	106	2001	435	946	1068	347	12.58	1.84	0.29	9.66	9	0.84	170.5	507.1	5:1352
9:31:03	1127.3	106	1915	437	879	971	189	12.82	1.68	0.38	9.4	9.66	0.81	167.45	507.36	5:1368
9:31:14	1127.55	107	1926	441	775	983	340	11.64	1.67	0.32	9.26	9.84	1.22	85.35	507.8	5:1385
9:31:27	1127.7	106	1831	438	814	1010	381	11.89	1.88	0.33	9.34	9.72	0.72	70.32	507.84	5:1402
9:31:37	1128.05	106	1894	436	456	1095	512	11.77	1.25	0.43	9.46	9.75	0.78	60.81	508.08	5:1418
9:31:45	1128.3	107	1881	440	326	1004	333	11.85	1.98	0.49	9.37	9.75	0.83	110.48	508.35	5:1438
9:31:50	1128.35	108	1754	444	719	850	207	11.99	1.85	0.22	9.44	9.98	0.38	80.65	508.38	5:1455
9:31:59	1128.9	107	1794	444	792	871	312	11.77	1.87	0.31	9.45	9.98	0.91	86.67	508.64	5:1462
9:32:10	1129.05	106	1842	438	824	965	251	11.87	1.98	0.3	9.36	9.74	0.74	98.08	509.11	5:1478
9:32:26	1129.3	106	1823	439	799	955	299	11.85	1.85	0.33	9.35	9.69	0.74	102.93	509.34	5:1484
9:32:37	1129.55	106	1843	436	846	988	284	11.91	1.87	0.34	9.32	9.69	0.88	102.50	509.59	5:1497
9:32:45	1129.8	105	1805	434	851	1020	240	12.04	1.87	0.30	9.19	9.62	0.89	117.58	509.86	5:1508
9:32:55	1130.25	107	1838	445	845	987	282	11.73	1.89	0.31	9.5	9.98	1.2	87.55	510.08	5:1529
9:33:11	1130.3	106	1844	439	826	1032	482	11.58	1.89	0.42	9.64	10.13	0.93	87.63	510.35	5:1541
9:33:30	1130.58	107	1845	441	819	1085	489	11.5	1.93	0.52	9.73	10.15	0.93	47.92	510.59	5:1573
9:33:41	1130.8	106	1845	438	894	1141	495	11.72	1.92	0.49	9.51	10.31	1.17	70.82	510.85	5:1603
9:33:50	1131.35	105	1935	433	880	1082	324	11.93	1.93	0.41	9.29	9.79	1.17	107.46	511.09	5:163
9:33:57	1131.3	105	1954	433	870	1182	401	12.04	1.94	0.44	9.18	9.76	1.40	121.08	511.35	5:165
9:34:03	1131.55	105	2025	427	942	1073	181	12.38	1.94	0.45	8.95	9.41	1.03	109.26	511.61	5:1664
9:34:10	1131.5	106	1971	437	946	1050	315	12.07	1.99	0.36	9.15	9.62	0.99	120.63	511.86	5:1687
9:34:17	1132.05	104	1899	432	827	1081	278	12.36	1.97	0.23	9.15	9.58	0.89	130.81	512.12	5:1704
9:34:25	1132.3	105	1898	434	983	1073	208	12.35	1.97	0.49	9.08	9.55	1.18	129.35	512.35	5:1723
9:34:32	1132.55	106	1867	438	914	1073	285	12.04	1.99	0.35	9.18	9.9	1.08	105.95	512.61	5:1745
9:34:41	1132.8	106	1831	438	885	1044	284	11.91	1.89	0.35	9.32	9.77	1.03	101.86	512.86	5:1767
9:34:57	1133.58	107	1915	442	840	1020	247	11.72	1.86	0.38	9.51	9.63	0.66	79.53	513.11	5:1803

Well No. 23
 Date: 2/26/88
 Starting Depth = 1091.27
 Ending Depth = 1082.14
 Total Depth Drilled = 359.87
 Hours Cr. Bit = 8.23
 Average ROP = 53.72
 Drilling (ft) = 1071.56

Bit Type = Walker-McDermid MP68H
 Bit Size = 4.75
 Bit Nozzles = 8, 9, 12, 12
 Mud Type = Water Based
 Mud Weight (lb/gal) = 9.60
 Pipe (ft) = 963.63
 Collar (ft) = 408.60

DOE high power mortar test Amaco Catoosa Test Site

TIME HH:MM:SS	BIT DEPTH FEET	FLOW GPM	PRESS PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELTA ft-lbs	HOBX LOAD KIPS	PEAK KIPS	DELTA KIPS	WOB KIPS	PEAK KIPS	DELTA KIPS	RDP FT/HR	Feet On Bit	Hours On Bit
8:40:05	1133.31	307	1867	441	822	1038	377	11.81	1.89	0.34	9.84	9.86	0.01	71.64	513.36	5.2636
8:40:19	1133.56	307	1868	441	836	1036	366	11.81	1.85	0.55	9.81	9.85	0.06	63.31	513.61	5.2676
8:40:29	1133.81	307	1881	442	810	978	312	11.79	1.84	0.32	9.47	9.81	0.01	61.35	513.86	5.2702
8:40:37	1134.06	304	1834	432	769	919	243	11.9	1.32	0.29	9.32	9.76	0.89	107.67	514.11	5.2728
8:40:46	1134.31	307	1819	440	800	864	170	11.9	1.84	0.25	9.33	9.98	0.81	102.49	514.37	5.2751
8:40:54	1134.56	308	1811	438	780	894	239	11.87	1.80	0.3	9.35	9.74	0.81	107.62	514.62	5.2774
8:41:03	1134.81	306	1822	430	803	874	198	11.8	1.83	0.3	9.32	9.73	0.79	106.29	514.86	5.2798
8:41:13	1135.06	307	1886	443	821	840	180	11.87	1.83	0.37	9.33	9.87	0.78	114.91	515.1	5.2822
8:41:19	1135.31	308	1833	439	789	880	174	11.83	1.87	0.28	9.29	9.89	0.89	107.46	515.36	5.2845
8:41:28	1135.56	307	1813	441	785	870	158	11.87	1.82	0.24	9.26	9.67	0.74	103.44	515.61	5.2869
8:41:37	1135.81	307	1822	442	781	875	178	11.84	1.80	0.37	9.36	9.94	0.91	100	515.86	5.2891
8:41:46	1136.06	307	1831	440	764	884	227	11.80	1.87	0.31	9.36	9.74	0.79	96.32	516.11	5.2912
8:41:55	1136.31	308	1804	449	763	863	180	11.82	1.85	0.26	9.4	9.74	0.61	105.27	516.36	5.2933
8:42:04	1136.56	307	1800	441	773	862	203	11.85	1.84	0.26	9.37	9.60	0.60	97.73	516.61	5.2956
8:42:13	1136.81	308	1809	438	764	866	247	11.80	1.86	0.3	9.58	9.74	0.79	94.86	516.86	5.2984
8:42:23	1137.06	308	1804	449	745	829	198	11.79	1.86	0.33	9.42	9.79	0.74	96.73	517.11	5.243
8:42:32	1137.31	307	1880	443	758	876	238	11.83	1.85	0.32	9.38	9.72	0.74	93.69	517.36	5.2446
8:42:41	1137.56	308	1837	439	770	806	259	11.88	1.85	0.28	9.36	9.69	0.74	106.54	517.6	5.2472
8:42:49	1137.81	308	1851	439	750	800	194	11.91	1.85	0.38	9.3	9.87	0.81	109.79	517.85	5.2495
8:42:58	1138.06	308	1847	435	804	873	275	11.84	1.86	0.39	9.28	9.66	0.80	111.25	518.1	5.2517
8:43:08	1138.31	307	1823	441	775	850	130	11.89	1.84	0.27	9.35	9.69	0.80	111.91	518.37	5.2543
8:43:16	1138.56	308	1829	437	779	882	166	11.9	1.80	0.28	9.32	9.67	0.77	100.2	518.6	5.2563
8:43:26	1138.81	307	1829	443	776	842	170	11.84	1.83	0.37	9.35	9.88	0.89	107.72	518.86	5.2589
8:43:34	1139.07	307	1782	441	719	802	268	11.80	1.84	0.37	9.33	9.91	0.89	81.75	519.13	5.2612
8:43:47	1139.32	308	1772	443	715	813	220	11.83	1.84	0.31	9.55	9.66	0.64	78.58	519.38	5.2635
8:44:01	1139.57	308	1819	448	763	1193	696	11.91	1.8	0.30	9.8	10.03	1.29	64.63	519.61	5.2652
8:44:07	1139.82	304	2087	430	7019	1192	395	12.21	1.54	0.81	9.01	9.53	1.00	198.46	519.87	5.2701
8:44:13	1140.07	304	2034	430	7836	1180	243	12.38	1.94	0.41	9.04	9.6	1.03	142.62	520.14	5.2723
8:44:20	1140.32	304	2132	428	1077	1160	174	12.10	1.94	0.37	9.03	9.63	1.03	125.03	520.38	5.2747
8:44:27	1140.57	301	2148	418	1055	1190	211	12.2	2.02	0.64	9.06	9.72	1.29	140.58	520.63	5.2794
8:44:32	1140.82	306	2146	439	1037	1173	260	12.31	2.05	0.64	9	9.89	1.20	182.38	520.89	5.2831
8:44:38	1141.07	303	2049	434	987	1064	184	12.24	1.82	0.44	9	9.93	1.1	139.33	521.11	5.2838
8:44:44	1141.32	302	2009	437	935	1044	267	12.38	1.9	0.4	8.83	9.24	0.89	178.45	521.36	5.2873
8:44:51	1141.57	302	2110	428	1084	1096	267	12.48	1.96	0.46	9.03	9.0	1.1	130.25	521.61	5.2923
8:44:57	1141.82	302	2143	427	1098	1038	258	12.17	1.98	0.54	9.0	9.0	1.13	140.66	521.86	5.2985
8:45:03	1142.07	301	2136	418	1073	1176	291	12.25	2.03	0.59	8.96	9.48	1.03	198.11	522.12	5.2987
8:45:18	1142.32	302	2131	424	1085	1214	299	12.15	1.88	0.64	9.03	9.8	1.2	129.5	522.4	5.2987

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TOURQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Moist
HH:MM:SS	FEET	GPM	PSI	RPM	%-in	ft-lbs	ft-sec	TOPS	%	%	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
9:40:10	1142.57	103	2130	433	1008	1549	320	12.32	8.1	0.70	8.99	8.57	1.47	167.81	522.0	5.2901
9:40:23	1142.92	104	2114	423	1080	1170	223	12.18	2.09	0.61	8.04	8.23	1.24	131.83	523.88	5.2921
9:40:26	1143.07	103	2122	425	1060	1202	271	12.25	2.73	0.63	8.97	8.52	1.33	159.27	525.12	5.2935
9:40:34	1143.32	103	2117	425	1055	1164	243	12.27	2.13	0.7	8.95	8.5	1.50	158.06	521.38	5.2953
9:40:40	1143.57	103	2040	433	9113	1109	211	12.33	1.01	0.56	8.89	8.65	1.29	150.93	523.52	5.297
9:40:46	1143.83	104	2063	432	1002	1141	243	12.33	2.09	0.59	8.89	8.83	1.15	160.18	523.9	5.2984
9:40:51	1144.08	109	2073	439	1020	1113	178	12.35	1.88	0.5	8.87	8.31	1.05	158	524.15	5.2998
9:40:57	1144.33	108	2117	430	1075	1263	337	12.39	2.02	0.63	8.94	8.5	1.24	147.01	524.28	5.3016
9:41:03	1144.58	104	2145	431	1115	1225	327	12.3	2.23	0.64	8.92	8.5	1.15	150.37	524.83	5.3033
9:41:10	1144.83	105	2070	430	989	1089	243	12.47	2.1	0.79	8.74	8.43	1.36	174.72	524.87	5.3047
9:41:15	1145.08	105	1975	433	864	973	195	12.54	1.85	0.44	8.67	8.34	1.32	196	525.15	5.3052
9:41:19	1145.33	105	1949	434	834	967	178	12.24	1.50	0.40	8.57	8.88	1.65	148.77	525.37	5.3079
9:41:28	1145.58	103	1947	444	953	1024	300	11.76	2.04	0.57	8.45	8.98	1.40	17.93	525.93	5.3106
9:41:41	1145.83	107	1948	443	886	929	306	11.84	2	0.3	8.57	10.03	0.26	78.8	525.88	5.3139
9:41:49	1146.08	109	2074	433	1034	1263	397	12.06	3.07	0.69	8.15	8.87	1.1	110.60	525.13	5.3159
9:41:56	1146.33	104	2043	432	973	1068	223	11.87	1.84	0.48	8.24	8.72	1.04	122.83	525.37	5.3183
9:42:05	1146.58	108	2031	436	958	1193	373	11.9	2.64	0.64	8.41	8.77	1.05	108.07	525.82	5.3205
9:42:14	1146.83	106	2003	434	958	1210	303	11.86	2.05	0.7	8.35	8.81	1.2	97.91	526.88	5.3231
9:42:20	1147.08	102	2134	423	1073	1195	235	12.21	2.13	0.81	8	8.55	1.13	148.97	527.12	5.3248
9:42:27	1147.33	104	2148	432	1070	1173	218	12.13	2.09	0.75	8.98	8.62	1.13	134.2	527.4	5.3264
9:42:34	1147.58	103	2170	427	1001	1251	316	12.09	2.58	1.05	8.18	8.72	1.17	160.34	527.63	5.3283
9:42:41	1147.84	103	2164	428	1067	1188	327	12.19	2.24	0.82	8.02	8.62	1.22	143.08	527.86	5.3302
9:42:48	1148.09	104	2152	432	1053	1210	380	12.1	2.35	1.08	8.11	8.62	1.05	129.15	528.14	5.3322
9:42:54	1148.34	104	2162	431	1033	1170	173	12.18	2.18	0.8	8.92	8.6	1.15	147.23	528.38	5.334
9:43:01	1148.59	104	2153	430	1092	1150	303	12.12	2.23	1.05	8.99	8.63	1.17	131.85	528.54	5.3368
9:43:07	1148.84	104	2171	431	1056	1251	274	12.19	2.22	0.9	8.68	8.63	1.08	136.83	528.59	5.3377
9:43:14	1149.09	103	2295	428	1138	1308	373	12.07	2.29	1.18	8.14	8.74	1.24	127.15	529.13	5.3387
9:43:21	1149.34	102	2236	425	1119	1250	270	12.17	2.31	1.18	8.04	8.6	1.58	139.38	529.38	5.3417
9:43:27	1149.59	105	2236	428	1123	1251	258	12.15	2.34	1.18	8.02	8.65	1.29	152.61	529.64	5.3434
9:43:34	1149.84	105	2348	437	1084	1190	320	12.16	2.26	1.15	8.05	8.68	1.32	127.61	529.88	5.3451
9:43:40	1150.09	105	2349	434	1072	1321	300	12.25	2.35	0.95	8.63	8.43	1.05	162.70	530.17	5.3469
9:43:47	1150.34	104	2114	431	1031	1180	300	12.39	2.04	0.81	9.10	8.69	1.17	138.78	530.4	5.3486
9:43:53	1150.59	109	1840	446	843	1050	273	11.87	1.83	0.58	9.34	8.88	1.1	100.63	530.64	5.3511
9:43:54	1150.64	106	1854	428	824	897	308	11.9	1.83	0.43	8.41	8.51	1.31	98.67	530.8	5.3527
9:43:58	1151.08	107	1844	441	776	973	397	11.80	1.80	0.34	8.52	8.66	1.31	77.89	531.14	5.3569
9:43:58	1151.34	107	1795	441	737	887	438	11.58	1.89	0.33	8.63	8.61	0.79	75.11	531.4	5.358
9:43:58	1151.8	107	1782	440	730	889	417	11.52	1.85	0.28	8.68	8.15	0.91	68.21	531.69	5.3603

DOE high power mortar test Amaco Catoosa Test Site

TIME HH:MM:SS	SIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE N-lbs	PEAK ft-lbs	DELT Nlbs	HOOK LOAD KIPS	PEAK G's	DELTA G's	WOB KIPS	PEAK KIPS	DELTA KIPS	ROP FT/HR	Feet OnBit	Hours OnBit
9:50:08	1151.85	109	1742	447	884	894	419	11.44	1.89	0.28	9.76	10.2	0.96	45.88	831.86	5.3761
9:50:23	1152.1	109	1722	447	860	878	408	11.44	1.85	0.28	9.79	10.44	1.2	45.92	832.18	5.3789
9:50:48	1152.35	109	1716	446	862	910	399	11.44	1.88	0.31	9.76	10.98	0.72	46.80	832.50	5.3816
9:51:03	1152.6	109	1714	448	846	868	368	11.44	1.84	0.38	9.76	10.25	0.56	44.87	832.86	5.3842
9:51:28	1152.85	108	1717	447	853	947	478	11.4	1.85	0.34	9.6	10.35	0.98	38.51	832.89	5.3868
9:51:53	1153.1	108	1711	448	808	874	395	11.38	1.87	0.33	9.82	10.25	0.54	25.68	833.14	5.4007
9:52:18	1153.35	107	1723	441	874	866	401	11.44	1.79	0.33	9.78	10.25	1.89	48.01	833.39	5.4061
9:52:28	1153.6	108	1747	444	887	919	377	11.59	1.85	0.31	9.61	10.03	0.81	60.88	833.87	5.4102
9:52:52	1153.85	108	1854	448	820	828	385	11.36	1.87	0.3	9.84	10.32	1.95	37.87	833.88	5.4187
9:53:15	1154.1	109	1897	448	889	956	417	11.33	1.83	0.25	9.81	10.1	0.72	38.11	834.14	5.4238
9:53:34	1154.38	111	1749	487	878	900	389	11.48	1.84	0.25	9.72	10.2	0.91	37.2	834.4	5.4295
9:54:03	1154.6	108	1876	450	811	798	377	11.35	1.81	0.22	9.87	10.2	0.77	32.32	834.65	5.4353
9:54:21	1154.85	107	1737	440	719	1141	880	11.83	1.95	0.48	9.68	10.15	1.84	36.86	834.9	5.4417
9:54:26	1155.1	108	1871	436	913	1049	381	12	0.1	0.77	9.69	9.74	1.22	129.23	835.15	5.4437
9:54:48	1155.38	108	1728	444	881	987	654	11.4	1.81	0.4	9.79	10.28	1.68	44.1	835.41	5.4484
9:55:19	1155.68	107	1885	442	822	825	381	11.38	1.87	0.3	9.81	10.28	0.72	29.81	835.8	5.4577
9:55:42	1155.81	108	1849	444	823	833	381	11.38	1.81	0.34	9.81	10.22	1.17	36.89	835.88	5.468
9:55:56	1156.05	107	1877	441	851	885	389	11.3	1.88	0.28	9.88	10.58	0.80	58.97	836.11	5.4677
9:56:04	1156.31	107	1731	442	898	898	395	11.81	1.91	0.38	9.58	9.68	0.81	65.56	836.35	5.4719
9:56:27	1156.58	107	1718	442	878	882	341	11.46	1.92	0.47	9.74	10.15	1.05	50.17	836.61	5.4763
9:56:44	1156.81	108	1704	444	892	885	398	11.48	1.88	0.36	9.71	10.08	0.83	51.64	836.86	5.4812
9:56:57	1157.08	107	1887	443	858	889	384	11.58	1.93	0.28	9.81	10.01	0.91	68.79	837.11	5.4845
9:57:05	1157.31	107	1748	449	738	842	327	11.84	1.95	0.3	9.26	9.66	0.98	108.44	837.37	5.4872
9:57:14	1157.58	108	1789	448	738	860	284	11.9	1.88	0.3	9.72	9.93	0.93	107.91	837.61	5.4886
9:57:25	1157.81	108	1870	454	848	1129	382	11.79	2.40	1.8	9.41	10.53	1.89	33.56	837.86	5.4927
9:57:30	1158.08	106	2008	457	868	1139	1142	12.03	2.21	1.08	9.46	9.72	1.2	189.48	838.15	5.4941
10:00:31	1158.37	108	1858	448	820	1154	819	13.28	1.98	0.54	8.74	14	13.84	122.91	838.32	5.4983
10:02:51	1158.52	107	1782	444	868	887	638	11.7	1.96	0.49	10.49	12.04	3.23	45.18	838.57	5.4974
10:03:06	1158.77	108	1732	441	740	1059	469	11.89	1.93	0.48	10.51	10.84	0.79	81.8	838.84	5.5028
10:03:28	1159.02	107	1781	443	787	947	382	11.71	1.95	0.42	10.41	10.78	0.78	63.08	839.08	5.5063
10:03:38	1159.27	106	1790	438	796	1060	421	11.75	1.98	0.56	10.38	10.71	0.80	72.29	839.32	5.5088
10:03:45	1159.52	104	2083	439	1002	1243	468	12	3.12	2.76	10.12	11.15	1.88	64.78	839.58	5.5123
10:03:52	1159.77	105	2053	438	893	1222	438	12.12	3.28	2.84	10	11.37	2.32	128.13	839.82	5.5143
10:04:03	1160.02	108	1881	441	897	1320	653	11.78	2.86	0.75	10.98	10.64	1.03	76.8	840.07	5.5175
10:04:23	1160.27	107	1787	444	743	992	454	11.6	2.95	0.84	10.82	11.08	1.45	50.27	840.34	5.5227
10:04:37	1160.52	108	1781	440	782	1080	470	11.88	2.87	1.11	10.68	11.54	1.91	84.14	840.57	5.5277
10:04:49	1160.78	104	1880	438	945	1210	470	11.87	2.88	0.88	10.28	10.8	1.08	83.5	840.84	5.5311

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23	Dist: 32286																
Starting Depth =	1031.27	Bit Type =	Water McDaniel L&PM														
Ending Depth =	1043.14	Bit Size =	4.75														
Total Depth Drilled =	11.87	Bit Nozzles =	9, 9, 12, 12														
Hours On Bit =	6.88	Mud Type =	Water Based														
Average ROP =	53.72	Mud Weight (lb/gal) =	6.09														
Drilling (ft) =	1071.58	Pipe (ft) =	863.68	Collar (ft) =	408.08												

TIME	BIT	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAR	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HR:MM:SS	DEPTH FEET	QPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	LOAD KIPS	LOSS	LOSS	KIPS	KIPS	KIPS	FT/HR	On-Bit	On-Bit
10:04:58	1161.03	104	1820	432	1190	1287	271	12.24	2.14	3.76	6.88	10.44	1.86	123.73	541.67	5.5324
10:05:16	1161.29	105	1850	437	852	1302	640	14.19	3.94	4.72	7.93	6.79	3.76	24.36	541.33	5.5328
10:05:22	1161.53	106	1875	441	881	1052	300	15.25	2.72	2.3	7.06	6.31	2.18	74.41	541.67	5.5332
10:05:34	1161.78	108	1906	447	836	1039	373	14.85	2.55	1.91	7.25	6.04	1.0	73.32	541.82	5.5337
10:05:46	1162.03	109	1940	452	846	1039	405	14.84	2.81	2.81	7.27	7.92	1.41	76.26	542.08	5.5341
10:05:57	1162.28	108	1854	443	804	910	311	14.83	2.28	1.59	7.28	7.73	0.86	76.21	542.33	5.5345
10:06:09	1162.53	109	1840	480	813	919	190	14.83	2.18	1.12	7.25	7.8	1.03	76.41	542.58	5.5349
10:06:20	1162.78	108	1846	482	831	947	247	14.85	2.13	1	7.25	7.88	1.18	80.83	542.83	5.5353
10:06:30	1163.03	106	1828	441	834	947	243	14.87	2.29	1.34	7.23	7.71	1.08	87.13	543.08	5.5358
10:06:36	1163.28	109	1901	442	910	1004	319	15.03	2.15	1.07	7.08	7.68	1.05	87.33	543.33	5.5362
10:06:47	1163.51	108	1892	430	897	987	308	15.98	2	0.6	7.05	7.82	0.88	113.05	543.61	5.5366
10:06:54	1163.78	104	1886	435	852	957	168	15.13	1.68	0.47	6.98	7.47	0.99	124.25	543.83	5.5371
10:07:02	1164.03	107	1853	443	879	947	102	15.17	1.63	0.4	6.93	7.35	0.83	131.18	544.08	5.5375
10:07:08	1164.28	109	1837	442	846	806	154	15.19	1.03	0.41	6.91	7.28	0.86	130.97	544.34	5.5379
10:07:16	1164.51	107	1807	484	812	802	178	15.2	1.93	0.5	6.9	7.37	0.91	122.46	544.62	5.5384
10:07:23	1164.72	105	1808	440	803	888	170	15.21	1.69	0.43	6.89	7.32	0.89	133.31	544.88	5.5388
10:07:29	1165.04	108	1795	445	781	896	203	15.21	1.69	0.25	6.84	7.38	0.84	143.49	545.11	5.5393
10:07:38	1165.29	103	1800	440	819	808	196	15.3	1.88	0.41	6.81	7.18	0.89	132.44	545.36	5.5397
10:07:42	1165.54	109	1800	440	819	882	184	15.27	1.84	0.48	6.83	7.35	0.91	145	545.61	5.5402
10:07:49	1165.78	105	1812	439	808	915	170	15.27	1.95	0.4	6.83	7.25	0.89	129.01	545.83	5.5406
10:07:55	1166.04	109	1812	436	819	902	188	15.24	1.5	0.4	6.76	7.21	0.89	151.71	546.08	5.5411
10:08:01	1166.29	107	1795	432	789	880	174	15.27	1.9	0.37	6.88	7.03	0.89	145.82	546.33	5.5415
10:08:08	1166.54	107	1795	448	808	831	207	15.21	1.93	0.44	6.88	7.07	0.88	119.07	546.58	5.5420
10:08:15	1166.78	108	1820	441	818	894	162	15.27	1.96	0.3	6.84	7.32	1.01	148.9	546.83	5.5424
10:08:22	1167.04	107	1818	444	818	882	139	15.25	1.62	0.48	6.83	7.21	0.81	134.23	547.08	5.5429
10:08:29	1167.29	107	1811	445	785	894	182	15.22	1.84	0.44	6.82	7.44	1.06	130.75	547.34	5.5433
10:08:38	1167.54	107	1775	445	760	815	284	14.97	1.95	0.48	7.14	7.82	0.81	96.75	547.58	5.5437
10:08:46	1167.78	108	1817	440	787	802	194	15.28	1.85	0.45	7.02	7.4	0.84	108.78	547.84	5.5442
10:08:53	1168.04	108	1810	448	792	850	182	15.11	1.8	0.35	6.99	7.32	0.89	128.93	548.1	5.5446
10:08:59	1168.28	109	1830	442	835	905	168	15.25	1.98	0.3	6.92	7.3	0.84	121.58	548.36	5.5451
10:09:06	1168.54	107	1780	445	777	942	271	15.1	1.97	0.45	7	7.37	0.91	114.9	548.61	5.5455
10:09:14	1168.78	107	1810	440	778	902	203	15.24	1.99	0.51	6.77	7.38	0.96	157.66	548.88	5.5459
10:09:23	1169.03	119	1742	480	888	870	280	15.05	2.01	0.88	7.05	7.44	0.88	103.83	549.12	5.5464
10:09:34	1169.3	119	1685	480	844	860	385	14.77	1.84	0.48	7.03	7.73	1.08	75.84	549.38	5.5468
10:09:44	1169.59	111	1675	457	535	785	371	14.48	1.97	0.45	7.07	8.04	0.81	23.07	549.63	5.5473
10:09:54	1169.89	107	1820	443	831	853	14.39	1.84	0.48	0.71	6.97	8.07	0.85	17.01	549.89	5.5477
10:10:04	1170.17	107	1848	440	844	871	275	14.37	1.82	0.33	7.03	7.97	0.75	27.8	549.81	5.5477

DOE high power mortar test Amaco Catoosa Test Site

TIME	SIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	RICOM	PEAK	DELTA	WOR	PEAK	DELTA	POP	Feet	Hour
HH:MM:SS	FEET	BPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	Gr	Gr	KIPS	KIPS	KIPS	FT/HR	ONEL	Gr/ft
10:11:34	1170.95	107	1871	445	689	740	300	13.53	1.06	0.44	8.87	10.08	2.7	32.15	580.1	5.843
10:11:35	1170.3	107	1858	444	652	350	351	12.43	1.06	0.63	8.88	10.1	1.08	43.04	550.35	5.8407
10:12:08	1170.80	106	1897	438	873	787	254	12.50	1.87	0.47	9.58	9.89	0.79	70.79	350.81	5.8321
10:12:24	1170.8	105	1773	436	772	1044	527	12.50	2.01	0.58	9.58	10.03	1.03	67.54	550.88	5.8384
10:12:40	1171.05	108	1758	442	801	873	539	12.46	2.03	0.65	9.65	10.1	1.25	54.87	551.1	5.861
10:13:10	1171.39	108	1805	447	827	758	350	12.5	1.87	0.54	9.81	10.2	0.81	28.87	551.38	5.8603
10:13:33	1171.54	106	1728	448	738	1071	510	12.41	3.19	0.88	9.68	10.22	1.1	39.8	551.58	5.8756
10:13:50	1171.75	107	1788	432	745	908	363	12.48	2.8	1.73	9.84	10.29	1.44	68.28	551.84	5.8858
10:14:03	1172.05	108	1863	438	818	1408	758	12.75	2.54	1.73	9.35	10.96	2.02	72.02	552.1	5.8839
10:14:10	1172.3	105	2083	436	1031	1268	352	13.81	2.18	0.84	8.21	9.28	1.08	117.73	352.34	5.8858
10:14:18	1172.38	104	2110	432	1048	1182	388	13.4	2.39	0.61	8.7	9.24	1.22	138.57	352.8	5.8888
10:14:28	1172.8	108	2091	441	1005	1168	388	13.44	2.07	0.89	8.68	9.14	0.88	169.83	352.04	5.8906
10:14:37	1173.05	107	1872	444	818	978	216	13.88	1.82	0.44	8.47	9.38	0.96	181.75	353.08	5.8824
10:14:43	1173.3	107	1813	444	749	878	255	13.3	1.84	0.36	8.8	9.19	0.68	84.83	353.36	5.8988
10:14:52	1173.58	107	1767	445	728	831	303	13.28	1.84	0.46	8.84	9.31	1.01	57.88	353.8	5.8977
10:15:02	1173.8	107	1708	444	738	868	327	13.28	1.82	0.4	8.81	9.19	0.89	51.47	353.84	5.7056
10:15:12	1174.08	107	1773	445	798	821	158	13.38	1.83	0.41	8.81	9.24	0.81	89.38	354.11	5.7034
10:15:27	1174.3	106	1788	440	761	802	258	13.83	1.84	0.44	8.78	9.22	0.88	68.41	354.34	5.7106
10:15:37	1174.58	107	1828	443	788	846	358	13.38	1.88	0.48	8.71	9.18	0.93	88.28	354.8	5.7088
10:15:38	1174.8	107	1848	445	758	880	211	13.2	1.9	0.42	8.7	9.14	1.01	70.7	354.84	5.7106
10:15:46	1175.08	107	1828	444	764	850	114	13.38	1.81	0.44	8.58	9.05	0.91	127.38	355.08	5.7126
10:15:54	1175.3	106	1848	445	828	818	188	13.38	1.89	0.52	8.68	9	0.95	118.84	355.35	5.7188
10:16:07	1175.58	106	1848	439	817	866	178	13.64	1.83	0.38	8.67	9.02	0.81	132.46	355.88	5.7188
10:16:13	1175.8	107	1814	438	788	884	158	13.82	1.87	0.48	8.78	9.17	0.86	93.08	355.86	5.7198
10:16:23	1176.04	107	1732	448	753	887	458	13.18	1.84	0.41	8.81	9.41	1.32	75.74	356.08	5.7238
10:16:38	1176.3	107	1737	444	862	888	388	13	1.88	0.45	8.65	9.05	1.37	67.4	356.38	5.7272
10:17:08	1176.55	108	1858	437	831	842	389	12.87	1.84	0.44	8.23	9.07	0.74	31.80	356.62	5.7348
10:17:38	1176.8	107	1843	443	821	842	348	12.64	1.84	0.41	8.25	9.82	0.84	31.84	356.85	5.7328
10:18:08	1177.08	108	1818	448	833	789	316	12.8	1.84	0.5	8.28	9.88	0.88	25.19	357.03	5.7313
10:18:35	1177.16	107	1810	443	823	799	283	12.81	1.88	0.48	8.38	9.67	0.74	24.49	357.25	5.7388
10:18:54	1177.34	107	1718	448	730	1039	472	12.88	2.08	0.58	8.1	9.67	1.32	47.34	357.6	5.7847
10:19:13	1177.68	108	1888	448	841	888	488	12.84	1.84	0.42	8.18	9.8	1.12	46.78	357.74	5.7763
10:19:23	1177.84	108	1778	437	802	1089	591	13.14	1.88	0.44	8.88	9.85	1.38	81.43	358.01	5.7742
10:19:34	1178.3	104	1862	438	838	1018	168	13.84	1.88	0.43	8.48	9.88	0.88	131.38	358.27	5.7762
10:19:38	1178.45	106	1854	438	818	1082	218	13.8	1.81	0.38	8.29	9.70	1.01	104.84	358.51	5.7778
10:19:48	1178.7	105	1841	437	818	1088	243	18.77	1.88	0.48	8.38	9.74	0.81	135.73	358.75	5.7783
10:19:53	1178.88	108	1904	440	874	868	180	13.97	1.88	0.50	8.43	9.88	1.01	138.74	359	5.7813

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK LOAD	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	GS	GS	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
10:20:00	1178.2	107	1888	443	856	1004	260	13.61	1.93	0.39	8.48	8.88	0.88	137.29	558.24	5.7893
10:20:07	1178.48	107	1881	448	858	847	251	13.5	1.92	0.41	8.58	8.92	0.83	122.70	558.3	5.7893
10:20:17	1179.7	107	1838	445	816	831	247	13.38	1.91	0.43	8.75	9.17	0.91	90.88	558.74	5.7878
10:20:28	1178.95	107	1858	444	813	879	292	13.32	1.93	0.58	8.77	9.17	0.79	103.41	560.03	5.7895
10:20:36	1180.2	108	1898	442	832	947	215	13.33	2.05	0.58	8.78	9.14	0.91	84.71	560.25	5.7881
10:20:43	1180.48	108	1877	441	854	871	190	13.32	1.89	0.37	8.88	8.97	0.79	118.34	560.61	5.7881
10:20:53	1180.7	106	1852	440	829	885	146	13.28	1.98	0.41	8.8	9.14	0.74	93.88	560.74	5.7878
10:21:03	1180.98	107	1885	440	884	1028	298	13.34	1.94	0.44	8.75	9.1	0.88	88.52	561.01	5.8035
10:21:08	1181.2	108	1898	438	938	1018	186	13.85	2.02	0.64	8.48	8.88	0.88	144.92	561.26	5.8028
10:21:18	1181.48	108	1814	440	888	975	198	13.84	1.94	0.48	8.48	8.88	0.84	128.82	561.52	5.8042
10:21:28	1181.71	108	1906	438	885	883	170	13.83	1.93	0.41	8.48	8.88	0.84	140.8	561.78	5.8038
10:21:29	1181.96	107	1903	444	880	1004	217	13.85	1.93	0.33	8.44	8.8	0.88	141.31	562	5.8038
10:21:38	1182.21	107	1888	443	827	869	289	13.48	1.8	0.31	8.61	8.88	0.81	130.18	562.25	5.81
10:21:42	1182.48	106	1838	440	823	849	182	13.85	1.87	0.32	8.58	8.9	0.81	130.91	562.41	5.812
10:21:56	1182.71	107	1832	443	815	882	170	13.58	1.91	0.33	8.58	8.98	0.84	121.08	562.79	5.814
10:21:57	1182.98	107	1883	444	838	888	188	13.82	1.9	0.32	8.47	8.98	0.83	143.09	563.01	5.8137
10:22:03	1183.21	107	1884	440	880	983	182	13.82	1.88	0.31	8.48	8.98	0.81	135.88	563.25	5.8134
10:22:10	1183.48	108	1878	438	887	1058	258	13.88	1.88	0.33	8.51	8.88	0.81	127.2	563.5	5.8184
10:22:17	1183.71	108	1887	442	902	1024	288	13.97	1.98	0.38	8.53	8.9	0.76	138.1	563.79	5.8214
10:22:24	1183.98	108	1848	438	904	1048	211	13.82	1.98	0.41	8.47	8.98	0.86	125.98	564	5.8238
10:22:38	1184.21	104	1832	438	813	1024	288	13.7	1.85	0.29	8.58	8.81	0.88	152.81	564.28	5.8248
10:22:38	1184.48	108	1892	440	874	1054	271	13.89	1.9	0.4	8.48	8.83	0.81	138.08	564.5	5.8288
10:22:43	1184.71	104	1808	438	807	883	148	13.66	1.8	0.38	8.43	8.8	0.88	138.83	564.75	5.8288
10:22:48	1184.98	107	1812	442	888	887	188	13.7	1.88	0.4	8.38	8.71	0.87	154.11	565.03	5.8303
10:22:58	1185.21	108	1822	441	802	880	118	13.71	1.84	0.48	8.38	8.78	0.84	141.82	565.28	5.831
10:23:02	1185.48	108	1814	437	808	888	174	13.72	1.8	0.37	8.37	8.74	0.78	148.84	565.53	5.8338
10:23:08	1185.71	108	1887	438	828	1024	194	13.88	1.9	0.34	8.42	8.88	0.84	138.83	565.78	5.8358
10:23:13	1185.98	106	1814	441	885	1044	278	13.87	1.88	0.36	8.42	8.88	0.88	138.18	566.01	5.8375
10:23:23	1186.22	108	1888	448	885	978	120	13.71	1.9	0.4	8.37	8.78	0.84	180.82	566.27	5.8388
10:23:28	1186.47	106	1884	440	881	843	170	13.82	1.88	0.37	8.47	8.83	0.77	124.18	566.54	5.8408
10:23:34	1186.72	108	1888	438	887	1088	340	13.7	1.81	0.38	8.38	8.8	0.13	148.18	566.77	5.8428
10:23:48	1186.97	108	1887	438	841	881	154	13.88	1.88	0.34	8.4	8.74	0.78	142.7	567.01	5.8446
10:23:47	1187.22	107	1871	438	847	888	203	13.78	1.88	0.43	8.38	8.74	0.88	145.75	567.27	5.8488
10:23:52	1187.47	106	1888	438	845	883	138	13.8	1.86	0.34	8.38	8.81	0.81	155.88	567.51	5.8478
10:24:03	1187.72	106	1882	441	822	1180	281	13.28	1.93	0.4	8.83	9.21	1.22	88.89	567.78	5.8501
10:24:10	1187.97	108	1811	438	885	875	211	13.45	1.93	0.42	8.84	9.14	0.88	118.84	568.01	5.8528
10:24:24	1188.22	108	1853	441	831	1052	428	13.11	1.94	0.44	8.87	9.42	0.98	88.84	568.28	5.8584

DOE high power mortar test Amaco Catosa Test Site

TIME	DEPTH FEET	FLYING WEIGHT LB	PRESS PSI	SPEED RPM	TORQUE FT-LBS	PEAK RPM	PEAK FT-LBS	LOAD LB	PEAK G'S	DELTA G'S	VOIB NIPS	PEAK RPM	DELTA RPM	HOP FT	FUEL GALL	HOURS
10:24:32	1186.22	106	1863	439	930	1339	263	13.48	2.02	0.86	9.55	9.55	1.00	167.02	687.93	5.322
10:24:34	1186.72	106	1844	442	913	1322	243	13.48	1.91	0.41	8.66	9.11	1.17	137.74	688.77	5.3617
10:24:32	1186.67	108	1895	442	951	1340	464	13.1	1.61	0.41	8.98	9.39	0.84	117.23	690.05	5.3834
10:24:27	1180.16	118	1685	434	828	947	458	12.78	1.03	0.48	8.38	9.72	0.76	81.97	693.2	5.3727
10:24:32	1180.41	117	1727	446	713	963	470	12.63	1.97	0.48	8.35	9.93	0.68	38.34	693.48	5.381
10:21:20	1180.83	106	1844	439	637	915	454	13.03	1.96	0.48	8.57	10.17	0.98	38.05	693.98	5.4078
10:24:40	1180	106	1681	439	690	1024	597	11.81	1.06	0.26	8.95	10.16	0.66	23.48	695.65	5.3665
10:24:40	1180.29	106	1815	434	847	1180	638	11.81	1.98	0.54	10.74	11.83	2.13	51.24	696.31	5.4165
10:24:42	1180.6	106	1890.6	432	1107	1236	435	10.7	2.8	0.79	10.97	11.97	2.25	8.77	697.58	5.4128
10:24:39	1180.75	104	2182	429	1038	1281	688	10.79	3.04	2.94	10.87	12.69	4.02	163.98	698.36	5.4145
10:24:34	1191.01	104	2023	430	1036	1221	597	12.3	3.76	3.24	8.31	12.54	0.94	93.66	699.66	5.4178
10:24:40	1191.23	108	1921	437	1106	1329	713	14.18	3.97	3.90	7.37	19.13	9.37	78.87	697.5	5.3913
10:24:37	1191.76	106	1948	437	992	1092	456	14.35	2.14	2.06	7.17	19.02	4.21	28.33	699.81	5.3833
10:24:45	1191.21	106	1973	436	982	1117	590	14.47	2.73	2.09	6.61	19.82	2.56	163.98	699.92	5.3844
10:24:37	1192.01	109	1896	430	546	1093	371	14.66	2.10	0.68	6.61	19.64	1.24	147.3	697.38	5.3881
10:23:57	1192.08	107	1984	439	990	1067	738	14.84	2.91	0.84	8.98	7.37	1.61	163.41	692.31	5.3568
10:24:03	1192.61	102	1885	437	895	1038	426	14.94	1.0	0.43	6.62	7.35	1.62	184.91	692.57	5.3815
10:24:10	1192.78	109	1893	439	747	985	318	14.93	1.96	0.68	7.18	7.46	1.5	148.7	692.81	5.3831
10:23:57	1193.01	106	1958	443	638	982	433	13.52	1.25	0.81	7.73	6.38	0.05	33.31	693.16	5.3907
10:23:58	1193.58	107	1871	444	672	937	838	13.57	1.98	0.54	7.61	8.11	0.67	6.57	693.5	5.3467
10:23:14	1193.71	108	1704	444	711	971	482	14.08	1.93	0.67	7.53	8	0.79	6.57	693.8	5.3951
10:23:54	1193.78	107	1873	440	893	918	482	13.58	1.98	0.58	7.68	8	0.77	24.08	693.8	5.3865
10:24:51	1194.01	107	1673	441	677	931	402	13.58	1.94	0.49	7.58	7.37	0.69	59.77	694.08	5.3913
10:23:18	1194.26	106	1644	443	638	986	421	13.3	1.94	0.51	7.73	8.04	0.6	38.64	694.3	5.3986
10:24:44	1194.56	108	1754	443	648	831	386	13.78	1.93	0.46	7.91	8.78	2.99	38.44	694.58	5.4053
10:24:52	1194.78	108	1721	436	782	838	372	12.51	2	0.88	8.68	10.03	0.73	37.81	694.81	5.3973
10:24:15	1195.02	107	1758	440	733	818	306	11.61	1.94	0.85	8.75	9.03	0.78	50.27	695.07	5.39845
10:24:32	1195.27	107	1753	442	749	856	312	11.89	1.97	0.8	8.77	10.1	2.74	42.61	695.32	5.3983
10:24:57	1195.52	107	1751	441	648	828	267	12.03	1.95	0.66	8.66	9.28	0.77	61.67	695.57	5.39234
10:27:04	1195.77	107	1738	440	633	843	318	11.3	1.98	0.81	8.76	10.25	1.01	50.77	695.81	5.3938
10:27:13	1196.02	105	1878	438	1611	1091	377	12.39	2.13	0.75	9.23	0.98	1.39	159.52	696.06	5.3938
10:27:20	1196.27	109	1646	436	872	1046	365	12.46	1.97	0.51	9.3	9.93	1.43	35.77	696.31	5.4038
10:27:54	1196.52	108	1783	444	758	923	318	11.96	1.92	0.68	9.69	10.48	1.1	84.57	696.56	5.4068
10:27:36	1196.77	106	1698	439	923	1036	638	12.19	1.94	0.68	9.47	9.93	1.22	76.54	696.81	5.4087
10:27:58	1197.02	109	1687	437	1063	1179	207	13.41	3.97	0.78	9.25	9.73	0.68	135.33	697.02	5.4113
10:28:05	1197.27	106	1658	438	866	1063	251	12.15	2.35	2.99	9.51	1.38	0.54	86.21	697.31	5.4148
10:28:12	1197.52	108	1821	438	831	873	373	12.27	2.86	3.03	9.28	12.3	3.17	61.3	697.8	5.4162

Motor Type = Walker-Scottwood-Bush
 Motor Size = 4.75
 Motor Voltage = 5.9, 12, 12
 Motor Speed = 1800
 Motor Weight (lb) = 400
 Paper # = 592.95
 Motor # = 48016
 Motor # = 592.95

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23		Date: 2/28/98															
Starting Depth =		1051.27		Bit Type =		Weiler McDonald MP65H											
Ending Depth =		1362.14		Bit Size =		4.75											
Total Depth Drilled =		310.87		Bit Nozzles =		5, 8, 12, 12											
Hours On Bit =		6.53		Mud Type =		Water Based											
Average ROP =		49.72		Mud Weight (lb/gal) =		8.00											
Drilling dia =		1074.30		Pipe (in) =		603.65		Collar (in) =		400.40							
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours	
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	ft-lbs	ft-lbs	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit	
10:38:47	1197.93	108	1823	449	489	892	389	17.8	4.54	3.92	2.82	10.48	9.53	13.34	577.85	6.0368	
10:39:15	1197.98	108	1819	438	476	882	381	14.35	2.15	3.94	7.29	8.19	3.97	33.2	577.85	6.0334	
10:39:51	1198.13	108	1800	444	520	934	448	15.84	3.85	4.2	8	10.72	8.95	33.88	578.18	6.0448	
10:40:11	1198.32	108	1854	447	568	935	450	16.08	2.09	5.74	4.87	5.55	1.38	22.71	578.37	6.0501	
10:40:41	1198.54	108	1876	440	589	983	484	16.45	1.99	6.68	5.18	6.81	0.41	26.34	578.59	6.0584	
10:41:11	1198.74	108	1885	448	589	839	422	16.46	2.1	6.76	5.17	5.48	0.62	24.87	578.78	6.0667	
10:41:41	1198.96	108	1888	445	588	871	498	16.46	2.12	6.77	5.18	5.65	0.14	25.37	579	6.0751	
10:42:11	1199.18	108	1897	447	587	893	393	16.46	2.07	6.8	5.18	5.88	0.81	27.36	579.28	6.0836	
10:42:49	1199.43	109	1829	447	612	744	494	16.63	2.08	6.83	5.36	5.48	0.62	32.63	579.48	6.0911	
10:43:24	1199.68	107	1705	442	735	967	382	16.42	2.03	6.99	5.2	6.67	2.39	34.66	579.73	6.0984	
10:43:53	1199.94	104	1899	439	1346	1355	344	13.6	2.07	6.71	8.05	9.5	3.67	104.3	580.04	6.106	
10:43:59	1200.19	104	2152	429	1140	1251	291	11.74	1.85	6.88	9.61	10.68	1.7	182.28	580.23	6.1084	
10:43:14	1200.44	104	2165	429	1073	1202	281	11.42	1.98	6.96	10.23	10.75	1.88	186.82	580.5	6.1151	
10:43:20	1200.59	105	2019	435	989	1081	182	11.54	2.03	6.88	10.11	10.6	1.59	184.74	580.73	6.1226	
10:43:25	1200.84	107	2018	449	1017	1097	182	11.55	2.03	6.95	10.1	10.56	0.98	178.78	580.98	6.1304	
10:43:32	1201.18	104	2118	429	1188	1380	389	11.82	2.44	7.23	10.33	10.82	1.33	124.14	581.23	6.138	
10:43:36	1201.34	103	2154	428	1508	1198	373	11.82	2.05	6.8	10.54	10.85	1.2	218.31	581.5	6.1451	
10:43:48	1201.68	103	2118	438	1448	2203	1471	11.82	2.14	7.83	10.88	11.85	2.05	93.18	581.74	6.1527	
10:43:54	1201.84	103	2237	427	1393	2582	2013	13.74	3.48	7.13	7.91	11.25	6.76	114.4	581.99	6.1612	
10:44:05	1202.18	108	1818	445	904	931	428	15.46	2.16	6.78	5.37	7.96	4.74	61.0	582.24	6.1687	
10:44:14	1202.44	106	1872	437	545	878	328	12.63	2.17	6.6	3.02	19.34	9.11	94.97	582.46	6.1772	
10:44:37	1202.82	108	1746	445	713	987	480	10.88	2.04	6.68	10.57	11.08	1.15	39.79	582.74	6.1844	
10:45:06	1203.84	108	1833	444	673	835	494	10.91	2.08	6.77	10.74	11.06	0.91	31.2	582.98	6.1921	
10:45:36	1203.18	108	1873	445	897	888	389	10.66	2.08	6.88	10.55	11.08	0.72	23.78	583.19	6.1994	
10:45:59	1203.39	107	1714	441	721	1065	393	10.89	2.04	6.68	10.65	11.06	1.27	39.28	583.45	6.2067	
10:46:07	1203.84	106	1858	439	885	1068	312	11.47	2	6.88	11.18	10.93	0.89	105.63	583.69	6.2159	
10:46:14	1203.89	109	1848	438	873	971	287	11.84	2.1	6.89	10.91	10.44	0.93	127.81	583.84	6.221	
10:46:22	1204.14	106	1850	439	882	1279	518	11.67	2.1	6.8	10.88	10.56	1.34	116.61	584.14	6.2282	
10:46:30	1204.39	104	2093	429	965	1285	310	11.64	2.25	6.58	10	10.83	1.32	121.3	584.44	6.2353	
10:46:39	1204.80	104	2217	431	1184	2521	1858	11.95	2.37	7.34	10.3	11.83	2.0	83.39	584.69	6.2431	
10:46:53	1204.8	108	1856	447	705	874	484	13.5	4.74	6.4	8.13	11.18	0.98	50.18	584.99	6.2503	
10:47:28	1205.05	107	1872	396	283	2490	2543	14.85	3.91	2.47	6.83	6.88	2.93	21.86	585.14	6.2575	
10:47:43	1205.33	108	1836	411	880	1364	782	13.4	2.07	6.88	8.24	8.75	1.2	98.98	585.38	6.2648	
10:47:50	1205.68	109	1836	420	753	947	312	13.73	1.85	6.4	7.8	8.83	1.13	113.74	585.63	6.2728	
10:48:02	1205.93	108	1832	415	788	979	373	12.39	1.89	6.3	9.25	8.84	1.89	74.66	585.89	6.281	
10:48:11	1206.08	105	1871	404	988	1218	514	12.87	2.08	6.63	8.13	8.5	0.89	183.28	586.17	6.2888	
10:48:18	1206.33	105	1874	406	907	1077	259	12.76	1.92	6.4	8.88	8.36	0.81	120.29	586.48	6.2952	

DOE high power mortar test Amaco Catoosa Test Site

Well No. 33		Date: 2/26/98															
Starting Depth =		1031.27		Bit Type =		Walker McDoanald MP66H											
Ending Depth =		1083.34		Bit Size =		4.75											
Total Depth Drilled =		52.07		Bit Nozzles =		6, 9, 12, 12											
Hours On Bit =		6.59		Mud Type =		Water Based											
Average ROP =		63.72		Mud Weight (lbs/gal)		9.04											
Circulating (ft) =		1071.36		Pipe (ft) =		662.93		Color (ft) =		408.68							
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours	
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit	
10:48:28	1206.98	108	1871	410	844	1058	304	12.50	1.91	0.98	8.08	8.41	0.74	115.35	568.63	6:1870	
10:48:34	1206.98	105	1985	403	840	1048	293	12.53	1.98	0.93	8.11	8.46	0.64	110.08	568.63	6:1885	
10:48:41	1207.00	105	2011	406	878	1056	178	12.54	1.84	0.91	8.1	8.43	0.72	110.38	567.19	6:1910	
10:48:45	1207.34	108	2043	404	1024	1156	267	12.56	1.97	0.93	8.08	8.48	0.81	112.72	567.38	6:1942	
10:48:57	1207.99	104	2096	398	1075	1278	324	12.58	2.06	0.82	8.11	8.42	0.74	111.15	567.68	6:1965	
10:49:08	1207.64	107	2016	413	958	1308	494	12.31	2.38	1.14	8.32	8.88	1.15	77.45	567.68	6:1987	
10:49:20	1208.06	108	2131	403	1178	3648	3111	12.35	2.49	1.75	8.40	10.94	2.79	47.33	568.19	6:2048	
10:49:33	1208.34	108	2303	444	1608	1814	1090	13.93	2.13	0.98	7.7	8.41	3.9	183.45	568.38	6:2083	
10:49:59	1208.99	107	1763	416	716	923	277	15.47	2.21	1.16	8.15	7.11	1.94	48.4	568.63	6:2114	
10:50:05	1208.64	108	1848	415	859	1608	650	15.48	2.08	0.76	8.14	8.68	1.3	65.62	568.63	6:2131	
10:50:16	1208.99	107	1677	424	633	898	405	15.96	1.93	0.43	8.26	8.58	1.01	70.29	569.19	6:2168	
10:50:35	1209.34	108	1704	426	731	894	334	15.33	2.39	0.27	8.29	8.69	0.79	60.62	569.38	6:2207	
10:50:51	1209.69	107	1720	424	798	898	194	15.38	2.17	0.83	8.38	8.73	0.31	58.65	569.63	6:2237	
10:51:21	1209.73	108	1863	405	338	943	1037	15.75	3.03	3.72	8.27	9.29	7.28	18.54	569.81	6:2263	
10:51:51	1209.94	108	1828	393	696	1024	429	15.38	1.94	0.68	8.28	8.58	1.18	28.89	569.98	6:2348	
10:52:02	1210.19	107	1767	384	800	896	170	15.71	2.01	0.58	8.31	8.32	0.74	83.65	569.98	6:2348	
10:52:13	1210.44	107	1758	383	812	906	208	15.71	3.08	0.84	8.31	8.27	0.74	83.4	569.98	6:2357	
10:52:32	1210.89	107	1710	381	752	850	132	15.48	1.98	0.48	8.14	8.48	0.75	45.68	569.74	6:2361	
10:53:02	1210.89	108	1838	384	864	909	186	15.38	1.95	0.68	8.14	8.56	0.62	28.83	569.94	6:2384	
10:53:20	1211.34	108	1864	384	767	893	265	15.33	2.11	0.71	8.28	8.51	0.89	31.75	569.12	6:2731	
10:54:09	1211.31	108	1822	398	898	730	95	15.37	1.61	0.41	8.34	8.91	0.89	29.31	569.36	6:2804	
10:54:30	1211.86	108	1864	393	793	1061	498	15.32	3.04	0.83	8.35	8.56	0.93	39.08	569.62	6:2868	
10:55:00	1211.76	109	1853	400	800	740	158	15.38	1.97	0.96	8.33	8.58	0.65	24.1	569.82	6:2871	
10:55:30	1211.84	108	1837	392	800	720	81	15.37	2.04	0.61	8.34	8.59	0.48	20.48	569.96	6:2957	
10:55:56	1213.19	108	1734	383	779	1295	583	14.77	2.64	0.58	8.35	10.73	0.44	40.98	569.24	6:3117	
10:56:02	1213.44	105	2224	383	1073	1178	214	11.89	1.98	0.61	8.78	10.13	0.31	94.35	569.48	6:3142	
10:56:15	1212.69	104	2006	378	1448	1355	307	12.03	1.93	0.39	9.1	9.65	0.77	118.28	569.74	6:3185	
10:56:17	1212.34	104	2119	376	1184	1355	235	12.03	1.84	0.4	9.01	10.04	0.81	121.53	569	6:3185	
10:56:26	1213.19	104	2146	378	1187	1384	198	11.8	2.07	0.64	8.73	10.15	0.31	101.66	569.24	6:3211	
10:56:32	1213.44	109	2153	375	1174	1287	182	11.99	1.94	0.49	9.03	9.63	0.62	125.4	569.5	6:3226	
10:56:43	1213.69	102	2108	374	1188	1356	328	11.84	2.28	0.82	8.78	10.36	1.01	82.88	569.74	6:3257	
10:56:50	1213.94	104	2141	378	1116	1372	499	11.88	2.02	0.77	9.77	10.25	0.88	118.33	569.96	6:3277	
10:57:07	1214.19	100	2046	383	1070	1367	927	11.8	2.48	1.95	8.83	11.3	4.38	78.16	569.28	6:3311	
10:57:28	1214.44	109	1842	386	890	1040	490	16.78	1.65	0.38	8.81	9.37	1.77	44.1	569.48	6:3382	
10:57:48	1214.89	109	1845	397	735	1034	373	15.84	1.81	0.45	8.78	8.14	1.91	35.04	569.78	6:3405	
10:57:58	1214.94	108	1784	386	868	847	117	16.13	1.84	0.31	8.41	8.67	0.95	85.12	569.98	6:3459	
10:58:11	1215.19	108	1787	387	843	836	207	16.16	1.87	0.3	8.44	8.7	0.88	77.38	569.28	6:3511	

DOE high power motor test Amaco Catoosa Test Site

Well No. 23	Date 2/26/96																
Starting Depth =	1861.27	Bit Type =	Weldon McDougald MP38M														
Ending Depth =	1862.14	Bit Size =	4.75														
Total Depth Drilled =	850.87	Bit Nozzles =	2, 9, 15, 15														
Hours On Bit =	6.83	Mud Type =	Water Based														
Average ROP =	53.72	Mud Weight (lb/ft³) =	9.30														
Collecting Bit =	1071.39	Pipe OD =	662.69							Color (Type) =	408.68						

TIME HH:MM:SS	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELTA ft-lbs	RROP KPS	PEAK G%	GELTA G%	WOB KIPS	PEAK KIPS	GELTA KIPS	ROP FT/HR	Feet OnBit	Hours OnBit
09:58:21	1215.44	107	1791	300	878	987	146	16.17	1.28	0.33	5.43	5.67	0.27	87.4	598.46	6.3529
09:58:34	1215.89	107	1784	308	872	983	132	16.18	1.34	0.33	5.47	5.74	0.25	88.47	598.79	6.3529
09:58:46	1215.94	107	1792	301	888	958	148	16.14	1.32	0.33	5.46	5.74	0.27	78.04	598	6.3528
09:58:58	1216.19	107	1789	306	874	991	113	16.13	1.31	0.36	5.47	5.72	0.25	74.45	598.26	6.3527
09:59:12	1216.44	107	1791	308	879	979	101	16.14	1.3	0.34	5.46	5.72	0.23	71.83	598.46	6.3527
09:59:23	1216.89	107	1786	300	873	927	117	16.09	1.33	0.41	5.51	5.72	0.43	77.09	598.74	6.3528
09:59:35	1216.94	108	1788	307	885	987	104	16.12	1.34	0.3	5.49	5.72	0.26	71.98	597	6.3734
09:59:46	1217.19	107	1779	309	887	927	126	16.11	1.34	0.44	5.46	5.62	0.27	77.01	597.24	6.3737
09:59:59	1217.44	108	1787	302	883	923	95	16.11	1.32	0.37	5.49	5.74	0.28	71.74	597.49	6.3831
10:00:13	1217.7	107	1782	300	846	892	113	16.08	1.34	0.38	5.51	5.74	0.3	82.1	597.75	6.3841
10:00:25	1217.95	108	1767	307	853	922	101	16.11	1.36	0.36	5.49	5.77	0.2	78.77	597.93	6.3875
10:00:39	1218.2	107	1779	301	860	931	138	16.08	1.36	0.3	5.5	5.74	0.2	85.3	598.24	6.3873
10:00:53	1218.46	108	1783	309	867	923	126	16.08	1.33	0.26	5.51	5.94	0.23	87.3	598.49	6.396
10:01:04	1218.7	107	1813	300	863	985	136	16.17	1.36	0.28	5.42	5.67	0.48	78.86	598.75	6.3922
10:01:17	1219.25	108	1787	304	866	947	122	16.15	1.37	0.27	5.48	5.67	0.62	72.66	598.98	6.4016
10:01:30	1219.2	107	1789	309	876	975	106	16.13	1.37	0.31	5.49	5.72	0.57	78.38	599.24	6.4051
10:01:41	1219.46	107	1781	308	868	925	134	16.11	1.37	0.26	5.48	5.7	0.43	88.6	599.5	6.4085
10:01:54	1219.7	107	1782	304	875	953	138	16.16	1.3	0.36	5.43	5.67	0.45	78.84	598.74	6.4118
10:02:09	1219.95	107	1783	300	873	931	122	16.16	1.37	0.29	5.43	5.7	0.33	78.07	598.99	6.4151
10:02:18	1220.2	107	1783	305	864	910	109	16.16	1.31	0.39	5.43	5.72	0.53	72.88	599.24	6.4185
10:02:29	1220.46	104	1783	304	868	931	122	16.15	1.36	0.31	5.44	5.74	0.66	80.43	602.5	6.4217
10:02:41	1220.7	107	1776	307	867	915	129	16.18	1.37	0.28	5.43	5.7	0.5	75.18	600.75	6.4251
10:02:53	1220.95	106	1779	308	868	906	113	16.18	1.33	0.26	5.44	5.7	0.36	74.03	601.01	6.4285
10:03:04	1221.2	106	1782	303	881	919	134	16.16	1.39	0.3	5.44	5.7	0.48	78.18	601.26	6.4317
10:03:19	1221.59	106	1870	308	891	916	814	19.3	1.36	0.37	5.6	4.74	3.85	46.47	601.82	6.438
10:03:34	1221.83	108	1845	307	888	732	33	16.09	1.33	0.23	3.87	4.17	0.43	41.84	601.87	6.4382
10:03:36	1222.08	107	1848	300	879	728	128	19.01	1.38	0.27	3.98	4.19	0.41	41.89	602.13	6.4448
10:03:50	1222.33	106	1885	305	812	1226	236	17.52	1.33	0.44	5.68	5.99	0.38	44.36	602.37	6.4536
10:04:05	1222.58	106	2017	306	1115	1332	336	14.89	3.01	0.54	5.94	6.19	0.58	103.68	602.83	6.4581
10:04:18	1222.83	104	2025	440	1136	1291	352	14.18	1.98	0.5	5.85	6.24	0.77	121.25	602.87	6.4581
10:04:38	1223.09	104	2038	408	1106	1243	290	14.25	1.97	0.51	6.1	6.22	0.79	136.66	603.16	6.4638
10:04:50	1223.34	104	2069	438	1139	1243	273	14.21	2.05	0.73	6.22	6.1	0.62	120.66	603.38	6.4631
10:05:03	1223.58	106	2033	441	1095	1287	410	14.18	1.96	0.53	6.25	6.17	0.67	127.51	603.63	6.4638
10:05:17	1223.83	106	1906	432	1025	1214	288	14.18	1.16	0.78	6.03	6.04	0.61	118.87	603.88	6.4661
10:05:49	1224.38	104	2062	438	1158	1298	292	14.2	3.06	0.81	6.33	6.14	0.63	113.98	604.14	6.4684
10:05:56	1224.33	105	2084	441	1078	1214	227	14.22	1.97	0.6	6.01	6.17	0.74	131.5	604.36	6.4701
10:06:03	1224.58	105	2047	441	1090	1178	211	14.24	2.02	0.64	6.23	6.19	0.81	128.32	604.55	6.4721

DOE high power mortar test Amaco Catoosa Test Site

TIME	SIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	ft-lbs	ft-lbs	KIPS	KIPS	KIPS	FT/HR	On/Off	On/Off
11:15:10	1224.03	104	2044	437	1084	1174	190	14.24	2	0.40	8.79	8.19	0.60	125.23	004.88	8.4745
11:15:17	1226.08	107	2026	447	1064	1174	229	14.26	2.01	0.60	8.78	8.17	0.61	121.94	005.37	8.4761
11:15:25	1228.30	106	2031	444	1067	1174	289	14.24	1.99	-0.26	8.79	8.19	0.61	119.47	005.4	8.4781
11:15:31	1229.86	104	2038	437	1066	1214	223	14.24	2.01	0.59	8.78	8.18	0.70	132.31	005.64	8.4801
11:15:38	1228.83	105	2024	442	1057	1154	218	14.27	2.01	0.68	8.78	8.17	0.61	127.12	005.88	8.4821
11:15:45	1226.08	105	2010	443	1042	1154	211	14.26	2.06	0.83	8.78	8.32	0.46	121.78	006.15	8.4850
11:15:52	1226.33	105	2006	443	1018	1109	179	14.26	2.05	0.59	8.78	8.19	0.64	134.68	006.37	8.4868
11:15:58	1226.58	106	1997	444	1024	1107	223	14.25	2.04	0.55	8.78	8.1	0.72	122.03	006.65	8.4876
11:16:06	1226.84	105	1983	443	1016	1129	207	14.23	1.80	0.44	8.79	8.34	0.45	135.25	006.89	8.4896
11:16:13	1227.09	105	1984	442	1010	1141	239	14.24	2.01	0.64	8.78	8.38	0.40	126.23	007.14	8.4916
11:16:20	1227.34	105	1984	442	1013	1119	190	14.23	2.03	0.59	8.78	8.19	0.77	128.89	007.41	8.4936
11:16:28	1227.58	106	1983	443	984	1079	235	14.15	1.87	0.58	8.78	8.19	0.69	124.44	007.63	8.4956
11:16:36	1227.84	106	1987	443	994	1141	251	14.16	2.03	0.58	8.77	8.31	0.46	110.77	007.86	8.4976
11:16:43	1228.09	106	1948	443	973	1099	174	14.17	2.07	0.68	8.78	8.24	0.77	126.14	008.14	8.4996
11:16:51	1228.34	107	1925	443	973	1053	180	14.13	2.02	0.63	8.69	8.28	0.41	119.38	008.38	8.5025
11:16:58	1228.58	105	1932	443	979	1089	170	14.14	2.08	0.67	8.68	8.24	0.74	115.28	008.63	8.5042
11:17:06	1228.84	106	1989	443	931	1000	174	14.08	1.98	0.50	8.66	8.29	0.69	117.87	008.88	8.5062
11:17:14	1229.08	107	1992	446	936	1029	211	14.04	2.08	0.61	8.36	8.29	0.67	94.97	009.13	8.5081
11:17:24	1229.34	108	1988	444	942	1054	271	14.09	2.04	0.69	8.36	8.30	0.74	111.96	009.41	8.5114
11:17:32	1229.59	106	1981	443	901	1019	221	14.04	2.03	0.63	8.99	8.29	0.69	107.28	009.64	8.5136
11:17:40	1229.84	108	1948	452	870	1069	352	13.98	2	0.60	8.15	8.62	0.51	78.63	009.88	8.5163
11:17:54	1230.08	107	1899	446	908	1083	476	13.78	2.14	0.74	8.27	16.01	1.29	64.57	010.13	8.5191
11:18:03	1230.34	106	2048	447	1102	1271	466	14.71	2.21	0.94	10.28	10.88	1.38	165.58	010.39	8.5222
11:18:18	1230.58	106	1832	438	790	1089	849	12.19	3.38	0.58	10.87	12.76	1.35	87.17	010.64	8.526
11:18:38	1230.77	106	1656	396	80	1174	1237	14.05	3.01	2.74	8.86	11.54	0.34	20.87	010.83	8.5312
11:18:45	1231.03	106	1745	388	1	651	705	13.63	2.79	2.49	1.81	10.39	1.04	36.83	011.07	8.5411
11:19:14	1231.27	106	1727	387	-42	-33	20	13.57	1.91	0.37	8.34	9.53	0.16	38.32	011.32	8.5474
11:19:23	1231.52	105	1647	382	-42	-33	20	14.92	2.05	0.36	8	8.86	0.6	87	011.56	8.5503
11:19:33	1231.77	105	1630	381	-43	-33	20	14.92	1.96	0.51	8.99	8.24	0.48	88.52	011.81	8.5535
11:19:44	1232.02	107	1741	399	-43	-33	20	13.75	1.84	0.42	9.27	6.53	0.62	48.19	012.07	8.5566
11:20:00	1232.27	107	1748	398	-43	-33	20	13.67	1.98	0.32	9.34	8.93	0.41	34.48	012.32	8.5608
11:20:08	1232.52	106	1863	388	-43	-33	20	13.70	1.96	0.61	9.28	8.53	0.57	48.45	012.56	8.5709
11:21:10	1232.77	105	1961	381	-42	-33	20	14.01	1.84	0.34	8	9.31	0.57	53.96	012.84	8.5747
11:21:21	1233.02	106	1946	385	-42	-33	20	14.04	1.97	0.48	8.88	9.29	0.58	81.67	013.07	8.5777
11:21:41	1233.27	108	1955	391	288	1382	1433	12.84	2.75	2.14	9.16	10.39	2.01	44.48	013.33	8.5827
11:21:50	1233.52	105	1935	387	298	989	893	13.92	3.24	3.94	9.1	10.7	3.47	101.91	013.57	8.5883
11:21:58	1233.77	106	2014	381	-43	-33	20	14.11	1.82	0.37	8.91	8.32	0.48	109.44	013.84	8.5976

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Feet	Hours
MM:SS.SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	ft-lbs	ft-lbs	ft-lbs	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
11:37:17	1253.58	108	1730	426	723	850	384	13.98	1.87	0.31	9.05	9.35	0.89	71.18	833.8	8:44:23
11:37:28	1252.8	106	1742	424	741	898	389	14.09	1.87	0.31	9.65	9.29	0.77	81.08	832.85	8:44:57
11:42:50	1253.96	106	1652	418	859	888	523	15.64	1.96	0.43	7.43	10.46	0.96	52.76	838.2	8:45:04
11:43:00	1253.61	106	1744	419	779	862	182	13	1.84	0.34	10.05	10.38	0.85	87.05	831.88	8:45:03
11:43:13	1253.86	106	1737	422	737	860	227	12.96	1.91	0.39	10.12	10.84	0.67	70.78	831.91	8:45:17
11:43:26	1254.11	107	1717	422	730	935	355	12.89	1.97	0.47	10.19	10.88	0.55	67.81	834.18	8:45:58
11:43:40	1254.36	106	1722	421	748	878	239	12.92	1.94	0.38	10.15	10.41	0.55	68.41	834.41	8:46:02
11:43:51	1254.61	108	1731	428	740	919	302	12.82	1.93	0.43	10.17	10.48	0.56	76.23	834.68	8:47:29
11:44:05	1254.86	107	1738	423	759	870	284	12.87	1.89	0.39	10.32	10.44	0.72	78.34	834.61	8:47:58
11:44:18	1255.11	107	1728	422	734	947	401	12.95	1.94	0.39	10.33	10.38	0.0	72.48	838.18	8:47:52
11:44:28	1255.36	106	1734	421	748	870	279	12.94	1.88	0.38	10.09	10.61	0.63	87.71	835.41	8:48:21
11:44:39	1255.61	107	1724	423	730	905	482	12.88	1.99	0.38	10.15	10.21	0.57	87.46	835.25	8:48:58
11:44:53	1255.86	106	1743	416	762	874	308	13.03	1.92	0.38	10.16	10.36	0.55	84.96	838.9	8:49:03
11:45:05	1256.11	106	1724	418	734	918	320	12.91	1.93	0.41	10.17	10.48	0.57	72.88	838.10	8:49:08
11:45:19	1256.36	106	1720	422	728	890	332	12.91	1.94	0.39	10.17	10.48	0.63	83.59	838.41	8:49:17
11:45:28	1256.61	106	1747	417	782	882	194	13.07	1.91	0.38	10	10.32	0.63	104.13	838.88	8:49:58
11:45:38	1256.86	108	1752	421	780	882	287	13.1	1.94	0.45	9.98	10.35	0.55	88.78	838.91	8:50:1
11:45:47	1257.11	108	1767	417	785	878	180	13.18	1.9	0.42	9.91	10.2	0.68	101.41	837.18	8:50:4
11:45:57	1257.36	108	1767	423	740	826	377	13.07	1.9	0.38	10.01	10.27	0.8	88.07	837.41	8:50:78
11:46:08	1257.61	106	1758	419	771	883	289	13.05	1.93	0.4	10.04	10.38	0.69	84.01	837.88	8:51:04
11:46:20	1257.86	106	1748	417	743	882	308	12.83	1.89	0.4	10.15	10.41	0.8	78.98	837.93	8:51:56
11:46:32	1258.11	105	1739	417	743	882	288	12.85	1.81	0.39	10.13	10.44	0.6	78.10	838.18	8:51:1
11:46:44	1258.36	108	1747	421	747	874	367	12.94	1.91	0.39	10.13	10.38	0.62	71.53	838.41	8:52:06
11:46:57	1258.61	106	1747	419	739	918	336	12.91	1.9	0.37	10.17	10.41	0.55	73.28	838.67	8:52:58
11:47:11	1258.86	107	1732	425	719	919	409	12.8	1.89	0.38	10.18	10.48	0.67	84.25	838.91	8:53:29
11:47:22	1259.12	107	1743	425	737	919	301	12.95	1.91	0.37	10.12	10.44	0.68	78.84	839.19	8:53:11
11:47:34	1259.37	108	1753	421	734	906	320	12.98	1.91	0.38	10.11	10.44	0.72	78.38	839.41	8:53:42
11:47:49	1259.62	107	1742	420	719	906	385	12.86	1.9	0.42	10.22	10.63	0.77	61.33	839.68	8:53:53
11:47:58	1259.87	108	1777	422	747	919	329	12.95	1.91	0.35	10.12	10.43	0.8	83	839.93	8:54:14
11:48:10	1260.12	108	1786	422	773	939	296	13.07	1.88	0.37	10	10.34	0.84	87.29	840.18	8:54:42
11:48:18	1260.37	105	1828	417	819	919	590	13.17	1.9	0.41	9.9	10.2	0.85	112.86	840.44	8:54:86
11:48:27	1260.62	105	1801	419	773	874	297	13.09	1.91	0.4	9.98	10.27	0.82	85.83	840.67	8:54:91
11:48:37	1260.87	107	1802	423	777	886	190	13.08	1.88	0.34	9.98	10.23	0.8	91.23	840.94	8:55:17
11:48:48	1261.12	108	1789	422	775	939	300	12.97	1.9	0.38	10.1	10.16	0.82	86.79	841.18	8:55:49
11:48:50	1261.37	108	1789	418	778	937	316	13.03	1.86	0.44	10.02	10.48	0.79	78.79	841.43	8:56:08
11:49:10	1261.62	108	1777	417	762	887	332	12.97	1.94	0.41	10.1	10.41	0.89	85.04	841.68	8:56:53
11:49:21	1261.87	105	1782	418	773	839	271	12.68	1.87	0.38	10.09	10.28	0.82	88.98	841.87	8:57:04

DOE high power mortar test Amaco Caloosa Test Site

Well No: 23		Date: 2/26/98															
Starting Depth =	1031.27			Bit Type =		Walker McDonald MP58H											
Ending Depth =	1382.14			Bit Size =		4.75											
Total Depth Drilled =	350.87			Bit Nozzles =		0, 9, 12, 32											
Losses On Bit =	6.53			Mud Type =		Water Based											
Average ROP =	53.72			Mud Weight (lbs/gal)		9.00											
Circulation (ft)	1071.30			Pipe (ft)		651.05				Collar (ft)		405.85					
TIME	BIT DEPTH	FLOW	PRESS	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours	
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G%	G%	KIPS	KIPS	KIPS	FT/HR	Crack	On/Off	
11:49:39	1262.12	103	1708	436	765	951	901	12.84	1.06	0.48	10.13	10.35	0.57	74.78	642.16	6:50:25	
11:49:45	1262.37	103	1706	421	732	838	944	12.59	1.03	0.4	10.19	10.51	0.74	73.16	642.42	6:50:36	
11:49:52	1262.62	105	1774	449	754	874	233	13.06	1.05	0.46	10.01	10.39	0.72	67.50	642.68	6:50:50	
11:50:00	1262.87	106	1731	421	691	505	235	12.93	1.04	0.48	10.14	10.59	0.87	62.13	643.01	6:51:06	
11:50:08	1263.12	107	1714	423	658	854	312	12.89	1.02	0.4	10.19	10.53	0.77	65.24	643.17	6:51:20	
11:50:14	1263.37	108	1743	421	713	813	247	13	1.01	0.41	10.07	10.36	0.67	61.88	643.41	6:51:36	
11:50:23	1263.62	108	1709	427	679	821	283	12.92	1.05	0.43	10.15	10.44	0.67	70.23	643.67	6:51:50	
11:50:29	1263.87	108	1724	422	698	810	381	12.83	1.01	0.44	10.19	10.48	0.65	62.43	643.95	6:52:07	
11:51:10	1264.12	107	1728	424	713	825	384	12.91	1.02	0.44	10.16	10.48	0.72	73.38	644.17	6:52:41	
11:51:22	1264.37	109	1757	431	734	947	328	12.94	1.05	0.37	10.13	10.44	0.67	73.84	644.43	6:52:56	
11:51:35	1264.62	107	1784	423	719	864	289	12.91	1.04	0.47	10.15	10.46	0.69	72.11	644.68	7:00:13	
11:51:48	1264.88	107	1723	425	698	509	247	12.67	1.04	0.48	10.2	10.48	0.67	65.78	644.93	7:00:25	
11:52:01	1265.13	107	1727	426	694	805	335	12.93	1.07	0.47	10.15	10.51	0.77	66.19	645.17	7:00:34	
11:52:14	1265.38	107	1718	411	695	1022	1829	12.89	1.02	0.44	10.18	10.83	0.77	70.78	645.43	7:01:21	
11:52:29	1265.63	107	1716	425	683	828	328	12.84	1.05	0.55	10.22	10.51	0.62	68.19	645.67	7:01:53	
11:52:43	1265.88	107	1725	422	698	821	238	12.83	2.08	0.71	10.17	10.48	0.69	66.16	645.92	7:02:02	
11:53:00	1266.13	107	1716	423	678	781	231	12.66	1.04	0.4	10.21	10.53	0.77	67.62	646.18	7:02:35	
11:53:08	1266.38	108	1703	421	743	1008	393	13.07	1.09	0.61	10.09	10.46	0.63	74.02	646.44	7:03:27	
11:53:19	1266.63	106	1753	426	739	821	190	13.03	1.05	0.48	10.04	10.41	0.67	67.86	646.67	7:03:58	
11:53:30	1266.88	106	1767	426	748	902	320	13.01	2.01	0.55	10.03	10.41	0.74	61.02	646.93	7:04:30	
11:53:40	1267.13	108	1744	421	747	642	267	13.01	1.06	0.35	10.09	10.41	0.68	64.05	647.18	7:05:02	
11:53:52	1267.38	108	1743	421	728	906	325	12.93	1.07	0.53	10.11	10.44	0.72	70.13	647.43	7:05:44	
11:54:05	1267.63	107	1715	420	690	821	308	12.93	1.04	0.43	10.14	10.41	0.65	69.7	647.67	7:06:28	
11:54:16	1267.88	107	1728	421	711	870	312	12.97	1.02	0.46	10.09	10.41	0.70	63.97	647.94	7:06:59	
11:54:28	1268.13	107	1739	432	732	848	310	13.06	2.01	0.61	9.87	10.34	0.98	62.74	648.19	7:07:05	
11:54:37	1268.38	108	1742	431	683	817	295	12.94	1.08	0.5	10.12	10.46	0.68	70.22	648.43	7:07:52	
11:54:51	1268.63	107	1685	424	667	793	227	12.67	1.01	0.37	10.18	10.51	0.88	66.64	648.68	7:08:37	
11:55:03	1268.88	106	1687	419	681	785	174	12.98	2.13	0.7	10.08	10.51	0.88	72.36	648.93	7:09:01	
11:55:13	1269.13	107	1689	423	640	785	223	13.01	1.09	0.6	10.06	10.32	0.74	69.56	649.18	7:09:17	
11:55:23	1269.38	107	1611	423	676	870	156	13.01	1.04	0.46	10.05	10.44	0.93	63.44	649.43	7:09:46	
11:55:32	1269.63	108	1635	426	824	728	180	13.14	1.9	0.4	9.92	10.41	0.88	68.02	649.68	7:09:57	
11:55:47	1269.88	107	1630	421	827	769	298	12.82	1.02	0.4	10.24	10.9	0.79	68.96	649.94	7:10:14	
11:55:58	1270.13	108	1686	419	679	777	207	13.02	1.88	0.4	10.04	10.48	0.66	63.33	650.18	7:10:43	
11:56:07	1270.38	107	1656	424	648	732	195	13.06	1.91	0.39	10	10.29	0.63	67.03	650.44	7:10:58	
11:56:18	1270.64	107	1633	424	828	708	182	13.26	1.91	0.41	10	10.34	0.69	68.16	650.68	7:11:17	
11:56:26	1270.89	107	1608	428	684	793	247	13.18	1.98	0.46	9.61	10.25	0.74	60.58	650.93	7:11:32	
11:56:38	1271.14	106	1651	422	846	765	211	13.03	1.85	0.57	10.03	10.38	0.76	62.9	651.18	7:11:48	

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK LOAD	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	%	GV	KIPS	KIPS	KIPS	FT/HR	Depth	Clock
11:58:46	1271.38	108	1878	421	674	757	182	13.1	1.89	0.35	9.86	10.34	0.44	88.73	651.44	7.0878
11:58:54	1271.64	107	1843	424	644	751	343	13.15	1.83	0.44	9.0	10.38	0.38	104.07	651.88	7.0901
11:59:04	1271.89	107	1727	422	749	882	433	13.19	1.89	0.51	9.91	10.44	1.58	85.14	651.93	7.0920
11:59:14	1272.08	108	1651	408	458	898	867	12.56	2	3.52	10.49	12.42	3.93	82.03	652.14	7.1009
11:59:24	1272.24	107	1800	380	792	2066	2771	19.4	2.81	2.46	8.63	13.79	9.1	10.38	652.39	7.1022
11:59:34	1272.32	107	1536	393	534	582	513	10.33	1.82	0.3	6.9	7.28	2.38	10.68	652.38	7.1178
11:59:04	1272.44	107	1364	388	569	676	374	14.13	1.84	0.3	6.91	10.33	2.73	14.4	652.49	7.1258
11:59:24	1272.61	108	1850	388	685	753	358	12.92	1.85	0.32	10.12	10.34	0.48	22.06	652.68	7.1343
12:00:03	1272.88	106	1706	387	724	809	184	12.88	1.85	0.35	10.06	10.25	0.43	33.84	652.91	7.1418
12:00:28	1273.13	106	1749	388	733	797	123	12.89	1.83	0.34	10.88	10.39	0.43	33.06	653.17	7.1462
12:00:54	1273.38	105	1726	382	752	834	342	13.53	1.81	0.35	10.64	10.39	0.45	35.29	653.43	7.1562
12:01:15	1273.63	108	1739	384	785	854	117	13.53	1.77	0.33	10.02	10.27	0.48	42.94	653.68	7.1622
12:01:41	1273.84	106	1730	388	767	852	170	13.81	1.72	0.69	10.04	10.25	0.5	54.42	653.94	7.1684
12:02:06	1274.13	108	1737	393	787	847	206	13	1.32	0.45	10.88	10.26	0.48	25.31	654.19	7.1766
12:02:35	1274.38	108	1723	387	876	903	1017	13.54	2.3	2.35	10.11	11.94	3.88	30.65	654.32	7.1848
12:03:05	1274.6	108	1746	388	876	748	388	12.54	2.18	2.93	10.11	12.02	1.87	28.79	654.68	7.1933
12:03:28	1274.84	107	1899	388	864	738	184	12.82	2.34	2.26	10.13	11.78	3.76	28.02	654.8	7.2016
12:04:08	1275.03	107	1898	389	858	724	117	12.8	2.82	2.69	10.18	13.59	3.85	22.91	655.08	7.2098
12:04:38	1275.24	107	1786	388	884	864	169	12.83	2.7	3.72	10.13	11.98	4	25.31	655.29	7.2181
12:05:06	1275.43	107	1897	390	813	2579	2679	17.51	2.5	2.59	8.4	11.75	1.39	29.42	655.48	7.2264
12:05:36	1275.6	108	1253	394	703	1384	814	16.56	1.88	0.61	8.44	8.05	7.88	19.38	655.64	7.2347
12:06:08	1275.81	108	1172	337	718	1348	1833	15.04	1.07	0.84	7.89	8.79	3.04	34.68	655.85	7.243
12:06:30	1276.06	106	1447	390	794	876	216	15.14	1.74	0.61	8.89	10.44	2.42	37.95	656.11	7.2489
12:06:48	1276.31	107	1848	388	886	883	173	12.82	1.89	0.39	10.12	10.36	0.3	33.37	656.38	7.2548
12:07:03	1276.58	107	1836	388	876	1032	189	12.89	1.75	0.44	10.04	10.29	0.37	41.09	656.63	7.2607
12:07:16	1276.81	108	1884	388	1078	1597	162	13.15	1.77	0.44	9.88	10.26	0.38	38.87	656.88	7.2689
12:07:28	1277.08	107	1703	389	1021	1377	488	13.07	1.78	0.45	9.67	10.25	0.57	49.1	657.1	7.2682
12:07:40	1277.31	105	1748	384	1076	1222	306	13.13	1.87	0.38	9.91	10.28	0.68	40.87	657.37	7.2684
12:08:01	1277.58	108	1711	385	1076	1194	245	13.15	1.89	0.43	9.86	10.27	0.72	32.58	657.6	7.2722
12:08:01	1277.81	105	1808	383	1122	1287	348	13.17	1.69	0.49	9.87	10.17	0.67	48.2	657.89	7.2755
12:08:13	1278.03	108	1886	388	1174	2589	2185	13.07	1.75	0.75	9.46	11.75	3.87	73.77	658.13	7.2793
12:08:29	1278.31	108	1885	387	868	1089	215	14.87	1.83	0.43	8.25	8.86	0.67	58.82	658.37	7.2828
12:08:43	1278.58	107	1848	388	872	1109	282	14.87	1.73	0.48	8.38	8.85	0.3	67.74	658.61	7.2866
12:08:58	1278.81	108	1987	382	828	1808	184	14.8	1.73	0.43	8.43	8.84	0.48	58.08	658.89	7.2911
12:09:17	1279.08	108	1888	393	893	1918	311	14.87	1.89	0.4	8.46	8.87	0.53	48.72	659.11	7.294
12:09:38	1279.31	108	1578	394	914	1049	313	14.89	1.88	0.35	8.44	8.54	0.43	54.18	659.38	7.2978
12:09:50	1279.58	107	1837	389	883	1133	235	14.87	1.71	0.4	8.38	8.84	0.55	44.08	659.6	7.3022

Well No: 23
 Date: 2/20/80
 Starting Depth = 1031.27
 Ending Depth = 1382.14
 Total Depth Drilled = 350.87
 Hours On Bit = 8.83
 Average RCP = 88.73
 Drilling (ft) = 1071.36

Bit Type = Wacker Mc Donalds MP68H
 Bit Size = 4.75
 Bit Nozzles = 5, 9, 12, 12
 Mud Type = Water Based
 Mud Weight (lb/gal) = 8.00
 Pipe (in) = 682.58
 Casing (in) = 482.68

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23		Date: 2/25/08															
Casing Depth = 1301.27				Bit Type = Walker McDonald MPRBH													
Landing Depth = 1302.14				Bit Size = 8.75													
Total Depth Drilled = 560.67				Bit Nozzle = 8, 9, 12, 13													
Hours On Bit = 6.55				Mud Type = Water Based													
Average ROP = 53.72				Mud Weight (lbs/gal) = 9.30													
Circulating (ft) = 1571.35				Pipe (ft) = 902.09				Collar (ft) = 408.65									
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours	
HH:MM:SS	FEET	CFM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	ft-lbs	%	%	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit	
12:10:04	1270.81	107	1861	389	937	1084	233	14.82	1.72	0.42	8.41	8.97	0.56	61.09	666.89	7.3089	
12:10:09	1280.06	107	1870	390	932	1165	250	14.72	1.71	0.49	8.31	8.52	0.21	62.58	668.12	7.3132	
12:10:31	1280.24	107	1873	388	900	1133	260	14.71	1.69	0.41	8.31	8.59	0.28	72	668.26	7.3166	
12:10:44	1290.68	106	1867	386	1017	1108	267	14.71	1.59	0.38	8.31	8.89	0.57	69.74	669.61	7.3204	
12:10:59	1300.81	106	1788	398	1144	1023	213	14.91	1.59	0.11	8.11	10.25	2.14	69.12	669.85	7.3244	
12:11:12	1261.07	109	1813	394	893	1024	186	15.07	1.89	0.44	7.38	7.63	0.25	68.83	669.11	7.3281	
12:11:29	1291.32	110	1503	401	868	987	166	15.59	1.66	0.43	7.43	7.68	0.25	64.93	669.36	7.3327	
12:11:44	1261.57	108	1814	392	890	1093	251	15.69	1.7	0.46	7.35	7.61	0.27	66.25	669.62	7.337	
12:11:58	1261.63	107	1894	396	833	1080	251	15.65	1.69	0.37	7.36	7.64	0.28	70.24	669.88	7.3404	
12:12:14	1292.07	109	1803	394	813	1054	193	15.81	1.81	0.38	7.41	7.61	0.2	62.18	669.11	7.3453	
12:12:30	1292.32	108	1641	398	897	1012	203	15.58	1.85	0.39	7.44	7.68	0.24	68.79	669.36	7.3499	
12:12:49	1262.57	107	1831	391	890	987	166	15.57	1.83	0.48	7.45	7.69	0.24	49.75	669.61	7.3536	
12:13:06	1262.63	106	1854	385	917	1008	176	15.81	1.69	0.39	7.41	7.68	0.27	54.19	669.86	7.3586	
12:13:22	1293.07	107	1823	395	942	1080	286	15.56	1.85	0.37	7.46	7.68	0.22	54.73	669.11	7.3642	
12:13:49	1293.32	107	1803	390	872	847	169	15.53	1.84	0.37	7.49	7.73	0.24	42.08	669.36	7.3702	
12:13:59	1293.57	108	1658	397	830	983	142	15.81	1.87	0.44	7.41	7.69	0.28	59.98	669.62	7.3749	
12:14:19	1293.82	107	1521	390	877	919	189	15.80	1.78	0.46	7.45	7.81	0.36	52.75	669.88	7.3791	
12:14:35	1264.07	107	1817	393	878	1008	281	15.84	1.89	0.38	7.47	7.63	0.16	44.48	669.11	7.3845	
12:14:52	1264.32	109	1825	391	878	1040	275	15.95	1.7	0.44	7.46	7.69	0.23	63.83	669.36	7.3894	
12:20:38	1294.71	106	1284	387	706	1113	709	16.18	1.99	0.48	4.02	9	0.5	28.05	669.62	7.4206	
12:20:53	1294.96	108	1814	395	645	1161	328	14.9	1.9	0.45	9.48	9.12	0.36	61.05	669.87	7.4248	
12:21:07	1295.21	108	1814	395	945	1129	275	14.9	1.86	0.36	8.79	9	0.21	63.08	669.62	7.4296	
12:21:28	1295.46	107	1861	399	863	947	105	14.85	1.57	0.42	8.49	8.97	0.48	49.19	669.87	7.4336	
12:21:45	1295.71	108	1854	392	856	1004	303	14.84	1.61	0.39	8.99	9.1	0.11	61.82	669.62	7.4386	
12:22:04	1295.96	109	1498	393	896	893	122	14.76	1.81	0.38	8.91	9.1	0.19	43.24	669.87	7.4434	
12:22:29	1296.21	109	1484	392	810	963	193	14.77	1.81	0.35	8.92	9.17	0.25	38.64	669.62	7.4483	
12:22:54	1296.46	108	1418	392	793	859	178	14.74	1.88	0.42	8.93	9.19	0.26	38.02	669.87	7.4531	
12:23:24	1296.69	108	1441	392	744	823	160	13.74	2.49	1.87	8.99	11.39	2.4	30	669.62	7.4464	
12:23:54	1306.91	109	1429	393	729	785	117	13.98	2.38	1.83	10.11	10.98	1.77	28.38	669.87	7.4516	
12:24:24	1297.13	108	1354	392	694	744	97	13.99	2.29	1.41	10.14	10.98	1.84	26.94	669.11	7.4556	
12:24:49	1297.38	107	1349	390	692	690	139	13.73	2.31	1.36	9.98	11.25	1.27	42.89	669.87	7.4601	
12:25:06	1297.63	108	1480	392	751	809	890	13.83	2.89	1.98	10.07	10.84	1.75	42.25	669.62	7.4701	
12:25:36	1297.85	108	1458	394	808	2097	2543	13.81	2.8	2.22	10.19	11.43	1.24	3.27	669.87	7.4804	
12:25:46	1297.61	107	1727	396	923	2216	1899	13.81	2.4	1.33	9.88	11.39	1.51	64.4	669.62	7.4886	
12:26:19	1308.07	108	1393	393	898	838	271	13.78	2.83	1.21	7.92	11.11	4.62	20.3	669.87	7.4943	
12:26:45	1298.3	108	1201	393	890	744	180	16.78	2.54	0.74	6.9	7.13	0.23	15.6	669.62	7.5029	
12:27:18	1298.36	106	1250	392	890	751	162	16.81	2	0.89	6.89	7.16	0.27	26.98	669.87	7.5106	

DOE high power mortar test Amaco Catoosa Test Site

TIME HH:MM:SS	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELT ft-lbs	HOCK LOAD NIPS	PEAK G/s	DELTA G/s	WOB KIPS	PEAK KIPS	DELTA KIPS	ROP FT/HR	Feet On Bit	Hours On Bit
12:27:40	1268.65	107	1301	380	692	753	126	16.82	1.06	0.4	8.85	7.08	0.43	18.23	668.59	7.5195
12:28:16	1268.75	106	1357	387	745	842	203	15.21	1.07	0.36	7.44	6.39	1.7	22.28	668.78	7.5278
12:28:46	1268.68	106	1420	387	700	858	142	15.58	1.04	0.37	8.12	6.39	0.48	30.15	669.04	7.5361
12:29:14	1269.29	106	1344	388	613	842	146	15.58	1.05	0.47	8.09	6.38	0.80	32.88	669.20	7.5438
12:29:58	1268.48	105	1447	387	608	879	142	15.89	1.0	0.45	8.08	6.34	0.43	38.99	669.59	7.5504
12:30:57	1268.75	107	1437	390	697	825	796	15.84	1.43	1.53	8.13	6.53	1.50	47.81	669.78	7.5566
12:30:27	1268.67	107	1404	391	57	27	73	15.8	1.81	0.39	8.18	6.31	0.34	28.59	670.03	7.5642
12:30:57	1268.15	106	1369	394	47	25	20	15.48	1.81	0.39	8.15	6.35	0.38	38.88	670.24	7.5725
12:31:27	1268.41	106	1374	392	48	25	24	15.47	1.89	0.4	8.18	6.35	0.41	35.34	670.42	7.5808
12:31:57	1268.62	107	1415	390	46	21	32	15.48	1.87	0.39	8.14	6.35	0.45	25.77	670.66	7.5891
12:32:27	1268.78	108	1361	392	47	25	24	15.43	1.81	0.38	8.19	6.36	0.45	19.4	670.93	7.5974
12:32:57	1269.03	108	1359	395	46	25	24	15.43	1.87	0.38	8.14	6.36	0.37	27.5	671.17	7.6057
12:33:19	1269.29	106	1487	392	46	25	24	15.6	1.81	0.45	8.03	6.28	0.69	46	671.5	7.612
12:33:49	1269.47	107	1391	390	47	25	24	15.48	1.81	0.27	8.15	6.33	0.38	28.27	671.82	7.6203
12:34:16	1269.63	107	1322	381	59	29	26	15.41	1.8	0.24	8.21	6.4	0.36	18.97	671.95	7.6286
12:34:46	1269.3	107	1348	388	58	17	31	15.44	1.88	0.31	8.18	6.43	0.8	20.45	672.38	7.6369
12:35:16	1269.65	107	1349	380	58	21	38	15.44	1.8	0.4	8.18	6.43	0.9	19.75	672.61	7.6452
12:35:49	1269.15	105	1345	397	56	17	41	15.43	1.99	0.37	8.18	6.43	0.48	21.6	672.99	7.6535
12:36:19	1267.8	107	1324	399	58	25	24	15.41	1.81	0.25	8.21	6.39	0.36	16.5	673.36	7.6618
12:36:49	1267.47	107	1353	388	49	25	28	15.44	1.8	0.25	8.18	6.4	0.35	23.77	673.52	7.6701
12:37:19	1267.62	107	1346	395	41	29	24	15.42	1.79	0.21	8.19	6.38	0.34	18.78	673.68	7.6784
12:37:49	1267.73	107	1336	392	59	29	20	15.41	1.78	0.24	8.21	6.38	0.34	18.98	673.83	7.6867
12:38:19	1267.08	107	1398	398	58	29	20	15.43	1.63	0.26	8.19	6.4	0.43	21.58	673.91	7.695
12:38:49	1268.14	107	1375	388	49	28	28	15.44	1.89	0.31	8.17	6.5	0.63	21.8	673.99	7.7033
12:39:19	1268.34	107	1381	390	42	26	24	15.43	1.85	0.24	8.2	6.35	0.45	19.78	673.38	7.7116
12:39:49	1268.47	107	1320	388	41	33	29	15.39	1.81	0.22	8.22	6.38	0.43	18.91	673.82	7.720
12:40:18	1268.61	103	1328	391	41	29	29	15.36	1.79	0.19	8.22	6.38	0.34	17.48	673.87	7.7283
12:40:49	1268.75	107	1331	391	46	33	31	15.4	1.51	0.23	8.21	6.38	0.36	17.88	673.61	7.7366
12:41:19	1268.91	107	1332	390	44	28	24	15.4	1.81	0.2	8.21	6.38	0.38	18	673.88	7.7449
12:41:49	1264.11	107	1354	390	49	29	20	15.43	1.82	0.22	8.18	6.38	0.41	24.48	674.18	7.7532
12:42:19	1264.51	108	1358	390	40	29	27	15.44	1.85	0.31	8.17	6.35	0.38	22.08	674.38	7.7615
12:42:49	1264.86	107	1314	391	41	21	41	15.4	1.87	0.33	8.21	6.45	0.38	17.6	674.51	7.7698
12:43:19	1264.69	107	1295	398	40	25	25	15.38	1.84	0.3	8.25	6.4	0.48	16.38	674.68	7.7781
12:43:49	1264.7	107	1398	391	17	485	836	15.33	1.93	0.64	8.28	6.59	2.13	13.8	674.78	7.7864
12:44:19	1264.86	107	1482	393	48	813	871	18.34	2.12	0.64	8.18	6.17	0.41	18.74	674.92	7.7947
12:44:49	1264.98	106	1423	397	5	863	721	14.93	2.01	0.61	8.09	6.39	1.77	16.57	675.06	7.803
12:45:19	1265.21	107	1426	398	58	848	865	18.77	2.13	0.72	7.82	6.63	0.62	26.46	675.26	7.8113

DOE high power mortar test Amaco Catoosa Test Site

TIME	RHT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	RPM	G's	G's	KIPS	KIPS	KIPS	FT/HR	Oned	CRBT
12:48:42	1285.28	104	1068	302	-41	-38	24	20.13	1.8	0.40	7.46	7.39	2.86	11.64	875.53	7.8203
12:48:18	1285.31	107	1037	300	-41	-33	19	21.28	1.81	0.29	7.5	7.39	0.3	4.04	875.57	7.8228
12:48:46	1285.41	107	1123	308	-41	-21	38	18.5	1.84	0.38	7.39	7.64	2.94	11.88	875.47	7.8243
12:47:15	1285.63	107	1241	308	-42	-25	32	16.03	1.81	0.21	7.57	7.76	0.41	13.82	875.57	7.8227
12:47:46	1285.82	107	1328	300	-42	-36	34	18.92	1.78	0.17	7.87	7.73	0.31	16.52	875.68	7.8209
12:48:18	1285.73	107	1235	309	-42	-33	19	18.94	1.8	0.18	7.86	7.8	0.43	12.81	875.77	7.8206
12:48:49	1285.83	107	1287	308	-43	-28	24	16.84	1.8	0.18	7.96	7.73	0.34	14.63	875.9	7.8178
12:49:15	1285.99	108	1242	308	-41	-33	20	16.98	1.8	0.19	7.93	7.86	0.31	15.86	876.03	7.8161
12:49:46	1286.11	106	1366	307	-41	-35	35	18.98	1.81	0.19	7.82	7.88	0.34	15.37	876.18	7.8144
12:50:18	1286.24	107	1389	300	-42	-25	32	18.97	1.8	0.19	7.82	7.88	0.48	18.84	876.28	7.8127
12:50:49	1286.37	108	1257	306	-41	-21	35	18.07	1.81	0.32	7.52	7.73	0.41	16.05	876.43	7.809
12:51:19	1286.49	108	1267	304	-40	-28	20	18.07	1.81	0.19	7.61	7.86	0.34	18.84	876.56	7.8073
12:51:49	1286.71	105	1360	304	-40	-30	16	18.96	1.8	0.19	7.5	7.71	0.36	21.87	876.78	7.8077
12:52:19	1286.83	108	1317	302	-40	-36	26	18.15	1.83	0.26	7.44	7.61	0.34	20.63	876.87	7.8028
12:52:49	1287.13	106	1303	307	-40	-33	21	18.98	1.81	0.18	7.8	7.68	0.36	22.4	877.18	7.8023
12:53:19	1287.31	108	1292	287	-40	-28	20	18.1	1.82	0.32	7.39	7.84	0.31	22.82	877.38	7.8026
12:53:49	1287.48	107	1298	308	-39	-28	30	18.11	1.81	0.3	7.48	7.64	0.31	21.87	877.54	7.8013
12:54:19	1287.67	108	1300	308	-38	-25	38	18.17	1.81	0.18	7.48	7.68	0.38	22.12	877.77	7.8006
12:54:49	1287.86	106	1356	307	-38	-21	36	18.1	1.85	0.37	7.48	7.68	0.41	23.88	877.91	7.8078
12:55:19	1288.08	108	1308	302	-38	-31	32	18.11	1.81	0.18	7.47	7.71	0.41	23.45	878.11	7.8061
12:55:49	1288.26	107	1312	300	-40	-28	36	18.11	1.81	0.22	7.47	7.64	0.34	22.85	878.3	7.8044
12:56:19	1288.48	108	1305	307	-38	-28	26	18.11	1.8	0.3	7.47	7.64	0.43	25.5	878.51	7.8027
12:56:49	1288.64	106	1303	307	-40	-29	30	18.09	1.81	0.21	7.48	7.64	0.34	21.88	878.68	8.001
12:57:19	1288.81	108	1378	307	-38	-28	26	18.07	1.81	0.2	7.5	7.86	0.34	19.17	878.85	8.0003
12:57:48	1288.87	107	1364	300	-40	-30	28	18.08	1.81	0.18	7.53	7.86	0.31	18.42	879.01	8.0176
12:58:19	1289.11	107	1263	300	-40	-20	24	18.03	1.81	0.2	7.58	7.9	0.33	17.92	879.16	8.0208
12:58:49	1289.29	107	1266	298	-39	-25	28	18.03	1.83	0.24	7.53	7.78	0.38	17.31	879.21	8.0243
12:59:19	1289.43	107	1307	290	-40	-14	31	17.71	2.17	0.81	6.83	6.99	0.32	19.17	879.47	8.0426
12:59:49	1289.56	107	1345	308	-38	-21	32	18.84	1.82	0.28	7.73	7.9	0.38	17.17	879.58	8.0511
13:00:19	1289.72	108	1271	307	-38	-25	24	18.85	1.82	0.2	7.72	7.88	0.31	19.13	879.78	8.0696
13:00:48	1289.87	107	1365	309	-38	-28	24	18.85	1.81	0.2	7.73	7.85	0.34	17.86	879.82	8.0878
13:01:19	1309	107	1281	300	-40	-20	24	18.86	1.78	0.18	7.73	7.85	0.3	16.13	880.05	8.0761
13:01:48	1309.28	108	1388	308	-41	-25	24	18.64	1.83	0.27	7.89	7.83	0.31	27.2	880.24	8.0847
13:02:19	1309.47	107	1348	301	-41	-25	26	18.65	1.85	0.27	7.83	7.84	0.43	28.95	880.32	8.0927
13:02:49	1309.72	107	1379	308	-41	-33	20	18.88	1.87	0.38	7.89	7.78	0.41	30.48	880.78	8.101
13:03:19	1309.87	108	1368	307	-40	-29	20	18.99	1.86	0.31	7.86	7.78	0.33	30.28	881.02	8.1078
13:03:48	1301.22	108	1403	325	-40	-29	20	18	1.86	0.32	7.67	7.73	0.43	38.05	881.37	8.1148

DOE high power motor test Amaco Catoosa Test Site

Well No. 23	Date: 026/98	Bit Type =	Water based mud	Motor MPM84	
Starting Depth =	1331.27	Bit Size =	4.75		
Ending Depth =	1352.14	Bit Pressure =	5, 9, 12, 12		
Total Depth Drilled =	20.87	Mud Type =	Water Based		
Spurs On Bit =	6.53	Mud Weight (lb/gal) =	8.00		
Average ROP =	53.72	Pipe (ft) =	862.65	Cable (ft) =	426.68
Drilling (ft) =	1077.91				

TIME	BIT DEPTH	FLOW	PRSS	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	ft-lbs	ft-lbs	KIPS	KIPS	KIPS	FT/HR	Drift	Count
12:04:32	1351.47	109	1403	384	-40	-29	20	18.01	1.85	0.3	7.39	7.73	0.6	38.94	681.93	8.1213
12:04:34	1351.73	107	1397	386	-42	-25	22	18.87	1.99	0.38	7.6	7.76	0.38	39.3	681.75	8.1258
12:04:36	1351.97	106	1327	392	-32	-33	20	15.6	1.84	0.28	7.66	7.82	0.38	28.34	681.96	8.1271
12:05:29	1353.08	109	1378	393	-41	-35	20	15.84	1.81	0.2	7.75	7.6	0.41	17.74	682.14	8.1284
12:06:59	1352.21	108	1380	392	-41	-35	32	15.64	1.81	0.21	7.72	7.92	0.38	17.97	682.95	8.1337
12:08:28	1352.57	108	1279	392	-40	-29	34	16.66	1.81	0.18	7.7	8	0.38	18.5	682.92	8.132
12:08:58	1352.89	107	1393	398	-32	-33	20	15.9	1.85	0.3	7.86	7.88	0.34	21.31	682.0	8.1353
12:09:29	1352.71	107	1270	390	-42	-35	30	15.97	1.81	0.25	7.69	7.85	0.35	18.38	682.76	8.1378
12:09:59	1352.85	108	1356	391	-42	-29	34	15.64	1.82	0.23	7.72	7.95	0.41	17.01	682.91	8.1372
12:08:28	1353.54	107	1268	391	-42	-33	28	15.69	1.88	0.36	7.87	8.05	1.38	19.41	683.08	8.1358
12:08:59	1353.28	105	1423	382	-38	-25	30	14.75	1.69	0.43	8.22	8.67	0.6	34.21	683.11	8.1327
12:09:29	1353.61	106	1430	398	-38	-29	20	14.78	1.65	0.47	8.71	9	0.45	36.43	683.95	8.1356
12:09:44	1353.79	107	1499	399	-38	-26	24	14.83	1.84	0.43	8.74	8.95	0.62	38.68	683.82	8.1361
12:10:12	1354.04	107	1428	395	-38	-29	26	14.71	1.86	0.33	8.79	9.02	0.3	32.21	684.05	8.1339
12:10:30	1354.28	106	1438	397	-38	-26	24	14.79	1.92	0.42	8.77	8.88	0.48	37.83	684.11	8.1305
12:10:52	1354.51	108	1548	384	-37	-25	38	14.65	1.96	0.5	8.61	9	0.93	85.29	684.98	8.1334
12:11:22	1354.7	108	1331	398	-37	-17	38	14.66	1.85	0.29	8.88	8.97	0.38	22.05	684.74	8.1434
12:11:47	1354.95	107	1397	390	-37	-17	38	14.79	1.8	0.39	8.72	8.13	1.15	38.08	684.99	8.1502
12:11:56	1355.2	107	1437	348	-37	-35	29	15.28	1.84	0.27	8.3	8.99	0.63	36.3	685.24	8.1528
12:12:36	1355.45	107	1443	349	-37	-25	29	15.18	1.82	0.22	8.43	8.69	0.6	46.23	685.46	8.1537
12:12:51	1355.7	106	1498	365	-37	-29	18	15.02	1.94	0.42	8.54	8.99	0.66	60.38	685.78	8.15
12:12:57	1355.81	107	1348	391	-38	-20	34	14.71	1.80	0.29	8.89	8.95	0.43	25.75	685.88	8.1503
12:13:21	1356.09	109	1297	393	-38	-25	20	14.95	1.81	0.23	8.6	8.65	0.29	19.91	686.13	8.1566
12:13:51	1356.32	108	1299	393	-38	-25	23	14.95	1.84	0.23	8.91	8.67	0.34	47.82	686.27	8.1649
12:14:21	1356.57	107	1328	391	-38	-25	28	14.88	1.82	0.21	8.99	9.13	0.41	18.35	686.42	8.1682
12:14:43	1356.62	107	1391	393	-37	-25	34	14.78	1.99	0.53	8.8	9.02	0.62	33.92	686.87	8.1667
12:15:18	1356.84	108	1389	393	-38	-25	29	14.7	1.86	0.3	8.85	9.05	0.31	28.24	688.88	8.1608
12:15:48	1357.05	106	1345	391	-36	-35	30	14.7	1.84	0.28	8.85	9.14	0.48	24.81	687.58	8.1718
12:16:48	1357.29	107	1357	390	-36	-25	30	14.72	1.89	0.29	8.93	8.98	0.38	29.49	687.35	8.1728
12:16:49	1357.5	108	1448	387	-18	770	770	16.58	2.22	0.45	8.88	9.77	7.78	29.13	687.95	8.1806
12:17:18	1357.62	107	1169	391	-38	-17	38	17.92	1.86	0.31	8.62	8.39	5.48	13.86	687.87	8.1822
12:17:48	1357.96	107	1387	398	-35	-21	24	15.49	1.87	0.32	8.11	8.35	0.5	26.05	687.61	8.1808
12:18:18	1358.02	109	1277	392	-35	-25	20	15.34	1.82	0.25	8.2	8.35	0.31	19.23	688.07	8.1868
12:18:48	1358.18	107	1308	389	-38	-25	20	15.38	1.88	0.25	8.17	8.35	0.34	18.52	688.23	8.1874
12:19:18	1358.42	107	1382	389	-38	-25	20	15.84	1.87	0.33	8.1	8.23	0.62	28.78	689.46	8.1787
12:19:39	1358.67	105	1458	386	-38	-28	30	15.9	1.88	0.44	7.94	8.16	0.53	34.11	688.71	8.1893
12:19:57	1358.92	108	1471	385	-35	-28	18	15.89	1.93	0.43	7.89	8.14	0.62	54.26	688.97	8.1928

DOE high power mortar test Amoco Catoba Test Site

DOE high power mortar test Amoco Catoba Test Site																	
Well No. 23	Date: 2/29/98																
Starting Depth =	1301.27	Bit Type = Walker McDonald MP 504															
Ending Depth =	1302.14	Bit Size = 4.75															
Total Depth Drilled =	350.67	Bit Nozzle = 5, 8, 12, 15															
Hours On Bit =	0.53	Mud Type = Water Based															
Average ROP =	53.72	Mud Weight (lb/gal) = 8.06															
Drilling Rate =	1071.36	Pipe (in) = 662.68															
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours	
HR:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	K-lbs	#-lbs	KIPS	Gr	lb's	KIPS	KIPS	KIPS	FT/HR	ONBIT	OnBit	
13:20:02	1300.17	108	1429	317	-35	-25	20	15.78	1.9	0.33	7.70	8	0.03	81.75	689.22	8.368	
13:20:16	1300.42	108	1320	393	-36	-25	18	15.69	1.61	0.2	7.86	8.09	0.3	64.03	689.48	8.3917	
13:20:34	1300.67	109	1282	306	-36	-22	20	15.59	1.61	0.29	7.96	8.23	0.28	51.78	689.71	8.3968	
13:20:52	1300.92	107	1537	390	-36	-25	20	15.88	1.85	0.28	7.89	8.33	0.5	48.19	689.97	8.4018	
13:21:11	1310.17	107	1388	391	-36	-25	24	15.90	1.93	0.26	7.90	8.16	0.48	48.84	690.22	8.4069	
13:21:34	1310.42	109	1301	369	-37	-35	35	15.48	1.61	0.24	6.96	8.38	0.6	39.39	690.48	8.4138	
13:21:50	1310.67	108	1309	370	-38	-29	18	15.62	1.82	0.22	7.82	8.14	0.43	58.91	690.74	8.4178	
13:22:03	1310.92	106	1474	388	-38	-25	24	15.74	1.86	0.3	7.81	8	0.41	70.43	690.97	8.4213	
13:22:19	1311.17	106	1446	397	-40	-23	18	15.64	1.81	0.19	7.98	8.09	0.46	70.49	691.23	8.425	
13:22:37	1311.42	107	1397	360	-38	-25	34	15.67	1.63	0.24	7.87	8.09	0.45	57.4	691.48	8.4288	
13:22:42	1311.67	107	1377	388	-40	-29	18	15.73	1.8	0.16	7.99	8.07	0.56	79.18	691.72	8.4324	
13:22:59	1311.92	106	1448	387	-39	-29	29	15.71	1.64	0.39	7.84	8.09	0.5	64.02	691.97	8.4381	
13:23:07	1312.17	106	1501	388	-38	-26	20	15.8	1.83	0.25	7.95	7.94	0.36	80.84	692.21	8.4433	
13:23:16	1312.42	105	1515	391	-29	-29	20	15.81	1.63	0.29	7.79	7.95	0.23	89.48	692.48	8.4422	
13:23:39	1312.67	106	1524	394	-39	-29	19	15.82	1.92	0.23	7.71	8	0.5	77.78	692.73	8.4456	
13:23:48	1312.92	107	1458	388	-39	-17	21	15.67	1.91	0.36	7.86	8.14	0.38	68.02	692.98	8.448	
13:23:57	1313.17	106	1408	387	-39	-21	38	15.69	1.69	0.36	7.88	8.11	0.48	61.11	693.23	8.4538	
13:24:12	1313.42	106	1482	397	-38	-25	20	15.69	1.85	0.28	7.88	8.04	0.41	63.13	693.47	8.4573	
13:24:39	1313.67	107	1482	395	-39	-29	24	15.7	1.87	0.29	7.99	8.02	0.39	70.92	693.72	8.4608	
13:24:39	1313.92	109	1468	397	-29	-29	20	15.71	1.67	0.33	7.82	8.14	0.33	64.71	694	8.4648	
13:24:52	1314.18	107	1452	399	-30	-29	35	15.7	1.68	0.35	7.94	8.02	0.38	88.1	694.23	8.4682	
13:25:05	1314.43	107	1467	389	-38	-28	20	15.69	1.87	0.33	7.85	8.04	0.48	69.62	694.47	8.472	
13:25:19	1314.68	107	1421	386	-39	-29	20	15.69	1.83	0.29	7.84	8.01	0.41	68.39	694.72	8.476	
13:25:33	1314.93	107	1442	393	-38	-29	18	15.68	1.84	0.27	7.86	7.98	0.5	90.03	694.98	8.4803	
13:25:55	1315.18	109	1485	398	-40	-29	35	15.85	1.67	0.31	7.96	8.08	0.5	85.98	695.23	8.4837	
13:26:22	1315.43	107	1598	390	-38	-29	20	15.43	1.69	0.32	8.08	8.21	0.5	83.08	695.49	8.4886	
13:26:37	1315.68	108	1478	389	-38	-23	18	15.63	1.67	0.39	7.8	8.09	0.39	66.32	695.73	8.4937	
13:26:55	1315.93	108	1451	385	-36	-29	22	15.9	1.96	0.27	7.94	8.28	0.5	61.36	695.98	8.5000	
13:27:06	1316.18	108	1482	391	-38	-29	20	15.85	1.96	0.3	7.88	8.11	0.45	63.65	696.23	8.5063	
13:28:27	1317.2	105	1282	385	7	0.13	699	18.43	1.99	0.24	3.77	4.9	0.4	49.63	697.47	8.5149	
13:33:46	1317.45	107	1399	393	-23	-21	20	17.05	1.66	0.3	5.13	8.23	4.38	47.31	697.49	8.52	
13:33:57	1317.7	109	1785	377	-34	-25	48	13.57	1.98	0.42	8.66	8.84	1.84	89.13	697.74	8.5282	
13:34:50	1317.95	108	1975	379	-38	-25	18	12.68	1.92	0.45	8.57	8.84	0.56	96.97	697.98	8.5338	
13:34:58	1318.2	104	1914	381	-33	-25	26	12.57	1.94	0.42	8.68	8.88	0.6	91.47	698.24	8.5388	
13:34:58	1318.41	109	1898	385	-17	0.10	692	17.33	2.36	1.11	4.68	10.89	13.05	25.88	698.46	8.5386	
13:35:04	1318.66	109	1447	323	-33	-21	20	17.08	1.83	0.22	5.11	6.47	1.69	67.34	698.71	8.5385	
13:36:12	1319.91	104	1581	378	-33	-28	18	16.04	1.91	0.31	6.17	6.37	0.93	83.16	698.97	8.5421	

DOE high power mortar test Amaco Cataoca Test Site

Well No. 23		Date: 2/26/99		BH Type = Walker McDonald MPBH		BH Size = 2.75		BH Nozzles = 3, 8, 12, 12		Mud Type = Water Based		Mud Weight (lb/gal) = 8.00		Pump (RPM) = 862.00		Collar (RPM) = 400.00	
TIME	BH DEPTH	FLOW	PRESS	SPEED	TORQUE	PEAR	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours	
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	Gr	Gr	KIPS	KIPS	KIPS	FT/HR	OnBH	OnBH	
13:55:23	1019.17	109	1592	376	-32	-38	48	18.13	1.87	0.3	8.08	8.27	0.43	84.02	689.23	8.5462	
13:55:33	1019.43	105	1573	382	-33	-35	45	18.13	1.85	0.26	8.08	8.3	0.43	88.09	689.46	8.5472	
13:55:43	1019.67	100	1514	354	-35	-25	35	16	1.98	0.28	8.2	8.53	0.72	84.8	689.71	8.5515	
13:56:00	1019.92	109	1587	365	-34	-38	48	18.01	1.9	0.35	8.19	8.50	0.67	87.45	689.97	8.5552	
13:56:08	1020.17	109	1585	382	-33	-41	50	18.14	1.88	0.33	8.06	8.25	0.58	92.65	700.23	8.5578	
13:56:21	1020.43	102	1575	368	-34	-35	40	18.13	1.87	0.27	8.07	8.32	0.49	78.42	700.48	8.561	
13:56:33	1020.67	100	1507	358	-33	-25	35	18.04	1.92	0.38	8.17	8.37	0.41	74.56	700.71	8.5644	
13:56:44	1020.92	108	1605	365	-34	-35	45	18.00	1.98	0.41	8.19	8.12	3.11	80.20	700.95	8.5676	
13:56:58	1021.17	104	1700	375	-34	-28	38	18.71	1.89	0.32	8.51	8.79	0.98	88.25	701.22	8.5719	
13:57:16	1021.43	104	1854	388	-17	810	647	18.37	3.53	0.98	5.83	10.65	3.24	53.24	701.47	8.5753	
13:57:28	1021.67	105	1828	383	-33	-25	35	18.54	1.83	0.24	5.86	5.86	0.45	75.43	701.72	8.5786	
13:57:39	1021.92	106	1518	365	-34	-25	35	18.55	1.83	0.24	5.85	5.82	0.38	80.34	701.98	8.5813	
13:57:50	1022.17	109	1520	385	-33	-25	35	18.56	1.83	0.23	5.92	5.84	5.44	87.27	702.23	8.5846	
13:58:01	1022.42	107	1518	365	-33	-25	35	18.5	1.83	0.21	5.8	5.79	0.38	81.83	702.47	8.5883	
13:58:11	1022.67	107	1487	388	-33	-38	43	18.69	1.83	0.28	5.81	5.88	0.45	85.75	702.72	8.5918	
13:58:24	1022.92	107	1425	381	-32	-25	35	18.5	1.84	0.2	5.7	5.86	0.45	88.83	702.98	8.5954	
13:58:37	1023.17	106	1461	387	-33	-25	35	18.47	1.85	0.38	5.73	5.84	0.41	88.04	703.21	8.5989	
13:58:51	1023.42	107	1485	385	-33	-28	38	18.45	1.91	0.35	5.78	5.84	0.38	88.88	703.46	8.6028	
13:59:10	1023.67	107	1402	385	-34	-21	24	18.35	1.92	0.34	5.83	6.2	0.65	58.38	703.72	8.6057	
13:59:40	1023.92	107	1387	391	-34	-25	35	18.35	1.83	0.25	5.86	6.3	0.45	21.80	703.98	8.6118	
14:00:16	1024.17	108	1318	383	-33	-28	38	18.15	1.83	0.39	5.86	6.32	0.48	19.04	704.16	8.6163	
14:00:48	1024.43	108	1345	382	-33	-21	20	18.15	1.89	0.38	6.03	6.2	0.50	19.87	704.23	8.6188	
14:01:09	1024.68	109	1445	385	-33	-21	24	18.29	1.86	0.38	5.8	6.15	0.61	38.95	704.47	8.6212	
14:01:18	1024.93	109	1604	385	-34	-17	38	18.7	1.86	0.33	5.40	5.74	0.47	88.2	704.74	8.6238	
14:01:36	1025.18	109	1583	385	-33	-13	36	18.84	1.92	0.33	5.58	5.85	0.35	83.76	704.97	8.6266	
14:01:41	1025.43	107	1598	389	-33	-13	36	18.53	1.88	0.29	5.86	5.84	0.29	73.61	705.24	8.6301	
14:01:56	1025.68	107	1502	388	-33	-21	30	18.38	1.91	0.35	5.72	5.84	0.45	80.78	705.47	8.6344	
14:02:00	1025.93	106	1614	382	-34	-25	35	18.52	1.92	0.32	5.67	5.84	0.38	68.87	705.73	8.6378	
14:02:28	1026.18	109	1515	385	-34	-29	38	18.5	1.9	0.39	5.69	5.85	0.34	88.9	705.98	8.6416	
14:02:35	1026.43	109	1521	385	-33	-21	24	18.83	1.91	0.31	5.87	5.94	0.5	68.48	706.22	8.6455	
14:02:48	1026.68	109	1478	382	-34	-21	20	18.47	1.91	0.31	5.72	5.80	0.38	65.51	706.47	8.6489	
14:03:03	1026.93	107	1476	388	-33	-21	39	18.3	1.88	0.29	5.7	5.80	0.38	64.14	706.73	8.6523	
14:03:28	1027.18	109	1429	391	-32	-21	30	18.31	1.87	0.26	5.87	6.1	0.57	42.81	706.98	8.6579	
14:03:53	1027.43	106	1374	382	-32	-21	20	18.21	1.85	0.25	5.87	6.15	0.41	37.33	707.21	8.6638	
14:04:25	1027.68	107	1893	390	-32	-21	38	15.19	1.82	0.32	7	7.48	1.8	24.14	707.41	8.6698	
14:04:50	1027.93	109	1452	385	-34	-17	24	14.91	1.88	0.28	7.33	7.47	0.41	38.07	707.66	8.6725	
14:05:17	1028.18	108	1454	385	-33	-21	29	14.91	1.87	0.27	7.39	7.44	0.38	34.04	707.9	8.6788	

DOE high power mortar test Amaco Cataoca Test Site

Well No. 23		Date: 2/25/98		BIT Type = Walker McDonald MPDSM		BIT Size = 4.75		BIT Nozzles = 3, 8, 12, 12		Mud Type = Water Based		Mud Weight (ppg) = 9.00		Pipe ID = 6.625		Color (Hr) = 4/3.68	
TIME	BIT DEPTH	FLOW	PRESS	SPEED	TORQUE	PEAK	DLT	HOCK	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Feet	Hours	
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	Gr	Gr	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit	
14:08:43	1328.11	107	1482	388	-30	-21	20	14.82	1.83	0.26	7.27	7.47	0.48	51.43	708.16	8.7171	
14:08:43	1328.28	107	1425	390	-30	-21	16	14.85	1.87	0.27	7.3	7.47	0.38	51.54	708.41	8.7201	
14:08:43	1328.59	107	1427	391	-30	-21	16	14.88	1.84	0.26	7.31	7.47	0.38	51.5	708.63	8.7234	
14:07:09	1328.84	107	1437	398	-30	-21	20	14.89	1.87	0.3	7.29	7.47	0.38	51.54	708.80	8.7412	
14:07:37	1329.09	107	1425	391	-21	-21	20	14.90	1.82	0.23	7.29	7.47	0.41	51.49	709.14	8.7402	
14:08:03	1329.34	107	1458	398	-30	-23	30	14.94	1.92	0.34	7.25	7.47	0.45	51.44	709.4	8.7368	
14:08:22	1329.59	106	1495	387	-31	-13	36	14.98	1.88	0.28	7.7	8.23	1.15	48.99	709.68	8.7518	
14:08:36	1329.84	106	1500	385	-32	-13	41	14.97	1.89	0.31	8.02	8.23	0.59	52.5	709.99	8.7601	
14:08:58	1330.09	104	1561	380	-21	-17	20	14.99	1.89	0.3	8	8.21	0.41	62.02	710.15	8.7701	
14:09:18	1330.34	105	1568	383	723	1494	1052	14.98	1.91	0.37	8.64	8.28	0.83	58.24	710.39	8.777	
14:09:30	1330.6	106	1537	369	945	1028	154	14.93	1.91	0.41	8.09	8.23	0.5	48.49	710.63	8.7821	
14:09:55	1330.85	105	1508	389	809	875	135	14.09	1.87	0.51	8.14	8.43	0.82	45.53	710.89	8.7876	
14:10:19	1331.1	106	1517	386	852	1036	207	14.07	2.85	1.91	8.16	8.14	1.77	38.89	711.16	8.7943	
14:10:47	1331.35	107	1517	388	865	851	154	14.07	2.68	1.82	8.18	8.17	1.82	40.4	711.39	8.8003	
14:11:03	1331.6	108	1539	388	812	1044	215	14.12	2.12	0.58	8.1	8.03	1.41	43.03	711.64	8.8058	
14:11:19	1331.85	107	1598	388	824	1000	159	14.15	1.81	0.41	8.27	8.33	0.53	52.13	711.89	8.8138	
14:11:39	1332.1	105	1672	384	945	1105	302	14.23	1.94	0.64	8.01	8.01	0.57	58.56	712.14	8.8191	
14:11:57	1332.35	105	1571	384	935	1108	287	14.2	1.94	0.67	8.03	8.31	0.69	57.17	712.39	8.8194	
14:12:08	1332.6	105	1624	384	989	1137	343	14.32	1.89	0.57	7.91	8.19	0.57	72.73	712.63	8.8228	
14:12:14	1332.85	104	1688	388	1017	1085	128	14.4	1.82	0.4	7.83	8.11	0.59	79.25	712.9	8.826	
14:12:28	1333.1	106	1672	383	1005	1073	134	14.58	1.82	0.39	7.85	8.11	0.57	88.14	713.16	8.8291	
14:12:38	1333.35	106	1685	386	1006	1150	327	14.36	1.82	0.4	7.85	8.11	0.62	88.88	713.39	8.833	
14:12:46	1333.6	104	1714	378	1067	1141	156	14.47	1.82	0.36	7.78	8.03	0.5	88.83	713.64	8.8348	
14:12:58	1333.85	104	1698	371	1028	1130	158	14.41	1.7	0.41	7.81	8.29	0.72	88.38	713.9	8.8374	
14:13:07	1334.1	105	1718	382	1065	1137	154	14.42	1.87	0.4	7.81	8.11	0.55	81.98	714.15	8.8406	
14:13:17	1334.35	105	1742	383	1075	1175	213	14.4	1.86	0.44	7.82	8.14	0.67	89.23	714.4	8.8434	
14:13:27	1334.6	104	1747	378	1093	1144	211	14.43	1.87	0.45	7.82	8.07	0.8	88.79	714.64	8.8463	
14:13:38	1334.85	104	1789	378	1093	1173	182	14.44	1.95	0.5	7.78	8.03	0.88	87	714.89	8.8483	
14:13:47	1335.1	104	1795	379	1080	1179	207	14.42	1.84	0.43	7.81	8.07	0.87	82.28	715.16	8.8517	
14:13:58	1335.35	103	1785	381	1075	1174	199	14.38	1.84	0.4	7.78	8.07	0.55	84.14	715.39	8.8548	
14:14:09	1335.6	103	1748	382	1042	1100	300	15.14	1.86	0.42	7.78	8	0.42	108.26	715.63	8.8577	
14:14:18	1335.85	107	1584	391	817	973	158	16.4	1.82	0.36	8.82	8.68	0.55	87.38	715.9	8.8601	
14:14:28	1336.1	107	1575	391	822	982	178	16.39	1.82	0.38	8.83	8.68	0.5	78.91	716.18	8.8632	
14:14:41	1336.35	108	1385	383	766	927	259	18.09	1.5	0.37	8.18	8.43	0.89	38.15	716.39	8.8658	
14:14:53	1336.6	105	1477	382	800	815	306	18.25	1.85	0.31	8.88	8.68	0.48	62.12	716.67	8.8718	
14:15:04	1336.85	105	1475	384	800	823	300	18.26	1.84	0.32	8.98	8.55	0.58	65.18	716.92	8.8773	
14:15:14	1337.1	105	1448	385	835	838	280	18.2	1.89	0.31	8.91	8.44	0.51	63.82	717.15	8.8815	

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	GELT	HOOK	PEAK	DELTA	WDB	PEAK	DELTA	ROP	Feet	Meters
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	MIPS	FT/HR	OnBit	OnBit
14:18:04	1337.31	102	1356	332	732	846	234	15.89	2.17	0.79	0.22	0.70	0.93	24.2	717.36	8.5886
14:18:30	1337.58	107	1411	290	777	874	174	15.87	1.92	0.34	0.14	0.34	0.42	31.22	717.8	8.5936
14:18:55	1337.61	107	1384	351	751	821	122	16.03	1.89	0.3	0.18	0.36	0.45	31.09	717.96	8.5936
14:19:18	1338.38	106	1441	307	813	804	154	16.13	1.91	0.39	0.27	0.37	0.6	42.83	718.1	8.5936
14:19:31	1338.31	107	1472	358	838	894	134	16.19	1.89	0.39	0.22	0.37	0.63	57.17	718.36	8.5942
14:19:47	1338.66	107	1434	326	858	918	164	16.25	1.92	0.34	0.28	0.27	0.57	57.17	718.61	8.595
14:19:50	1338.61	108	1503	387	870	850	142	16.29	1.94	0.4	0.34	0.18	0.53	68.03	718.65	8.5929
14:19:16	1339.38	108	1458	395	847	961	211	16.31	1.93	0.37	0.30	0.37	0.67	59.04	718.72	8.5928
14:19:48	1339.25	107	1390	351	793	842	190	16.39	2.28	1.03	0.22	0.75	0.96	27.33	718.94	8.5936
14:19:16	1339.45	108	1323	334	658	716	85	16.51	2.24	0.89	0.3	0.77	1.03	33.72	719.5	8.5951
14:19:46	1339.6	108	1327	335	678	716	85	16.54	2.23	0.84	0.27	0.77	1.05	33.14	719.65	8.5944
14:20:16	1339.77	108	1300	394	713	761	87	16.55	2.17	0.93	0.23	0.82	1.13	33.53	719.81	8.5937
14:20:48	1340.51	108	1362	393	730	850	169	16.62	2	0.85	0.18	0.61	0.74	39.36	720.68	8.595
14:21:04	1340.26	107	1450	340	827	851	211	16.14	1.89	0.33	0.30	0.3	0.57	33.23	720.3	8.5932
14:21:32	1340.51	108	1485	380	841	807	180	16.2	1.91	0.41	0	0.23	0.65	31.36	720.88	8.5951
14:21:35	1340.78	108	1489	385	857	827	170	16.26	1.92	0.4	0.24	0.2	0.57	30.37	720.8	8.5948
14:21:51	1341.51	105	1463	384	858	910	170	16.21	1.93	0.38	0.30	0.37	0.57	37.57	721.05	8.5951
14:22:03	1341.26	107	1441	368	812	906	174	16.13	1.92	0.35	0.27	0.37	0.62	43.98	721.32	8.5953
14:22:29	1341.69	108	1329	394	693	834	219	16.66	1.92	0.35	0.23	0.43	0.57	29.88	721.54	8.5955
14:22:59	1341.81	108	1275	336	651	882	84	16.69	1.89	0.3	0.3	0.7	0.07	15.37	721.87	8.5979
14:23:39	1341.75	109	1277	397	651	863	87	16.6	1.87	0.3	0.26	0.51	0.02	15.72	721.6	8.5952
14:24:03	1341.89	108	1276	395	650	794	99	16.6	1.89	0.3	0.26	0.46	0.38	17.58	721.89	8.5943
14:24:28	1342.03	108	1264	356	647	709	105	16.5	1.89	0.31	0.23	0.51	0.43	38.38	722.07	8.5928
14:25:00	1342.26	107	1361	338	731	856	283	16.52	2.2	0.99	0.17	0.89	1.38	28.31	722.31	8.5941
14:25:28	1342.51	108	1407	358	752	892	154	16.1	1.91	0.31	0.19	0.33	0.46	44.89	722.57	8.5956
14:25:49	1342.76	107	1420	389	812	951	190	16.12	1.92	0.38	0.28	0.48	0.53	45.87	722.8	8.5958
14:26:07	1343.51	108	1463	398	851	919	130	16.15	1.89	0.31	0.21	0.35	0.48	49.7	723.06	8.5974
14:26:21	1343.26	108	1462	398	874	931	99	16.22	1.9	0.31	0.27	0.32	0.57	53.1	723.31	8.5974
14:26:58	1343.81	108	1499	390	800	947	140	16.24	1.89	0.33	0.25	0.31	0.61	63.38	723.56	8.5984
14:27:50	1343.76	105	1489	382	879	975	327	16.24	1.89	0.34	0.24	0.25	0.83	63.81	723.8	8.5986
14:27:14	1344.51	107	1372	350	758	878	163	16.53	1.91	0.23	0.18	0.30	0.5	36.90	724.07	8.5977
14:27:39	1344.37	107	1428	385	815	871	271	16.1	1.90	0.35	0.19	0.38	2.47	38.46	724.32	8.5985
14:27:58	1344.52	108	1434	386	835	871	189	14.48	1.88	0.34	0.71	0	0.6	54.14	724.54	8.5979
14:28:12	1344.77	108	1435	387	814	883	146	14.54	1.88	0.36	0.66	0.65	0.46	58.11	724.83	8.5984
14:28:27	1345.03	108	1472	385	841	1032	178	14.58	1.91	0.32	0.64	0.68	0.43	63.21	725.08	8.5984
14:28:39	1345.27	104	1620	378	889	1080	142	14.67	1.92	0.34	0.53	0.8	0.32	73.21	725.31	8.5988
14:28:53	1345.53	108	1376	333	808	1146	490	14.59	1.89	0.35	0.6	0.69	0.49	72.93	725.56	8.5993

DOE high power mortar test Amasco Calcoosa Test Site

TIME	DEPTH FEET	FLOW GPM	FREQ PSI	SPEED RPM	TORQUE FT-LBS	PEAK FSS	DELT FSS	HOOK LOAD KIPS	PEAK GS	DELTA %E	WOB KIPS	SEAN KIPS	DELTA KIPS	WOB FT/KR	FEET CORR	MORTAR CSH
12:28:23	1343.76	107	1403	301	746	801	103	13.28	2.41	0.89	7.52	8.76	1.88	23.93	725.81	9.173
12:28:25	1343.97	108	1389	303	757	797	117	14.26	2.34	1.18	7.52	8.83	1.07	25.08	726.84	9.158
12:28:27	1344.14	107	1366	301	753	797	52	14.28	2.24	0.84	7.48	8.76	1.79	23.39	726.21	9.1363
12:28:29	1344.31	107	1348	407	754	1085	405	14.31	2.38	1.16	7.66	8.76	1.7	25.3	728.46	9.1305
12:28:31	1344.47	105	1336	416	860	797	256	14.30	2.31	1.07	7.03	8.79	1.88	26.13	728.33	9.1484
12:28:33	1344.74	108	1362	403	743	813	196	14.26	2.4	1.4	7.03	8.83	1.26	26.09	728.76	9.1531
12:28:35	1344.91	108	1338	407	753	817	199	14.24	2.3	1.43	7.05	8.83	1.8	30.39	728.91	9.1616
12:28:37	1345.08	108	1348	408	853	801	258	14.26	2.58	1.58	7.03	8.76	1.61	20.62	727.92	9.1897
12:28:39	1345.25	108	1348	406	883	813	224	14.30	2.38	1.2	7.42	8.79	2.03	16.1	727.31	9.1775
12:28:41	1345.42	107	1363	403	759	838	216	14.28	2.06	1.7	7.01	8.79	1.8	16.86	727.45	9.1963
12:28:43	1345.59	108	1362	407	716	813	184	14.28	2.53	1.43	7.81	8.86	1.79	23.83	727.83	9.1966
12:28:45	1345.76	108	1359	392	824	13	20	14.3	1.87	1.3	2.98	15.63	0.68	34.46	727.81	9.2146
12:28:47	1345.93	108	1334	396	840	15	26	14.42	1.5	1.62	8.83	17.13	0.38	31.84	728.06	9.2328
12:28:49	1346.10	105	1334	397	88	-6	36	14.26	1.86	0.27	8.17	15.38	0.43	34.77	728.36	9.2515
12:28:51	1346.27	108	1451	389	717	1247	1204	14.3	1.34	1.21	8.11	10.17	1.84	37.7	728.48	9.2368
12:28:53	1346.44	106	1511	385	685	1036	307	14.4	2.18	0.96	8.05	8.84	1.36	48.1	728.74	9.2195
12:28:55	1346.61	108	1459	397	926	926	222	14.3	2.08	0.98	8.04	9.57	2.32	41.96	728.88	9.253
12:28:57	1346.78	105	1511	393	863	180	14.43	1.61	1.91	0.38	8.03	8.39	0.6	32.31	729.23	9.2558
12:28:59	1346.95	108	1525	395	840	156	14.43	1.91	1.91	0.84	8.03	8.81	0.83	48.78	729.48	9.2413
12:29:01	1347.12	105	1527	394	895	375	174	14.64	1.93	0.4	8.91	8.33	0.59	53.57	729.77	9.2858
12:29:03	1347.29	108	1543	387	878	378	22	14.43	1.98	0.43	8.03	8.21	0.24	48.11	728.88	9.2711
12:29:05	1347.46	107	1651	398	813	910	170	14.37	2.93	1.23	8.03	10.15	1.91	36.89	730.36	9.2772
12:29:07	1347.63	108	1601	390	332	871	216	14.67	2.28	1.13	8.08	10.23	2.06	40.3	730.49	9.2736
12:29:09	1347.80	108	1471	396	674	883	267	14.35	3.81	1.23	8.13	10.84	2.19	34.25	730.77	9.2917
12:29:11	1347.97	108	1552	394	843	1036	39	14.46	2.06	0.85	8.03	9.77	1.51	25.15	730.86	9.2983
12:29:13	1348.14	108	1549	385	888	1316	483	14.45	2.25	1.81	8	11.13	1.84	35.37	731.24	9.3011
12:29:15	1348.31	105	1633	387	911	1020	186	14.46	1.97	0.88	8.08	8.24	0.45	40.37	731.46	9.3103
12:29:17	1348.48	108	1549	394	965	1079	193	14.52	1.99	0.33	8.03	8.13	0.48	60.25	731.74	9.3103
12:29:19	1348.65	104	1652	391	1096	1329	201	14.33	1.94	0.31	8.03	8.62	0.86	62.67	731.99	9.314
12:29:21	1348.82	108	1751	370	690	1329	313	14.03	1.83	0.31	8.08	8.05	0.57	86.13	732.26	9.3172
12:29:23	1348.99	104	1802	378	1137	1343	336	14.13	1.84	0.34	8.02	8.85	0.58	67.06	732.46	9.3132
12:29:25	1349.16	108	1838	376	1159	1359	315	14.16	1.89	0.41	8.23	8.04	0.57	84.66	732.73	9.3258
12:29:27	1349.33	108	1784	390	1036	1356	404	14.12	2.01	0.48	8.33	8.37	0.62	102.84	733	9.3434
12:29:29	1349.50	108	1841	392	831	843	182	13.79	2.57	1.33	8.08	11.38	0.71	86.89	733.28	9.3518
12:29:31	1349.67	108	1867	393	779	838	113	13.65	2.87	1.87	8.76	11.48	2.61	28.94	733.41	9.4011
12:29:33	1349.84	107	1450	391	771	829	193	13.69	2.78	1.88	8.77	11.81	2.42	27.77	733.71	9.3454
12:29:35	1349.98	107	1483	388	818	1036	304	13.71	2.77	1.65	8.71	11.13	2.54	36.63	733.93	9.3765

Column 10 = 400.08

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HCOR LOAD	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	Depth	Cost
14:38:52	1354.15	105	1558	384	805	883	138	13.85	2.27	1.02	8.6	10.58	1.09	88.89	734.2	8.388
14:39:07	1354.4	105	1555	383	1008	1170	318	13.97	1.56	0.53	9.47	8.98	0.51	89.87	734.45	8.388
14:39:17	1354.65	105	1709	381	1007	1210	189	14.1	2.04	0.56	9.35	9.68	1.01	89.32	734.73	8.388
14:39:27	1354.9	104	1518	385	1131	1251	251	14.14	1.67	0.48	9.3	9.74	0.54	89.13	734.95	8.3757
14:39:37	1355.15	104	1610	385	1111	1273	273	14.16	2.04	0.58	9.3	9.88	1.32	88.8	735.22	8.3756
14:39:46	1355.4	103	1502	377	1105	1125	211	14.18	1.27	0.53	9.29	8.85	0.67	103.91	735.45	8.3762
14:39:57	1355.65	103	1782	388	1082	1210	267	14.19	1.82	0.43	9.38	9.67	0.88	85.85	735.7	8.379
14:40:07	1355.9	103	1774	384	1081	1188	188	14.28	1.84	0.44	9.35	9.72	0.67	85.8	735.95	8.3818
14:40:20	1356.15	108	1651	394	958	1125	264	13.95	1.94	0.44	9.49	8.74	0.67	83.13	736.2	8.3858
14:40:34	1356.41	107	1692	389	1003	1188	328	13.94	1.81	0.44	9.47	10.1	0.93	83.75	736.45	8.3886
14:40:46	1356.66	105	1690	388	871	1083	210	13.98	1.81	0.4	9.46	9.72	0.57	80.53	736.7	8.3825
14:40:58	1356.91	105	1689	389	1035	1199	325	14.04	1.95	0.42	9.48	9.72	0.57	72.75	736.95	8.3856
14:41:08	1357.16	103	1768	377	1060	1234	312	14.09	1.93	0.36	9.35	9.67	0.68	81.36	737.21	8.3891
14:41:18	1357.41	104	1615	378	1128	1285	280	14.17	1.9	0.34	9.27	9.79	0.77	90.66	737.46	8.4017
14:41:28	1357.66	105	1765	383	1075	1182	312	14.06	1.91	0.38	9.35	9.69	0.98	85.68	737.72	8.4048
14:41:38	1357.91	107	1578	388	875	1084	262	13.89	2.42	1.48	8.81	10.8	2.11	84.67	737.95	8.4081
14:41:48	1358.16	108	1518	382	830	921	162	13.75	2.45	1.4	9.7	10.7	1.81	88.56	738.2	8.416
14:41:58	1358.41	108	1523	383	830	982	182	13.74	2.47	1.38	9.7	10.78	2.03	80.6	738.46	8.4228
14:42:08	1358.66	108	1518	383	828	888	109	13.74	2.4	1.25	9.7	10.89	2.01	86.84	738.7	8.4291
14:42:21	1358.91	107	1576	381	899	1188	405	13.82	2.3	1.22	8.62	10.87	2.13	89.88	738.95	8.4368
14:42:31	1359.16	104	1742	379	696	1185	263	14.11	1.64	0.45	9.59	8.84	0.67	92.1	739.2	8.4388
14:42:41	1359.41	105	1798	383	1113	1255	283	14.16	1.89	0.44	9.27	9.67	0.69	88.99	739.45	8.4415
14:42:55	1359.66	105	1626	384	1115	1323	229	14.2	1.89	0.47	9.24	9.8	0.72	106.2	739.72	8.4488
14:43:08	1359.91	104	1642	378	1144	1238	170	14.24	1.85	0.42	9.2	9.48	0.67	108.04	739.95	8.4564
14:43:18	1360.16	105	1768	383	1108	1104	182	14.16	1.84	0.39	9.29	9.88	0.77	89.37	740.21	8.4628
14:43:17	1360.42	103	1830	377	1150	1288	178	14.24	1.99	0.48	9.2	9.62	0.72	112.89	740.47	8.4582
14:43:28	1360.67	104	1801	378	1111	1322	323	14.18	1.86	0.5	9.26	9.85	0.68	89.75	740.74	8.4638
14:43:37	1360.92	105	1985	381	1018	1200	285	14.00	1.95	0.52	9.4	9.77	0.61	80.58	740.98	8.457
14:43:45	1361.17	106	1883	385	992	1213	459	13.99	1.86	0.5	9.44	9.91	0.76	88.81	741.24	8.4684
14:43:51	1361.42	105	1723	383	1048	1128	182	14.1	1.95	0.43	9.34	9.63	0.65	79.24	741.46	8.4835
14:43:57	1361.67	105	1935	383	841	1012	243	13.8	1.97	0.43	9.34	9.81	0.89	56.79	741.71	8.4881
14:44:06	1361.92	108	1482	384	796	858	361	13.66	2.64	1.66	9.74	10.8	1.88	31.82	741.95	8.4761
14:44:14	1362.17	108	1483	383	831	868	313	13.88	2.68	1.71	9.74	10.7	1.8	31.88	742.23	8.4838
14:44:37	1362.42	107	1521	381	847	943	179	13.76	2.05	1.59	9.81	10.58	1.7	29.91	742.48	8.4902
14:44:57	1362.67	107	1528	381	891	981	117	13.83	2.5	1.45	9.8	10.38	1.88	36.39	742.71	8.4956
14:45:12	1362.92	107	1579	383	893	1013	166	13.89	1.84	0.44	9.84	9.84	0.53	59.31	742.97	8.4996
14:45:31	1363.17	106	1535	381	896	1030	186	13.84	1.87	0.39	9.81	9.48	0.48	46.85	743.23	8.5051

DOE high power mortar test Amaco Catonsa Test Site

TIME HH:MM:SS	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE FT-LBS	PEAK FT-LBS	DELTA FT-LBS	HOOK LOAD KIPS	PEAK G'S	DELTA G'S	WOB KIPS	PEAK KIPS	DELTA KIPS	ROP FT/HR	Feet Drift	Hours OnBit
14:57:52	1383.42	109	1400	398	834	1200	343	18.78	2.8	2.02	9.69	10.28	1.72	42.89	743.47	9.5111
14:58:20	1383.07	109	1417	395	797	854	147	19.36	2.96	2.5	10.18	11.3	2.3	31.84	743.72	9.5188
14:58:50	1383.89	109	1470	398	787	250	105	15.08	3.11	2.8	10.35	11.42	1.08	26.84	743.84	9.5271
14:59:17	1384.34	110	1464	399	804	854	98	15.08	3.2	2.63	10.35	11.55	1.2	33.75	744.19	9.5346
14:59:47	1384.4	110	1484	399	805	874	122	13.08	3.1	2.79	10.35	11.23	1.68	30.37	744.44	9.5425
15:00:12	1384.05	109	1480	399	834	898	139	13.11	3.07	2.72	10.32	11.35	2.39	32.3	744.68	9.5501
15:00:35	1384.0	108	1492	392	828	894	117	13.11	3.00	2.69	10.32	11.38	1.98	38.71	744.84	9.5584
15:01:02	1385.15	109	1479	394	819	878	117	13.08	3.13	2.68	10.34	11.11	1.83	32.48	745.16	9.5641
15:01:29	1385.4	108	1473	395	818	874	97	13.08	3.2	2.88	10.35	11.2	1.86	35.32	745.45	9.5712
15:01:54	1385.05	108	1485	392	843	850	134	13.1	3.1	2.86	10.32	11.22	1.82	35.94	745.68	9.5781
15:02:20	1385.0	108	1483	393	832	886	122	13.08	3.24	2.87	10.34	11.47	2.08	33.89	745.96	9.5856
15:02:45	1386.15	108	1485	393	836	878	93	13.08	3.3	3	10.34	11.37	1.8	30.9	746.16	9.5924
15:03:15	1386.4	107	1473	391	826	874	109	13.08	3.3	2.94	10.36	11.2	1.68	30	746.44	9.5998
15:03:43	1386.05	107	1463	393	818	882	106	13.08	3.36	3.18	10.37	11.37	2.01	32.32	746.68	9.6062
15:04:12	1386.0	107	1475	391	828	890	122	13.08	3.34	3.12	10.36	11.32	1.77	30.68	746.94	9.6135
15:04:40	1387.15	107	1474	390	831	898	113	13.07	3.35	3.14	10.35	11.39	1.89	32.14	747.16	9.6202
15:05:06	1387.4	107	1461	388	814	874	100	13.04	3.31	3.18	10.37	11.32	1.84	32.36	747.48	9.6272
15:05:36	1387.63	107	1460	391	815	870	101	13.05	3.32	3.09	10.37	11.38	3.04	27.63	747.68	9.6343
15:06:06	1387.88	107	1469	391	823	878	101	13.05	3.26	2.98	10.37	11.58	2.23	32.02	747.92	9.6403
15:06:35	1388.13	108	1465	392	818	884	130	13.05	3.33	3.41	10.38	11.63	3.54	31.08	748.17	9.6463
15:07:05	1388.38	108	1475	395	818	888	117	13.06	3.17	3.05	10.38	11.59	2.27	30.38	748.42	9.6546
15:07:31	1388.63	109	1476	393	824	870	86	13.06	3.24	3.13	10.38	11.54	2.13	34.42	748.68	9.6615
15:08:01	1388.87	108	1444	393	806	858	93	13.06	2.95	2.84	10.35	11.68	1.39	29.18	748.91	9.6681
15:08:28	1389.13	108	1473	391	822	888	80	13.05	3.22	2.94	10.37	11.3	1.77	34.53	749.17	9.6748
15:08:57	1389.38	107	1462	391	815	868	98	13.05	3.28	2.94	10.38	11.54	2.3	31.75	749.44	9.6826
15:09:26	1389.63	107	1466	390	822	878	105	13.05	3.32	2.94	10.38	11.3	1.82	30.95	749.69	9.6900
15:09:52	1389.88	107	1463	390	814	878	117	13.05	3.09	2.81	10.39	11.2	1.58	33.92	749.92	9.6971
15:10:21	1379.13	108	1451	393	815	862	97	13.06	3.03	2.81	10.38	11.35	1.98	31.48	750.17	9.7041
15:10:47	1379.38	107	1472	391	828	868	123	13.06	3.18	3.7	10.34	11.5	1.77	35.54	750.42	9.7122
15:11:14	1379.63	108	1488	398	817	868	101	13.06	3.06	2.5	10.34	11.2	1.63	32.74	750.67	9.7194
15:11:41	1379.88	109	1466	396	814	879	106	13.06	2.83	2.88	10.34	11.54	1.38	33.01	750.94	9.7274
15:12:07	1371.13	108	1488	396	820	874	102	13.08	2.86	2.81	10.34	11.23	1.66	34.57	751.19	9.7348
15:12:36	1371.38	109	1473	390	830	868	134	13.08	2.94	2.22	10.34	11.04	1.34	32.38	751.43	9.7423
15:13:01	1371.63	108	1462	388	840	854	162	13.07	3.02	2.85	10.33	11.08	1.48	35.34	751.68	9.7498
15:13:26	1371.88	108	1469	395	820	882	100	13.07	2.88	3.2	10.34	11.11	1.48	35.36	751.93	9.7578
15:13:53	1372.13	108	1444	398	817	874	97	13.06	2.67	1.63	10.34	10.63	1.61	33.78	752.18	9.7651
15:14:17	1372.38	108	1442	394	823	882	113	13.07	1.89	0.37	10.32	10.75	0.85	37.34	752.43	9.7717

DOE high power motor test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	MOTOR LOAD	PEAK	DELTA	MOR	PEAK	DELTA	RCP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	%	%	KIPS	KIPS	KIPS	FT/HR	GPH	On/Off
15 14:42	1372.63	108	1447	304	828	878	97	13.08	1.89	0.98	10.32	10.87	0.75	30.66	752.89	9.7915
15 15:09	1372.85	109	1463	303	858	915	113	13.09	2.01	2.19	10.31	11.2	1.89	40.8	752.93	9.7978
15 15:28	1373.13	107	1489	301	851	896	109	13.07	2.04	2.22	10.32	11.32	1.84	37.02	753.17	9.8043
15 15:54	1373.56	107	1499	301	857	923	128	13.07	2.08	2.08	10.33	11.32	1.84	35.91	753.45	9.8110
15 16:19	1373.63	108	1493	303	921	898	139	13.09	2.08	2.08	10.34	11.11	1.48	39.77	753.69	9.8186
15 16:49	1373.84	110	1461	308	735	825	146	12.97	2.28	0.89	10.42	10.72	0.77	24.82	753.88	9.8265
15 17:19	1374.03	108	1501	304	777	874	169	13.98	2.03	2.19	10.41	11.2	1.66	32.79	754.07	9.8351
15 17:43	1374.26	107	1489	300	854	890	168	13.07	2.08	2.12	10.33	11.61	2.42	37.82	754.33	9.8417
15 18:08	1374.63	107	1493	308	857	857	201	13.07	2.70	2.15	10.33	11.89	1.84	38.98	754.58	9.8481
15 18:39	1374.79	107	1515	305	878	883	178	13.11	2.7	1.87	10.39	11.32	1.82	44.4	754.83	9.8548
15 18:56	1375.03	108	1518	308	879	1000	213	11.08	2.60	2.29	11.74	13.26	1.84	35.03	755.08	9.862
15 19:19	1375.26	105	1530	304	912	1058	163	11.93	2.82	2.27	12.48	13.88	2.8	38.24	755.33	9.8686
15 19:41	1375.63	108	1533	306	855	855	184	11.04	2.88	2.08	12.37	12.89	2.78	36.8	755.58	9.8749
15 20:07	1375.79	105	1573	307	911	1049	201	11.04	3.07	2.49	12.36	14.27	3.42	31.89	755.82	9.8821
15 20:28	1376.03	105	1634	308	818	1173	231	11.05	3.19	3.46	12.25	14.34	3.57	40.99	756.05	9.8872
15 20:50	1376.26	107	1624	309	888	1177	305	10.98	3.29	2.76	12.42	14.15	3.33	34.74	756.32	9.8944
15 21:22	1376.41	109	1412	306	792	855	339	10.87	2.82	2.25	13.53	18.14	1.72	48.99	756.46	9.9003
15 21:52	1376.63	108	1448	303	828	890	382	10.80	2.44	1.44	13.46	19	0.88	28.25	756.69	9.9113
15 22:23	1376.78	109	1338	305	713	850	269	12.46	3.08	0.59	10.94	12.73	2.51	17.64	756.85	9.9166
15 22:52	1376.86	109	1368	308	694	749	361	12.8	1.99	0.36	10.58	12.88	0.57	2.4	756.9	9.9279
15 23:23	1376.93	108	1307	352	765	871	332	12.82	2.37	1.15	10.58	13.11	1.17	8.67	756.97	9.9362
15 23:48	1377.18	107	1503	309	870	1054	199	12.99	2.88	2.48	10.48	13.49	1.8	37.97	757.23	9.9428
15 24:14	1377.43	109	1408	306	794	858	211	13.81	3.17	0.64	10.37	10.88	0.81	32.38	757.48	9.9508
15 24:44	1377.88	108	1339	304	738	895	324	12.74	2.89	0.67	10.84	10.82	0.4	17.58	757.69	9.9588
15 25:18	1377.7	104	1463	308	691	788	358	12.7	1.32	0.37	10.88	10.89	0.66	18.28	757.75	9.9674
15 25:44	1377.9	107	1484	303	705	835	384	12.8	2.89	2.44	10.58	11.71	2.08	23.28	757.85	9.9754
15 26:07	1378.15	107	1497	300	856	835	430	12.99	2.76	2.08	10.49	11.9	2.43	38.49	758.2	9.982
15 26:31	1378.4	108	1502	302	856	916	480	12.57	2.72	1.94	10.47	11.73	2.37	38.83	758.46	9.9883
15 27:01	1378.56	109	1353	307	737	890	251	12.79	2.56	1.71	10.93	11.23	1.44	32.35	758.64	9.9969
15 27:27	1378.84	107	1468	308	640	843	190	13.89	3.87	3.03	10.52	13	4.67	34.3	758.88	10.0041
15 27:52	1379.09	107	1464	308	830	895	123	12.88	2.36	2.66	10.48	11.87	3.71	39.24	759.19	10.0111
15 28:18	1379.34	108	1483	302	825	923	180	12.87	2.18	2.91	10.51	13.59	1.99	38.01	759.58	10.0176
15 28:33	1379.59	108	1338	416	809	780	307	17.19	2.84	2.39	8.69	11.85	1.75	34.3	759.83	10.0266
15 28:54	1379.75	107	1385	417	729	761	184	14.02	2.81	3.22	8.83	13.42	3.13	33.38	759.9	10.0349
15 29:21	1379.65	105	1401	412	728	787	196	14.95	2.48	1.4	8.87	13.01	2.58	27.25	760.04	10.0432
15 29:51	1380.17	108	1381	420	846	740	194	10.88	2.52	1.76	9.94	11.58	1.85	27.15	760.21	10.0515
15 30:21	1380.24	107	1277	419	596	543	130	13.92	2.7	2.11	9.82	13.28	3.66	3.88	760.31	10.0609

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23		Date: 3/26/98		Bit Type =		Weaker McGonigle MP-8841											
Starting Depth =		1331.21		Bit Size =		4.75											
Ending Depth =		1382.14		Bit Nozzles =		8, 9, 12, 12											
Total Depth Drilled =		50.93		Mud Type =		Water Based											
Hours On Bit =		6.53		Mud Weight (lb/cu ft)		9.01											
Average ROP =		53.72		Purge (ft)		692.58		Cutter (ft) =		608.88							
Drilling (ft) =		1973.36															
TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours	
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	RPS	ft-lbs	ft-lbs	KIPS	RIPS	RIPS	FT/HR	OnBit	OnBit	
15:36:57	1380.20	107	1283	423	529	635	89	13.9	2.86	2.52	9.09	11.81	3.09	6.31	780.54	10.0864	
15:36:59	1380.32	107	1289	419	591	631	61	10.86	3.05	2.76	10.01	11.65	3.51	3.25	780.38	10.0867	
15:36:59	1380.54	107	1294	419	636	843	85	13.75	2.99	2.58	10.14	11.75	3.54	2.01	780.38	10.0868	
15:37:27	1380.56	107	1293	423	630	1198	843	13.66	2.94	2.63	10.24	12.11	4.05	1.35	780.41	10.0870	
15:37:50	1380.8	105	1374	411	814	1029	1040	13.43	3.1	2.37	10.46	11.85	2.82	51.25	780.68	10.1014	
15:38:20	1380.75	106	1431	397	-8	-9	24	10.36	2.79	2.21	10.1	11.5	1.58	17.05	780.8	10.1087	
15:38:50	1380.76	107	1332	391	-17	-5	30	13.3	2.73	1.97	10.45	11.44	1.77	4.25	780.83	10.1138	
15:39:29	1380.81	108	1328	392	-8	-8	30	13.26	2.7	1.83	10.6	11.58	2.05	3.48	780.85	10.1183	
15:39:59	1380.84	107	1330	388	-36	3	30	13.23	2.81	1.99	10.69	11.81	2.21	3.69	780.81	10.1206	
15:40:30	1380.86	107	1340	394	-17	4	30	13.67	2.83	2.19	10.62	11.78	3.2	3.33	780.81	10.1236	
15:40:50	1380.88	107	1382	399	-17	-5	24	13.61	2.84	2.27	10.60	11.83	1.94	2.26	780.82	10.1243	
15:41:29	1380.9	106	1374	387	-20	-5	24	13	2.87	2.11	10.89	11.69	1.7	2.85	780.86	10.1266	
15:41:59	1380.93	106	1414	388	-25	-8	20	13	3.03	2.99	10.88	11.48	1.83	3.57	780.89	10.1291	
15:42:20	1380.92	105	1469	345	139	1433	1458	13.03	3.83	4.22	10.54	14.29	7.75	-0.32	781.00	10.1294	
15:42:30	1381.1	107	1426	348	20	493	522	13.1	3.27	3.48	10.78	13.81	8.81	21.78	781.36	10.1347	
15:43:29	1381.15	107	1353	391	-10	-5	30	13.61	2.76	2.21	10.86	13.54	2.35	3.14	781.2	10.1393	
15:43:54	1381.16	107	1337	385	-24	-9	20	13.01	2.83	1.87	10.87	12.99	2.42	3.33	781.23	10.2013	
15:44:24	1381.18	107	1328	393	-14	-1	28	13	2.87	1.87	10.87	12.23	2.78	1.93	781.24	10.2038	
15:44:30	1381.18	107	1327	394	-14	7	41	13	2.82	1.68	10.87	12.23	2.73	0.92	781.34	10.2176	
15:45:30	1381.2	104	1332	393	-14	-8	20	13	2.6	1.74	10.87	12.28	2.82	1.76	781.38	10.2263	
15:45:59	1381.19	107	1318	394	246	1093	1116	13	2.92	2.47	10.85	12.66	3.05	7.07	781.28	10.2348	
15:46:29	1381.21	108	1309	393	346	733	746	13	3.04	2.86	10.87	12.84	3.78	6.84	781.28	10.2422	
15:46:30	1381.23	107	1321	390	-15	-9	24	13	3.13	2.67	10.87	11.89	2.18	1.87	781.28	10.2513	
15:47:30	1381.25	104	1321	394	-15	-8	20	13	3.09	3.19	10.87	11.94	2.19	0.33	781.29	10.2626	
15:48:30	1381.18	108	1323	425	414	1522	1546	13	3.44	3.87	10.87	12.97	4.4	-8	781.39	10.2681	
15:48:30	1381.18	107	1318	438	721	797	136	12.89	3.59	3.83	11.18	13.92	5.05	2.38	781.29	10.2764	
15:48:59	1381.21	107	1337	443	747	621	761	13.41	3.57	3.96	11.46	13.0	4.52	3.89	781.29	10.2847	
15:49:30	1381.23	107	1359	444	736	825	148	12.42	3.73	4	11.88	13.52	4.28	2.67	781.29	10.2939	
15:49:59	1381.27	106	1408	442	805	1024	385	12.64	3.54	3.7	11.44	13.26	3.95	5.26	781.33	10.3013	
15:50:30	1381.28	105	1405	430	779	983	320	12.47	3.12	2.85	11.41	13.2	4.33	12.74	781.43	10.3066	
15:50:59	1381.41	107	1317	446	695	742	409	12.43	3.08	2.74	11.43	13.67	4.64	3.57	781.46	10.3179	
15:51:29	1381.44	107	1321	443	699	757	381	12.82	3.1	2.75	11.45	13.74	4.67	3.11	781.49	10.3262	
15:51:59	1381.48	107	1321	446	688	757	384	13.47	3.15	2.77	11.46	13.67	4.84	2.8	781.5	10.3345	
15:52:29	1381.46	108	1315	446	686	769	389	13.43	3.13	2.8	11.49	13.74	4.72	2.39	781.56	10.3409	
15:52:59	1381.5	108	1310	446	679	748	394	13.41	3.2	2.88	11.48	13.67	4.72	2.97	781.59	10.3514	
15:53:30	1381.52	107	1311	447	673	744	339	12.41	3.17	3.04	11.46	13.67	4.82	3.86	781.64	10.3587	
15:53:59	1381.54	107	1315	447	672	740	338	12.41	3.15	2.98	11.46	13.61	5.08	3.28	781.61	10.3681	

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Feet	Hours
HOURS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	PS	PS	KIPS	KIPS	KIPS	FT/HP	CoM	CoM
15:54:20	1381.58	508	1334	448	889	787	134	12.42	3.2	2.9	11.44	13.84	4.5	2.45	761.81	10.3784
15:54:50	1381.58	507	1456	445	830	2543	2137	13.5	3.61	3.33	11.36	13.67	4.83	3.28	761.88	10.3847
15:55:20	1381.58	508	1358	451	878	1324	856	12.72	3.1	2.54	11.14	13.45	5.38	11.51	761.74	10.3935
15:55:50	1381.71	507	1303	446	865	756	183	12.54	3.25	3.05	11.35	13.45	4.43	3.13	761.77	10.4013
15:56:20	1381.73	507	1288	447	858	732	180	12.59	3.24	3.15	11.38	13.48	4.62	2.93	761.76	10.4050
15:56:50	1381.75	508	1293	449	847	716	142	13.88	3.25	3.05	11.35	13.48	4.62	2.21	761.83	10.4128
15:57:20	1381.77	508	1308	448	883	734	156	12.53	3.36	3.42	11.31	13.48	4.52	3.48	761.83	10.4202
15:57:50	1381.79	508	1309	449	888	730	134	13.53	3.36	3.54	11.35	13.52	4.57	2.52	761.86	10.4255
15:58:20	1381.82	508	1342	448	884	744	150	12.59	3.23	2.95	11.38	13.53	4.31	3.22	761.88	10.4314
15:58:50	1381.84	507	1314	447	883	740	150	12.52	3.14	2.9	11.34	13.58	4.38	2.5	761.88	10.4344
15:59:20	1381.86	507	1307	448	888	736	128	12.52	3.48	3.26	11.33	13.38	4.31	2.83	761.91	10.4397
15:59:50	1381.88	508	1308	449	889	734	134	12.53	3.13	2.89	11.33	13.33	4.31	2.87	761.95	10.4462
16:00:20	1381.9	508	1362	451	842	754	142	12.83	3.25	3.04	11.35	13.49	4.45	2.98	761.95	10.4763
16:00:50	1381.91	505	1290	481	833	704	138	12.52	3.25	3.13	11.34	13.48	4.52	1.42	761.87	10.4848
16:01:20	1381.83	508	1293	449	834	712	142	12.52	3.15	2.87	11.34	13.48	4.57	3.32	762.05	10.4926
16:01:50	1381.86	507	1286	447	830	706	134	12.53	3.36	3.18	11.38	13.45	4.45	2.84	762.02	10.5013
16:02:20	1381.98	507	1287	447	834	688	150	12.51	3.25	3.15	11.34	13.5	4.48	2.18	762.02	10.5096
16:02:50	1381.97	507	1278	445	823	704	150	12.51	3.22	3.14	11.34	13.6	4.78	0.58	762.02	10.5179
16:03:20	1381.98	507	1279	446	821	684	150	12.51	3.23	2.84	11.34	13.57	4.73	1.27	762.04	10.5262
16:03:50	1381.96	507	1291	446	823	684	126	12.51	3.17	2.95	11.34	13.52	4.52	1.41	762.04	10.5345
16:04:20	1382	508	1286	448	828	695	150	12.5	3.1	2.95	11.38	13.55	4.72	1.14	762.06	10.5431
16:04:50	1382.02	508	1289	449	834	700	146	12.5	3.12	2.98	11.38	13.62	4.75	1.41	762.06	10.5514
16:05:20	1382.03	508	1293	449	834	683	138	12.5	3.22	3.12	11.38	13.55	4.78	1.63	762.06	10.5597
16:05:50	1382.04	507	1288	448	825	688	142	12.5	3.17	3.08	11.38	13.5	4.68	1.04	762.1	10.5683
16:06:20	1382.05	507	1290	447	830	685	154	12.5	3.18	3.01	11.34	13.55	4.91	1.88	762.1	10.5763
16:06:50	1382.06	507	1286	447	828	688	130	12.5	3.25	3.03	11.34	13.55	4.48	1.04	762.12	10.5848
16:07:20	1382.07	507	1288	448	825	682	138	12.48	3.38	3.03	11.36	13.63	4.57	1.51	762.12	10.5928
16:07:50	1382.08	508	1292	449	824	688	139	12.5	3.14	3.01	11.34	13.58	4.76	1.85	762.15	10.6012
16:08:20	1382.1	508	1294	448	822	688	139	12.49	3.09	3.11	11.36	13.62	4.31	1.36	762.15	10.6098
16:08:50	1382.11	507	1282	447	825	680	117	12.5	3.34	3.43	11.34	13.68	5.12	1.74	762.17	10.6178
16:09:20	1382.12	507	1292	447	824	696	126	12.49	3.14	3.28	11.34	13.67	5.07	1.1	762.17	10.6264
16:09:50	1382.14	508	1298	450	822	688	122	12.5	3.31	3.24	11.34	13.68	5.07	3.71	762.2	10.6347

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HCOR	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hour
HR:MM:SS	FEET	GPM	PSI	RPM	Lbs	Lbs	Lbs	KIPS	G/s	G/s	KIPS	KIPS	KIPS	FT/HR	CON	CON
7:46:20	1382.4	103	1213	385	90	108	24	11.45	1.93	0.23	7.14	13.24	19.48	21.88	782.45	10.6477
7:46:30	1382.41	103	1269	383	92	104	20	11.81	1.93	0.28	10.14	13.14	19.38	1.85	782.45	10.6477
7:47:00	1382.44	110	1408	401	314	1333	1250	11.72	1.7	3.87	10.24	12.57	5.17	14.12	782.51	10.6477
7:48:20	1382.45	104	1415	395	81	104	20	11.48	3.31	2.32	10.49	12.47	4.97	1.88	782.51	10.6477
7:48:30	1382.47	110	1417	393	91	104	24	11.47	3.05	2.61	10.49	12.42	3.65	1.25	782.51	10.6477
7:48:40	1382.47	110	1423	400	92	104	24	11.46	3.1	2.64	10.48	12.5	4.09	0.84	782.53	10.6477
7:48:50	1382.48	108	1418	397	92	104	28	11.47	3.18	2.6	10.48	12.5	4	1.41	782.53	10.6477
7:49:00	1382.49	108	1407	396	94	104	20	11.47	2.99	2.52	10.48	12.18	3.89	1.03	782.57	10.6477
7:50:00	1382.5	111	1401	402	92	104	24	11.48	3.12	2.78	10.48	12.4	3.88	1	782.57	10.6477
7:50:30	1382.52	109	1396	397	94	108	26	11.48	3.15	2.64	10.47	12.3	4.17	3.86	782.57	10.6477
7:51:00	1382.52	110	1398	399	94	104	24	11.46	2.68	2.48	10.47	12.4	3.9	0.56	782.57	10.6477
7:52:00	1382.53	110	1401	399	95	108	28	11.5	2.91	2.37	10.48	12.23	3.76	0.6	782.57	10.6477
7:52:30	1382.54	109	1394	394	94	108	32	11.5	3.04	2.6	10.48	12.34	4.36	1.2	782.59	10.6477
7:53:00	1382.55	109	1397	393	95	108	24	11.5	3.04	2.63	10.48	12.45	4.09	1.22	782.61	10.6477
7:53:30	1382.56	110	1403	398	96	108	28	11.51	2.97	2.52	10.44	12.25	3.78	1.05	782.61	10.6477
7:54:00	1382.56	110	1409	399	94	108	38	11.51	3.01	2.42	10.44	12.25	3.69	0.84	782.61	10.6477
7:54:30	1382.57	109	1410	397	96	108	38	11.51	3.06	2.6	10.44	12.25	3.65	0.78	782.64	10.6477
7:55:00	1382.58	108	1418	396	95	108	38	11.53	2.85	2.45	10.43	12.26	3.88	0.73	782.64	10.6477
7:55:30	1382.59	110	1422	395	95	112	20	11.52	2.84	2.39	10.43	12.3	3.8	1.01	782.64	10.6477
7:56:00	1382.59	109	1424	397	94	108	26	11.53	2.69	2.21	10.42	12.23	4.81	1.3	782.64	10.6477
7:56:30	1382.6	110	1420	401	94	104	24	11.52	2.67	2.25	10.42	12.16	3.54	0.82	782.64	10.6477
7:57:00	1382.61	110	1428	398	96	104	28	11.53	2.76	2.09	10.42	11.95	3.23	0.65	782.66	10.6477
7:57:30	1382.62	110	1430	401	95	104	26	11.52	2.93	2.11	10.42	12.18	3.73	1.44	782.68	10.6477
7:58:00	1382.63	104	1412	394	92	108	28	11.52	3	2.44	10.42	12.28	3.9	1.16	782.68	10.6477
7:58:30	1382.64	107	1413	399	94	108	28	11.52	2.91	2.39	10.42	12.14	3.26	1.58	782.68	10.6477
7:59:00	1382.66	108	1407	395	95	108	24	11.51	2.83	2.36	10.17	14.31	5.51	1.28	782.72	10.6477
8:00:00	1382.66	108	1408	394	96	106	26	11.51	2.83	1.71	10.04	14.22	2.59	1.57	782.72	10.6477
8:00:30	1382.67	108	1408	394	96	106	24	11.51	2.5	1.53	10.01	14.15	2.25	1.41	782.73	10.6477
8:01:00	1382.67	108	1410	395	95	108	28	11.51	2.91	1.88	13	14.1	2.27	3.29	782.74	10.6477
8:01:30	1382.68	109	1413	397	90	108	36	11.51	2.39	1.19	12.97	13.91	1.8	8.12	782.74	10.6477
8:02:00	1382.69	110	1422	399	95	108	28	11.52	2.64	1.54	12.93	14.1	2.23	3.49	782.81	10.6477
8:02:30	1382.7	110	1422	399	95	108	24	11.52	2.57	1.75	13	14.24	2.59	2.43	782.86	10.6477
8:03:00	1382.72	110	1422	399	95	108	24	11.52	2.57	1.75	13	14.24	2.59	2.43	782.86	10.6477
8:03:30	1382.73	109	1426	395	94	104	24	11.52	2.67	1.87	13	14.36	2.8	1.58	782.9	10.6477
8:04:00	1382.73	110	1429	398	92	108	24	11.52	2.68	1.81	12.95	14.38	2.82	1.73	782.9	10.6477
8:04:30	1382.75	108	1423	394	91	104	26	11.51	2.65	1.99	13	14.41	2.8	1.98	782.92	10.6477
8:04:50	1382.76	110	1427	401	91	104	28	11.51	2.66	1.78	13	14.31	2.68	2.14	782.92	10.6477

Well No. 23
 Date: 2/27/96
 Starting Depth = 1382.40
 Ending Depth = 1420.08
 Total Depth Drilled = 67.68
 Hours On Bit = 8.73
 Average ROP = 11.30
 Drilling Rate = 1419.89

Bit Type = Walker McDonald M808H
 Bit Size = 4.75
 Bit Nozzles = 9, 9, 12, 12
 Mud Type = Water Based
 Mud Weight (lbs/gal) = 8.00
 Pipe O.D. = 1010.22
 Collar I.D. = 998.60

DOE high power mortar test Amaco Caloosa Test Site

TIME	DEPTH	FLOW	FREQ	SPEED	TORQUE	PEAK	DELT	MCCR	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	RGI	RPM	ft-lbs	ft-lbs	ft-lbs	RPS	%	%	RPS	RPS	RPS	FT/HR	Depth	Used
8:24:20	1384.8	111	1400	403	1007	1121	186	10	3.74	3.69	13.95	14.57	4.74	5.04	764.88	11.2851
8:24:50	1384.8	111	1376	404	970	1044	126	9.99	3.94	3.9	11.90	14.20	5.07	3.5	764.88	11.2854
8:25:20	1384.87	110	1380	404	976	1080	130	9.96	3.98	3.82	11.90	14.19	4.84	4.06	764.71	11.2857
8:25:50	1384.79	111	1625	405	1187	1478	1890	10.07	4.55	5.25	11.87	14.1	4.57	13.46	764.86	11.2860
8:26:20	1385	110	1530	401	1188	1287	219	10.12	4.40	4.93	11.82	14.27	4.69	26.39	765.06	11.2863
8:26:50	1385.07	111	1453	405	1046	1182	178	10	3.39	3.08	11.95	13.79	4.09	7.94	765.12	11.2866
8:27:20	1385.13	110	1489	402	1120	1388	287	10.01	3.81	4.32	11.93	13.81	5.05	7.94	765.19	11.2869
8:27:50	1385.27	110	1560	401	1084	1214	198	10.02	4.55	5.54	11.92	14.34	4.98	12.64	765.28	11.2872
8:28:20	1385.38	111	1419	402	1012	1109	174	9.97	3.29	2.99	11.97	13.93	4.95	5.2	765.35	11.2875
8:28:50	1385.3	110	1383	401	972	1130	85	9.96	3.20	3.09	11.99	13.98	4.17	3.58	765.33	11.2878
8:29:20	1385.33	111	1376	404	936	1012	97	9.95	3.32	3.19	11.99	14.03	4.51	2.58	765.29	11.2881
8:29:50	1385.34	110	1369	398	852	890	81	9.95	3.39	3.3	11.99	13.91	4.07	1.56	765.29	11.2884
8:30:20	1385.35	110	1363	406	858	1000	85	9.94	3.42	3.21	12	14	4.26	1.8	765.49	11.2887
8:30:50	1385.39	111	1308	403	903	1012	83	9.93	3.49	3.45	12	13.93	4.07	2.8	765.43	11.2890
8:31:20	1385.4	110	1376	400	970	1012	89	9.94	3.45	3.18	12	13.96	4.14	2.94	765.45	11.2893
8:31:50	1385.43	109	1389	394	889	1048	109	9.94	3.46	3.27	12	13.93	4.03	2.89	765.48	11.2896
8:32:20	1385.49	109	1456	397	1099	1036	117	9.96	3.31	3.03	11.94	13.91	3.95	3.45	765.51	11.2899
8:32:50	1385.5	110	1413	398	1008	1099	142	9.95	3.04	2.89	11.98	13.78	3.97	4.5	765.54	11.2902
8:33:20	1385.56	110	1398	400	983	1091	178	9.96	3.29	3.00	11.98	13.93	4.21	5.86	765.59	11.2905
8:33:50	1385.59	110	1357	398	839	1032	162	9.94	3.68	3.69	11.99	14.12	4.9	4.41	765.64	11.2908
8:34:20	1385.61	111	1337	402	912	979	117	9.94	3.72	3.67	11.99	14.19	4.36	2.89	765.67	11.2911
8:34:50	1385.63	110	1362	400	903	1000	113	9.95	3.58	3.45	11.99	14.03	4.29	3.76	765.66	11.2914
8:35:20	1385.68	110	1328	398	940	1016	134	9.94	3.7	3.73	11.98	13.96	4.39	3.75	765.71	11.2917
8:35:50	1385.69	110	1358	399	925	992	109	9.94	3.7	3.59	11.99	14.09	4.39	3.05	765.75	11.2920
8:36:20	1385.72	110	1357	399	929	971	93	9.93	3.79	3.66	12	14	3.91	3.97	765.79	11.2923
8:36:50	1385.75	111	1383	403	923	963	109	9.94	3.78	3.74	11.99	13.93	4.12	3.16	765.78	11.2926
8:37:20	1385.75	109	1417	397	972	1000	130	9.96	3.89	3.29	11.98	13.78	3.85	3.47	765.82	11.2929
8:37:50	1385.84	110	1487	400	1005	1099	134	9.96	3.2	2.85	11.99	13.09	3.54	2.33	765.9	11.2932
8:38:20	1385.93	109	1570	398	1102	1425	436	10.02	3.89	4.09	11.9	14.46	5.03	11.18	766	11.2935
8:38:50	1385.98	109	1857	397	1197	1610	870	10.13	3.5	3.56	11.79	13.69	4.24	13.09	766.31	11.2938
8:39:20	1386.06	110	1399	398	1116	1307	198	10.09	3.78	2.68	11.89	13.24	2.88	24.02	766.43	11.2941
8:39:50	1386.07	109	1579	397	1110	1226	186	10.07	2.82	2	11.86	13.25	2.89	12.08	766.61	11.2944
8:40:18	1386.77	109	1587	398	1132	1243	223	10.07	2.81	1.94	11.84	13.24	2.92	13.98	766.82	11.2947
8:40:48	1386.84	109	1476	397	1074	1037	162	10	3.32	2.69	11.92	13.58	2.47	13.81	766.86	11.2950
8:41:18	1386.99	110	1478	400	1017	1085	181	9.99	3.18	2.67	11.94	13.6	3.49	13.71	767.04	11.2953
8:41:48	1387.19	109	1647	398	1168	1207	184	10.1	2.95	2.38	11.82	13.5	3.23	24.24	767.24	11.2956
8:42:18	1387.4	110	1578	400	1082	1308	304	10.05	2.77	3.88	11.85	13.38	3.03	25.42	767.46	11.2959

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE ft-lbs	PEAK ft-lbs	DELTA ft-lbs	HOOK LOAD KIPS	PEAK C%	DELTA C%	WOB KIPS	PEAK KIPS	DELTA KIPS	RDP FT/HR	Feet OnSt	Hours OnSt
Well No. 29	Date: 2/27/88															
Starting Depth =	1382.40															
Ending Depth =	1450.02															
Total Depth Drilled	67.62															
Hours On Bit =	8.72															
Average RDP =	11.80															
Drilling Bit =	1410.50															
Bit Type =	Wacker McDermold MP58H															
Bit Size =	4.75															
Bit Horzles =	8, 9, 12, 12															
Mud Type =	Water Based															
Mud Weight (lbs/gal)	8.04															
Pipe (in)	1.910.02															
Collar (ft)	400.00															
8:42:48	1387.62	111	1407	483	1122	1231	211	10.26	2.73	1.91	11.84	13.38	3.69	26.59	767.87	11.5288
8:43:18	1387.77	111	1481	402	1001	1145	271	9.9	3.42	3.12	11.92	13.69	3.61	17.98	767.65	11.5071
8:43:48	1387.51	109	1438	397	957	1133	263	9.98	3.68	3.22	11.88	13.72	3.73	4.75	767.58	11.6052
8:44:18	1388	100	1364	362	1103	1288	178	10.05	2.75	2.06	11.88	13.21	3.75	23.81	768.08	11.6127
8:44:48	1388.22	110	1553	461	1087	1347	251	10.66	2.95	2.43	11.85	13.69	2.78	28.5	768.27	11.622
8:45:18	1388.31	110	1418	402	958	1089	164	9.96	3.33	3.12	11.95	13.48	3.28	10.33	768.36	11.6303
8:47:01	1388.33	107	1288	291	937	1020	256	11.15	3.44	3.28	12.25	13.84	18.03	25.39	768.46	11.6449
8:47:31	1388.43	108	1301	282	959	1012	113	9.82	3.31	3.52	11.94	13.81	4.13	5.55	768.48	11.6532
8:48:01	1388.48	108	1358	293	948	1004	117	8.83	3.44	3.21	11.97	13.93	4.14	8.2	768.57	11.6615
8:48:31	1388.53	108	1352	294	940	1012	134	9.94	3.68	3.35	11.98	13.88	3.93	5	768.58	11.6658
8:49:01	1388.68	104	1571	358	1141	1215	159	10.06	3.1	2.68	11.84	13.56	3.62	16.02	768.73	11.6741
8:49:31	1388.93	104	1534	389	1102	1259	312	10.88	3.22	2.61	11.82	13.69	3.66	20.75	768.97	11.6864
8:50:01	1389.03	107	1389	393	957	1016	117	9.86	3.51	3.28	11.95	13.81	3.85	7.81	769.04	11.6938
8:50:31	1389.05	106	1302	362	980	1020	117	9.94	3.42	3.18	11.86	13.67	3.46	6.77	769.09	11.7003
8:51:01	1389.1	108	1371	362	968	1020	101	8.95	3.02	2.63	11.95	13.98	3.54	8.68	769.15	11.7118
8:51:31	1389.15	108	1362	344	959	908	87	9.65	3.13	2.88	11.86	13.79	3.97	8.06	769.21	11.7198
8:52:01	1389.18	108	1354	394	882	1012	129	9.94	3.18	2.78	11.96	13.68	3.81	4.84	769.28	11.7283
8:52:31	1389.25	108	1306	383	852	1058	142	9.88	3.15	2.51	11.95	13.57	3.52	7.83	769.3	11.7363
8:53:01	1389.44	107	1528	391	1092	1328	244	10.08	3	2.58	11.84	13.24	3.08	25.15	769.48	11.7445
8:53:31	1389.52	107	1481	391	1054	1154	162	10.22	3.03	2.81	11.88	13.22	3.04	15.78	769.63	11.7532
8:54:01	1389.7	108	1476	393	943	1125	150	10.27	3.13	2.95	11.98	13.28	3.88	13.34	769.78	11.7615
8:54:31	1389.75	107	1473	391	1018	1138	174	9.96	3.39	3.1	11.93	13.36	3.64	6.47	769.81	11.7698
8:55:01	1389.86	107	1557	399	1026	1168	148	10.02	2.67	2.36	11.97	13.32	2.54	15.56	769.95	11.7781
8:56:31	1390.13	107	1398	390	1177	1381	234	10.1	2.7	2.05	11.79	13.03	3.3	20.49	770.2	11.7867
8:58:01	1390.38	107	1389	281	1248	2941	1750	10.14	2.87	2.24	11.75	13.29	3.64	30.93	770.44	11.7947
8:58:31	1390.53	110	1378	402	964	1502	762	11.07	4.08	4.3	10.88	13.48	7.54	16.9	770.58	11.803
8:59:01	1390.62	109	1480	396	1074	1389	484	10.78	3.71	3.67	11.11	13.48	4.87	11.57	770.67	11.8113
8:59:31	1390.88	108	1514	294	1062	1205	216	10.84	3.57	3.48	11.08	13.17	4.69	26.87	770.9	11.8195
9:00:01	1390.89	113	1310	398	837	979	154	10.7	4.09	4.45	11.18	13.98	5.6	3.64	770.95	11.8279
9:00:31	1390.82	111	1280	403	877	937	183	10.13	4.31	4.69	11.79	14.55	6.76	3.53	770.98	11.8363
9:01:01	1390.82	108	1391	394	1038	1177	215	10	3.44	3.2	11.89	13.78	3.93	4.78	771.04	11.8438
9:01:31	1390.83	107	1437	391	1048	1113	126	10.03	3.69	2.37	11.85	13.23	3.66	11.07	771.11	11.8513
9:02:01	1391.17	107	1436	389	1035	1351	330	10.03	2.84	2.44	11.88	13.51	3.26	13.88	771.25	11.8598
9:01:01	1391.26	107	1345	340	896	1064	138	10.02	3.36	2.95	11.87	13.43	3.58	10.84	771.32	11.8673
9:01:31	1391.34	107	1381	391	987	1038	185	10	3.68	3.89	11.89	13.5	3.84	8.8	771.39	11.8748
9:02:01	1391.41	108	1357	294	858	1038	185	10	3.13	2.81	11.88	13.72	3.97	6.41	771.46	11.8823

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	GELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
MM:SS	FEET	GPM	PSI	RPM	1000	RPS	RPS	KIPS	CS	CS	KIPS	KIPS	KIPS	FT/HR	OnSd	OnBt
8:02:31	1381.47	107	1363	391	859	1004	168	8.88	3.37	3.08	11.3	13.68	3.88	7.1	771.81	11.803
8:03:01	1381.52	108	1387	391	827	1005	123	8.88	3.53	3.74	11.3	14	4.38	6.31	771.88	11.8113
8:03:31	1381.55	109	1388	395	884	951	117	8.96	3.97	4.04	11.92	14.24	4.81	3.96	771.6	11.8196
8:04:01	1381.57	109	1394	395	885	927	101	8.94	4.04	4.38	11.94	14.43	5.22	2.18	771.64	11.8273
8:04:31	1381.58	109	1380	398	858	902	77	9.04	4.08	4.61	11.94	14.51	5.54	1.58	771.64	11.8352
8:05:01	1381.59	109	1277	398	859	810	93	8.93	4.09	4.8	11.94	14.59	5.84	1.59	771.84	11.8435
8:05:31	1381.6	108	1254	398	881	955	117	8.93	4.14	4.96	11.98	14.59	4.96	0.69	771.65	11.8511
8:06:01	1381.62	109	1324	395	815	1008	180	8.92	3.74	4.08	11.86	14.52	4.64	2.58	771.69	11.8594
8:06:31	1381.65	108	1423	392	1016	1154	239	8.95	3.88	3.4	11.82	13.68	3.78	3.78	771.71	11.8677
8:07:01	1381.61	107	1540	388	1118	1231	188	18.06	3.11	2.46	11.82	13.31	2.97	19.82	771.67	11.8754
8:07:28	1382.06	107	1662	382	1257	1384	271	19.18	3.25	2.95	11.89	13.39	3.42	42.82	772.12	11.8838
8:07:52	1382.17	108	1411	428	894	1182	271	10	3.91	3.95	11.88	14.03	4.33	13.48	772.23	11.8921
8:08:22	1382.22	100	1382	424	931	992	113	8.95	3.9	3.94	11.82	14.15	4.52	5.23	772.27	12.0094
8:08:52	1382.25	110	1318	433	806	943	79	8.94	4.14	4.44	11.94	14.26	4.96	3.28	772.3	12.0177
8:09:22	1382.28	109	1328	429	818	907	93	8.93	3.94	4.07	11.95	14.15	4.69	2.39	772.31	12.0260
8:09:52	1382.3	108	1414	428	1004	1141	289	8.96	3.98	3.98	11.82	13.68	3.97	4.2	772.34	12.0343
8:10:22	1382.44	108	1508	425	1067	1188	148	19.02	2.83	2.18	11.85	13.24	2.94	16.7	772.48	12.0426
8:10:52	1382.49	107	1598	422	1188	1388	308	19.13	3.25	3.18	11.74	13.26	3.92	32.52	772.4	12.0509
8:11:12	1382.88	108	1528	428	1094	1243	247	19.97	2.93	3.25	11.8	13.4	3.59	22.51	772.85	12.0592
8:11:48	1383.32	108	1414	427	977	1437	563	19.91	3.95	4.31	11.88	14.12	3.4	17.11	773.06	12.0675
8:12:18	1383.05	108	1392	430	913	947	89	8.95	3.73	3.8	11.92	14	4.31	3.92	773.1	12.0758
8:12:48	1383.58	108	1393	431	981	959	81	8.94	3.89	3.49	11.92	14.17	4.97	4.22	773.13	12.0841
8:13:18	1383.13	109	1367	438	858	1000	161	8.98	3.89	3.95	11.91	14.06	4.5	8.67	773.21	12.0924
8:13:48	1383.3	108	1388	431	869	1000	83	8.98	3.71	3.74	11.93	14.06	4.51	8.03	773.25	12.1007
8:14:18	1383.34	108	1415	427	888	1080	117	8.97	3.92	4.02	11.89	13.81	3.89	8.81	773.32	12.1090
8:14:48	1383.36	108	1426	428	897	1081	158	10	3.8	3.72	11.86	13.81	4.82	13.69	773.44	12.1173
8:15:18	1383.47	107	1417	426	807	1077	154	18.01	3.85	3.91	11.86	13.88	4.36	9.8	773.51	12.1256
8:15:48	1383.6	107	1454	425	1036	1105	138	18.04	3.29	3.28	11.82	13.59	3.73	16.25	773.63	12.1339
8:16:18	1383.71	107	1511	425	1096	1372	418	18.08	3.17	3.91	11.78	13.57	3.92	25.42	773.66	12.1422
8:16:48	1384.02	106	2080	418	1884	1734	890	18.43	3.31	2.92	11.42	13.52	4.38	85.4	774.12	12.1505
8:17:18	1384.34	106	1521	430	1072	1798	948	18.67	3.71	3.85	11.79	13.67	3.9	28.96	774.29	12.1588
8:17:48	1384.38	106	1413	432	886	1081	198	18.61	3.74	3.88	11.85	13.84	4.69	15	774.41	12.1671
8:18:18	1384.39	106	1298	434	883	839	101	8.93	4.91	4.4	11.83	14.02	4.79	3.98	774.46	12.1754
8:18:48	1384.41	110	1388	434	873	810	81	8.92	4.27	5.07	11.93	14.19	4.74	2.67	774.48	12.1837
8:19:18	1384.43	108	1392	432	885	935	87	8.93	4.08	4.79	11.95	14.19	4.84	2.68	774.48	12.1920
8:19:48	1384.45	108	1313	433	812	891	89	8.93	4.17	4.58	11.92	14	4.88	2.69	774.4	12.1999
8:20:18	1384.48	108	1317	433	813	847	83	8.94	4.18	4.56	11.92	14.04	4.58	3.24	774.55	12.2082

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	MDRQ	LOAD	PEAK	DELTA	WOB	PEAK	DELTA	RDP	Feet	Meters
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	R-Rps	R-Rps	R-Rps	KIPS	G's	G's	KIPS	MIPS	KIPS	FT/HR	OnSp	OnRk
9:20:33	1394.5	104	1353	430	930	996	113	8.93	4.02	4.31	11.82	13.88	4.17	2.01	774.55	12.3034	
9:21:03	1394.55	104	1458	429	1038	1125	182	8.98	3.83	3.8	11.87	13.79	4.21	1.84	774.6	12.3121	
9:21:33	1394.88	107	1472	406	1089	1141	194	10.02	3.47	3.44	11.82	13.43	3.76	14.88	774.74	12.3208	
9:22:03	1394.81	107	1471	425	1028	1132	138	10.04	3.3	3.17	11.81	13.43	3.59	16.22	774.86	12.3287	
9:22:33	1394.93	107	1399	428	990	1117	223	19	3.73	3.61	11.84	14.08	4.87	14.23	774.97	12.337	
9:23:03	1394.88	108	1351	429	825	987	85	8.98	3.88	4.01	11.88	14.34	4.65	5.84	775.03	12.3453	
9:23:33	1395.03	108	1323	429	925	989	81	8.98	3.56	3.34	11.88	14.36	5.03	4.79	775.09	12.3538	
9:24:03	1395.07	107	1355	428	938	1048	194	8.98	3.8	3.4	11.87	14.24	4.88	5.89	775.11	12.3618	
9:24:33	1395.19	107	1400	423	1048	1109	134	10.03	3.14	2.77	11.82	13.98	4.19	8.87	775.25	12.3703	
9:25:03	1395.28	107	1479	424	1054	1170	174	10.07	2.98	3.19	11.78	13.74	4.21	17.84	775.29	12.3785	
9:25:33	1395.5	107	1478	423	1051	1178	251	10.07	3.3	3.1	11.77	13.97	3.07	20.26	775.37	12.3871	
9:26:03	1395.58	108	1357	430	977	983	89	8.98	3.37	3.49	11.87	14	4.43	5.15	775.52	12.3954	
9:26:33	1395.83	108	1343	429	987	983	73	8.97	3.3	3.18	11.88	14.65	4.65	6.23	775.71	12.4038	
9:27:03	1395.87	108	1343	432	923	983	89	8.98	3.22	3.16	11.88	14	4.82	5.41	775.73	12.4121	
9:27:33	1395.74	108	1367	429	938	983	85	9.08	3.38	3.21	11.88	13.79	4.14	8.38	775.8	12.4204	
9:28:03	1395.85	108	1434	426	989	1214	308	10.03	3.31	3.84	11.8	13.67	3.77	12.84	775.89	12.4287	
9:28:33	1396.06	107	1342	428	1083	1259	289	10.13	3.23	3.31	11.73	13.33	3.28	24.55	775.91	12.437	
9:29:03	1396.27	108	1331	429	1084	1287	324	10.1	3.44	3.49	11.74	13.33	3.38	25.43	776.32	12.4453	
9:29:33	1396.57	108	1407	430	989	1028	122	10.05	3.38	3.28	11.83	13.4	3.23	11.84	776.42	12.4538	
9:30:03	1396.44	108	1363	431	929	987	85	8.99	3.23	3.37	11.84	13.55	3.45	8.82	776.48	12.4619	
9:30:33	1396.54	108	1434	428	988	1077	174	10.03	3.21	3.13	11.81	13.48	3.35	12.81	776.8	12.4703	
9:31:03	1396.72	108	1388	428	1058	1136	129	10.08	3.91	3.27	11.75	13.65	3.99	21.43	776.78	12.4785	
9:31:33	1396.84	108	1420	428	988	1044	138	10.01	3.38	3.58	11.82	13.29	3.21	13.47	776.9	12.4871	
9:32:03	1396.98	108	1451	428	1004	1081	156	10.03	3.47	3.56	11.8	13.18	3.04	10.32	777.03	12.4954	
9:32:33	1397.14	108	1462	427	984	1073	146	10.03	3.41	3.46	11.8	13.31	3.23	19.5	777.19	12.5037	
9:33:03	1397.27	108	1482	428	1054	1083	182	10.02	3.43	3.37	11.81	13.21	3.02	15.47	777.36	12.5121	
9:33:33	1397.47	108	1527	428	1054	1132	154	10.08	3.28	3.29	11.77	13.63	2.58	24.43	777.82	12.5204	
9:34:03	1397.72	108	1527	425	1058	1141	158	10.08	3.35	3.38	11.78	13.92	2.54	29	777.74	12.5287	
9:34:33	1397.87	108	1783	421	1303	2409	2469	19.21	3.85	4.03	11.61	13.17	3.09	38.32	777.92	12.5368	
9:34:48	1398.22	110	1482	432	1083	2029	1681	13.01	3.71	4.97	8.8	11.83	6.34	45.88	778.28	12.5441	
9:35:18	1398.39	109	1388	431	958	108	12.87	3.75	4.18	4.18	11.44	4.82	14.3	778.29	12.5489		
9:35:48	1398.47	108	1488	429	958	1004	140	12.81	3.88	3.77	8.2	10.89	4.17	18.28	778.45	12.5571	
9:36:18	1398.58	109	1371	430	888	973	180	12.88	4.08	4.36	9.26	11.28	4.48	13.84	778.63	12.5654	
9:36:48	1398.84	109	1385	429	977	927	93	12.54	3.88	4.31	9.27	11.58	4.84	10.83	778.72	12.5745	
9:37:18	1398.75	110	1316	432	848	959	117	12.53	3.98	4.89	9.27	11.81	4.06	8.14	778.79	12.5828	
9:37:48	1398.83	108	1392	428	854	888	101	12.53	4.82	4.81	9.28	11.88	5.1	7.83	778.86	12.5911	
9:38:18	1398.86	109	1387	430	842	894	87	12.53	3.84	4.49	9.38	11.75	5.16	6.84	778.94	12.5994	

DOE high power mortar test Amaco Cataosa Test Site

Well No. 23	Date: 2/27/98																
Starting Depth =	1392.40	Bit Type =		Walker McQuay MP58M													
Ending Depth =	1450.92	Bit Size =		4 1/2"													
Total Depth (feet)	57.52	Bit Nozzles =		8, 8, 12, 12													
Hours On Bit =	8.73	Mud Type =		Water Based													
Average ROP =	11.89	Mud Weight (lb/gal)		8.00													
Drilling @ =	1419.50	Pipe (in)		10 5/8		Casing (in)		40R 60									

TIME	DEPTH	FLOW	PRES	SPRNG	TORQUE	PEAK	DELTA	HOOK	LOAD	PEAK	DELTA	WOB	PEAK	DELTA	RDP	Feed	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	Lb-ft	R-lbs	R-lbs	KIPS	KIPS	Gs	IS	KIPS	KIPS	KIPS	FOHR	Cost	Cost
9:08:48	1398.95	110	1323	423	858	919	109	12.24	3.93	4.05	3.26	11.82	3.22	8.35	779	12.6077	
9:09:18	1399.03	110	1326	422	880	915	97	12.24	4.12	4.38	3.26	11.73	5.1	9.52	779.4	12.616	
9:10:48	1399.98	109	1357	431	889	947	139	12.17	4.17	4.83	3.23	12.08	6.26	6.96	779.13	12.6243	
9:12:18	1399.18	110	1409	436	922	975	97	12.86	4.07	4.89	10.68	13.61	4.14	11.16	779.34	12.6396	
9:13:48	1399.28	108	1416	439	958	1012	109	12.88	3.54	3.81	10.63	13.66	5.9	12.66	779.82	12.6490	
9:14:18	1399.43	108	1434	427	975	1046	138	12.89	3.48	3.3	10.92	13.62	3.85	17.12	779.47	12.6489	
9:15:48	1399.93	108	1375	428	928	972	97	12.89	3.71	4.18	10.95	12.88	4.67	12.93	779.58	12.6578	
9:16:18	1399.92	108	1398	427	924	971	92	12.86	4.68	4.7	10.95	12.97	4.26	10.56	779.67	12.6681	
9:17:48	1399.71	107	1358	425	917	958	93	12.87	4.13	4.61	10.94	12.97	4.33	10.78	779.78	12.6744	
9:18:18	1399.73	109	1381	429	909	947	61	12.86	4.12	4.51	10.94	12.95	4.31	9.49	779.88	12.6828	
9:19:48	1399.29	108	1387	429	919	951	68	12.87	3.68	4.25	10.94	12.86	4.34	10.71	779.93	12.6911	
9:21:18	1399.97	109	1374	421	930	983	109	12.87	3.64	4.05	10.94	12.88	4.23	10.37	780.03	12.6994	
9:22:48	1400.97	109	1379	428	927	987	77	12.87	3.89	4.44	10.93	12.95	4.36	12.44	780.13	12.6977	
9:23:18	1400.19	108	1384	438	936	983	89	12.87	3.88	4.23	10.93	12.78	4.39	12.99	780.22	12.698	
9:24:48	1400.31	108	1414	428	974	1008	154	12.8	3.85	4.32	10.9	12.63	4.14	10.19	780.38	12.6943	
9:26:18	1400.94	107	1526	424	1083	1099	199	11	3.82	4.44	10.8	12.82	3.81	27.09	780.59	12.6926	
9:27:48	1400.54	107	1526	423	1191	1169	235	11.19	3.83	3.95	10.83	12.89	4.28	37.96	780.69	12.6972	
9:29:18	1401.94	107	1576	427	1114	1247	211	11.09	3.77	4.28	10.78	12.82	3.96	35.82	781.08	12.6941	
9:30:48	1401.29	107	1693	423	1217	1340	207	11.15	3.91	4.37	10.82	12.84	4.07	52.5	781.36	12.6989	
9:31:18	1401.83	107	1627	426	1153	1282	174	11.11	3.84	4.36	10.89	12.84	3.85	48.82	781.59	12.6998	
9:32:48	1401.79	107	1624	426	1129	1299	158	11.12	3.87	4.08	10.89	12.47	3.71	35.69	781.87	12.6992	
9:34:18	1402.94	108	1649	426	1192	1394	204	11.18	3.66	3.94	10.85	12.47	3.86	87.8	782.06	12.6942	
9:35:48	1402.29	107	1569	423	1183	1380	232	11.13	3.81	3.99	10.87	12.93	3.85	48.44	782.34	12.696	
9:37:18	1402.64	108	1637	426	1095	1184	199	11.07	3.9	4.11	10.78	12.06	3.97	34.83	782.56	12.6781	
9:38:48	1402.74	109	1484	421	1028	1037	117	10.84	3.93	4.18	10.85	12.98	3.81	24.92	782.78	12.6544	
9:40:18	1402.62	108	1479	421	1023	1037	138	10.89	3.69	3.83	10.86	12.71	3.88	21.99	782.99	12.6498	
9:41:48	1403.17	107	1567	426	1116	1267	243	11.35	3.69	3.61	10.74	12.82	3.73	35.34	783.23	12.6999	
9:43:18	1403.12	107	1603	424	1149	1216	134	11.08	3.62	3.48	10.7	13.5	3.64	44.86	783.52	12.7052	
9:44:48	1403.89	108	1621	427	1199	1243	162	11.12	3.52	3.29	10.69	12.52	3.83	48.97	783.72	12.7111	
9:46:18	1403.93	107	1558	425	1199	1344	207	11.14	3.54	3.26	10.65	12.84	4.66	62.57	784.01	12.7157	
9:47:48	1404.18	106	1598	429	1304	1282	186	11.04	3.53	3.38	10.76	12.84	3.81	80	784.24	12.722	
9:49:18	1404.43	107	1653	429	1118	1199	148	11.03	3.48	3.23	10.77	12.67	3.81	38.93	784.46	12.7286	
9:50:48	1404.98	107	1620	427	1082	1146	130	10.99	3.44	3.21	10.8	12.84	3.64	38.82	784.73	12.7383	
9:52:18	1404.83	107	1611	428	1168	1264	124	11.1	3.49	3.36	10.69	12.84	3.75	41.88	784.98	12.7423	
9:53:48	1405.38	107	1569	424	1115	1199	138	11.05	3.53	3.01	10.74	12.16	3.28	41.05	785.23	12.7486	
9:55:18	1405.43	108	1544	428	1192	1188	129	11.02	3.28	2.79	10.77	12.84	3.52	35.75	785.48	12.7565	
9:56:48	1405.66	108	1507	428	1180	1251	170	11.11	3.17	2.61	10.88	12.21	3.13	43.62	785.73	12.7616	

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23		Date: 2/27/08															
Starting Depth =		1382.40'		Bit Type =		Walker McDouglass KP60M											
Ending Depth =		1488.02'		Bit Size =		4.75'											
Total Depth Drilled		87.62'		Bit Nozzles =		9, 9, 12, 12											
Hours On Bit =		5.75		Mud Type =		Water Based											
Average ROP =		15.00'		Mud Weight (lb/cc)		8.90											
Drilling (ft) =		1419.50'		Pipe (ft) =		5916.82'		Collar (ft) =		408.00'							
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	BELT	HOOK	PEAK	DELTA	WOS	PEAK	DELTA	ROP	Feet	Hours	
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit	
9:54:17	1408.93	108	1627	429	1173	1389	162	11.14	3.21	2.73	10.68	12.58	3.3	58.39	765.88	12.7858	
9:54:28	1406.18	108	1606	429	1165	1343	164	11.11	3.19	2.65	10.68	12.30	3.28	42.73	786.25	12.7710	
9:54:34	1406.43	107	1630	425	1187	1271	162	11.14	3.63	2.52	10.65	12.23	3.18	84.96	786.48	12.7761	
9:55:10	1406.68	107	1657	420	1201	1302	225	11.16	3.14	2.91	10.63	13.08	3.64	56.87	796.74	12.7827	
9:55:35	1406.93	107	1665	427	1138	1299	203	11.04	3.65	2.47	10.75	13.35	3.78	48.64	797	12.7877	
9:56:05	1407.18	107	1688	427	1154	1380	324	11.05	2.68	2.5	10.7	13.08	3.16	45.3	797.26	12.7924	
9:56:45	1407.43	108	1688	429	1130	1335	166	11.06	3.09	2.83	10.72	12.15	3.11	40.26	797.47	12.7987	
9:56:58	1407.68	108	1688	427	1143	1322	162	11.07	2.97	2.44	10.71	12.15	3.05	43.16	797.74	12.8048	
9:56:59	1407.94	108	1678	428	1212	1344	251	11.18	3.08	2.59	10.69	12.15	3.14	59.26	797.95	12.8088	
9:57:05	1408.19	108	1705	421	1208	1433	384	11.26	3.69	2.48	10.62	11.97	3.21	60.08	798.21	12.8138	
9:57:18	1408.44	107	1705	426	1314	1454	365	11.32	3.63	2.57	10.46	11.78	3.0	68	798.42	12.8198	
9:57:34	1408.69	108	1701	428	1250	1624	680	11.38	3.09	2.47	10.8	11.87	2.78	49.8	798.78	12.8288	
9:57:45	1408.94	108	1702	427	1301	1439	385	11.29	3.06	2.54	10.49	11.87	2.82	63.28	798.99	12.8337	
9:57:57	1409.19	105	1653	418	1448	1725	518	11.35	3.82	2.77	10.43	11.94	3.29	75.44	799.25	12.8371	
9:58:11	1409.44	107	1738	425	1341	1481	478	11.15	3.25	2.72	10.68	12.28	3.89	63.4	799.51	12.8411	
9:58:41	1409.69	108	1612	430	1677	1271	381	10.92	2.73	1.88	10.85	12.4	3.35	27.44	799.73	12.8484	
9:58:41	1409.94	110	1427	434	1658	1125	309	10.86	2.69	1.8	10.92	12.48	3.42	13.8	799.95	12.8477	
9:59:41	1408.69	105	1408	433	980	1101	245	10.85	2.83	2	10.53	12.66	3.57	12.57	799.99	12.8486	
10:00:11	1410.01	108	1456	431	881	1089	231	10.84	2.65	1.88	10.64	12.78	3.47	14.49	799.88	12.8643	
10:00:41	1410.13	109	1397	432	871	1064	229	10.86	2.45	1.93	10.91	12.71	3.57	15.54	799.17	12.8726	
10:01:11	1410.23	108	1398	436	868	1058	230	10.85	2.53	2.41	10.92	12.88	3.67	12.99	799.29	12.881	
10:01:41	1410.35	108	1391	432	967	1077	271	10.84	2.94	2.19	10.93	12.71	3.54	14.27	799.37	12.8863	
10:02:11	1410.46	108	1405	430	1037	1182	340	10.89	2.86	2.18	10.88	12.4	3.66	15.63	799.53	12.8876	
10:02:32	1410.74	109	1493	436	1230	1515	608	11.12	3.32	3.03	10.85	12.69	3.69	44.39	799.78	12.8933	
10:02:46	1410.86	108	1840	428	1143	1380	468	11.07	3.41	3.3	10.7	12.5	3.59	57.69	799.85	12.8976	
10:14:07	1411.16	108	885	394	84	88	34	81.25	1.94	0.33	1.68	2.2	2.37	88.89	799.21	12.92	
10:16:37	1411.34	107	1329	381	84	88	24	15.08	1.98	0.32	1.24	19.44	3.74	21.45	799.35	12.9263	
10:18:07	1411.59	107	1535	385	85	88	34	12.82	1.89	0.41	10.28	10.83	0.77	38.09	799.64	12.9349	
10:18:21	1411.77	107	1458	389	84	88	24	12.48	1.89	0.35	10.41	11.91	1.01	21.62	799.82	12.9433	
10:18:51	1411.85	106	1444	387	86	86	30	12.48	1.88	0.37	10.41	10.98	0.59	31.72	799	12.9515	
10:18:51	1412.1	107	1413	388	85	86	24	12.45	1.88	0.33	10.42	10.7	0.58	17.88	799.15	12.9598	
10:19:01	1412.27	107	1425	388	88	86	24	12.48	1.89	0.31	10.4	10.68	0.5	19.37	799.31	12.9683	
10:19:31	1412.37	108	1313	394	88	88	24	12.49	1.88	0.35	10.44	10.73	0.82	12.8	799.45	12.9765	
10:19:51	1412.43	108	1138	392	88	88	24	12.57	1.88	0.36	10.5	11.39	1.51	4.1	799.48	12.9848	
10:18:24	1412.43	109	1085	398	85	105	28	12.97	1.95	0.59	11.5	10.73	0.81	3.08	799.46	12.9931	
10:19:01	1412.45	108	1021	397	85	85	24	12.38	2	0.55	10.5	10.75	0.63	1.7	799.49	13.0014	
10:18:31	1412.46	109	1084	398	85	88	24	12.39	1.89	0.36	10.48	10.75	0.87	1.16	799.51	13.01	

DOE high power mortar test Amaco Catoosa Test Site

Well No. 20		Date: 2/27/96		Well Type =		Washer McDevens MP62H		SIP Size =		4.75		SR Nozzles =		R. R. 13. 42		Mud Type =		Water Based		Mud Weight (lbs/gal)		9.00		Pipe (in) =		1010.23		Color (ppm)		400.67	
Starting Depth =		1432.40		SR Type =				SR Size =		4.75																					
Ending Depth =		1430.52		SR Nozzles =				SR Size =		4.75																					
Total Depth Drilled		57.82		SR Nozzles =				SR Size =		4.75																					
Hours On Bit =		5.72		Mud Type =		Water Based		SR Size =		4.75																					
Average ROP =		11.90		Mud Weight (lbs/gal)		9.00		SR Size =		4.75																					
Cuttings (%) =		1410.50		Pipe (in) =		1010.23		SR Size =		4.75																					
TIME	SIP DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	LOAD	PEAK	DELTA	WOR	PEAK	DELTA	ROP	Feet	Hours														
HH:MM:SS	FEET	GPM	PSI	RPM	N-lbs	N-lbs	N-lbs	KIPS	OPS	OPS	OPS	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit														
10:20:01	1412.47	130	895	389	67	86	24	11.39	2.02	0.44	10.49	11.39	1.17	1.63	792.53	13.0183															
10:20:33	1412.48	130	897	387	68	90	20	12.33	1.95	0.30	10.48	10.72	0.6	1.48	792.53	13.0286															
10:21:01	1412.5	130	899	389	69	86	20	12.39	1.97	0.30	10.49	10.72	0.59	1.6	792.56	13.0348															
10:21:31	1412.52	109	1021	939	86	92	20	11.18	1.98	0.35	11.66	12.09	2.47	2.29	792.56	13.0433															
10:22:01	1412.54	109	1054	294	86	95	24	10.88	1.84	0.31	12.42	13.02	0.89	2.4	792.56	13.0515															
10:22:31	1412.56	108	1054	305	85	98	26	10.68	1.97	0.32	12.41	13.05	0.93	2.33	792.56	13.0598															
10:23:01	1412.57	108	1061	385	83	104	28	10.48	1.88	0.33	12.41	13.68	0.8	2.63	792.56	13.0681															
10:23:31	1412.58	108	1064	394	80	99	24	10.47	1.95	0.33	12.4	12.73	0.62	2.29	792.56	13.0754															
10:24:01	1412.61	108	1061	398	80	99	24	10.47	1.87	0.33	12.4	13.68	0.58	2.67	792.56	13.0847															
10:24:31	1412.63	108	1057	395	83	98	29	10.43	1.95	0.31	12.41	12.71	0.6	2.4	792.56	13.093															
10:25:01	1412.65	108	1056	397	83	98	26	10.49	1.87	0.35	12.41	13.68	0.59	2.65	792.7	13.1016															
10:25:31	1412.68	109	1041	395	83	98	24	10.45	1.86	0.33	12.42	12.95	1.13	1.61	792.71	13.1098															
10:26:01	1412.68	108	1053	398	82	98	29	10.45	1.96	0.38	12.42	13.09	0.67	2.64	792.75	13.1183															
10:26:31	1412.7	108	1060	393	82	96	24	10.43	1.93	0.38	12.42	13.09	0.86	1.76	792.79	13.1268															
10:27:01	1412.71	109	1077	395	81	98	28	10.44	1.98	0.36	12.43	13.73	0.57	1.63	792.77	13.1349															
10:27:31	1412.73	108	1081	395	80	92	29	10.44	2	0.39	12.42	13.72	0.66	2.6	792.79	13.1431															
10:28:01	1412.75	109	1073	397	80	92	24	10.45	1.89	0.36	12.42	13.78	0.68	2.66	792.8	13.1515															
10:28:31	1412.77	106	1082	395	80	92	24	10.44	1.89	0.32	12.42	13.71	0.6	2.42	792.82	13.1598															
10:29:01	1412.79	109	1081	399	80	92	24	10.44	1.87	0.34	12.43	12.89	0.62	1.98	792.84	13.1681															
10:30:01	1412.85	108	1431	433	1951	2510	1156	10.57	2.24	0.8	12.26	12.78	1.09	32.76	792.82	13.1847															
10:30:31	1412.88	109	1383	435	1997	2644	1459	10.53	2.3	0.88	12.23	12.93	1.13	7.78	793.01	13.1933															
10:31:01	1412.89	109	1387	430	1951	2681	1849	10.5	2.29	0.84	12.38	13.05	1.22	7.63	793.08	13.2016															
10:31:31	1413.1	108	1426	434	2009	2861	1744	10.53	2.23	2.62	12.38	11.6	2.3	18.3	793.15	13.2098															
10:32:01	1413.3	108	1508	433	2140	3070	1877	10.65	3.86	3.67	13.21	13.45	2.39	24.11	793.39	13.2182															
10:32:24	1413.58	108	1590	430	2123	3957	1673	10.69	2.2	0.76	12.17	12.68	1.01	40.17	793.62	13.2345															
10:32:45	1413.9	107	1621	427	2117	3438	2374	10.7	2.13	0.69	12.18	11.43	3.98	41.54	793.88	13.2508															
10:32:15	1414.02	108	1535	432	2027	3258	2062	10.68	2.35	0.78	12.17	13.25	1.93	26.13	794.1	13.2689															
10:32:45	1414.3	108	1475	434	1958	2627	1292	10.57	3.1	2.61	12.39	13.4	2.42	22.1	794.24	13.2772															
10:33:15	1414.34	108	1499	432	2000	2616	1353	10.8	2.99	2.37	12.25	13.31	2.11	18.69	794.44	13.2855															
10:33:39	1414.59	108	1487	430	2008	2957	1426	10.85	2.23	0.74	12.21	12.89	0.95	38.63	794.63	13.2937															
10:34:08	1414.75	108	1457	433	1892	2442	1379	10.56	2.66	2.33	12.29	13.4	2.25	19.67	794.81	13.3024															
10:34:39	1414.95	108	1456	431	1838	2857	1301	10.8	2.82	1.91	12.25	12.97	1.51	29.69	795.08	13.3107															
10:35:09	1415.14	107	1438	429	1815	2391	1290	10.55	2.49	0.73	12.3	13.88	1.89	20.14	795.13	13.3189															
10:35:34	1415.26	107	1483	428	1930	2561	1248	10.62	2.13	0.67	12.33	12.95	1.56	35.68	795.41	13.3288															
10:36:03	1415.62	108	1819	428	1937	3577	1264	10.64	2.13	0.74	12.31	12.99	0.86	34.38	795.67	13.3379															
10:36:39	1415.62	108	1819	428	1937	3577	1264	10.64	2.13	0.74	12.31	12.99	0.86	34.38	795.67	13.3379															
10:37:09	1415.57	109	1663	423	1893	2867	1742	10.77	2.2	1.01	12.27	13.22	2.18	53.38	795.93	13.3467															
10:37:32	1415.52	107	1829	428	1818	3988	1827	10.89	2.12	0.87	11.98	12.17	2.11	11.58	796.16	13.3559															

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	CPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
10:37:59	1416.37	107	1589	428	1780	2391	1278	10.08	2.2	0.70	12.36	12.07	0.81	38.19	798.34	13.3178
10:38:17	1418.62	107	1619	439	1749	2095	1037	10.74	2.37	0.86	13.13	12.98	0.86	39.43	798.30	13.3226
10:38:35	1416.27	107	1593	431	1890	2037	717	10.72	2.14	0.82	12.12	12.84	0.93	40.19	798.33	13.3270
10:38:53	1417.54	108	1459	435	1819	1700	695	10.53	2.09	0.96	12.32	13.38	2.08	36.17	797.69	13.3303
10:39:10	1417.10	107	1490	424	1818	1798	828	10.51	2.75	2.1	12.34	13.48	2.37	34.83	797.21	13.3346
10:39:28	1417.28	109	1440	439	1817	1814	728	10.49	2.84	2.18	12.35	13.69	2.56	34.47	797.35	13.3389
10:40:06	1417.42	109	1447	433	1837	1871	818	10.5	2.86	2.44	12.35	13.82	2.61	37.12	797.46	13.3432
10:41:06	1417.58	108	1512	433	1804	2020	894	10.85	2.91	3.06	12.39	13.64	3.08	35.44	797.63	13.3475
10:42:04	1417.81	108	1738	434	1911	2828	1086	10.72	2.72	1.81	12.09	13.29	2.35	51.11	797.69	13.3518
10:43:07	1418.08	107	1967	429	1964	3045	1698	11.02	2.38	1.53	11.83	13.33	3.38	72.56	798.12	13.3561
10:44:01	1418.31	109	1345	437	1917	2114	1171	10.82	2.77	0.7	5.89	10.08	4.91	36.33	798.36	13.3604
10:45:04	1418.38	110	1198	432	1440	1700	867	10.96	3.11	0.65	5.85	7.06	1.53	4.95	798.46	13.3647
10:46:04	1418.48	109	1387	434	1525	1668	1005	13.37	2.19	0.80	3.46	10.68	3.76	15.20	798.54	13.3690
10:47:04	1418.59	109	1331	434	1612	2007	1178	12.49	3.86	0.58	10.34	10.77	1.05	12.69	798.71	13.3733
10:48:04	1418.79	108	1288	433	1673	2187	1151	13.3	2.67	0.57	10.33	10.82	1.22	17.89	799.83	13.3776
10:49:04	1418.87	107	1380	431	1772	2292	1211	12.58	2.12	0.64	10.27	10.89	0.79	17.11	799.92	13.3819
10:50:04	1419.08	107	1304	430	1768	2328	1248	12.64	2.11	0.64	10.28	10.88	0.79	20.21	798.15	13.3862
10:51:04	1418.59	107	1411	430	1813	2124	1207	12.89	2.14	0.67	10.24	10.8	0.79	22.56	798.35	13.3905
10:52:06	1419.23	109	1456	428	1812	2348	1307	12.63	2.00	0.58	10.19	10.93	1.27	32.93	799.58	13.3948
10:53:06	1419.78	107	1512	431	1855	2354	1190	12.88	2.13	0.89	10.14	10.8	1.13	44.21	799.84	13.4008
10:54:09	1420.03	108	1582	429	1901	2388	1195	12.74	2.05	0.65	10.04	10.9	1.01	47.09	800.69	13.4068
10:55:09	1420.28	109	1947	429	1928	2422	1183	12.73	2.09	0.63	10.09	10.86	0.84	47.78	800.33	13.4128
10:56:21	1420.53	108	1479	432	1917	2470	1360	13.88	2.18	0.64	10.17	10.72	1.1	38.83	800.6	13.4175
10:57:38	1420.79	108	1437	432	1823	2301	1203	13.81	2.1	0.77	10.23	10.85	0.89	31.28	800.86	13.4235
10:58:22	1420.98	109	1377	434	1878	2204	1114	12.33	2.14	0.72	10.26	10.7	0.81	22.9	801.01	13.4295
10:59:30	1421.14	107	1389	432	1885	1938	828	12.5	2.13	0.67	10.32	10.89	0.72	19.1	801.12	13.4355
10:59:20	1421.35	108	1385	434	1819	2052	845	13.5	2.14	0.88	10.32	10.73	0.73	15.23	801.33	13.4407
10:59:30	1421.39	108	1350	438	1825	2061	855	12.91	2.10	0.89	10.31	10.7	0.84	15.4	801.49	13.4455
10:59:20	1421.58	108	1382	438	1859	1982	729	12.53	2.18	0.81	10.3	10.86	0.79	19.12	801.59	13.4510
10:59:38	1421.8	108	1691	433	1779	2041	821	12.75	2.18	0.81	10.07	10.7	1.1	48.71	801.84	13.4565
10:59:38	1422.08	107	1546	432	1749	2089	829	12.73	2.13	0.64	10.09	10.36	0.73	45	802.09	13.4622
10:59:19	1422.35	108	1594	433	1733	2159	858	12.89	2.12	0.84	10.14	10.48	0.65	44.98	802.26	13.4682
10:59:19	1422.55	108	1491	435	1889	2077	867	12.86	2.13	0.89	10.16	10.9	0.81	34.58	802.41	13.4741
10:59:21	1422.8	107	1671	431	1891	2387	1265	12.92	2.08	0.87	10.09	11.27	2.35	55.28	802.88	13.4814
10:59:18	1423.05	107	1001	432	1789	2977	1882	12.73	2.19	0.84	10.09	11.32	2.27	62.31	803.05	13.4877
10:59:48	1423.2	109	1094	430	1699	2247	1256	12.53	2.1	0.57	10.26	10.7	0.84	18.83	803.29	13.4934
10:59:18	1423.41	109	1398	436	1881	2284	1304	12.5	2.15	0.85	10.31	10.63	0.72	21.42	803.46	13.4995

DOE high power motor test Amaco Caloosa Test Site

Well No. 23	Date: 2/27/00																
Starting Depth =	1392.48'			Bit Type =	Wasker McCosmond MP06H												
Ending Depth =	1430.02'			Bit Size =	4.75'												
Total Depth Drilled	37.54'			Bit Nozzles =	9, 9, 12, 12												
Hours On Bit =	8.73			Mod. Type =	Water Based												
Average ROP =	11.80			Mod. Weight (lb/ft) =	9.00												
Drilling (lb) =	1419.69			Pipe (lb) =	1010.82				Collar (lbs) =	101.68							
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DEL T	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hour	
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit	
10:32:45	1423.50	388	1370	430	1706	2286	1523	12.6	2.08	0.92	10.31	10.77	0.81	18.57	803.64	13.5808	
10:34:16	1423.78	388	1429	434	1730	2353	1990	12.54	2.11	0.91	10.37	10.72	0.88	23.57	803.83	13.5860	
10:34:32	1424.01	407	1537	439	1782	2312	1235	12.68	2.11	0.90	10.34	10.58	0.81	53.89	804.07	13.5925	
10:34:46	1424.38	407	1632	438	1854	2001	1885	12.68	2.21	0.94	10.33	11.40	2.32	87.16	804.3	13.6001	
10:35:08	1424.51	408	1613	428	1769	2266	1134	12.74	2.15	0.90	10.07	10.77	1.37	88.41	804.58	13.6035	
10:35:39	1424.77	368	1483	433	1718	2508	1356	12.69	2.12	0.7	10.21	10.6	0.74	35.48	804.66	13.6104	
10:35:54	1425.00	403	1524	432	1782	2524	1207	12.65	2.08	0.87	10.16	10.65	1.83	43.11	805.11	13.6184	
10:36:19	1425.27	407	1526	431	1831	2054	1037	12.64	2.15	0.73	10.17	10.44	0.62	36.11	805.36	13.6233	
10:36:38	1425.52	406	1629	427	1775	2115	754	12.78	2.18	0.75	10.03	10.19	0.88	65.84	805.58	13.627	
10:36:51	1425.77	406	1623	431	1732	2003	721	12.74	2.03	0.63	10.07	10.41	0.69	60.97	805.82	13.6322	
10:37:04	1426.02	407	1768	429	1812	2783	1665	12.82	2.17	0.79	9.98	11.25	2.23	71.21	806.1	13.6398	
10:37:17	1426.27	407	1654	426	1715	2015	766	12.77	2.13	0.89	10.04	10.34	0.87	60.88	806.32	13.6433	
10:37:34	1426.52	407	1613	423	1708	2154	1021	12.72	2.08	0.6	10.08	10.58	0.77	54.1	806.51	13.6479	
10:37:51	1426.78	407	1833	430	1803	2057	1686	12.71	2.09	0.92	10.09	11.25	1.94	53.47	806.86	13.6508	
10:38:07	1427.03	407	1623	430	1782	2358	1203	12.7	2.08	0.90	10.3	10.65	1.83	54.75	807.26	13.6534	
10:38:36	1427.28	408	1515	433	1835	2097	1028	12.63	2.3	0.83	10.2	10.56	0.88	40.79	807.36	13.6594	
10:38:49	1427.53	407	1532	429	1822	2033	936	12.6	2.38	0.74	10.2	10.48	0.87	42.75	807.82	13.6634	
10:39:13	1427.78	408	1532	432	1822	2081	936	12.60	2.11	0.87	10.18	10.51	0.72	45.73	807.92	13.6708	
10:39:27	1428.03	408	1587	426	1836	2085	891	12.68	2.18	0.81	10.12	10.63	0.83	36.14	808.04	13.6761	
10:39:53	1428.28	408	1489	432	1868	1803	719	12.61	2.1	0.83	10.24	10.63	0.81	34.54	808.33	13.6826	
11:00:30	1428.54	409	1475	433	1867	1940	693	12.63	2.18	0.86	10.25	11.06	1.32	33.17	808.6	13.68	
11:00:44	1428.78	407	1508	431	1875	1850	620	12.57	2.18	0.88	10.23	10.88	0.74	37.48	808.83	13.6868	
11:01:14	1429.03	406	1449	433	1838	1777	595	12.61	2.21	0.88	10.28	10.7	1.09	26	809.05	13.6932	
11:01:38	1429.24	408	1536	431	1812	2126	822	12.61	2.29	1.01	10.15	10.68	1.29	37.06	809.28	13.7118	
11:01:52	1429.46	408	2032	427	1864	3195	2094	12.61	2.13	0.94	9.88	11.25	2.08	72.85	809.59	13.7132	
11:02:03	1429.74	406	1672	428	1725	2754	1685	12.65	2.21	0.90	7.43	11.15	4.88	71.36	809.61	13.7187	
11:02:35	1430.38	409	1511	437	1481	1866	1083	15.81	2.1	0.90	6.97	7.39	1.24	28.07	810.03	13.727	
11:03:08	1430.16	408	1322	434	1580	2029	1143	15.63	2.19	0.73	6.85	7.4	0.90	21.72	810.25	13.7353	
11:03:33	1430.24	408	1257	434	1499	1927	1086	16.72	2.46	0.77	7.95	7.43	1.00	8.64	810.26	13.7436	
11:04:02	1430.33	409	1257	434	1481	1548	1123	15.63	2.18	0.81	7.68	7.43	0.72	10.3	810.30	13.7519	
11:04:33	1430.43	408	1268	431	1488	1576	1175	15.63	2.15	0.77	7.3	7.46	0.77	12.73	810.47	13.7605	
11:05:03	1430.48	406	1292	433	1505	2008	1209	15.68	2.18	0.78	7.39	7.49	0.87	8.5	810.67	13.7685	
11:05:33	1430.58	406	1291	430	1543	2152	1292	15.71	2.09	0.83	7.37	7.42	0.79	8.85	810.65	13.7771	
11:06:03	1430.72	406	1283	431	1533	2049	1272	15.71	2.04	0.82	7.05	7.49	0.84	10.57	810.78	13.7854	
11:06:28	1430.81	403	1228	432	1501	2041	1252	15.68	2.13	0.7	7.06	7.49	0.84	10.85	810.67	13.7937	
11:07:00	1431.31	407	1397	429	1590	2089	1256	15.85	2.13	0.79	6.92	7.37	1.03	24.4	811.12	13.8053	
11:07:15	1431.25	407	1423	428	1628	2353	1065	15.95	2.08	0.83	6.82	7.21	0.77	57.82	811.33	13.8083	

DOE high power motor test Amaco Cataosa Test Site

Run No.	Date	Time	Run Type	Voltage	Current	Power	Speed	Temp	Vib	Motor				Gen		Total	Time
										P	V	I	W	P	V		
11205	11/25/96	14:31:32	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:41:32
11206	11/25/96	14:32:10	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:42:10
11207	11/25/96	14:32:48	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:42:48
11208	11/25/96	14:33:26	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:43:26
11209	11/25/96	14:34:04	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:44:04
11210	11/25/96	14:34:42	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:44:42
11211	11/25/96	14:35:20	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:45:20
11212	11/25/96	14:35:58	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:45:58
11213	11/25/96	14:36:36	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:46:36
11214	11/25/96	14:37:14	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:47:14
11215	11/25/96	14:37:52	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:47:52
11216	11/25/96	14:38:30	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:48:30
11217	11/25/96	14:39:08	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:49:08
11218	11/25/96	14:39:46	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:49:46
11219	11/25/96	14:40:24	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:50:24
11220	11/25/96	14:41:02	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:51:02
11221	11/25/96	14:41:40	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:51:40
11222	11/25/96	14:42:18	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:52:18
11223	11/25/96	14:42:56	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:52:56
11224	11/25/96	14:43:34	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:53:34
11225	11/25/96	14:44:12	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:54:12
11226	11/25/96	14:44:50	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:54:50
11227	11/25/96	14:45:28	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:55:28
11228	11/25/96	14:46:06	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:56:06
11229	11/25/96	14:46:44	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:56:44
11230	11/25/96	14:47:22	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:57:22
11231	11/25/96	14:48:00	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:58:00
11232	11/25/96	14:48:38	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:58:38
11233	11/25/96	14:49:16	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:59:16
11234	11/25/96	14:49:54	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	14:59:54
11235	11/25/96	14:50:32	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:00:32
11236	11/25/96	14:51:10	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:01:10
11237	11/25/96	14:51:48	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:01:48
11238	11/25/96	14:52:26	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:02:26
11239	11/25/96	14:53:04	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:03:04
11240	11/25/96	14:53:42	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:03:42
11241	11/25/96	14:54:20	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:04:20
11242	11/25/96	14:54:58	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:04:58
11243	11/25/96	14:55:36	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:05:36
11244	11/25/96	14:56:14	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:06:14
11245	11/25/96	14:56:52	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:06:52
11246	11/25/96	14:57:30	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:07:30
11247	11/25/96	14:58:08	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:08:08
11248	11/25/96	14:58:46	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:08:46
11249	11/25/96	14:59:24	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:09:24
11250	11/25/96	14:59:58	Run	410	16.8	6880	3300	70	0.3	38.0	102.5	6.4	0.7	44.4	1.5	68.5	15:10:14

DOE high power mortar test Amaco Catsosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	FT-LBS	FT-LBS	FT-LBS	KIPS	CF	CF	KIPS	KIPS	KIPS	FT/HR	OnBit	OnBit
11:25:30	1436.83	108	1291	437	1328	1494	1069	12.81	2.25	0.23	9.94	15.25	0.73	8.97	815.04	14.1511
11:26:25	1436.87	108	1293	434	1442	1267	971	12.74	2.29	0.52	9.96	15.32	0.79	4.97	815.04	14.1577
11:27:05	1436.89	108	1314	452	1469	2033	1134	12.82	2.29	2.5	9.95	15.82	2.06	7.06	815.98	14.1638
11:27:25	1436.95	107	1305	452	1432	2251	1276	12.86	2.28	2.85	10.09	11.75	3.06	26.65	816.26	14.1649
11:28:00	1436.8	107	1470	437	1753	2434	1597	12.93	2.13	0.75	10.72	11.18	1.03	33.49	818.44	14.1618
11:28:40	1436.85	107	1578	428	1670	2486	1365	12.10	2.22	0.83	10.59	11.13	1.05	52.4	818.7	14.1597
11:29:45	1436.83	108	1340	445	1529	2203	1337	11.86	2.13	0.74	10.08	11.63	1.48	21.42	819.89	14.1659
11:30:15	1436.84	108	1354	441	1521	2016	1138	11.88	2.14	0.83	10.19	11.27	0.74	12.08	818.86	14.1733
11:30:45	1437.06	108	1375	436	1459	1873	1038	11.89	2.11	0.71	10.65	11.2	0.75	10.15	817.15	14.1816
11:31:18	1437.04	107	1350	437	1489	2585	1740	12.13	2.18	0.81	10.71	11.78	2.01	30.73	817.38	14.1898
11:31:45	1437.55	110	1436	446	1606	3171	2370	11.13	2.13	0.89	10.82	11.97	2.23	26.59	817.63	14.1982
11:31:15	1437.61	109	1294	444	1502	2110	1244	11.3	2.34	0.94	10.84	11.37	0.89	5.79	817.60	14.2069
11:31:49	1437.71	109	1392	441	1680	2300	1361	11.88	2.3	0.72	10.65	11.73	2.01	32.14	817.79	14.2140
11:32:19	1437.86	109	1405	440	1782	2438	1490	11.93	2.19	0.72	10.81	11.32	1.08	30.05	818.03	14.2231
11:32:40	1438.15	109	1415	441	1746	2563	1584	11.93	2.19	0.79	10.81	11.2	0.81	22.15	818.23	14.2314
11:33:15	1438.27	109	1398	442	1736	2523	1576	11.84	2.34	1.07	10.87	11.02	1.03	34.38	818.39	14.2397
11:33:45	1438.43	108	1451	440	1702	2575	1564	11.69	2.88	2.42	10.83	11.87	2.18	27.14	818.54	14.2465
11:34:15	1438.69	108	1374	441	1690	2692	1754	11.68	3.28	1.13	10.89	11.75	1.48	16.01	818.71	14.2564
11:34:45	1438.78	109	1360	444	1629	2272	1488	11.82	3.44	3.17	10.91	12.39	3.63	15.91	818.81	14.2641
11:35:15	1438.86	108	1430	441	1519	2188	1341	11.97	3.25	2.63	10.82	11.82	3.36	34.51	819.63	14.2723
11:35:45	1439.2	108	1426	441	1509	2065	1323	11.91	2.12	0.69	10.82	11.37	1.06	27.88	819.19	14.2815
11:36:15	1438.39	109	1435	440	1592	1911	1189	11.86	3.09	3.23	10.88	12.3	2.85	21.14	819.38	14.2893
11:36:45	1439.53	106	1413	441	1257	1729	840	11.82	3.43	3.39	10.91	12.56	3.49	18.97	819.69	14.2982
11:37:15	1439.8	108	1300	442	1168	1579	857	11.74	3.78	3.65	11	12.73	3.57	6.14	819.86	14.3069
11:37:45	1439.83	109	1362	443	1147	1420	774	11.74	4.1	4.39	11	12.54	3.46	3.82	819.87	14.3148
11:38:18	1439.86	110	1316	448	1141	1485	729	11.74	3.85	4.11	10.89	12.69	3.74	4.13	819.74	14.3231
11:38:45	1439.72	109	1241	444	1138	1445	685	11.76	3.64	3.05	10.97	12.72	3.06	7.19	819.79	14.3313
11:39:18	1439.79	109	1332	444	1174	1413	644	11.76	3.59	3.7	10.97	12.68	3.83	7.71	819.85	14.3397
11:39:45	1439.88	104	1335	442	1130	1364	596	11.78	3.77	3.99	10.93	12.71	3.64	19.69	819.94	14.3478
11:40:15	1439.84	109	1375	444	1135	1360	638	11.78	3.53	3.6	10.94	12.85	3.63	42	820.02	14.3569
11:40:45	1440.06	108	1393	443	1127	1338	488	11.78	3.83	3.94	10.84	13.05	3.4	10.18	820.11	14.3660
11:41:15	1440.17	108	1411	441	1095	1291	429	11.81	3.76	3.79	10.92	13.14	4.74	12.86	820.23	14.3752
11:41:45	1440.24	109	1394	443	1094	1303	455	11.82	3.82	3.78	10.81	13.09	4.57	14.84	820.34	14.3845
11:42:15	1440.41	108	1430	444	1074	1644	798	11.83	3.28	3.83	10.85	13.67	4.38	15.97	820.47	14.3939
11:42:45	1440.54	110	1418	445	1048	1633	628	11.81	2.81	2.88	10.91	13.4	2.97	15.8	820.59	14.4032
11:43:15	1440.66	110	1373	446	1207	1630	830	11.78	2.81	2.85	10.94	13.28	2.94	18.9	820.71	14.4126
11:43:48	1440.71	109	1378	428	1203	1483	616	11.77	2.69	2.86	10.95	13.28	2.8	8.82	820.81	14.4218

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRESS	SPEED	TORQUE	PEAK	DELTA	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	RCP	Feet	Hours
MM:SS	FEET	GPM	PSI	RPM	FT-LBS	INCH	INCH	KIPS	INCH	INCH	KIPS	KIPS	KIPS	FT/HR	DRIFT	DRIFT
11:44:50	1440.81	109	1409	429	1232	1500	885	13.77	2.98	2.43	10.04	12.42	2.94	12.20	820.87	14.4234
11:44:49	1440.82	110	1344	429	1296	1725	1081	13.77	3.02	2.52	10.05	12.4	2.85	0.48	820.85	14.4314
11:45:19	1440.67	111	1376	428	1313	1708	1089	13.75	2.96	0.81	10.96	11.33	0.72	6.15	820.95	14.4367
11:45:49	1440.82	108	1259	424	1233	1706	893	13.75	2.98	0.57	10.96	11.3	0.85	0.77	821	14.4428
11:46:19	1440.81	108	1269	425	1347	1713	903	13.78	2.98	0.99	10.98	11.25	0.52	-1.0	821	14.4503
11:46:49	1440.84	109	1273	421	1343	1788	887	13.78	2.92	0.52	10.98	11.49	1.08	0.31	821.02	14.4549
11:47:19	1441.01	109	1274	428	1336	1717	967	13.77	2.1	0.63	10.94	11.27	0.66	8.75	821.08	14.4732
11:47:49	1441.03	109	1280	424	1348	1731	1017	13.77	2.3	0.78	10.94	11.23	1.13	8.16	821.13	14.4815
11:48:19	1441.00	108	1321	424	1375	1815	1076	13.78	3.78	0.11	10.92	12.14	2.50	0.25	821.13	14.4898
11:48:49	1441.09	106	1404	421	1302	2010	1219	13.8	3.23	2.77	10.91	12.45	3.04	0.92	821.2	14.4981
11:49:19	1441.21	108	1349	422	1363	2080	1493	13.81	2.90	2.41	10.89	12.11	2.68	15.21	821.20	14.5064
11:49:49	1441.37	108	1332	421	1384	2077	1519	13.82	2.39	1.92	10.88	11.78	2.15	7.76	821.32	14.5147
11:50:19	1441.2	108	1321	421	1380	2202	1454	13.82	3.46	0.18	10.89	11.89	0.79	3.71	821.32	14.523
11:50:49	1441.34	108	1299	423	1397	2150	1343	13.8	2.3	0.94	10.8	11.27	0.72	4.68	821.36	14.5314
11:51:19	1441.33	106	1346	423	1690	2393	1380	13.81	3.34	0.35	10.89	12.35	2.32	10.63	821.36	14.5397
11:51:49	1441.51	107	1372	398	1417	2118	2005	13.84	2.82	2.19	10.88	12.11	2.88	9.24	821.58	14.548
11:52:19	1441.6	107	1381	393	1521	2085	1252	13.84	3.18	2.58	10.88	12.3	2.92	10.37	821.71	14.5563
11:52:49	1441.73	107	1405	393	1617	3005	2220	13.84	0.76	2.3	10.88	12.06	2.7	16.05	821.78	14.5646
11:53:19	1441.51	108	1384	428	1734	2607	1873	13.92	2.15	0.75	10.78	11.14	0.69	12.03	822.01	14.573
11:53:49	1442.13	108	1439	434	1689	3498	1897	13.92	3.36	3.06	10.77	12.26	2.33	15.99	822.14	14.5813
11:54:19	1442.38	109	1393	428	1726	2485	1710	13.93	2.13	0.64	10.8	11.28	0.89	10.82	822.35	14.5896
11:54:49	1442.34	109	1362	428	1753	2519	1581	13.95	0.68	2.31	10.84	12.0	2.99	10.24	822.48	14.598
11:55:19	1442.51	108	1352	403	1762	2571	1746	13.87	2.98	2.41	10.82	12.93	3.73	29.3	822.87	14.6063
12:00:23	1442.72	110	1401	413	1868	3227	1608	17.3	2.34	0.64	8.8	8.63	0.53	18.31	822.82	14.63
12:01:23	1442.78	109	1454	431	1461	2128	1454	14.07	2.04	0.51	9.44	11.44	3.39	8.04	822.86	14.6283
12:01:52	1442.84	108	1238	437	1486	3239	1595	13.96	3.06	1.04	11.86	12.58	2.39	7.16	822.88	14.6366
12:02:22	1442.87	105	1443	424	1485	2232	1438	13.16	3.94	2.60	10.26	12.28	3.26	15.13	822.95	14.6449
12:02:52	1443.06	109	1347	432	1371	1721	978	13.1	3.29	3.26	11.01	13.28	2.8	10.01	823.15	14.6532
12:03:22	1443.1	108	1217	430	1229	1887	814	13.84	2.98	0.88	11.07	11.44	0.73	4.7	823.19	14.6615
12:03:52	1443.14	108	1235	429	1288	1832	803	13.03	2.04	0.56	11.98	11.71	1.01	5.18	823.23	14.6698
12:04:22	1443.2	107	1282	428	1277	1890	803	13.05	2.12	0.87	11.98	11.39	0.87	6.88	823.29	14.678
12:04:52	1443.26	107	1278	427	1288	1866	875	13.08	2.06	0.82	11.95	11.48	0.77	7.29	823.38	14.6863
12:05:22	1443.34	107	1277	425	1278	1944	847	13.03	2.12	0.7	11.95	11.58	0.81	10.89	823.4	14.6946
12:05:52	1443.37	108	1278	429	1284	1911	774	13.04	2.15	0.89	11.07	11.48	0.84	3.81	823.47	14.7029
12:06:22	1443.43	107	1341	424	1228	3638	796	13.01	3.44	3.07	11.08	12.42	2.62	6.46	823.5	14.7112
12:06:52	1443.47	106	1385	422	1291	1417	498	13.03	3.45	3.18	13.08	12.1	2.8	5.43	823.52	14.7195
12:07:22	1443.49	107	1380	425	1304	1421	468	13.03	3.67	3.63	13.08	12.4	3.76	2.49	823.56	14.7278

DOE high power mortar test Amaco Caloosa Test Site

TIME	BIT DEPTH FEET	FLOW GPM	PRES PSI	SPEED RPM	TORQUE K-lbs	PEAK K-lbs	DELTA K-lbs	HOOK LOAD KIPS	PEAK G%	DELTA G%	WOB KIPS	PEAK KIPS	DELTA KIPS	RSP FT/HR	Feed QnSk	Hours CnSk
12:07:52	1443.49	108	1371	428	1210	1453	558	13.01	3.44	3.10	11.08	12.42	2.7	0.15	823.58	14.7368
12:08:22	1443.52	108	1358	427	1250	1522	624	13.01	2.5	3.24	11.1	12.90	3.47	3.51	823.58	14.7449
12:08:52	1443.56	108	1349	427	1241	1610	782	13	3.08	2.86	11.1	12.25	2.23	4.2	823.6	14.7532
12:09:22	1443.56	108	1308	431	1275	1600	819	12.99	2.09	3.69	11.1	11.63	0.93	0.54	823.63	14.7619
12:10:22	1443.57	107	1314	425	1268	1608	822	12.99	2.08	3.41	11.1	11.63	0.96	1.52	823.66	14.7782
12:10:52	1443.61	107	1311	424	1303	1684	851	12.99	2.93	3.59	11.1	11.58	0.69	4.98	823.68	14.7985
12:11:22	1443.64	107	1315	425	1250	1676	835	12.98	2.07	3.55	11.11	11.64	0.98	3.55	823.68	14.7984
12:11:52	1443.68	107	1318	425	1256	1680	830	13	2.08	3.59	11.09	11.59	0.80	2.48	823.7	14.8034
12:12:22	1443.68	108	1324	427	1224	1737	878	13.01	3.13	3.69	11.08	11.59	0.93	1.9	823.73	14.8117
12:12:52	1443.69	108	1331	430	1321	1717	883	13.01	2.98	3.61	11.08	11.63	1.08	3.45	823.73	14.82
12:13:22	1443.73	108	1329	430	1308	1808	902	13.01	3.03	3.58	11.08	11.63	0.98	2.72	823.78	14.8283
12:13:52	1443.73	108	1340	434	1317	1872	898	13.02	3.05	3.55	11.08	11.63	1.01	1.9	823.78	14.8366
12:14:22	1443.73	107	1323	428	1338	1705	847	13.02	2.04	3.54	11.08	11.68	1.03	0.7	823.79	14.8449
12:14:52	1443.73	107	1316	427	1338	1806	839	13.01	2.93	3.58	11.08	11.63	0.98	3.93	823.83	14.8532
12:15:22	1443.77	107	1300	427	1307	1708	819	13.02	2.96	2.39	11.07	12.14	2.68	4.91	823.85	14.8615
12:15:52	1443.80	108	1303	422	1326	1858	871	13.01	2.98	2.44	11.04	12.21	2.47	10.83	823.91	14.8698
12:16:22	1443.80	108	1393	428	1252	1251	891	13.03	3	3.93	11.08	12.4	2.44	3.34	823.95	14.8781
12:16:52	1443.82	108	1342	425	1372	1672	774	13.01	3.99	3.31	11.07	12.16	2.32	3.21	823.98	14.8864
12:17:22	1443.85	107	1342	427	1368	1628	819	13.02	3.37	1.69	11.07	11.85	1.41	4.25	824	14.8947
12:17:52	1443.90	108	1343	425	1282	1642	871	13.03	2.54	1.03	11.08	11.9	1.38	1.01	824.01	14.903
12:18:22	1443.93	108	1333	430	1278	1638	850	13.03	3.56	1.53	11.08	11.6	1.38	4.08	824.08	14.9113
12:18:52	1444.01	110	1384	436	1290	1571	816	13.03	2.66	3.47	11.05	11.6	1.38	1.74	824.07	14.9196
12:19:22	1444.07	108	1464	431	1378	1834	870	13.09	2.92	2.6	11	12.38	3.8	7.92	824.13	14.9279
12:19:52	1444.08	108	1285	432	1446	2005	1178	13.08	2.13	3.69	11.02	11.88	1.15	1.51	824.18	14.9362
12:20:22	1444.04	108	1284	430	1486	2185	1238	13.05	2.68	3.41	11.01	11.68	1.15	7.38	824.18	14.9445
12:21:22	1444.17	108	1285	439	1448	1919	1066	13.02	3.08	3.55	11.08	11.85	1.32	4.69	824.24	14.9528
12:21:52	1444.31	107	1311	428	1414	1857	1005	12.72	3.08	3.68	11.08	11.99	1.17	4.1	824.3	14.9611
12:22:22	1444.31	107	1306	428	1375	1741	895	12.93	3.17	3.65	11.25	11.85	1.05	0.67	824.3	14.9694
12:22:52	1444.38	108	1298	429	1380	1815	885	12.82	2.12	3.67	11.25	11.8	1.03	5.68	824.32	14.9767
12:23:22	1444.3	107	1297	427	1315	1822	855	12.52	2.07	3.65	11.28	11.8	1.06	3.54	824.34	14.985
12:23:52	1444.31	108	1308	429	1268	1930	843	12.83	3	2.58	11.24	12.33	2.29	2.02	824.38	15.0033
12:24:22	1444.38	108	1400	425	1275	1988	898	12.65	3.04	2.53	11.23	12.38	2.33	5.75	824.43	15.0116
12:24:52	1444.48	108	1382	425	1282	1908	819	12.65	3.03	2.51	11.23	12.64	2.78	8.35	824.48	15.0199
12:25:22	1444.5	108	1422	425	1278	1928	843	12.88	3.1	2.58	11.21	12.47	2.75	8.35	824.55	15.0282
12:25:52	1444.56	107	1398	428	1257	1980	892	12.85	3.1	2.6	11.23	12.38	2.49	6.68	824.61	15.0365
12:26:22	1444.56	107	1404	427	1274	1987	890	12.85	3.23	2.68	11.23	12.47	2.63	3.51	824.66	15.0448
12:26:52	1444.75	107	1352	426	1381	1741	861	12.8	3.1	2.68	11.17	12.83	3.38	19.47	824.61	15.0531

DOE high power mortar test Amaco Catoosa Test Site

Web No. 23	Date: 2/27/98																
Starting Depth =	1382.61	Bit Type = Walker McDonnell MPD-1															
Ending Depth =	1450.32	Bit Size = 4.75															
Total Depth Drilled	67.71	Bit Nozzles = 8, 8, 12, 12															
Hours On Bit =	5.73	Mud Type = Water Based															
Average ROP =	11.83	Mud Weight (lb/gal) = 8.00															
Graveling (G) =	1419.50	Plan (I) = 1010.82															
		Collar (R) = 408.80															
TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAR	DELT	RODR	LOAD	PEAK	DELTA	WOB	PEAK	DELTA	RQP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	R-lbs	R-lbs	RPS	G%	G%	RIPS	KIPS	KIPS	KIPS	FT/HR	DRSS	DRSS
12:27:22	1448.88	100	1458	431	1317	1579	543	12.88	3.13	2.8	11.19	12.35	2.68	12.68	824.9	15.0615	
12:27:53	1448.64	100	1498	429	1324	1534	538	12.89	3.09	2.6	11.19	12.39	2.39	15.24	825	15.0626	
12:28:22	1448.09	100	1488	431	1308	1555	535	12.91	3.08	2.59	11.18	12.39	2.3	17.4	825.13	15.0784	
12:28:52	1448.24	100	1488	429	1285	1589	536	12.9	3.16	2.8	11.17	12.57	3.12	14.77	825.28	15.0867	
12:29:22	1448.34	100	1478	434	1223	1518	533	12.99	3.14	2.68	11.18	12.47	2.8	14.43	825.38	15.095	
12:29:52	1448.41	100	1487	429	1284	1510	510	12.98	3.14	2.72	11.19	12.52	3.02	8.81	825.48	15.1033	
12:30:22	1448.53	100	1450	429	1251	1481	488	12.87	3.00	2.68	11.2	12.4	2.73	14.34	825.58	15.1116	
12:30:52	1448.81	107	1398	427	1185	1425	535	12.85	3.22	2.89	11.21	12.57	2.94	8.43	825.68	15.1199	
12:31:22	1448.65	108	1354	431	1186	1384	547	12.82	3.3	3.08	11.24	12.58	2.69	4.18	825.71	15.1262	
12:31:52	1448.7	108	1432	437	1200	1408	438	12.83	3.14	2.8	11.23	12.54	2.8	7.83	825.75	15.1305	
12:32:22	1448.73	107	1433	427	1210	1417	478	12.84	3.25	2.89	11.23	12.57	2.62	10.29	825.84	15.1448	
12:32:52	1448.79	108	1426	427	1203	1421	482	12.84	3.19	2.77	11.23	12.58	2.63	11.7	825.91	15.1531	
12:33:22	1448.88	108	1377	428	1185	1380	478	12.87	3.31	3.02	11.24	12.64	3.03	8.87	826	15.1614	
12:33:52	1448.9	108	1365	431	1169	1344	488	12.8	3.25	2.98	11.26	12.62	3.04	4.79	826.09	15.17	
12:34:22	1448.03	108	1349	429	1130	1248	482	12.78	3.38	3.22	11.27	12.54	2.6	3.26	826.11	15.1783	
12:34:52	1448.08	108	1361	429	1134	1306	494	12.76	3.33	3.22	11.28	12.59	2.7	3.63	826.13	15.1866	
12:35:23	1448.1	108	1418	428	1189	1417	531	12.78	3.19	2.93	11.27	12.57	2.92	5.7	826.15	15.1949	
12:35:52	1448.12	108	1518	429	1282	1518	527	12.79	3.23	2.86	11.27	12.62	2.8	2.49	826.21	15.2032	
12:36:22	1448.25	108	1549	429	1315	1514	488	12.83	3.14	2.76	11.27	12.52	2.87	12.69	826.32	15.2115	
12:36:52	1448.41	108	1545	429	1277	1519	555	12.83	3.16	2.79	11.22	12.69	3.18	18.93	826.47	15.2206	
12:37:22	1448.38	111	1395	438	1124	1308	454	12.76	3.46	3.52	11.28	12.78	3.04	4.73	826.51	15.2289	
12:37:52	1448.38	109	1394	434	1137	1320	460	12.75	3.4	3.21	11.31	12.61	3.06	4.18	826.53	15.2365	
12:38:22	1448.34	108	1388	437	1148	1308	413	12.74	3.21	3.68	11.31	12.66	2.99	1.81	826.56	15.2448	
12:38:52	1441.84	-1	244	12	84	202	189	23.48	1.8	0.16	0.51	0.03	0.01	1.74	826.59	15.2531	
12:39:22	1441.83	-1	238	12	84	100	32	22.72	1.79	0.36	1.27	1.53	0.58	-0.13	826.59	15.2703	
12:39:52	1441.83	-1	239	12	82	96	32	22.53	1.79	0.35	1.48	1.72	0.48	-0.03	826.59	15.2840	
12:40:22	1441.83	-1	208	12	85	700	32	22.27	1.78	0.05	1.89	1.84	0.48	-0.18	826.59	15.2933	
12:40:52	1441.83	-1	204	12	85	700	32	22.22	1.79	0.04	1.77	1.93	0.45	0.22	826.59	15.3015	
12:41:22	1441.83	-1	204	12	84	109	32	22.06	1.8	0.05	1.94	2.10	0.6	-0.21	826.59	15.3098	
12:41:52	1441.82	-1	203	12	84	109	32	21.81	1.8	0.05	2.08	2.27	0.41	-0.28	826.59	15.3181	
12:42:22	1441.82	-1	203	12	84	109	32	21.63	1.8	0.05	2.17	2.39	0.43	0.4	826.59	15.3264	
12:42:52	1441.82	-1	201	12	85	104	32	21.67	1.8	0.08	2.32	2.56	0.5	-0.23	826.59	15.3347	
12:43:22	1441.82	-1	201	12	85	104	28	21.89	1.78	0.04	2.45	2.76	0.43	0.67	826.59	15.343	
12:43:52	1441.82	-1	204	12	85	104	32	21.43	1.8	0.06	2.55	2.75	0.38	0.09	826.59	15.3513	
12:44:22	1441.82	-1	182	12	87	104	32	21.22	1.8	0.06	2.67	2.94	0.48	-0.47	826.59	15.3596	
12:44:52	1441.82	-1	199	12	87	104	38	21.19	1.78	0.04	2.82	3.02	0.41	-0.89	826.59	15.3679	
12:45:22	1448.81	108	1221	428	1231	1834	788	14.27	3.29	3.36	7.78	11.75	12.83	1.71	406.88	15.3762	

DOE high power mortar test Amaco Catoosa Test Site

Well No. 23	Date: 2/27/06																	
Starting Depth =	1380.40'																	
Ending Depth =	1418.00'																	
Total Depth Drilled	37.60'																	
Hours On Bit =	5.73																	
Average ROP =	11.80																	
Collaring (ft) =	1418.00																	
		Bit Type =	Walker McDermid MP68H															
		Bit Size =	4.75															
		Bit Nozzles =	3, 9, 12, 12															
		Mud Type =	Water Based															
		Mud Weight (lbs/gal)	8.00															
		Pipe (in) =	7010.82															
		Collar (ft) =	408.80															

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	ROCK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	RPS	RPS	RPS	FY/HR	OnBit	OnBit
14:22:58	1446.82	107	1433	490	1233	1930	571	11.88	3.36	3.91	10.21	11.9	5.73	1.56	826.86	15.3863
14:27:28	1446.93	106	1478	492	1403	2484	1531	11.89	3.96	4.44	10.17	12.4	5.65	1.73	826.7	15.3948
14:27:58	1446.70	106	1763	429	1495	2927	1543	11.92	4.19	4.51	10.13	12.38	5.03	18.63	826.85	15.4032
14:30:28	1446.81	107	1421	436	1292	1488	507	11.91	3.5	4.24	10.15	12.18	4.34	6.24	826.87	15.4115
14:30:58	1446.84	107	1488	432	1273	1396	535	11.92	3.94	4.27	10.14	12.06	4.36	5.72	826.88	15.4198
14:30:58	1446.87	108	1406	439	1283	1437	489	11.94	3.7	4.05	10.14	12.04	4.32	3.95	826.83	15.4282
14:32:58	1446.89	109	1403	438	1321	1417	470	11.93	3.79	4.17	10.14	11.99	4.31	2.2	826.91	15.4365
14:33:28	1446.86	108	1308	437	1347	1453	806	11.92	3.69	4.11	10.13	11.92	4.05	0	826.96	15.4449
14:33:58	1446.83	107	1431	431	1280	1403	498	11.93	3.51	3.98	10.12	12.04	4.24	0.95	826.96	15.4531
14:31:28	1446.52	108	1451	434	1299	1426	462	11.94	3.44	3.94	10.11	11.97	4.14	3.08	826.98	15.4615
14:31:58	1446.98	106	1471	430	1313	1490	458	11.96	3.35	3.39	10.09	11.84	4.26	4.94	827.01	15.4697
14:32:28	1447	106	1483	429	1319	1516	506	11.97	3.69	3.74	10.08	12.02	4.34	4.73	827.06	15.478
14:32:58	1447.05	107	1476	420	1304	1519	514	11.98	3.82	3.86	10.07	11.99	4.2	5.08	827.12	15.4863
14:33:28	1447.06	107	1479	431	1303	1519	484	11.99	3.85	3.68	10.06	11.97	4.4	4.95	827.15	15.4949
14:33:58	1447.12	108	1472	437	1285	1526	507	11.99	3.61	3.76	10.06	12.04	4.87	3.82	827.19	15.5032
14:34:28	1447.15	108	1629	428	1394	2539	1350	12.02	4.1	4.41	10.03	12.8	5.39	3.13	827.25	15.5115
14:34:58	1447.24	107	1595	432	1336	2923	1738	12.04	4.22	4.06	10	11.99	5.17	11.07	827.31	15.5198
14:35:28	1447.28	108	1429	436	1299	1449	509	12.01	3.77	4.43	10.04	12.04	4.52	5.15	827.34	15.5281
14:35:58	1447.3	106	1375	439	1171	1324	466	12.01	3.74	4.14	10.04	11.85	4.69	1.85	827.39	15.5364
14:36:28	1447.31	108	1378	436	1174	1380	476	12	3.91	3.94	10.04	11.97	4.69	1.74	827.34	15.5447
14:36:58	1447.34	107	1387	438	1189	1378	458	12.01	3.62	3.65	10.03	11.94	4.51	2.86	827.4	15.5531
14:37:28	1447.36	108	1420	435	1200	1384	502	12.01	3.88	2.78	10.03	11.93	4.38	3.6	827.41	15.5615
14:37:58	1447.38	108	1412	438	1187	1372	474	12.01	3.74	4.13	10.03	12.08	4.38	0.42	827.43	15.5697
14:38:28	1447.4	108	1408	433	1183	1344	442	12.02	3.43	3.44	10.02	12.06	4.24	4.43	827.45	15.5781
14:38:58	1447.4	108	1390	438	1161	1349	429	12.01	3.83	3.88	10.02	11.86	4.83	0.41	827.46	15.5864
14:39:28	1447.42	108	1367	433	1150	1324	425	12.02	3.49	3.74	10.01	11.92	4	2.31	827.49	15.5947
14:39:58	1447.44	107	1368	429	1153	1304	405	12.01	3.76	4.28	10.02	11.97	4	2.36	827.49	15.6031
14:40:28	1447.45	104	1335	435	1151	1318	401	12.02	3.77	3.88	10.02	11.9	3.93	0.87	827.5	15.6115
14:40:58	1447.46	104	1383	434	1169	1312	387	12.01	3.88	3.56	10.02	11.76	3.81	0.78	827.51	15.6198
14:41:28	1447.47	108	1357	434	1166	1300	383	12.02	3.4	3.75	10.01	11.97	3.83	1.17	827.53	15.6281
14:41:58	1447.48	107	1358	429	1182	1336	317	12.02	3.26	3.66	10.01	11.75	3.76	1.74	827.55	15.6364
14:42:28	1447.5	108	1405	434	1150	1329	405	12.01	3.33	3.42	10.02	11.85	4.12	1.78	827.55	15.6447
14:42:58	1447.51	108	1417	438	1160	1339	439	12.02	3.75	4.19	10.01	11.99	4.07	1.83	827.59	15.6531
14:43:28	1447.54	109	1419	438	1151	1352	417	12.01	3.86	3.3	10.02	11.88	3.92	3.08	827.59	15.6615
14:43:58	1447.55	107	1408	430	1147	1319	361	12.01	3.8	3.82	10.01	11.73	3.72	2.08	827.6	15.6697
14:44:28	1447.57	109	1490	430	1143	1303	385	12.01	3.5	3.65	10.01	11.98	3.89	1.51	827.62	15.6781
14:44:58	1447.58	107	1401	431	1140	1312	381	12.01	3.47	3.83	10.01	11.91	3.67	1.44	827.64	15.6864

DOE high power mortar test Amaco Catoosa Test Site

TIME	SHT DEPTH	FLOW	PRESS	SPEED	TORQUE	PEAK	DELT	HOCK LOAD	PEAR	DELTA	WOB	PEAK	DELTA	RCF	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPI	PS	CS	KIPI	KIPI	KIPI	FT/HR	DRPH	ONHR
14:45:29	1447.6	109	1389	434	1123	1259	381	12.01	3.56	3.83	10.02	11.64	3.73	2.33	827.85	15.6848
14:45:58	1447.62	107	1390	429	1116	1255	428	12	3.56	3.65	10.02	11.68	3.76	2.31	827.67	15.7022
14:46:28	1447.63	108	1390	432	1116	1304	482	12	3.61	3.73	10.02	11.69	3.95	1.67	827.69	15.7115
14:46:54	1447.65	108	1381	435	1114	1324	439	12	3.69	3.77	10.02	12.24	4.02	1.08	827.7	15.7198
14:47:24	1447.65	109	1384	433	1128	1303	401	11.99	3.40	3.63	10.03	11.75	3.73	0.94	827.71	15.7281
14:47:54	1447.67	107	1400	428	1128	1312	428	11.99	3.47	3.56	10.03	11.78	3.61	0.89	827.72	15.7364
14:48:29	1447.68	107	1411	431	1136	1304	421	11.99	3.53	3.56	10.02	11.75	3.68	1.98	827.74	15.7447
14:48:59	1447.71	108	1414	422	1139	1344	448	11.99	3.74	3.82	10.03	11.8	3.93	3.46	827.76	15.753
14:49:29	1447.72	107	1427	429	1155	1362	382	11.99	3.70	4.11	10.03	11.9	4.24	3.27	827.8	15.7616
14:49:59	1447.74	107	1499	422	1217	1348	393	11.99	3.72	3.78	10.03	11.85	4.79	1.15	827.8	15.7699
14:50:29	1447.9	107	1706	432	1281	2583	3838	12.01	3.7	4.06	10.43	12.26	6.56	7.2	827.89	15.7782
14:50:59	1447.83	108	1464	404	1168	1387	514	11.64	3.86	4.4	10.37	12.23	5	3.63	827.89	15.7865
14:51:29	1447.85	109	1424	436	1162	1352	439	11.53	3.76	4.21	10.49	12.33	3.95	3.64	827.91	15.7948
14:51:59	1447.87	108	1412	439	1145	1326	421	11.54	4.04	4.57	10.47	12.33	3.97	3.24	827.93	15.8031
14:52:29	1447.89	109	1404	434	1140	1332	413	11.55	3.69	4.14	10.47	12.09	3.65	2.56	827.94	15.8114
14:52:59	1447.91	103	1402	435	1140	1328	406	11.54	3.61	4.11	10.47	12.21	3.65	2.68	827.96	15.8197
14:53:29	1447.91	103	1405	439	1148	1340	421	11.53	3.61	4.32	10.48	12.26	3.65	0.32	827.97	15.828
14:53:59	1447.92	107	1416	430	1145	1340	425	11.53	3.77	4.37	10.48	12.3	3.65	2.42	828	15.8363
14:54:29	1447.95	109	1429	430	1157	1356	433	11.53	3.79	4.21	10.47	12.32	4.33	2.69	828	15.8447
14:54:59	1447.95	107	1464	438	1156	1376	425	11.54	3.92	4.19	10.47	12.29	4.09	0.19	828	15.853
14:55:29	1448.01	106	1317	427	1246	1432	539	11.38	3.71	4.04	10.45	12.11	3.83	2.47	828.06	15.8616
14:55:59	1448.09	108	1367	417	1121	1332	488	11.54	3.6	4.37	10.47	12.28	4.63	1.81	828.1	15.8699
14:56:29	1448.06	107	1378	431	1163	1308	448	11.54	4.03	4.05	10.37	12.4	3.17	4.84	828.07	15.8782
14:56:59	1448.08	109	1388	436	1129	1320	454	11.54	3.87	4.25	10.47	12.4	3.21	3.38	828.12	15.8865
14:57:29	1448.09	104	1413	434	1149	1338	445	11.38	3.83	4.27	10.48	12.5	4.57	0.7	828.16	15.8948
14:57:59	1448.12	108	1419	424	1151	1335	438	11.54	3.86	4.81	10.48	12.35	4.59	3.38	828.18	15.9031
14:58:29	1448.14	108	1421	425	1161	1368	459	11.56	3.64	4.04	10.45	12.38	4.17	3.76	828.2	15.9114
14:58:59	1448.21	107	1442	432	1178	1398	433	11.56	3.65	3.69	10.44	12.26	4.24	2.97	828.27	15.9197
14:59:29	1448.27	106	1432	433	1167	1255	438	11.57	3.23	4.01	10.43	12.28	4.36	2.12	828.33	15.928
14:59:59	1448.33	108	1425	435	1158	1348	433	11.57	3.89	4.18	10.43	12.28	4.21	8.59	828.39	15.9363
15:00:29	1448.38	107	1435	436	1169	1382	423	11.57	3.72	4.26	10.43	12.23	4.21	8.87	828.43	15.9447
15:00:59	1448.44	107	1411	432	1148	1348	459	11.57	4.11	4.62	10.43	12.3	4.23	2.19	828.49	15.953
15:01:29	1448.46	108	1384	426	1137	1299	446	11.58	4	4.84	10.45	12.29	4.23	4.83	828.52	15.9616
15:01:59	1448.51	103	1379	432	1130	1303	462	11.58	4.27	5.13	10.44	12.5	4.21	3.76	828.58	15.9699
15:02:29	1448.53	104	1391	439	1124	1344	478	11.56	3.96	4.53	10.44	12.4	4.26	1.83	828.64	15.9782
15:02:59	1448.57	107	1332	432	1252	1423	510	11.36	3.62	4.02	10.42	12.06	4.12	4.51	828.62	15.9865
15:03:29	1448.59	107	1490	432	1259	1453	498	11.59	3.7	4.02	10.41	12.11	4.14	9.11	828.69	15.9948

DOE high power mortar test Amaco Catoosa Test Site

TIME	DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELT	HOOK	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Hours
HH:MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	IN/PSI	GS	GS	KIPS	KIPS	KIPS	FT/HR	Depth	Onbit
15:03:58	1448.73	107	1502	431	1546	1502	543	11.58	3.64	3.1	10.3	12.14	4.34	10.98	824.77	15:03:58
15:04:28	1448.76	109	1364	438	1527	1368	519	11.56	3.93	4.44	10.43	12.3	4.06	3.47	824.81	15:04:28
15:04:58	1448.77	108	1302	436	1144	1288	474	11.56	4.02	4.51	10.43	12.09	3.93	1.90	828.83	15:04:58
15:05:28	1448.84	107	1407	430	1254	1478	478	11.56	3.9	4.39	10.47	11.94	3.9	7.32	828.88	15:05:28
15:05:58	1448.81	107	1458	438	1201	1441	534	11.56	3.81	4.05	10.43	12.09	4	5.32	828.90	15:05:58
15:06:28	1448.84	107	1411	431	1452	1348	421	11.54	3.83	4.38	10.45	12.26	4.19	3.68	829	15:06:28
15:06:58	1448.85	108	1404	435	1154	1344	457	11.58	3.93	4.58	10.44	12.08	4.17	1.99	829.02	15:06:58
15:07:28	1448.89	106	1364	434	1140	1338	421	11.56	4.07	4.58	10.42	12.11	4.02	3.9	829.04	15:07:28
15:07:58	1448.91	107	1427	431	1367	1378	446	11.57	3.86	4.22	10.47	12.09	3.97	2.81	829.06	15:07:58
15:08:28	1448.97	105	1525	428	1291	1488	438	11.54	3.44	3.86	10.38	12.06	4.14	7.18	829.14	15:08:28
15:08:58	1449.15	107	1504	432	1239	1445	456	11.62	3.3	3.58	10.27	12.18	3.97	9.18	829.19	15:08:58
15:09:28	1449.13	107	1682	437	1348	2493	570	11.6	3.68	4.19	10.37	12.79	6.55	2.53	829.26	15:09:28
15:09:58	1449.24	109	1354	435	1230	2207	3309	11.50	3.69	3.76	10.38	12.80	6.27	13.98	829.28	15:09:58
15:10:28	1449.32	109	1507	434	1338	2507	1612	11.61	3.45	3.45	10.37	12.78	6.22	16.24	829.36	15:10:28
15:10:58	1449.43	109	1674	436	1177	1388	446	11.68	3.59	3.67	10.4	12.18	4.24	11.63	829.47	15:10:58
15:11:28	1449.43	109	1359	438	1908	1298	465	11.64	4.3	5.12	10.44	12.18	3.83	3.45	829.49	15:11:28
15:11:58	1449.48	108	1359	433	1073	1247	383	11.62	4.1	5.01	10.48	12.23	3.9	-0.28	829.51	15:11:58
15:12:28	1449.47	106	1373	433	1023	1288	382	11.53	4.03	4.21	10.45	12.18	3.83	2.2	829.53	15:12:28
15:12:58	1449.40	109	1385	437	1099	1283	365	11.52	3.88	4.62	10.42	12.14	2.73	2.98	829.54	15:12:58
15:13:28	1449.51	108	1391	434	1131	1271	382	11.52	3.94	4.38	10.45	12.14	3.86	2.88	829.56	15:13:28
15:13:58	1449.54	107	1408	431	1129	1279	329	11.52	3.77	4.82	10.45	12.08	3.84	2.53	829.58	15:13:58
15:14:28	1449.58	107	1416	430	1134	1275	329	11.54	3.79	4.13	10.45	12.08	3.78	2.63	829.61	15:14:28
15:14:58	1449.59	109	1431	434	1147	1288	320	11.52	3.49	3.52	10.45	12.18	3.73	4.09	829.64	15:14:58
15:15:28	1449.59	109	1453	432	1162	1302	312	11.53	3.5	3.39	10.44	11.97	3.52	6.21	829.7	15:15:28
15:15:58	1449.64	108	1453	432	1162	1302	312	11.53	3.5	3.39	10.44	11.97	3.52	6.21	829.7	15:15:58
15:16:28	1449.71	108	1429	431	1148	1309	338	11.54	3.37	3.45	10.45	12.04	3.63	7.34	829.76	15:16:28
15:16:58	1449.77	109	1425	430	1141	1293	349	11.54	3.4	3.44	10.43	12.11	3.73	7.28	829.82	15:16:58
15:17:28	1449.83	107	1427	430	1135	1283	336	11.53	3.5	3.44	10.44	12.14	3.81	6.13	829.86	15:17:28
15:17:58	1449.86	108	1429	432	1133	1282	349	11.53	3.33	3.25	10.44	11.94	3.63	6.13	829.92	15:17:58
15:18:28	1449.93	108	1386	433	1030	1283	365	11.52	3.73	4	10.45	11.87	3.57	5.14	829.97	15:18:28
15:18:58	1449.98	109	1385	438	1089	1326	366	11.51	4.06	4.82	10.46	12.06	3.59	3.15	830.01	15:18:58
15:19:28	1449.98	107	1388	431	1089	1326	369	11.5	3.97	3.82	10.47	12.06	3.59	1.7	830.03	15:19:28
15:19:58	1450.06	106	1435	427	1129	1308	389	11.5	3.66	3.98	10.46	12.14	3.78	0.93	830.05	15:19:58
15:20:28	1450.08	107	1484	429	1188	1344	352	11.5	3.43	3.26	10.46	12.11	3.65	4.45	830.06	15:20:28
15:20:58	1450.01	108	1523	428	1228	1401	381	11.55	3.43	3.84	10.43	12.18	3.83	8.29	830.14	15:20:58
15:21:28	1450.18	106	1454	427	1201	1401	401	11.54	3.26	3.13	10.43	12.09	3.78	12.33	830.23	15:21:28
15:21:58	1450.24	107	1427	430	1184	1384	421	11.53	3.33	3.12	10.43	12.08	3.65	12.17	830.34	15:21:58
15:22:28	1450.35	106	1407	428	1204	1426	443	11.54	3.34	3.18	10.42	11.99	3.66	7.92	830.4	15:22:28

Well No. 33
 Starting Depth = 1382.40
 Ending Depth = 1450.99
 Total Depth Drilled = 67.62
 Hours On Bit = 5.93
 Average ROP = 11.39
 Drilling Off = 1419.30

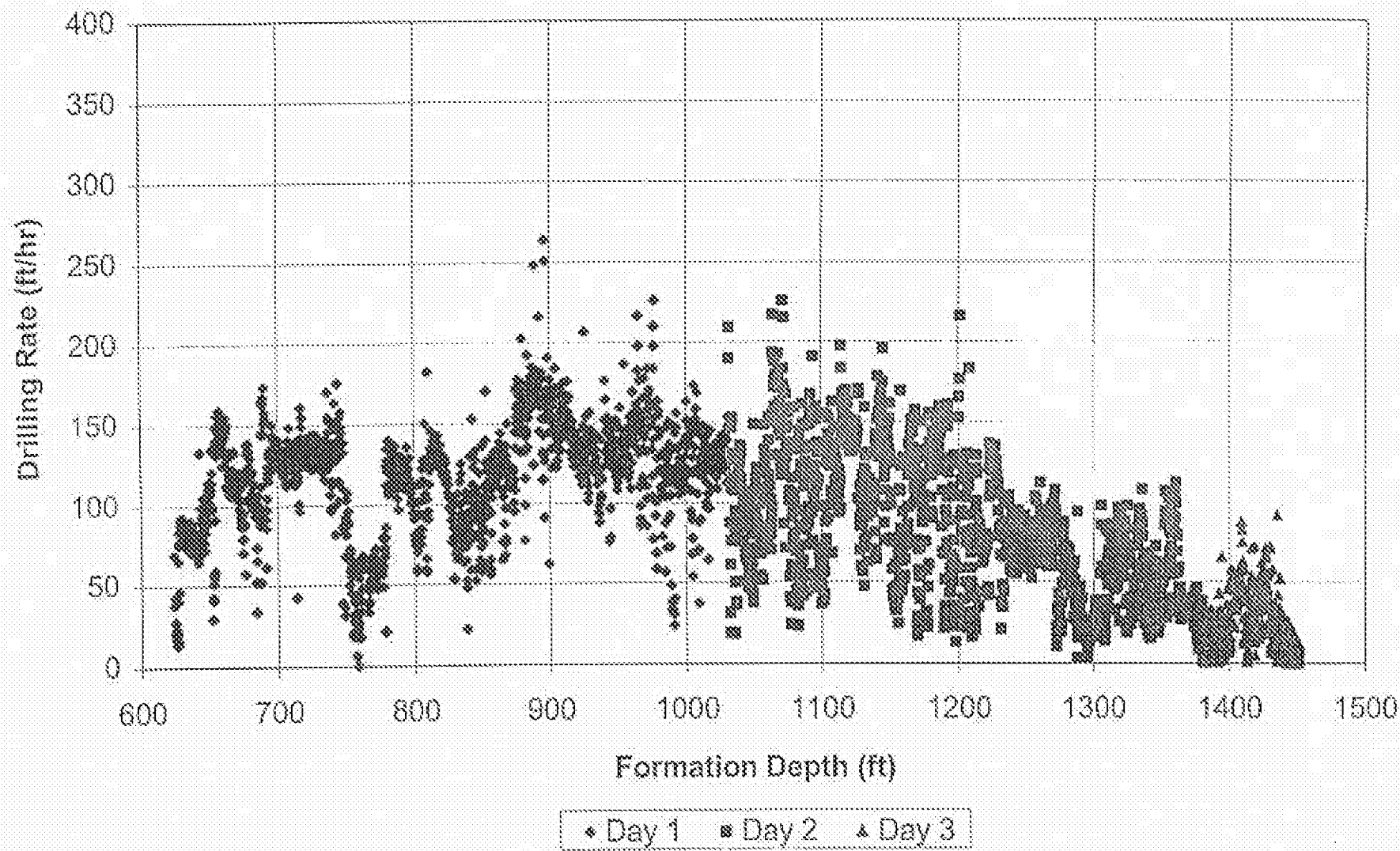
Bit Type = Walker McDowell M26RH
 Bit Size = 8.75
 Bit Nozzles = 3, 6, 12, 12
 Mud Type = Water Based
 Mud Weight (lb/gal) = 9.00
 Flow (GPM) = 1010.01
 Cost (hr) = 480.00

DOE high power mortar test Amaco Catoosa Test Site

TIME	BIT DEPTH	FLOW	PRES	SPEED	TORQUE	PEAK	DELTA	HOOK LOAD	PEAK	DELTA	WOB	PEAK	DELTA	ROP	Feet	Feet
MM:SS	FEET	GPM	PSI	RPM	ft-lbs	ft-lbs	ft-lbs	KIPS	G's	G's	KIPS	lbf/s	lbf/s	FT/MS	Depth	Depth
Well No. 23	Date: 09/27/08															
Starting Depth =	1482.40															
Ending Depth =	1450.00															
Total Depth Drilled	37.60															
Meters On Bit =	9.73															
Average ROP =	11.80															
Drilling (ft) =	1419.80								Collar (ft) =	408.50						
Bit Type =	Walker McClenahd MP58H															
Bit Size =	4.75															
Bit Nozzles =	6, 8, 12, 12															
Mud Type =	Water Based															
Mud Weight (lbs/gal)	8.98															
Pipe (ft) =	1010.82															
15:22:26	1450.44	107	1480	438	1167	1380	436	11.56	3.27	2.97	10.41	11.87	3.88	10.87	830.81	16.3116
15:22:56	1450.52	107	1432	430	1136	1368	422	11.55	3.28	4.54	10.40	11.83	3.26	6.60	830.57	16.3120
15:23:28	1450.54	108	1356	433	1069	1100	373	11.49	3.98	4.66	10.46	11.82	3.38	2.67	830.6	16.3282
15:23:58	1450.55	106	1397	434	1028	1198	284	11.48	4.62	4.83	10.46	11.84	3.26	1.79	830.61	16.3385
15:24:28	1450.57	108	1371	432	1076	1318	306	11.6	3.95	4.54	10.45	12.11	3.58	1.61	830.61	16.3448
15:24:58	1450.64	108	1368	432	1117	1283	336	10.68	3.81	3.28	11.26	13.59	4.43	3.59	830.62	16.3531
15:25:28	1450.58	108	1438	429	1159	1283	263	10	3.8	6.38	11.95	13.58	3.9	1.67	830.68	16.3614
15:25:58	1450.59	107	1448	430	1185	1295	267	10.91	3.85	4.17	11.85	13.50	3.54	0.36	830.68	16.3687
15:26:30	1450.51	107	1483	431	1183	1324	280	10.91	3.53	3.88	11.95	13.52	3.21	1.85	830.68	16.378
15:27:28	1450.32	109	953	429	918	1128	466	24.36	2.68	8.87	-2.27	-2.01	0.57	2.12	830.7	16.3788
15:27:58	1450.32	111	962	444	918	1150	506	24.16	3.04	8.6	-2.28	-2.03	0.53	-0.13	830.7	16.3789
15:28:28	1450	110	901	441	935	1166	494	24.17	2.56	8.57	-2.28	-2.91	0.55	-1.48	830.7	16.3789

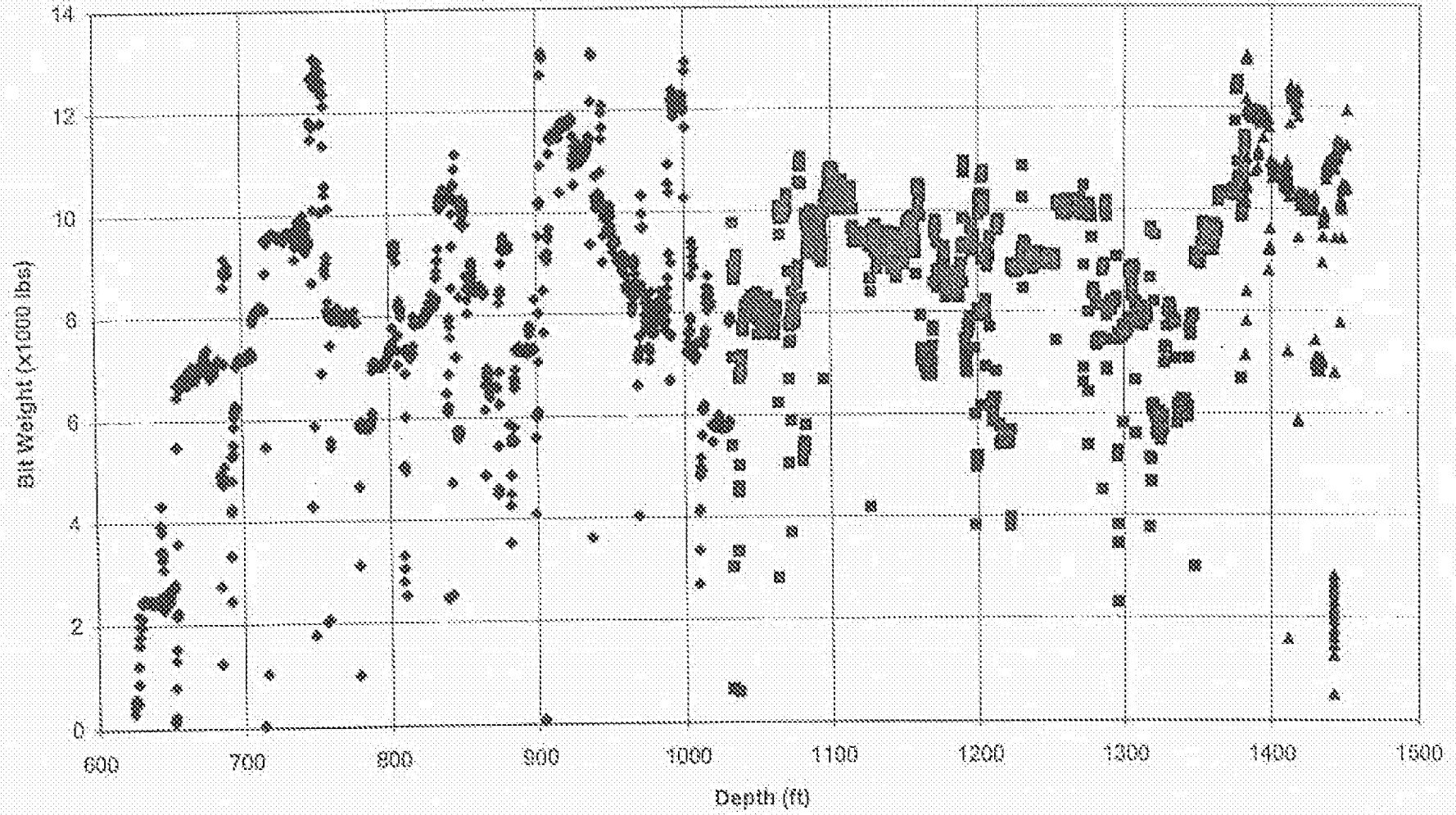
DOE Slim-Hole System Test

Prototype Test



Bit Weight As A Fuction Of Depth

Prototype Test



APPENDIX C
DOE High-Power Slim-Hole System
Catoosa Field Test No. 2

- BHA 1
- BHA 2
- BhA 3

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 1

Well No. 6		Date: 12/14/98 to 12/15/98		Bit Type = Walker McDaniel MP65H		Average ROP Excluding Hard Streak								
Starting Depth = 1586.53		Bit Size = 4.75		Bit Nozzles = 9, 9, 12, 12		Depth Drilled = 91.64								
Ending Depth = 1694.42		Mud Type = Water Based		Mud Weight (lb/gal) = 9.00		Hours On Bit = 3.38								
Total Depth Drilled = 97.79		Pipe (ft) = 883.16		Collar (ft) = 748.54		Average ROP = 27.32								
Hours On Bit = 4.2080		Calculated Speed (rpm)		Hook Load (Kips)		WOB (Kips)								
Average ROP = 20.81		Flow (gpm)		Pressure (psi)		Average WOB (Kips)								
Drilling (ft) = 1651.79		Instant. ROP (ft/hr)		Feet On Bit		Incremental Hours On Bit								
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
18:16:00	0.0000	1586.53	183	311	657	25.82	2.71		53.37	0.00	0.0000	0.0000		
18:16:10	0.0026	1586.58	108	319	395	28.81	-0.52		90.75	0.25	0.0026	0.0026		
18:17:07	0.0186	1587.14	86	993	313	29.27	-0.50		15.84	0.51	0.0186	0.0186		
18:18:07	0.0353	1588.90	78	849	288	28.83	-2.50		-14.13	0.27	0.0187	0.0353		
18:18:27	0.0408	1587.15	78	812	383	27.72	0.37	-0.88	-47.15	0.52	0.0356	0.0408		
18:18:32	0.0450	1587.41	77	831	387	27.88	0.21	-0.83	58.38	0.70	0.0442	0.0450		
18:18:45	0.0458	1587.86	78	831	388	27.90	-0.10	-0.54	335.10	1.00	0.0458	0.0458		22.47
18:18:50	0.0472	1587.92	78	832	289	27.87	0.12	-0.42	196.36	1.29	0.0614	0.0472		
18:18:52	0.0478	1588.17	78	835	288	27.70	0.08	0.10	362.50	1.54	0.0606	0.0478		
18:18:55	0.0486	1588.42	78	836	289	27.84	-0.12	0.00	303.66	1.79	0.0609	0.0486	36.82	
18:18:59	0.0497	1588.68	78	838	288	27.70	0.11	0.03	248.67	2.05	0.0613	0.0497	38.34	262.29
18:19:01	0.0503	1588.84	77	840	287	27.69	0.10	0.06	409.57	2.31	0.0606	0.0503	39.84	
18:19:04	0.0511	1589.19	79	839	290	27.88	-0.08	0.02	313.55	2.56	0.0608	0.0511	44.53	
18:19:10	0.0528	1589.44	79	841	291	27.71	0.09	0.02	151.37	2.81	0.0617	0.0528	191.73	
18:19:16	0.0544	1589.69	78	845	290	27.68	0.10	0.06	152.20	3.06	0.0617	0.0544	241.41	213.88
18:19:21	0.0559	1589.94	80	847	294	27.67	0.13	0.07	183.63	3.31	0.0614	0.0559	228.00	
18:19:23	0.0569	1589.19	80	850	295	27.68	0.11	0.07	208.71	3.56	0.0611	0.0569	213.49	
18:19:31	0.0586	1600.43	80	853	295	27.83	-0.01	0.05	184.99	3.82	0.0617	0.0586	210.46	
18:19:35	0.0597	1600.70	80	855	296	27.65	0.14	0.09	248.48	4.07	0.0611	0.0597	205.20	191.37
18:19:39	0.0609	1600.95	80	856	297	27.81	0.18	0.11	205.71	4.32	0.0611	0.0609	204.38	
18:19:41	0.0614	1601.20	81	858	298	27.80	0.18	0.12	356.81	4.57	0.0606	0.0614	203.45	
18:19:44	0.0622	1601.46	81	861	298	27.88	0.12	0.12	331.75	4.83	0.0608	0.0622	204.39	
18:19:59	0.0656	1601.71	81	867	298	27.59	0.12	0.15	77.35	5.08	0.0603	0.0656	177.65	
18:19:59	0.0661	1601.96	81	873	300	27.74	0.08	0.13	373.37	5.33	0.0606	0.0661	194.67	197.22
18:20:03	0.0678	1602.21	81	876	301	27.73	0.07	0.11	178.52	5.58	0.0614	0.0678	184.57	
18:20:13	0.0703	1602.47	82	882	302	27.66	0.14	0.10	68.20	5.84	0.0606	0.0703	171.00	
18:20:14	0.0708	1602.72	82	887	302	27.69	0.11	0.10	871.60	6.09	0.0603	0.0708	186.05	
18:20:26	0.0739	1602.97	82	883	303	27.89	-0.06	0.08	74.34	6.34	0.0603	0.0739	180.24	129.86
18:20:34	0.0751	1603.23	83	902	307	27.77	0.09	0.08	125.97	6.60	0.0622	0.0751	149.24	
18:20:39	0.0773	1603.48	83	908	307	27.72	0.09	0.08	188.16	6.85	0.0614	0.0773	141.52	
18:20:47	0.0787	1603.73	84	914	308	27.72	0.08	0.08	117.37	7.10	0.0622	0.0787	129.71	
18:20:55	0.0810	1603.99	84	925	311	27.58	0.21	0.07	114.12	7.35	0.0622	0.0810	139.12	128.62
18:21:00	0.0847	1604.24	85	937	312	27.72	0.09	0.10	90.90	7.61	0.0626	0.0847	122.51	

DOE high power mortar test Amaco Catoosa Test Site							DOE HP Motor No. 1							
Well No. 6	Date: 12/14/99 to 12/15/99													
Starting Depth =	1555.53					Bit Type =	Walker McDonald MPG&H			Average ROP Excluding Hard Street				
Ending Depth =	1559.42					Bit Size =	4.75							
Total Depth Drilled	37.79					Bit Nozzles =	9, 9, 12, 12			Depth Drilled =	61.84			
Hours On Bit =	4.7900					Mud Type =	Water Based			Hours On Bit =	2.36			
Average ROP =	20.51					Mud Weight (lb/gal) =	9.60			Average ROP	27.32			
Drilling (ft) =	1631.70					Pipe (ft) =	883.16	Dollar (ft) =	748.54					
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
18:21:17	0.0891	1604.43	86	953	317	27.52	0.18	0.19	76.77	7.89	0.0033	0.0921	118.92	
18:21:28	0.0911	1604.74	87	968	319	27.52	0.26	0.16	80.33	8.11	0.0031	0.0911	159.96	
18:21:30	0.0917	1604.89	87	975	319	27.54	0.28	0.20	426.43	8.36	0.0008	0.0917	167.53	192.86
18:21:34	0.0928	1605.25	87	989	320	27.59	0.23	0.21	362.63	8.63	0.0011	0.0928	120.71	
18:21:37	0.0936	1605.50	87	983	321	27.76	0.07	0.23	268.93	8.87	0.0008	0.0936	129.71	
18:21:41	0.0947	1605.75	87	987	320	27.62	0.18	0.20	244.93	9.13	0.0011	0.0947	131.81	
18:21:57	0.0992	1606.09	88	1099	323	27.66	0.13	0.18	56.20	9.37	0.0044	0.0992	116.74	134.67
18:22:21	0.1058	1606.25	89	1026	328	27.57	0.25	0.17	36.70	9.62	0.0067	0.1058	84.60	
18:22:49	0.1136	1606.51	90	1047	332	27.64	0.16	0.18	33.31	9.89	0.0078	0.1136	78.58	
18:23:19	0.1208	1606.75	92	1058	336	27.59	0.21	0.19	35.22	10.13	0.0073	0.1208	69.59	
18:23:27	0.1242	1607.04	93	1084	343	27.55	0.26	0.20	72.37	10.38	0.0013	0.1242	88.67	40.48
18:23:40	0.1278	1607.27	93	1094	341	27.54	0.21	0.22	70.92	10.64	0.0006	0.1278	63.14	
18:24:03	0.1339	1607.52	94	1109	345	27.53	0.25	0.22	41.43	10.89	0.0061	0.1339	66.32	
18:24:10	0.1376	1607.77	95	1127	349	27.55	0.24	0.23	74.14	11.14	0.0036	0.1376	51.72	
18:24:47	0.1464	1608.03	96	1147	362	27.61	0.16	0.23	39.62	11.40	0.0069	0.1464	44.33	43.60
18:24:48	0.1467	1608.29	97	1160	357	27.55	-0.05	-1.43	711.10	11.66	0.0003	0.1467	48.21	
18:25:48	0.1633	1608.45	98	1162	358	27.55	-0.94	-1.86	10.33	11.93	0.0167	0.1633	35.43	
18:26:14	0.1706	1608.71	98	1160	360	27.58	0.22	-1.97	38.19	12.20	0.0073	0.1706	38.63	
18:26:48	0.1810	1608.97	99	1167	362	27.53	0.26	-1.67	37.98	12.54	0.0094	0.1810	37.35	
18:27:11	0.1894	1609.22	99	1183	363	27.51	0.28	-1.66	40.11	12.89	0.0094	0.1894	35.92	29.79
18:27:29	0.1911	1609.47	99	1182	361	27.50	0.29	0.03	54.92	12.84	0.0047	0.1911	34.74	
18:28:02	0.2006	1609.73	100	1265	366	27.56	0.24	0.26	29.54	13.19	0.0094	0.2006	33.15	
18:28:24	0.2067	1609.98	99	1144	350	27.53	0.27	0.27	41.30	13.35	0.0061	0.2067	31.95	
18:28:58	0.2161	1610.23	99	1185	361	27.54	0.26	0.27	37.18	13.60	0.0094	0.2161	31.56	31.98
18:29:22	0.2228	1610.48	98	1144	353	27.59	0.20	0.25	37.07	13.85	0.0067	0.2228	29.77	
18:29:37	0.2269	1610.74	99	1180	361	27.54	0.26	0.24	60.17	14.11	0.0042	0.2269	35.84	
18:29:59	0.2331	1610.99	100	1202	366	27.50	0.28	0.25	41.53	14.36	0.0061	0.2331	38.48	
18:30:26	0.2406	1611.24	99	1183	362	27.50	0.29	0.26	33.02	14.61	0.0075	0.2406	37.49	41.32
18:30:53	0.2481	1611.49	99	1197	363	27.50	0.29	0.27	34.15	14.86	0.0078	0.2481	35.81	
18:31:08	0.2517	1611.74	100	1245	365	27.47	0.31	0.29	70.59	15.11	0.0036	0.2517	37.43	
18:31:21	0.2558	1611.99	101	1229	369	27.52	0.24	0.28	60.28	15.36	0.0042	0.2558	45.88	
18:31:45	0.2638	1612.25	100	1213	366	27.58	0.20	0.27	36.19	15.62	0.0089	0.2638	40.48	65.45

DOE high power mortar test Amaco Catroosa Test Site

DOE HP Motor No. 1

Well No. 5	Date: 12/22/09 to 12/15/09	HP Type =	Meteor MacGinnis HP-804	Average ROP Excluding Head Stroke										
Starting Depth =	1524.02	HP Size =	4.75	Depth Drilled =										
Ending Depth =	57.73	RI Location =	9.0.12.13	Hours On Bit =										
Total Depth Drilled	4.7300	Head Type =	Water Based	Average ROP										
Hours On Bit =	29.81	Head Weight (lbs) =	9.90	Hours On Bit =										
Average ROP =	1531.70	Diam (in) =	853.95	Average ROP										
Drilling (ft) =	1531.70													
Time (HH:MM:SS)	Start (Hours)	Bit Depth (feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (klbs)	WGS (klps)	Average WGS (klps)	Instant ROP (ft/hr)	Feed In Bit	Incremental Hours On Bit	Hours On Bit	Average ROP (ft/hr)	Per Foot ROP (ft/hr)
15:15:00	0.00:00	1525.63	183	21	657	22.82	-2.71	0.10	83.37	0.80	0.0000	0.0000		
15:16:10	0.00:28	1525.68	198	219	350	28.81	-0.52	0.10	90.75	0.25	0.0028	0.0028		
15:17:07	0.01:05	1527.14	89	693	313	28.37	-0.56	0.06	18.04	0.81	0.0105	0.0133		
15:18:07	0.01:53	1528.60	78	849	288	28.63	-2.56	-0.09	-14.15	0.27	0.0167	0.0300		
15:18:27	0.02:08	1529.15	75	812	293	27.72	-3.37	0.08	47.15	0.52	0.0056	0.0404		
15:18:42	0.02:30	1529.41	77	831	297	27.86	-0.61	-0.63	58.06	0.78	0.0042	0.0450		
15:18:45	0.02:38	1529.69	78	831	299	27.98	-0.10	-0.54	335.10	1.03	0.0006	0.0458		22.87
15:18:50	0.02:42	1529.92	78	832	299	27.87	0.12	-0.52	196.30	1.29	0.0054	0.0472		
15:18:52	0.02:43	1530.17	78	835	298	27.79	0.06	0.18	392.80	1.54	0.0066	0.0478		
15:18:55	0.02:48	1530.42	78	838	299	27.94	-0.12	0.03	391.68	1.79	0.0068	0.0482		
15:18:59	0.02:52	1530.68	78	838	299	27.70	0.14	0.02	246.57	2.05	0.0071	0.0497		
15:19:01	0.02:53	1530.94	77	835	287	27.89	0.10	0.05	405.52	2.31	0.0068	0.0503		
15:19:04	0.02:57	1531.19	79	838	290	27.88	-0.08	0.62	371.50	2.56	0.0068	0.0508		
15:19:10	0.03:03	1531.44	79	841	291	27.71	0.09	0.62	151.37	2.81	0.0077	0.0526		151.72
15:19:18	0.03:14	1531.69	78	845	296	27.68	0.10	0.66	159.30	3.06	0.0077	0.0544		241.43
15:19:21	0.03:23	1531.94	80	847	294	27.67	0.15	0.67	189.54	3.31	0.0078	0.0556		232.00
15:19:26	0.03:33	1532.19	80	856	295	27.68	0.11	0.67	505.71	3.58	0.0077	0.0569		332.46
15:19:31	0.03:45	1532.45	80	853	295	27.83	-0.01	0.68	154.98	3.82	0.0077	0.0585		210.48
15:19:33	0.03:57	1532.70	83	853	296	27.86	0.18	0.09	248.40	4.07	0.0077	0.0597		205.20
15:19:39	0.04:09	1532.95	81	856	297	27.61	0.16	0.11	205.71	4.32	0.0077	0.0611		204.20
15:19:41	0.04:24	1533.20	81	858	298	27.86	0.16	0.12	358.51	4.57	0.0078	0.0634		203.40
15:19:44	0.04:38	1533.46	81	861	298	27.85	0.12	0.12	331.73	4.83	0.0078	0.0658		204.60
15:19:48	0.04:56	1533.71	81	867	298	27.85	0.13	0.18	77.38	5.08	0.0078	0.0682		177.65
15:19:53	0.05:14	1533.96	81	873	300	27.74	0.08	0.13	373.27	5.33	0.0078	0.0706		154.57
15:20:00	0.05:36	1534.21	81	878	301	27.73	0.07	0.11	178.92	5.58	0.0078	0.0730		197.23
15:20:13	0.06:03	1534.47	82	892	302	27.66	0.14	0.10	98.29	5.86	0.0078	0.0754		171.90
15:20:14	0.06:27	1534.72	82	897	302	27.65	0.11	0.10	671.60	6.09	0.0078	0.0780		180.05
15:20:26	0.06:55	1534.97	82	893	303	27.89	-0.05	0.06	74.33	6.33	0.0078	0.0803		180.24
15:20:34	0.07:31	1535.23	83	892	307	27.77	0.04	0.06	195.97	6.63	0.0078	0.0827		188.06
15:20:38	0.07:55	1535.49	83	898	307	27.72	0.09	0.08	188.18	6.88	0.0078	0.0851		181.52
15:20:47	0.08:37	1535.74	84	913	308	27.72	0.06	0.05	117.37	7.13	0.0078	0.0875		156.71
15:20:55	0.09:19	1535.98	84	925	311	27.88	0.21	0.07	114.18	7.38	0.0078	0.0902		159.12
15:21:05	0.09:47	1536.24	85	937	312	27.72	0.09	0.10	60.56	7.61	0.0078	0.0928		152.51

DOE high power mortar test Amaco Catoosa Test Site											DOE HP Motor No. 1					
Well No. 8	Date: 12/14/98 to 12/15/98															
Starting Depth =	1808.63					Bit Type =	Wacker McDougald KIP68H					Average ROP Excluding Hard Streak				
Ending Depth =	1894.42					Bit Size =	4.75									
Total Depth Drilled	85.79					Bit Nozzles =	9, 9, 12, 12					Depth Drilled =	85.84			
Hours On Bit =	4.7889					Mud Type =	Water Based					Hours On Bit =	3.36			
Average ROP =	20.81					Mud Weight (lbs/gal) =	11.00					Average ROP	27.32			
Casing (ft) =	1831.76					Pipe (ft) =	883.16		Collar (ft) =	743.54						
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Fast On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)		
18:32:05	0.2681	1612.50	88	1184	380	27.61	0.15	0.24	48.43	15.87	0.0053	0.2681	43.70			
18:32:27	0.2742	1612.75	89	1185	383	27.54	0.25	0.24	40.59	16.12	0.0061	0.2742	44.17			
18:32:54	0.2817	1613.00	89	1191	382	27.54	0.25	0.22	33.73	16.37	0.0075	0.2817	41.30			
18:33:06	0.2859	1613.25	88	1179	389	27.49	0.29	0.23	78.75	16.63	0.0033	0.2859	43.70	45.45		
18:33:37	0.2899	1613.51	88	1180	380	27.55	0.23	0.24	28.55	16.88	0.0086	0.2899	42.79			
18:34:02	0.3006	1613.76	100	1153	365	27.69	0.27	0.26	35.80	17.13	0.0059	0.3006	43.24			
18:34:21	0.3058	1614.01	99	1180	361	27.51	0.27	0.26	46.30	17.38	0.0051	0.3058	41.61			
18:34:34	0.3094	1614.26	88	1189	360	27.47	0.32	0.28	66.77	17.63	0.0038	0.3094	42.34	40.91		
18:35:34	0.3261	1614.54	99	1331	361	28.82	1.89	0.60	4.99	17.71	0.0167	0.3261	33.00			
18:36:34	0.3428	1614.84	100	1442	367	29.08	3.57	1.26	0.20	17.71	0.0167	0.3428	24.62			
18:37:34	0.3594	1614.44	101	1393	369	34.89	2.79	1.77	5.73	17.91	0.0167	0.3594	19.82			
18:38:34	0.3761	1614.82	99	1367	364	24.86	2.73	2.28	4.68	17.86	0.0167	0.3761	18.09			
18:39:34	0.3928	1614.37	95	1311	359	28.36	2.34	2.88	3.03	17.94	0.0167	0.3928	12.18			
18:40:34	0.4094	1614.73	97	1317	358	24.80	2.88	2.88	9.36	18.08	0.0167	0.4094	10.38			
18:41:34	0.4261	1614.76	89	1323	358	25.14	2.85	2.68	3.36	18.13	0.0167	0.4261	7.96			
18:42:34	0.4428	1614.81	89	1320	360	25.32	2.38	2.58	2.94	18.18	0.0167	0.4428	3.84			
18:43:34	0.4594	1614.87	98	1300	358	25.64	2.07	2.44	3.27	18.24	0.0167	0.4594	4.07			
18:44:34	0.4761	1614.91	88	1319	353	24.88	2.82	2.84	2.55	18.28	0.0167	0.4761	3.80			
18:45:34	0.4928	1614.98	99	1240	363	24.64	1.03	2.57	3.85	18.35	0.0167	0.4928	4.27			
18:46:34	0.5094	1613.54	97	1182	353	27.60	-0.90	1.88	-86.29	16.91	0.0167	0.5094	-8.06			
18:48:57	0.5158	1613.78	104	1253	381	28.05	-1.11	-1.13	39.73	17.18	0.0084	0.5158	-5.22			
18:47:57	0.5325	1613.53	109	1361	396	28.11	-1.69	0.55	-68.07	16.89	0.0167	0.5325	-7.61			
18:48:39	0.5482	1612.77	109	1365	397	27.81	-0.01	-0.02	21.64	17.14	0.0117	0.5482	-6.98			
18:48:59	0.5485	1614.83	109	1351	397	27.95	0.32	-0.58	57.36	17.39	0.0044	0.5485	-6.34			
18:49:28	0.5572	1614.28	109	1356	398	27.59	0.16	-0.36	28.89	17.65	0.0066	0.5572	-4.81			
18:49:49	0.5639	1613.53	109	1399	399	27.97	0.31	-0.10	40.02	17.90	0.0064	0.5639	-3.26			
18:50:36	0.5764	1614.79	109	1374	398	27.98	0.20	0.15	19.78	18.16	0.0128	0.5764	-1.20			
18:51:36	0.5931	1614.96	109	1353	387	28.22	1.51	0.47	10.44	18.33	0.0167	0.5931	-9.30			
18:51:53	0.5981	1615.21	98	1398	353	22.21	4.88	1.40	51.61	18.58	0.0050	0.5981	15.66	3.29		
18:52:54	0.6150	1614.99	103	1364	375	24.97	2.26	1.81	-83.35	17.85	0.0189	0.6150	2.92			
18:53:54	0.6317	1614.94	113	1380	415	28.12	-0.42	1.89	-2.70	17.91	0.0167	0.6317	5.24			
18:54:27	0.6408	1614.29	113	1385	411	27.81	-0.02	1.54	27.85	17.86	0.0092	0.6408	5.38			

DOE high power motor test Amaco Catoosa Test Site										DOE HP Motor No. 1				
Well No. =	Date: 12/14/98 to 12/15/98													
Starting Depth =	1696.53				Bit Type =	Walker McCannale MF68H					Average ROP Excluding Hard Streak			
Ending Depth =	1694.42				Bit Size =	4.75								
Total Depth Drilled	97.79				Bit Nozzle =	9, 9, 12, 12					Depth Cooled =	21.84		
Hours On Bit =	4.7630				Mod Type =	Water Based					Hours On Bit =	3.36		
Average ROP =	20.51				Mod Weight (lb/gal) =	9.00					Average ROP =	27.32		
Drilling (ft) =	1631.70				Pipe (ft) =	883.15	Collar (ft) =	748.54						
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
18:54:40	0.6467	1614.56	113	1383	412	27.57	0.22	1.35	43.40	17.92	0.0038	0.6467	5.41	
18:55:08	0.6522	1614.80	113	1381	413	27.60	0.16	0.45	44.95	18.17	0.0038	0.6522	5.47	
18:55:49	0.6536	1615.05	113	1382	413	27.57	0.21	0.04	22.73	18.42	0.0114	0.6636	5.20	
18:56:49	0.6603	1615.16	102	1386	372	24.06	3.58	0.64	6.93	18.93	0.0167	0.6603	3.56	
18:57:36	0.6639	1615.41	93	1372	334	20.83	6.68	2.19	18.44	18.78	0.0136	0.6639	3.40	
18:58:36	0.7106	1614.77	114	1379	413	28.16	-0.96	1.94	-38.45	18.14	-0.0167	0.7106	-3.51	
18:59:36	0.7272	1614.89	29	596	182	28.44	-0.62	1.78	7.59	18.27	0.0167	0.7272	7.31	
19:00:36	0.7439	1614.79	71	766	294	28.10	-0.29	1.68	-8.34	18.15	0.0167	0.7439	6.68	
19:01:36	0.7606	1614.75	112	1355	409	26.06	-0.95	0.77	-2.76	18.12	0.0167	0.7606	3.64	
19:02:33	0.7731	1615.09	119	1387	413	27.86	-0.03	-0.57	20.32	18.37	0.0125	0.7731	3.68	
19:02:37	0.7769	1615.26	113	1369	410	27.84	0.14	-0.35	69.61	18.62	0.0039	0.7769	3.81	
19:03:39	0.7933	1615.59	111	1332	405	25.50	2.26	0.22	15.13	18.87	0.0164	0.7933	3.47	
19:04:09	0.8014	1615.75	110	1326	400	22.11	6.45	1.37	31.47	19.12	0.0081	0.8014	4.87	
19:04:13	0.8092	1616.09	109	1645	398	18.70	8.72	3.38	38.98	19.37	0.0079	0.8092	5.12	
19:04:59	0.8164	1616.28	109	1860	398	20.13	7.36	4.77	34.05	19.63	0.0072	0.8164	14.68	4.81
19:05:09	0.8231	1616.58	113	1519	411	26.39	0.35	4.82	-22.92	19.20	0.0167	0.8231	5.26	
19:11:56	0.9322	1615.92	112	1313	408	27.57	0.21	4.42	33.90	18.29	0.0092	0.9322	6.10	
19:12:07	0.9363	1616.17	112	1338	407	27.35	0.21	3.37	62.69	19.54	0.0061	0.9363	8.13	
19:12:47	0.9464	1616.43	111	1452	405	24.83	2.83	2.19	32.87	19.60	0.0111	0.9464	8.25	
19:13:12	0.9533	1616.68	111	1604	403	19.80	7.60	2.24	35.59	20.65	0.0069	0.9533	8.11	
19:13:39	0.9608	1616.93	110	1500	400	19.39	7.86	3.74	38.37	20.30	0.0075	0.9608	8.63	
19:14:12	0.9708	1617.18	111	1642	403	19.32	8.12	5.32	27.45	20.55	0.0062	0.9708	8.48	5.89
19:14:41	0.9781	1617.43	111	1648	404	19.20	8.23	6.93	31.75	20.80	0.0081	0.9781	8.47	
19:15:01	0.9838	1617.68	113	1820	407	20.76	9.55	7.67	49.00	21.05	0.0056	0.9838	3.49	
19:16:02	1.0006	1618.75	111	1946	404	20.21	9.62	7.38	-2.86	21.52	0.0169	1.0006	13.56	34.79
19:16:35	1.0057	1618.10	111	1746	405	22.48	5.88	8.72	28.80	21.77	0.0062	1.0057	22.60	
19:17:19	1.0194	1618.65	112	1785	407	18.77	7.88	6.63	26.90	22.62	0.0097	1.0194	28.47	
19:17:39	1.0272	1618.90	111	1835	403	19.80	7.88	8.56	33.17	22.27	0.0078	1.0272	39.56	
19:18:05	1.0347	1619.16	112	1803	406	21.94	5.80	6.91	33.62	22.69	0.0075	1.0347	30.47	29.56
19:18:29	1.0414	1619.41	111	1678	404	19.47	7.86	6.78	37.23	22.78	0.0067	1.0414	30.79	
19:19:00	1.0500	1619.66	112	1819	408	19.67	7.75	7.31	28.83	23.03	0.0066	1.0500	31.66	32.73

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 1

Well No. 8	Date: 12/14/98 to 12/15/98														
Starting Depth =	1695.83												Average ROP Excluding Hard Streak		
Ending Depth =	1694.42														
Total Depth Drilled	87.79												Depth Drilled =	81.84	
Hours On Bit =	4.7600												Hours On Bit =	3.36	
Average ROP =	20.91												Average ROP	27.32	
Drilling (ft) =	1631.70														

Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
8:18:08	1.0500	1618.81	119	1487	433	28.33	6.35		-35.91	22.18	0.0500	1.0500		
8:18:37	1.0506	1619.06	119	1492	433	28.53	-1.35		30.02	22.43	0.0066	1.0566		
8:19:37	1.0753	1619.85	119	1396	421	28.56	-1.91		-13.04	22.22	0.0167	1.0733		
8:19:58	1.0814	1619.11	110	1277	400	28.60	-0.93		43.99	22.48	0.0061	1.0814		
8:20:58	1.0981	1619.96	119	1280	400	28.29	-0.41	-0.75	-18.24	22.33	0.0167	1.0981		
8:21:07	1.1003	1619.31	111	1254	400	28.33	0.71	-0.68	198.70	22.68	0.0032	1.1003		
8:21:26	1.1056	1619.56	110	1285	400	28.34	0.72	-0.25	48.32	22.93	0.0033	1.1056		
8:22:09	1.1178	1619.81	110	1600	401	23.72	4.95	1.09	20.87	23.18	0.0119	1.1178		14.81
8:22:36	1.1259	1620.08	110	1786	400	20.79	7.77	2.75	33.72	23.43	0.0075	1.1259		
8:23:06	1.1333	1620.32	111	1773	404	20.35	8.18	4.37	29.77	23.68	0.0083	1.1333	18.12	
8:23:37	1.1419	1620.57	111	1758	404	21.84	7.65	5.75	39.88	23.94	0.0086	1.1419	18.12	
8:24:08	1.1508	1620.82	111	1781	405	22.95	8.07	8.00	28.87	24.19	0.0088	1.1508	36.17	30.85
8:24:36	1.1583	1621.07	111	1791	405	23.14	5.50	9.91	32.68	24.44	0.0078	1.1583	25.47	
8:25:10	1.1678	1621.32	112	1717	407	22.90	5.76	9.51	36.09	24.69	0.0094	1.1678	32.41	
8:25:39	1.1758	1621.57	111	1895	408	20.82	7.91	8.46	31.43	24.94	0.0081	1.1758	50.01	
8:26:02	1.1822	1621.82	112	1790	407	22.82	5.99	8.25	38.67	25.19	0.0084	1.1822	29.48	31.58
8:26:33	1.1908	1622.07	112	1743	409	23.38	8.22	8.08	29.33	25.44	0.0086	1.1908	50.62	
8:26:59	1.1981	1622.32	113	1960	412	21.31	7.39	8.42	35.33	25.69	0.0072	1.1981	30.94	
8:27:22	1.2044	1622.57	114	1777	415	23.47	5.18	6.31	38.28	25.94	0.0064	1.2044	31.64	
8:27:57	1.2142	1622.83	115	1769	417	23.28	5.37	5.90	26.10	26.20	0.0097	1.2142	31.25	31.69
8:28:24	1.2217	1623.08	115	1852	417	22.98	6.33	5.67	33.20	26.45	0.0073	1.2217	31.75	
8:28:47	1.2291	1623.33	115	1794	417	23.18	5.44	8.91	36.90	26.70	0.0084	1.2291	32.41	
8:29:24	1.2383	1623.58	115	1772	418	23.90	5.35	5.63	24.95	26.95	0.0103	1.2383	32.03	
8:29:51	1.2458	1623.83	115	1854	420	21.85	6.70	5.84	32.44	27.20	0.0075	1.2458	32.29	31.58
8:30:22	1.2544	1624.08	116	1780	421	24.28	4.38	5.64	29.31	27.45	0.0086	1.2544	31.29	
8:30:54	1.2633	1624.34	116	1789	421	23.13	5.45	5.47	28.95	27.71	0.0089	1.2633	31.31	
8:31:21	1.2708	1624.59	116	1867	420	22.69	5.95	5.97	33.69	27.96	0.0075	1.2708	23.19	
8:31:58	1.2811	1624.84	116	1745	422	28.43	4.30	5.46	24.54	28.21	0.0103	1.2811	29.61	28.03
8:32:32	1.2906	1625.09	117	1794	425	24.23	4.48	4.66	26.46	28.46	0.0091	1.2906	23.29	
8:33:07	1.3003	1625.34	118	1762	427	24.52	4.14	4.90	25.92	28.71	0.0097	1.3003	28.75	
8:33:44	1.3106	1625.60	117	1772	426	24.76	3.98	4.80	24.93	28.97	0.0103	1.3106	27.52	
8:34:08	1.3172	1625.85	118	1890	428	21.09	5.46	4.81	39.04	29.22	0.0087	1.3172	26.77	27.97

DOE high power motor test Amaco Cataosa Test Site										DOE HP Motor No. 1					
Well No. 5	Date: 12/14/98 to 12/15/98														
Starting Depth =	1596.63	Bit Type = Walker McDonald MP58H								Average ROP Excluding Hard Streak:					
Ending Depth =	1694.42	Bit Size = 4.75													
Total Depth Drilled	97.79	Bit Nozzles = 9, 9, 12, 12								Depth Drilled = 91.84					
Hours On Bit =	4.7000	Mud Type = Water Based								Hours On Bit = 3.38					
Average ROP =	20.81	Mud Weight (lb/gal) = 9.00								Average ROP = 27.32					
Drilling (ft) =	1831.70	Pipe (ft) = 883.16								Collar (ft) = 748.54					
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (fpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)	
8:34:31	1.3292	1826.10	116	1790	428	24.88	3.80	4.37	20.53	29.47	0.0119	1.3292	27.24		
8:35:40	1.3428	1826.35	117	1767	427	23.74	4.88	4.45	18.61	29.72	0.0136	1.3428	26.70		
8:36:09	1.3503	1826.60	117	1805	427	25.18	3.51	4.33	31.52	29.97	0.0081	1.3506	26.83		
8:37:09	1.3673	1826.81	117	1706	427	23.65	4.88	4.53	12.58	30.18	0.0167	1.3876	22.97	49.06	
8:37:47	1.3794	1827.17	118	1790	427	26.78	7.72	4.95	34.12	30.58	0.0106	1.3791	24.03	34.11	
8:50:34	1.3781	1831.79	113	1813	412	29.00	8.72		48.53	30.16	0.0000	1.3781			
8:51:34	1.3947	1831.57	113	1907	410	28.16	6.95		13.12	34.94	0.0167	1.3947			
8:52:34	1.4114	1831.59	112	1292	410	28.21	6.43		1.14	34.96	0.0167	1.4114			
8:53:34	1.4281	1831.79	112	1395	410	29.89	6.34		11.69	30.16	0.0167	1.4281			
8:54:17	1.4400	1832.34	112	1302	410	28.04	6.15	0.44	20.84	30.41	0.0119	1.4400			
8:55:09	1.4544	1832.26	113	1634	410	24.81	4.41	7.18	17.44	30.66	0.0144	1.4544			
8:56:08	1.4692	1832.54	113	1694	410	23.66	5.94	3.25	17.17	30.91	0.0147	1.4692			
8:56:43	1.4800	1832.78	113	1758	413	22.91	6.06	1.38	23.17	30.16	0.0108	1.4800		9.81	
8:57:14	1.4892	1833.04	113	1861	412	20.94	8.23	4.98	27.21	30.41	0.0092	1.4892			
8:57:47	1.4983	1833.28	114	1796	414	22.68	6.38	5.19	27.59	30.66	0.0092	1.4983	12.47		
8:58:00	1.5103	1833.55	114	1721	413	23.31	5.88	6.44	21.22	30.92	0.0139	1.5103	17.13		
8:59:01	1.5459	1834.90	114	1893	415	30.18	3.59	8.28	29.82	37.17	0.0089	1.5459	20.56	25.97	
8:59:36	1.5286	1834.05	115	1770	417	22.49	6.43	7.07	26.32	37.42	0.0097	1.5286	22.48		
9:00:27	1.5428	1834.30	114	1707	414	23.44	5.30	6.92	17.96	37.67	0.0142	1.5428	21.99		
9:01:04	1.5631	1834.55	115	1818	419	21.90	6.94	6.64	24.36	37.92	0.0103	1.5631	22.92		
9:01:38	1.5523	1834.80	115	1793	426	23.62	5.37	6.59	25.52	38.17	0.0094	1.5625	24.21	24.93	
9:02:24	1.5753	1835.06	115	1739	417	24.34	4.65	5.78	19.68	38.43	0.0128	1.5753	23.83		
9:03:11	1.5863	1835.31	116	1801	420	21.39	7.49	5.99	18.48	38.68	0.0131	1.5863	23.89		
9:04:04	1.6031	1835.56	116	1788	418	21.44	7.48	6.39	17.08	38.93	0.0147	1.6031	21.88		
9:04:35	1.6172	1835.81	116	1799	421	22.71	6.19	6.24	17.58	39.18	0.0142	1.6172	21.13	18.46	
9:05:06	1.6258	1836.07	115	1849	419	21.85	7.00	6.58	29.39	39.44	0.0086	1.6258	21.20		
9:05:38	1.6342	1836.32	119	1878	422	22.31	6.91	6.93	30.67	39.69	0.0083	1.6342	21.61		
9:06:23	1.6433	1836.57	118	1848	430	22.06	5.73	6.75	27.63	39.94	0.0092	1.6433	22.97		
9:06:51	1.6494	1836.82	117	2020	428	19.30	9.49	7.18	41.74	40.19	0.0081	1.6494	23.66	31.34	
9:07:13	1.6568	1837.07	117	2014	425	21.01	7.72	7.46	35.97	40.44	0.0081	1.6568	24.39		
9:07:38	1.6625	1837.32	119	1908	431	21.77	6.95	7.48	37.39	40.69	0.0089	1.6625	25.91		

DOE high power mortar test Amaco Catoosa Test Site							DOE HP Motor No. 1								
Well No. 6	Date: 12/14/88 to 12/15/88														
Starting Depth =	1596.83				Bit Type =	Walter McDougal MP58H							Average ROP Excluding Hard Streak		
Ending Depth =	1694.42				Bit Size =	4.75									
Total Depth Drilled	97.59				Bit Necks =	9, 9, 13, 12							Depth Drilled =	91.84	
Hours On Bit =	4.7086				Mud Type =	Water Based							Hours On Bit =	3.36	
Average ROP =	20.81				Mud Weight (lb/gal) =	8.06							Average ROP	27.33	
Circulating (ft) =	1631.79				Pipe (ft) =	883.18			Collar (ft) =	748.64					
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psf)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)	
9:08:04	1.6827	1637.58	115	1973	429	19.24	8.41	8.06	34.81	40.68	0.0072	1.6827	27.89		
9:08:30	1.6789	1637.52	115	1995	423	19.13	8.45	8.69	34.23	41.29	0.0072	1.6789	30.72	36.73	
9:09:03	1.6861	1638.08	117	1990	425	20.35	8.27	8.38	27.16	41.45	0.0092	1.6861	32.95		
9:09:33	1.6944	1638.33	115	1983	423	18.61	8.94	8.81	30.66	41.70	0.0083	1.6944	32.64		
9:09:55	1.7006	1638.59	118	1974	430	20.24	8.38	9.09	41.48	41.95	0.0081	1.7006	34.04		
9:10:24	1.7086	1638.83	117	1954	424	20.37	8.25	8.98	30.76	42.20	0.0081	1.7086	34.52	31.58	
9:10:47	1.7150	1639.09	119	1993	431	19.89	8.63	8.99	39.63	42.46	0.0064	1.7150	34.63		
9:11:08	1.7208	1639.34	119	1990	425	20.94	7.70	8.58	42.94	42.71	0.0058	1.7208	34.77		
9:11:32	1.7275	1639.59	117	1998	426	20.60	7.84	9.16	37.77	42.95	0.0067	1.7275	34.62		
9:11:53	1.7333	1639.84	118	1981	436	19.63	8.92	8.28	43.68	43.21	0.0058	1.7333	35.53	40.85	
9:12:13	1.7389	1640.09	117	1988	427	19.37	9.22	8.47	45.15	42.45	0.0056	1.7389	36.48		
9:12:38	1.7458	1640.35	117	1953	426	20.33	8.18	8.38	38.34	43.72	0.0069	1.7458	36.01		
9:12:59	1.7517	1640.60	118	1966	427	20.88	7.79	8.40	43.93	43.97	0.0068	1.7517	36.67		
9:13:21	1.7578	1640.85	117	2032	424	19.97	8.66	8.75	49.34	44.23	0.0061	1.7578	36.67	41.32	
9:13:45	1.7644	1641.10	120	1932	435	21.53	7.14	8.39	38.08	44.47	0.0067	1.7644	40.66		
9:14:12	1.7718	1641.35	119	1912	431	21.17	7.50	9.04	35.83	44.72	0.0075	1.7718	39.89		
9:14:33	1.7778	1641.60	119	2031	430	18.87	8.99	8.34	44.51	44.97	0.0059	1.7778	39.68		
9:15:09	1.7881	1641.85	119	1958	428	20.85	7.95	8.38	39.82	45.22	0.0083	1.7881	38.56	36.29	
9:15:29	1.7917	1642.10	117	2132	424	18.86	9.72	8.30	43.95	45.37	0.0058	1.7917	38.74		
9:15:59	1.8022	1642.36	117	1971	428	20.47	8.16	8.58	23.91	45.72	0.0105	1.8022	35.68		
9:16:32	1.8108	1642.60	118	2001	428	20.23	8.38	8.75	29.64	45.97	0.0086	1.8108	34.62		
9:17:01	1.8189	1642.85	117	2117	428	18.24	12.20	9.28	31.28	46.22	0.0061	1.8189	33.47	38.51	
9:17:25	1.8256	1643.10	116	2114	429	18.87	9.60	8.63	38.37	46.47	0.0067	1.8256	39.20		
9:17:59	1.8350	1643.35	118	2074	429	18.10	10.42	9.77	27.99	46.72	0.0094	1.8350	31.88		
9:18:23	1.8417	1643.61	119	2280	433	17.09	11.40	10.42	38.05	46.98	0.0067	1.8417	32.41		
9:18:40	1.8464	1643.86	120	2153	435	18.74	9.82	10.71	53.55	47.23	0.0047	1.8464	32.94	36.73	
9:19:04	1.8531	1644.11	117	2127	437	18.58	8.64	9.98	36.69	47.48	0.0087	1.8531	33.75		
9:19:27	1.8594	1644.37	116	2042	422	21.37	7.30	8.52	39.89	47.74	0.0064	1.8594	33.49		
9:19:46	1.8647	1644.62	118	2063	428	21.39	7.28	8.99	48.02	47.99	0.0033	1.8647	36.32		
9:20:11	1.8717	1644.87	120	1924	435	19.48	9.11	8.43	36.01	48.24	0.0069	1.8717	37.32	39.98	
9:20:29	1.8764	1645.12	116	2110	433	14.46	13.83	9.28	32.98	48.49	0.0078	1.8764	37.49		
9:20:59	1.8853	1645.37	115	2100	419	16.74	11.73	9.87	45.89	48.74	0.0091	1.8853	38.19		

DOE high power motor test Amaco Catoosa Test Site

DOE HP Motor No. 1

Well No. 5	Date: 12/14/88 to 12/15/88													
Starting Depth =	1598.63	Bit Type =	Walker McCosnair MP88H	Average ROP Excluding Hard Sizer										
Ending Depth =	1694.42	Bit Size =	4.75											
Total Depth Drilled	97.79	Bit Nozzle =	A, B, 12, 12	Depth Drilled = 81.84										
Hours On Bit =	4.7088	Mud Type =	Water Based	Hours On Bit = 3.35										
Average ROP =	30.81	Mud Weight (lb/gal) =	9.00	Average ROP = 27.33										
Drilling (ft) =	1631.78	Pipe (ft) =	883.16	Collar (ft) =	748.64									

Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WDB (Kips)	Average WDB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
9:21:24	1.8819	1645.63	118	2121	428	15.82	12.91	10.99	36.48	48.99	0.0080	1.8819	39.86	
9:21:44	1.8875	1645.87	116	2152	427	14.99	13.47	12.23	44.94	49.24	0.0058	1.8875	40.38	38.73
9:22:12	1.8953	1646.13	115	2191	427	17.85	10.88	12.59	32.71	49.49	0.0078	1.9033	38.38	
9:22:37	1.9122	1646.37	120	2109	438	16.55	12.88	12.38	35.39	49.74	0.0069	1.9132	38.20	
9:23:00	1.9188	1646.63	119	2177	430	15.03	12.41	12.51	40.72	50.00	0.0064	1.9188	38.20	
9:23:21	1.9244	1646.88	117	2052	426	18.70	8.89	11.71	41.88	50.25	0.0058	1.9244	37.84	37.48
9:23:42	1.9303	1647.13	118	2143	432	16.85	11.81	11.28	44.05	50.50	0.0058	1.9303	38.56	
9:23:51	1.9338	1647.39	114	2088	414	14.92	12.89	11.68	197.31	50.76	0.0026	1.9338	42.56	
9:24:49	1.9469	1647.89	119	2068	422	17.44	9.86	11.08	15.72	51.26	0.0191	1.9469	39.44	41.32
9:25:07	1.9538	1648.14	119	2082	434	17.34	11.78	10.83	48.74	51.51	0.0080	1.9538	40.69	
9:25:22	1.9591	1648.40	119	2062	432	17.41	11.99	11.27	61.16	51.77	0.0082	1.9591	41.78	
9:25:44	1.9643	1648.65	119	2128	432	15.84	12.79	11.46	40.93	52.02	0.0081	1.9643	42.86	
9:25:59	1.9683	1648.90	125	2113	435	16.46	12.11	11.89	58.02	52.27	0.0042	1.9683	45.09	81.94
9:26:19	1.9739	1649.15	119	2093	433	15.83	12.78	11.96	48.84	52.52	0.0058	1.9739	45.59	
9:26:42	1.9863	1649.40	118	2135	439	16.23	12.28	12.18	39.10	52.77	0.0064	1.9803	45.13	
9:27:03	1.9961	1649.65	117	2088	424	18.61	9.98	11.90	41.82	53.02	0.0088	1.9961	45.13	
9:27:27	1.9828	1649.90	118	2139	425	15.31	13.11	12.01	38.75	53.27	0.0087	1.9928	41.83	49.68
9:27:51	1.9884	1650.15	115	2179	420	15.10	13.31	12.27	37.73	53.52	0.0067	1.9884	44.75	
9:28:22	2.0061	1650.40	115	2147	417	16.22	13.19	12.36	25.17	53.77	0.0080	2.0061	41.72	
9:28:44	2.0142	1650.66	113	2245	422	17.31	11.18	12.15	41.35	54.03	0.0081	2.0142	40.26	
9:29:02	2.0188	1650.91	118	2089	426	20.40	8.23	11.80	50.35	54.28	0.0050	2.0188	41.09	38.27
9:29:33	2.0278	1651.16	118	1923	431	21.64	7.04	10.99	28.99	54.53	0.0068	2.0278	38.62	
9:29:49	2.0322	1651.41	119	2043	429	21.72	7.64	9.48	58.82	54.78	0.0044	2.0322	38.74	
9:30:14	2.0396	1651.67	119	1906	432	21.24	7.56	8.33	36.06	55.04	0.0089	2.0392	38.35	
9:30:38	2.0458	1651.92	117	2064	427	17.04	11.56	8.43	37.83	55.29	0.0087	2.0458	38.01	37.87
9:30:58	2.0508	1652.17	118	2170	428	17.15	11.53	9.97	48.71	55.54	0.0050	2.0508	39.10	
9:31:18	2.0564	1652.42	119	2005	429	20.07	8.88	9.39	48.34	55.79	0.0056	2.0564	39.86	
9:31:33	2.0611	1652.68	113	2100	413	22.28	8.84	9.19	52.28	56.05	0.0047	2.0611	42.07	
9:31:50	2.0658	1652.93	118	1977	427	22.92	8.70	9.02	53.91	56.30	0.0047	2.0658	41.84	88.80
9:32:10	2.0714	1653.18	113	1981	410	25.93	9.29	8.37	46.73	56.55	0.0056	2.0714	41.47	
9:32:28	2.0764	1653.44	118	2177	430	17.83	11.09	8.28	51.13	56.81	0.0050	2.0764	46.89	
9:32:50	2.0825	1653.69	118	2080	427	20.34	8.75	8.29	41.83	57.06	0.0061	2.0825	43.36	

DOE high power motor test Amaco Catoosa Test Site

DOE HP Motor No. 1

Well No. 6	Date: 12/14/98 to 12/15/98	Bit Type = Walker McDonald MP68H	Average ROP Excluding Hard Steak
Starting Depth = 1595.53	Bit Size = 4.75		
Ending Depth = 1694.42	Bit Nozzles = 9, 9, 12, 12		Depth Drilled = 98.84
Total Depth Drilled 97.79	Mud Type = Water Based		Hours On Bit = 3.36
Hours On Bit = 4.7000	Mud Weight (lb/gal) = 9.00		Average ROP = 27.32
Average ROP = 20.21	Pipe (in) = 863.16	Collar (ft) = 748.54	
Drilling (ft) = 9831.70			

Time (MM:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	TD Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
9:25:11	2.0883	1653.94	117	1974	429	21.59	7.28	8.42	43.68	57.31	0.0058	2.0883	46.17	46.29
9:25:29	2.0933	1654.26	118	2151	430	20.04	8.74	8.83	45.25	57.57	0.0056	2.0933	48.65	
9:31:53	2.1000	1654.45	112	2077	405	19.62	9.17	9.31	37.41	57.82	0.0087	2.1000	45.27	
9:34:34	2.1114	1654.70	120	1907	435	20.35	9.46	8.48	22.59	58.07	0.0134	2.1114	41.45	
9:34:56	2.1183	1654.85	121	2035	435	17.34	11.34	9.00	36.42	58.32	0.0069	2.1183	59.87	33.87
9:35:28	2.1294	1655.21	118	1959	430	17.16	11.49	9.84	31.54	58.58	0.0081	2.1294	37.85	
9:35:49	2.1322	1655.45	118	2169	428	14.85	13.81	10.87	42.93	58.83	0.0058	2.1322	37.49	
9:35:54	2.1392	1655.72	118	2174	430	14.23	14.29	11.90	36.18	59.09	0.0069	2.1392	36.32	
9:36:01	2.1467	1655.87	116	2100	423	15.03	12.50	12.32	30.36	59.34	0.0075	2.1467	35.53	39.00
9:37:11	2.1550	1656.22	115	2109	429	14.12	14.39	13.33	30.51	59.59	0.0083	2.1550	34.20	
9:37:32	2.1600	1656.47	119	2126	431	12.74	15.69	14.37	42.87	59.84	0.0058	2.1600	33.23	
9:37:47	2.1650	1656.73	117	2138	424	15.87	12.71	13.93	61.92	60.10	0.0042	2.1650	35.08	
9:38:04	2.1697	1656.98	114	2195	416	15.80	12.75	13.82	63.66	60.35	0.0047	2.1697	38.03	43.81
9:38:26	2.1758	1657.23	116	2102	400	15.38	13.18	13.74	41.13	60.60	0.0051	2.1758	38.65	
9:39:57	2.1844	1657.48	116	2147	418	13.87	14.83	13.79	29.55	60.85	0.0098	2.1844	39.10	
9:39:21	2.1913	1657.73	118	2155	422	13.82	14.54	13.62	37.11	61.10	0.0067	2.1913	38.55	
9:39:38	2.1958	1657.99	117	2150	427	14.68	13.81	13.84	54.53	61.36	0.0047	2.1958	40.06	36.88
9:40:11	2.2050	1658.24	116	2111	422	15.59	12.97	13.89	28.26	61.61	0.0092	2.2050	38.91	
9:40:38	2.2129	1658.49	117	2189	424	14.91	13.54	13.98	32.82	61.86	0.0075	2.2129	39.48	
9:41:18	2.2236	1658.75	117	2079	424	13.31	15.19	14.09	22.76	62.12	0.0111	2.2236	36.32	
9:41:49	2.2323	1659.00	117	2163	425	12.86	15.53	14.22	29.42	62.37	0.0088	2.2323	33.77	37.76
9:42:26	2.2408	1659.25	117	2086	427	13.58	15.01	14.45	28.86	62.62	0.0088	2.2408	31.82	
9:42:57	2.2511	1659.50	117	2089	427	14.33	14.15	14.69	24.47	62.87	0.0103	2.2511	30.15	
9:43:30	2.2603	1659.75	118	2134	428	13.23	15.29	15.01	27.34	63.12	0.0092	2.2603	29.90	
9:44:02	2.2692	1660.00	117	2099	426	13.30	15.19	15.01	29.00	63.37	0.0080	2.2692	29.08	27.67
9:44:31	2.2809	1660.30	117	2067	424	14.58	13.83	14.70	23.45	63.63	0.0108	2.2809	28.97	
9:45:12	2.2898	1660.51	118	2185	431	13.81	14.76	14.83	20.53	63.88	0.0089	2.2898	27.15	
9:45:38	2.2959	1660.76	117	2178	424	16.39	12.20	14.24	35.47	64.13	0.0072	2.2959	27.24	
9:45:56	2.3014	1661.01	115	2099	417	19.38	9.34	13.97	43.83	64.38	0.0106	2.3014	28.06	31.34
9:46:32	2.3108	1661.26	117	2120	408	17.18	11.45	12.32	25.01	64.63	0.0094	2.3108	28.75	
9:46:57	2.3179	1661.51	121	2143	439	18.62	10.55	11.87	36.20	64.88	0.0089	2.3179	29.37	
9:47:28	2.3264	1661.76	119	2009	434	20.63	8.70	10.47	25.51	65.13	0.0089	2.3264	30.02	

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 1

Well No. 5	Date: 12/14/88 to 12/15/88	Bit Type = Walker McCoscoald MFSBH	Average ROP Excluding Hard Streak
Starting Depth = 1696.83	Bit Size = 4.75		
Ending Depth = 1694.43	Bit Sizes = 9, 8, 12, 12	Mud Type = Water Based	Depth Drilled = 81.84
Total Depth Drilled = 97.79	Mud Weight (lbs/gal) = 8.00		Hours On Bit = 5.98
Hours On Bit = 4.7689	Pipe (ft) = 893.16	Collar (ft) = 748.54	Average ROP = 27.32
Average ROP = 20.81			
Drilling (ft) = 1631.70			

Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	16 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
9:47:53	2.3333	1692.91	118	2064	429	17.59	11.06	10.24	36.42	65.56	0.0066	2.3333	35.94	31.30
9:48:17	2.3400	1692.26	116	2088	422	18.17	12.42	10.85	37.08	65.53	0.0067	2.3400	31.91	
9:48:43	2.3472	1692.91	115	2067	419	17.91	11.66	10.89	36.17	65.88	0.0072	2.3472	33.47	
9:49:10	2.3547	1692.76	118	2048	428	17.96	11.98	11.08	32.43	66.13	0.0075	2.3547	34.03	
9:49:42	2.3626	1693.02	120	1943	435	18.07	10.61	11.46	28.54	66.39	0.0089	2.3626	33.24	33.38
10:03:26	2.3636	1693.09	114	1357	416	28.49	0.30		118.32	66.48	0.0050	2.3636		
10:03:32	2.3653	1693.34	119	1356	428	29.50	0.20		189.70	66.71	0.0017	2.3653		
10:04:32	2.3613	1693.12	118	1384	433	29.65	0.17		-13.11	66.49	0.0167	2.3613		
10:05:17	2.3944	1693.38	119	1381	433	28.78	0.04		20.18	66.75	0.0125	2.3944		
10:05:59	2.4061	1693.93	115	1663	419	21.19	8.32	1.41	21.50	67.00	0.0117	2.4061		
10:06:24	2.4131	1693.89	118	2083	428	14.85	14.48	4.24	38.08	67.25	0.0069	2.4131		
10:06:48	2.4197	1694.13	115	2149	417	14.30	14.93	7.19	38.82	67.50	0.0067	2.4197		18.93
10:06:51	2.4206	1694.40	118	2161	414	15.61	10.35	9.21	267.59	67.77	0.0008	2.4206		
10:07:52	2.4375	1694.56	118	2091	428	16.84	11.49	11.00	-0.33	68.03	0.0169	2.4375		
10:08:11	2.4428	1694.92	115	2177	420	14.80	14.35	13.10	45.64	68.29	0.0053	2.4428	23.12	
10:08:32	2.4485	1695.17	118	2147	428	17.06	12.32	12.65	44.18	68.54	0.0056	2.4485	21.96	35.00
10:09:09	2.4584	1695.42	117	2104	427	18.40	10.93	11.85	32.86	68.79	0.0070	2.4584	30.90	
10:09:19	2.4617	1695.97	120	2133	438	16.80	12.67	12.33	48.96	69.04	0.0053	2.4617	34.07	
10:09:39	2.4672	1696.32	120	2165	435	15.26	13.91	12.82	44.54	69.29	0.0059	2.4672	37.47	
10:10:08	2.4753	1696.17	121	2041	439	17.24	12.91	12.35	31.34	69.54	0.0061	2.4753	35.80	37.50
10:10:39	2.4816	1696.92	116	3061	418	18.10	14.03	12.71	28.74	69.79	0.0066	2.4816	35.89	
10:11:04	2.4906	1696.68	119	2312	432	12.44	16.60	13.84	37.10	70.04	0.0069	2.4906	32.44	
10:11:26	2.4975	1696.93	119	2126	433	14.41	14.75	14.28	37.59	70.30	0.0067	2.4975	37.83	
10:11:50	2.5038	1697.18	118	2626	426	11.65	17.37	14.95	41.89	70.55	0.0061	2.5038	37.15	35.65
10:49:47	2.5036	1696.90	118	1406	430	29.51	-0.02		15.48	69.97	0.0000	2.5036		
10:49:51	2.5047	1696.85	119	1403	431	29.83	0.88		230.52	70.22	0.0011	2.5047		
10:49:56	2.5068	1697.11	117	1406	428	29.80	0.39		223.05	70.48	0.0011	2.5068		
10:50:28	2.5150	1697.36	120	1928	435	26.04	3.57		26.21	70.73	0.0082	2.5150		
10:50:35	2.5226	1697.61	116	2007	421	20.56	9.31	3.73	32.82	70.98	0.0075	2.5226		
10:51:28	2.5308	1697.57	119	2072	431	19.63	11.27	4.98	31.17	71.24	0.0083	2.5308		

DOE high power mortar test Amaco Catoosa Test Site										DOE HP Motor No. 1				
Well No. 6	Date: 12/14/96 to 12/15/96													
Starting Depth =	1896.83									Bit Type =	Walsco McSwaind MP60H	Average ROP Excluding Hard Green		
Ending Depth =	1894.43									Bit Size =	4.75			
Total Depth Drilled	97.75									Bit Nozzles =	9, 9, 12, 12	Depth Drilled =	61.84	
Hours On Bit =	4.7000									Mod Type =	Water Based	Hours On Bit =	3.36	
Average ROP =	20.51									Mod Weight (lbs/gal) =	6.80	Average ROP	27.33	
Grilling (ft) =	1631.70									Pipe (ft) =	883.18	Collar (ft) =	748.54	
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
10:51:54	2.5388	1698.12	120	2035	438	19.96	9.73	6.85	31.17	71.48	0.0081	2.5388		43.06
10:52:27	2.5481	1698.37	117	1694	424	21.36	8.16	6.43	27.04	71.74	0.0082	2.5481		
10:52:56	2.5561	1698.63	116	2063	439	18.31	10.99	9.89	31.72	72.00	0.0081	2.5561		
10:53:18	2.5622	1698.88	117	2223	425	15.86	13.89	10.75	41.86	72.26	0.0081	2.5622	38.90	
10:53:44	2.5684	1699.13	119	2097	423	16.73	12.49	10.69	34.36	72.50	0.0072	2.5684	39.23	33.95
10:54:10	2.5767	1699.38	119	2135	419	18.26	12.64	11.63	33.89	72.75	0.0072	2.5767	32.05	
10:54:33	2.5811	1699.63	121	2178	449	15.72	13.45	12.69	40.95	73.00	0.0064	2.5811	33.96	
10:55:00	2.5908	1699.88	121	2129	449	17.45	11.00	12.85	34.03	73.25	0.0075	2.5908	33.96	
10:55:26	2.5986	1670.13	119	2053	430	17.58	11.71	12.48	30.62	73.50	0.0081	2.5986	33.54	34.29
10:55:53	2.6073	1670.38	117	2078	424	14.64	14.54	12.69	36.97	73.76	0.0087	2.6073	34.19	
10:56:18	2.6117	1670.64	119	2123	430	16.40	12.84	13.67	39.33	74.01	0.0084	2.6117	35.69	
10:56:48	2.6197	1670.89	119	2103	428	16.37	12.86	12.75	30.76	74.26	0.0081	2.6197	36.53	
10:57:09	2.6261	1671.14	118	2191	430	14.82	14.77	13.34	38.88	74.51	0.0084	2.6261	35.37	38.73
10:57:32	2.6328	1671.39	122	2134	441	16.69	12.53	13.51	36.63	74.76	0.0087	2.6328	36.59	
10:58:02	2.6411	1671.64	119	2022	434	17.83	11.49	12.90	29.43	75.01	0.0083	2.6411	35.07	
10:58:28	2.6475	1671.89	119	2203	431	14.24	14.91	13.21	39.68	75.26	0.0084	2.6475	35.07	
10:58:49	2.6539	1672.13	117	2134	425	15.91	13.26	13.41	39.23	75.52	0.0064	2.6539	36.84	36.35
10:59:21	2.6631	1672.40	119	2091	434	17.84	13.45	12.74	27.89	75.77	0.0082	2.6631	36.22	
10:59:47	2.6703	1672.65	117	2094	424	14.54	14.55	13.17	35.38	76.02	0.0072	2.6703	34.77	
11:00:14	2.6778	1672.90	119	2214	434	14.91	14.27	12.73	33.60	76.27	0.0075	2.6778	34.18	
11:00:40	2.6865	1673.16	119	2132	432	17.67	12.22	13.19	35.17	76.53	0.0072	2.6865	34.77	32.46
11:01:07	2.6925	1673.41	115	2167	419	16.27	12.99	13.12	33.73	76.78	0.0075	2.6925	34.18	
11:01:45	2.7031	1673.66	121	2057	436	16.89	13.30	13.29	23.47	77.03	0.0166	2.7031	32.30	
11:02:18	2.7132	1673.91	119	2116	426	14.88	14.38	13.23	27.68	77.28	0.0092	2.7132	31.92	
11:02:49	2.7183	1674.16	119	2183	422	16.68	12.62	12.90	39.60	77.53	0.0081	2.7183	32.05	36.09
11:03:08	2.7261	1674.41	122	2042	443	17.87	11.38	12.73	33.29	77.78	0.0076	2.7261	31.29	
11:03:25	2.7308	1674.66	116	2659	452	16.33	12.26	12.60	51.18	78.03	0.0047	2.7308	13.33	
11:04:08	2.7428	1674.92	118	2173	437	17.89	11.79	12.49	21.42	78.29	0.0119	2.7428	31.31	
11:04:36	2.7503	1675.17	120	2019	438	15.74	13.48	12.36	33.05	78.54	0.0075	2.7503	31.31	31.66
11:05:05	2.7581	1675.43	119	2194	433	13.07	15.16	12.81	39.59	78.80	0.0086	2.7581	30.72	
11:05:43	2.7682	1675.69	114	2389	415	14.30	14.85	13.51	25.06	79.05	0.0103	2.7682	29.61	
11:06:43	2.7858	1675.97	117	1502	428	26.42	1.33	11.31	-0.59	79.04	0.0167	2.7858	24.28	

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 1

Well No. 6	Date: 12/14/98 to 12/15/98													
Starting Depth =	1595.63	Bit Type =	Walker McDeenard MP68H		Average ROP Excluding Hard Strike									
Ending Depth =	1694.42	Bit Size =	4.75											
Total Depth Drilled	97.79	Bit Nozzles =	9, 9, 12, 12		Depth Drilled =		91.84							
Hours On Bit =	4.7000	Mud Type =	Water Based		Hours On Bit =		3.98							
Average ROP =	20.81	Mud Weight (lbs/gal) =	8.00		Average ROP =		27.32							
Diluting (H) =	1531.70	Pipe (H) =	383.18		Collar (H) =		748.54							

Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Klps)	WOB (Klps)	Average WOB (Klps)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
11:07:16	2.7950	1675.92	117	1828	426	22.15	7.33	10.43	27.53	79.29	0.0092	2.7950	24.28	
11:07:44	2.8028	1676.16	118	2059	421	19.13	10.22	9.78	32.65	79.53	0.0079	2.8028	23.92	19.24
11:08:10	2.8114	1676.43	116	2039	421	18.42	10.89	9.93	29.21	79.80	0.0086	2.8114	23.89	
11:08:51	2.8214	1676.68	121	1973	438	16.87	12.42	8.44	25.20	80.05	0.0100	2.8214	23.31	
11:09:09	2.8264	1676.93	120	2119	437	14.53	14.68	11.19	49.41	80.30	0.0050	2.8264	24.04	
11:09:34	2.8333	1677.18	120	2144	436	15.24	13.98	12.44	39.80	80.55	0.0069	2.8333	24.20	32.78
11:10:00	2.8419	1677.44	119	2095	433	15.87	13.29	13.85	29.65	80.81	0.0088	2.8419	24.26	
11:10:24	2.8473	1677.69	121	2114	439	13.54	15.48	13.87	46.53	81.06	0.0053	2.8473	25.79	
11:10:51	2.8547	1677.94	118	2150	432	16.46	12.79	14.04	34.04	81.31	0.0075	2.8547	25.95	
11:11:19	2.8635	1678.19	117	2098	432	15.87	15.47	13.20	32.13	81.56	0.0078	2.8635	26.23	34.03
11:11:42	2.8689	1678.44	119	2154	432	15.05	13.87	13.15	38.41	81.81	0.0064	2.8689	26.18	
11:12:10	2.8787	1678.69	121	2095	430	18.50	10.85	12.83	32.89	82.06	0.0078	2.8787	24.62	
11:12:49	2.8875	1678.95	121	1918	439	21.51	7.97	11.10	23.56	82.32	0.0108	2.8875	24.34	
11:13:27	2.8981	1679.20	119	2064	433	18.44	10.88	10.74	23.97	82.57	0.0168	2.8981	24.67	28.41
11:14:05	2.9088	1679.46	117	2108	425	17.82	11.82	10.97	33.00	82.83	0.0070	2.9088	24.45	
11:14:28	2.9144	1679.71	119	1968	434	18.69	10.83	10.39	29.96	83.08	0.0080	2.9144	24.31	
11:14:59	2.9209	1679.96	120	2129	437	19.37	12.85	10.79	40.40	83.33	0.0064	2.9209	25.64	
11:15:15	2.9269	1680.22	120	2043	436	19.34	9.99	11.70	32.02	83.58	0.0081	2.9269	25.74	33.02
11:15:47	2.9369	1680.47	118	2083	430	16.85	12.37	11.46	31.83	83.84	0.0081	2.9369	26.81	
11:16:09	2.9431	1680.73	121	2123	438	19.55	12.86	11.70	41.99	84.10	0.0061	2.9431	26.89	
11:16:45	2.9539	1680.98	118	2160	430	19.48	12.75	12.13	30.19	84.35	0.0108	2.9539	28.60	
11:17:20	2.9628	1681.24	118	2133	428	18.18	14.94	12.54	27.96	84.61	0.0089	2.9628	30.42	35.19
11:18:06	2.9758	1681.48	117	2085	424	12.62	19.44	13.83	20.03	84.86	0.0128	2.9758	29.95	
11:18:47	2.9864	1681.74	120	2090	438	11.52	17.47	14.85	22.01	85.11	0.0114	2.9864	28.11	
11:19:43	3.0031	1681.99	119	2025	431	12.74	16.21	15.86	15.70	85.36	0.0151	3.0031	28.73	
11:20:23	3.0136	1682.25	119	2060	430	11.20	17.79	19.97	23.79	85.62	0.0186	3.0136	24.82	19.87
11:21:03	3.0247	1682.50	118	1993	429	10.72	18.24	17.83	22.94	85.87	0.0111	3.0247	23.79	
11:22:03	3.0414	1682.88	116	1978	430	10.38	18.77	16.19	16.95	86.13	0.0187	3.0414	21.16	
11:22:51	3.0547	1683.33	116	1988	430	10.85	18.99	18.26	18.59	86.38	0.0133	3.0547	19.79	
11:23:29	3.0644	1683.18	118	2132	430	12.34	16.79	17.98	28.49	86.63	0.0097	3.0644	19.50	
11:24:26	3.0811	1683.29	117	1947	424	22.47	9.99	15.82	8.61	86.88	0.0167	3.0811	17.32	15.41
11:25:20	3.0961	1683.55	117	1801	425	18.17	9.49	14.07	18.69	87.12	0.0150	3.0961	17.00	

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 1

Well No. 8	Date: 12/14/88 to 12/15/88													
Starting Depth =	1598.63	Bit Type =	Walker McCleanair MP68H	Average ROP Excluding Hard Streak										
Ending Depth =	1684.42	Bit Size =	4.75											
Total Depth Drilled	97.78	Bit Nozzles =	9, 9, 12, 12										Depth Drilled =	81.84
Hours On Bit =	4.7600	Mud Type =	Water Based										Hours On Bit =	3.36
Average ROP =	20.81	Mud Weight (lb/gal) =	9.00										Average ROP	27.32
Dialstring (ft) =	1631.76	Pipe (ft) =	883.16	Collar (ft) =	748.54									

Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOR (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
11:26:20	3.1128	1683.64	118	1999	430	16.29	12.67	12.55	8.84	87.01	0.0167	3.1128	15.40	
11:26:59	3.1236	1683.86	119	2014	433	15.72	15.95	12.27	23.59	87.26	0.0108	3.1236	15.76	
11:27:23	3.1303	1684.14	119	2157	426	16.76	12.45	11.40	36.73	87.51	0.0097	3.1303	16.20	
11:28:17	3.1453	1684.39	121	2018	441	16.31	12.31	12.46	16.70	87.76	0.0150	3.1453	15.68	17.14
11:28:52	3.1550	1684.65	118	2112	435	16.76	13.48	13.66	28.20	88.02	0.0097	3.1550	17.34	
11:29:22	3.1635	1684.90	119	1970	434	18.36	10.90	12.71	50.19	88.27	0.0083	3.1635	18.14	
11:30:16	3.1783	1685.15	119	1900	433	15.62	13.52	12.33	19.68	88.52	0.0100	3.1783	17.30	
11:31:10	3.1930	1685.39	118	1706	430	25.77	8.80	10.60	5.08	88.56	0.0167	3.1930	17.09	
11:31:55	3.2058	1685.46	121	1884	441	19.89	9.38	10.02	22.54	88.85	0.0168	3.2058	17.89	16.50
11:32:26	3.2144	1685.74	115	2221	419	16.31	13.86	10.29	20.31	89.11	0.0086	3.2144	20.66	
11:33:26	3.2311	1685.90	118	1421	429	29.30	8.44	8.20	-14.42	89.37	0.0167	3.2311	14.98	
11:33:38	3.2344	1685.75	124	1392	450	29.17	8.61	5.62	79.04	89.32	0.0033	3.2344	15.26	
11:34:35	3.2503	1686.00	118	1785	429	21.48	7.94	6.45	15.85	89.37	0.0158	3.2503	15.33	
11:35:10	3.2600	1686.25	120	1648	405	19.37	9.45	6.47	28.83	89.62	0.0097	3.2600	15.24	
11:35:10	3.2757	1686.45	117	1987	426	16.75	12.44	8.18	11.70	89.88	0.0167	3.2757	13.88	13.89
11:35:38	3.2900	1686.70	119	1979	432	18.20	11.09	8.36	19.27	90.07	0.0133	3.2900	13.88	
11:37:33	3.2997	1686.95	115	1902	421	20.56	8.80	9.84	25.36	90.32	0.0097	3.2997	16.42	
11:38:09	3.3097	1687.20	119	1900	425	20.62	8.49	10.64	35.42	90.59	0.0100	3.3097	16.56	
11:39:00	3.3258	1687.45	118	1881	428	19.43	9.88	10.12	17.67	90.84	0.0142	3.3258	15.73	21.35
11:39:37	3.3342	1687.71	119	1898	432	20.97	8.43	9.32	24.36	91.08	0.0103	3.3342	21.44	
11:40:14	3.3444	1687.86	121	1883	441	21.83	7.58	8.63	35.67	91.31	0.0103	3.3444	20.89	
11:40:38	3.3514	1688.24	117	1938	424	21.37	7.83	8.44	35.83	91.58	0.0069	3.3514	21.86	
11:41:14	3.3611	1688.47	119	1913	434	25.65	8.74	8.50	25.87	91.84	0.0097	3.3611	21.93	27.13
11:42:01	3.3742	1688.72	118	1809	426	20.94	8.44	8.21	19.52	92.08	0.0131	3.3742	23.28	
11:42:39	3.3839	1688.97	119	1906	431	20.89	8.50	8.22	23.53	92.34	0.0087	3.3839	24.18	
11:43:08	3.3938	1689.22	118	1933	427	20.54	8.26	8.49	28.26	92.59	0.0089	3.3938	24.10	
11:44:08	3.4094	1689.35	120	1930	435	20.86	9.27	8.75	7.73	92.82	0.0167	3.4094	21.98	
11:45:09	3.4251	1689.35	115	1996	419	18.98	10.33	9.06	-0.07	92.72	0.0167	3.4251	19.49	
11:45:08	3.4428	1689.41	120	2007	435	20.38	9.25	8.24	3.74	92.76	0.0167	3.4428	15.63	
11:47:09	3.4584	1689.48	118	2008	431	21.64	7.78	8.10	2.87	92.83	0.0167	3.4584	13.04	19.07
11:48:09	3.4761	1689.53	118	1807	427	26.95	3.86	7.86	-7.75	92.76	0.0167	3.4761	8.88	
11:49:08	3.4919	1689.56	120	1881	434	25.34	4.01	6.81	17.41	92.97	0.0158	3.4919	8.54	

DOE high power motor test Amaco Cataosa Test Site

DOE HP Motor No. 1

Well No. 6	Date: 12/14/98 to 12/15/98			
Starting Depth =	1596.53	Bit Type =	Walker McDonald MP06H	Average ROP Excluding Hoist Street
Ending Depth =	1694.42	Bit Size =	4.75	
Total Depth Drilled	97.75	Bit Nozzles =	9, 9, 12, 12	Depth Drilled = 91.84
Hours On Bit =	4.7000	Mud Type =	Water Based	Hours On Bit = 3.35
Average ROP =	20.81	Mud Weight (lbs/gal) =	9.38	Average ROP = 27.32
Drillstring (ft) =	1631.70	Pipe (ft) =	883.16	Collar (ft) = 748.54

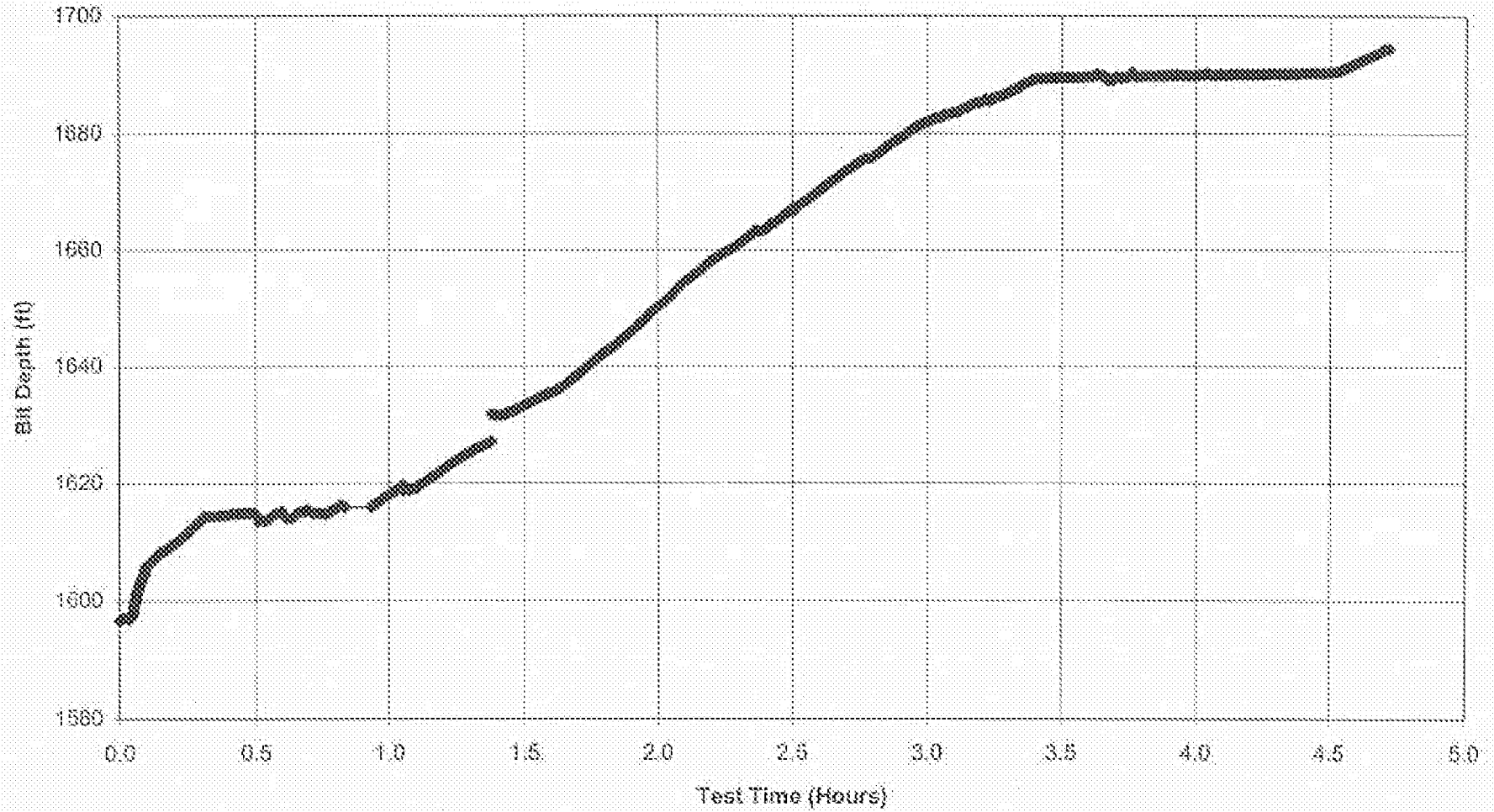
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (klips)	WOB (klips)	Average WOB (klips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
11:50:09	3.3089	1599.53	120	1991	437	20.06	5.22	5.76	-37.02	92.57	0.0169	3.5055	5.73	
11:51:09	3.3206	1599.54	119	2022	425	19.44	6.83	5.90	2.43	92.91	0.0167	3.5258	4.02	
11:52:06	3.3422	1599.54	119	2067	432	19.26	10.95	6.53	-0.16	92.91	0.0167	3.5422	2.34	
11:53:06	3.3589	1599.53	118	2020	423	19.27	9.44	7.89	0.66	92.92	0.0167	3.5589	1.34	
11:54:06	3.3756	1599.53	118	1974	430	21.10	8.25	8.74	2.59	92.98	0.0167	3.5756	1.81	
11:55:06	3.3922	1599.73	118	1962	428	22.14	7.29	9.15	8.99	93.10	0.0167	3.5922	2.14	
11:56:06	3.4089	1599.53	119	2010	433	21.39	7.99	8.78	-3.91	93.05	0.0167	3.6089	1.47	
11:57:03	3.4347	1599.93	121	1982	438	22.10	7.10	8.61	15.80	93.30	0.0158	3.6247	4.04	
11:57:27	3.4300	1599.18	124	1956	451	22.00	3.99	6.92	47.49	93.56	0.0053	3.6300	4.20	
11:58:23	3.4407	1599.71	119	1905	452	22.88	6.77	6.83	-28.32	93.08	0.0167	3.6407	1.92	
11:58:43	3.4525	1599.96	120	1546	436	28.45	-0.91	4.98	43.20	93.33	0.0058	3.6525	3.31	
11:59:43	3.4632	1599.10	119	1392	433	29.32	-0.58	3.27	-61.72	92.47	0.0167	3.6632	-1.47	
11:59:50	3.4711	1599.57	121	1365	440	25.40	-1.43	1.96	144.29	92.74	0.0019	3.6711	-1.80	
12:00:30	3.4878	1599.14	120	1375	434	29.40	-1.51	9.50	-29.23	92.51	0.0167	3.6878	-4.01	
12:01:19	3.4959	1599.40	118	1375	430	29.20	0.33	-0.78	31.09	92.77	0.0091	3.6959	-3.16	
12:01:30	3.4989	1599.65	119	1373	432	29.36	-1.64	-0.93	69.22	93.03	0.0031	3.6989	-0.33	
12:02:30	3.7156	1599.28	121	1373	438	29.25	-0.04	-0.82	-31.64	92.75	0.0167	3.7156	-6.08	
12:03:08	3.7261	1599.63	119	1372	434	29.66	0.04	-0.40	23.77	93.00	0.0108	3.7261	-5.72	
12:04:08	3.7428	1599.63	120	1359	436	26.64	3.00	0.46	0.11	93.00	0.0167	3.7428	-0.33	
12:04:53	3.7553	1599.89	118	2026	429	19.64	9.55	2.30	21.01	93.28	0.0125	3.7553	-0.68	1.35
12:05:07	3.7582	1599.46	118	2036	429	20.13	4.40	3.81	86.37	93.77	0.0039	3.7582	14.44	
12:06:07	3.7758	1599.76	121	2003	439	19.06	9.59	5.43	-41.45	93.07	0.0167	3.7758	3.16	
12:07:07	3.7925	1599.76	119	2018	432	19.91	9.44	7.16	3.23	93.13	0.0167	3.7925	5.02	
12:08:07	3.8092	1599.76	119	1991	430	20.52	8.85	8.35	2.12	93.16	0.0167	3.8092	3.24	
12:09:07	3.8258	1599.20	117	2094	424	19.76	9.60	6.36	9.54	93.17	0.0167	3.8258	1.18	
12:10:07	3.8425	1599.77	119	2060	424	20.35	9.01	9.28	-1.82	93.14	0.0167	3.8425	3.97	
12:11:07	3.8582	1599.87	120	2011	437	20.92	8.47	9.07	-5.87	93.24	0.0167	3.8582	1.20	
12:12:07	3.8750	1599.86	118	2030	439	20.44	8.94	8.97	-0.57	93.23	0.0167	3.8750	1.73	
12:13:07	3.8925	1599.92	118	2018	428	20.60	8.80	8.66	3.69	93.29	0.0167	3.8925	0.22	
12:14:07	3.9062	1599.91	118	2010	428	20.55	8.88	8.62	-1.13	93.29	0.0167	3.9062	-3.27	
12:15:07	3.9258	1599.82	119	2026	432	19.38	9.99	9.01	0.78	93.29	0.0167	3.9258	1.47	
12:16:07	3.9425	1599.82	120	2030	434	19.85	8.81	9.22	0.29	93.29	0.0167	3.9425	1.07	

DOE high power motor test Amaco Catoosa Test Site										DOE HP Motor No. 1						
Well No. 6		Date: 12/14/98 to 12/15/98														
Starting Depth = 1598.63					Bit Type = Walker McDougald MPESH					Average ROP Excluding Hard Streak						
Ending Depth = 1684.42					Bit Size = 4.75											
Total Depth Drilled = 87.79					Bit Nozzles = 9, 9, 12, 12					Depth Drilled = 91.54						
Hours On Bit = 4.7010					Mud Type = Water Based					Hours On Bit = 3.36						
Average ROP = 20.81					Mud Weight (lb/gal) = 9.02					Average ROP = 27.32						
Drillstring (ft) = 1631.70					Pipe (ft) = 883.16					Collar (ft) = 748.54						
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)		
12:17:07	3.9592	1689.92	119	2035	434	19.99	9.38	9.31	-0.34	93.29	0.0167	3.9592	0.87			
12:18:07	3.9738	1689.91	118	2009	429	20.26	9.10	9.37	-0.49	93.28	0.0167	3.9738	0.73			
12:19:07	3.9885	1689.87	120	2034	436	20.29	9.10	9.42	-2.47	93.24	0.0167	3.9885	0.67			
12:20:07	4.0032	1689.92	119	2039	434	20.61	8.78	9.17	2.13	93.26	0.0167	4.0032	0.83	0.10		
12:21:07	4.0208	1689.98	119	2007	433	20.60	8.75	9.02	3.86	93.35	0.0167	4.0208	0.80			
12:22:01	4.0408	1689.34	119	2007	430	20.41	8.68	8.88	17.46	93.61	0.0150	4.0408	2.18			
12:23:01	4.0575	1689.94	117	2008	427	20.39	8.41	8.78	-38.71	93.11	0.0167	4.0575	0.39			
12:24:01	4.0742	1689.92	119	2004	431	19.75	8.59	8.84	4.86	93.38	0.0167	4.0742	0.67			
12:25:01	4.0908	1689.97	116	2012	423	19.32	8.96	9.28	3.08	93.44	0.0167	4.0908	1.01			
12:26:01	4.1075	1689.96	120	2008	435	18.37	10.92	9.71	-6.55	93.33	0.0167	4.1075	0.27			
12:27:01	4.1242	1689.96	117	2086	432	18.44	10.84	10.14	6.83	93.43	0.0167	4.1242	1.01			
12:28:01	4.1408	1689.98	118	2034	428	19.10	10.14	10.49	-0.24	93.43	0.0167	4.1408	1.26			
12:29:01	4.1575	1689.98	123	2034	440	19.79	9.61	10.49	1.41	93.35	0.0167	4.1575	1.08			
12:30:01	4.1742	1689.98	118	2038	428	19.85	9.88	10.26	0.24	93.48	0.0167	4.1742	0.67			
12:31:01	4.1908	1689.10	120	2039	435	19.89	9.86	10.67	2.93	93.50	0.0167	4.1908	-0.73			
12:32:01	4.2075	1689.07	120	2033	437	19.19	10.14	9.93	-3.98	93.44	0.0167	4.2075	0.67			
12:33:01	4.2242	1689.10	116	2033	421	18.89	10.36	9.97	3.24	93.49	0.0167	4.2242	0.67			
12:34:01	4.2408	1689.12	120	2093	438	17.31	11.66	10.84	-0.20	93.49	0.0167	4.2408	0.39			
12:35:01	4.2575	1689.10	119	2134	430	17.89	11.40	10.74	-1.04	93.47	0.0167	4.2575	0.33			
12:36:01	4.2742	1689.17	115	2091	419	18.82	10.78	10.82	3.93	93.54	0.0167	4.2742	0.73			
12:37:01	4.2908	1689.20	118	2053	428	19.09	10.38	10.95	2.19	93.67	0.0167	4.2908	0.93			
12:38:01	4.3075	1689.18	119	2038	432	19.43	9.84	10.85	-1.66	93.56	0.0167	4.3075	0.67			
12:39:01	4.3242	1689.19	117	2017	427	19.60	8.73	10.43	5.64	93.66	0.0167	4.3242	0.73			
12:40:01	4.3408	1689.15	120	2026	435	19.13	10.20	10.17	-2.09	93.52	0.0167	4.3408	0.13			
12:41:01	4.3575	1689.21	116	2117	422	19.41	12.81	10.97	3.20	93.56	0.0167	4.3575	0.23			
12:42:01	4.3742	1689.23	118	2206	429	14.65	14.40	11.41	1.38	93.60	0.0167	4.3742	0.73			
12:43:01	4.3908	1689.34	115	2256	430	14.46	14.86	12.38	6.89	93.71	0.0167	4.3908	1.47			
12:44:01	4.4075	1689.26	118	2392	432	14.85	14.28	13.28	-6.49	93.62	0.0167	4.4075	1.60			
12:45:01	4.4242	1689.15	119	2282	434	15.24	13.91	14.83	-5.88	93.72	0.0167	4.4242	1.36			
12:46:01	4.4408	1689.23	115	2240	418	14.85	14.29	14.33	-1.26	93.70	0.0167	4.4408	0.67			
12:47:01	4.4575	1689.31	119	2288	432	13.65	15.24	14.48	-1.09	93.88	0.0167	4.4575	0.87			
12:48:01	4.4742	1689.33	116	2346	420	14.08	15.02	14.55	-1.31	93.70	0.0167	4.4742	0.93			

DOE high power motor test Amaco Catoosa Test Site										DOE HP Motor No. 1				
Well No. 5	Date: 12/14/88 to 12/15/88													
Starting Depth =	1856.83			Bit Type = Walker McDonald MP68H						Average ROP Excluding Hard Streaks				
Ending Depth =	1894.42			Bit Size = 4.75										
Total Depth Drilled	37.59			Bit Nozzles = 8, 8, 12, 12						Depth Drilled = 93.84				
Hours On Bit =	4.7000			Mud Type = Water Based						Hours On Bit = 3.38				
Average ROP =	20.81			Mud Weight (lbs/gal) = 9.00						Average ROP = 27.32				
Drillstring (ft) =	1831.70			Pipe (ft) = 883.16		Collars (ft) = 748.54								
Time (HH:MM:SS)	Time From Start (Hours)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	Instant. ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	10 Point Average ROP (ft/hr)	Per Foot ROP (ft/hr)
12:49:03	4.4906	1890.37	120	2320	436	13.98	15.12	14.72	2.58	93.74	0.0167	4.4906	1.47	
12:50:03	4.5076	1890.45	118	2270	427	12.64	16.40	15.21	4.48	93.82	0.0167	4.5076	1.60	(3.9)
12:51:03	4.5246	1890.52	118	2155	429	13.47	15.59	15.47	4.64	93.89	0.0167	4.5246	1.63	
12:51:44	4.5381	1890.78	117	2048	424	14.58	14.51	15.33	21.34	94.15	0.0168	4.5381	3.68	
12:52:38	4.5511	1891.03	118	2039	419	14.21	14.99	15.30	16.76	94.49	0.0168	4.5511	3.43	
12:53:12	4.5669	1891.98	119	2043	431	14.06	15.02	15.28	26.36	94.68	0.0168	4.5669	8.82	
12:53:59	4.5736	1891.53	119	2027	423	14.14	14.94	14.90	19.23	94.90	0.0151	4.5736	8.04	16.34
12:54:41	4.5853	1891.79	119	2037	434	14.03	15.00	14.88	22.19	95.16	0.0117	4.5853	11.68	
12:55:21	4.5984	1892.04	117	2039	427	14.37	14.73	14.92	22.28	95.41	0.0111	4.5984	13.99	
12:56:01	4.6076	1892.29	120	2039	433	14.67	15.01	14.95	32.22	95.66	0.0113	4.6076	16.86	
12:56:47	4.6203	1893.54	118	1884	431	14.82	14.38	14.80	16.87	95.91	0.0128	4.6203	18.53	21.64
12:57:32	4.6328	1892.79	120	1995	438	14.47	14.82	14.74	26.01	96.16	0.0129	4.6328	20.00	
12:58:18	4.6458	1893.04	119	2013	433	13.71	15.38	14.80	30.12	96.41	0.0128	4.6458	20.65	
12:58:53	4.6553	1893.36	121	2016	436	14.46	14.84	14.79	35.46	96.67	0.0097	4.6553	21.79	
12:59:44	4.6684	1893.56	121	2016	439	15.02	14.30	14.82	17.80	96.92	0.0142	4.6684	20.85	20.64
13:00:29	4.6808	1893.80	117	2092	427	14.23	14.95	14.79	22.52	97.17	0.0114	4.6808	21.17	
13:01:34	4.6909	1894.05	120	2187	434	14.03	15.12	14.88	30.68	97.42	0.0081	4.6909	21.61	
13:01:37	4.6981	1894.31	114	2143	416	15.50	12.79	14.34	27.83	97.68	0.0082	4.6981	22.33	
13:02:37	4.7147	1894.42	112	2269	428	17.93	11.41	13.69	6.70	97.76	0.0187	4.7147	19.07	19.21

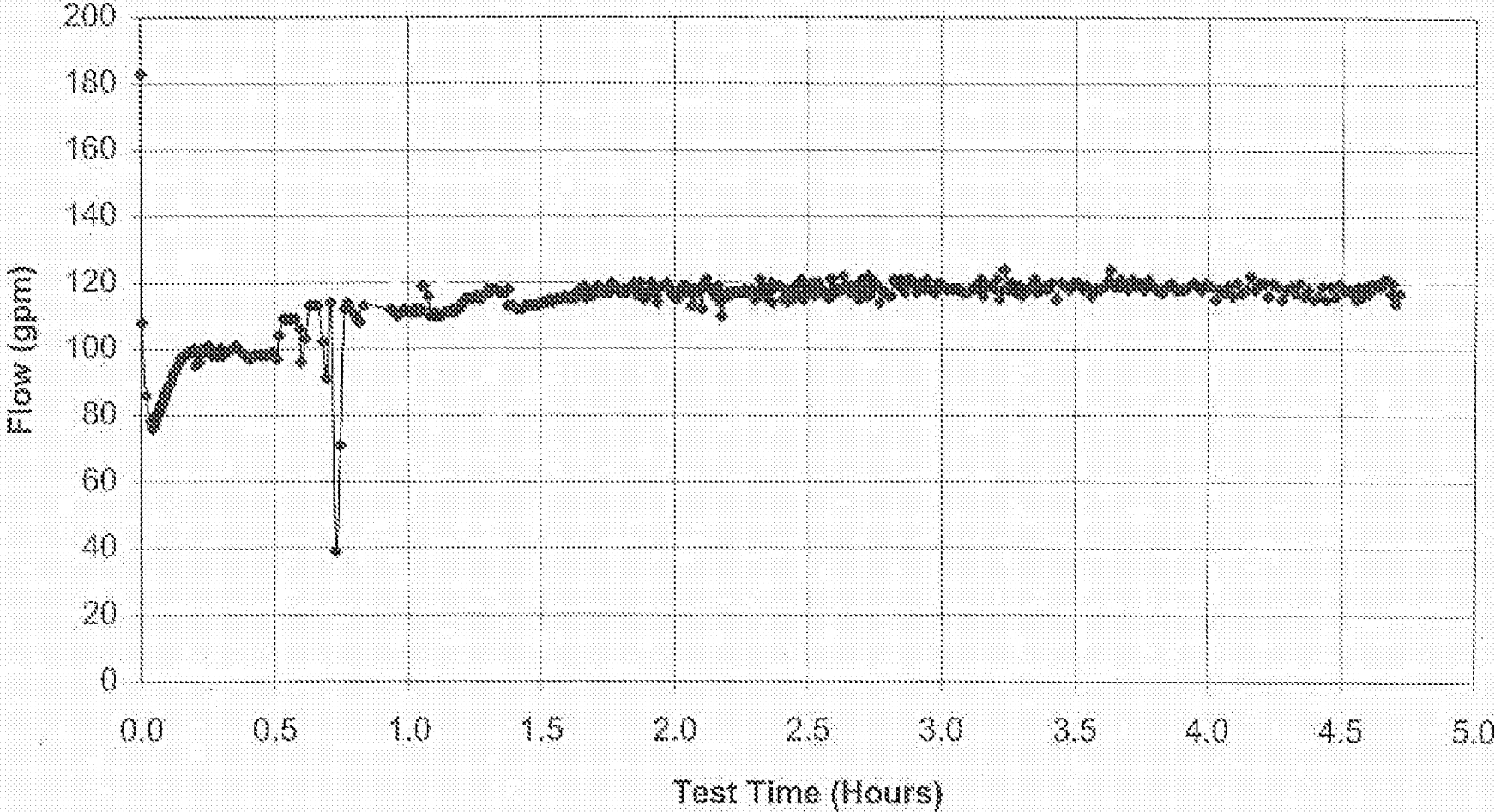
Bit Depth DOE HP Motor Test

HP Motor No. 1



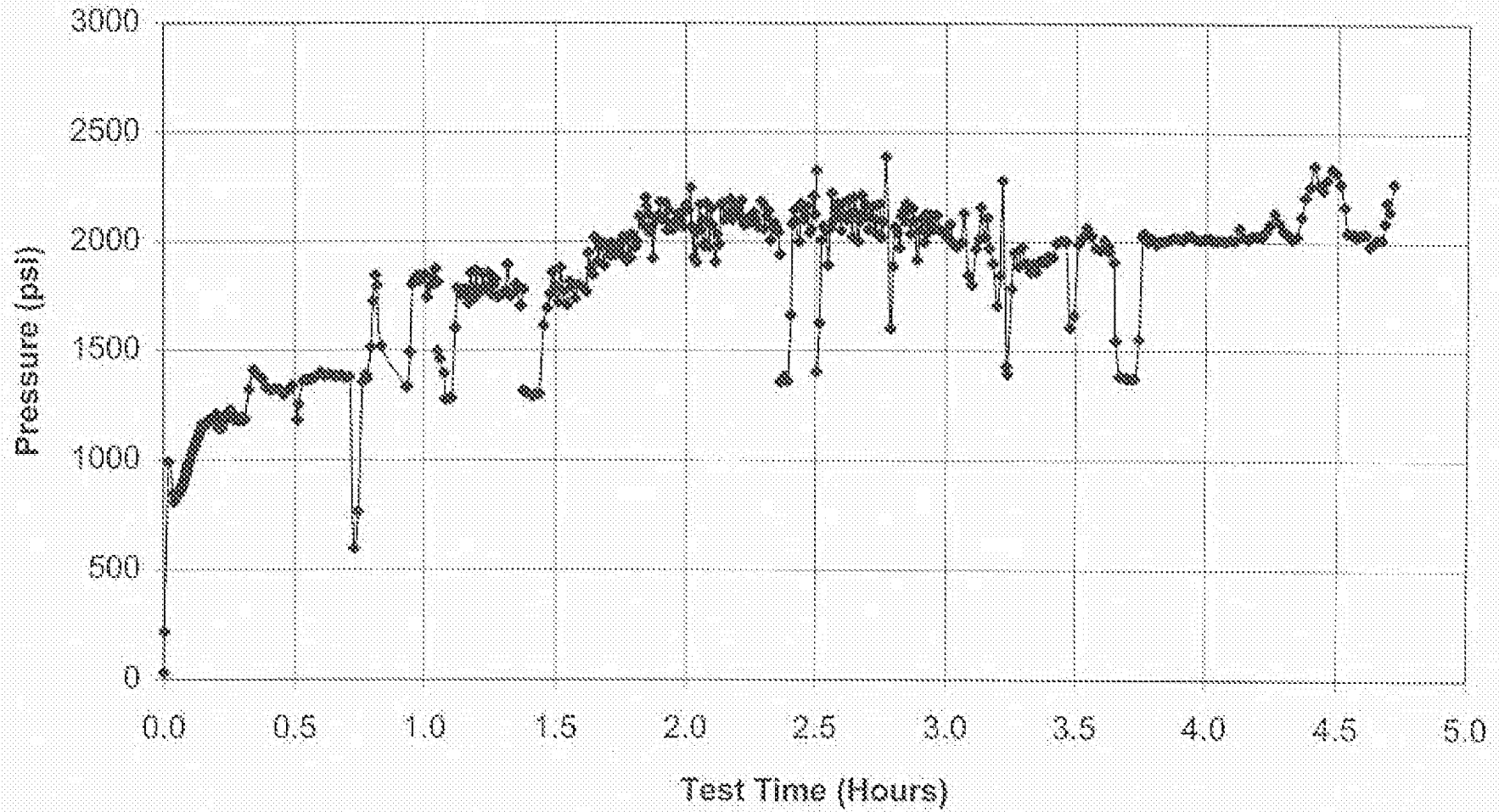
Flow Rate DOE SH-HP Motor Test

Hp Motor No. 1



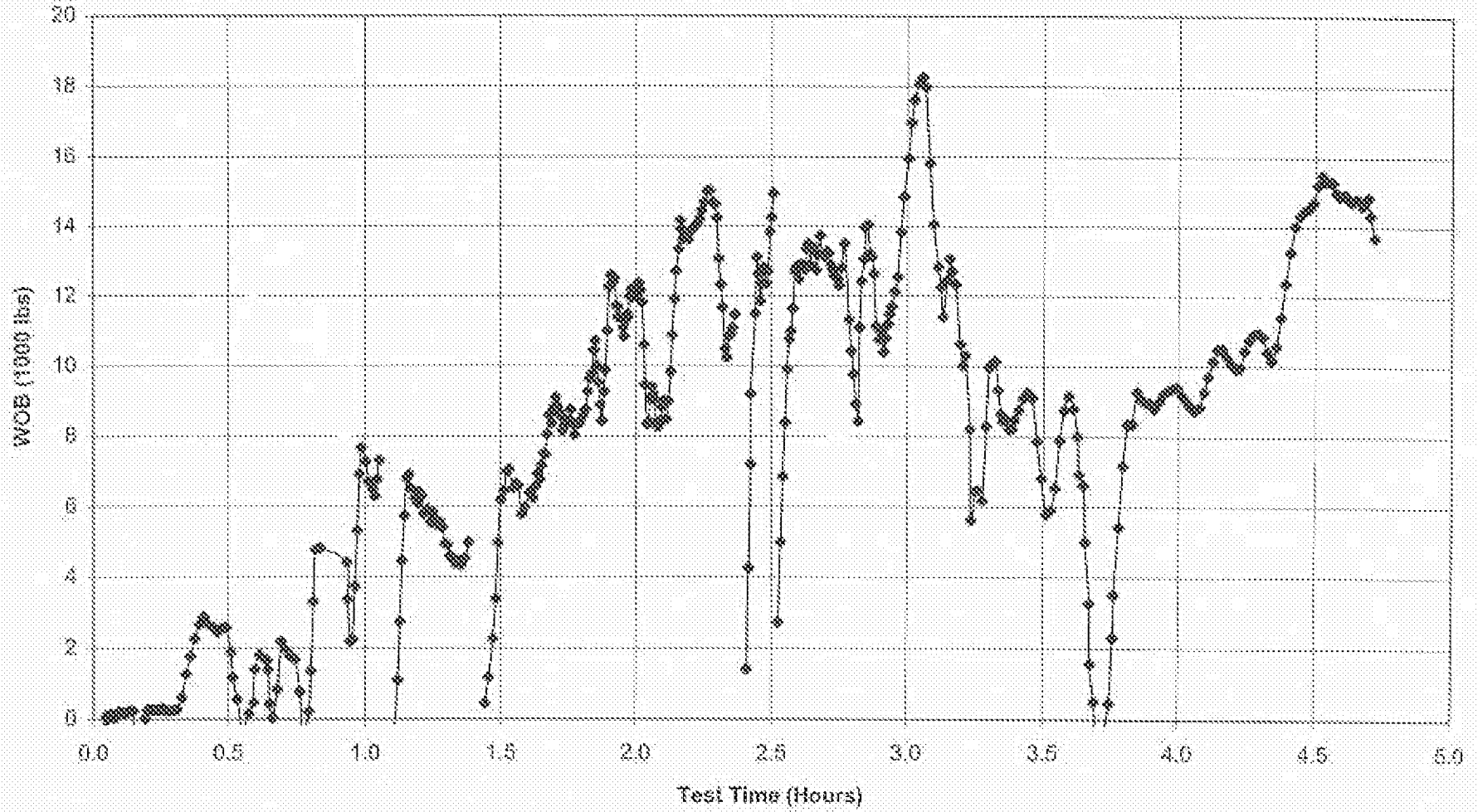
Stand Pipe Pressure DOE SH-HP Motor Test

HP Motor No. 1



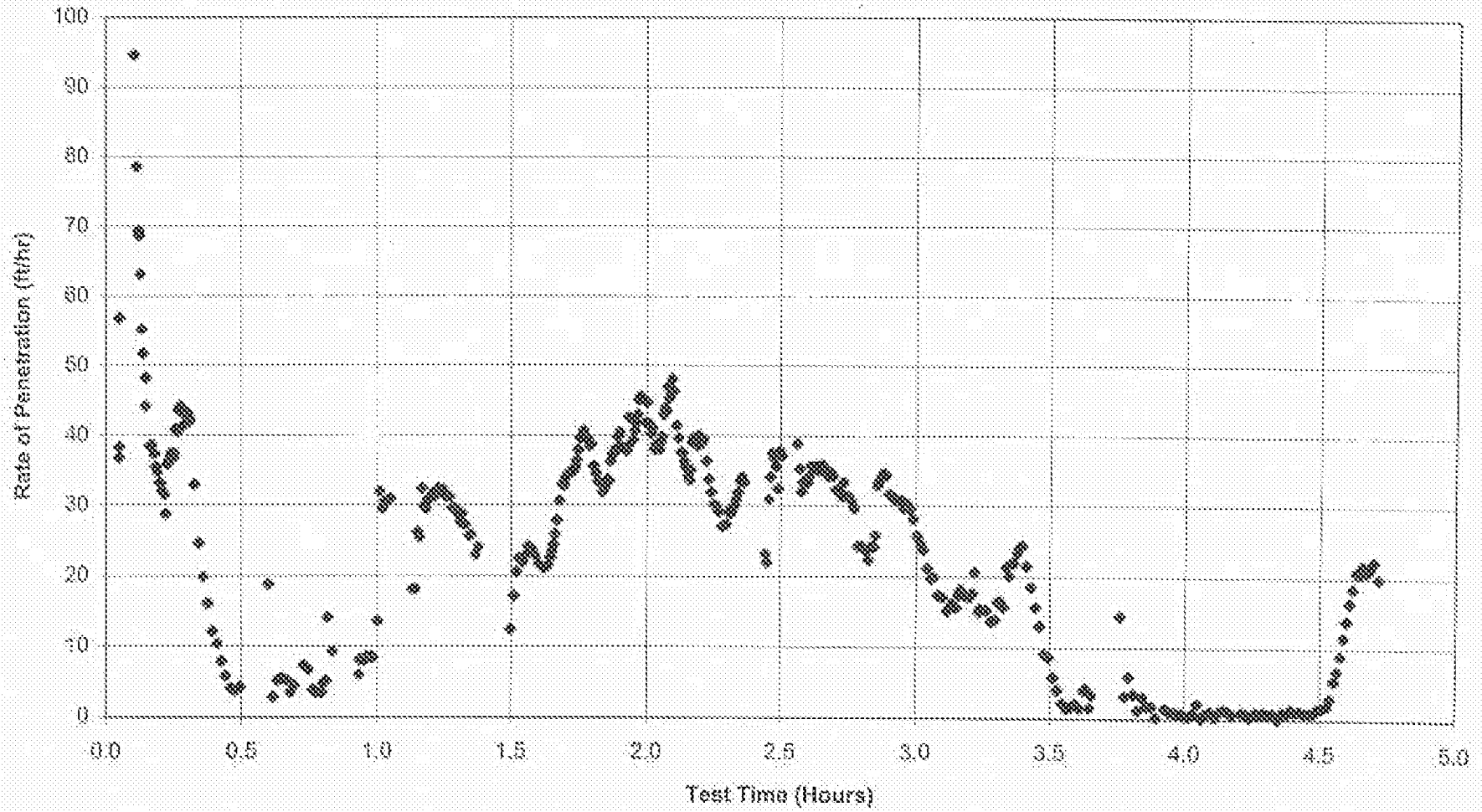
Bit Weight DOE HP Motor Test

HP Motor No. 1



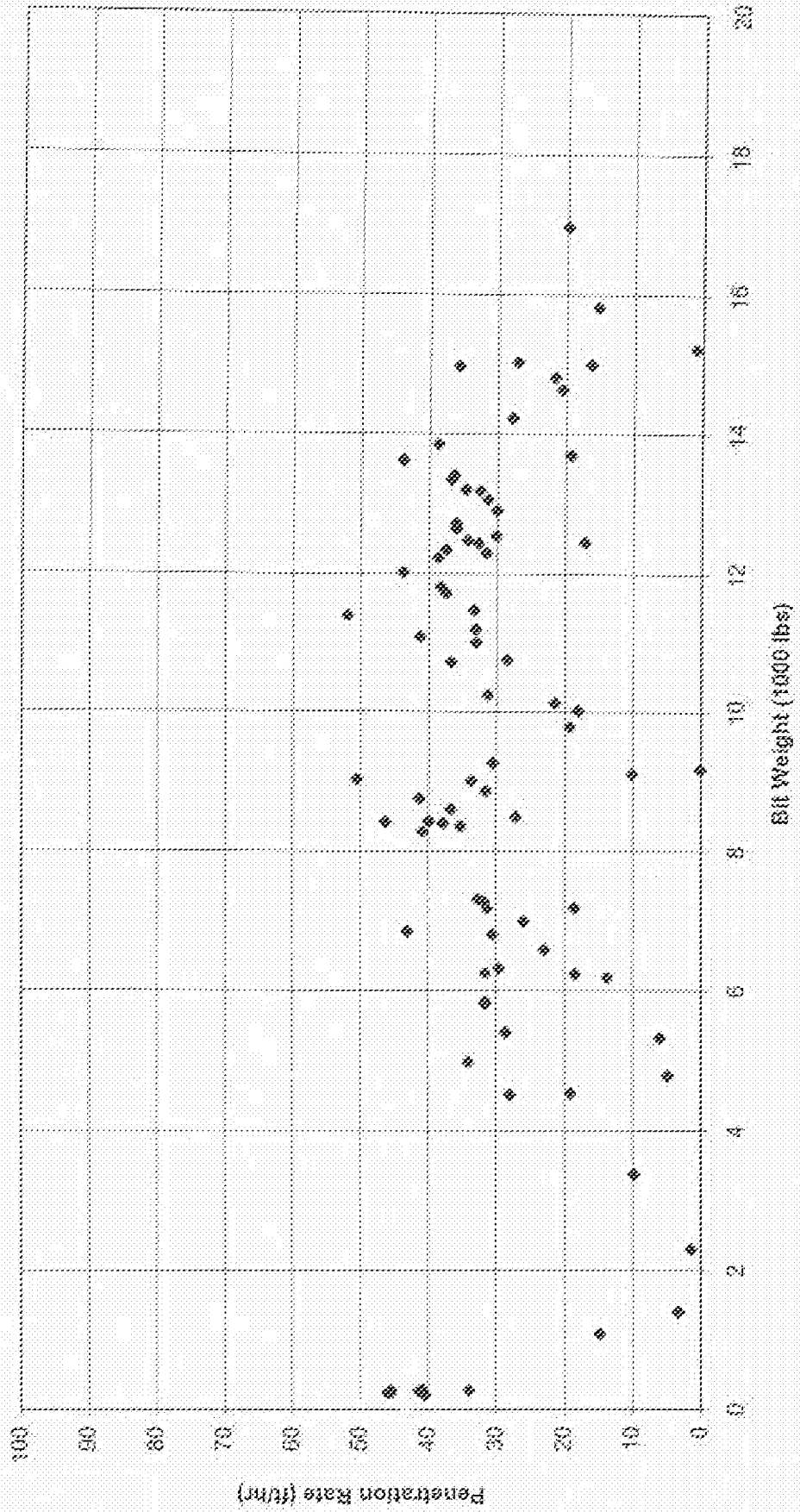
Penetration Rate DOE HP Motor Test

HP Motor No. 1



ROP As A Function Of Bit Weight

DOE HP Motor No. 1



DOE high power mortar test Amaco Cataoosa Test Site										Commercial Motor					
Well No. 5	Date: 12/16/98														
Starting Depth =	1693.65				Bit Type =	Walker McDonald MP68+				Average ROP Excluding Stops					
Ending Depth =	1781.24				Bit Size =	4.75									
Total Depth Drilled	87.59				Bit Nozzles =	3, 9, 12, 12				Depth Drilled	87.59				
Hours On Bit =	4.10				Mud Type =	Water Based				Hours On Bit	3.82				
Average ROP =	21.35				Mud Weight (lbs/gal) =	8.70				Average ROP	22.32				
Drillstring (ft) =	1718.05				Pipe (ft) =	977.74		Collar (ft)	740.31						
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Klps)	WOB (Klps)	Average WOB (Klps)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)	
08:28:08	0.0000	1693.65		1137	421	29.54	0.33		19.79	0.0000	0.0000	0.0000			
08:27:01	0.0147	1693.90	116	1240	423	28.41	1.40		16.91	0.2665	0.0147	0.0147			
08:28:01	0.0314	1694.08	116	1264	423	28.01	1.76		10.88	0.4360	0.0187	0.0314			
08:28:35	0.0458	1694.33	117	1332	427	27.65	1.90		26.73	0.5509	0.0094	0.0408			
08:29:27	0.0553	1694.55	118	1381	428	27.91	1.95	1.45	17.8	0.5400	0.0144	0.0553	17.81	17.01	
08:30:19	0.0697	1694.54	117	1342	427	27.76	1.96	1.78	17.3	1.1900	0.0144	0.0697	17.09		
08:31:04	0.0822	1695.09	119	1379	432	27.35	2.37	1.97	20.02	1.4400	0.0125	0.0822	18.87		
08:31:52	0.0956	1695.34	118	1378	428	27.52	2.24	2.07	19.22	1.6900	0.0133	0.0956	18.46		
08:32:49	0.1093	1695.60	118	1380	430	26.96	2.79	2.35	19.31	1.9500	0.0133	0.1089	18.84	18.84	
08:33:35	0.1242	1695.65	119	1393	432	27.15	2.59	2.39	18.34	2.2000	0.0153	0.1242	18.55	18.55	
08:34:30	0.1408	1695.68	119	1381	432	27.14	2.58	2.51	12.49	2.4100	0.0167	0.1408	15.06		
08:35:16	0.1522	1696.04	119	1387	431	27.3	2.34	2.52	22.38	2.6600	0.0114	0.1522	17.12		
08:36:15	0.1666	1696.58	119	1282	433	29.01	0.35	2.12	18.56	2.9300	0.0164	0.1686	18.41	18.41	
08:37:15	0.1853	1696.92	119	1183	433	29.54	0.00	1.56	-39.3	2.2700	0.0167	0.1853	1.15		
08:37:35	0.1894	1696.19	115	1133	434	29.66	0.00	1.04	53.51	2.5400	0.0042	0.1894	2.67	2.67	
08:37:51	0.1953	1696.44	114	1083	434	29.84	0.00	0.53	44.23	2.7900	0.0058	0.1953	3.02		
08:38:51	0.2119	1696.94	110	1029	400	29.87	0.00	0.04	-30.37	2.9900	0.0157	0.2119	-14.77		
08:39:48	0.2272	1696.19	110	1019	400	29.7	0.10	0.04	16.44	2.5400	0.0153	0.2272	6.44		
08:40:07	0.2331	1696.44	110	1022	400	29.5	0.34	0.10	41.6	2.7900	0.0068	0.2331	6.73		
08:41:02	0.2483	1696.69	108	1249	395	29.8	2.93	0.69	16.56	3.0400	0.0153	0.2483	4.71	4.71	
08:41:34	0.2572	1696.94	109	1316	398	29.95	3.75	1.44	28.29	3.2900	0.0086	0.2572	22.89		
08:42:34	0.2739	1696.93	106	1230	385	28.29	1.51	1.74	-9.84	3.5800	0.0157	0.2739	15.86		
08:43:13	0.2847	1697.19	105	1135	396	28.21	1.56	2.02	23	3.5300	0.0108	0.2847	14.32		
08:44:13	0.3014	1697.35	109	1230	396	28	1.90	2.32	6.86	3.8500	0.0157	0.3014	11.50		
08:45:00	0.3144	1697.65	108	1250	395	28.67	3.01	2.31	19.42	3.9000	0.0131	0.3144	10.60	0.60	
08:46:38	0.3250	1697.80	108	1290	395	28.87	3.05	2.35	21.9	4.1580	0.0106	0.3250	17.09		
08:48:33	0.3394	1698.05	109	1310	397	25.21	4.49	2.85	17.46	4.4000	0.0144	0.3394	15.90		
08:47:12	0.3511	1698.30	107	1308	391	25.12	4.56	3.54	21.45	4.6500	0.0117	0.3511	20.11		
08:47:56	0.3633	1698.56	106	1339	393	24.89	5.23	4.23	20.83	4.9100	0.0132	0.3633	20.56	20.56	
08:48:34	0.3739	1698.81	108	1387	398	25.89	5.75	4.78	24.22	5.1600	0.0108	0.3739	26.86		
08:49:07	0.3831	1699.67	108	1443	397	23.4	6.13	5.23	27.97	5.4200	0.0092	0.3831	23.36		

DOE high power mortar test Amaco Caloosa Test Site								Commercial Motor							
Well No. 8	Date: 12/18/98														
Starting Depth =	1693.65			Bit Type = Walker McDonald MP68H				Average ROP Excluding Stops							
Ending Depth =	1781.24			Bit Size = 4.75											
Total Depth Drilled	87.58			Bit Sizes = 5, 8, 12, 12				Depth Grilled 07.58							
Hours On Bit =	3.10			Mud Type = Water Based				Hours On Bit 3.02							
Average ROP =	27.95			Mud Weight (Rapiol) = 8.70				Average ROP 22.52							
Circulating (ft) =	1718.05			Pipe (ft) = 977.74				Collar (ft) 740.31							
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Foot)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	SOP (ft/hr)	ROP (ft/hr)	
08:49:44	0.3933	1693.32	109	1422	395	24.38	5.22	5.38	24.15	5.0700	0.0103	0.3933	24.15		
08:50:11	0.4008	1699.57	106	1442	388	24.28	5.35	5.54	33.37	5.8208	0.0075	0.4008	26.83	26.83	
08:50:45	0.4103	1699.82	109	1441	396	24.03	5.59	5.61	27	6.1700	0.0094	0.4103	27.76		
08:51:22	0.4206	1700.07	109	1438	398	24.11	5.48	5.55	24.82	6.4209	0.0103	0.4206	26.87		
08:51:52	0.4289	1700.33	108	1446	394	23.95	5.63	5.45	30.25	6.5809	0.0081	0.4289	28.41		
08:52:52	0.4456	1700.53	113	1313	388	26.47	3.23	6.05	12.17	6.8800	0.0157	0.4456	21.47	21.47	
08:53:29	0.4558	1700.75	109	1370	388	24.73	4.54	4.97	24.75	7.1300	0.0103	0.4558	21.37		
08:54:09	0.4669	1701.03	109	1371	397	24.97	4.66	4.78	22.56	7.3800	0.0111	0.4669	20.89		
08:54:43	0.4764	1701.28	111	1418	403	24.71	4.91	4.67	25.35	7.6300	0.0094	0.4764	20.60		
08:55:43	0.4931	1701.42	109	1370	398	27.02	2.71	4.69	8.42	7.7700	0.0167	0.4931	18.74	18.74	
08:56:23	0.5069	1701.67	110	1391	401	26.45	3.27	4.18	17.94	8.0200	0.0139	0.5069	17.41		
08:57:03	0.5153	1701.92	107	1419	382	24.97	4.68	4.54	30.92	8.2700	0.0083	0.5153	18.41		
08:58:03	0.5319	1702.03	110	1348	438	27.49	3.24	3.56	5.35	8.3600	0.0167	0.5319	13.80		
08:58:53	0.5458	1702.26	109	1361	399	25.76	3.91	3.38	17.9	8.6300	0.0139	0.5458	15.25	15.25	
08:59:53	0.5625	1702.52	110	1386	400	25.96	3.79	3.56	14.22	8.8700	0.0167	0.5625	15.38		
09:00:53	0.5732	1702.75	109	1295	399	26.9	2.85	3.47	13.67	9.1800	0.0167	0.5792	12.68		
09:01:24	0.5878	1703.00	110	1384	432	24.91	4.78	3.49	29.88	9.3500	0.0083	0.5878	17.32		
09:02:21	0.6036	1703.25	108	1316	384	26.88	3.41	3.72	15.81	9.5000	0.0183	0.6036	16.79	16.79	
09:03:08	0.6144	1703.50	111	1266	404	25.79	3.98	3.72	23.04	9.8500	0.0108	0.6144	18.87		
09:03:37	0.6247	1703.75	110	1338	401	25.58	4.28	3.84	24.7	10.1000	0.0103	0.6247	21.96		
09:04:34	0.6247	1704.07	110	1334	403	25.81	3.89		27.48	10.4200	0.0000	0.6247			
09:04:54	0.6331	1704.27	111	1330	408	25.74	3.53		23.29	10.6200	0.0083	0.6331			
09:05:24	0.6416	1704.42	110	1329	399	25.94	3.76		18.08	10.7700	0.0083	0.6416			
09:06:54	0.6497	1704.62	110	1330	399	25.87	3.83		24.3	10.9700	0.0083	0.6497			
09:08:24	0.6681	1704.83	110	1359	401	24.69	5.32	4.18	24.99	11.1800	0.0083	0.6681	22.80		
09:09:54	0.6854	1705.02	111	1389	405	23.98	5.60	4.62	22.83	11.3780	0.0083	0.6854	22.50	22.50	
09:07:24	0.6747	1705.14	111	1306	403	25.3	4.36	4.61	14.36	11.4900	0.0083	0.6747	21.60		
09:07:54	0.6831	1705.33	111	1304	403	25.72	3.97	4.63	23.67	11.6800	0.0083	0.6831	21.36	21.36	
09:08:22	0.6908	1705.38	108	1394	394	26.28	3.44	4.58	32.08	11.8300	0.0078	0.6908	22.88		
09:08:52	0.6992	1705.76	111	1314	404	26.78	2.93	4.63	20.16	12.1000	0.0083	0.6992	22.27		

DOE high power mortar test Amaco Catoosa Test Site											Commercial Motor			
Well No. 6	Date: 12/16/98													
Starting Depth =	1793.65											Average ROP Excluding Stops		
Ending Depth =	1791.34													
Total Depth Drilled	87.59											Depth Drilled	87.59	
Hours On Bit =	4.10											Hours On Bit	3.82	
Average ROP =	21.35											Average ROP	22.92	
Orifitting (#) =	1718.05													
						Bit Type =	Walker McClean& MPRH							
						Bit Size =	4.75							
						Bit Nozzles =	8, 9, 12, 12							
						Mud Type =	Water Based							
						Mud Weight (lbs/gal) =	8.70							
						Pipe (ft) =	977.74		Collar (ft) =	748.33				
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	SR Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (fpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
09:03:22	0.7375	1705.94	109	1291	398	28.2	3.43	3.63	23	12.2900	0.0083	0.7375	24.41	
09:09:32	0.7158	1706.15	111	1342	403	26.77	2.92	3.34	24.84	12.5000	0.0083	0.7158	25.02	
09:10:22	0.7242	1706.34	111	1340	405	26.7	3.00	3.14	22.91	12.6900	0.0083	0.7242	22.89	24.67
09:16:52	0.7326	1706.51	109	1294	398	27.19	2.49	2.95	20.95	12.8600	0.0083	0.7326	22.89	
09:11:16	0.7400	1706.77	119	1353	401	26.73	2.97	2.96	33.71	13.1200	0.0078	0.7400	25.94	
09:11:49	0.7483	1706.85	118	1303	401	26.79	2.90	2.86	19.47	13.2000	0.0083	0.7483	21.54	
09:12:15	0.7567	1707.00	113	1330	413	24.51	4.09	3.27	17.89	13.3500	0.0083	0.7567	20.31	
09:12:49	0.7650	1707.22	113	1310	408	26.82	2.89	3.24	25.78	13.5700	0.0083	0.7650	21.85	
09:13:15	0.7733	1707.38	113	1314	408	27	2.74	3.29	19.5	13.7300	0.0083	0.7733	18.39	21.15
09:13:49	0.7817	1707.56	113	1314	411	27.07	2.65	3.23	21.82	13.9100	0.0083	0.7817	21.39	
09:14:18	0.7900	1707.71	111	1308	405	25.73	3.09	3.35	18.41	14.0800	0.0083	0.7900	21.39	
09:14:49	0.7983	1707.84	112	1308	405	26.73	2.85	2.84	15.57	14.1900	0.0083	0.7983	18.99	
09:15:19	0.8067	1708.06	112	1292	408	28.89	2.84	2.84	23.9	14.4100	0.0083	0.8067	20.49	
09:15:49	0.8150	1708.16	112	1313	406	28.53	3.23	3.93	11.94	14.5100	0.0083	0.8150	18.69	
09:16:17	0.8228	1708.31	112	1341	406	28.65	3.06	3.02	32.12	14.7800	0.0078	0.8228	21.35	20.83
09:16:47	0.8311	1708.53	112	1331	408	28.59	3.11	3.04	30.16	14.9300	0.0083	0.8311	22.59	
09:17:17	0.8394	1708.79	110	1354	408	36.3	3.43	3.14	20.77	15.1100	0.0083	0.8394	21.36	
09:17:47	0.8478	1708.95	113	1355	411	26.2	3.49	3.27	23.29	15.3000	0.0083	0.8478	24.10	
09:18:17	0.8561	1709.14	111	1331	403	25.73	3.95	3.41	22.69	15.4900	0.0083	0.8561	21.90	
09:18:47	0.8644	1709.38	113	1337	413	25	4.85	3.73	28.34	15.7300	0.0083	0.8644	24.60	23.28
09:19:17	0.8728	1709.54	111	1271	404	27.3	2.46	3.59	19.07	15.8900	0.0083	0.8728	23.40	
09:19:39	0.8789	1709.79	111	1477	405	25.85	3.89	3.57	41.9	16.1400	0.0081	0.8789	27.00	
09:20:09	0.8872	1709.83	111	1313	405	27.62	2.18	3.40	3.94	16.1800	0.0083	0.8873	22.18	
09:20:39	0.8956	1709.97	112	1263	408	27.05	2.67	3.15	16.99	16.3200	0.0083	0.8956	18.96	
09:21:07	0.9033	1710.22	112	1245	409	25.97	3.74	2.87	32.14	16.5700	0.0078	0.9033	22.25	
09:21:37	0.9117	1710.43	113	1314	412	25.83	3.59	3.19	24.77	16.7800	0.0083	0.9117	19.53	22.24
09:22:07	0.9200	1710.63	110	1384	408	25.8	4.08	3.25	23.91	16.9800	0.0083	0.9200	24.41	
09:22:37	0.9283	1710.84	111	1324	405	26.14	3.54	3.52	25.33	17.1800	0.0083	0.9283	28.54	
09:23:07	0.9367	1711.00	112	1325	407	25.9	3.78	3.75	20.02	17.3500	0.0083	0.9367	23.48	
09:23:34	0.9452	1711.26	111	1344	405	25.86	3.72	3.74	33.29	17.6100	0.0078	0.9452	26.54	
09:24:04	0.9525	1711.41	118	1386	402	25.57	4.11	3.85	18.44	17.7600	0.0063	0.9525	24.99	24.20

DOE high power mortar test Amaco Catoosa Test Site

Commercial Motor

Well No. 6	Date: 12/15/98												
Starting Depth =	1693.55			Bit Type =	Walker McGoonsald MP68H							Average ROP Excluding Steps	
Ending Depth =	1751.34			Bit Size =	4.75								
Total Depth Drilled	57.79			Bit Nozzles =	8, 9, 12, 13						Depth Drilled	57.79	
Hours On Bit =	4.10			Mud Type =	Water Based						Hours On Bit	3.82	
Average ROP =	21.35			Mud Weight (lbs/gal) =	8.70						Average ROP	22.92	
Circulating (ft) =	1715.85			Pipe (ft) =	977.74	Collar (ft)	740.33						

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
09:24:34	0.6308	1711.61	111	1369	403	25.95	4.14	3.86	23.87	17.9300	0.0083	0.6308	23.68	
09:25:04	0.6492	1711.73	111	1323	405	26.41	4.32	3.81	34.9	18.0800	0.0083	0.9393	22.46	
09:25:33	0.6772	1711.99	111	1375	404	25.74	3.95	3.85	32.15	18.3300	0.0083	0.9772	21.78	
09:26:03	0.6855	1712.18	113	1358	408	26.1	3.80	3.82	25.15	18.5100	0.0083	0.9856	22.89	
09:26:33	0.6939	1712.34	113	1345	410	26.1	3.89	3.72	22	18.6900	0.0083	0.9939	22.09	22.47
09:27:03	1.0022	1712.58	108	1351	398	26.84	4.43	3.78	28.62	18.8300	0.0083	1.0022	25.71	
09:27:33	1.0108	1712.75	112	1485	408	26.01	3.69	3.85	21.21	19.1000	0.0083	1.0106	23.19	
09:28:03	1.0189	1712.87	112	1169	408	28.67	1.15	3.29	14.34	19.2200	0.0083	1.0189	21.39	
09:28:33	1.0272	1713.01	110	1257	402	27.61	2.14	3.00	15.92	19.3600	0.0083	1.0272	30.15	
09:29:03	1.0356	1713.19	113	1299	413	27.3	2.48	2.77	22.09	19.5400	0.0083	1.0356	19.38	
09:29:33	1.0439	1713.42	114	1352	418	27.3	2.43	3.37	27.77	19.7700	0.0083	1.0439	20.10	21.80
09:30:03	1.0522	1713.57	111	1500	404	27.03	2.71	2.18	17.37	19.9200	0.0083	1.0522	21.00	
09:30:33	1.0606	1713.52	118	1221	426	28.84	0.99	2.15	-6.15	19.9700	0.0083	1.0606	15.30	
09:31:03	1.0689	1713.69	113	1315	412	27.81	1.99	2.11	20.73	20.0400	0.0083	1.0689	15.00	
09:31:33	1.0773	1713.63	113	1390	411	25.99	2.83	2.19	17.5	20.1800	0.0083	1.0773	12.30	
09:32:03	1.0856	1713.99	111	1322	405	26.73	3.02	2.31	18.41	20.3400	0.0083	1.0856	12.60	
09:32:33	1.0939	1714.17	111	1348	408	26.5	3.12	2.39	22.35	20.5000	0.0083	1.0939	19.50	
09:33:03	1.1022	1714.37	112	1322	406	26.83	2.91	2.77	23.5	20.7200	0.0083	1.1022	20.40	18.25
09:33:33	1.1106	1714.52	112	1328	409	27.07	2.87	2.91	17.56	20.8700	0.0083	1.1106	20.70	
09:34:03	1.1189	1714.71	111	1322	405	26.89	2.85	2.91	23.25	21.0500	0.0083	1.1189	21.60	
09:34:33	1.1272	1714.89	114	1355	418	26.37	3.16	3.04	21.05	21.2400	0.0083	1.1272	21.60	
09:35:03	1.1356	1715.04	111	1288	404	26.95	2.80	2.88	17.84	21.3900	0.0083	1.1356	20.10	
09:35:27	1.1422	1715.29	111	1343	408	25.34	4.35	3.17	38.98	21.6400	0.0083	1.1422	24.32	
09:35:57	1.1506	1715.43	113	1386	410	34.33	5.31	3.69	17.09	21.7900	0.0083	1.1506	22.74	21.63
09:36:27	1.1589	1715.55	113	1347	412	23.56	6.94	4.33	14.72	21.9000	0.0083	1.1589	20.84	
09:36:57	1.1672	1715.76	114	1338	415	23.55	6.06	4.91	25.21	22.1100	0.0083	1.1672	22.74	
09:37:27	1.1756	1715.75	113	1475	412	25.88	3.86	5.12	-0.97	22.1000	0.0083	1.1756	13.80	
09:37:57	1.1839	1715.93	112	1285	418	35.33	4.37	5.13	21.25	22.3800	0.0083	1.1839	15.00	
09:38:27	1.1922	1716.01	113	1283	410	25.88	3.87	4.84	10.12	22.3800	0.0083	1.1922	13.80	
09:38:57	1.2006	1716.22	112	1341	407	24.18	5.47	4.73	26.15	22.5700	0.0083	1.2006	13.80	
09:39:27	1.2089	1716.34	113	1313	413	24.25	6.26	4.59	14.11	22.6900	0.0083	1.2089	17.75	

DOE high power mortar test Amaco Catoosa Test Site								Commercial Motor							
Well No. 6	Date: 12/15/98														
Starting Depth =	1695.65					Bit Type =	Walker McDevanold MP98H				Average ROP	Excluding Steps			
Ending Depth =	1781.34					Bit Size =	4.75								
Total Depth Drilled	87.59					Bit Nozzles =	3, 9, 12, 12				Depth Drilled	87.59			
Hours On Bit =	4.10					Mud Type =	Water Based				Hours On Bit	3.82			
Average ROP =	21.35					Mud Weight (lbs/gal) =	8.70				Average ROP	22.92			
Drillstem (ft) =	1718.65					Pipe (ft) =	977.74	Collar (ft)	740.31						
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)	
09:39:57	1.2172	1716.62	115	1298	420	24.61	5.06	4.93	9.02	23.7700	0.0003	1.2172	14.70	14.65	
09:40:27	1.2256	1716.61	113	1312	411	36.6	4.11	4.78	22.95	22.9600	0.0003	1.2256	18.00		
09:40:57	1.2339	1716.78	109	1431	387	26.68	3.28	4.62	20.7	23.1300	0.0003	1.2339	16.88		
09:41:19	1.2400	1717.05	112	1260	408	26.56	2.81	4.09	43.51	23.4000	0.0001	1.2400	32.82		
09:41:20	1.2403	1717.32	111	1374	409	32.65	1.84	3.40	4590.95	23.8700	0.0003	1.2403	38.64	39.04	
09:54:22	1.2403	1717.57	121	1120	438	29.0	0.44		448.97	23.9200	0.0000	1.2403			
09:54:23	1.2408	1717.82	115	1117	418	30.26	0.09		931.57	24.1700	0.0003	1.2408			
09:54:28	1.2419	1718.08	122	1121	441	30.08	0.27		186.24	24.4300	0.0014	1.2419			
09:54:38	1.2447	1718.33	118	1124	420	30.11	0.24		91.20	24.6800	0.0028	1.2447			
09:55:08	1.2531	1718.17	117	1134	436	30.18	0.18		-19.34	24.9300	0.0083	1.2531	38.68		
09:55:38	1.2614	1718.16	115	1128	418	30.41	0.00	0.18	-0.42	24.8100	0.0083	1.2614	16.32		
09:56:08	1.2697	1718.20	116	1128	422	30.41	0.00	0.14	-4.46	24.8500	0.0083	1.2697	4.32		
09:58:38	1.2781	1718.18	117	1115	424	30.25	0.1	0.11	-2.34	24.6300	0.0083	1.2781	-4.50		
09:57:08	1.2864	1718.37	116	1103	420	30.18	0.18	0.09	22.67	24.7200	0.0083	1.2864	6.00		
09:57:38	1.2947	1718.54	103	1160	377	27.44	2.81	0.62	20.38	24.8500	0.0083	1.2947	11.40	17.82	
09:58:08	1.3031	1718.00	89	907	299	28.29	1.89	0.94	-424.25	21.3500	0.0083	1.3031	-96.00		
09:58:18	1.3114	1714.92	104	918	384	30.58	0.00	0.94	-9.80	21.2700	0.0083	1.3114	-97.80		
09:58:08	1.3197	1714.93	116	1128	422	30.56	0.00	0.92	-0.84	21.2700	0.0083	1.3197	-103.80		
09:58:28	1.3247	1715.17	116	1137	423	30.4	0.00	0.88	80.39	21.8300	0.0080	1.3247	-112.33		
09:58:28	1.3247	1715.43	123	1163	440	29.8	0.52	0.42	1886.75	21.7800	0.0000	1.3247	19.85		
09:59:27	1.3250	1715.68	120	1160	438	28.83	0.55	0.21	2685.88	22.0300	0.0003	1.3250	65.84		
09:59:27	1.3250	1715.94	115	1159	417	29.92	0.38	0.29	2700.70	22.2900	0.0000	1.3250	193.26		
09:59:27	1.3250	1716.21	107	1162	361	29.59	0.78	0.45	2790.01	22.5800	0.0000	1.3250	3744.00		
09:59:28	1.3253	1716.47	106	1161	386	30.01	0.37	0.52	2951.2	22.8200	0.0003	1.3253	1872.00		
09:59:28	1.3253	1716.73	107	1166	389	30.57	0.80	0.42	2979.29	23.0800	0.0003	1.3253	3780.00		
09:59:28	1.3253	1716.98	110	1150	401	31.01	0.60	0.31	2281.69	23.3300	0.0000	1.3253	3744.00		
09:59:29	1.3258	1717.24	110	1147	421	29.93	0.00	0.33	1031.58	23.5800	0.0003	1.3258	1884.00		
09:59:30	1.3258	1717.49	116	1135	400	30.38	0.90	0.07	1325.38	23.6800	0.0003	1.3258	1696.00		
09:59:32	1.3364	1717.74	117	1061	428	30.23	0.12	0.02	381.64	24.0900	0.0006	1.3364	893.00		
09:59:37	1.3378	1717.99	124	1103	449	30.17	0.21	0.07	202.26	24.3400	0.0014	1.3378	494.00		

DOE high power mortar test Amaco Catoosa Test Site								Commercial Motor							
Well No. G		Date: 12/16/98													
Starting Depth =		1693.55		Bit Type = Walker McDonald MP50H				Average ROP Excluding Slips							
Ending Depth =		1781.24		Bit Size = 4.75											
Total Depth Drilled		87.59		Bit Nozzles = 8, 9, 12, 12				Depth Drilled				87.59			
Hours On Bit =		4.10		Mud Type = Water Based				Hours On Bit				3.82			
Average ROP =		21.35		Mud Weight (lb/gal) = 8.70				Average ROP				22.52			
Circulating (ft)		1718.05		Pipe (ft) = 577.74				Casing (ft) 748.31							
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)	
09:28:37	1:33:08	1718.25	109	1067	393	30.13	0.22	0.11	50.02	24.6000	0.0028	1.3308	302.50		
10:08:04	1:33:53	1718.50	107	980	392	29.63	0.51	0.21	53.86	24.6500	0.0047	1.3353	196.94		
10:08:34	1:34:36	1718.14	90	804	330	28.69	0.64	0.34	-402.25	21.4500	0.0083	1.3436	-155.97		
10:08:51	1:34:53	1718.40	93	360	131	30.86	0.60	0.33	52.58	21.7300	0.0047	1.3483	-138.03		
10:09:21	1:35:07	1718.36	1	97	28	30.83	0.00	0.27	-4.37	21.7100	0.0083	1.3507	-119.60		
10:09:51	1:35:50	1718.38	1	86	28	30.77	0.00	0.23	3.49	21.7300	0.0083	1.3550	-104.97		
10:09:24	1:37:33	1718.38	1	83	28	30.72	0.00	0.13	0	21.7300	0.0083	1.3733	0.07		
10:09:54	1:38:17	1718.37	1	81	20	30.66	0.00	0.00	-1.74	21.7200	0.0083	1.3817	-0.90		
10:09:21	1:39:00	1718.36	1	79	20	30.65	0.00	0.00	-0.86	21.7100	0.0083	1.3900	0.00		
10:09:51	1:39:03	1718.36	1	78	20	30.62	0.00	0.00	0.59	21.7100	0.0083	1.3963	-0.60		
10:09:21	1:40:07	1718.36	1	77	20	30.62	0.00	0.00	-0.85	21.7100	0.0083	1.4087	-0.60		
10:09:51	1:41:50	1718.36	1	78	20	30.61	0.00	0.00	0.22	21.7100	0.0083	1.4150	-0.30		
10:09:21	1:42:33	1718.35	1	78	20	30.6	0.00	0.00	-0.57	21.7000	0.0083	1.4233	-0.30		
10:09:51	1:43:17	1718.38	1	75	20	30.5	0.00	0.00	2.81	21.7300	0.0083	1.4317	0.60		
10:18:50	1:51:50	1718.17	117	1143	426	30.64	0.00	0.00	320.37	21.5200	0.1639	1.6158	-0.91		
10:17:23	1:52:38	1718.13	119	1153	433	30.58	0.00	0.00	-5.33	21.4800	0.0083	1.6239	-1.10		
10:17:03	1:53:22	1718.16	127	1171	445	30.58	0.00	0.00	3.57	21.5100	0.0083	1.6322	-0.91		
10:18:23	1:54:05	1718.14	130	1177	435	30.57	0.00	0.00	-2.45	21.4900	0.0083	1.6405	-1.15		
10:18:53	1:54:08	1718.18	121	1173	428	30.60	0.00	0.00	4.35	21.5300	0.0083	1.6488	0.30		
10:18:51	1:55:50	1718.27	120	1177	434	30.07	0.00	0.06	138.94	24.6500	0.0161	1.6650	75.38		
10:20:17	1:57:23	1718.52	122	1355	443	28.87	1.84	0.38	34.48	24.8700	0.0072	1.6723	64.00		
10:20:47	1:58:06	1718.69	118	1420	434	30.25	3.96	1.18	20.42	26.0400	0.0083	1.6806	88.75		
10:21:17	1:58:09	1718.92	120	1451	437	27.12	3.12	1.80	27.28	25.2700	0.0083	1.6889	90.50		
10:21:47	1:59:73	1719.09	121	1387	438	27.63	2.65	2.33	30.52	25.4400	0.0083	1.6972	25.45		
10:22:14	1:70:47	1719.34	122	1445	442	26.43	3.73	3.02	33.71	25.6900	0.0075	1.7047	25.28		
10:22:44	1:71:31	1719.45	118	1398	433	26.91	3.32	3.36	14.98	26.8100	0.0083	1.7131	23.80	2.30	
10:23:14	1:72:14	1719.67	119	1444	434	26.63	3.60	3.28	25.06	26.0200	0.0083	1.7214	23.00		
10:23:44	1:72:57	1719.85	119	1392	433	26.94	3.35	3.32	21.61	26.3000	0.0083	1.7297	23.38		
10:24:14	1:73:41	1720.04	122	1440	442	26.96	4.25	3.64	22.25	26.3900	0.0083	1.7381	21.60		
10:24:44	1:74:24	1720.17	119	1368	431	26.28	3.91	3.68	15.41	26.6200	0.0083	1.7464	21.30		
10:25:14	1:75:07	1720.38	121	1424	440	25.65	4.52	3.92	26.34	26.7300	0.0083	1.7547	21.30		

DOE high power mortar test Amaco Catoosa Test Site**Commercial Motor**

Well No. 6

Date: 12/16/99

Starting Depth =	1693.65	Bit Type =	Walker McCornald MP98H	Average ROP	Excluding Steps
Ending Depth =	1781.24	Bit Size =	4.75	Depth Drilled	87.59
Total Depth Drilled	87.59	Bit Nozzles =	9, 9, 12, 12	Hours On Bit	3.82
Hours On Bit =	4.30	Mud Type =	Water Based	Average ROP	22.92
Average ROP =	21.35	Mud Weight (lbs/gal) =	8.76		
Drilling (ft) =	1715.05	Pipe (ft) =	977.74	Collar (ft)	740.31

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
10:25:44	1.7531	1720.54	117	1439	427	26.5	4.68	4.13	18.53	26.8900	0.0083	1.7531	30.76	21.60
10:26:14	1.7714	1720.74	118	1451	428	25.03	5.13	4.50	23.59	27.0900	0.0083	1.7714	21.00	
10:26:44	1.7797	1720.94	118	1460	425	25.1	5.05	4.66	24.17	27.2900	0.0083	1.7797	23.10	
10:27:14	1.7881	1721.13	120	1458	437	25.81	4.56	4.79	22.62	27.4800	0.0083	1.7881	22.50	
10:27:44	1.7964	1721.37	123	1453	441	25.84	4.26	4.74	23.47	27.7200	0.0083	1.7964	24.90	
10:28:14	1.8047	1721.55	120	1491	434	25.38	4.80	4.76	22.34	27.9100	0.0083	1.8047	24.80	34.45
10:28:39	1.8117	1721.81	118	1431	428	25.91	4.07	4.67	26.44	28.1600	0.0083	1.8117	27.23	
10:29:09	1.8209	1721.95	118	1503	422	25.41	4.78	4.61	18.49	28.3100	0.0083	1.8200	25.90	
10:29:39	1.8283	1722.11	119	1333	432	27.00	3.15	4.93	17.59	28.4600	0.0083	1.8283	23.17	
10:30:09	1.8367	1722.34	120	1428	436	26.11	4.00	4.25	27.25	28.6900	0.0083	1.8367	24.42	
10:30:37	1.8444	1722.59	118	1400	429	25.86	4.53	4.24	32.2	28.9400	0.0078	1.8444	23.80	25.93
10:31:07	1.8528	1722.72	118	1470	429	25.26	4.90	4.28	15.63	29.0700	0.0083	1.8528	23.19	
10:31:35	1.8606	1722.97	121	1460	439	25.43	3.78	4.00	31.26	29.3200	0.0078	1.8608	26.69	
10:32:06	1.8689	1723.07	120	1469	435	25.47	4.71	4.40	11.84	29.4200	0.0083	1.8689	22.00	
10:32:36	1.8772	1723.29	123	1458	446	24.69	5.40	4.66	27.16	29.6400	0.0083	1.8772	21.36	
10:33:01	1.8844	1723.56	118	1489	426	25.56	4.60	4.08	34.89	29.8900	0.0072	1.8844	25.99	23.75
10:33:31	1.8928	1723.88	120	1402	426	26.11	4.08	4.52	18.81	30.0300	0.0083	1.8928	22.03	
10:33:45	1.8967	1723.94	118	1526	427	25.83	3.59	4.49	66.21	30.2900	0.0029	1.8967	31.32	
10:34:15	1.9050	1724.08	119	1423	433	26.04	4.16	4.36	7.79	30.3500	0.0083	1.9050	26.56	
10:34:26	1.9108	1724.25	118	1480	427	25.71	4.48	4.16	42.39	30.6000	0.0058	1.9108	36.91	
10:35:08	1.9192	1724.47	122	1444	444	25.93	3.30	3.92	25.82	30.8200	0.0083	1.9192	29.94	26.70
10:35:36	1.9275	1724.68	118	1456	439	26.5	3.72	3.85	25.9	31.0300	0.0083	1.9275	24.00	
10:36:06	1.9358	1724.87	124	1445	440	26.09	4.10	3.85	22.35	31.2200	0.0083	1.9358	28.22	
10:36:36	1.9442	1725.03	120	1433	427	26.6	3.62	3.64	19.76	31.3600	0.0083	1.9442	23.40	
10:37:04	1.9519	1725.29	119	1454	432	25.72	4.47	3.94	32.39	31.6400	0.0078	1.9519	26.62	
10:37:31	1.9594	1725.54	120	1532	434	26.25	3.96	3.97	34.23	31.8900	0.0075	1.9594	26.62	26.67
10:38:01	1.9678	1725.75	121	1471	448	26.04	4.10	4.06	25.98	32.1000	0.0083	1.9678	27.56	
10:38:27	1.9753	1725.90	121	1491	439	25.59	4.59	4.36	33.89	32.3500	0.0072	1.9750	31.46	
10:38:57	1.9833	1726.21	120	1527	438	25.35	3.88	4.21	25.25	32.5600	0.0083	1.9833	26.31	
10:39:27	1.9917	1726.43	117	1415	424	27.24	3.08	3.91	26.29	32.7900	0.0083	1.9917	27.62	27.62
10:39:57	2.0000	1726.68	121	1629	438	25.11	4.09	3.94	39.01	33.0300	0.0083	2.0000	28.05	

DOE high power mortar test Amaco Catoosa Test Site

Well No. 6	Date: 12/16/98	Blk Type = Walker McSwain's MP6EH	Blk Size = 4.75	Blk Nozzles = 8, 9, 12, 12	Slud Type = Water Based	Mud Weight (lb/gal) = 8.70	Pipe (in) = 972.74	Collar (ft)	Commercial Motor		ROP (ft/hr)		
									Average ROP	Excluding Slugs			
Starting Depth =	1093.55												
Ending Depth =	1781.24												
Test Depth Chilled	87.53												
Hours On Bit =	4.19												
Average ROP =	21.35												
Drilling (ft) =	1718.95												
Time From Start (HH:MM:SS)	(HH:MM:SS)	SR Depth (ft)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Rlps)	WOB (Klps)	Average WOB (Klps)	ROP (ft/hr)	Hours On Bit	Incremental Hours On Bit	ROP (ft/hr)
10:40:27	2:55:03	1720.91	119	1457	433	26.71	3.56	3.61	3.61	27.22	21.2000	0.0000	27.22
10:40:57	2:55:33	1727.10	120	1420	435	25.28	4.87	3.96	3.96	28.19	33.4500	0.0054	20.957
10:41:27	2:56:03	1727.28	119	1455	432	24.66	5.43	4.19	4.19	22.08	33.6100	0.0000	25.00
10:41:57	2:56:33	1727.53	119	1681	432	25.74	4.48	4.48	4.48	30.33	33.8000	0.0000	28.96
10:42:27	2:57:03	1727.70	119	1455	431	25.36	4.81	4.82	4.82	20.7	34.0500	0.0000	23.76
10:42:57	2:57:33	1727.86	120	1488	431	25.91	4.28	4.76	4.76	23.55	34.3500	0.0023	24.00
10:43:27	2:58:03	1728.11	121	1473	428	26.09	4.16	4.62	4.62	24.66	34.4800	0.0023	24.00
10:43:57	2:58:33	1728.26	118	1435	429	25.91	4.28	4.38	4.38	22.38	34.8400	0.0053	23.68
10:44:26	2:59:02	1728.54	121	1458	428	26.15	4.08	4.31	4.31	31.41	34.8900	0.0000	25.41
10:44:56	2:59:32	1728.87	123	1393	428	26.07	4.14	4.17	4.17	14.34	35.0300	0.0000	23.29
10:45:25	2:59:61	1728.92	118	1483	428	25.02	5.13	4.34	4.34	31.23	35.1700	0.0000	24.71
10:45:52	2:59:88	1729.17	119	1494	419	26.21	3.98	4.32	4.32	32.23	35.5200	0.0073	27.55
10:46:15	2:59:53	1729.42	120	1436	424	27.36	3.96	4.04	4.04	38.51	35.7700	0.0000	28.66
10:46:45	3:00:23	1729.64	120	1426	425	25.37	3.83	4.00	4.00	25.61	35.9500	0.0000	31.76
10:47:15	3:00:53	1729.82	119	1465	431	25.04	5.14	4.20	4.20	22.24	35.1700	0.0000	25.12
10:47:45	3:01:23	1729.99	120	1433	427	24.7	5.43	4.26	4.26	20.79	35.9400	0.0000	25.85
10:48:13	3:01:53	1730.24	123	1487	421	24.11	6.03	4.06	4.06	34.37	36.9300	0.0076	25.23
10:48:42	3:02:23	1730.44	119	1487	422	25.26	5.43	5.06	5.06	23.01	36.3800	0.0000	24.82
10:49:13	3:02:54	1730.65	118	1409	430	25.02	5.14	5.32	5.32	25.39	37.0000	0.0000	25.51
10:49:38	3:03:14	1731.90	117	1465	425	26.67	3.74	6.06	6.06	35.51	37.9500	0.0000	28.28
10:50:08	3:03:44	1732.95	123	1819	422	28.63	1.68	4.29	4.29	5.34	37.3000	0.0000	22.23
10:50:34	3:04:14	1731.20	120	1485	426	27.33	2.92	3.67	3.67	35.11	37.5500	0.0072	24.69
10:51:04	3:04:44	1731.37	118	1400	433	26.72	3.59	3.39	3.39	20.08	37.9000	0.0000	23.95
10:51:34	3:05:14	1731.46	116	1325	434	27.81	2.46	3.66	3.66	10.69	37.9000	0.0000	17.07
10:52:04	3:05:44	1731.65	123	1491	427	26.13	4.08	3.42	3.42	23.01	38.0300	0.0000	21.72
10:52:28	3:06:08	1731.80	118	1485	431	25.93	4.28	3.94	3.94	42.09	38.2500	0.0000	23.50
10:52:53	3:06:33	1732.35	120	1546	427	25.62	3.56	3.77	3.77	33.2	38.5000	0.0091	26.76
10:53:18	3:07:03	1732.41	116	1571	420	26.61	3.73	3.61	3.61	41.88	38.7800	0.0000	34.22
10:53:48	3:07:33	1732.63	119	1458	424	27.03	3.21	3.96	3.96	15.31	38.8600	0.0000	31.37
10:54:18	3:08:03	1732.78	125	1549	428	26.49	4.79	4.00	4.00	59.78	39.1500	0.0042	33.70
10:54:48	3:08:33	1732.93	120	1510	425	28.66	3.57	3.95	3.95	17.48	39.3800	0.0000	28.95

DOE high power motor test Amaco Catoosa Test Site

Commercial Motor

Well No. 5	Date: 12/16/99													
Starting Depth =	1693.65					Bit Type =	Walker McCranck MP66H					Average ROP Excluding Skips		
Ending Depth =	1731.24					Bit Size =	4.75							
Total Depth Drilled	87.59					Bit Nozzles =	8, 9, 12, 12					Depth Drilled	87.59	
Hours On Bit =	4.19					Mud Type =	Water Based					Hours On Bit	3.83	
Average ROP =	21.35					Mud Weight (lbs/gal) =	8.79					Average ROP	22.32	
Drilling (ft) =	1718.05					Pipe (ft) =	577.74		Collar (ft)	740.31				
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
10:54:55	2:2494	1733.10	118	1309	430	24.61	5.54	4.15	36.1	39.5300	0.0069	2.2494	27.72	
10:55:18	2:2538	1733.43	118	1614	438	24.04	6.07	4.52	39.91	39.7800	0.0064	2:2558	34.84	29.85
10:55:27	2:2639	1733.68	118	1441	428	26.3	3.91	4.76	31.19	40.0300	0.0081	2:2638	30.29	
10:55:17	2:2732	1733.73	123	1521	442	25.1	5.05	4.93	5.88	40.0600	0.0083	2:2732	28.52	
10:56:47	2:2806	1733.87	123	1366	437	27.95	2.82	4.58	19.42	40.2200	0.0083	2:2806	22.10	
10:57:17	2:2889	1734.05	119	1522	423	24.87	3.27	4.53	21.09	40.4000	0.0083	2:2889	18.76	
10:57:31	2:2956	1734.36	119	1870	431	24.74	5.43	4.39	37.15	40.5500	0.0087	2:2956	19.58	
10:58:11	2:3039	1734.34	123	1316	442	28.03	2.25	4.06	4.67	40.6000	0.0083	2:3039	19.25	18.94
10:58:30	2:3119	1734.55	118	1481	429	25.36	4.82	4.01	31.64	40.8400	0.0081	2:3119	22.04	
10:59:16	2:3203	1734.83	119	1519	433	24.9	5.26	4.60	28.73	41.1800	0.0083	2:3203	24.65	
10:59:37	2:3278	1735.98	115	1862	429	24.92	5.22	4.59	33.05	41.4500	0.0075	2:3278	24.21	
11:00:07	2:3381	1735.23	117	1468	427	26.88	3.54	4.23	17.49	41.8800	0.0083	2:3381	27.82	
11:00:37	2:3444	1735.38	119	1436	434	27.99	2.20	4.22	15.44	41.7100	0.0083	2:3444	23.69	25.15
11:01:00	2:3508	1735.61	123	1488	446	28.62	4.56	4.17	45.48	41.9600	0.0084	2:3508	25.93	
11:01:36	2:3592	1735.82	123	1463	448	25.43	4.73	4.06	25.91	42.1700	0.0083	2:3592	23.58	
11:01:56	2:3669	1736.05	124	1550	448	24.56	5.58	4.14	32.1	42.4300	0.0078	2:3669	27.57	
11:02:28	2:3753	1736.39	122	1673	441	23.46	6.53	4.75	23.69	42.6300	0.0089	2:3753	29.84	
11:02:58	2:3836	1736.44	121	1418	439	25.56	4.51	5.26	19.35	42.7900	0.0083	2:3836	28.32	27.50
11:03:27	2:3917	1736.69	121	1462	440	25.21	4.85	5.34	31.85	43.0400	0.0081	2:3917	26.77	
11:03:56	2:3981	1736.85	117	1504	428	25.36	4.89	5.35	39.18	43.3000	0.0084	2:3981	27.98	
11:04:16	2:4053	1737.29	139	1510	431	25.16	5.00	5.24	35.39	43.5500	0.0072	2:4053	30.67	
11:04:46	2:4138	1737.40	117	1539	425	24.56	5.38	6.63	24.43	43.7900	0.0083	2:4136	32.00	32.00
11:05:13	2:4211	1737.66	118	1501	430	24.38	6.25	6.22	32.99	44.0100	0.0075	2:4211	32.94	
11:05:49	2:4286	1737.91	120	1570	437	23.67	6.42	6.51	34.2	44.2600	0.0075	2:4286	31.42	
11:06:09	2:4356	1738.15	121	1570	439	24.9	5.28	6.80	39.36	44.5100	0.0069	2:4356	31.71	
11:06:39	2:4438	1738.37	118	1493	424	27.13	3.11	6.22	25.24	44.7200	0.0083	2:4439	32.64	32.64
11:07:05	2:4522	1738.57	120	1498	437	24.73	5.40	6.19	23.62	44.9300	0.0083	2:4522	29.25	
11:07:31	2:4584	1738.82	118	1505	429	24.23	5.87	6.21	34.77	45.1700	0.0072	2:4584	29.51	
11:07:59	2:4664	1739.07	139	1547	435	24.29	5.83	6.05	35.73	45.4200	0.0069	2:4664	29.51	
11:08:21	2:4733	1739.32	120	1545	437	24.36	5.76	6.19	38.53	45.6700	0.0069	2:4733	32.28	32.28
11:08:51	2:4817	1739.54	121	1661	435	29.07	4.11	6.39	27.21	45.8600	0.0083	2:4817	31.92	

DOE high power mortar test Amaco Catoosa Test Site								Commercial Motor						
Well No. 5	Date: 12/16/98													
Starting Depth =	1893.85	Bit Type = Walker McDonald MP58H					Average ROP Excluding Steps							
Ending Depth =	1781.24	Bit Size = 4.75												
Total Depth Drilled	87.59	Bit Nozzles = 8, 9, 12, 12					Depth Drilled 87.59							
Hours On Bit =	4.16	Mud Type = Water based					Hours On Bit 3.52							
Average ROP =	21.35	Mud Weight (lbs/gal) = 8.70					Average ROP 22.93							
Drilling (ft) =	1718.05	Pipe (ft) = 977.74					Casing (ft) 740.31							
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (fpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
11:09:23	2.4690	1739.60	119	1311	431	27.08	3.34	4.93	16.79	46.9500	0.0083	2.4690	25.53	
11:09:48	2.4975	1739.89	121	1456	439	24.66	5.47	4.86	34.09	46.2000	0.0075	2.4975	25.67	
11:10:18	2.5068	1740.09	119	1658	431	23.88	6.22	4.94	28.88	45.4400	0.0083	2.5068	23.69	
11:10:46	2.5136	1740.34	124	1513	451	24.24	5.59	4.87	31.83	45.6900	0.0078	2.5136	26.98	25.32
11:11:05	2.5189	1740.59	134	1588	448	24.89	5.17	5.18	47.16	46.9400	0.0083	2.5189	34.27	
11:11:32	2.5254	1740.84	122	1513	443	25.33	4.84	5.52	34.43	47.1800	0.0075	2.5254	34.27	
11:12:03	2.5347	1741.00	119	1456	433	25.05	6.11	5.35	19.28	47.3500	0.0083	2.5347	31.50	
11:12:29	2.5422	1741.35	121	1453	436	25.34	4.82	5.17	33.41	47.6000	0.0075	2.5422	31.81	31.81
11:12:59	2.5506	1741.41	117	1462	424	25.88	4.49	4.89	18.43	47.7600	0.0083	2.5506	25.83	
11:13:26	2.5581	1741.56	122	1595	444	25.25	4.92	4.84	33.5	46.9100	0.0075	2.5581	25.89	
11:13:56	2.5664	1741.89	121	1549	439	23.68	6.42	5.15	27.44	45.2400	0.0083	2.5664	28.11	
11:14:16	2.5719	1743.14	117	1637	427	23.11	6.98	5.52	43.94	48.4900	0.0086	2.5719	29.94	
11:14:46	2.5803	1742.29	115	1478	415	24.39	5.72	5.70	16.47	48.6400	0.0083	2.5803	29.61	27.33
11:15:13	2.5878	1743.54	118	1658	427	23.23	6.76	6.16	23.51	48.8900	0.0075	2.5878	29.61	
11:15:46	2.5953	1742.50	117	1638	426	23.3	6.77	6.53	33.5	49.1500	0.0075	2.5953	31.50	
11:16:07	2.6028	1743.06	124	1606	449	23.67	6.42	6.53	33.14	49.4000	0.0075	2.6028	29.51	
11:16:36	2.6108	1743.30	130	1697	435	24.35	6.85	6.31	31.89	49.6500	0.0081	2.6108	33.05	33.05
11:17:00	2.6175	1743.55	117	1606	426	24.53	5.86	6.28	37.84	49.8600	0.0067	2.6175	33.98	
11:17:30	2.6258	1743.87	119	1658	433	24.8	6.34	6.00	14.77	50.0200	0.0083	2.6258	28.47	
11:17:57	2.6317	1743.93	118	1660	429	24.8	5.35	6.71	42.86	50.2700	0.0086	2.6317	30.12	
11:18:15	2.6383	1744.17	116	1696	427	24.5	6.83	6.58	37.8	50.5300	0.0067	2.6383	31.64	
11:18:45	2.6467	1744.39	122	1542	442	24.71	6.43	6.47	21.87	50.7100	0.0083	2.6467	27.77	29.58
11:19:09	2.6533	1744.51	119	1529	433	24.02	6.06	5.57	36.85	50.9600	0.0087	2.6533	34.18	
11:19:39	2.6617	1744.88	117	1595	426	25.7	4.47	5.39	6.56	51.0400	0.0083	2.6617	25.67	
11:20:09	2.6705	1744.90	117	1504	425	24.16	5.98	6.52	13.35	51.1800	0.0083	2.6705	19.89	
11:20:30	2.6788	1745.08	122	1521	443	24.41	5.71	5.53	43.7	51.4000	0.0081	2.6788	29.66	
11:21:00	2.6843	1745.22	129	1600	436	24.79	5.35	5.82	19.79	51.5700	0.0083	2.6843	19.79	
11:21:18	2.6892	1745.47	118	1696	423	24.73	5.42	5.38	49.25	51.8200	0.0080	2.6892	29.58	26.12
11:21:48	2.6975	1745.68	116	1512	429	25	5.18	5.52	25.42	52.0300	0.0083	2.6975	32.89	
11:22:14	2.7047	1745.94	116	1527	420	25.25	4.92	6.31	35.24	52.2900	0.0072	2.7047	30.81	
11:22:44	2.7131	1746.11	117	1621	427	24.45	5.89	5.31	20.54	52.4800	0.0083	2.7131	30.81	

DOE high power mortar test Amaco Catoosa Test Site										Commercial Motor				
Well No. 6	Date: 12/15/98													
Starting Depth =	1593.85									Average ROP Excluding Steps				
Ending Depth =	1781.24	Bit Type = Walker McClean/old MP68H												
Total Depth Drilled	87.59	Bit Size = 4.75								Depth Drilled 87.59				
Hours On Bit =	4.10	Bit Nozzles = S, S, 12, 12								Hours On Bit 3.82				
Average ROP =	21.35	Mod Type = Water Based								Average ROP 22.02				
Drilling (ft) =	1719.95	Mud Weight (lb/qt) = 8.70												
		Pipe (ft) = 577.74								Collar (ft) 749.31				
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
11:23:09	2.7197	1746.39	120	1589	435	23.83	6.28	5.49	37.75	52.7100	0.0087	2.7197	29.13	
11:23:39	2.7291	1746.51	119	1609	434	34.33	5.79	5.57	17.94	52.9800	0.0083	2.7291	27.18	26.74
11:24:08	2.7358	1746.76	120	1594	435	24.11	6.00	5.73	32.82	53.1100	0.0078	2.7358	26.38	
11:24:32	2.7431	1747.02	116	1589	423	24.21	5.91	5.93	34.88	53.3700	0.0072	2.7431	30.33	
11:24:58	2.7503	1747.27	120	1499	436	24.55	5.58	5.91	34.88	53.6200	0.0072	2.7503	29.78	
11:25:26	2.7586	1747.46	119	1523	432	24.83	5.33	5.72	23.55	53.8100	0.0069	2.7586	31.09	31.09
11:25:48	2.7642	1747.72	120	1555	437	24.71	5.43	5.65	46.43	54.0700	0.0066	2.7642	33.88	
11:26:19	2.7725	1747.93	121	1522	419	25.37	4.89	5.41	24.99	54.2800	0.0069	2.7725	30.91	
11:26:41	2.7789	1748.18	120	1571	435	24.99	5.55	5.34	40.47	54.5300	0.0064	2.7789	31.81	
11:27:11	2.7872	1748.35	120	1703	438	25.55	4.83	6.15	20.40	54.7000	0.0063	2.7872	31.11	
11:27:41	2.7956	1748.47	123	1396	443	26.99	5.83	4.66	14.18	54.8200	0.0063	2.7956	23.89	27.34
11:28:03	2.8017	1748.73	118	1511	435	25.13	5.03	4.77	89.64	55.0700	0.0061	2.8017	27.09	
11:28:33	2.8100	1748.88	119	1602	438	24.23	5.89	4.89	15.83	55.2300	0.0063	2.8100	22.50	
11:28:58	2.8189	1749.13	122	1504	444	24.7	5.44	4.86	35.83	55.4800	0.0060	2.8189	28.24	
11:29:26	2.8253	1749.29	120	1474	436	25.14	5.01	5.54	18.88	55.6400	0.0065	2.8253	27.59	
11:29:51	2.8317	1749.54	119	1698	429	23.59	6.49	5.57	38.99	55.8900	0.0064	2.8317	27.33	39.43
													19.65	
11:40:34	2.8317	1749.79	120	1187	437	30.53	0.10		20.68	56.1400	0.0060	2.8317	44.82	
11:41:04	2.8400	1749.78	119	1176	431	30.75	0.00		-1.75	56.1300	0.0063	2.8400	33.29	
11:41:34	2.8483	1749.74	120	1179	436	30.73	0.00		-4.01	56.0900	0.0063	2.8483	12.00	
11:42:04	2.8567	1749.71	118	1173	429	30.72	0.00		-3.72	56.0500	0.0063	2.8567	19.82	
11:42:54	2.8650	1749.79	117	1173	427	30.69	0.00		4.38	56.1000	0.0063	2.8650	-1.20	
11:43:02	2.8728	1750.00	122	1174	443	30.51	0.10	0.52	32.07	56.3500	0.0078	2.8728	6.71	
11:43:32	2.8811	1750.09	117	1208	427	29.71	0.97	6.20	11	56.4400	0.0063	2.8811	10.58	
11:44:02	2.8894	1750.16	119	1347	431	27.26	3.23	0.84	10.83	56.5300	0.0063	2.8894	14.36	
11:44:32	2.8978	1750.19	116	1284	428	28.38	2.76	1.27	1.39	56.5400	0.0063	2.8978	13.42	
11:45:02	2.9061	1750.42	115	1362	429	26.89	3.78	2.83	27.35	56.7700	0.0063	2.9061	12.50	
11:45:32	2.9144	1750.59	117	1495	425	25.24	5.08	3.02	18.43	56.9300	0.0063	2.9144	14.70	
11:45:43	2.9175	1750.83	117	1638	425	26.93	3.88	3.62	82.13	57.1600	0.0031	2.9175	23.17	12.12
11:46:13	2.9258	1750.88	116	1483	432	25.83	4.80	3.94	14.5	57.3800	0.0063	2.9258	27.66	
11:46:43	2.9342	1751.13	122	1469	442	25.58	5.04	4.52	26.02	57.6100	0.0063	2.9342	29.38	

DOE high power mortar test Amaco Catrosa Test Site

Commercial Motor

Well No. 6	Date: 12/16/98													
Starting Depth =	1693.68					Bit Type =	Walker McDoanaki MPBTH					Average ROP	Excluding Stops	
Ending Depth =	1781.24					Bit Size =	4.75							
Total Depth Drilled	87.56					Bit Nozzles =	9, 9, 12, 12					Depth Drilled	87.56	
Hours On Bit =	4.18					Mud Type =	Water Based					Hours On Bit	3.82	
Average ROP =	21.35					Mud Weight (lbs/gal) =	8.70					Average ROP	22.92	
Drilling (ft) =	1718.06					Pipe (") =	97.74	Collar (m)	740.51					

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
11:47:08	2.9406	1751.41	121	1528	440	25.11	5.30	4.82	48.45	57.7600	0.0064	2.9406	31.75	
11:47:35	2.9439	1751.67	120	1488	435	24.78	5.02	4.93	30.61	58.0200	0.0083	2.9489	28.76	
11:48:01	2.9538	1751.92	117	1870	424	23.38	5.96	5.54	34.97	58.2700	0.0069	2.9558	32.33	28.83
11:48:27	2.9631	1752.17	118	1615	427	24.28	6.05	5.79	35.73	58.5200	0.0072	2.9631	34.96	
11:48:57	2.9714	1752.33	120	1501	438	25.1	5.26	5.84	19.06	58.6800	0.0083	2.9714	29.64	
11:49:17	2.9769	1752.58	116	1549	433	24.92	5.43	5.86	44.79	58.9300	0.0056	2.9769	32.44	
11:49:47	2.9853	1752.73	121	1738	436	24.17	6.16	5.97	18.34	59.0900	0.0083	2.9853	27.51	
11:50:17	2.9936	1753.84	120	1523	435	27.37	3.08	5.20	13.39	59.1900	0.0083	2.9936	21.83	
11:50:47	3.0019	1753.02	120	1377	437	27.21	3.24	4.63	20.64	59.3700	0.0083	3.0019	22.58	23.86
11:51:14	3.0094	1753.27	120	1304	436	26.17	4.23	4.43	35.43	59.6200	0.0075	3.0094	21.23	
11:51:44	3.0178	1753.39	120	1542	437	26.65	4.72	4.29	14.12	59.7400	0.0083	3.0178	20.31	
11:52:05	3.0236	1753.64	118	1461	428	24.51	5.82	4.22	43.14	59.9900	0.0058	3.0236	26.87	
11:52:35	3.0319	1753.71	119	1735	433	26.19	4.22	4.45	8.85	60.0600	0.0069	3.0319	23.01	
11:53:05	3.0403	1753.80	117	1341	424	26.76	3.63	4.52	10.81	60.1500	0.0083	3.0403	17.19	
11:53:35	3.0486	1753.98	122	1443	442	25.04	5.31	4.74	21.17	60.3300	0.0083	3.0486	19.14	25.57
11:54:05	3.0569	1754.21	118	1402	420	25.46	4.89	4.78	27.52	60.5600	0.0083	3.0569	17.10	
11:54:35	3.0653	1754.36	122	1367	443	25.44	4.93	4.60	10.81	60.6900	0.0083	3.0653	17.70	
11:55:05	3.0736	1754.47	120	1413	434	25.48	4.90	4.73	20.63	60.8200	0.0083	3.0736	30.10	
11:55:35	3.0819	1754.68	118	1409	426	25.34	5.11	5.03	22.21	61.0100	0.0083	3.0819	20.40	
11:56:05	3.0903	1754.91	121	1522	438	24.87	3.89	5.10	30.64	61.2600	0.0083	3.0903	21.00	23.32
11:56:28	3.0967	1755.16	118	1627	428	24.41	5.92	5.31	39.26	61.5100	0.0084	3.0987	27.40	
11:56:58	3.1050	1755.30	118	1485	429	23.7	4.87	5.26	16.27	61.6500	0.0083	3.1050	26.44	
11:57:26	3.1129	1755.55	120	1485	447	25.58	4.89	5.24	34.8	61.9000	0.0079	3.1128	28.86	
11:57:56	3.1211	1755.75	120	1454	437	24.35	5.07	5.41	21.47	62.0800	0.0083	3.1211	26.99	
11:58:20	3.1278	1755.98	120	1548	454	23.92	6.40	5.59	37.73	62.3200	0.0057	3.1278	26.39	28.53
11:58:59	3.1361	1756.19	119	1456	433	23.95	6.36	5.64	16.32	62.4700	0.0083	3.1361	26.36	
11:59:16	3.1433	1756.37	123	1652	447	24.33	6.00	5.91	34.18	62.7200	0.0072	3.1433	26.84	
11:59:41	3.1503	1756.62	120	1622	457	24.9	5.48	6.04	36.15	62.9700	0.0069	3.1503	36.51	
12:00:11	3.1586	1756.83	119	1548	433	25.37	5.60	5.64	24.87	63.1800	0.0083	3.1586	27.57	
12:00:41	3.1669	1757.01	119	1513	431	25.46	4.90	5.54	21.74	63.3600	0.0083	3.1669	28.88	28.39
12:01:06	3.1747	1757.26	122	1386	441	26.13	5.23	5.32	32.38	63.6100	0.0078	3.1747	28.35	

DOE high power motor test Amaco Cataosa Test Site

Commercial Motor

Well No. 8	Date: 12/16/08	BR Type = Walker McDaniel MP5SH	BR Size = 4.75	Motor Type =	Motor Weight (lbs/gal) = 8.75	Water Eased	Motor (hp)	Average WDSI (Klbs)	RDP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	RDP (ft/hr)
Spending Depth =	1693.55													
Ending Depth =	1781.24													
Total Depth Drilled	87.69													
Hours On Bit =	4.10													
Average ROP =	21.38													
Drilling (H) =	1718.05													
Time From Start (HH:MM:SS)	HH:MM:SS	BR Depth (feet)	Flow (gpm)	Pressure (psi)	Calculator Speed (rpm)	Moist Load (Klbs)	WOB (Klbs)	Average WDSI (Klbs)	RDP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	RDP (ft/hr)
12:01:36	3:18:22	1757.51	132	1611	434	25.31	5.32	5.14	34.39	57.8500	0.0073	1.1822	27.83	
12:02:06	3:19:06	1757.89	119	1685	413	25.05	4.35	4.52	21.56	64.0400	0.0065	1.1906	28.62	
12:02:36	3:19:50	1757.89	118	1585	421	25.26	5.10	4.98	24.52	64.2400	0.0093	1.1989	27.35	
12:03:06	3:20:32	1758.06	119	1618	414	26.39	4.95	4.65	25.52	64.4100	0.0083	1.2072	24.83	
12:03:36	3:21:16	1758.32	122	1625	411	26.33	4.80	4.91	26.43	64.5700	0.0094	1.2156	25.85	
12:04:06	3:22:00	1758.49	120	1631	417	25.85	4.82	4.87	26.55	64.8400	0.0083	1.2239	25.48	
12:04:36	3:22:44	1758.74	120	1554	416	24.77	5.82	5.11	16.42	65.0000	0.0056	1.2275	29.71	
12:05:06	3:23:28	1758.94	119	1512	432	24.51	5.83	5.28	23.44	65.1600	0.0083	1.2358	30.76	
12:05:36	3:24:12	1759.19	122	1583	425	25	5.35	5.33	42.12	65.3400	0.0056	1.2442	31.01	
12:06:06	3:24:56	1759.36	118	1435	435	25.24	5.15	5.35	20.35	65.7100	0.0083	1.2526	31.51	22.81
12:06:36	3:25:40	1759.62	118	1525	438	24.12	6.21	5.62	62.16	65.9700	0.0083	1.2610	33.58	
12:07:06	3:26:24	1759.87	117	1602	437	24.13	6.18	5.74	42.37	66.2200	0.0058	1.2694	38.48	
12:07:36	3:27:08	1759.97	121	1465	440	24.94	6.41	6.55	16.69	66.4800	0.0083	1.2778	38.25	
12:08:06	3:27:52	1760.22	121	1365	438	24.95	5.42	5.95	59.97	66.5700	0.0047	1.2771	37.30	35.61
12:08:36	3:28:36	1760.48	121	1452	438	25.06	6.44	5.53	27.52	66.8300	0.0083	1.2855	31.49	
12:09:06	3:29:20	1760.73	121	1504	439	24.8	6.74	5.23	31.59	67.0500	0.0083	1.2939	25.79	
12:09:36	3:30:04	1760.99	120	1571	437	21.72	6.92	5.61	87.73	67.2900	0.0065	1.3023	27.14	
12:10:06	3:30:48	1761.09	119	1473	439	25.07	6.29	5.49	17.15	67.4500	0.0083	1.3107	28.08	
12:10:36	3:31:32	1761.34	119	1820	435	24.73	6.61	6.51	39	67.6000	0.0084	1.3191	31.72	30.78
12:11:06	3:32:16	1761.63	119	1820	431	24.44	5.69	5.78	24.86	67.8600	0.0083	1.3275	35.50	
12:11:36	3:33:00	1761.89	124	1957	439	24.63	5.72	5.79	48.09	68.1300	0.0063	1.3359	31.09	
12:12:06	3:33:44	1762.15	117	1552	436	23.68	6.32	5.73	29.58	68.3700	0.0083	1.3443	22.82	
12:12:36	3:34:28	1762.43	117	1728	437	24.26	6.05	6.03	10.45	68.6200	0.0081	1.3527	27.78	
12:13:06	3:35:12	1762.72	121	1809	438	27.45	6.00	6.37	10.45	68.8700	0.0083	1.3611	23.74	34.09
12:13:36	3:35:56	1762.98	119	1421	431	28.52	4.08	6.05	26.09	69.1300	0.0083	1.3695	29.49	
12:14:06	3:36:40	1763.26	121	1525	431	28.61	4.57	4.80	24.06	69.3900	0.0083	1.3779	28.16	
12:14:36	3:37:24	1763.54	118	1482	431	28.48	3.94	4.33	34.53	69.6500	0.0072	1.3863	23.56	
12:15:06	3:38:08	1763.83	120	1521	435	28.83	5.72	4.26	13.34	69.9100	0.0083	1.3947	24.51	
12:15:36	3:38:52	1764.11	118	1573	430	28.41	5.88	5.04	68.11	70.1700	0.0082	1.4031	18.23	28.31
12:16:06	3:39:36	1764.39	116	1515	432	24.44	5.82	5.40	32.59	70.4300	0.0081	1.4115	17.32	
12:16:36	3:40:20	1764.67	116	1531	432	24.75	5.59	5.96	33.59	70.6900	0.0075	1.4199	17.01	

DOE high power mortar test Amaco Catoosa Test Site										Commercial Motor					
Well No. 6	Date: 12/16/98														
Starting Depth =	1693.55						Bit Type =	Walker McDonald MP88H			Average ROP Excluding Stops				
Ending Depth =	1791.34						Bit Size =	4.75							
Total Depth Drilled	87.59						Bit Nozzles =	3 9, 12, 12			Depth Drilled	87.59			
Hours On Bit =	4.10						Mud Type =	Water Based			Hours On Bit	3.82			
Average ROP =	21.35						Mud Weight (lb/gal) =	8.78			Average ROP	22.92			
Circulating (ft) =	1718.66						Pipe (ft) =	577.74		Collar (ft)	740.31				
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)	
12:15:08	3:4972	1764.07	119	1845	431	28.58	5.77	5.97	35.5	70.8200	0.0072	3:4972	37.86		
12:15:38	3:4158	1764.11	125	1878	438	37.82	2.84	5.38	5.54	70.4800	0.0083	3:4158	26.04		
12:16:06	3:4239	1764.29	115	1440	434	28.38	3.85	4.83	21.49	70.6400	0.0083	3:4239	23.28	35.43	
12:16:36	3:4319	1764.55	120	1456	434	28.2	4.21	4.49	32.23	70.9000	0.0083	3:4319	23.17		
12:17:03	3:4337	1764.80	119	1554	432	28.56	4.83	4.34	31.34	71.1500	0.0078	3:4337	22.48		
12:17:33	3:4483	1764.97	122	1496	443	25.95	4.44	4.07	20.3	71.3200	0.0083	3:4483	36.46		
12:18:00	3:4558	1765.22	115	1808	423	24.41	5.22	4.59	39.42	71.5700	0.0075	3:4558	29.37	28.37	
12:18:30	3:4639	1765.36	121	1659	430	36.42	4.39	4.68	18.52	71.7100	0.0083	3:4639	25.36		
12:19:00	3:4723	1765.39	116	1305	427	27.42	3.03	4.44	3.39	71.7400	0.0083	3:4723	18.15		
12:19:30	3:4806	1765.54	120	1356	437	25.58	4.80	4.14	18.34	71.9800	0.0083	3:4806	17.53		
12:20:00	3:4889	1765.78	120	1600	437	23.2	7.09	4.97	26.51	72.1100	0.0083	3:4889	15.29		
12:20:39	3:4950	1766.02	119	1676	431	34.56	5.77	4.94	32.8	72.3700	0.0083	3:4950	21.21		
12:20:58	3:5034	1766.15	120	1872	437	24.8	5.95	5.28	16	72.5000	0.0083	3:5034	24.43	18.47	
12:21:14	3:5084	1766.40	119	1495	434	28.61	4.76	5.59	41.09	72.7500	0.0083	3:5084	28.77		
12:21:44	3:5178	1766.51	118	1538	438	24.36	5.97	5.83	12.64	72.8600	0.0083	3:5178	23.86		
12:21:56	3:5217	1766.76	119	1496	434	24.43	5.89	5.50	65.05	73.1100	0.0039	3:5217	27.75		
12:22:28	3:5300	1766.88	119	1573	431	34.33	6.00	5.53	15.06	73.2900	0.0083	3:5300	27.38		
12:22:49	3:5358	1767.14	119	1535	431	34.68	5.71	5.67	43.22	73.4900	0.0058	3:5358	28.04	38.96	
12:23:19	3:5442	1767.36	122	1565	442	24.99	5.35	5.78	26.36	73.7100	0.0083	3:5442	32.21		
12:23:43	3:5506	1767.61	122	1594	443	25.37	4.99	5.58	36.87	73.9600	0.0087	3:5506	29.14		
12:24:13	3:5592	1767.86	119	1533	431	35.87	4.52	5.31	30.94	74.2100	0.0083	3:5592	33.60		
12:24:45	3:5675	1767.97	115	1654	417	25.32	4.09	4.93	13.61	74.3200	0.0083	3:5675	26.21		
12:25:13	3:5758	1768.16	120	1358	435	27.29	5.08	4.90	23.44	74.5100	0.0083	3:5758	35.28	25.50	
12:25:45	3:5836	1768.41	118	1518	429	26.23	4.19	4.17	31.41	74.7600	0.0078	3:5836	24.41		
12:26:17	3:5919	1768.59	119	1610	433	26.49	3.68	3.96	21.2	74.9400	0.0083	3:5919	27.27		
12:26:41	3:5993	1768.60	121	1371	440	29.46	1.08	3.27	0.59	74.9500	0.0083	3:5993	19.23		
12:27:09	3:5981	1768.85	119	1383	434	27.88	2.75	3.01	35.72	75.2000	0.0078	3:5981	21.41		
12:27:39	3:6184	1769.00	120	1625	435	27.23	3.22	3.04	18.78	75.3500	0.0083	3:6184	18.00		
12:28:05	3:6347	1769.08	121	1326	438	28.88	2.40	2.68	19.78	75.4400	0.0083	3:6347	15.25	19.62	
12:28:39	3:6331	1769.23	128	1352	438	27.1	3.34	2.58	16.89	75.8800	0.0083	3:6331	18.38		
12:29:07	3:6408	1769.38	115	1352	419	26.39	3.82	3.13	32.0	75.8300	0.0078	3:6408	18.22		

DOE high power mortar test Amaco Catoosa Test Site

Commercial Motor

Well No. 6		Date: 12/18/98		Bit Type = Walker McDoanale MP68H		Bit Size = 4.75		Average ROP Excluding Stops						
Starting Depth = 1693.89		Ending Depth = 1781.24		Bit Nozzles = 9, 9; 12, 12		Mud Type = Water Based		Depth Drilled 87.35						
Total Depth Drilled 87.35		Hours On Bit = 4.19		Mud Weight (lbs/gal) = 8.70		Average ROP = 21.39		Hours On Bit 3.62						
Average ROP = 21.39		Casing (ft) = 1718.01		Pipe (ft) = 977.74		Casing (ft) = 746.31		Average ROP = 22.92						
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
12:29:37	3.6493	1769.53	119	1447	421	29.31	4.10	3.49	5.87	75.8800	0.0083	3.6493	16.17	
12:29:57	3.6547	1769.79	120	1472	445	29.65	4.83	3.72	45.19	76.1400	0.0056	3.6547	23.33	
12:30:27	3.6631	1769.89	121	1421	439	29.99	4.79	4.29	8.33	76.2100	0.0083	3.6631	21.00	
12:30:47	3.6689	1770.11	119	1442	434	24.7	5.64	4.88	45.32	76.4600	0.0058	3.6689	22.68	23.24
12:31:17	3.6789	1770.26	118	1487	427	24.77	6.57	4.89	18.31	76.6100	0.0083	3.6789	36.28	
12:31:47	3.6883	1770.48	119	1499	434	24.44	5.89	5.34	25.33	76.8900	0.0083	3.6883	28.58	
12:32:17	3.6908	1770.69	118	1508	428	25.57	4.82	5.24	24.14	77.0300	0.0083	3.6908	26.84	
12:32:47	3.7019	1770.72	122	1476	442	28.74	1.77	4.74	4.85	77.0700	0.0083	3.7019	16.30	
12:33:17	3.7109	1770.87	122	1375	441	28.83	3.79	4.37	18.06	77.2200	0.0083	3.7109	16.30	
12:33:47	3.7189	1771.10	117	1492	436	29.81	4.66	4.17	27.66	77.4500	0.0083	3.7189	18.69	19.89
12:34:17	3.7269	1771.32	122	1454	444	29.11	4.29	3.85	35.77	77.6700	0.0083	3.7269	19.20	
12:34:47	3.7353	1771.55	119	1458	432	28.49	3.93	3.67	27.89	77.9000	0.0083	3.7353	24.90	
12:35:17	3.7436	1771.87	121	1443	439	28.36	4.05	4.13	14.43	78.0200	0.0083	3.7436	24.00	
12:35:36	3.7497	1771.92	123	1479	447	29.93	4.47	4.29	40.95	78.3700	0.0051	3.7497	26.36	
12:36:09	3.7581	1773.09	122	1423	444	28.5	3.92	4.13	19.83	78.4400	0.0083	3.7581	24.75	25.10
12:36:39	3.7684	1772.31	118	1438	434	28.17	4.23	4.12	28.46	78.6600	0.0083	3.7684	24.43	
12:37:05	3.7739	1772.59	120	1476	437	29.54	4.84	4.39	14.81	78.9100	0.0075	3.7739	25.39	
12:37:36	3.7823	1772.84	117	1461	426	29.88	4.43	4.28	9.86	78.9900	0.0083	3.7823	32.15	
12:37:52	3.7867	1772.93	117	1549	427	29.42	4.96	4.48	55.1	79.2500	0.0044	3.7867	28.31	
12:38:22	3.7956	1773.12	119	1483	432	29.91	4.59	4.61	27.2	79.4700	0.0083	3.7956	28.31	27.88
12:38:52	3.8033	1773.28	119	1477	432	29.37	4.99	4.76	16.05	79.5100	0.0083	3.8033	13.77	
12:39:06	3.8072	1773.51	119	1504	431	29.53	4.89	4.76	37.56	79.8600	0.0039	3.8072	34.80	
12:39:36	3.8156	1773.64	117	1477	427	29.58	4.89	4.84	15.41	79.8900	0.0083	3.8156	25.62	
12:40:03	3.8231	1773.89	121	1497	438	35.1	6.26	4.99	33.44	80.2400	0.0075	3.8231	27.48	
12:40:33	3.8314	1774.07	117	1486	427	24.51	6.82	6.14	22.08	80.4200	0.0083	3.8314	38.87	36.11
12:41:03	3.8397	1774.23	117	1469	426	24.77	6.57	5.26	22.97	80.6100	0.0083	3.8397	24.68	
12:41:33	3.8481	1774.47	120	1481	437	23.78	6.58	5.00	24.35	80.8200	0.0083	3.8481	25.54	
12:41:58	3.8559	1774.72	118	1516	429	23.62	6.77	6.99	36.03	81.0700	0.0069	3.8559	25.98	
12:42:26	3.8633	1774.91	118	1471	426	23.79	6.51	6.24	22.24	81.2600	0.0063	3.8633	26.38	
12:42:49	3.8692	1775.16	120	1514	436	23.57	6.71	6.42	14.08	81.5100	0.0058	3.8692	38.57	28.85
12:43:19	3.8775	1775.33	121	1504	438	23.27	7.02	6.71	30.48	81.6800	0.0083	3.8775	29.21	

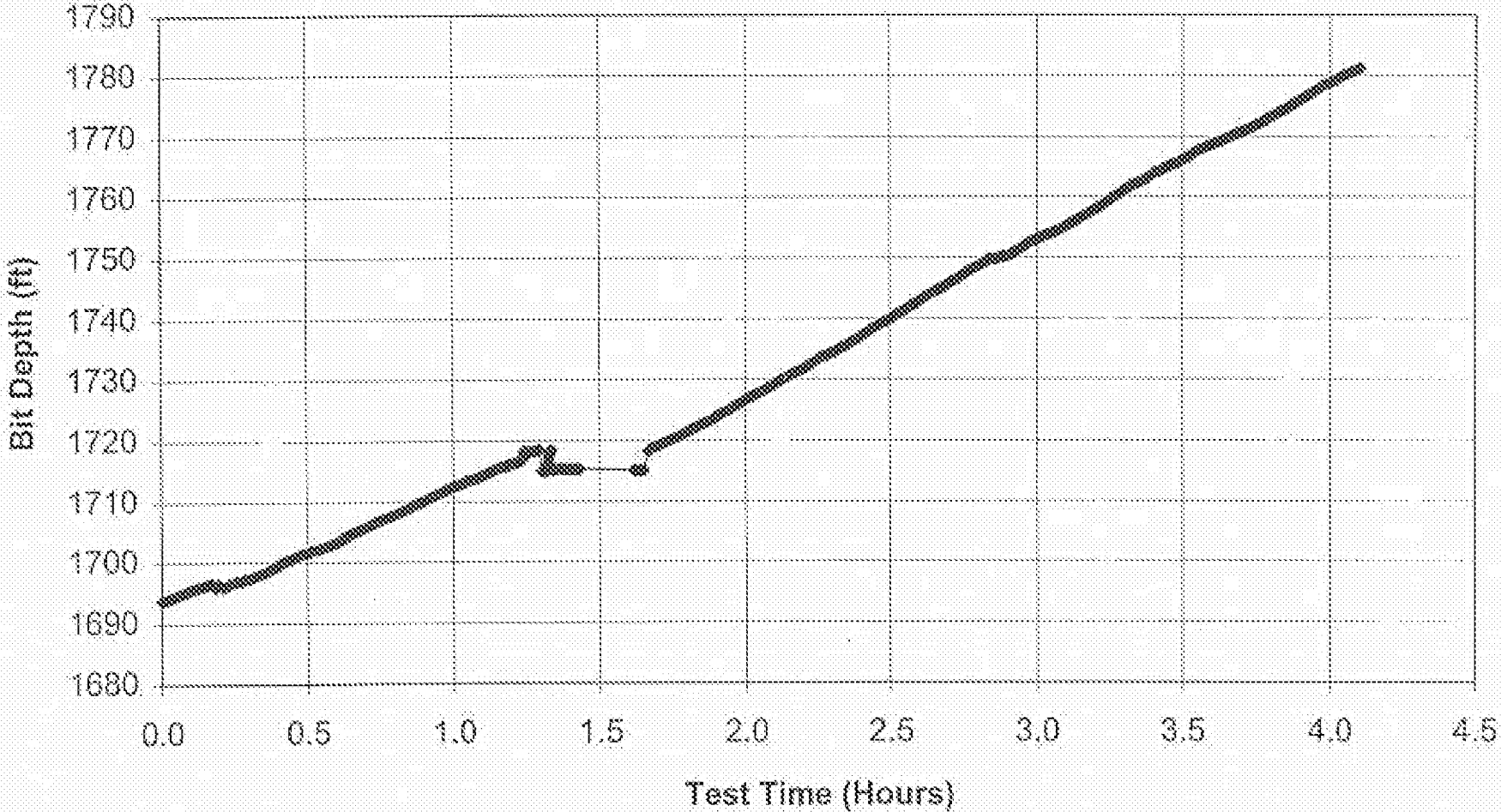
DOE high power mortar test Amaco Catoosa Test Site

Commercial Motor

Well No. 6	Date: 12/16/98														
Starting Depth =	1693.85	Bit Type = Walker McDonald MP68H										Average ROP Excluding Slugs			
Ending Depth =	1781.24	Bit Size = 4.75													
Total Depth Drilled	87.39	Bit Nozzles = 5, 9, 12, 12										Depth Drilled			
Hours On Bit =	4.10	Mud Type = Water Based										Hours On Bit			
Average ROP =	21.35	Mud Weight (lb/gal) = 9.70										Average ROP			
Drilling (ft) =	1718.05	Pipe (ft) = 977.74										Casing (ft) 740.31			
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)	
12:43:47	3.8853	1775.58	121	1498	439	23.97	6.34	6.67	31.44	81.9300	0.0078	3.8853	26.41		
12:44:12	3.8928	1776.84	119	1579	431	23.19	7.16	6.75	37.32	82.1900	0.0089	3.8922	32.19		
12:44:50	3.9000	1776.09	119	1487	433	25.73	4.65	6.38	32.19	89.4499	0.0078	3.9000	30.16	30.16	
12:45:38	3.9078	1776.34	121	1475	441	25.27	5.10	6.05	32.13	82.6900	0.0078	3.9078	33.36		
12:45:38	3.9151	1775.48	119	1501	433	28.37	5.01	5.65	34.11	82.8100	0.0083	3.9163	38.54		
12:45:58	3.9211	1776.71	120	1467	436	24.77	6.57	5.80	51.12	83.0800	0.0050	3.9211	30.12		
12:46:29	3.9294	1776.99	123	1497	448	24.74	5.60	5.18	21.78	83.2400	0.0083	3.9294	27.17		
12:46:55	3.9378	1777.12	121	1478	438	24.86	5.67	5.39	26.83	83.4700	0.0081	3.9378	26.00	27.26	
12:47:23	3.9460	1777.37	119	1485	431	24.37	6.06	5.50	34.87	83.7200	0.0072	3.9460	31.50		
12:47:51	3.9531	1777.62	118	1578	439	24.41	5.92	5.76	30.76	83.9700	0.0081	3.9531	28.49		
12:48:21	3.9614	1777.83	122	1483	444	29.47	5.86	5.82	25.96	84.1900	0.0083	3.9614	29.43		
12:48:49	3.9692	1778.05	123	1467	445	23.83	6.17	5.99	32.65	84.4100	0.0078	3.9692	30.80	30.80	
12:49:11	3.9783	1778.34	118	1505	430	23.75	6.58	6.17	41.89	84.6900	0.0061	3.9783	32.04		
12:49:41	3.9836	1778.52	121	1823	440	22.71	7.55	6.47	21.14	84.8700	0.0081	3.9836	29.45		
12:50:11	3.9819	1779.51	119	1373	434	25.04	5.32	6.35	11.84	84.9600	0.0083	3.9819	26.53		
12:50:41	4.0003	1778.76	119	1472	427	24.67	5.76	6.33	19.54	85.1300	0.0083	4.0003	23.18		
12:51:09	4.0091	1779.03	122	1477	442	24.67	5.67	6.17	32.62	85.3800	0.0078	4.0091	21.09	24.17	
12:51:38	4.0184	1779.32	119	1489	421	24.81	5.54	5.97	31.18	85.4700	0.0083	4.0184	19.31		
12:51:38	4.0217	1779.37	118	1859	423	23.47	5.83	5.82	47.4	85.7200	0.0053	4.0217	25.57		
12:52:29	4.0306	1779.58	117	1934	427	23.68	6.61	6.08	25.06	85.9300	0.0083	4.0306	26.82		
12:52:54	4.0372	1779.83	119	1537	431	24.29	6.03	6.34	34.16	86.1600	0.0078	4.0372	27.43		
12:53:24	4.0459	1780.02	117	1884	425	24.98	5.37	6.08	23.2	86.3700	0.0083	4.0456	30.85	26.40	
12:53:54	4.0539	1780.17	120	1386	437	27.06	3.29	5.65	17.2	86.5200	0.0083	4.0539	24.63		
12:54:24	4.0622	1780.33	117	1500	425	25.28	3.08	5.30	19.87	86.6800	0.0083	4.0622	21.28		
12:54:52	4.0700	1780.58	122	1464	443	26.5	4.65	4.95	32.63	86.9300	0.0078	4.0700	22.88		
12:55:22	4.0783	1780.65	113	1629	418	25.38	5.82	4.75	6.89	87.0000	0.0083	4.0783	19.32		
12:55:52	4.0857	1780.78	118	1406	421	26.01	4.39	4.53	15.66	87.1000	0.0083	4.0857	18.81		
12:56:22	4.0950	1780.99	120	1474	439	23.45	4.93	4.86	23.31	87.3400	0.0083	4.0950	30.14		
12:56:52	4.1016	1781.24	117	1438	426	26.74	3.68	4.58	35.71	87.5800	0.0069	4.1016	23.66	21.64	

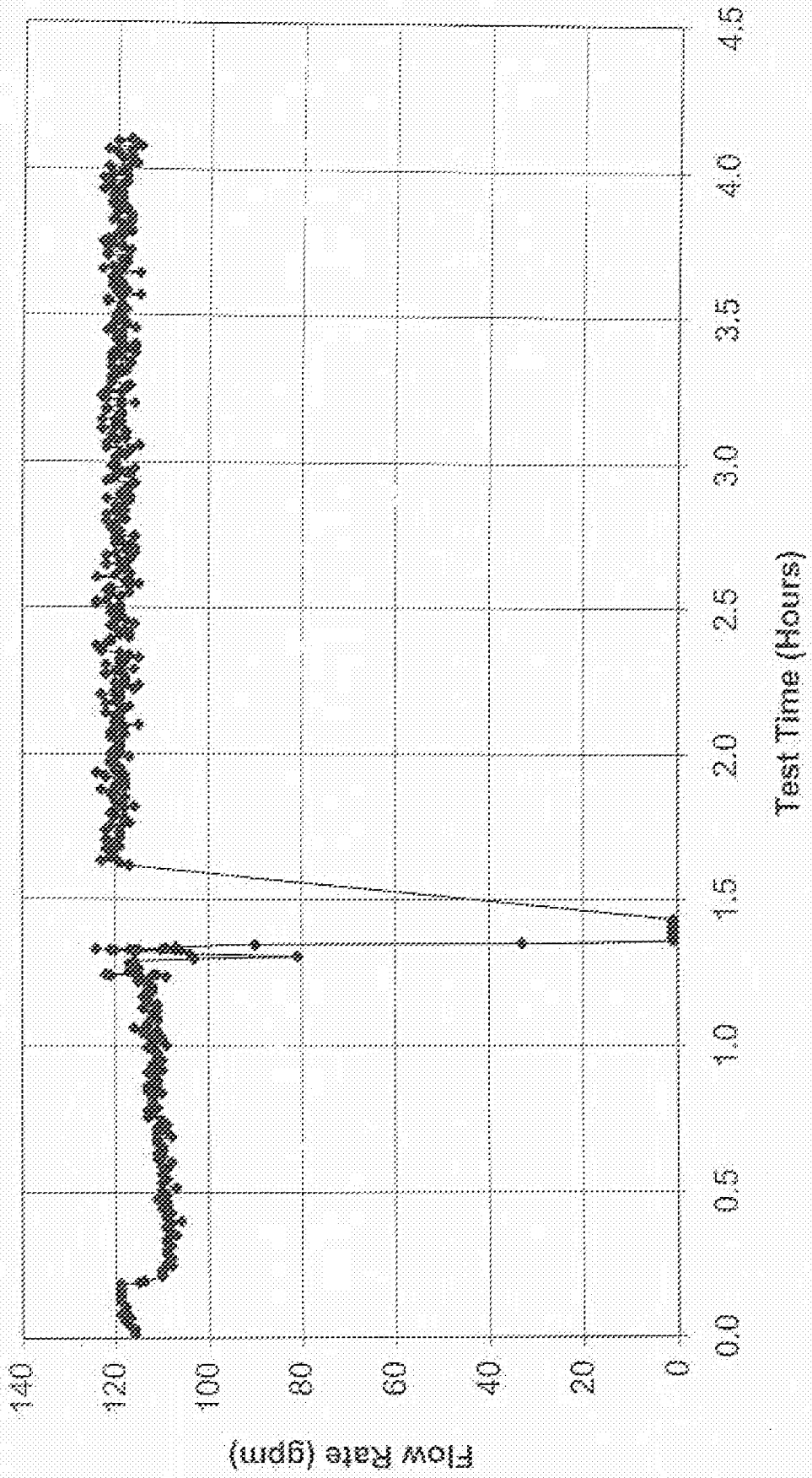
Bit Depth DOE HP Motor Test

Commercial Motor



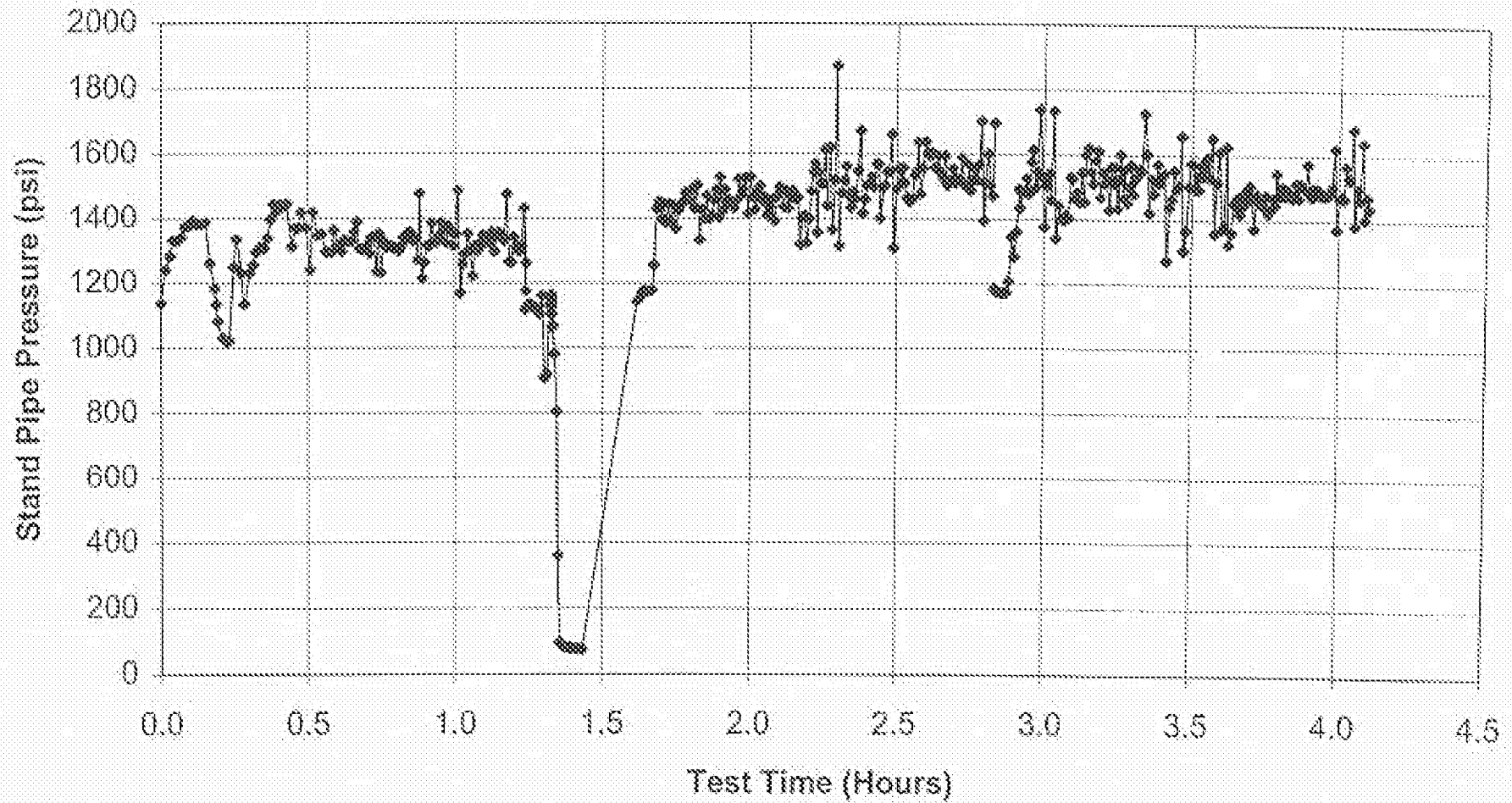
Flow DOE SH-HP Motor Test

Commercial Motor



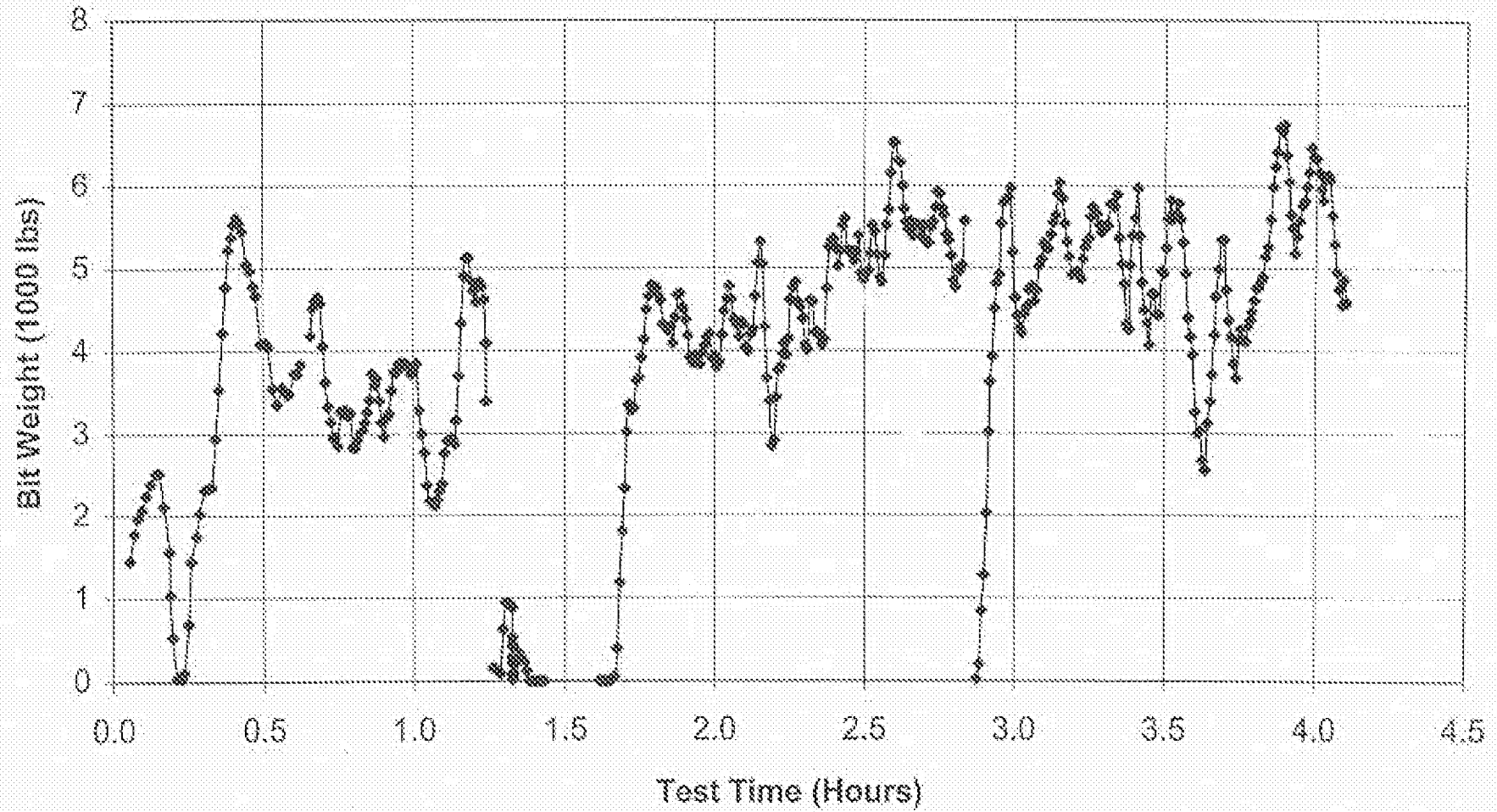
Pressure DOE SH-HP Motor Test

Commercial Motor



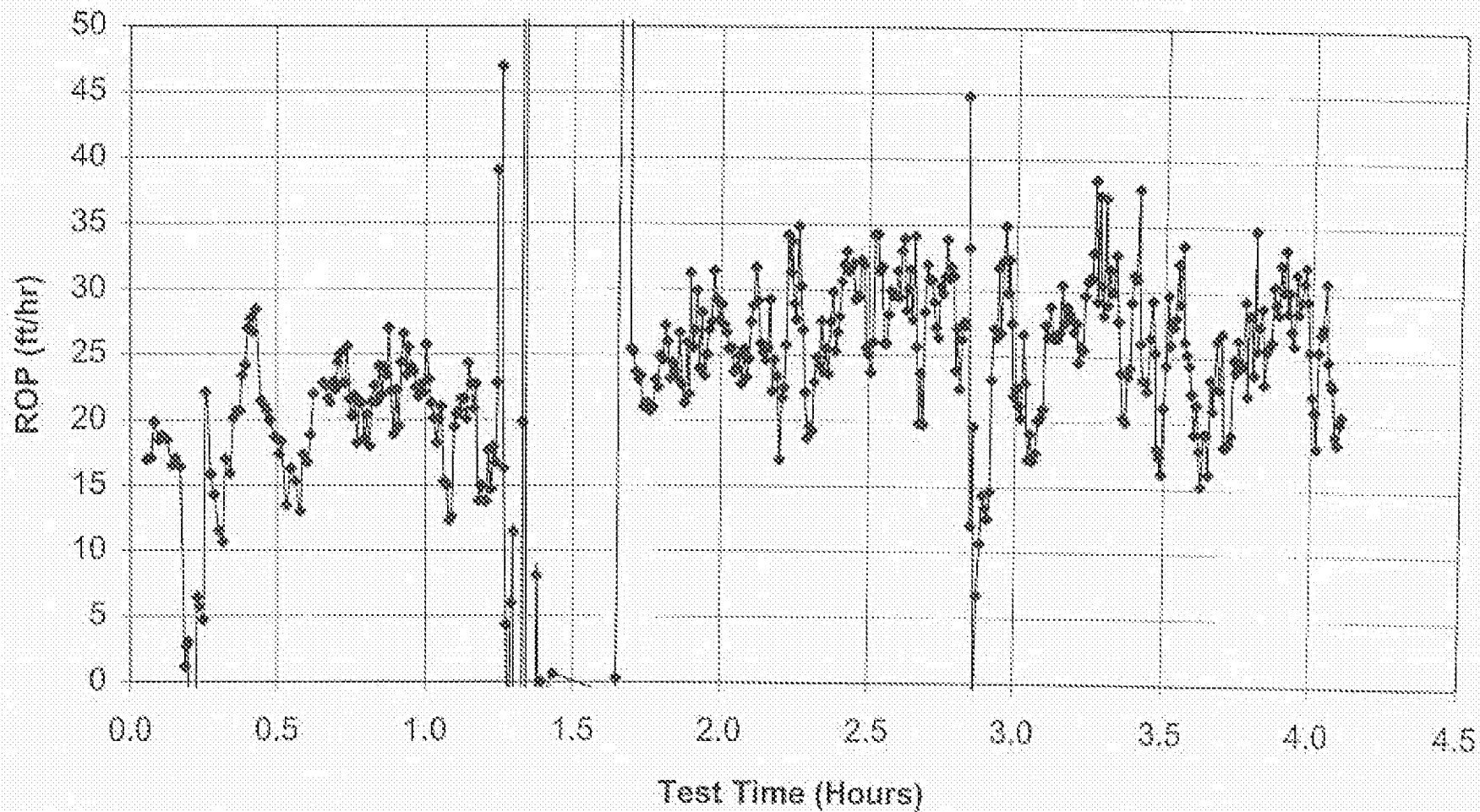
Weight On Bit DOE SH-HP Motor Test

Commercial Motor



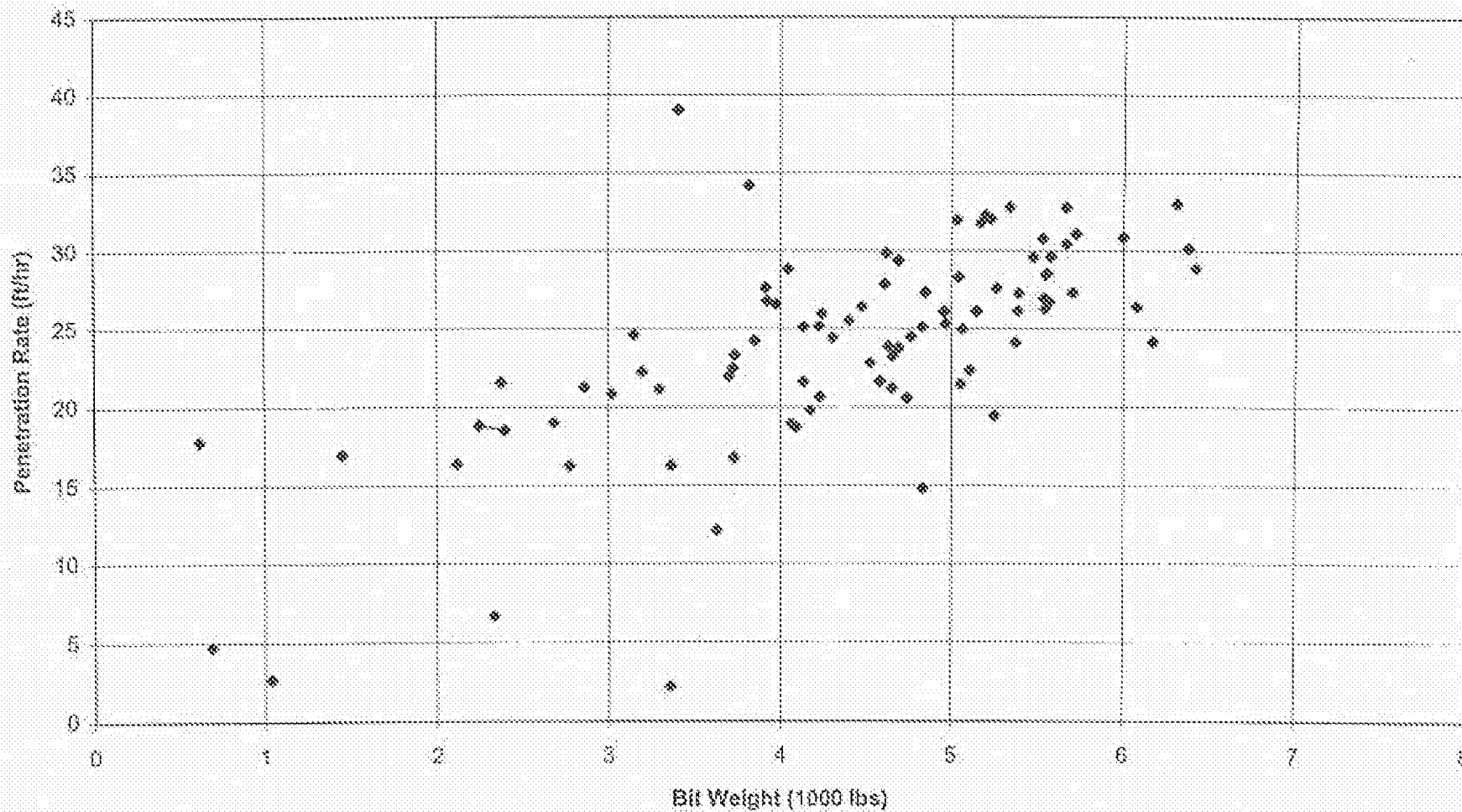
Penetration Rate DOE SH-HP Motor Test

Commercial Motor



ROP As Function Of Bit Weight DOE HP Motor Test

Commercial Motor



DOE high power motor test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/99														
Starting Depth =	1781	Bit Type =	Walker McDoanstd MP68H										Average ROP Excluding Stops		
Ending Depth =	1919	Bit Size =	4.75												
Total Depth Drilled	138	Bit Nozzles =	9, 9, 12, 12										Depth Drilled =	135.33	
Hours On Bit =	2.89	Mud Type =	Water Based										Hours On Bit =	2.89	
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70										Average ROP	48.34	
Drilling (ft) =	1789.68	Pipe (ft) =	1041.35	Collar (ft)	740.61										
Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Fest On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)	
8:06:36	0.0000	1780.94	116	1962	418	29.63	0.76		8.16	88.85	0.0000	0.0000			
8:06:56	0.0003	1780.65	116	1926	421	27.40	3.09		13.33	86.86	0.0003	0.0003	0.00		
8:07:28	0.0107	1780.94	117	1938	424	35.15	4.30		20.41	86.66	0.0003	0.0107	0.00		
8:07:56	0.0254	1780.99	118	1960	423	36.44	4.01		17.94	86.65	0.0003	0.0250	0.00		
8:08:25	0.0333	1781.13	117	1932	425	28.76	3.72	3.18	17.01	86.65	0.0003	0.0333	0.00		
8:08:55	0.0417	1781.30	117	1955	424	28.75	3.72	3.77	20.35	86.65	0.0003	0.0417	0.00		
8:09:28	0.0500	1781.40	117	1973	425	26.61	3.86	3.92	13.95	86.7	0.0003	0.0500	0.00		
8:09:55	0.0583	1781.52	118	1957	426	26.98	3.50	3.76	14.08	86.87	0.0003	0.0583	20.40		
8:10:25	0.0667	1781.75	118	1938	426	26.17	4.20	3.82	27.47	87.04	0.0003	0.0667	20.40		
8:10:51	0.0738	1782.00	118	1956	428	25.55	4.87	4.05	35.55	87.27	0.0072	0.0730	31.82	19.76	
8:11:21	0.0822	1782.21	118	1987	426	25.36	5.04	4.31	34.93	87.52	0.0003	0.0822	38.06	21.11	
8:11:39	0.0869	1782.46	117	1995	427	22.43	7.88	5.11	50.77	87.72	0.0047	0.0869	42.95	23.05	
8:11:59	0.0903	1782.71	117	2080	424	21.75	8.49	5.11	77.33	87.97	0.0053	0.0903	75.90	26.39	
8:12:04	0.0942	1782.98	118	2001	420	21.39	8.69	7.03	66.14	88.34	0.0039	0.0942	85.14	28.08	
8:12:34	0.1025	1783.02	118	1942	428	27.42	3.08	6.69	0.53	88.24	0.0003	0.1025	0.00	28.27	
8:12:59	0.1084	1783.27	118	1790	431	22.86	7.44	7.16	35.29	88.6	0.0003	0.1084	37.44	31.65	
8:13:14	0.1136	1783.52	120	1936	436	21.51	8.75	7.33	61.34	88.65	0.0042	0.1136	52.69	38.19	
8:13:44	0.1219	1783.71	118	1930	427	37.61	2.91	6.23	22.69	89.01	0.0003	0.1219	22.88	35.86	
8:14:14	0.1303	1783.91	118	1845	431	23.97	8.39	5.72	24.66	89.18	0.0003	0.1303	38.45	33.87	
8:14:34	0.1359	1784.17	118	1825	430	22.50	7.80	6.66	14.75	89.45	0.0056	0.1358	59.46	36.56	
8:14:47	0.1394	1784.42	118	2067	429	20.49	9.73	7.12	69.94	89.73	0.0036	0.1394	72.00	37.33	
8:15:02	0.1436	1784.67	118	1924	430	21.75	8.54	7.67	61.51	89.94	0.0042	0.1435	52.50	35.75	
8:15:15	0.1464	1784.92	117	2069	425	22.23	8.08	8.10	95.30	90.2	0.0028	0.1464	93.00	37.53	
8:15:22	0.1492	1785.17	118	2062	430	22.37	7.93	8.51	84.87	90.32	0.0029	0.1492	115.20	38.87	
8:15:33	0.1522	1785.43	117	2047	425	21.69	8.57	8.86	82.50	90.7	0.0004	0.1522	58.91	39.49	
8:15:49	0.1558	1785.68	118	1983	429	23.15	7.19	8.95	73.88	90.94	0.0006	0.1558	66.46	41.16	
8:15:58	0.1585	1785.94	118	2126	428	21.58	8.71	8.99	65.77	91.13	0.0028	0.1586	50.00	60.83	
8:16:05	0.1611	1786.19	116	2109	428	22.47	7.83	8.04	110.47	91.49	0.0025	0.1611	120.00	73.95	
8:16:22	0.1638	1786.44	119	1938	431	20.38	9.82	8.44	53.00	91.78	0.0047	0.1658	61.41	75.87	
8:16:32	0.1685	1786.69	117	2588	425	17.78	12.32	9.19	84.63	91.95	0.0028	0.1686	61.20	77.63	

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/98													
Starting Depth =	1781	Bit Type =	Walker McDonald MP68H	Average ROP Excluding Slips										
Ending Depth =	1916	Bit Size =	4.75											
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12	Depth Drilled =	135.33									
Hours On Bit =	2.80	Mud Type =	Water Based	Hours On Bit =	2.80									
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.75	Average ROP	48.34									
Drillstring (ft) =	1789.66	Pipe (ft) =	1041.85	Collar (ft)	749.61									

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Klps)	WOB (Klps)	Average WOB (Klps)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
8:17:02	0.1789	1786.70	120	1527	437	28.74	1.78	8.11	1.36	92.62	0.0063	0.1789	8.40	60.90
8:17:23	0.1836	1788.85	119	1698	433	24.75	6.61	7.49	37.98	92.21	0.0067	0.1836	28.50	54.54
8:17:42	0.1881	1787.20	119	1972	434	24.19	8.14	7.19	58.12	92.5	0.0044	0.1881	69.28	52.20
8:17:54	0.1914	1787.45	119	1953	433	22.31	7.97	5.78	73.36	92.72	0.0033	0.1914	68.65	51.57
8:18:09	0.1956	1787.70	118	1923	430	23.81	6.82	5.69	69.97	93.02	0.0042	0.1956	72.66	50.85
8:18:29	0.2011	1787.95	117	1942	427	22.87	7.42	6.73	43.88	93.23	0.0056	0.2011	37.80	47.53
8:18:45	0.2058	1788.21	120	1903	435	21.53	6.71	7.35	59.20	93.53	0.0047	0.2058	63.53	48.17
8:19:05	0.2111	1788.46	118	1869	427	21.81	8.63	7.85	49.29	93.73	0.0053	0.2111	97.59	44.81
8:39:22	0.2111	1788.53	116	1355	423	30.79	0.47		147.34	93.97	0.0000	0.2111	0.00	
8:39:29	0.2131	1788.79	118	1354	422	30.81	0.38		131.73	94.18	0.0019	0.2131	87.43	
8:39:57	0.2206	1789.04	117	1507	426	27.82	4.00		33.00	94.3	0.0078	0.2206	29.87	
8:40:23	0.2281	1789.29	118	1586	421	23.82	7.09		34.75	94.6	0.0072	0.2281	31.54	
8:40:53	0.2364	1789.45	117	1557	425	26.86	1.27	2.64	19.17	94.76	0.0083	0.2364	19.20	
8:41:22	0.2444	1789.70	119	1691	423	27.86	3.17	3.19	31.33	94.97	0.0081	0.2444	26.07	
8:41:43	0.2503	1789.95	115	1718	419	25.85	5.80	4.38	41.42	95.26	0.0058	0.2503	49.71	
8:41:58	0.2539	1790.30	119	1976	431	22.64	8.22	5.13	79.69	95.48	0.0036	0.2539	55.38	
8:42:10	0.2578	1790.46	118	1894	428	24.66	6.27	4.97	69.67	95.78	0.0039	0.2578	74.67	
8:42:24	0.2617	1790.71	117	1912	426	23.41	7.47	6.21	62.79	96	0.0039	0.2617	64.28	43.12
8:42:35	0.2650	1790.96	118	2011	428	22.90	7.98	7.17	77.68	96.34	0.0033	0.2650	72.66	41.78
8:42:50	0.2689	1791.21	119	1921	433	24.01	6.80	7.37	66.83	96.48	0.0039	0.2689	61.71	48.16
8:43:00	0.2717	1791.46	119	2131	430	32.80	8.25	7.37	87.80	96.77	0.0028	0.2717	104.40	49.76
8:43:13	0.2753	1791.71	117	1998	424	25.04	5.92	7.30	78.89	96.97	0.0036	0.2753	65.38	58.11
8:43:27	0.2792	1791.96	118	1923	428	23.86	7.06	7.22	61.13	97.38	0.0039	0.2792	76.71	55.89
8:43:40	0.2828	1792.21	119	1991	432	23.58	7.31	7.69	72.67	97.51	0.0036	0.2828	68.89	69.54
8:43:51	0.2858	1792.46	118	2016	429	23.58	7.31	7.17	80.39	97.73	0.0031	0.2858	72.00	70.75
8:44:05	0.2897	1792.72	117	1982	424	24.43	6.81	6.82	63.00	98.04	0.0039	0.2897	79.71	70.75
8:44:23	0.2947	1792.97	118	1943	436	21.98	6.86	7.41	93.26	98.33	0.0050	0.2947	98.00	68.37
8:44:32	0.2972	1793.23	115	2156	416	21.02	9.79	7.95	94.03	98.68	0.0028	0.2972	140.00	70.14
8:44:50	0.3022	1793.47	118	1963	428	22.54	6.31	8.15	51.00	98.74	0.0050	0.3022	92.00	57.60

DOE high power motor test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. #	Date: 12/17/88													
Starting Depth =	1781	Bit Type =	Walker McDevanast MP88H	Average ROP Excluding Stops										
Ending Depth =	1916	Bit Size =	4.75											
Total Depth Drilled	135	Bit Nozzles =	8, 9, 12, 12	Depth Drilled =	135.33									
Hours On Bit =	2.89	Mud Type =	Water Based	Hours On Bit =	2.89									
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.76	Average ROP =	48.34									
Drilling (ft) =	1789.66	Pipe (ft) =	1043.06	Collar (ft)	740.61									

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
8:45:02	0.3056	1793.72	119	2052	423	22.26	8.59	8.41	77.63	99.02	0.0033	0.3056	84.00	66.69
8:45:14	0.3089	1793.98	118	2023	430	22.77	8.09	8.72	70.97	98.28	0.0033	0.3089	70.00	67.54
8:45:26	0.3125	1794.23	117	1969	427	23.11	7.77	8.51	64.77	98.54	0.0039	0.3125	68.88	67.54
8:45:40	0.3161	1794.48	117	2064	426	23.82	7.86	8.12	76.99	98.79	0.0033	0.3161	72.00	68.10
8:45:54	0.3209	1794.73	119	2089	431	22.42	8.82	8.22	66.95	100.01	0.0039	0.3209	68.14	66.44
8:46:08	0.3233	1794.98	118	2015	428	22.50	8.86	8.28	73.51	100.29	0.0033	0.3233	81.00	67.24
8:46:19	0.3267	1795.23	118	2164	429	22.81	8.84	8.43	76.97	100.51	0.0033	0.3267	69.00	70.75
8:46:30	0.3300	1795.49	119	1952	434	23.91	7.52	8.38	74.77	100.76	0.0033	0.3300	75.00	68.25
8:46:43	0.3336	1795.74	119	1981	433	24.07	7.39	8.29	69.60	101.03	0.0036	0.3336	80.31	72.32
8:46:52	0.3361	1795.99	119	2062	432	24.78	6.73	7.87	101.04	101.32	0.0025	0.3361	108.00	74.29
8:47:04	0.3394	1796.24	117	2063	426	25.06	6.46	7.98	74.67	101.61	0.0033	0.3394	67.00	73.86
8:47:14	0.3460	1796.49	118	1793	428	26.68	4.90	8.69	46.34	101.89	0.0098	0.3460	61.26	70.14
8:47:45	0.3494	1796.74	117	1922	424	24.71	5.76	8.45	59.38	102	0.0044	0.3494	31.75	67.80
8:47:50	0.3623	1797.00	117	2152	428	22.46	8.96	8.76	87.64	102.28	0.0028	0.3623	100.00	70.49
8:48:01	0.3653	1797.25	117	2168	424	22.84	8.85	7.19	78.65	102.64	0.0031	0.3653	85.09	71.06
8:48:11	0.3683	1797.50	120	2134	435	23.33	8.11	7.52	96.44	102.6	0.0028	0.3681	98.00	72.32
8:48:22	0.3611	1797.75	119	2126	426	23.24	8.30	6.16	89.04	103.65	0.0031	0.3611	81.69	72.64
8:48:35	0.3650	1798.00	118	2044	430	23.20	8.28	8.47	84.66	103.92	0.0039	0.3650	69.43	72.06
8:49:01	0.3719	1798.26	117	2227	424	22.37	8.98	8.48	36.73	103.83	0.0069	0.3719	36.24	63.35
8:49:13	0.3753	1798.51	119	2027	431	22.19	9.18	8.55	76.85	103.84	0.0033	0.3753	93.00	63.35
8:49:36	0.3786	1798.76	118	2050	430	24.01	7.44	8.41	82.42	104.11	0.0033	0.3786	81.00	67.54
8:49:40	0.3828	1799.01	118	1998	428	24.16	7.31	8.23	59.19	104.29	0.0042	0.3828	43.20	66.10
8:49:52	0.3861	1799.26	121	2056	436	23.53	8.44	8.27	72.02	104.54	0.0033	0.3861	75.00	66.60
8:50:07	0.3909	1799.52	119	1981	433	23.93	7.99	7.89	61.68	104.76	0.0042	0.3903	67.60	64.86
8:50:19	0.3936	1799.77	118	2096	429	23.91	7.69	7.47	77.46	105.05	0.0033	0.3936	81.00	63.84
8:50:29	0.3964	1800.02	120	2081	435	24.68	6.27	7.24	86.26	105.27	0.0028	0.3964	79.20	64.35
8:50:42	0.4000	1800.27	118	2036	430	24.58	6.36	7.05	71.11	105.58	0.0036	0.4000	66.31	64.86
8:50:58	0.4044	1800.53	120	1934	436	24.46	6.47	8.88	95.79	105.8	0.0044	0.4044	64.00	69.54
8:51:14	0.4089	1800.77	121	1998	438	22.62	8.23	8.88	58.19	106.98	0.0044	0.4089	58.50	67.24
8:51:23	0.4114	1801.02	118	2634	431	24.72	6.23	6.71	102.49	108.31	0.0025	0.4114	108.00	68.96

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 13/17/98														
Starting Depth =	1781	Bit Type =	Walker McDonald MP68H				Average ROP Excluding Staps								
Ending Depth =	1919	Bit Size =	4.75												
Total Depth Drilled	139	Bit Nozzles =	9, 9, 12, 12				Depth Drilled =	135.33							
Hours On Bit =	2.80	Mud Type =	Water Based				Hours On Bit =	2.80							
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70				Average ROP	48.34							
Drilling (ft) =	1789.66	Pipe (ft) =	1041.05	Collar (ft)	740.61										

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOR (Kips)	Average WOR (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
8:51:41	0.4164	1801.26	116	1803	423	23.56	8.39	7.11	49.37	108.53	0.0050	0.4164	49.00	67.54
8:51:51	0.4192	1801.53	117	2174	426	20.82	9.36	7.83	92.50	106.81	0.0028	0.4192	100.80	68.67
8:52:06	0.4233	1801.78	118	2038	432	21.68	9.13	8.37	81.37	107.07	0.0042	0.4233	82.40	68.37
8:52:14	0.4269	1802.03	118	2158	428	19.16	11.61	9.84	194.17	107.33	0.0022	0.4269	117.00	70.75
8:52:28	0.4289	1802.28	119	2065	432	20.03	10.74	9.95	75.58	107.62	0.0033	0.4289	87.00	69.64
8:52:37	0.4319	1802.53	118	2024	439	23.84	7.25	9.74	84.09	107.81	0.0031	0.4319	62.18	70.75
8:52:50	0.4356	1802.79	119	2043	432	23.63	7.37	9.20	72.83	108.06	0.0036	0.4356	89.23	72.64
8:53:04	0.4394	1803.03	120	1976	435	22.58	8.28	9.63	64.45	108.32	0.0039	0.4394	66.95	73.96
8:53:14	0.4422	1803.28	117	2321	426	20.70	10.06	8.72	86.44	108.55	0.0028	0.4422	69.90	73.63
8:53:26	0.4453	1803.54	118	2151	429	22.70	8.17	8.21	83.72	108.8	0.0031	0.4453	81.32	78.23
8:53:38	0.4483	1803.79	118	2058	438	24.21	8.70	8.10	81.40	109.07	0.0031	0.4483	58.38	77.49
8:53:49	0.4519	1804.04	119	2049	434	22.60	8.38	8.30	72.17	109.32	0.0036	0.4519	69.29	78.99
8:53:58	0.4544	1804.29	117	2178	426	22.77	8.09	8.26	95.24	109.6	0.0025	0.4544	112.00	75.29
8:54:13	0.4586	1804.54	119	2003	434	21.37	9.43	8.13	60.85	109.81	0.0042	0.4586	56.40	76.04
8:54:27	0.4628	1804.79	119	2110	431	19.73	12.54	9.05	84.86	110.06	0.0039	0.4625	84.29	73.96
8:54:42	0.4667	1805.05	118	2132	428	18.83	11.87	13.84	81.89	110.33	0.0042	0.4667	64.80	72.96
8:54:50	0.4699	1805.30	119	2196	434	19.11	11.60	10.71	107.12	110.61	0.0022	0.4686	126.00	77.09
8:55:02	0.4722	1805.56	118	2189	428	22.01	8.83	10.86	77.93	110.83	0.0033	0.4722	60.50	75.33
8:55:15	0.4758	1805.80	118	2045	430	23.01	7.85	10.54	70.69	111.06	0.0039	0.4758	77.54	71.96
8:55:29	0.4794	1806.05	118	2092	428	22.97	7.99	9.81	69.53	111.36	0.0039	0.4794	74.77	72.64
8:55:39	0.4822	1806.30	118	2189	437	21.99	8.93	9.92	88.61	111.59	0.0028	0.4822	82.80	74.64
8:55:50	0.4858	1806.56	118	2052	423	23.61	7.10	8.12	73.36	111.86	0.0033	0.4858	91.00	72.96
8:56:07	0.4903	1806.81	120	1960	435	22.62	8.23	8.00	54.41	112.1	0.0047	0.4903	50.62	71.68
8:56:32	0.4972	1807.06	119	2145	429	23.26	7.62	7.98	36.82	112.38	0.0069	0.4972	33.12	65.36
8:56:48	0.5017	1807.31	121	1920	439	24.02	6.89	7.76	58.52	112.6	0.0044	0.5017	60.75	64.67
8:57:02	0.5056	1807.56	119	2036	432	22.51	8.35	7.84	63.48	112.84	0.0059	0.5056	61.71	61.64
8:57:10	0.5078	1807.81	118	2141	426	20.42	10.39	8.29	109.89	113.09	0.0022	0.5078	112.80	63.56
8:57:23	0.5114	1808.06	119	2144	433	20.73	10.85	8.65	68.34	113.36	0.0039	0.5114	72.00	63.56
8:57:36	0.5150	1808.32	119	2202	433	21.30	8.50	9.03	72.97	113.56	0.0036	0.5150	66.46	63.84
8:57:46	0.5178	1808.57	123	2155	445	21.56	9.25	9.50	85.45	113.87	0.0028	0.5178	109.80	63.64

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 5	Date: 12/17/88													
Starting Depth =	1781	Bit Type =	Walker McCosmas MP28H	Average ROP Excluding Stops										
Ending Depth =	1916	Bit Size =	4.75											
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12	Depth Drilled =	135.33									
Hours On Bit =	2.80	Mud Type =	Water Based	Hours On Bit =	2.80									
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70	Average ROP	48.34									
Drillstring (ft) =	1785.66	Pipe (ft) =	1041.05	Collar (ft)	740.61									

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
8:58:00	0.5217	1808.82	122	2014	442	21.56	9.23	9.67	65.58	114.1	0.0038	0.5217	59.14	62.53
8:58:10	0.5243	1809.87	118	2235	429	20.37	10.40	9.88	64.88	114.35	0.0028	0.5244	90.00	68.15
8:58:24	0.5275	1809.32	118	2098	430	20.84	9.95	9.88	78.60	114.59	0.0031	0.5275	78.55	74.64
8:58:38	0.5317	1809.67	119	2094	431	21.28	9.93	9.88	60.18	114.82	0.0042	0.5317	59.20	75.83
8:58:47	0.5347	1809.82	118	2312	433	20.91	10.19	9.86	68.14	115.05	0.0031	0.5347	65.08	77.49
8:58:57	0.5375	1810.97	119	2144	432	21.97	8.86	9.79	66.92	115.38	0.0026	0.5375	100.80	78.04
8:59:12	0.5417	1810.32	119	2068	431	19.99	10.78	9.86	60.62	115.99	0.0042	0.5417	55.30	74.54
8:59:28	0.5483	1810.57	119	1889	434	22.91	7.96	9.47	38.55	115.85	0.0067	0.5483	38.09	67.90
8:59:48	0.5511	1810.82	120	2074	435	22.43	8.42	9.23	83.60	116.11	0.0028	0.5511	93.60	87.50
8:59:58	0.5544	1811.08	119	2161	431	21.80	8.01	9.00	76.06	116.35	0.0033	0.5544	72.00	88.98
9:00:07	0.5588	1811.33	119	2161	432	22.26	8.88	9.00	161.81	116.63	0.0025	0.5588	112.00	69.54
9:00:21	0.5608	1811.58	118	2038	435	23.04	8.32	8.92	65.88	116.85	0.0039	0.5608	58.57	87.80
9:00:32	0.5639	1811.83	120	2188	436	22.28	8.87	8.70	82.69	117.12	0.0031	0.5639	88.78	70.14
9:00:46	0.5661	1812.08	118	2176	427	22.92	7.96	8.81	134.75	117.35	0.0022	0.5661	103.50	72.00
9:01:00	0.5717	1812.33	118	1914	427	23.54	7.38	8.28	44.04	117.58	0.0056	0.5717	41.40	68.15
9:01:12	0.5750	1812.58	118	2268	430	21.12	9.87	8.34	76.19	117.88	0.0033	0.5750	90.00	67.80
9:01:23	0.5781	1812.83	115	1998	420	23.40	7.86	8.51	61.39	118.17	0.0031	0.5781	94.91	76.04
9:01:40	0.5828	1813.08	120	2058	437	21.90	8.27	8.41	51.69	118.38	0.0047	0.5828	48.24	71.37
9:01:50	0.5886	1813.33	118	3032	430	23.44	7.87	8.39	97.20	118.68	0.0028	0.5886	115.20	72.32
9:02:01	0.5888	1813.59	119	2140	433	23.14	8.18	8.56	79.28	118.9	0.0031	0.5888	73.00	71.37
9:02:14	0.5922	1813.84	120	2532	436	24.66	6.77	7.98	72.94	119.1	0.0036	0.5922	59.33	72.00
9:02:21	0.5942	1814.09	118	2177	428	34.23	7.14	7.87	130.61	119.38	0.0019	0.5942	144.00	74.64
9:02:36	0.5983	1814.34	117	1981	426	22.84	8.40	7.67	62.11	119.6	0.0042	0.5983	52.80	70.14
9:02:43	0.6003	1814.59	117	2385	428	21.41	9.73	8.04	118.11	119.88	0.0019	0.6003	148.14	78.60
9:02:55	0.6036	1814.84	118	2138	434	22.29	8.74	8.16	81.60	120.15	0.0033	0.6036	78.00	79.96
9:03:08	0.6072	1815.09	117	3080	425	23.64	7.26	8.25	65.73	120.17	0.0036	0.6072	60.90	77.49
9:03:18	0.6094	1815.34	118	2145	425	21.17	9.83	8.75	113.89	120.62	0.0023	0.6094	112.80	84.75
9:03:27	0.6125	1815.60	118	2283	420	21.28	9.53	8.98	81.78	120.91	0.0031	0.6125	94.91	84.28
9:03:45	0.6186	1815.85	119	1937	412	24.06	8.85	8.40	41.74	121.13	0.0061	0.6186	38.00	75.03
9:03:59	0.6214	1816.10	117	2351	427	20.17	18.50	8.77	82.31	121.38	0.0038	0.6214	80.80	77.49

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 5	Date: 12/17/86														
Starting Depth =	1781	Bit Type =	Walker McDoanald MP88H	Average ROP Excluding Stops											
Ending Depth =	1816	Bit Size =	4.75												
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12	Depth Drilled =	135.33										
Hours On Bit =	2.80	Mud Type =	Water Based	Hours On Bit =	2.80										
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70	Average ROP	48.34										
Grubstring (ft) =	1789.62	Pipe (ft) =	1941.05	Collar (ft)	748.61										

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Klps)	WOB (Klps)	Average WOB (Klps)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
9:04:11	0.6237	1815.35	120	2148	438	21.95	8.89	9.10	73.05	121.83	0.0033	0.6247	75.00	75.96
9:04:23	0.6281	1815.60	121	2187	441	19.81	10.85	9.33	74.23	121.9	0.0033	0.6281	81.00	76.04
9:04:36	0.6314	1815.85	123	2166	437	20.50	9.89	9.42	75.26	122.12	0.0033	0.6314	86.00	72.64
9:04:48	0.6342	1817.10	119	2179	433	23.71	7.20	9.49	89.47	122.37	0.0038	0.6342	80.00	73.95
9:05:01	0.6386	1817.35	118	1977	428	23.11	7.79	9.52	88.28	122.65	0.0044	0.6386	83.50	72.60
9:05:12	0.6417	1817.61	117	2267	427	20.72	10.07	9.19	84.81	122.97	0.0031	0.6417	104.73	70.45
9:05:23	0.6447	1817.86	118	2140	428	22.40	9.45	8.68	78.32	123.12	0.0031	0.6447	49.00	70.14
9:05:36	0.6489	1818.11	113	2770	413	20.37	10.41	8.73	62.63	123.41	0.0042	0.6489	69.60	74.64
9:06:08	0.6572	1818.36	118	1815	430	25.41	4.61	9.26	20.46	123.65	0.0083	0.6572	28.80	60.64
9:06:23	0.6614	1818.53	120	1957	417	25.62	8.24	8.26	60.66	123.85	0.0042	0.6614	48.00	66.45
9:06:36	0.6647	1818.78	118	2130	429	19.34	11.38	8.62	72.97	124.05	0.0033	0.6647	60.00	59.45
9:06:48	0.6678	1819.03	116	2175	424	19.29	11.44	9.22	86.84	124.29	0.0031	0.6678	75.55	69.91
9:07:00	0.6717	1819.28	118	2028	429	21.33	9.48	9.03	66.17	124.53	0.0039	0.6717	66.89	58.13
9:07:13	0.6753	1819.54	120	2082	417	21.88	9.13	8.83	71.36	124.83	0.0038	0.6753	105.23	59.73
9:07:26	0.6789	1819.79	121	1997	439	22.39	8.47	9.88	77.05	125.07	0.0033	0.6789	42.00	59.61
9:07:46	0.6844	1820.04	119	1503	432	22.15	8.70	9.34	42.98	125.31	0.0068	0.6844	41.14	64.89
9:07:55	0.6869	1820.31	116	1813	424	25.14	6.84	8.36	103.19	125.41	0.0036	0.6869	440.00	67.81
9:19:13	0.6889	1820.57	109	1269	396	31.43	0.10		7.83	125.49	0.0000	0.6889	0.00	
9:19:23	0.6894	1821.12	110	1379	399	31.03	0.46		105.66	126.49	0.0025	0.6894	0.00	
9:19:32	0.6922	1821.37	113	1272	403	31.09	0.40		91.85	126.83	0.0029	0.6922	59.40	
9:19:49	0.6953	1821.82	114	1265	413	31.17	0.34		79.39	126.89	0.0031	0.6953	85.00	
9:20:13	0.7039	1821.79	111	1467	408	27.32	4.09	1.97	19.91	127.05	0.0003	0.7039	19.20	
9:20:37	0.7103	1822.04	110	1762	402	22.20	8.06	3.64	37.59	127.37	0.0067	0.7103	48.00	
9:20:59	0.7147	1822.39	109	1826	399	22.63	9.11	4.57	68.68	127.56	0.0044	0.7147	42.75	
9:21:06	0.7181	1822.54	112	1963	419	22.24	8.91	6.27	78.55	127.8	0.0033	0.7181	72.00	
9:21:15	0.7208	1822.79	111	2013	404	21.81	9.32	6.07	86.99	128.13	0.0028	0.7208	116.80	
9:21:29	0.7247	1823.04	111	1837	405	23.62	7.89	6.78	63.81	128.33	0.0039	0.7247	61.43	57.44
9:21:42	0.7283	1823.29	111	1941	404	23.29	7.80	6.57	70.38	128.58	0.0036	0.7283	69.33	65.80
9:21:53	0.7314	1823.55	108	1915	398	23.85	7.75	6.29	84.46	128.83	0.0031	0.7314	81.83	55.66

DOE high power motor test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 8	Date: 10/17/98																				
Starting Depth =	1761					Bit Type =	Walker McQuinn WP68H													Average ROP Excluding Steps	
Ending Depth =	1919					Bit Size =	8.75														
Total Depth Drilled	135					Bit Nozzles =	9, 9, 12, 12													Depth Drilled =	135.33
Hours On Bit =	2.80					Mud Type =	Water Based													Hours On Bit =	2.80
Average ROP =	48.34					Mud Weight (lb/gal) =	8.70													Average ROP	48.34
Drilling (%) =	1789.86					Pipe (ft) =	1041.05		Collar (ft)	740.51											

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
9:22:42	0.7387	1823.80	109	1790	397	23.54	7.67	8.05	47.69	129.06	0.0053	0.7387	43.59	52.67
9:22:52	0.7394	1824.07	113	1850	411	22.91	8.19	7.82	52.91	129.93	0.0026	0.7394	319.56	63.63
9:23:53	0.7481	1824.56	113	1907	411	22.22	7.68	7.94	-6.12	129.98	0.0086	0.7481	5.01	68.44
9:23:04	0.7511	1824.90	113	1812	410	25.03	5.37	7.33	82.90	130.07	0.0031	0.7511	28.48	68.98
9:23:20	0.7556	1825.56	111	1885	408	23.98	8.89	7.40	89.07	130.33	0.0044	0.7556	69.50	67.20
9:23:35	0.7597	1826.31	110	1860	402	23.91	7.31	7.38	58.57	130.59	0.0042	0.7597	62.90	64.80
9:23:52	0.7644	1826.56	110	1910	408	24.06	7.36	7.12	55.37	130.83	0.0047	0.7644	56.82	63.44
9:24:08	0.7681	1826.51	112	1772	408	26.13	5.18	6.92	68.71	131.08	0.0036	0.7681	69.23	63.44
9:24:20	0.7722	1826.07	110	1818	403	24.50	6.17	6.82	59.94	131.54	0.0042	0.7722	62.90	61.71
9:24:38	0.7772	1826.32	114	1814	416	26.11	6.16	6.43	49.58	131.58	0.0059	0.7772	48.00	62.14
9:24:50	0.7808	1826.57	113	1968	403	24.19	7.06	6.36	70.14	131.84	0.0032	0.7808	78.00	60.81
9:25:07	0.7853	1826.83	111	1848	404	24.07	7.16	6.36	54.39	132.11	0.0047	0.7853	57.18	60.99
9:25:26	0.7908	1827.07	113	1869	411	20.65	10.43	7.44	48.49	132.36	0.0053	0.7908	47.37	67.55
9:25:38	0.7939	1827.32	113	2436	410	19.57	11.48	8.46	70.48	132.6	0.0033	0.7939	72.00	68.85
9:26:06	0.8022	1827.42	114	1567	414	26.76	4.50	8.14	11.21	132.76	0.0093	0.8022	21.60	49.65
9:26:25	0.8069	1827.67	111	1762	406	21.82	9.31	6.59	56.90	132.94	0.0047	0.8069	33.86	49.66
9:26:40	0.8111	1827.82	113	1937	403	22.00	9.15	6.99	57.26	133.2	0.0042	0.8111	62.40	49.61
9:26:54	0.8156	1828.17	112	1902	408	23.25	7.94	6.49	64.98	133.46	0.0039	0.8156	64.29	49.00
9:27:11	0.8197	1828.43	111	1829	404	23.13	6.06	7.91	54.80	133.71	0.0047	0.8197	56.86	49.85
9:27:24	0.8233	1828.68	113	2017	410	21.21	9.90	6.87	66.12	133.95	0.0036	0.8233	69.48	49.32
9:27:41	0.8281	1828.93	114	1819	416	23.50	7.32	6.47	66.35	134.19	0.0047	0.8281	80.82	49.32
9:27:55	0.8319	1829.18	112	1821	408	23.47	7.72	6.19	61.94	134.5	0.0035	0.8319	79.71	50.68
9:28:14	0.8372	1829.43	111	1908	406	21.26	9.83	6.57	47.50	134.7	0.0053	0.8372	37.80	48.69
9:28:31	0.8419	1829.69	113	1718	406	23.87	7.16	6.42	62.86	134.93	0.0047	0.8419	49.71	56.00
9:28:50	0.8472	1829.93	113	1852	410	23.15	8.05	8.05	49.80	135.21	0.0058	0.8472	53.05	56.11
9:29:06	0.8517	1830.18	112	1904	408	20.99	8.21	8.23	60.00	135.45	0.0044	0.8517	54.00	55.73
9:29:22	0.8581	1830.44	113	1961	410	22.71	8.43	8.37	64.96	135.74	0.0044	0.8581	65.25	65.22
9:29:40	0.8611	1830.69	113	1849	410	23.35	7.84	7.88	49.98	136.02	0.0050	0.8611	58.00	54.80
9:29:58	0.8656	1830.94	115	1845	417	23.18	8.01	8.11	59.30	136.22	0.0044	0.8656	45.00	53.53
9:30:12	0.8700	1831.19	112	1908	408	23.49	7.72	8.04	59.33	136.49	0.0044	0.8700	66.75	53.80

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/88													
Starting Depth =	1781	Bit Type =	Walker McClean's 40PMSH	Average ROP Excluding Stops										
Ending Depth =	1818	Bit Size =	4.75											
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12	Depth Drilled =	135.33									
Hours On Bit =	2.89	Mud Type =	Water Based	Hours On Bit =	2.89									
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70	Average ROP	48.34									
Drilling (R) =	1789.88	Pipe (ft) =	1041.65	Color (R)	745.81									

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psf)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
9:30:39	0.8750	1831.44	114	1827	414	24.16	7.98	7.83	50.53	138.77	0.0050	0.8780	56.00	52.49
9:30:50	0.8806	1831.69	113	1899	412	21.90	7.34	7.89	44.54	138.87	0.0056	0.8806	56.00	52.18
9:31:05	0.8847	1831.96	115	1742	419	25.94	4.41	8.81	61.88	137.21	0.0042	0.8847	57.50	53.08
9:31:25	0.8903	1832.20	116	1764	417	25.50	5.90	9.47	43.23	137.39	0.0056	0.8903	52.40	52.72
9:31:43	0.8958	1832.45	112	1831	408	24.74	6.52	6.23	52.45	137.72	0.0060	0.8958	56.00	52.66
9:31:57	0.8992	1832.70	114	1913	414	24.30	6.86	6.18	63.22	137.98	0.0059	0.8992	61.71	52.48
9:32:18	0.9044	1832.95	113	1831	412	24.95	6.32	5.98	47.45	138.29	0.0053	0.9044	53.35	52.15
9:32:31	0.9086	1833.20	112	1932	409	22.67	6.51	6.80	59.91	138.46	0.0042	0.9086	52.50	52.46
9:32:48	0.9133	1833.45	113	1867	410	24.30	7.21	7.08	53.49	138.78	0.0047	0.9133	67.78	52.19
9:33:06	0.9189	1833.70	114	1888	415	23.81	7.61	7.30	50.80	139.01	0.0050	0.9189	48.00	52.15
9:33:27	0.9242	1833.95	116	1852	422	22.24	8.91	7.71	43.20	139.25	0.0058	0.9242	41.14	51.82
9:33:45	0.9289	1834.21	116	1864	423	20.99	10.11	8.47	69.79	139.52	0.0050	0.9289	54.00	50.89
9:34:06	0.9359	1834.48	116	1918	423	22.28	10.80	8.93	34.17	139.84	0.0068	0.9359	54.86	50.93
9:34:28	0.9389	1834.71	116	1876	421	22.15	9.01	9.20	61.33	140.07	0.0058	0.9389	59.14	51.82
9:34:41	0.9447	1834.96	113	1874	411	22.48	6.67	9.50	44.32	140.23	0.0058	0.9447	27.43	49.61
9:34:58	0.9489	1835.21	112	1810	409	23.35	7.37	9.19	65.29	140.54	0.0039	0.9486	79.71	51.17
9:35:17	0.9547	1835.46	115	1850	417	20.40	10.68	9.21	30.14	140.73	0.0061	0.9547	31.09	49.01
9:35:37	0.9603	1835.71	117	1879	427	20.39	10.69	9.26	44.60	140.96	0.0059	0.9603	45.00	48.14
9:35:53	0.9647	1835.97	115	1954	417	20.17	10.80	9.66	58.74	141.22	0.0044	0.9647	54.00	48.93
9:36:10	0.9694	1836.22	117	1887	425	22.16	9.09	9.73	51.87	141.48	0.0047	0.9694	55.05	50.19
9:36:39	0.9750	1836.47	116	1802	422	22.78	8.41	9.94	46.05	141.75	0.0056	0.9750	48.50	49.31
9:36:58	0.9802	1836.72	112	1872	407	20.92	10.19	9.64	34.08	141.98	0.0072	0.9822	31.85	47.86
9:37:14	0.9872	1836.98	118	2025	420	21.00	16.12	9.72	52.67	142.28	0.0060	0.9872	56.00	48.07
9:37:33	0.9925	1837.23	113	1784	412	25.12	6.17	6.78	47.40	142.52	0.0063	0.9925	49.26	47.91
9:37:51	0.9975	1837.48	113	1573	410	22.18	9.00	8.76	49.10	142.71	0.0058	0.9975	50.00	46.43
9:38:08	1.0025	1837.73	115	1887	417	22.75	8.43	8.76	61.30	143.03	0.0060	1.0025	52.00	47.51
9:38:33	1.0092	1837.98	115	1873	420	21.90	9.25	9.59	37.48	143.25	0.0067	1.0092	37.50	46.43
9:38:53	1.0175	1838.14	116	1579	421	25.86	8.46	7.96	19.00	143.44	0.0083	1.0175	19.20	41.12
9:39:25	1.0236	1838.39	115	1840	418	21.94	9.21	8.27	42.94	143.68	0.0061	1.0236	39.27	40.66
9:39:43	1.0288	1838.64	117	1814	425	23.65	7.58	7.98	49.68	143.91	0.0059	1.0286	46.00	40.48

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/88													
Starting Depth =	1781	Bit Type =	Walker McDonnell MP38H										Average ROP Excluding Steps	
Ending Depth =	1918	Bit Size =	4.75											
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12										Depth Drilled =	135.33
Hours On Bit =	2.89	Mud Type =	Water Based										Hours On Bit =	2.89
Average ROP =	48.34	Mud Weight (lb/gal) =	8.70										Average ROP =	48.34
Drilling (ft) =	1789.66	Pipe (ft) =	1941.65	Collar (ft)	740.81									

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
9:40:02	1:03:39	1830.89	118	1850	428	23.74	7.48	7.79	47.57	144.15	0.0053	1:03:39	45.47	42.03
9:40:15	1:03:79	1839.18	118	1858	429	23.75	7.47	7.44	71.55	144.48	0.0036	1:03:79	91.38	43.18
9:40:43	1:04:53	1839.40	117	1897	424	25.22	8.97	7.58	32.37	144.88	0.0078	1:04:53	25.71	41.12
9:41:02	1:05:08	1839.85	114	1870	415	23.15	8.88	7.33	45.89	144.95	0.0053	1:05:08	51.16	40.90
9:41:24	1:05:67	1839.30	113	1809	418	24.01	7.24	7.25	41.58	145.19	0.0061	1:05:67	37.84	40.08
9:41:38	1:05:09	1840.19	117	1894	428	23.82	7.60	7.29	68.08	145.47	0.0039	1:05:06	74.87	42.23
9:41:54	1:05:50	1849.41	114	1888	415	24.51	8.75	7.14	58.34	145.87	0.0044	1:05:50	45.88	47.79
9:42:15	1:07:08	1840.85	116	1854	421	22.58	8.52	7.83	42.39	146.09	0.0058	1:07:08	46.71	45.07
9:42:32	1:07:55	1840.91	115	1958	419	23.88	10.23	8.97	35.18	146.18	0.0047	1:07:56	48.59	46.38
9:42:51	1:08:08	1841.78	117	1937	425	22.73	8.41	8.30	46.31	146.44	0.0053	1:08:08	49.26	48.38
9:43:11	1:08:54	1841.51	117	1814	423	25.08	8.28	8.02	48.81	146.68	0.0056	1:08:54	43.30	46.20
9:43:27	1:08:58	1841.86	118	1900	429	22.41	8.78	8.42	58.35	146.85	0.0044	1:08:58	83.00	49.81
9:43:48	1:09:07	1841.91	114	1809	415	23.58	7.73	8.27	43.33	147.2	0.0068	1:09:07	41.14	49.01
9:44:18	1:10:50	1842.11	118	1865	433	26.05	8.22	7.46	34.29	147.42	0.0083	1:10:50	26.40	46.72
9:44:42	1:1117	1842.36	118	1824	427	21.81	9.52	7.89	37.39	147.64	0.0087	1:1117	33.00	43.24
9:44:59	1:1154	1842.62	115	1902	420	23.21	10.76	8.60	53.38	147.88	0.0047	1:1154	58.82	43.01
9:45:17	1:13:14	1842.87	115	1904	419	22.42	8.75	8.90	50.18	148.14	0.0050	1:13:14	59.50	43.71
9:45:36	1:1267	1843.12	118	1878	429	21.44	9.79	8.99	48.55	148.46	0.0053	1:1267	80.93	43.24
9:45:51	1:1308	1843.37	116	1957	421	22.58	8.59	9.45	61.88	148.63	0.0042	1:1308	48.80	44.20
9:46:10	1:1361	1843.82	117	1935	426	22.59	8.63	9.27	47.67	148.88	0.0053	1:1361	47.37	44.48
9:46:33	1:1397	1843.87	118	2017	421	24.21	7.04	8.52	58.72	149.14	0.0036	1:1397	72.58	45.26
9:46:42	1:1450	1844.12	117	1877	425	23.82	7.32	8.23	47.92	149.39	0.0053	1:1450	45.47	45.73
9:46:55	1:1486	1844.38	118	1908	428	23.73	7.50	7.80	57.57	149.72	0.0036	1:1486	122.46	52.05
9:47:15	1:1542	1844.83	117	1883	425	23.44	7.78	7.85	45.50	149.89	0.0058	1:1542	25.30	53.41
9:47:38	1:1600	1844.86	115	1878	418	22.78	8.40	7.81	44.57	150.19	0.0058	1:1600	51.43	51.82
9:47:54	1:1650	1845.12	118	1931	430	23.58	7.64	7.73	49.58	150.46	0.0060	1:1650	54.00	51.82
9:48:18	1:1684	1845.38	117	1944	425	22.58	8.62	7.89	58.25	150.67	0.0044	1:1684	47.28	52.83
9:48:31	1:1753	1845.53	120	1987	437	23.17	8.03	8.09	43.98	150.9	0.0058	1:1753	39.43	50.85
9:48:49	1:1803	1845.89	120	1988	438	23.24	7.86	8.13	48.81	151.30	0.0050	1:1803	88.09	51.40
9:49:01	1:1836	1846.14	118	1974	431	23.33	7.88	8.03	74.78	151.43	0.0032	1:1836	87.06	51.72

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/96													
Starting Depth =	1781	Bit Type =	Walker McDonald MP58H	Average ROP Excluding Stags										
Ending Depth =	1916	Bit Size =	4.75											
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12	Depth Drilled =	135.33									
Hours On Bit =	2.80	Mud Type =	Water Based	Hours On Bit =	2.80									
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70	Average ROP	48.34									
Drilling (ft) =	1789.66	Pipe (ft) =	1041.98	Collar (ft)	746.61									

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Foot)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WDS (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
9:48:20	1:1917	1843.39	118	1773	430	25.04	6.25	7.75	31.34	151.66	0.0081	1:1917	22.34	48.04
9:48:46	1:1961	1843.54	117	1929	425	23.07	8.19	7.88	55.92	151.93	0.0044	1:1951	60.75	47.98
9:50:08	1:2017	1846.89	119	1833	431	23.38	7.63	7.83	45.95	152.17	0.0056	1:2017	43.20	47.58
9:50:33	1:2062	1847.14	118	1849	432	30.76	10.33	8.10	32.55	152.43	0.0075	1:2092	34.67	45.97
9:51:03	1:2175	1847.30	118	1876	423	26.87	4.39	7.49	18.58	152.64	0.0083	1:2175	25.20	41.33
9:51:21	1:2225	1847.55	117	1853	425	23.31	7.90	7.73	48.91	152.91	0.0060	1:2225	54.05	45.99
9:51:40	1:2278	1847.80	116	1923	422	23.42	7.90	7.89	49.30	153.08	0.0053	1:2278	32.21	41.33
9:52:03	1:2339	1848.05	120	1962	435	21.98	9.48	7.98	40.90	153.36	0.0061	1:2309	45.62	40.29
9:52:19	1:2368	1848.31	119	1845	431	24.19	7.06	7.53	51.95	153.59	0.0047	1:2368	48.71	35.45
9:53:46	1:2414	1848.51	117	1901	437	22.98	8.30	8.09	33.78	153.82	0.0079	1:2451	30.67	39.86
9:53:05	1:2514	1848.81	117	1901	425	22.81	8.35	8.18	47.03	154.09	0.0053	1:2514	51.18	38.26
9:53:29	1:2581	1849.16	119	1872	434	21.23	9.96	8.56	38.43	154.32	0.0087	1:2581	34.50	35.48
9:53:46	1:2628	1849.31	119	1984	434	22.69	9.07	8.51	55.02	154.63	0.0047	1:2628	65.65	40.46
9:53:59	1:2654	1849.57	118	2014	429	23.29	7.91	9.38	66.54	154.9	0.0035	1:2654	74.77	46.43
9:54:13	1:2703	1849.82	114	1908	416	23.85	8.80	8.38	64.17	155.09	0.0039	1:2703	48.86	47.51
9:54:34	1:2733	1850.07	117	2034	426	23.26	7.93	8.29	68.09	155.33	0.0031	1:2733	78.59	49.63
9:54:46	1:2794	1850.32	116	1917	424	24.49	8.78	7.65	41.28	155.63	0.0081	1:2794	49.09	40.83
9:55:02	1:2839	1850.57	118	1871	428	24.91	6.36	7.11	54.07	155.84	0.0044	1:2839	47.25	45.91
9:55:16	1:2876	1850.82	119	1858	417	24.06	7.22	8.97	64.27	156.1	0.0039	1:2876	66.86	54.24
9:55:33	1:2928	1851.08	117	1993	426	23.86	7.35	7.13	56.24	156.34	0.0047	1:2928	56.22	55.22
9:55:48	1:2987	1851.33	121	1946	439	24.38	8.87	8.91	58.78	156.62	0.0042	1:2987	57.20	58.79
9:56:17	1:3047	1851.58	118	2058	424	25.50	8.78	8.72	31.92	156.86	0.0081	1:3047	29.76	54.12
9:56:36	1:3100	1851.83	119	1907	403	24.74	6.53	8.78	47.15	157.11	0.0053	1:3100	47.37	61.62
9:56:54	1:3150	1852.08	118	1848	431	26.32	5.98	8.90	50.61	157.38	0.0050	1:3150	54.00	65.53
9:57:07	1:3189	1852.33	118	2073	422	24.04	7.20	8.47	67.01	157.61	0.0038	1:3189	63.69	49.91
9:57:23	1:3231	1852.58	115	1883	418	25.17	8.12	8.32	68.63	157.88	0.0044	1:3231	60.75	51.82
9:57:37	1:3269	1852.83	114	1833	415	25.48	5.82	8.33	65.23	158.21	0.0039	1:3269	64.66	65.48
10:08:28	1:3269	1853.03	110	1299	408	31.64	8.16		65.05	158.75	0.0060	1:3269	6.09	
10:08:46	1:3319	1853.28	113	1410	412	28.51	2.74		52.69	158.75	0.0053	1:3319	6.00	

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/88														
Starting Depth =	1781	Bit Type =	Walker McDonald MFS&H												Average ROP Excluding Steps
Ending Depth =	1915	Bit Size =	4.75												
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12											Depth Drilled =	135.33
Hours On Bit =	2.80	Mud Type =	Water Based											Hours On Bit =	2.80
Average ROP =	48.34	Mud Weight (lb/gal) =	8.78											Average ROP	48.34
Drilling (ft) =	1789.68	Pipe (ft) =	1041.05	Collar (ft)	748.61										

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
10:09:00	1.3358	1853.53	110	1824	401	25.08	6.70		64.72	158.82	0.0038	1.3358	18.00	
10:09:20	1.3418	1853.79	112	1819	409	25.28	6.88		45.19	159.08	0.0066	1.3414	43.23	
10:09:33	1.3459	1854.04	113	1803	413	25.17	6.53	4.51	65.67	159.32	0.0036	1.3459	72.00	
10:09:47	1.3489	1854.29	110	1895	401	24.69	7.08	5.90	65.15	159.58	0.0039	1.3489	61.71	
10:09:59	1.3519	1854.54	111	1884	394	25.90	5.71	6.49	81.44	159.81	0.0031	1.3519	81.82	
10:10:13	1.3561	1854.79	109	1795	398	25.32	6.42	6.24	59.42	160.05	0.0042	1.3561	57.80	
10:10:27	1.3600	1855.04	110	1881	400	24.24	7.45	6.54	68.28	160.32	0.0038	1.3600	88.43	
10:10:44	1.3647	1855.29	111	1836	405	24.18	7.50	6.23	51.60	160.6	0.0047	1.3647	59.29	59.29
10:11:14	1.3731	1855.43	113	1705	410	24.24	7.47	6.91	16.71	160.8	0.0083	1.3731	34.38	52.30
10:11:31	1.3778	1855.68	111	1699	406	24.24	7.39	7.23	53.23	160.86	0.0047	1.3778	33.38	61.26
10:12:01	1.3861	1855.93	112	1883	404	24.42	7.35	7.81	39.73	161.22	0.0063	1.3861	31.20	47.85
10:12:21	1.3917	1856.18	113	1752	409	24.34	6.64	7.29	44.90	161.48	0.0066	1.3917	43.80	45.86
10:12:32	1.3947	1856.44	112	1873	408	25.41	6.33	7.06	78.02	161.69	0.0031	1.3947	76.37	46.91
10:12:55	1.4014	1856.69	118	1712	418	24.78	7.02	6.97	57.94	161.99	0.0067	1.4014	45.00	43.88
10:13:15	1.4067	1856.94	112	1788	407	25.39	6.51	6.81	49.64	162.24	0.0053	1.4067	47.37	42.53
10:13:35	1.4122	1857.19	113	1759	408	25.05	6.75	6.69	44.85	162.48	0.0066	1.4122	39.50	41.17
10:13:54	1.4175	1857.45	115	1817	429	24.35	7.43	6.81	47.66	162.71	0.0083	1.4175	47.37	40.03
10:14:08	1.4209	1857.70	111	1743	405	25.00	6.77	6.90	79.74	163.02	0.0033	1.4208	93.00	47.81
10:14:32	1.4281	1857.95	113	1830	413	24.10	7.68	7.02	34.64	163.21	0.0072	1.4281	26.31	45.15
10:14:47	1.4322	1858.20	109	1847	380	24.56	7.22	7.16	68.91	163.47	0.0042	1.4322	62.40	45.23
10:15:07	1.4378	1858.45	115	1788	419	25.49	6.22	7.08	47.19	163.79	0.0058	1.4378	67.60	49.25
10:15:37	1.4449	1858.69	114	1862	415	25.17	6.52	6.88	29.45	163.96	0.0083	1.4449	22.50	43.76
10:16:09	1.4539	1858.94	114	1751	419	23.04	6.69	7.45	32.07	164.20	0.0078	1.4539	32.14	42.85
10:16:24	1.4592	1859.19	111	1774	416	23.17	6.88	7.64	47.29	164.48	0.0053	1.4592	47.37	42.86
10:16:42	1.4643	1859.44	112	1871	398	22.34	9.44	8.06	50.48	164.71	0.0050	1.4643	46.00	43.32
10:17:01	1.4694	1859.69	110	1910	403	23.07	8.73	6.59	45.11	164.96	0.0033	1.4694	47.37	43.12
10:17:18	1.4742	1859.94	114	1846	415	24.57	7.29	8.79	69.92	165.23	0.0047	1.4742	67.18	42.00
10:17:38	1.4800	1860.20	112	1790	408	25.23	6.51	8.10	43.37	165.54	0.0038	1.4800	53.14	43.32
10:18:01	1.4861	1860.45	114	1766	415	25.71	6.16	7.62	41.40	165.71	0.0061	1.4861	27.89	41.75
10:18:17	1.4906	1860.70	113	1797	432	25.21	6.96	7.06	69.25	166.03	0.0044	1.4906	72.00	42.63

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/98														
Starting Depth =	1781	Bit Type =	Walker McGovern MP65H	Average ROP Excluding Stops											
Ending Depth =	1916	Bit Size =	4.75												
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12	Depth Drilled =	135.33										
Hours On Bit =	2.80	Mud Type =	Water Based	Hours On Bit =	2.80										
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70	Average ROP	48.34										
Drilling (ft) =	1789.66	Pipe (ft) =	1041.05	Collar (ft)	746.61										

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psl)	Calculated Speed (rpm)	Hook Load (Klps)	WOB (Klps)	Average WOB (Klps)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
10:18:42	1:4975	1860.35	114	1781	414	25.51	6.31	6.68	36.71	166.26	0.0069	1.4975	33.12	43.98
10:18:56	1:5014	1861.21	112	1881	409	24.35	7.30	6.81	68.53	166.47	0.0039	1.5014	54.00	47.79
10:19:10	1:5053	1861.46	114	1809	414	25.70	6.10	6.54	51.75	166.73	0.0039	1.5053	84.25	39.23
10:19:34	1:5119	1861.71	114	1793	413	25.92	6.66	6.56	37.42	166.97	0.0097	1.5119	37.50	37.51
10:19:46	1:5153	1861.26	116	1845	421	24.92	6.91	6.59	76.84	167.25	0.0033	1.5153	84.00	49.53
10:20:00	1:5192	1862.21	116	1833	421	25.80	6.05	6.49	68.55	167.5	0.0039	1.5192	64.25	50.44
10:20:30	1:5275	1862.46	113	1735	410	26.17	5.68	6.15	30.14	167.75	0.0083	1.5275	30.00	47.56
10:20:47	1:5322	1862.71	114	1624	414	25.34	6.48	6.22	51.27	168.01	0.0047	1.5322	95.06	49.01
10:21:06	1:5375	1862.97	113	1631	413	25.04	6.77	6.36	49.82	168.22	0.0053	1.5375	39.75	48.36
10:21:22	1:5419	1863.22	113	1788	411	26.61	5.83	6.18	58.11	168.48	0.0034	1.5419	69.75	51.87
10:21:42	1:5478	1863.48	115	1868	418	25.44	6.36	6.23	46.48	168.73	0.0056	1.5478	41.25	49.23
10:22:01	1:5528	1863.73	118	1855	428	25.70	6.14	6.32	46.88	168.99	0.0033	1.5528	49.25	47.79
10:22:23	1:5586	1863.98	117	1764	426	26.40	5.48	6.12	44.30	169.26	0.0058	1.5586	51.43	48.64
10:22:47	1:5658	1864.27	117	1736	436	26.17	5.66	5.90	41.43	169.5	0.0069	1.5658	30.24	35.94
10:23:17	1:5739	1864.45	119	1793	431	24.85	6.61	6.10	15.83	169.74	0.0093	1.5739	28.80	40.62
10:23:33	1:5783	1864.65	115	1678	416	23.85	6.73	6.58	56.96	169.95	0.0044	1.5783	47.25	49.08
10:23:49	1:5828	1864.81	113	1847	410	22.43	9.14	7.19	67.96	170.23	0.0044	1.5828	61.00	43.52
10:24:14	1:5887	1865.16	117	1820	426	24.74	6.04	7.47	35.27	170.43	0.0069	1.5887	37.36	41.64
10:24:38	1:5954	1865.41	116	1774	424	24.94	6.74	7.88	38.93	170.67	0.0067	1.5954	37.50	40.23
10:24:56	1:6011	1865.66	118	1915	426	23.43	6.14	7.95	52.44	170.92	0.0047	1.6011	52.94	40.60
10:25:17	1:6072	1865.91	117	1788	427	25.29	6.44	7.48	39.93	171.22	0.0061	1.6072	48.00	46.64
10:25:47	1:6156	1866.11	116	1709	428	25.39	6.42	6.94	34.40	171.42	0.0083	1.6156	36.30	37.40
10:26:06	1:6208	1866.37	115	1859	429	26.98	10.65	7.69	47.92	171.64	0.0083	1.6208	49.25	37.95
10:26:28	1:6269	1866.62	118	1806	430	24.53	7.20	7.77	42.68	171.86	0.0061	1.6269	39.75	41.64
10:26:57	1:6350	1866.97	116	1733	421	24.91	6.89	7.52	31.68	172.16	0.0061	1.6350	34.75	39.18
10:27:22	1:6419	1867.12	116	1834	423	20.73	10.84	8.40	38.07	172.36	0.0069	1.6419	31.68	37.36
10:27:45	1:6483	1867.36	117	1789	427	24.56	7.08	8.53	30.03	172.56	0.0064	1.6483	48.93	37.88
10:28:09	1:6550	1867.53	118	1812	429	24.54	7.64	7.83	38.68	172.82	0.0067	1.6550	54.00	37.88
10:28:34	1:6619	1867.98	116	1803	423	22.29	6.42	8.38	35.06	173.14	0.0069	1.6619	17.00	36.45
10:29:00	1:6692	1868.13	119	1841	431	22.97	8.68	8.91	34.80	173.43	0.0073	1.6692	37.50	35.84

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/88															
Starting Depth =	1781	Bit Type =	Walker McDonald MP68H													
Ending Depth =	1936	Bit Size =	4.75												Average ROP Excluding Slugs	
Total Depth Drilled	155	Bit Nozzles =	9, 9, 12, 13												Depth Drilled =	155.33
Hours On Bit =	2.80	Mud Type =	Water Based												Hours On Bit =	2.80
Average ROP =	48.34	Mud Weight (lb/gal) =	8.70												Average ROP	48.34
Drilling (ft) =	1789.66	Pipe (ft) =	1041.85	Collar (ft)	746.61											

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours-On Bit	Hours On Bit	ROP (#/hr)	ROP (#/hr)
10:28:17	1:07:39	1863.38	118	1834	418	23.83	8.07	8.36	52.84	173.89	0.0047	1:07:39	58.29	38.91
10:29:39	1:09:00	1868.53	115	1847	419	22.99	8.01	8.74	41.23	173.82	0.0051	1:09:00	58.54	38.20
10:30:09	1:09:30	1868.77	123	1748	425	23.67	8.09	8.83	16.85	174.14	0.0053	1:09:30	28.40	35.03
10:30:22	1:09:43	1869.02	117	1893	427	21.50	10.24	8.95	68.74	174.32	0.0036	1:09:43	48.86	37.78
10:30:48	1:09:59	1869.27	118	1822	433	23.28	8.88	8.75	34.99	174.65	0.0072	1:09:59	31.85	37.57
10:31:10	1:10:21	1869.53	118	1766	430	25.53	5.93	8.34	41.09	174.79	0.0081	1:10:21	39.27	37.76
10:31:40	1:10:51	1869.73	120	1868	437	25.38	5.48	7.63	24.98	175.03	0.0083	1:10:51	38.80	38.83
10:32:10	1:11:21	1869.97	119	1720	433	24.57	7.21	7.45	28.26	175.23	0.0085	1:11:21	24.00	34.83
10:32:35	1:11:46	1870.22	122	1763	443	25.56	6.21	8.05	36.06	175.5	0.0235	1:11:46	38.68	35.06
10:32:57	1:12:08	1870.47	129	1906	437	22.43	9.23	8.88	40.05	175.79	0.0061	1:12:08	47.45	34.26
10:33:12	1:12:23	1870.73	114	1894	414	22.58	8.88	7.43	60.50	176.06	0.0042	1:12:23	64.80	35.49
10:33:42	1:12:53	1870.92	120	1738	435	24.78	6.94	7.72	23.70	176.25	0.0063	1:12:53	32.50	38.34
10:34:09	1:13:20	1871.15	117	1840	424	23.93	7.78	7.83	34.63	176.5	0.0075	1:13:20	33.33	34.25
10:34:33	1:13:44	1871.43	118	1847	430	24.23	7.49	8.09	38.41	176.75	0.0067	1:13:44	37.50	34.55
10:35:03	1:14:14	1871.61	117	1726	425	25.86	5.91	7.42	21.58	176.92	0.0093	1:14:14	28.40	32.14
10:35:24	1:14:35	1871.86	116	1844	421	22.50	8.13	7.45	43.45	177.22	0.0059	1:14:35	51.43	34.23
10:35:47	1:14:58	1872.11	118	1872	429	22.20	9.28	7.92	48.30	177.57	0.0064	1:14:58	23.48	35.60
10:36:05	1:15:16	1872.36	120	1791	437	24.52	7.19	7.80	38.40	177.88	0.0081	1:15:16	56.73	35.60
10:36:37	1:15:48	1872.61	118	1878	400	21.26	10.34	8.37	33.02	177.86	0.0078	1:15:48	55.71	35.02
10:36:53	1:16:04	1872.86	117	1881	427	22.54	9.11	9.01	54.94	178.13	0.0044	1:16:04	33.25	34.76
10:37:23	1:16:34	1873.37	116	1708	423	24.34	7.33	8.68	12.54	178.31	0.0083	1:16:34	21.26	33.39
10:37:42	1:16:53	1873.32	119	1870	432	23.27	8.33	8.46	48.83	178.51	0.0053	1:16:53	37.68	34.48
10:37:59	1:17:10	1873.47	125	1779	436	24.75	5.95	8.42	54.66	178.76	0.0047	1:17:10	52.94	35.65
10:38:26	1:17:37	1873.72	116	1741	427	25.31	6.40	7.63	38.32	178.96	0.0075	1:17:37	29.33	37.42
10:38:54	1:18:05	1873.98	120	1775	428	25.59	8.16	7.04	32.47	179.29	0.0078	1:18:05	29.64	36.04
10:39:19	1:18:30	1874.23	117	1686	425	27.32	4.48	6.48	37.03	179.52	0.0089	1:18:30	33.12	36.00
10:39:46	1:18:57	1874.42	117	1695	420	28.52	5.10	5.82	22.89	179.72	0.0083	1:18:57	24.00	33.71
10:40:09	1:19:20	1874.67	119	1794	432	25.19	8.62	5.75	43.41	179.93	0.0058	1:19:20	37.80	34.88
10:40:28	1:19:39	1874.92	117	1823	425	25.29	6.51	5.77	45.89	180.21	0.0058	1:19:39	48.43	34.33
10:40:55	1:19:56	1875.17	119	1728	433	26.82	4.66	5.53	35.00	180.55	0.0072	1:19:56	34.62	37.36

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/98														
Starting Depth =	1781	Bit Type =	Walker McDonald MP68H	Average ROP Excluding Stops											
Ending Depth =	1818	Bit Size =	4.75												
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12										Depth Drilled =	135.33	
Hours On Bit =	2.80	Mud Type =	Water Based										Hours On Bit =	2.80	
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70										Average ROP =	48.34	
Drillstring (R) =	1789.65	Pipe (R) =	1041.05	Collar (R)	740.61										

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
10:41:17	1:87:39	1875.42	118	1790	428	26.15	6.71	6.76	40.60	180.72	0.0081	1:87:39	26.49	36.64
10:41:37	1:87:59	1875.86	117	1775	424	26.25	6.21	6.08	45.71	180.66	0.0096	1:87:59	48.60	36.58
10:42:06	1:88:25	1875.93	118	1747	426	26.53	6.38	5.99	36.99	181.21	0.0081	1:88:25	27.31	38.16
10:43:26	1:89:31	1876.18	116	1891	430	26.05	5.73	5.78	46.78	181.45	0.0096	1:89:31	43.20	37.36
10:42:50	1:89:07	1876.43	116	1785	430	25.25	6.52	6.09	37.36	181.69	0.0067	1:89:07	36.03	37.54
10:43:15	1:89:37	1876.88	119	1787	431	24.69	7.20	6.39	36.47	181.97	0.0069	1:89:37	40.32	39.50
10:43:31	1:89:53	1876.93	115	1689	426	22.78	6.61	6.91	55.57	182.2	0.0044	1:89:53	51.75	40.28
10:43:56	1:90:18	1877.15	116	1826	427	22.85	6.61	7.37	36.75	182.49	0.0069	1:90:18	41.79	39.48
10:44:26	1:90:44	1877.38	117	1716	426	25.19	6.38	7.50	22.55	182.74	0.0083	1:90:44	30.00	37.71
10:44:39	1:90:59	1877.63	118	1911	428	24.65	6.56	7.51	72.92	182.9	0.0038	1:90:59	44.31	39.36
10:45:00	1:91:20	1877.85	121	1791	439	25.73	6.62	7.24	42.77	183.15	0.0058	1:91:20	42.66	39.19
10:45:30	1:91:52	1878.06	119	1899	433	25.23	6.26	6.79	26.36	183.38	0.0093	1:91:52	27.60	37.69
10:45:44	1:92:06	1878.31	120	1834	435	23.69	6.33	6.67	63.76	183.55	0.0039	1:92:06	54.00	38.73
10:46:00	1:92:25	1878.56	120	1625	435	26.01	6.68	6.71	59.19	183.82	0.0044	1:92:25	74.26	40.36
10:46:30	1:92:56	1878.75	120	1779	437	23.35	6.18	6.63	26.37	184.16	0.0053	1:92:56	26.60	38.95
10:46:44	1:93:17	1879.05	118	1970	429	22.89	6.55	7.10	63.37	184.33	0.0039	1:93:17	43.71	38.54
10:46:58	1:93:31	1879.30	116	1823	424	24.76	6.77	7.29	65.58	184.6	0.0039	1:93:31	69.43	41.74
10:47:26	1:93:59	1879.56	119	1737	432	25.45	6.39	6.90	33.01	184.84	0.0078	1:93:59	30.66	43.60
10:47:44	1:94:14	1879.81	117	1901	427	22.51	6.95	7.37	49.50	185.09	0.0050	1:94:14	48.00	42.42
10:48:09	1:94:33	1880.08	117	1798	427	23.99	7.50	7.84	38.20	185.33	0.0069	1:94:33	36.00	41.33
10:48:39	1:95:07	1880.11	121	1672	438	26.52	5.09	6.94	6.23	185.85	0.0083	1:95:07	26.40	39.69
10:48:49	1:95:14	1880.36	122	2062	441	22.80	6.68	7.32	93.44	185.8	0.0028	1:95:14	60.00	36.89
10:49:07	2:00:44	1880.61	118	1759	429	24.61	6.72	7.39	48.77	186.04	0.0050	2:00:44	48.00	39.47
10:49:37	2:01:28	1880.91	123	1685	435	25.69	5.88	6.79	23.42	186.11	0.0083	2:01:28	8.40	38.89
10:49:56	2:01:58	1881.06	114	2148	416	20.44	10.91	7.46	59.88	186.51	0.0060	2:01:58	60.00	37.68
10:50:22	2:02:53	1881.31	117	1827	427	22.79	6.75	8.19	33.74	186.62	0.0075	2:02:53	14.67	36.47
10:50:35	2:03:17	1881.56	120	1776	434	24.35	6.96	7.85	38.99	186.83	0.0054	2:03:17	32.87	36.18
10:51:13	2:03:54	1881.81	115	1775	418	24.00	7.23	7.95	52.83	187.07	0.0078	2:03:54	30.86	34.45
10:51:43	2:04:28	1882.05	121	1757	408	24.68	6.67	8.10	22.63	187.35	0.0083	2:04:28	33.60	32.64
10:52:05	2:05:09	1882.25	118	1737	429	24.43	6.53	7.29	41.26	187.66	0.0081	2:05:09	56.73	37.40

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/17/98														
Starting Depth =	1781	Bit Type =	Walker McDonald MF-88H	Average ROP Excluding Stops											
Ending Depth =	1916	Bit Size =	4.75												
Total Depth Drilled	135	Bit Nozzles =	9, 8, 12, 12	Depth Drilled =	135.33										
Hours On Bit =	2.80	Mud Type =	Water Based	Hours On Bit =	2.80										
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.73	Average ROP	48.34										
Drillstring (ft) =	1789.86	Pipe (ft) =	1841.95	Collar (ft)	740.61										

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
10:52:57	2:00:00	1882.50	118	1855	430	31.78	8.26	7.41	39.76	187.78	0.0001	2:00:00	19.64	35.29
10:52:58	2:00:01	1882.75	120	1782	435	23.89	7.33	7.48	31.51	188.03	0.0001	2:00:01	31.03	33.64
10:53:21	2:07:50	1883.00	117	1751	427	24.88	6.89	7.36	36.03	188.34	0.0009	2:07:50	44.64	35.26
10:53:43	2:09:11	1883.26	117	1855	425	34.28	9.96	7.43	41.23	188.52	0.0061	2:09:11	31.09	34.74
10:54:10	2:08:08	1883.51	121	1801	438	35.57	8.72	7.21	34.43	188.76	0.0075	2:08:08	36.67	34.74
10:54:40	2:09:09	1883.62	123	1819	448	27.24	4.32	6.18	13.76	188.94	0.0083	2:09:09	21.83	31.56
10:55:08	2:10:47	1883.88	116	1740	423	24.97	6.31	5.65	32.47	189.22	0.0078	2:10:47	36.00	31.71
10:55:32	2:11:14	1884.13	118	1821	420	23.95	7.59	6.08	36.94	189.44	0.0057	2:11:14	33.00	33.48
10:55:53	2:11:72	1884.38	117	1851	424	23.73	7.51	6.19	42.48	189.69	0.0056	2:11:72	42.86	33.53
11:05:53	2:11:72	1884.48	111	1857	404	31.69	0.33		115.36	189.88	0.0000	2:11:72	0.00	
11:05:59	2:11:94	1884.73	114	1259	418	31.82	0.87		158.78	190.01	0.0022	2:11:94	58.90	
11:06:29	2:12:78	1884.96	108	1488	398	38.89	4.79		27.26	190.26	0.0003	2:12:78	28.80	
11:06:42	2:13:14	1885.21	104	2309	380	21.58	9.91		79.69	190.46	0.0036	2:13:14	68.46	
11:07:12	2:13:97	1885.33	106	1497	388	27.05	4.86	3.93	14.34	190.69	0.0083	2:13:97	24.66	
11:07:38	2:14:09	1885.58	108	1578	398	25.87	5.79	6.04	34.86	191	0.0073	2:14:09	42.92	
11:07:57	2:15:22	1885.89	109	1763	397	23.67	7.90	6.61	48.25	191.08	0.0053	2:15:22	17.65	
11:08:19	2:15:67	1886.09	107	1818	390	23.22	8.25	7.30	84.03	191.35	0.0044	2:15:67	58.59	
11:08:33	2:16:22	1886.34	105	1812	382	23.30	8.25	6.97	46.59	191.66	0.0086	2:16:22	65.80	
11:08:47	2:16:61	1886.59	105	1862	393	23.12	8.43	7.72	64.28	191.85	0.0039	2:16:61	48.86	43.16
11:09:06	2:17:03	1886.84	106	1918	388	22.76	8.76	8.32	59.30	192.39	0.0042	2:17:03	105.80	41.51
11:09:37	2:17:44	1887.10	109	1841	396	23.74	7.83	8.39	63.26	192.44	0.0042	2:17:44	36.00	45.86
11:09:31	2:17:83	1887.35	107	1898	380	23.29	8.38	8.31	83.58	192.63	0.0039	2:17:83	48.88	45.59
11:09:47	2:18:28	1887.55	109	1904	398	23.48	8.07	8.27	95.68	192.84	0.0044	2:18:28	69.73	52.72
11:10:04	2:19:75	1887.85	106	1819	393	23.39	8.26	8.23	94.21	193.13	0.0047	2:19:75	49.24	55.97
11:10:19	2:19:17	1888.10	107	1888	391	23.78	8.78	8.23	98.87	193.4	0.0042	2:19:17	64.80	67.56
11:10:33	2:19:58	1888.36	108	1904	388	22.71	8.81	8.42	88.57	193.68	0.0039	2:19:58	72.00	68.37
11:10:52	2:20:08	1888.61	102	1830	373	23.31	8.24	8.42	46.69	193.62	0.0053	2:20:08	48.47	58.76
11:11:06	2:20:47	1888.88	103	1938	376	22.42	9.09	8.62	66.73	194.12	0.0039	2:20:47	51.43	58.73
11:11:22	2:20:92	1889.11	108	1883	387	23.25	8.31	8.84	54.14	194.43	0.0044	2:20:92	69.75	58.37

DOE high power motor test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 5	Date: 12/17/88														
Starting Depth =	1781	Bit Type =	Walker McDonald MF68H	Average ROP Excluding Stags											
Ending Depth =	1916	Bit Size =	4.75												
Total Depth Drilled	135	Bit Nozzles =	3, 9, 12, 12	Depth Drilled =	135.33										
Hours On Bit =	2.80	Mud Type =	Water Based	Hours On Bit =	2.80										
Average ROP =	48.34	Mud Weight (lb/gal) =	8.70	Average ROP =	48.34										
Drilling (ft) =	1789.66	Pipe (ft) =	1041.05	Collar (ft)	740.51										

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WGB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
11:11:38	2:21:00	1889.37	105	1532	384	22.00	8.57	8.50	57.50	194.92	0.0044	2:21:00	42.75	57.95
11:11:57	2:21:59	1889.52	108	1540	384	21.88	9.62	8.81	47.62	194.94	0.0053	2:21:59	60.63	55.97
11:12:22	2:22:58	1889.67	105	1726	382	21.75	9.73	9.10	37.32	195.27	0.0056	2:22:58	47.32	52.72
11:12:41	2:23:11	1890.32	106	1772	386	22.65	8.92	9.07	47.89	195.4	0.0053	2:23:11	34.65	52.05
11:13:05	2:23:78	1890.38	108	1760	388	20.83	10.86	9.59	37.63	195.71	0.0067	2:23:78	48.59	49.45
11:13:16	2:24:08	1890.53	105	1873	382	23.44	8.11	9.50	81.72	195.9	0.0031	2:24:08	62.18	50.10
11:13:40	2:24:75	1890.68	107	1891	391	25.44	5.21	8.77	39.67	196.15	0.0057	2:24:75	37.59	48.64
11:13:53	2:25:11	1891.14	104	1817	379	24.23	6.58	8.16	62.28	196.4	0.0036	2:25:11	69.23	49.15
11:14:19	2:25:58	1891.30	105	1891	384	24.28	7.30	7.84	54.35	196.65	0.0047	2:25:58	52.94	48.86
11:14:26	2:26:03	1891.54	106	1793	385	25.03	6.58	6.98	55.47	196.96	0.0044	2:26:03	60.78	48.84
11:14:40	2:26:42	1891.89	104	1838	380	25.19	6.47	6.05	64.47	197.19	0.0038	2:26:42	59.57	50.13
11:14:54	2:26:51	1892.14	111	1849	405	25.41	6.23	6.65	66.44	197.49	0.0039	2:26:51	75.71	53.76
11:15:13	2:27:33	1892.49	108	1718	386	25.34	6.29	6.87	46.33	197.67	0.0053	2:27:33	34.11	54.00
11:15:38	2:28:03	1892.85	107	1816	392	21.30	10.16	7.18	37.38	197.83	0.0069	2:28:03	37.44	51.41
11:16:00	2:28:54	1892.91	108	1828	394	21.29	10.20	7.87	42.35	198.2	0.0061	2:28:54	44.16	50.85
11:16:17	2:29:11	1893.17	109	1776	366	20.32	11.18	8.81	54.12	198.3	0.0047	2:29:11	63.53	52.51
11:16:32	2:29:53	1893.42	105	1944	382	21.16	10.28	9.82	61.51	198.61	0.0042	2:29:53	56.40	51.62
11:16:41	2:29:78	1893.68	108	1821	388	20.82	5.72	9.51	58.05	198.88	0.0035	2:29:78	28.99	54.60
11:16:55	2:30:17	1893.93	107	1783	391	28.35	6.25	8.73	67.92	199.22	0.0039	2:30:17	61.71	55.33
11:17:16	2:30:75	1894.18	108	1698	388	25.21	8.42	7.97	42.09	199.47	0.0056	2:30:75	42.86	52.89
11:17:34	2:31:23	1894.43	103	1755	385	21.23	8.30	7.39	50.47	199.7	0.0050	2:31:23	46.00	51.52
11:17:56	2:31:56	1894.69	110	1751	400	23.36	8.19	5.98	41.38	199.93	0.0081	2:31:56	39.37	56.56
11:18:15	2:32:39	1894.94	103	1815	376	21.16	10.30	7.89	45.16	200.24	0.0083	2:32:39	55.84	52.61
11:18:31	2:32:53	1895.19	106	1771	366	23.24	9.21	8.29	55.06	200.45	0.0044	2:32:53	47.25	54.36
11:18:52	2:33:42	1895.44	111	1769	404	22.34	9.17	8.89	44.10	200.77	0.0058	2:33:42	54.86	52.72
11:19:07	2:33:83	1895.69	108	1956	366	19.72	11.67	9.51	58.93	201	0.0042	2:33:83	55.20	52.72
11:19:33	2:34:58	1895.94	110	1802	359	19.97	11.44	19.16	34.78	201.22	0.0072	2:34:58	30.48	47.30
11:19:51	2:35:08	1896.20	108	1791	395	19.70	11.69	10.44	49.76	201.48	0.0059	2:35:08	52.00	48.43
11:20:13	2:35:57	1896.45	110	1896	400	19.54	11.75	11.34	41.54	201.73	0.0061	2:35:57	40.91	45.17
11:20:31	2:36:17	1896.70	112	1855	408	21.00	9.48	11.21	51.89	202.04	0.0050	2:36:17	62.00	46.17

DOE high power motor test Amaco Catrosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 13/17/98	Bit Type =	Water Motorcase M88-04
Starting Depth =	1721	Bit Size =	4.75
Ending Depth =	1916	Bit No/Case =	9. 9. 12. 12
Total Depth Drilled	126	Bit Type =	Water Based
Hours On Bit =	2.89	Motor Weight (lbs/gal) =	8.70
Average ROP =	48.34	Spore (ft) =	1041.05
Drilling Bit =	1799.68	Collar (ft)	740.61
Average ROP Excluding Stops			
Depth Drilled = 126.00			
Hours On Bit = 2.89			
Average ROP = 48.34			

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psil)	Calculated Speed (fpm)	Load (lbs)	WOB (kips)	Average WOB (klbs)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
11:20:53	2:59:22	1938.96	109	1894	388	21.20	10.26	16.82	45.27	202.32	0.0056	2:59:22	36.46	46.29
11:21:13	2:59:35	1897.21	110	1854	802	19.95	11.46	10.83	39.92	202.59	0.0061	2:59:33	36.96	46.91
11:21:28	2:59:48	1860.46	108	1880	394	22.02	9.47	10.48	69.12	202.62	0.0062	2:59:42	67.20	46.17
11:21:50	2:59:58	1830.71	104	1773	380	22.10	9.28	10.03	49.76	202.66	0.0061	2:59:56	66.19	45.91
11:22:10	2:59:58	1817.96	103	1876	176	19.49	11.69	10.49	44.08	202.25	0.0056	2:59:52	52.40	44.66
11:22:30	2:59:58	1836.10	106	1807	385	27.31	4.41	9.32	16.22	203.4	0.0063	2:59:55	18.69	41.68
11:23:10	2:40:58	1836.32	110	1720	403	22.62	8.99	8.86	27.41	203.65	0.0063	2:40:58	35.69	38.35
11:23:24	2:41:07	1898.58	113	1997	403	18.81	11.99	8.29	68.95	203.86	0.0059	2:41:07	64.70	40.16
11:24:03	2:42:06	1898.98	109	1874	403	21.24	10.23	8.35	41.09	204.11	0.0061	2:41:59	40.91	39.52
11:24:18	2:42:17	1899.34	107	1839	399	21.29	10.18	8.35	53.95	204.34	0.0062	2:42:08	48.71	39.94
11:24:36	2:42:36	1898.56	113	1832	480	19.74	11.68	10.51	68.27	204.67	0.0063	2:42:17	79.39	41.35
11:25:01	2:42:57	1898.94	110	1788	399	22.59	8.92	10.52	53.19	204.9	0.0062	2:42:58	55.36	41.86
11:25:20	2:43:15	1898.98	158	1879	394	22.01	9.49	10.95	32.93	205.12	0.0072	2:43:15	28.29	40.14
11:25:43	2:44:02	1902.34	110	1902	432	21.87	5.60	9.89	39.21	205.61	0.0064	2:44:02	66.32	40.56
11:25:57	2:44:22	1902.58	109	1935	393	19.37	11.93	9.89	47.03	205.47	0.0064	2:44:19	31.91	44.97
11:26:06	2:45:03	1902.88	107	1814	369	28.93	10.52	9.89	65.32	206.98	0.0069	2:45:03	95.14	49.15
11:26:49	2:45:57	1910.41	118	1749	400	21.88	9.79	10.25	31.83	208.53	0.0083	2:46:15	33.52	46.10
11:27:06	2:47:11	1901.39	110	1881	399	19.24	12.12	10.89	39.88	208.47	0.0064	2:46:57	34.43	44.25
11:27:26	2:47:37	1901.62	110	1832	399	18.94	12.41	11.97	55.45	206.67	0.0064	2:47:11	48.09	46.10
11:27:42	2:48:14	1901.97	109	1831	395	20.99	10.89	14.13	45.68	206.8	0.0064	2:47:57	41.69	43.93
11:28:01	2:48:37	1902.32	111	1863	404	22.90	8.93	15.79	53.23	207.13	0.0067	2:48:14	48.71	43.81
11:28:31	2:49:22	1902.38	111	1758	482	24.74	8.85	16.17	49.09	207.52	0.0053	2:49:17	73.89	45.80
11:28:36	2:49:54	1902.63	113	1887	411	23.47	8.86	8.30	44.81	207.68	0.0058	2:49:22	73.89	45.80
11:28:51	2:50:38	1902.88	109	1861	395	23.93	7.64	9.30	59.02	207.87	0.0062	2:50:34	89.80	47.55
11:29:11	2:50:61	1903.18	106	1813	365	26.42	7.17	7.68	83.16	208.17	0.0042	2:50:58	69.20	47.85
11:29:26	2:51:23	1901.40	111	1726	403	26.74	5.99	7.13	41.34	208.42	0.0052	2:51:28	40.80	49.25
11:29:46	2:51:54	1903.88	109	1875	398	23.88	7.71	7.38	39.19	208.60	0.0056	2:51:58	40.80	49.66
11:30:06	2:52:19	1903.66	113	1810	413	26.32	7.07	7.18	72.81	208.97	0.0056	2:52:19	60.92	51.58
11:30:26	2:53:03	1904.06	110	1926	400	35.32	8.31	6.83	44.45	209.33	0.0083	2:53:03	75.95	60.35
									76.11	209.58			1.30	44.89

DOE high power mortar test Amaco Catoosa Test Site

DOE HP Motor No. 2

Well No. 6	Date: 12/7/88														
Starting Depth =	1781	Bit Type =	Walker McDonnell MP55H									Average ROP Excluding Stops			
Ending Depth =	1916	Bit Size =	4.75												
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12									Depth Drilled =	135.31		
Hours On Bit =	2.60	Mud Type =	Water Based									Hours On Bit =	2.60		
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70									Average ROP	48.34		
Drilling (ft) =	1789.66	Rpm (ft) =	1041.05	Collar (ft)	740.61										

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
11:30:54	2:5347	1904.30	108	1859	393	23.51	8.05	7.01	58.44	209.58	0.0044	2:5347	51.00	45.36
11:31:35	2:5406	1904.55	107	1753	396	24.73	8.87	7.20	41.74	209.53	0.0028	2:5406	42.88	45.18
11:31:30	2:5447	1904.81	111	1936	483	32.17	8.33	7.53	59.93	210.36	0.0042	2:5447	103.20	48.10
11:31:45	2:5489	1905.06	107	1900	388	22.91	8.61	7.83	64.20	210.37	0.0042	2:5459	26.49	44.90
11:32:08	2:5553	1905.31	112	1807	410	25.81	7.77	8.13	38.48	210.34	0.0064	2:5553	42.28	44.14
11:32:25	2:5606	1905.57	111	1914	405	21.98	9.51	8.42	62.71	210.08	0.0047	2:5600	50.82	45.98
11:32:34	2:5625	1905.82	104	2001	379	21.32	10.15	8.07	104.83	211.25	0.0025	2:5625	148.00	47.08
11:33:01	2:5700	1906.07	103	1939	396	21.88	9.61	8.13	34.35	211.34	0.0075	2:5700	12.02	45.15
11:33:14	2:5736	1906.32	107	1872	390	21.75	9.78	8.35	66.33	211.65	0.0036	2:5736	85.85	52.36
11:33:31	2:5783	1906.57	112	1941	407	21.48	8.96	9.81	54.33	211.65	0.0047	2:5783	42.35	52.05
11:33:56	2:5836	1906.82	106	1950	398	18.42	12.81	10.49	46.53	212.1	0.0053	2:5836	47.37	52.49
11:34:06	2:5886	1907.07	111	1927	404	17.01	14.25	11.31	51.52	212.37	0.0050	2:5886	54.66	51.48
11:34:34	2:5931	1907.32	109	1918	358	18.36	12.97	11.86	58.93	212.78	0.0044	2:5931	87.75	51.40
11:34:46	2:5975	1907.59	110	1926	401	19.50	11.48	12.32	37.15	213.92	0.0044	2:5975	38.00	54.00
11:34:56	2:6019	1907.84	108	1939	390	21.02	10.43	12.41	59.83	213.16	0.0044	2:6019	54.00	54.12
11:35:15	2:6072	1908.09	111	1868	405	18.19	12.95	12.42	47.48	213.35	0.0033	2:6072	35.00	53.76
11:35:25	2:6100	1908.34	108	2177	395	19.33	13.04	11.87	57.48	213.74	0.0038	2:6100	140.40	56.75
11:35:54	2:6181	1908.59	110	1783	401	23.92	7.85	10.51	38.68	213.89	0.0081	2:6181	18.62	51.08
11:36:11	2:6238	1908.84	116	1853	421	24.88	7.11	10.04	54.47	214.11	0.0047	2:6228	48.59	61.08
11:36:17	2:6244	1909.10	133	2026	375	22.28	8.28	9.81	155.21	214.42	0.0017	2:6244	188.00	88.84
11:36:39	2:6306	1909.35	112	1801	407	21.23	10.23	8.36	40.73	214.86	0.0061	2:6306	37.84	54.36
11:36:56	2:6360	1909.60	113	1912	411	20.73	10.71	8.00	57.88	215.53	0.0044	2:6350	85.59	54.12
11:37:13	2:6400	1909.85	110	1902	401	20.12	11.28	9.72	49.89	215.11	0.0050	2:6400	78.00	53.18
11:37:27	2:6439	1910.11	109	2302	397	19.84	11.58	10.61	63.54	215.47	0.0039	2:6439	93.57	54.12
11:37:57	2:6522	1910.28	111	1898	405	24.13	7.45	10.25	22.71	215.61	0.0083	2:6522	16.80	48.69
11:38:14	2:6569	1910.53	109	1952	397	20.42	11.00	10.40	54.39	215.81	0.0047	2:6559	42.35	46.88
11:38:36	2:6631	1910.78	111	1885	405	21.66	8.91	10.22	40.55	216.12	0.0081	2:6631	50.73	46.67
11:38:55	2:6683	1911.04	110	1898	401	20.82	10.81	10.13	49.05	216.21	0.0083	2:6683	36.00	48.23
11:39:12	2:6731	1911.29	105	1992	384	20.87	10.57	9.83	53.75	216.82	0.0047	2:6731	85.65	45.00
11:39:33	2:6789	1911.54	113	1855	411	21.67	9.61	10.40	42.88	216.86	0.0081	2:6789	41.14	45.21

DOE high power mortar test Amaco Catoosa Test Site

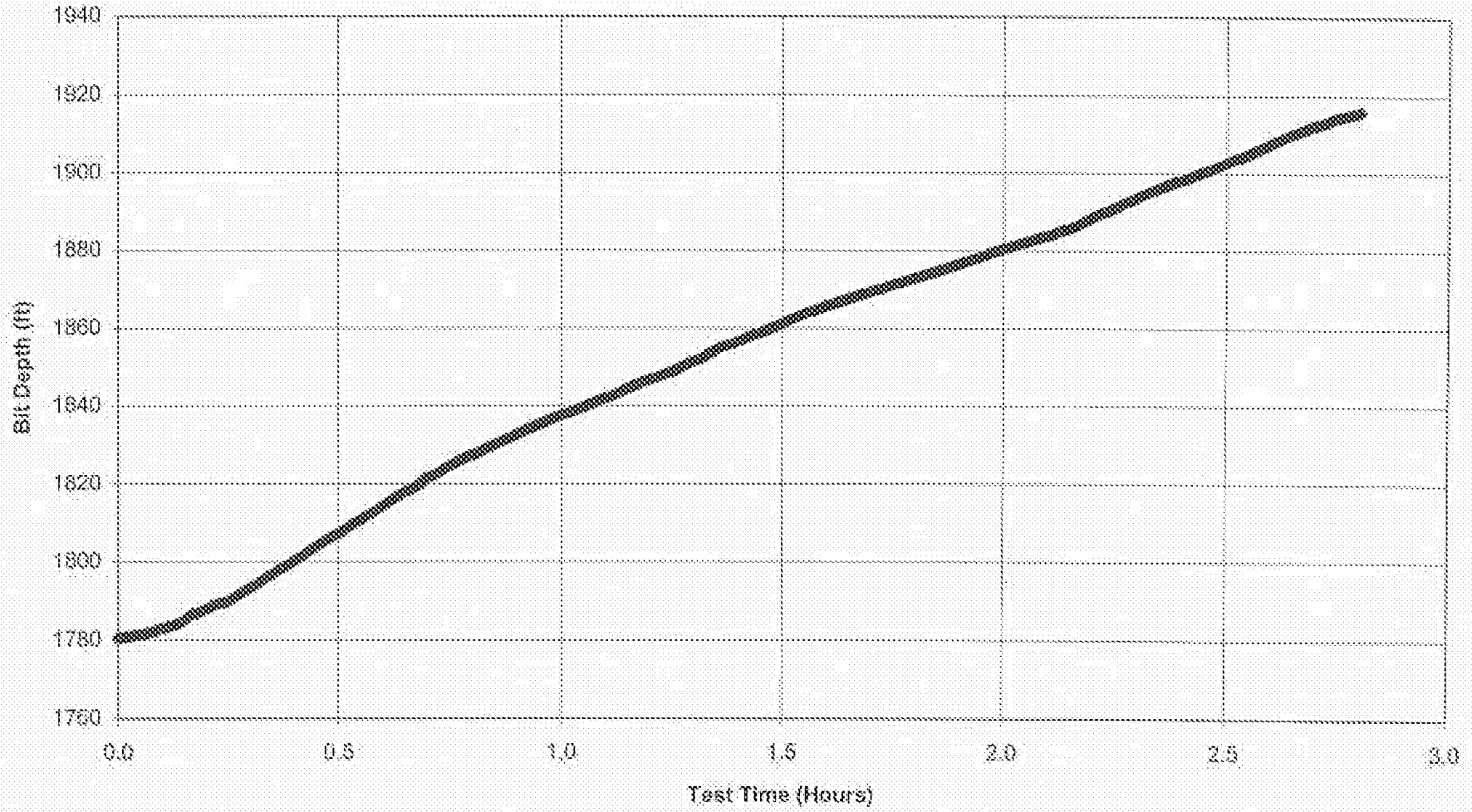
DOE HP Motor No. 2

Well No. #	Date: 12/17/88													
Starting Depth =	1751	Bit Type =	Walker McDonald MP88H	Average ROP Excluding Slips										
Ending Depth =	1916	Bit Size =	4.75											
Total Depth Drilled	135	Bit Nozzles =	9, 9, 12, 12	Depth Drilled =	135.33									
Hours On Bit =	2.80	Mud Type =	Water Based	Hours On Bit =	2.80									
Average ROP =	48.34	Mud Weight (lbs/gal) =	8.70	Average ROP =	48.34									
Drilling (ft) =	1769.66	Flow (ft) =	1041.05	Color (#)	740.61									

Time (HH:MM:SS)	Time From Start (HH:MM:SS)	Bit Depth (Feet)	Flow (gpm)	Pressure (psi)	Calculated Speed (rpm)	Hook Load (Kips)	WOB (Kips)	Average WOB (Kips)	ROP (ft/hr)	Feet On Bit	Incremental Hours On Bit	Hours On Bit	ROP (ft/hr)	ROP (ft/hr)
11:39:54	2.6847	1911.79	109	1912	398	21.81	9.87	10.17	42.08	217.06	-0.0058	2.6847	34.29	41.04
11:40:06	2.6861	1912.03	111	1920	403	22.55	9.91	9.99	79.06	217.49	0.0033	2.6881	129.00	45.79
11:40:24	2.6931	1912.30	109	2284	398	23.23	8.32	9.50	59.00	217.56	0.0030	2.6931	14.00	44.54
11:40:54	2.7014	1912.41	110	1629	400	27.39	4.32	6.25	12.73	217.76	0.0033	2.7014	24.00	43.32
11:41:08	2.7083	1912.65	113	1930	410	22.83	8.68	8.02	66.85	217.96	0.0039	2.7053	51.43	44.67
11:41:36	2.7136	1912.85	109	1899	395	27.19	4.53	6.95	23.29	218.13	0.0033	2.7158	29.40	46.88
11:42:00	2.7197	1913.10	112	1763	408	24.31	7.25	6.59	41.21	218.55	0.0061	2.7197	70.36	49.09
11:42:19	2.7250	1913.25	108	1918	393	22.65	8.66	6.69	47.93	218.83	0.0063	2.7256	33.26	39.66
11:42:34	2.7292	1913.61	108	1905	394	22.31	9.19	7.87	58.36	219.83	0.0042	2.7292	72.00	41.17
11:42:56	2.7363	1913.85	112	1892	408	22.82	8.69	7.67	41.15	219.15	0.0051	2.7353	36.00	30.99
11:43:08	2.7388	1914.11	112	1976	409	22.91	9.48	6.66	75.44	219.44	0.0033	2.7388	67.00	40.75
11:43:33	2.7456	1914.35	112	1785	407	25.82	8.03	8.41	36.15	219.63	0.0068	2.7456	25.62	39.24
11:44:03	2.7539	1914.55	113	1626	410	28.10	5.58	7.79	22.18	219.89	0.0083	2.7539	32.40	40.75
11:44:30	2.7614	1914.80	110	1617	398	25.85	5.81	7.11	33.76	220.15	0.0075	2.7614	32.00	38.14
11:45:00	2.7697	1914.97	112	1843	409	25.30	6.33	6.64	30.36	220.29	0.0063	2.7697	13.26	37.78
11:45:24	2.7764	1915.23	112	1843	408	25.25	6.37	6.02	37.59	220.62	0.0067	2.7764	34.50	37.41
11:45:52	2.7842	1915.47	112	1659	409	25.62	6.49	6.02	32.65	220.76	0.0078	2.7842	30.86	35.83
11:46:22	2.7925	1915.81	114	1631	415	23.57	6.00	6.51	17.75	221.65	0.0088	2.7925	34.80	31.56
11:46:47	2.7984	1916.07	112	1680	407	24.38	7.22	6.79	36.20	221.13	0.0069	2.7984	11.52	31.33

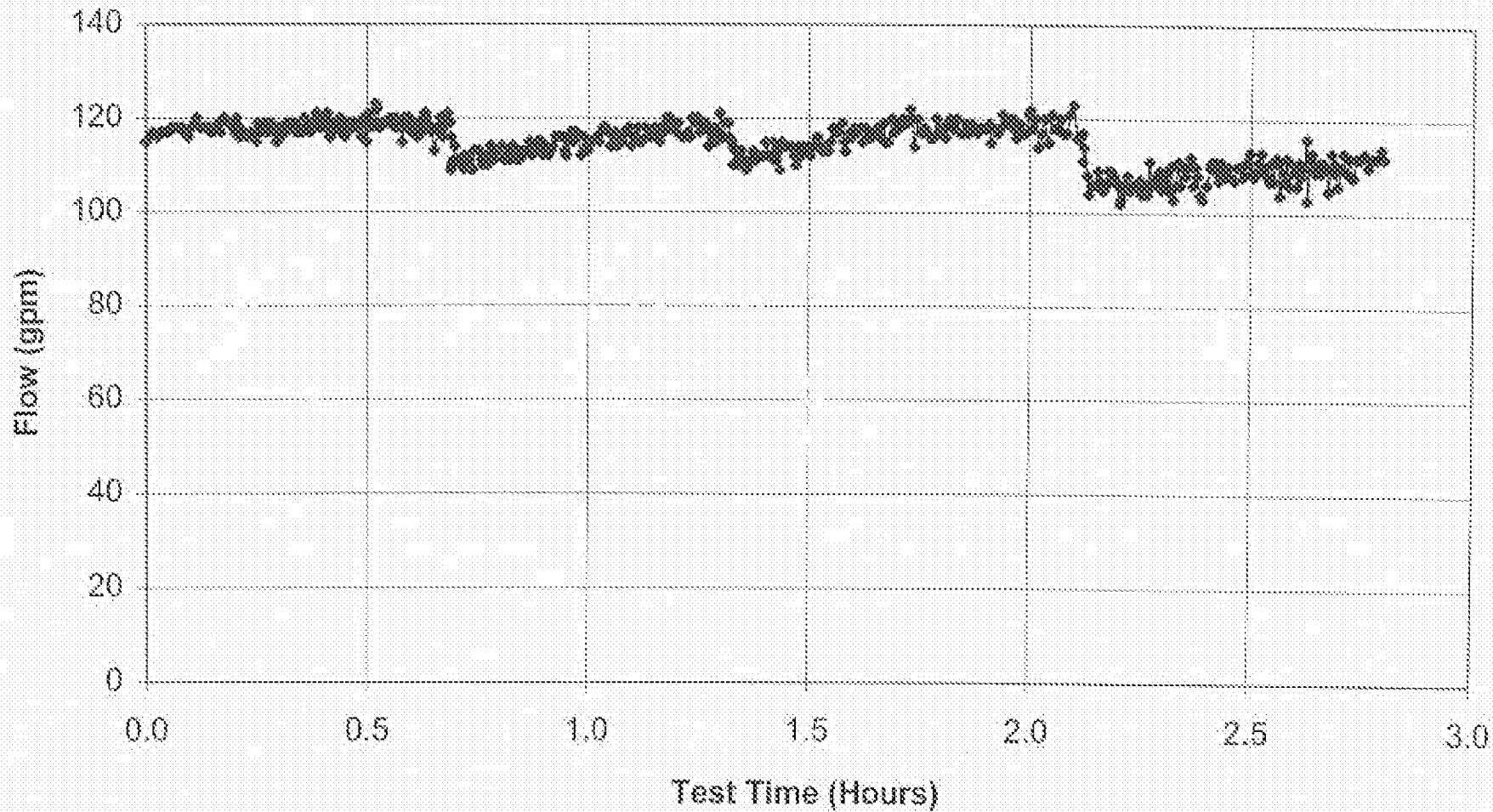
Bit Depth DOE HP Motor Test

HP Motor No. 2



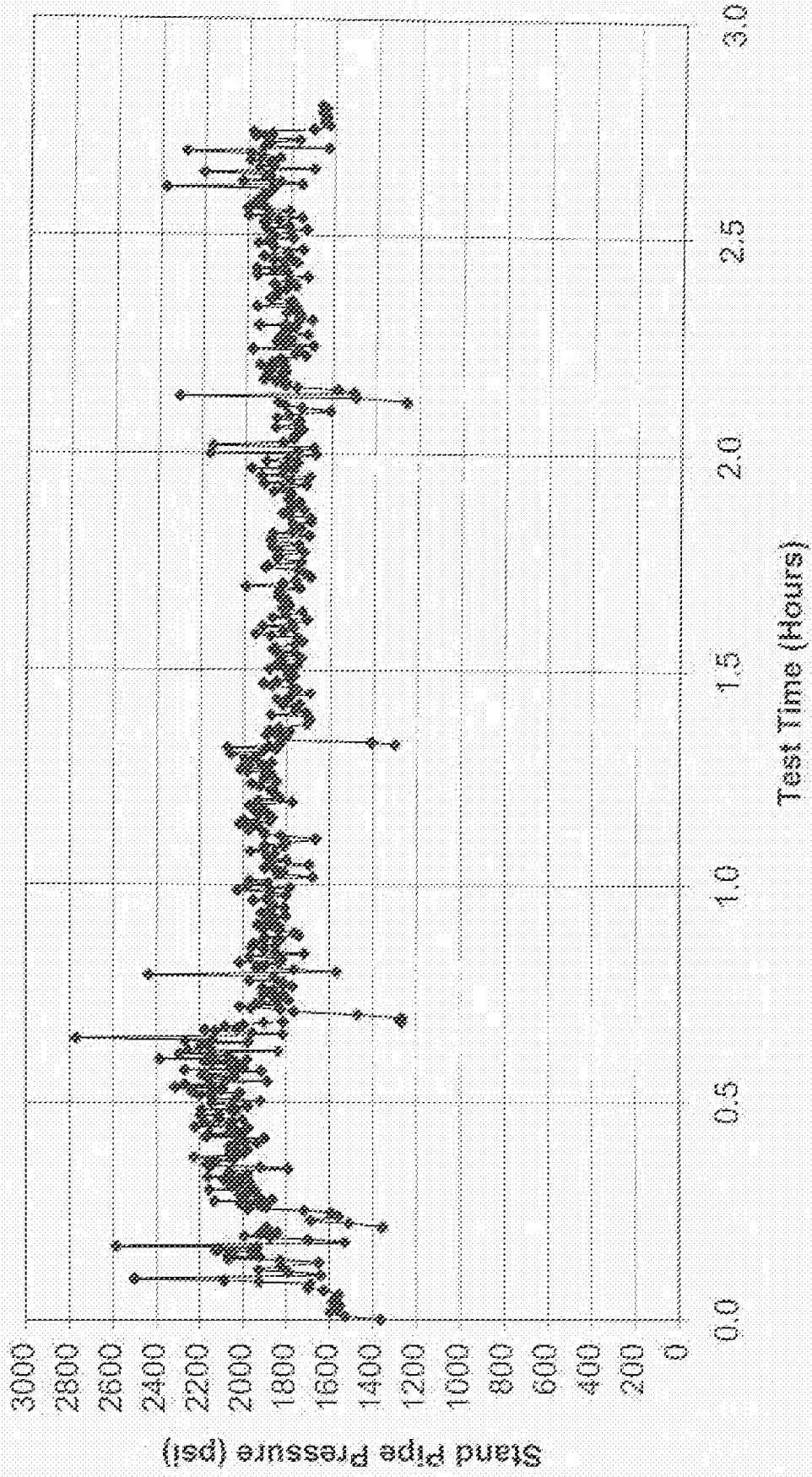
Flow Rate DOE SH-HP Motor Test

Hp Motor No. 2



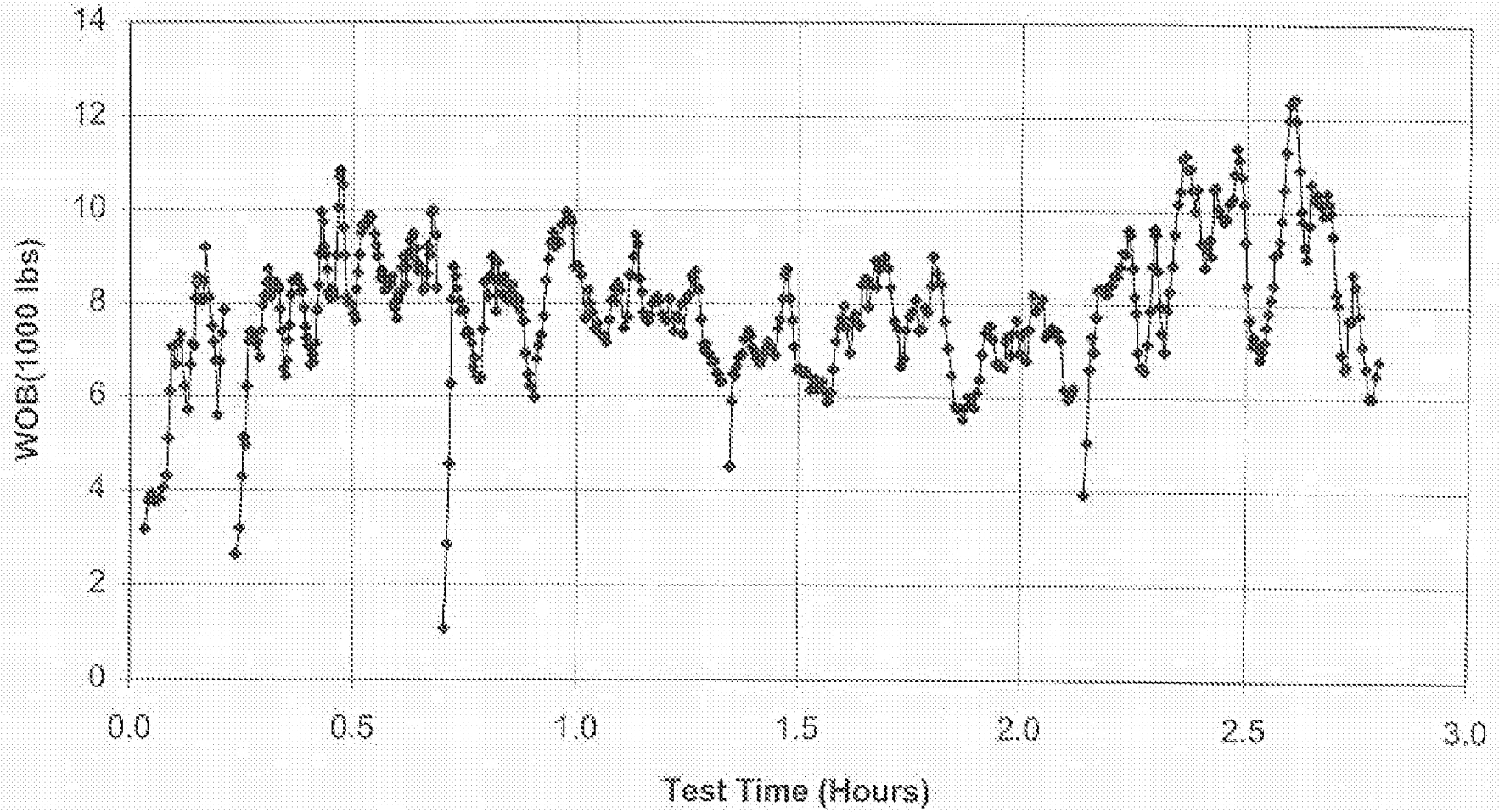
Stand Pipe Pressure DOE SH-HP Motor Test

HP Motor No. 2



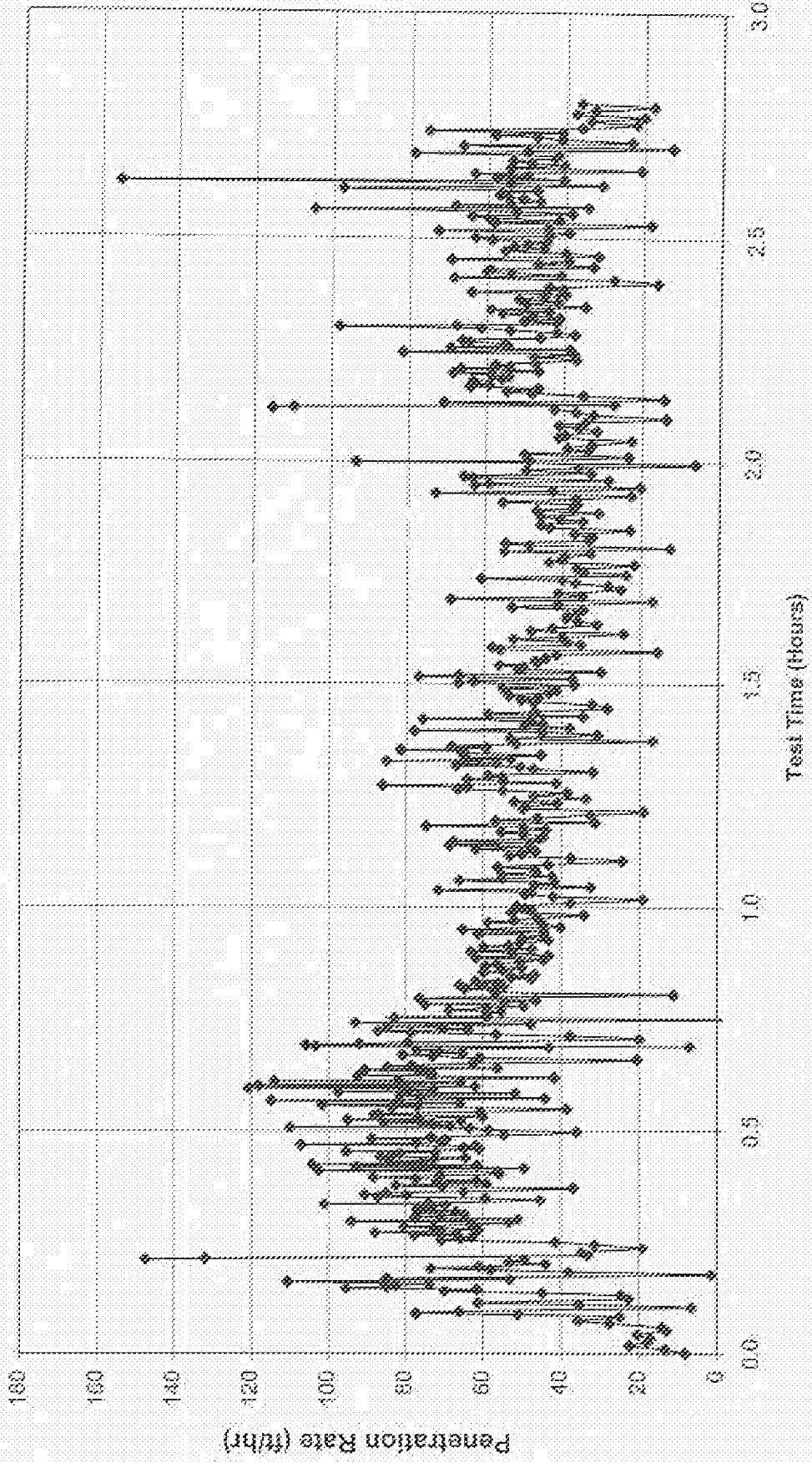
Bit Weight DOE SH-HP Motor Test

HP Motor No. 2



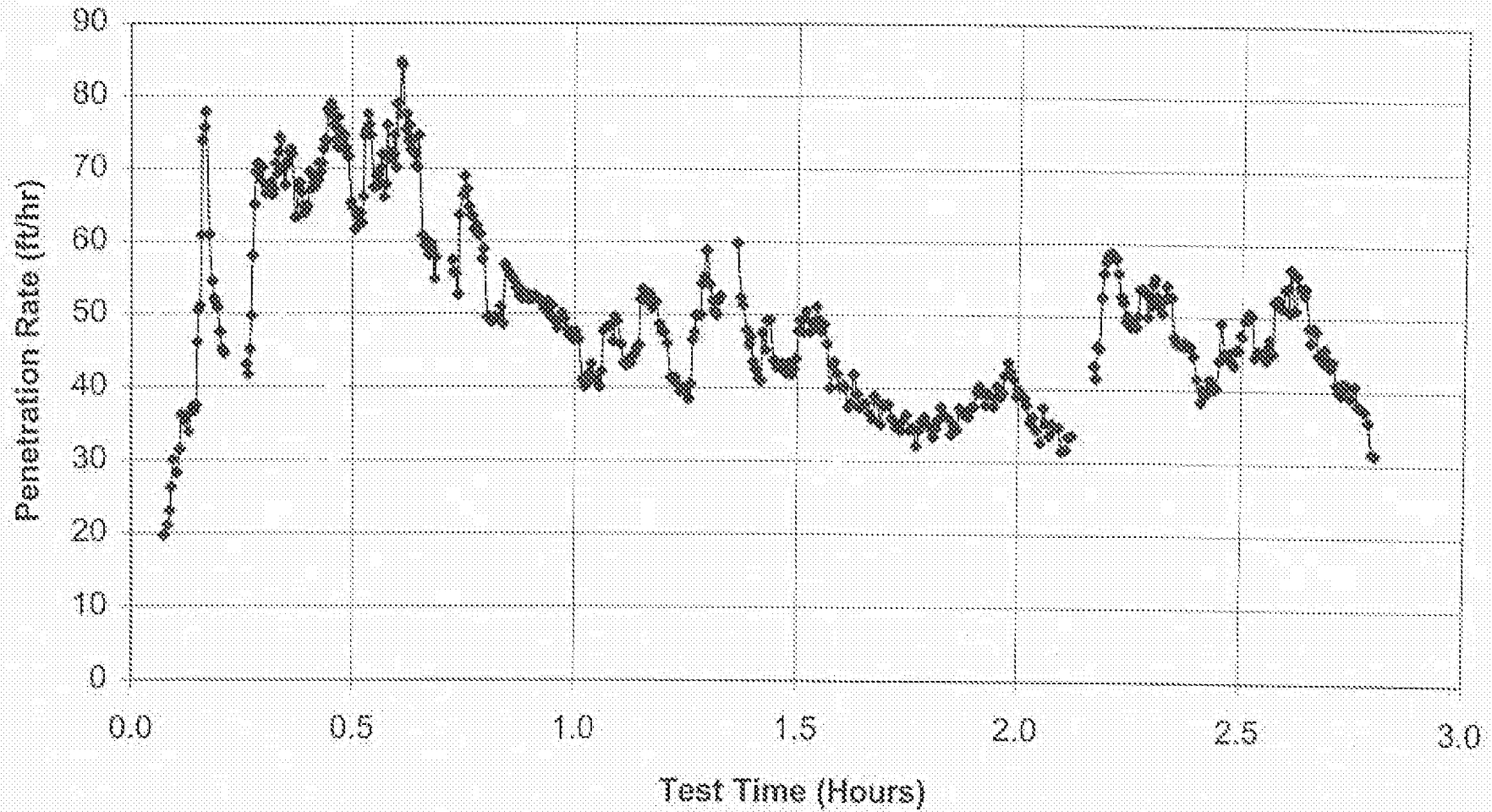
Penetration Rate DOE HP Motor Test

HP Motor No. 2



Penetration Rate DOE SH-HP Motor Test

HP Motor No. 2



ROP As A Function Of Bit Weight

DOE HP Motor No. 2

