

Characterization and Decant of Tank 42H Sludge Sample ESP-200

by

M. S. Hay

Westinghouse Savannah River Company

Savannah River Site

Aiken, South Carolina 29808

N. E. Bibler

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Westinghouse Savannah River Company
Savannah River Technology Company
Aiken, SC 29808

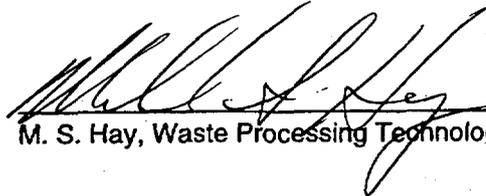


SAVANNAH RIVER SITE

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Authors


M. S. Hay, Waste Processing Technology 6/12/98
Date


N. E. Bibler, Immobilization Technology Section 6/12/98
Date

Design Check


D. D. Walker, Waste Processing Technology 6/12/98
Date

Approvals/Review


S. D. Fink, Level 4 Manager, Waste Processing Technology 6/12/98
Date


W. L. Tamosaitis, Level 3 Manager, Waste Processing Technology 6/12/98
Date

Summary

DWPF Engineering requested that the Savannah River Technology Center (SRTC) provide a demonstration of the DWPF flowsheet on sludge from Tank 42H in the Shielded Cell facility. A 5 liter sample of the Tank 42H sludge (ESP-200), obtained with the tank contents fully mixed, arrived at SRTC on January 20, 1998. This report details receipt of the 5 Liter sample at SRTC, the decant of the sample, and the characterization of the pre- and post-decant Tank 42H sludge.

Evaluation of the measured composition of the supernate indicates Sample ESP-200 became diluted approximately 20% by volume prior to receipt. This dilution complicates the relationship of the characterization of Post-Decant ESP-200 to the current contents of Tank 42H. For the purposes of modeling the current tank contents of Tank 42H, this report provides an estimated composition based on analytical data of recent samples from Tank 42H.

Introduction

The Defense Waste Processing Facility (DWPF) currently operates on a Sludge-Only flowsheet with feed from Tank 51H. Less than half of the initial amount of sludge in Tank 51H remains after approximately 2 years of processing. To provide continuous feed to DWPF, future operations will blend sludge from Tank 42H into the sludge remaining in Tank 51H. Before the transfer, Operations will decant excess supernate from the sludge in Tank 42H. DWPF Engineering requested that the Savannah River Technology Center (SRTC) provide a demonstration of the DWPF Sludge-Only flowsheet on sludge from Tank 42H in the Shielded Cell facility.¹ In addition, since the sample was obtained before decanting excess supernate from Tank 42H, DWPF requested the sludge sample be characterized and decanted to closely model expected ESP operations.

For the purpose of the demonstration, a 5 liter sample of the Tank 42H sludge, obtained with the tank contents fully mixed, was sent to SRTC on January 20, 1998. The sample was designated ESP-200. Sample analysis complied with the Task Plan² and Analytical Study Plan.³ The measured composition of the as-received sample and the Sludge Washing Model⁴ allow one to determine the volume of supernate to remove to simulate the expected decant in the Extended Sludge Processing (ESP) facility. After decanting, the resulting sludge was characterized again before starting the demonstration of the DWPF Sludge-Only flowsheet.

This document reports the receipt of the 5 liter sample at SRTC, the decant of the sample, and the determination of the pre- and post-decant compositions of the sample.

Experimental

Analytical Development Section (ADS) performed all analytical measurements with the exception of weight percent solids and density measurements conducted in the Shielded Cells.

Weight Percent Solids Analysis

The weight percent of total solids in the sludge were measured using a conventional drying oven at 100 °C and stainless steel or Teflon beakers. The weight percent of dissolved solids in a sample of the filtered supernate were measured in the same manner. The weight percent insoluble solids and soluble solids in the sludge were calculated from the measurements of the weight percent total solids of the sludge and the weight percent dissolved solids in the supernate. Obtaining the weight percent solids analysis of sludge samples in this manner avoids difficulties associated with reproducibly measuring the insoluble solids directly. Equations 1 and 2 allow calculation of the weight percent of insoluble and soluble solids. The weight percent of soluble solids gives the mass of the dissolved solids in the supernate expressed as a percentage of the mass of the sludge sample. The weight

percent of insoluble solids represents the mass of insoluble solids expressed as a percentage of the mass of the sludge sample.

w_{ds} = weight fraction of dissolved solids (wt dissolved solids/ wt of supernate)
 w_{ts} = weight fraction of total solids (wt total solids/ wt of sludge slurry)
 w_{is} = weight fraction of insoluble solids (wt insoluble solids/ wt of sludge slurry)
 w_{ss} = weight fraction of soluble solids (wt dissolved solids/ wt of sludge slurry)

$$w_{is} = (w_{ts} - w_{ds}) / (1 - w_{ds}) \quad \text{Eq. 1}$$

$$w_{ss} = w_{ts} - w_{is} \quad \text{Eq. 2}$$

A 15 wt % or a 1 wt % NaCl standard solution was measured concurrently during the analysis of the sludge and supernate samples. During the course of these measurements, tests found that a high bias can result from use of aluminum vessels or glass fiber pads when measuring high pH solutions. For this reason, all weight percent solids measurements used stainless steel or Teflon beakers.

Density Measurements

Density measurements were made on both the sludge and the filtered supernate using a pipette tip in with the small end heat-sealed. After heat sealing, these pipette tips provide a reproducible volume of 8.25 mL. The sludge does not wet the pipette tips eliminating problems with entrained air bubbles when filling a narrow cylinder with thick sludge.

Determination of the Calcine Conversion Factor

Two samples of the Post-Decant ESP-200 sludge slurry having known weight were calcined to 1000 °C to allow determination of the conversion factor from a weight percent total dried solids basis to weight percent calcined solids basis. Dividing the previously measured weight percent total dried solids (100 °C) by the weight percent calcined solids (1000 °C) yields the calcine conversion factor. Once can convert the concentration of an element in the sludge expressed as a weight percent of the total dried solids to a weight percent calcine basis by dividing by the calcine conversion factor.

Sample Preparation

A 5 to 10-fold dilution with deionized, distilled water was generally necessary to lower the radiation levels on supernate samples before submittal to ADS for analysis. Dissolution of samples of dried sludge solids were performed in quadruplicate by contacting with aqua-regia or by fusion with sodium peroxide. Contacting the sodium peroxide fusion with nitric acid allows determination of the composition of the total sample. Water uptake of the sodium peroxide fusion was used to determine the total phosphate and sulfate in the sludge. The digested sludge samples were diluted to 250 mL with deionized, distilled water before analysis. Quality control included dissolving a glass standard concurrently with the sludge samples and submitting for analysis. An ICP-ES standard containing 100 mg/L of several metals of interest (nitric acid matrix) also accompanied all samples. The analytical results of the standards indicated complete dissolution methods and accurate analyses.

Analytical Methods

ADS uses the following analytical methods for determination of specific species. Nitrate, nitrite, sulfate, oxalate and phosphate were measured by ion chromatography (IC). Chloride and fluoride were determined by the ion selective electrode (ISE) method. Aluminate, carbonate, and hydroxide were measured using a titration method employing BaCl_2 to precipitate carbonate allowing the determination of all three species. Sodium, aluminum, and iron, as well as other metallic elements, were measured using inductively-coupled plasma-emission spectroscopy (ICP-ES). Potassium and mercury were measured using atomic adsorption spectroscopy (AA) with mercury determined using the cold-vapor technique (CV). Gamma emitting fission products were measured using gamma

spectroscopy. Actinides were determined by a combination of inductively-coupled plasma mass spectrometry (ICP-MS) and alpha counting spectroscopy. Sr^{90} was determined from the beta liquid scintillation counting. Strontium separation was performed on selected samples as necessary.

Preparation of the Decanted Sludge

After mixing the tank containing the 5 liter sample for 1 hour a 2 liter aliquot was pumped into a volume calibrated 3 liter polyethylene bottle. The 2 liters of sludge settled undisturbed. After approximately 2 weeks, the sludge solids settled to approximately 1/2 the total volume of the sample. A pump was used to remove 654 mL of supernate from the settled sludge. The decanted supernate was pumped into a graduated cylinder to allow accurate measurement of the volume of supernate removed. The settled sludge was mixed and a sample removed for analysis. The sample was dried and the total dried solids dissolved in quadruplicate by two methods.

Receipt of the Tank 42H 5 Liter Sample

A 5 liter sample of Tank 42H sludge (sample ID: ESP-200) arrived at SRTC on January 20, 1998. The sample was obtained from Tank 42H after thoroughly mixing the tank and lowering the sampler into the middle of the slurry. Approximately 3 liters of thick slurry resided in the body of the sampler with approximately 2 liters of supernate containing sludge solids found in the secondary container.⁵ Subsequent testing found the sampler contained a leak through a cover plate. A decision was made to combine the two parts of the sample based on the following information.

- Tank Farm personnel involved in the sampling expressed concern that the sampler might be leaking.
- The combined volume of the two fractions of the sample agreed with the volume of sampler body.
- The sample contained in the body of the sampler appeared to have a very thick consistency and the fraction in the secondary container contained a significant amount of sludge solids.

The material in the body of the sampler was emptied into a small stainless steel tank in the Shielded Cells. The material in the secondary container was mixed to suspend the solids and pumped into the same tank. No rinse water was used to remove the sludge from the sampler or the secondary container. Visual inspection of the secondary container found negligible sludge residue remained after the transfer. The volume of sludge removed from the sampler and the secondary container was $4.8 \text{ L} \pm 200 \text{ mL}$. Samples of the supernate and dissolutions of the total dried solids from the combined sludge slurry were sent to ADS for characterization.

Characterization of As Received ESP-200 Slurry Sample

Tables 1 and 2 show the composition of the Pre-Decant ESP-200. Table 1 gives the weight percent solids and density measurements on the Pre-Decant ESP-200. The table also lists the composition of ESP-190, a slurry dip sample obtained in September of 1997, for comparison.⁶ Table 2 provides a comparison of the major components of the supernates and total dried solids from Pre-Decant ESP-200 and ESP-190. (Tables 6 and 7 provide a more detailed analysis for Pre-Decant ESP-200.)

The weight percent dissolved solids data in Table 1 and the supernate compositions in Table 2 indicate dilution of ESP-200 relative to ESP-190. From the supernate data in Table 2, the dilution of ESP-200 appears approximately 20% by volume. Although an error of $\pm 15\%$ exists for analytical measurement on samples from HLW tanks,⁷ the values in ESP-190 supernate prove consistently higher than ESP-200. The dilution value of 20% derives from the average difference in the concentration of the major species in the supernate ($[\text{Na}^+]$, $[\text{NO}_3^-]$, $[\text{NO}_2^-]$, $[\text{OH}^-]$, $[\text{CO}_3^{2-}]$) and the

weight percent dissolved solids for ESP-200 and ESP-190. A slurry dip sample (ESP-199) was obtained from Tank 42H at the same time as the 5 liter sample (ESP-200). The composition of ESP-199 supernate agrees with ESP-190 indicating that ESP-200 has indeed been diluted.⁸ The source of the dilution water remains unknown.

The analytical results on Pre-Decant ESP-200 appear self-consistent. When corrected for dilution, the results from Pre-Decant ESP-200 agree with ESP-190. The anion/cation balance in the supernate exceeds 95%. With the composition of the Pre-Decant ESP-200 established, development of a decant strategy to match the expected decant in ESP proceeded.

Decant Strategy

The development of a decant strategy for sample ESP-200 became more complex due to the inadvertent dilution of the sample. The decant strategy assumed that ESP would decant Tank 42H to a maximum level of 110 inches⁹ and that sample ESP-190 (Sept. 1997 dip sample) provided the best representation of the current composition of the tank.¹⁰ The assumptions seemed reasonable given the supernate compositions from the last three dip samples -- ESP-190, ESP-191 (October of 1997)¹⁰, and ESP-199 (January of 1998) -- from Tank 42H showed good agreement. In addition, the concentration of the major elements of the total dried solids in ESP-190 agreed with a sludge sample obtained from Tank 42H in October of 1992.¹² The target decant level for Tank 42H was 90 to 110 inches.⁸ For the Shielded Cells demonstration, a decant level of 110 inches in Tank 42H was simulated on the basis that the higher tank level (less supernate decanted) introduces conservatism with respect to glass properties and processing.

The Sludge Washing Model was used to estimate the composition of Tank 42H decanted to 110 inches based on a starting composition of sample ESP-190. The decanted composition was then used as the target for decanting the 2 liter aliquot of sample ESP-200 for use in the SRTC demonstration. Table 3 shows the projected composition of Tank 42H decanted to 110 inches based on a starting composition of sample ESP-190.

Compositional differences between samples ESP-190 and ESP-200 presented difficulties in matching the decanted composition of ESP-200 to that estimated for Tank 42H. These differences in the compositions include the following.

- The ~20% dilution of sample ESP-200 results in a lower solids content for a given volume relative to Sample ESP-190.
- Sample ESP-200 has a lower ratio of soluble to insoluble solids than sample ESP-190
- The weight percent insoluble sodium in sample ESP-200 appears lower than sample ESP-190.

Because of the differences in the compositions, the decant strategy sought to provide the same or slightly greater equivalents of components in the slurry that effect key processing parameters in DWPF. These components include species affecting hydrogen generation (i.e., OH⁻, NO₂⁻, NO₃⁻, CO₃²⁻) and glass quality (i.e., Na, Al, Fe).

Based on the analysis of several different decanting scenarios, the best alternative involved decanting the 2 liter aliquot of sample ESP-200 to 1.35 liters. Table 4 shows the projected composition of the decanted material. This composition provides equal or greater base equivalents, nitrate and nitrite equivalents, sodium equivalents, and mass of sludge solids. Due to the extra water in sample ESP-200, a larger volume of the slurry was needed relative to the estimated Tank 42H slurry to provide the same or greater equivalents of important components.

Characterization of Post-Decant ESP-200 Sludge

After decanting the 2 liter aliquot of sample ESP-200 sludge, samples of the supernate and total dried solids were submitted for characterization of both radioactive and non-radioactive species. Tables 5 through 8 list the results of the characterization of the Post-Decant ESP-200 sample. Some of the tables also list the composition of a 25 liter sludge sample of Tank 42H obtained in 1992 for comparison.¹² The 1992 sample was the last Tank 42H sample to undergo a complete characterization. Some tables also provide the composition of the Pre-Decant ESP-200 sludge for reference.

In Table 5, the weight percent total solids of the decanted sludge (16.0 wt %) closely matches the value predicted by the Sludge Washing Model for the decant (16.1 wt %). The small difference in the weight percent dissolved solids of the supernate between the Pre- and Post-Decant sample are attributable to analytical error. Table 5 also gives a calcine conversion factor. The calcine conversion factor resulted from drying a sample of Post-Decant ESP-200 to 1000 °C. The ratio of the weight percent calcined solids to the weight percent total dried solids yields a calcine conversion factor. One can convert the concentration of an element in the sludge expressed as a weight percent of the total dried solids to a weight percent calcine basis by multiplying by the calcine conversion factor.

Theoretically, the supernate compositions of the Pre-Decant and Post-Decant ESP-200 sludge listed in Table 6 should equate. The differences prove small and attributable to analytical error.

The composition of the total dried solids in the Post-Decant ESP-200, listed in Table 7 and 8, agrees with previous measurements from the 1992 sludge sample and with the measured Pre-Decant ESP-200 composition. As expected after decanting, insoluble species show a slight increase in concentration due to the removal of soluble salt.

The total phosphate and total sulfate were also measured in the Post-Decant ESP-200. The results indicate that essentially all of the sulfate is soluble with all of the phosphate insoluble. The phosphate and sulfate results agree with previous analyses made on the 1992 Tank 42H sludge sample.

A portion of the Post-Decant ESP-200 sludge was placed in a filter and washed with a large volume of inhibited water. Table 9 shows the composition of the resulting solids. The weight percent insoluble sodium matches previous measurements of Tank 42H and 51H sludge that found ~3 wt % insoluble sodium. In the far right column of Table 9, the ratio of the weight percent insoluble solids to the weight percent total dried solids equals ~1.15 for most of the species listed. A lower ratio exists for some species indicating some solubility in the wash solutions.

Relationship of Post-Decant ESP-200 to the Current Contents of Tank 42H

The observed dilution of the as received ESP-200 sample obscures the relationship of the characterization of Post-Decant ESP-200 to the current contents of Tank 42H. Also, the decant of the 2 liter aliquot of sample ESP-200 in the Shielded Cells assumed decanting Tank 42H to 110 inches. Operations actually decanted Tank 42H to 100 inches. Fortunately, Tank 42H contains a fairly dilute supernate so the removal of an extra 10 inches of supernate does not largely alter the bulk sludge composition. The biggest difference in the composition of the Post-Decant ESP-200 and the current contents of Tank 42H involves the weight percent total solids of the slurry due to the dilution of sample ESP-200.

Table 10 shows the estimated composition of Tank 42H assuming a starting composition matching ESP-190 and matching ESP-200 each decanted to 100 inches using the Sludge Washing Model. The third column lists the measured composition of Post-Decant ESP-200 for comparison. The

composition of the ESP-200 case includes adjustment to remove the dilution water. As seen in the table, the decanted compositions of the two cases do not differ markedly from the measured composition of Post-Decant ESP-200 with the exception of weight percent solids values.

Table 11 lists the recommended values for use in estimating the current composition of Tank 42H. The supernate composition should not be changed by decanting the tank. The estimated supernate composition is the result of averaging the compositions of the three previous dip samples (ESP-190, ESP-191, ESP-199) from Tank 42H. Complete supernate analyses were not conducted on all three samples. Therefore, not all of the values are the average of three measurements. For example, the U, Pu, and Sr⁹⁰ were only measured in ESP-191.

The estimated composition of the total dried solids in Table 11 were taken from the measured composition of Post-Decant ESP-200 (Tables 6-8). The weight percent solids and specific gravity of the sludge were taken from the estimated composition of ESP-190 decanted to 100 inches (Table 10).

Quality Assurance

Sample identification within the Shielded Cells conformed with Procedure 2.21, "Radioactive Sample Receiving, Labeling, and Tracking," of the L1 Manual. Laboratory notebooks WSRC-NB-97-00513, WSRC-NB-98--00082, and WSRC-NB-98-00083 record all data from the study.

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Table 1. Results of the Weight Percent Solids and Density Measurements for the Pre-Decant ESP-200 and ESP-190 Tank 42H Sludge Samples.

Species	Pre-Decant ESP-200 Sludge	ESP-190 Sludge*
wt % Dissolved Solids	2.07	2.68
wt % Soluble Solids	1.86	2.39
wt % Insoluble Solids	9.94	10.7
wt % Total Solids	11.8	13.1
Sp. g. (slurry)	1.08	1.09
Sp. g. (supernate)	1.02	1.02

*The values for ESP-190 come from reference 6.

Table 2. Analytical Results of the Pre-Decant ESP-200 and ESP-190 Tank 42H Slurry Sample.

Species		Pre-Decant ESP-200 Slurry	ESP-190 Slurry*
Supernate Analysis			
[NO ₃]	M	0.038 (10)	0.050
[NO ₂]	M	0.18 (8.5)	0.20
[SO ₄ ²⁻]	M	0.007 (12)	0.009
[C ₂ O ₄ ²⁻]	M	0.003 (1.1)	0.004
[CO ₃ ²⁻]	M	0.051 (1.7)	0.064
[AlO ₂]	M	0.003 (4.2)	0.004
[OH] _{free}	M	0.022 (3.1)	0.031
[Cl]	M	0.001 (22)	0.001
[F]	M	0.002 (3.4)	0.003
Na	M	0.38 (0.3)	0.44
Cs ¹³⁷	μCi/mL	2.30 (6.1)	2.88
Total Dried Solids Analysis			
Fe	wt %	20.1 (4.0)	18.4
Na	wt %	7.99 (3.6)	9.41
Al	wt %	7.49 (5.7)	6.97
Mn	wt %	3.46 (3.8)	3.18
Ca	wt %	2.15 (4.3)	2.32
Mg	wt %	1.12 (4.2)	1.06

Value in parenthesis indicates percent relative standard deviation of four or more determinations on aliquots of the same sample. This value provides a measure of the analytical precision and does not account for the sampling uncertainty.

*The values for ESP-190 come from reference 6.

Table 3. Composition of ESP-190 Slurry Dip Sample from Tank 42H and Estimated Composition Decanted to 110 inches.

Species		Measured Composition of ESP-190*	Estimated Composition of ESP-190 Decanted to 110 in.
Na	wt %	9.41	7.36
Fe	wt %	18.4	19.8
Al	wt %	6.97	7.51
Mn	wt %	3.18	3.43
Ca	wt %	2.32	2.50
Mg	wt %	1.06	1.14
Si	wt %	1.20	1.30
P	wt %	0.66	0.71
Ni	wt %	0.37	0.40
Cr	wt %	0.14	0.17
wt % Total Solids		13.1	18.5
wt % Dissolved Solids		2.68	2.68
wt % Insoluble Solids		10.7	16.3
wt % Soluble Solids		2.39	2.15

*The values for ESP-190 come from reference 6.

Table 4. Comparison of the Estimated Decanted Compositions of ESP-200 and ESP-190.

Species		Estimated Composition of ESP-190 Decanted to 110 in.	Estimated Composition of Decanted ESP-200 Sludge*
Na	wt %	7.36	6.06
Fe	wt %	19.8	21.8
Al	wt %	7.51	7.92
Mn	wt %	3.43	3.65
Ca	wt %	2.50	2.28
Mg	wt %	1.14	1.18
Si	wt %	1.30	1.38
P	wt %	0.71	0.85
Ni	wt %	0.40	0.34
Cr	wt %	0.17	0.13
wt % Total Solids		18.5	16.1
wt % Dissolved Solids		2.67	2.07
wt % Insoluble Solids		16.3	14.3
wt % Soluble Solids		2.15	1.72

*ESP-200 decanted to the equivalent of ESP-190 decanted to 110 inches.

Table 5. Results of the Weight Percent Solids and Density Measurements for the Pre-Decant and Post-Decant Tank 42H Sludge Sample ESP-200.

Species	Pre-Decant ESP-200	Post-Decant ESP-200
wt % Dissolved Solids	2.07	2.29
wt % Soluble Solids	1.86	1.97
wt % Insoluble Solids	9.94	14.1
wt % Total Solids	11.8	16.0
Sp. g. (slurry)	1.08	1.13
Sp. g. (supernate)	1.02	1.02
Calcine Conversion Factor*		0.79

*The calcine conversion factor allows converting sludge concentrations from a weight percent total dried solids basis to a weight percent calcined solids basis by multiplying by the calcine conversion factor.

Table 6. Analytical Results of the Pre-Decant and Post-Decant Tank 42H Sludge Supernates of ESP-200.

Species		Pre-Decant ESP-200 Supernate	Post-Decant ESP-200 Supernate
[NO ₃]	M	0.038 (10)	0.043 (1.9)
[NO ₂]	M	0.18 (8.5)	0.16 (4.0)
[SO ₄ ²⁻]	M	0.007 (12)	0.007 (3.7)
[C ₂ O ₄ ²⁻]	M	0.003 (1.1)	0.003 (2.2)
[CO ₃ ²⁻]	M	0.051 (1.7)	0.054 (1.0)
[AlO ₂]	M	0.003 (4.2)	0.002 (1.9)
[OH] _{free}	M	0.022 (3.1)	0.015 (1.3)
[Cl]	M	0.001 (22)	0.001 (22)
[F]	M	0.002 (3.4)	0.002 (5.8)
Na	M	0.38 (0.3)	0.40 (2.0)
K	M	Not Measured	0.001
Fe	mg/L	<1.69	<0.28
Al	mg/L	67 (4.2)	62 (1.9)
Mn	mg/L	<0.25	<0.079
Mg	mg/L	0.82 (33)	<0.064
Cr	mg/L	26.7 (0.3)	27.4 (2.0)
P	mg/L	3.26 (13)	3.43 (4.2)
Hg	mg/L	Not Measured	12.2 (5.0)
Cs ¹³⁷	μCi/mL	2.30 (6.1)	2.23 (1.0)
Sr ⁹⁰	μCi/mL	Not Measured	0.008 (20)
U	mg/L	Not Measured	0.40 (4.3)
Pu	mg/L	Not Measured	Not Detected

Value in parenthesis indicates percent relative standard deviation of four or more determinations on aliquots of the same sample. This value gives a measure of the analytical precision and does not account for the sampling uncertainty.

Table 7. Total Dried Solids Composition of the Pre-Decant and Post-Decant Tank 42H Sludge Sample ESP-200 and the Unwashed Sludge from the 1992 Tank 42H Sludge Sample.

Species		Pre-Decant ESP-200 Sludge	Post-Decant ESP-200 Sludge	1992 Unwashed Tank 42H Sludge*
Fe	wt %	20.1 (4.0)	22.2 (4.6)	21.2 (5.7)
Na	wt %	7.99 (3.6)	6.94 (4.9)	8.52 (2.1)
Al	wt %	7.49 (5.7)	8.04 (3.5)	7.76 (4.6)
U	wt %	Not measured	2.63 (3.7)	2.66 (3.2)
Mn	wt %	3.46 (3.8)	3.82 (3.8)	3.52 (3.1)
Ca	wt %	2.15 (4.3)	2.41 (3.6)	2.20 (5.0)
Mg	wt %	1.12 (4.2)	1.25 (3.9)	1.23 (4.5)
Si	wt %	1.30 (3.4)	1.39 (1.7)	-
Hg	wt %	Not measured	1.26 (4.4)	0.94 (3.9)
P	wt %	0.80 (6.6)	0.90 (3.3)	0.94 (3.3)
Ni	wt %	0.32 (7.4)	0.38 (4.5)	0.34 (5.9)
Cr	wt %	0.12 (9.0)	0.14 (3.8)	0.13 (8.2)
Cd	wt %	0.10 (7.0)	0.11 (5.6)	-
K	wt %	Not measured	<0.1	-
Cu	wt %	0.020 (15)	0.033 (17)	0.027 (2.1)
Ti	wt %	0.013 (13)	0.019 (3.8)	0.016 (5.8)
Pu	wt %	Not measured	0.0085(3.0)	0.0092 (1.2)
Ag	wt %	Not measured	0.036 (5.7)	0.015 (4.4)
Pd	wt %	Not measured	0.0021 (12)	0.0013 (1.1)
Ru	wt %	Not measured	0.021 (4.9)	0.017 (4.7)
Rh	wt %	Not measured	0.0051 (6.1)	0.0041 (5.5)

Table 7. (Continued)

Species		Pre-Decant ESP-200 Sludge	Post-Decant ESP-200 Sludge	1992 Unwashed Tank 42H Sludge*
Sr ⁹⁰	μCi/g	Not measured	4.94E+03 (5.9)	5.63E+03 (2.4)
Cs ¹³⁷	μCi/g	1.84E+02 (3.2)	1.94E+02 (2.5)	1.56E+02 (3.7)
Cm ²⁴⁴	μCi/g	Not measured	5.21E+00 (23)	6.03E+00 (15)
Am ²⁴¹	μCi/g	7.10E+00 (5.6)	7.39E+00 (11)	5.86E+00 (20)
Eu ¹⁵⁴	μCi/g	1.42E+01 (3.4)	1.53E+01 (3.2)	1.62E+01 (2.8)
Eu ¹⁵⁵	μCi/g	2.00E+00 (10)	1.98E+00 (18)	3.12E+00 (8.1)
Co ⁶⁰	μCi/g	8.10E-01 (6.8)	8.62E-01 (2.0)	1.55E+00 (11)
Np ²³⁷	μCi/g	Not measured	1.37E-02 (8.6)	-
Ru ¹⁰⁶	μCi/g	Not measured	<2.6E+00	-
Sb ¹²⁵	μCi/g	Not measured	<1.2E+00	-
Ce ¹⁴⁴	μCi/g	Not measured	<2.3E+00	-
Te ^{125m}	μCi/g	Not measured	<1.2E+00	-
Alpha _{Total}	μCi/g	Not measured	1.09E+02 (2.8)	-
Beta _{Total}	μCi/g	Not measured	1.26E+04 (4.2)	-

* The composition for the 1992 unwashed Tank 42H sludge sample comes from reference 12.

Value in parenthesis indicates percent relative standard deviation of four or more determinations on aliquots of the same sample. This value gives a measure of the analytical precision and does not account for the sampling uncertainty.

Table 8. Uranium and Plutonium Isotopes from Total Dried Solids Analysis of the Post-Decant Tank 42H Sludge Sample ESP-200 and the Unwashed Sludge from the 1992 Tank 42H Sludge Sample.

Isotope		Post-Decant ESP-200 Sludge	1992 Unwashed Tank 42H Sludge*
Isotopic Distribution as Weight Percent of Total Dried Solids			
U ²³³	wt %	3.98E-04 (13)	2.86E-04 (2.0)
U ²³⁴	wt %	4.38E-04 (13)	3.09E-04 (3.2)
U ²³⁵	wt %	1.59E-02 (6.1)	1.48E-02 (2.4)
U ²³⁶	wt %	1.44E-03 (8.0)	1.23E-03 (2.4)
U ²³⁸	wt %	2.62E+00 (3.6)	2.64E+00 (3.2)
U ^{total}	wt %	2.63E+00 (3.7)	2.66E+00 (3.2)
Pu ²³⁸	wt %	5.37E-04 (3.0)	5.14E-04 (11)
Pu ²³⁹	wt %	7.13E-03 (2.8)	7.00E-03 (3.4)
Pu ²⁴⁰	wt %	6.97E-04 (9.9)	5.79E-04 (3.7)
Pu ²⁴¹	wt %	2.90E-05 (4.0)	4.57E-05 (52)
Pu ²⁴²	wt %	7.42E-05 (33)	7.73E-05 (2.6)
Pu ^{total}	wt %	8.47E-03 (3.0)	8.20E-03 (3.4)
Isotopic Distribution as Percent of Total Uranium and Plutonium			
U ²³³		0.015 (9.0)	0.011 (5.0)
U ²³⁴		0.017 (12)	0.012 (6.4)
U ²³⁵		0.60 (2.7)	0.56 (5.5)
U ²³⁶		0.055 (5.0)	0.046 (5.6)
U ²³⁸		99.3 (0.1)	99.4 (0.1)
Pu ²³⁸		6.34 (3.2)	6.27 (12)
Pu ²³⁹		84.2 (0.8)	85.4 (1.1)
Pu ²⁴⁰		8.22 (8.8)	7.06 (1.0)
Pu ²⁴¹		0.35 (3.8)	0.55 (48)
Pu ²⁴²		0.87 (30)	0.94 (2.2)

* The composition for the 1992 unwashed Tank 42H sludge sample comes from reference 12.

Value in parenthesis indicates percent relative standard deviation of four or more determinations on aliquots of the same sample. This value gives a measure of the analytical precision and does not account for the sampling uncertainty.

Table 9. Insoluble Solids* Composition of the Post-Decant Tank 42H Sludge Sample ESP-200.

Species		Post-Decant ESP-200 Sludge Insoluble Solids	Ratio to Post-Decant ESP-200 Sludge Total Dried Solids
Fe	wt %	25.6 (2.3)	1.15
Na	wt %	2.63 (2.2)	0.38
Al	wt %	8.78 (1.6)	1.09
Mn	wt %	4.36 (2.7)	1.14
Ca	wt %	2.74 (2.6)	1.14
Mg	wt %	1.43 (2.7)	1.14
P	wt %	1.01 (2.0)	1.12
Ni	wt %	0.42 (2.3)	1.11
Cr	wt %	0.13 (2.3)	0.93
Cd	wt %	0.13 (2.5)	1.18
Cu	wt %	0.032 (3.9)	0.97
Ti	wt %	0.017 (3.1)	0.90

*The insoluble solids composition results from washing an aliquot of the sludge sample with large volumes of water to remove soluble material.

Value in parenthesis indicates percent relative standard deviation of four or more determinations on aliquots of the same sample. This value gives a measure of the analytical precision and does not account for the sampling uncertainty.

Table 10. Estimated Composition of ESP-190 and Post-Decant ESP-200 decanted to 100 inches Compared with the Measured Composition of Post-Decant ESP-200.

Species		Estimated Composition of ESP-190 Decanted to 100 in.	Estimated Composition of ESP-200 Decanted to 100 in.	Measured Composition of Post-Decant ESP-200
Na	wt %	7.00	5.42	6.94
Fe	wt %	20.1	21.7	22.2
Al	wt %	7.60	8.06	8.04
Mn	wt %	3.47	3.72	3.84
Ca	wt %	2.53	2.32	2.41
Mg	wt %	1.15	1.21	1.25
Si	wt %	1.31	1.40	1.38
P	wt %	0.72	0.86	0.90
Ni	wt %	0.40	0.34	0.38
Cr	wt %	0.17	0.13	0.14
Sp. G. of Supernate	g/mL	1.02	1.02	1.02
Sp. G. of Slurry	g/mL	1.16	1.17	1.13
wt % Total Solids		19.9	21.3	16.0
wt % Dissolved Solids		2.67	2.51	2.29
wt % Insoluble Solids		17.8	19.3	14.1
wt % Soluble Solids		2.10	1.94	1.97

Table 11. Estimated Current Composition of Tank 42H Sludge Decanted to 100 inches.

Estimated Composition of Tank 42H Sludge Decanted to 100 inches		
Species		
Supernate*		
[NO ₃]	M	0.052
[NO ₂]	M	0.21
[SO ₄ ²⁻]	M	0.009
[PO ₄ ³⁻]	M	0.0001
[C ₂ O ₄ ²⁻]	M	0.003
[CO ₃ ²⁻]	M	0.065
[AlO ₂]	M	0.003
[OH] _{free}	M	0.022
[Cl]	M	0.001
[F]	M	0.003
Na	M	0.45
Cr	mg/L	29.8
Hg	mg/L	2.6
U	mg/L	0.4
Pu	mg/L	0.0005
Cs ¹³⁷	μCi/mL	2.97
Sr ⁹⁰	μCi/mL	0.008
Sp. g.	g/mL	1.02
Wt % Dissolved Solids		2.59

*The estimated supernate composition is the average of the supernate compositions from Tank 42H dip samples ESP-190, ESP-191, and ESP-199. Not all analyses were conducted on every sample. For example, U, Pu and Sr⁹⁰ were only measured in ESP-191.

Table 11. (Continued)

Estimated Composition of Tank 42H Sludge Decanted to 100 inches	
Species	
Total Dried Solids**	
Fe	wt % 22.2
Na	wt % 6.94
Al	wt % 8.04
U	wt % 2.63
Mn	wt % 3.82
Ca	wt % 2.41
Mg	wt % 1.25
Si	wt % 1.39
Hg	wt % 1.26
P	wt % 0.90
Ni	wt % 0.38
Cr	wt % 0.14
Cd	wt % 0.11
K	wt % <0.1
Cu	wt % 0.033
Ti	wt % 0.019
Pu	wt % 0.0085
Ag	wt % 0.036
Pd	wt % 0.0021
Ru	wt % 0.021
Rh	wt % 0.0051
Sp. g.	g/mL 1.16
Wt % Total Solids	19.9
Wt % Insoluble Solids	17.8
Wt % Soluble Solids	2.10

Table 11. (Continued)

		Estimated Composition of Tank 42H Sludge Decanted to 100 inches
Species		
Total Dried Solids**		
Sr ⁹⁰	μCi/g	4.94E+03
Cs ¹³⁷	μCi/g	1.94E+02
Cm ²⁴⁴	μCi/g	5.21E+00
Am ²⁴¹	μCi/g	7.39E+00
Eu ¹⁵⁴	μCi/g	1.53E+01
Eu ¹⁵⁵	μCi/g	1.98E+00
Co ⁶⁰	μCi/g	8.62E-01
Np ²³⁷	μCi/g	1.37E-02
Ru ¹⁰⁶	μCi/g	<2.6E+00
Sb ¹²⁵	μCi/g	<1.2E+00
Ce ¹⁴⁴	μCi/g	<2.3E+00
Te ^{125m}	μCi/g	<1.2E+00
Alpha _{Total}	μCi/g	1.09E+02
Beta _{Total}	μCi/g	1.26E+04
U ²³³	wt %	3.98E-04
U ²³⁴	wt %	4.38E-04
U ²³⁵	wt %	1.59E-02
U ²³⁶	wt %	1.44E-03
U ²³⁸	wt %	2.62E+00
U ^{total}	wt %	2.63E+00
Pu ²³⁸	wt %	5.37E-04
Pu ²³⁹	wt %	7.13E-03
Pu ²⁴⁰	wt %	6.97E-04
Pu ²⁴¹	wt %	2.90E-05
Pu ²⁴²	wt %	7.42E-05
Pu ^{total}	wt %	8.47E-03

**The estimated composition of the total dried solids was taken from the measured composition of Post-Decant ESP-200 (Tables 6-8). The weight percent solids and specific gravity of the sludge were taken from estimated composition of ESP-190 decanted to 100 inches (Table 10).

Distribution

M. K. Andrews, 773-A
D. A. Barber, 241-120H
T. E. Britt, 703-H
K. G. Brown, 704-1T
M. C. Chandler, 703-H
A. S. Choi, 704-1T
C. J. Coleman, 773-A
C. L. Crawford, 773-41A
N. R. Davis, 719-4A
W. E. Daniels, 704-1T
R. E. Edwards, 704-25S
H. H. Elder, 704-S
T. L. Fellingner, 773-A
S. D. Fink, 773-A
C. R. Goetzman, 773-A
J. R. Harbor, 773-43A
J. R. Hester, 703-H
D. T. Hobbs, 773-A
E. W. Holtzscheiter, 773-A
R. A. Jacobs, 704T
M. D. Johnson, 703-H
D. P. Lambert, 704-1T
L. F. Landon, 704-T
E. D. Lee, 241-152H
B. L. Lewis, 703-H
T. J. Lex, 703-H
S. L. Marra, 704-25S
K. M. Marshall, 773-A
M. S. Miller, 704-56H
J. E. Occhipinti, 704-27S
J. F. Ortaldo, 704-S
T. L. Ortner, 241-152H
S. F. Piccolo, 704-3N
M. R. Poirier, 676-T
W. L. Tamosaitis, 773-A
D. D. Walker, 773-A
W. R. Wilmarth, 773-42A
WPT-LWG Files, 773-A
TIM(4), 703-43A
Record Administration, 773-52A