LASNEX Modeling of Target Expansion in the ETA-II Experiment

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We have used the hydrodynamics code LASNEX to model the hydro-expansion of the tantalum target for the ETA-II experiment. The electron beam has kinetic energy of 6 MeV and has a total energy ranges from 720 to 1440 J. The electron beam profile resembles that of a Bennett pinch. The radius for the full-width-at-half-maximum ranges from 1 to 3 mm. For all these parameters, simulations show that the electron beam is able to ablate the central portion of the target. The expansion velocity of the target ranges from about $10^4$ to $5 \times 10^5$ cm/s. The target is hot enough so that the surrounding low-density air is ionized and is expanding at a considerably higher velocity than the target itself. Therefore, care must be taken during the experiment to ensure that the measurement is for the tantalum and not for the ionized air front.

The typical target in the ETA-II experiment is made of tantalum with a density of 16.6 g/cm$^3$ and a thickness of 1 mm. The target is surrounded by low-density air with a density about $1.5 \times 10^6$ torr. The electron beam has kinetic energy of 6 MeV and a current of 2 kA. The pulse has a duration of 60 ns and the total beam energy is about 720 J. In this memo, we simulate the target expansion using the radiation hydrodynamics code LASNEX.

The initial configuration of the mesh is shown in Fig. 1a and the enlarged plot of the mesh near the target is shown in Fig. 1b. In order to speed up the simulation, we only simulate the left-hand-side of the problem. The electron beam is assumed to be coming in from the left and therefore the hydro-expansion is more rapid on the left-hand side. This is because the rate of electron energy deposition decreases with penetration depth. Note that the stopping distance for electrons at 6 MeV in normal density tantalum is a little greater than 2 mm. In Fig. 1, no left and right motion is allowed at the right-hand boundary but the material is allowed to slide up and down along this boundary.

The energy deposition into the target by the electrons is simulated by putting on energy source in the target. The intensity of the source has a radial profile that resembles a Bennett pinch with full-width-at-half-maximum ranges from 1 to 3 mm. The energy source has an intensity that decreases with the depth of the penetration. Since we only model the left-hand-side of the problem, we assume the energy deposited on the left-hand-side is half of the total energy, i.e., 360 J (case I). We then doubled this to 720 J (case II) to investigate the hydro-motion when the electron beam intensity is increased. For both cases I and II, the radius of full-width-at-half-maximum of the Bennett profile is 3 mm. For case I, the spatial energy dependence of the energy source results in radial and axial temperature profiles as shown in Figs. 2a and 2b, respectively, for the time corresponding to the end of the pulse at 60 ns. Using the energy source in the target to model the electron-target interaction is valid.
here since for all the cases simulated here the target does not expand much during the pulse (see Fig. 3).

We ran the problem to 5 \( \mu \)s. Figures 4a, 4b, and 4c, show the target configuration, temperature profile along the axis, and average ionization contours, respectively, for case I at 5 \( \mu \)s. The corresponding plots for case II are shown in Figures 5a, 5b, and 5c. From these plots, we notice that the electron beam is able to ablate the central part of the target since the temperature for vaporization of tantalum is about 5700 K. The average expansion velocity for the target along the axis to the left is about \( 10^4 \) and \( 2 \times 10^4 \) cm/s for cases I and II, respectively. The corresponding distance moved in 5 \( \mu \)s is therefore about 0.5 and 1 mm as shown in Figs. 4a and 5a. Figures 4c and 5c show that the target temperature is sufficiently high so that the surrounding air is ionized. The expansion velocity of the ionized air is considerably higher than that of the tantalum. Figures 4c and 5c show that in 5 \( \mu \)s the ionization front of the air has moved 2 and 3 mm for case I and case II, respectively.

The last simulation (case III) that we have performed is identical to case I except that the Bennett profile of the energy deposition is more peaked at the center (radius at full-width-at-half-maximum is about 1 mm vs 3 mm for case I). The resultant radial temperature profile near the target surface at the end of the pulse is therefore also more peaked at the center as shown in Fig. 6. The higher temperature along the axis results in a higher expansion velocity of the air and the target. As a consequence, the expansion of the air and the target shown in Fig. 7a at 0.3 \( \mu \)s is already greater than that for case I at 50 \( \mu \)s shown in Fig. 4c. The temperature along the axis, the average ionization, and the density along the axis for case III at 0.3 \( \mu \)s are shown in Figs. 7b, 7c, and 7d, respectively. The average expansion velocity of the target along the axis is about \( 5 \times 10^4 \) cm/s and the distance moved travelled by the target at 5 \( \mu \)s is about 2 mm. Comparing Figs. 7a and 7c, we note that because of the high temperature, the ionization front of the air moves faster than the front for the hydro-expansion of the air.

Note that the peak temperatures shown in Fig. 6 for case III is more than five times higher than that for case I. The average expansion velocities for these two cases are, however, not proportional to the square root of the temperature (or, proportional to the sonic velocity -- i.e., the sonic velocity measured at the end of the pulse on the surface of the target along the axis). This is because in case I, although the maximum temperature at the end of the pulse on the surface is slightly above the temperature for vaporization, the temperature drops below the temperature for vaporization just slightly below the surface. In addition, the temperature drops somewhat during the expansion. Therefore, the average expansion velocity for this case is below the sonic velocity. On the other hand, in case III, the temperature along the axis is considerably above the temperature for vaporization and the average expansion velocity is close to the sonic velocity.
Initial Mesh Configuration

direction of electron beam

Fig. 1a
Initial Mesh Configuration near the Target

Fig. 1b
Radial & Axial Temperature Profile
at the End of the Pulse

Case I: Total Energy $720\,\text{J}$,
narrowing of the Bevatron profile at full-width-at-half-maximum
$= 3\,\text{mm}$

Fig. 2a

Fig. 2b
Mesh & Target Configuration at the end of the pulse at 60ns

Case I: Total beam energy = 720 J, full-width at half-maximum = 3 mm

Fig. 3
Target Configuration at 5 μs

Case I:
Total beam energy = 720 J, radius of the Bevelled pinch at full-width at half-maximum = 3.0 mm

Fig. 4a
Temperature along the axis

Fig. 4b

Average ionization $\bar{z}$

Fig. 4c
Target Configuration at 5 ms

Case II

Total beam energy = 1410 J, radius of the beam

Pitch at full-width-at-half-maximum = 3 mm

density g/cm³
Case II

Temperature Along the Axis

Average Ionization

Fig. 5b

Fig. 5c
Radial Temperature at the End of the Pulse

Case III vs Case I

Fig. 6
Target Configuration at 0.3 us density g/cm^3

Case III

Fig 7a