Plutonium Immobilization Program - Cold Pour Phase 1 Test Results

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Introduction

The Plutonium Immobilization Project will disposition excess weapons grade plutonium. It uses the can-in-canister approach that involves placing plutonium-ceramic pucks in sealed cans that are then placed into Defense Waste Processing Facility canisters. These canisters are subsequently filled with high-level radioactive waste glass. This process puts the plutonium in a stable form and makes it unattractive for reuse. A cold (non-radioactive) glass pour program was performed to develop and verify the baseline design for the canister and internal hardware. This paper describes the Phase 1 scoping test results.

Background

The Plutonium Immobilization Program (PIP) is a DOE-sponsored joint venture combining the talents of the Savannah River Site (SRS), Lawrence Livermore National
Laboratory (LLNL), Argonne National Laboratory (ANL), and Pacific Northwest National Laboratory (PNNL) to disposition excess weapons grade plutonium. This program uses the “Can-in-Canister” (CIC) approach. CIC involves encapsulating plutonium in ceramic forms (or pucks), placing the pucks in sealed stainless steel cans, placing the cans in long cylindrical magazines, latching the magazines to racks inside Defense Waste Processing Facility (DWPF) canisters, and filling the DWPF canisters with high-level waste glass. This process puts the plutonium in a stable form and makes it unattractive for reuse.

The DWPF has successfully poured hundreds of empty canisters, so glass flow behavior in empty canisters is well understood. However, the CIC hardware presents a new set of operational concerns. Among these, premature glass freezing and CIC hardware structural integrity are issues that require additional study. Both modeling and test programs are underway to address these issues. Described herein are the results of the first phase (Phase 1) of non-radioactive glass pour tests designed to assess hardware structural integrity and glass flow characteristics under prototypic DWPF conditions. The Phase 1 Test pours are intended to provide scoping quality verification of design concepts prior to the more extensive and quality controlled Phase 2 Tests. The Phase 2 Tests will incorporate changes based on the results of the Phase 1 Tests and verify the adequacy of the baseline design.

Discussion

The objective of Phase 1 testing was to observe the effects of the glass on the hardware, and vise versa. The Phase 1 cold pours tested three hardware configurations. All three configurations consisted of fully equipped DWPF canisters (i.e. internal rack and full
compliment of magazines and cans). Three rack designs, eight magazine designs, and
two lateral latching configurations were tested in the Phase 1 pours. Each rack carried
seven magazines, and each magazine held four cans. All internal hardware (rack,
magazines, and cans) was made of 304L stainless steel. The cans were loaded with either
non-radioactive titanate-based ceramic pucks (fabricated by LLNL), ceramic surrogate
logs, or stainless steel bars. The ceramic pucks could not be used exclusively because not
enough were available in time for the test. Therefore ceramic logs (Harbison-Walker
Aurex 90 chrome-alumina brick) were used because their thermal properties were similar
to the ceramic pucks. These ceramic logs were lighter than the pucks, therefore stainless
steel bars were installed in appropriate can locations to simulate the effects of a full
weight magazine. For these tests, the racks were configured with four different magazine
types. Three of the magazine types were arranged in pairs (taking up six positions) and a
fourth type was placed in the seventh position. Magazine pairing was done to observe
glass flow between like magazine types. Finally, two canister assemblies were filled with
simulated DWPF waste glass. Typical magazine and rack designs are shown in Figures 1
and 2.

**Test Results**

Phase 1 test results consist of temperature measurements, observation of glass flow, and
hardware deformation measurements.

**Temperature Measurements**

One of the three test configurations was instrumented (23 thermocouples, digital video
camera, and scale). Both glass and metal temperatures were measured at various heights
and radial locations. Figure 3 shows glass temperatures at various heights, measured
roughly 6'' from the center of the canister. This figure gives a good indication of maximum glass temperatures inside the canister. Can temperatures were also measured, and Figure 4 shows temperature data taken from the can OD on the inboard side. This temperature reading is an important parameter in determining can material strength and internal pressure. Preliminary modeling showed that temperatures must exceed 1100C to affect can structural integrity. As shown in Figure 4, can temperatures stayed below 900C.

Glass Flow
Digital video recorded during the pour and post-test destructive analysis were used to assess glass flow.

A video recording taken during the pour provided larger-scale visual information on glass flow phenomena. Frames from that recording are shown in Figures 5 and 6. Figure 5 shows the pour just beginning. Figure 6 was taken at a glass height of approximately 6'', and glass can be seen flowing over the rack’s lower plate. No voiding or premature glass freezing was observed.

Post-test destructive analysis consisted of making radial cuts at different elevations through each of the test canisters using either a diamond wire saw or large band saw. These cuts exposed glass and metal cross-sections for inspection. Figure 7 shows a typical cutaway. Figure 8 is a closer look at a magazine and can. A visual examination verified that the simulated waste glass filled small crevices in the magazine and completely filled the annular spaces between the magazines and cans, indicating good glass flow.
Hardware Deformation Measurements

In addition to thermal and glass flow data, spatial measurements of canister hardware were made. Dimensions such as magazine OD, can OD, support rod OD, and support rod spacing were taken at each of the exposed cut faces. These measurements verified that the CIC hardware did not experience measurable plastic deformation during the pour or later as the glass cooled.

Conclusions

Favorable results were achieved in the PIP Phase 1 cold pour test program. No voiding was observed, and glass appeared to have filled all spaces in the canister including small crevices between steel parts. No measurable plastic deformation was observed in any of the CIC hardware.
Figure 3: Glass temperatures at various heights (height measured from canister bottom).

Figure 4: Can temperatures at various heights (height measured from canister bottom).
Figure 5: Glass pour video (beginning of pour).

Figure 6: Glass pour video (fill height ~6").
Figure 7: Typical canister cutaway.

Figure 8: Close-up of magazine and can.