

**Comment on "Simulation of a Two-Dimensional  
Rayleigh-Bénard System Using the Direct  
Simulation Monte Carlo Method"**

**Alejandro L. Garcia  
Florence Baras  
M. Malek Mansour**

**RECEIVED  
SEP 06 1996  
OSTI**

**June 30, 1994**



This is an informal report intended primarily for internal or limited external distribution. The opinions and conclusions stated are those of the author and may or may not be those of the Laboratory.

Work performed under the auspices of the U.S. Department of Energy by the Lawrence Livermore National Laboratory under Contract W-7405-Eng-48.

**MASTER**

DISTRIBUTION OF THIS DOCUMENT IS UNLIMITED

*ng*

#### DISCLAIMER

This document was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor the University of California nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or the University of California, and shall not be used for advertising or product endorsement purposes.

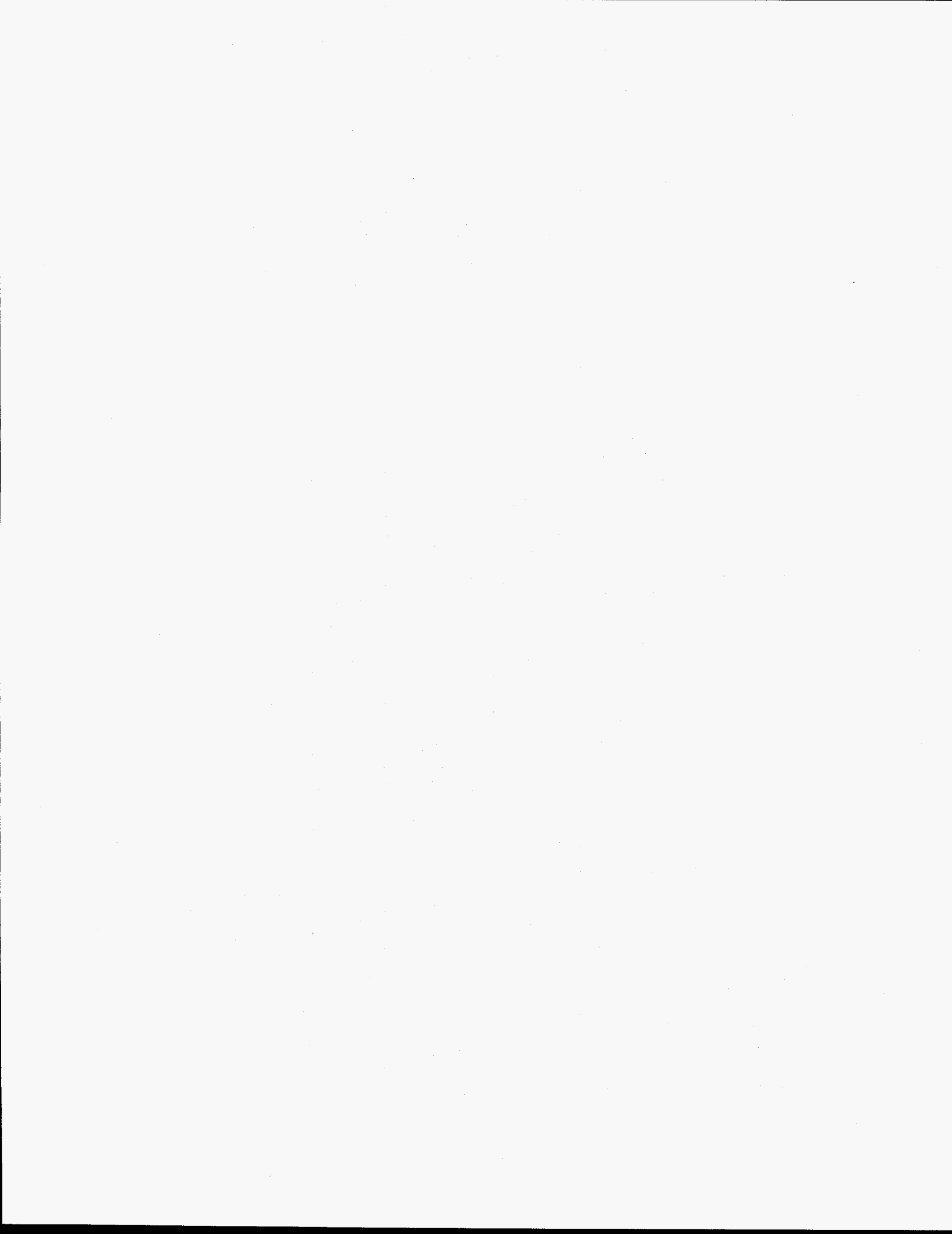
This report has been reproduced  
directly from the best available copy.

Available to DOE and DOE contractors from the  
Office of Scientific and Technical Information  
P.O. Box 62, Oak Ridge, TN 37831  
Prices available from (615) 576-8401, FTS 626-8401

Available to the public from the  
National Technical Information Service  
U.S. Department of Commerce  
5285 Port Royal Rd.,  
Springfield, VA 22161

**DISCLAIMER**

**Portions of this document may be illegible in electronic image products. Images are produced from the best available original document.**



Comment on “Simulation of a two-dimensional  
Rayleigh-Bénard system using  
the direct simulation Monte Carlo method”

Alejandro L. Garcia\*

*Institute for Scientific Computing Research L-416, Lawrence Livermore National Laboratory,  
Livermore, California 94550*

Florence Baras and M. Malek Mansour

*Center for Nonlinear Phenomena and Complex Systems and Faculté des Sciences, Université  
Libre de Bruxelles, Campus Plaine, Code Postal 231, B-1050 Brussels, Belgium*

(June 30, 1994)

Abstract

In a recent paper, Watanabe, *et. al.* [Phys. Rev. E 49 4060 (1994)] used direct simulation Monte Carlo to study Rayleigh-Bénard convection. They reported that, using stress-free boundary conditions, the onset of convection in the simulation occurred at a Rayleigh number much larger than the critical Rayleigh number predicted by linear stability analysis. We show that the source of their discrepancy is their failure to include the temperature jump effect in the calculation of Rayleigh number.

Typeset using REVTeX

The direct simulation Monte Carlo method (DSMC), introduced by G. A. Bird, is a popular numerical scheme for computing rarefied gas flows [1]. The method is particularly useful in the simulation of flows with high Knudsen number (ratio of mean free path to characteristic length), where the conventional Navier-Stokes description of hydrodynamics breaks down. Numerical and experimental tests have confirmed the validity and accuracy of the DSMC algorithm in diverse scenarios [2]. Theoretical studies have also shown the mathematical convergence of DSMC methods to the solution of the fluctuating Boltzmann equation [3].

Consider a fluid confined between horizontal walls held at fixed temperatures  $T_L$  (lower wall) and  $T_U$  (upper wall), with  $T_L > T_U$ . When a critical value of the temperature gradient is exceeded, the purely conductive state becomes unstable and a transition to well structured convective behavior occurs [4]. This transition, known as the Rayleigh-Bénard (RB) instability, is governed by the Rayleigh number,  $Ra$ , defined as:

$$Ra = \frac{\alpha \Delta T g L^3}{\nu \lambda_T} \quad (1)$$

where  $L$  is the distance between the horizontal boundaries,  $g$  the gravitational acceleration,  $\Delta T = T_L - T_U$  is the temperature difference,  $\nu$  and  $\lambda_T$  are the kinematic viscosity and thermal diffusivity, respectively, and  $\alpha = -(\partial \log \rho / \partial T)_P$  is the thermal expansion coefficient.

In a recent paper, Watanabe, Kaburaki and Yokokawa [5] discuss DSMC simulations of Rayleigh-Bénard convection in low Knudsen number systems. The study of RB convection using DSMC is not new [6–8] and numerous molecular dynamics (MD) studies have also appeared [9–11]. In their paper, Watanabe, *et. al.* consider two types of boundary conditions for the upper and lower boundaries: fully thermalizing and stress-free conditions. Varying  $\Delta T$ , they found that, for fully thermalizing boundaries, the onset of convection occurs at a Rayleigh number which roughly agrees with linear stability theory (see their Fig. 4). On the other hand, for stress-free boundaries (which they call “semislip”) they found the onset of convection occurring at a significantly higher temperature difference than predicted by theory (see their Fig. 6). They concluded that the “semislip boundary condition, which

has been frequently used in MD and DSMC simulations, was shown to be inadequate to simulate the thermal boundary condition.”

Particle-based simulations of RB convection often use stress-free boundary conditions because convection occurs at a significantly lower Ra than with fully thermalizing boundaries. Since computational costs increase rapidly with Rayleigh number, it is more economical to study RB convection using stress-free boundaries. Furthermore, particle simulations with stress-free boundaries are found to be in excellent agreement with numerical solutions of the Navier-Stokes equations (e.g., see Fig. 6 in [7], Fig. 1 in [8], Figs. 2-5 in [10], and Fig. 7 in [11]). Thus the question arises, why did Watanabe, *et. al.* find disagreement between the linear stability prediction for the critical Ra and their DSMC simulations using stress-free boundaries?

The answer is they neglected to account for “temperature jump” in their calculation of Rayleigh number. It was first pointed out by Maxwell that in a gas with a temperature gradient, the temperature of the gas near a wall does not match the wall’s temperature. This phenomenon is known as temperature jump or temperature slip [12,13]. Specifically, the difference between the temperature of the wall and the temperature of the gas near the wall is  $\delta \nabla_{\perp} T$  where  $\nabla_{\perp} T$  is the temperature gradient normal to the wall. For fully thermalizing boundaries,  $\delta \approx 2\lambda$  where  $\lambda$  is the mean free path in the gas [14]. For stress-free boundaries, where only the normal component of velocity is thermalized, the temperature jump can be significantly larger [15]. In some circumstances (e.g., the onset of explosion in exothermal gas-phase reactions [16]) the temperature jump effect can be dramatic.

For a dilute gas, the density profile in the conduction state goes as  $\rho \propto T^{-c}$  where  $c = 1 - mgL/k\Delta T$ ,  $m$  is the mass of a particle and  $k$  is Boltzmann’s constant. To maintain an approximately constant density, one often fixes the gravity in a simulation as  $g = k\Delta T/mL$  and Watanabe, *et. al.* set  $g$  in this manner. Using the Chapman–Enskog expressions for  $\nu$  and  $\lambda_T$ , we may write the Rayleigh number as

$$\text{Ra} = \frac{256}{125\pi} \left( \frac{\Delta T}{T_0} \right)^2 \left( \frac{L}{\lambda} \right)^2 \quad (2)$$

where  $T_0$  is the mean temperature in the system. From this expression one sees that, keeping all else constant, the Rayleigh number varies quadratically with  $\Delta T$ .

The vertical temperature gradient measured in a DSMC simulation of RB convection using stress-free boundary conditions is shown in Fig. 1. The gas is convecting and the vertical cross-section shown in Fig. 1 is centered on one of the rolls. The system size is  $L = 40\lambda$  and the wall temperatures are  $T_U = 0.5$  and  $T_L = 2.0$ . The important feature to notice is that the temperature gradient in the gas is significantly reduced due to the temperature jump at the walls. For this reason, linear stability analysis using  $\Delta T = T_L - T_U$  will not correctly predict the onset of convection in the simulation. Previous work comparing MD or DSMC simulations to Navier-Stokes solutions *did* account for temperature jump and thus found no discrepancy. Even non-linear stability analysis was shown to give quantitative agreement with hard disk MD simulations of RB convection provided the temperature jump was included in the analysis [11].

For fully thermalizing walls, a temperature jump is present but its magnitude,  $\delta$ , is smaller. In the Watanabe, *et. al.* simulations using this boundary condition, if the critical Rayleigh number was shifted by about 10%, the effect would not be noticeable in their data.

In conclusion, even at relatively low Knudsen numbers, microscopic effects, such as temperature jump, are important in particle simulations of fluids. Great care must be taken when comparing simulation results with continuum theory.

The authors wish to acknowledge helpful discussions with M. Mareschal. This work was performed under the auspices of the U.S. Department of Energy Lawrence Livermore National Laboratory under Contract No. W-7405-ENG-48.



## REFERENCES

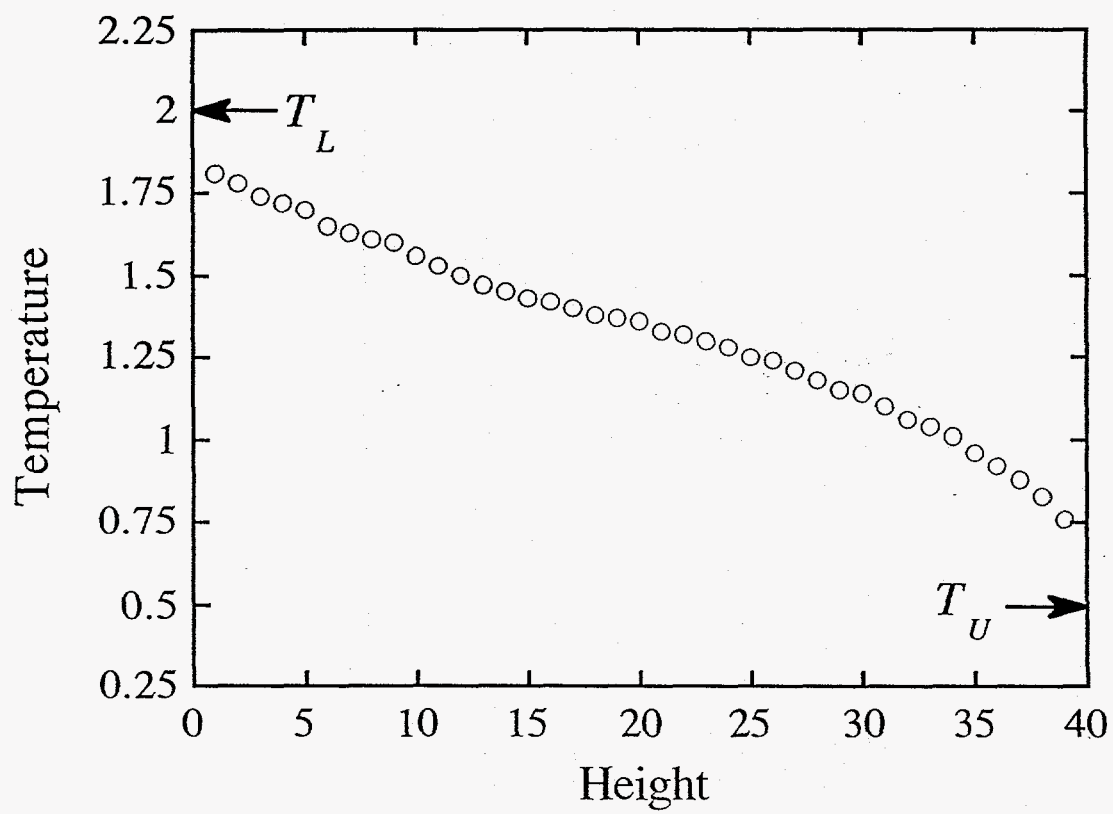
\* Permanent address: Department of Physics, San José State University, San Jose, CA 95192-0106

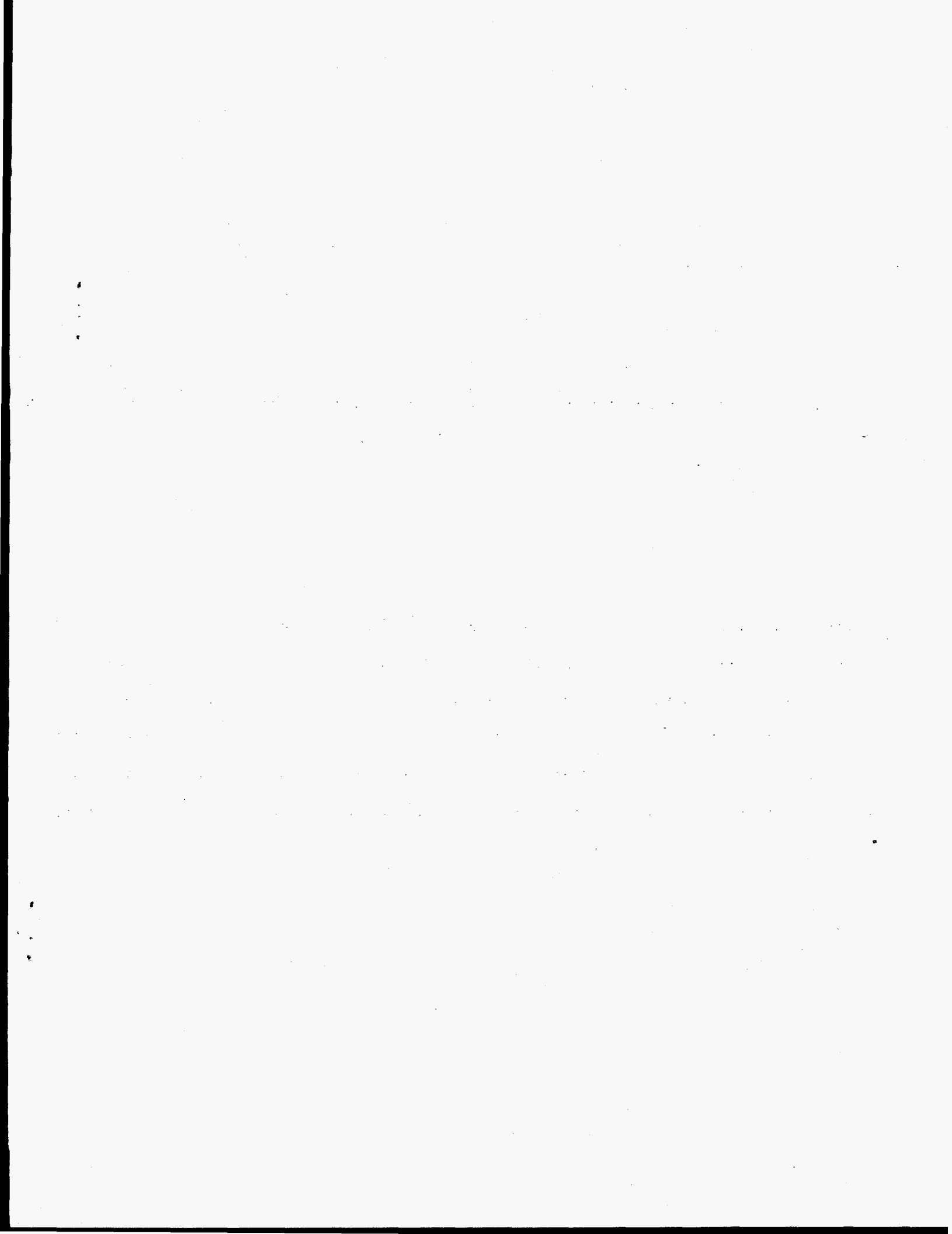
- [1] G. A. Bird, *Molecular Gas Dynamics and the Direct Simulation of Gas Flows* (Clarendon, Oxford, 1994); A. L. Garcia, *Numerical Methods for Physics*, Chapter 10 (Prentice Hall, Englewood Cliffs NJ, 1994).
- [2] E.P. Muntz, *Ann. Rev. Fluid Mech.* **21** 387 (1989); D. A. Erwin, G. C. Pham-Van-Diep and E. P. Muntz, *Phys. Fluids A* **3** 697 (1991); D. L. Morris, L. Hannon and A. L. Garcia, *Phys. Rev. A* **46**, 5279 (1992); E. Salomons and M. Mareschal, *Phys. Rev. Lett.* **69**, 269 (1992); M. Malek Mansour, A. L. Garcia, G. C. Lie and E. Clementi, *Phys. Rev. Lett.* **58**, 874 (1987).
- [3] See, for example, W. Wagner, *J. Stat. Phys.* **66**, 1011 (1992).
- [4] S. Chandrasekhar, *Hydrodynamic and Hydromagnetic Stability* (Dover, New York, 1961).
- [5] T. Watanabe, H. Kaburaki and M. Yokokawa, *Phys. Rev. E* **49** 4060 (1994).
- [6] A. L. Garcia, in *Microscopic Simulations of Complex Flows* (Plenum, New York, 1990), p. 177.
- [7] A. L. Garcia and C. Penland, *J. Stat. Phys.* **64** 1121 (1991).
- [8] F. Baras, M. Malek Mansour and A. L. Garcia, *Phys. Rev. E* **49** 3512 (1994).
- [9] M. Mareschal and E. Kestemont, *Nature*, **329**, 427 (1987); M. Mareschal and E. Kestemont, *J. Stat. Phys.* **48**, 1187 (1987); D. C. Rapaport, *Phys. Rev. Lett.* **60**, 2480 (1988).
- [10] M. Mareschal, M. Malek Mansour, A. Puhl and E. Kestemont, *Phys. Rev. Lett.* **61**, 2550 (1988).
- [11] A. Puhl, M. M. Mansour, and M. Mareschal, *Phys. Rev. A* **40** 1999 (1989).

- [12] J.C. Maxwell, *Philos. Trans. London* **170** 231 (1867); E. H. Kennard, *Kinetic theory of gases* (McGraw-Hill, New York, 1938).
- [13] In a similar effect, called “velocity slip”, the velocity of a gas near a moving wall does not match the wall’s velocity.
- [14] D. C. Wadsworth, *Phys. Fluids A* **5**, 1831 (1993).
- [15] In semistress-free boundaries, the normal component and one of the two parallel components of velocity are thermalized. This boundary condition can be useful if only one direction needs to be stress-free. The temperature jump for a semistress-free boundary is smaller than the jump for a stress-free boundary.
- [16] M. Malek Mansour and F. Baras, *Physica A* **188** 253 (1992).

## FIGURES

FIG. 1. Temperature profile measured in a DSMC simulation for a convecting Rayleigh-Bénard system with stress-free boundaries. Wall temperatures are  $T_L = 2.0$  and  $T_U = 0.5$ ; note that the temperature of the fluid near the wall does not match the wall's temperature.





*Technical Information Department • Lawrence Livermore National Laboratory*  
*University of California • Livermore, California 94551*

