Title: Evaluation of Linear Solvers for Oil Reservoir Simulation Problems Part 2: the Fully Implicit Case

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Evaluation of Linear Solvers for Oil Reservoir Simulation Problems
Part 2: The Fully Implicit Case

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Abstract. A previous paper [Joubert/Biswas 1997] contained investigations of linear solver performance for matrices arising from Amoco’s Falcon parallel oil reservoir simulation code using the IMPES formulation. In this companion paper, similar issues are explored for linear solvers applied to matrices arising from more difficult fully implicit problems. The results of numerical experiments are given.

1 Introduction
In [Joubert/Biswas 1997], a wide range of linear solver techniques was tested on a class of model problems simulated using Amoco’s Falcon simulator under the IMPES model. In this companion paper, we perform similar linear solver experiments for fully implicit compositional simulations.

Though IMPES (implicit pressure, explicit saturation) simulations are effective in many practical oilfield situations, more complex fields such as those manifesting complicated phase change behavior require more highly accurate fully implicit simulations.

The matrices which arise from such simulations are significantly more challenging for sparse linear solvers, in particular parallel iterative solvers. The matrices are bordered, with added unknowns to account for well pressures. Furthermore, each grid cell is associated with multiple unknowns, for variables such as pressure, oil, gas and water.

Whereas IMPES matrices are typically nearly symmetric and have good diagonal dominance properties, matrices from fully implicit simulations are typically highly nonsymmetric and not diagonally dominant. These properties make it difficult to solve such problems by iterative methods, and it is commonly necessary to utilize strong preconditioning techniques, such as incomplete factorization methods with options for additional matrix fill-in.

This paper presents comparative results for various linear solvers applied to fully implicit simulations. The methodology follows along similar lines to the previous paper [Joubert/Biswas 1997].

2 Description of the Simulator
The numerical experiments in this paper were performed using the Amoco IGCOMP simulator [Amoco 1992b]. This simulator is a modification of Amoco’s proprietary simulator, GCOMP [Amoco 1992a], [Young/Stephenson 1983]. This serial code has full capabilities for performing fully implicit compositional simulations for structured 3-D grids. This code was used rather than Amoco’s Falcon code [Shiralkar et. al. 1997] because at the time these
experiments were performed, Falcon's fully implicit capabilities were not yet functional. It is expected that similar linear solver performance would be obtained for matrices from Falcon simulations.

3 Description of the Test Problems

Below is a set of sample datasets used with IGCOMP. The datasets were selected to give a range of problem behaviors that might be encountered in fully implicit simulations, including difficult ones. Though most of the datasets have fixed problem size, the "S" dataset has variable problem dimensions, facilitating the possibility of performing scalability studies with the code.

- **FRAC1GN.** This is a 2-d black oil model to simulate a fracture. The model generates matrices of dimension $15 \times 23 \times 1$ times the number of unknowns per grid block. The model has 1 well. The simulation time is 100 days.
- **FRAC35.C.** This is a 3-d implicit black oil model to simulate a fracture. The geometry represents a quarter of a five spot pattern. The model generates matrices of dimension $18 \times 34 \times 2$ times the number of unknowns per grid block. The model has 2 wells. The simulation time is 100 days.
- **GAS.** This is a 3-d gas problem. The model generates matrices of dimension $8 \times 8 \times 2$ times the number of unknowns per grid block. The model has 2 wells. The simulation time is 2800 days.
- **GCONEB.** This is a 2-d coning simulation. The model generates matrices of dimension $1 \times 11 \times 21$ times the number of unknowns per grid block. The model has 1 well. The simulation time is 360 days.
- **S.** This is a 3-d black oil model. The geometry represents a quarter of a five spot pattern. The model is identical to the one used in [Joubert/Biswas 1997] except for a small change to force one of the wells to be implicit for part of the run. The model generates matrices of dimension $8 \times 8 \times 2$ times the number of unknowns per grid block; however, for some studies we will change the grid refinement in order to test scalability of linear solvers. The model has 2 wells. The simulation time is 1000 days.
- **ANTONBO.** This is a 3-d, 5 layer 11x11 5-spot problem. The model generates matrices of dimension $11 \times 11 \times 5$ times the number of unknowns per grid block. The model has 5 wells. The simulation time is 6174 days.
- **ARSHAD.** This case represents the combination of the five adjacent 7-spot patterns with no-flow boundaries around the edge. The model generates matrices of dimension $33 \times 15 \times 6$ times the number of unknowns per grid block. The model has 10 wells. The simulation time is 13140 days.
- **BIGN.** This is a 3-d waterflood model. The model generates matrices of dimension $37 \times 59 \times 6$ times the number of unknowns per grid block. The model has 60 wells. The simulation time is 6909 days.

4 Matrix Properties

In order to get a better understanding of the expected linear solver performance for fully implicit simulations, in this section we examine the properties of the matrices over a simulation run. For this run, the linear systems are solved to a very accurate tolerance, to disallow for any effects of the linear solver on the matrix properties for the run.

In particular, we consider the properties of matrices arising from the "S" dataset. This problem has $8 \times 8 \times 2$ grid blocks and two vertical wells. In the resulting matrix, each well gives rise to one unknown, in addition to the grid unknowns (four per grid cell), and each well is coupled to the grid variables in each block it passes through. The well-well coupling matrix is diagonal (in fact, the identity), and the grid-grid coupling matrix corresponds to a 3-D 7-point finite difference stencil with multiple degrees of freedom per grid block.

Figures 1 and 2 in the Appendix section show basic run information for the simulation. For this and all cases, the x-axis of the graph is the linear solve number. The following observations may be made for this case:
The "Day #" and "Time step size" data indicate that the simulation began at a very small time step size and gradually increased this time step as it was determined by the code that this could be done without loss of accuracy of the simulated solution. The time step also was decreased briefly at the 500 day mark when the injection well was turned on.

Only 1-2 Newton steps were required per time step, until injection was begun, at which time the number of Newtons increased.

The code determines automatically at each time step which wells, if any, must be made implicit.

Figure 3 gives the magnitudes of the largest and smallest entries of different sections of the matrix. Here it is assumed that the matrix is partitioned

\[
\begin{bmatrix}
A_{gg} & A_{gw} \\
A_{wg} & A_{ww}
\end{bmatrix},
\]

where the subscripts \(g\) and \(w\) pertain to the grid and well parts, respectively. The data indicate that \(A_{gg}\) and \(A_{wg}\) contain the entries of largest magnitude. In particular, \(A_{wg}\) becomes large when the water injection begins.

On the other hand, Figure 4 shows the same information for the matrix with a left block diagonal scaling applied, where the blocks are the \(4 \times 4\) diagonal blocks for the grid submatrix. Performing this scaling significantly improves the sizes of the entries of the matrix.

Figures 5 through 8 give the extremal entries of the main \(4 \times 4\)-block main diagonal part of \(A_{gg}\), where the minimum or maximum is taken across all grid cells. It should be noted that the largest entries can be found in the fourth row of the \(4 \times 4\) blocks, corresponding to the pressure equation. This suggests that the CPR or Combinative methods may be effective for these problems. Also, the sizes are large even near the beginning of the run, when the time step is small and the matrix properties would be expected to be well-behaved.

Figures 9 and 10 give similar results for the off-diagonal blocks, which refer to the connections of grid blocks to their neighbors. These entries are considerably smaller in magnitude than the entries of the main diagonal blocks. Also, the entries are small at the beginning of the run when the time step is small. Similar results are given in Figures 11 and 12 for the block diagonal scaled matrix.

Figures 13 through 15 give extremal values pertaining to the connection of the wells to the four grid unknowns, for the unscaled and the scaled matrices. Apparently the largest entries are the connection of the wells to the first of the four grid components in \(A_{wg}\).

Figures 16 through 18 denote diagonal dominance matrix properties for the unscaled and scaled matrices. These figures have to do with \(\max_i \sum_{j \neq i} |a_{ij}|/|a_{ii}|\). This calculation is first performed within the main diagonal grid blocks, then within the grid matrix as a whole, then across the \(A_{gg}/A_{gw}\) submatrix, and finally across the \(A_{wg}/A_{ww}\) submatrix. The results again show that much of the difficulty in these matrices is in the main diagonal blocks, particularly the fourth equation, and can be remedied by a block scaling.

Figures 19 through 21 denote the largest absolute value of any entry in the skew-symmetric part of the matrix, \((A + A^T)/2\). This is given for the diagonal blocks and for the off-diagonal blocks for the unscaled and scaled cases, for the grid submatrix. The results show high nonsymmetry, particularly in the main diagonal blocks, and particularly in the fourth row and column of the main diagonal blocks.

Figures 22 and 23 give similar results for the well-grid part of the skew-symmetric part of the matrix.

The main result of these studies is that most of the difficulty with these matrices seem to come from the diagonal blocks of the grid matrices, and the largest of these entries are those associated with the pressure equation.

5 Performance of Some Basic Iterative Methods

The following is a basic set of experiments with linear solvers applied to the model problems. For these experiments, GMRES(s) is applied, with the maximum allowable number of iterations specified by itsmax=100. These tables give the following information for the simulations:

- The stopping tolerance \(\zeta\), assuming stopping test \(\|Q_Lr^{(n)}\|/\|Q_Lr^{(0)}\| \leq \zeta\), where \(Q_L\) is the left preconditioner, if any.
- The type of preconditioning of the grid matrix, either none, point Jacobi, block Jacobi, or relaxed no-fill ILU preconditioning on the grid matrix.
• Whether the iteration is performed on the Schur complement system $A_{gg} - A_{gw}A_{wu}^{-1}A_{wg}$ or on the original system.

• The number of days of simulation performed.

• The ILU relaxation parameter $\omega$ ($\omega = 0$ gives ILU, $\omega = 1$ gives MILU).

• Whether the preconditioning is applied on the left or the right side. When not specified, the preconditioning is on the left.

• The GMRES restart frequency $s$.

• The total number of time steps in the simulation.

• The number of time steps that were forced to repeat, e.g. due to inaccuracy in the linear solve.

• The total number of linear solves.

• The total number of linear solver iterations for all solves.

• The number of linear solves that iterated to itsmax without indicating convergence according to the stopping test.

• The number of ILU factorizations which incurred a negative pivot.

• Number of negative pivot ILU factorizations which also failed to give convergence in itsmax iterations.

• The flops per unknown per linear solve incurred by the linear solver.

• The flops per unknown per linear solve incurred by the preconditioning setup phase of the linear solves.

• The flops per unknown per linear solve incurred by the preconditioning application phase of the linear solves.
Table 1. S dataset, \(nx \times ny \times nz = 8 \times 8 \times 2\).

We may draw the following conclusions from the runs for dataset S in Table 1, a relatively easy and small problem:

- The simulation problem could be successfully solved by all linear solution techniques. Difficulties occurred (e.g., unconverged linear solves or repeated time steps) due to weak preconditioning, e.g., none or point Jacobi, or a weak convergence tolerance.

- Decreasing the convergence tolerance increased the number of unconverged linear solves but decreased the number of time step repeats. In general, decreasing the tolerance, as could be expected, increased the number of linear solver iterations.

- ILU preconditioning with \(\zeta = 10^{-4}\) was the most efficient solver, by up to about a factor of five. At least block Jacobi preconditioning is necessary in order to give effective solution to these problems.

- In general, it was slightly more efficient to use Schur complement than not to.

- In general, ILU was slightly more efficient than MILU.

- Increasing \(s\) increased the solver robustness but also increased the work required.

Let us now considered some more difficult simulations. The following runs assume \(\zeta = 10^{-6}\).
Table 2. FRAC1GN dataset.

- The problem was too difficult to solve by anything less than ILU/MILU preconditioning.
- Increasing $\omega$ decreased efficiency by as much as a factor of four. $\omega = 1$ is best. Increasing $\omega$ increased the number of negative pivots, unconverted linear solves, and repeated time steps.
- In most cases, right preconditioning was slightly better than left preconditioning.
- For right preconditioning, Schur complement was slightly worse, whereas the opposite was true for left preconditioning.
- $s = 50$ was more efficient than $s = 20$, both in operation counts and linear solve iterations.

Table 3. FRAC35.C dataset.

The following observations can be drawn from the FRAC35.C dataset:
- The problem could be solved only by ILU preconditioning with $\omega = 0$.
- The Schur complement iteration was better than the full system iteration.
- In some cases left preconditioning was more efficient, and in some cases right preconditioning.
- $s = 50$ was more efficient than $s = 20$, both in operation counts and linear solve iterations.

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Table 4. GAS dataset.

The following observations can be drawn from the GAS dataset:
- Block Jacobi and M/ILU preconditionings all performed adequately for this problem. ILU variants with $\omega > 0$ performed worse, sometimes resulting in negative pivots or failure to converge. Block Jacobi took significantly more work but always converged.
- The value of $s$ didn’t matter, presumably because few iterations were required and thus no restarts were performed.
- Schur complement and full system iteration apparently performed equivalently.
- Left preconditioning was slightly better than right preconditioning.
The following observations can be drawn from the GCONEB dataset:

- Only variants of ILU preconditioning were able to solve the linear systems for the whole simulation. $\omega = 0$ performed best, whereas $\omega = 1$ performed much worse.
- The value of $s$ didn’t matter, presumably because few iterations were required and thus no restarts were performed.
- Use of the Schur complement technique was slightly better than solving the full system.
- Left preconditioning was slightly better than right preconditioning.

Table 5. GCONEB dataset.

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The following observations can be drawn from the S dataset data in Table 6:

- Both Block Jacobi and ILU variants were able to solve the problem, though ILU variants were much more efficient. $\omega = 0$ was best.
- Right preconditioning was slightly better than left preconditioning.
- Schur complement iteration was slightly better than full system iteration.
- The value of $s$ didn’t matter, presumably because few iterations were required and thus no restarts were performed.

Table 6. S dataset.

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Table 7. ANTONBO dataset.
Table 8. ARSHAD dataset.

For the ANTONBO and ARSHAD datasets, Schur complement iteration was slightly better than full system iteration, and right preconditioning was slightly better than left preconditioning. ILU with $\omega = 0$ was an effective solution technique.

6 Conclusions

This paper has presented some matrix analyses and linear solver experiments using linear systems from a variety of fully implicit reservoir simulations.

The matrices examined exhibited most of their difficulties in the main diagonal blocks, particularly in the pressure equations. Though block Jacobi preconditioning is not adequate to solve very difficult problems, it does improve the matrices significantly.

It was found that hard problems require a comparatively strong preconditioner such as ILU(0). MILU preconditioning was always worse than ILU preconditioning. Using a higher value of the GMRES restart frequency $s$ such as 50 was better than using a lower value such as 20 for the more difficult problems. In some experiments not reported here, some of the difficult problems required a tighter convergence tolerance of $\zeta = 10^{-6}$ rather than $10^{-4}$ in order to run the simulation in a reasonable time period. There was no clear winner between left and right preconditioning or Schur complement and full system iteration, though there was a general trend that right preconditioning was better and Schur complement iteration was better.

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References


Appendix: Figures
basic run data

Figure 1: Basic run characteristics, dataset S.

Dataset S

Figure 2: Basic run characteristics, dataset S, magnified view.
unscaled matrix extremals

Dataset S

Figure 3: Extremal entries of unscaled matrix, grid/well submatrices.

scaled matrix extremals

Dataset S

Figure 4: Extremal entries of block scaled matrix, grid/well submatrices.
Figure 5: Minimal diagonal block entries.

Figure 6: Minimal diagonal block entries, magnified view.
Figure 6: Maximal diagonal block entries, magnified view.

Dataset 5

Figure 7: Maximal diagonal block entries, unselected max A d (2)}
Dataset S

Figure 9: Minimal off-diagonal block entries, unscaled matrix.

Dataset S

Figure 10: Maximal off-diagonal block entries, unscaled matrix.
Figure 11: Minimal off-diagonal block entries, block scaled matrix.

Figure 12: Maximal off-diagonal block entries, block scaled matrix.
Figure 13: Extremal grid-to-well connections, unscaled matrix.

Figure 14: Extremal grid-to-well connections, block scaled matrix.
Figure 15: Extremal grid-to-well connections, block scaled matrix, magnified view.

Figure 16: Diagonal dominance, unscaled matrix.
Figure 17: Diagonal dominance, block scaled matrix.

Figure 18: Diagonal dominance, block scaled matrix, magnified view.
Figure 19: Extremal magnitudes of skew-symmetric part, block diagonal.

Figure 20: Extremal magnitudes of skew-symmetric part, off-diagonal, unscaled.
Figure 21: Extremal magnitudes of skew-symmetric part, off-diagonal, block scaled.

Figure 22: Extremal magnitudes of skew-symmetric part, grid-well, unscaled.
Figure 23: Extremal magnitudes of skew-symmetric part, grid-well, block scaled.