

ANL/ET/CP-70202

# PREPARATION OF ULTRALOW FRICTION SURFACE FILMS ON VANADIUM DIBORIDE\*

A. Erdemir,<sup>#</sup> M. Halter,<sup>+</sup> and G. R. Fenske  
Argonne National Laboratory  
Energy Technology Division  
Argonne, IL 60439

RECEIVED  
OCT 13 1999  
OSTI

August 1996

The submitted manuscript has been authored by a contractor of the U. S. Government under contract No. W-31-109-ENG-38. Accordingly, the U. S. Government retains a nonexclusive, royalty-free license to publish or reproduce the published form of this contribution, or allow others to do so, for U. S. Government purposes.

For presentation at 11th International Conference on Wear of Materials, San Diego, CA, April 21-24, 1997.

\*Work supported by the U.S. Department of Energy under Contract W-31-109-Eng-38.

<sup>#</sup>To whom all correspondence should be sent.

<sup>+</sup> Permanent Address: Purdue University, Department of Materials Engineering, West Lafayette, IN 60515.

## **DISCLAIMER**

**This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, make any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.**

## **DISCLAIMER**

**Portions of this document may be illegible in electronic image products. Images are produced from the best available original document.**

## PREPARATION OF ULTRALOW FRICTION SURFACE FILMS ON VANADIUM DIBORIDE

A. Erdemir, M. Halter, and G. R. Fenske  
Argonne National Laboratory  
Energy Technology Division  
Argonne, IL 60439

### ABSTRACT

In this paper, we present a simple annealing procedure (which we refer to as "flash-annealing" because of short duration) that results in the formation of an ultralow friction surface film on vanadium diboride ( $\text{VB}_2$ ) surfaces. This annealing is done in a box furnace at  $800^\circ\text{C}$  for a period of 5 min. During annealing, the exposed surface of the  $\text{VB}_2$  undergoes oxidation and forms a layer of boron oxide ( $\text{B}_2\text{O}_3$ ). In open air, the  $\text{B}_2\text{O}_3$  layer reacts spontaneously with moisture and forms a boric acid ( $\text{H}_3\text{BO}_3$ ) film. The friction coefficient of a 440C steel pin against this  $\text{H}_3\text{BO}_3$  film is  $\approx 0.05$ , compared to 0.8 against the as-received  $\text{VB}_2$ . Based on Raman spectroscopy and electron microscopy studies, we elucidate the ultralow friction mechanism of the flash-annealed  $\text{VB}_2$  surfaces.

## INTRODUCTION

Many transition metal diborides, i.e.,  $TiB_2$ ,  $ZrB_2$ ,  $VB_2$ , etc. possess exceptional hardness, high elastic modulus, and excellent thermal and electrical conductivity [1,2]. Chemically, most of them are very inert and provide excellent protection against oxidation at elevated temperatures. Some borides (e.g.,  $TiB_2$  and  $ZrB_2$ ) are metallic conductors [2]. Owing to a high elastic modulus and good chemical stability at elevated temperatures,  $TiB_2$  fibers and particulates are used extensively in the production of reinforced ceramic composites [3]. In short, because of their unique thermal, mechanical, electrical, and chemical properties, borides are expected to find increased usage in a variety of industrial applications.

In past years, coatings of transition metal diborides (e.g.,  $TiB_2$ ,  $ZrB_2$  etc.) have been produced by reactive sputtering and chemical vapor deposition on a variety of metalforming dies and machine parts to combat wear [4,5]. Despite their excellent chemical stability and high wear resistance over a wide range of temperatures, most borides cannot afford low friction to dry sliding surfaces. In this paper, we introduce a very simple annealing procedure that results in the formation of a low friction film on the surface of vanadium debarred ( $VB_2$ ). In a series of studies, Bindal and Erdemir [6], and Erdemir et al. [7] used a similar annealing procedure to achieve ultralow friction surface films on borided steels and boron carbide. The annealing procedure of this study results in the formation of a lubricious surface film providing friction coefficients as low as 0.05. The goal of this paper is to elucidate the formation and ultralow friction mechanisms of this surface film on  $VB_2$  surfaces.

## EXPERIMENTAL DETAILS

The  $\text{VB}_2$  material used in our experiments was in the form of a 200  $\mu\text{m}$  thick coating attached to a copper plate by means of explosion bonding. In order to achieve strong adhesion between  $\text{VB}_2$  and copper plate, a layer (50  $\mu\text{m}$  thick) of pure vanadium was first applied onto copper plate again by explosion bonding. The test pieces for tribotesting were in the shape of squares with nominal dimensions of 40 X 40 mm and 6 mm. The surface finish of the test pieces was in the range of 0.2 to 0.3  $\mu\text{m}$  center-line-average (CLA). The annealing of the test pieces was performed in a box furnace at 800°C for 5 min. Specifically, the  $\text{VB}_2$  test pieces were placed on a ceramic plate and inserted into the box furnace at 800°C. After 5 min exposure time, they were taken out of the furnace and cooled to room temperature in open air.

Friction and wear tests were performed in a tribometer with ball-on-disk type contact geometry under a load of 5 N and at room temperature (about 23°C). The relative humidity of the test chamber varied between 38 and 84%. Rotational velocity was 6 to 8  $\text{rev. min}^{-1}$  which translated into a sliding velocity of 5.3  $\text{mm.s}^{-1}$ . The counterface materials were made of 440C steel pins (9.5 mm in diameter). One end of each pin was rounded to a radius of curvature of 127 mm and used as the contact surface. It was polished to a surface finish of 0.01  $\mu\text{m}$  CLA roughness. The sliding distance was 275 m (or 5000 cycles). Before each sliding test and annealing heat - treatment, the ceramic pins and flats were cleaned ultrasonically in acetone and methanol for 300 s each and then oven-dried at 110°C for 10 min. Laser-Raman spectroscopy was used to characterize the structure and chemical nature of the sliding surfaces. The Raman spectroscope used an HeNe laser at 632.8

nm with an output power of 25 mW focused to a spot size of 2 to 3  $\mu\text{m}$ . Duplicate tests were run with flash-annealed  $\text{VB}_2$  surfaces to check the reproducibility of test results.

## RESULTS AND DISCUSSION

Figure 1 shows the variation of friction coefficients of 440C steel pins during sliding against an as-received and flash-annealed  $\text{VB}_2$  sample. The friction coefficient of steel pin is initially 0.15 against  $\text{VB}_2$ , but increases rapidly as sliding continues and reaches a value of 0.8 toward the end of the test. The initially low friction coefficient may have been due to the presence of some surface adsorbates and/or a thin chemical film. As the adsorbed film is removed or worn through, the friction coefficient increases and the frictional trace becomes very unsteady, possibly because of increased metal-to- $\text{VB}_2$  contact and greater stick-slip. In short, the test result confirms that  $\text{VB}_2$  is not a low friction material and cannot provide lubrication under dry sliding conditions. The wear rate of steel pin used against the as-received  $\text{VB}_2$  was  $1.7 \times 10^{-4} \text{ mm}^3 \cdot \text{N}^{-1} \cdot \text{m}^{-1}$ .

The initial friction coefficient of a 440C steel pin sliding against the flash-annealed  $\text{VB}_2$  surface is 0.1, but decreases to 0.05 after about 8000 s and remains constant for the rest of the test. This result confirms that the simple annealing procedure used in our study produces a slippery film on the sliding contact surface of  $\text{VB}_2$ . Also, the frictional behavior of this test pair is very steady and does not show much fluctuation. The wear rate of 440C pin used against the flash-annealed  $\text{VB}_2$  is  $3.5 \times 10^{-6} \text{ mm}^3 \cdot \text{N}^{-1} \cdot \text{m}^{-1}$ . This is nearly 50 times lower than that of the pin slid against the as-received  $\text{VB}_2$ .

In an attempt to elucidate the structural chemistry as well as the fundamental mechanisms of the low friction films on annealed  $\text{VB}_2$  surfaces, we used a Raman spectroscope equipped with an HeNe laser operating at 632.8 nm with an output power of 25 mW focused to a spot size of 2 to 3  $\mu\text{m}$ . The Raman spectrum of the flash-annealed  $\text{VB}_2$  surface revealed two strong Raman bands centered at approximately 498 and 880  $\text{cm}^{-1}$  (see Fig. 2a). We found that these values were very close to those (i.e., 500 and 881  $\text{cm}^{-1}$ ) of the bulk boric acid ( $\text{H}_3\text{BO}_3$ ) reported in Refs. 8 and 9. Furthermore, in previous studies, we have verified that films forming on  $\text{B}_2\text{O}_3$  has a similar  $\text{H}_3\text{BO}_3$  structure [5,6].

In order to better make sure and further verify that the surface reaction film was indeed  $\text{H}_3\text{BO}_3$ , we obtained Raman spectrum of a piece of standard boric acid and have included its spectrum in Fig. 2b for comparison. As is clear, the principal Raman bands of this spectrum match perfectly with those from on the surface of the annealed  $\text{VB}_2$ . Note that the Raman spectrum of as-received  $\text{VB}_2$  is very different from those of the boric acid standard and annealed  $\text{VB}_2$  sample. In short, the low friction behavior of annealed  $\text{VB}_2$  surface (see Fig. 1) must have been closely related to the formation of a thin boric acid film on the exposed surface.

Based on some thermodynamics and kinetics considerations, we can provide some explanation for the formation of lubricious  $\text{H}_3\text{BO}_3$  film on  $\text{VB}_2$  surface. We believe that during exposure to 800°C, the boron atoms within  $\text{VB}_2$  structure gain high mobility and activation energies for diffusion. Those boron atoms reaching the surface can readily react with oxygen in open air to form  $\text{B}_2\text{O}_3$  (e.g., layer 1 in Fig. 3). The standard heat of reaction for  $\text{B}_2\text{O}_3$  formation at 800°C is -290.6



kcal/mol [10], hence the formation of  $B_2O_3$  is thermodynamically favorable at  $800^\circ C$ . As indicated in Ref. 10, V can also readily oxidize at  $800^\circ C$ , and the range of vanadium oxides includes  $V_2O_3$  and  $V_2O_5$ . The standard heats of reaction for  $V_2O_3$  formation is  $-291.5$  kcal/mol and for  $V_2O_5$  formation is  $-362.3$  kcal/mol [10]. During our annealing experiments, we noticed that if we held the  $VB_2$  sample in the furnace for more than 5 min, we would see the formation of some liquidlike islands on the surface. We believe that these islands were primarily composed of vanadium oxides.  $V_2O_5$  melts at  $670^\circ C$  [10].

It is our opinion that  $B_2O_3$  layer forming at  $800^\circ C$  during short duration results from the oxidation of interstitially accommodated boron atoms within the  $VB_2$  structure. The oxidation of  $VB_2$  is also possible at high temperatures (especially when exposure time and/or temperature is higher than 5 min or  $800^\circ C$ ) but as a very stable compound, it will be rather difficult to extract free boron atoms from the highly stable  $VB_2$ . Obviously, the thermodynamics and kinetics of the physical/chemical events taking place at  $800^\circ C$  are rather complex and require more in-depth studies, but in general the short-duration annealing procedure adopted in our study seems to result in  $B_2O_3$  formation.

As illustrated in Fig. 3 and described in detail in Refs. 9 and 11, boron oxide undergoes a secondary reaction with moisture in surrounding air (because of a negative standard heat of reaction). The end product is a thin boric acid film on the upper surface as verified by Raman spectroscopy in Fig. 2.

The ultralow friction mechanism of boric acid film forming on the surface can be explained as

follows. Boric acid has a layered triclinic crystal structure as described in Ref. 12. The atomic layers in its crystal structure are parallel to the basal plane and they are made up of boron, oxygen, and hydrogen atoms. These atoms are closely packed and strongly bonded to each other by covalent, ionic, and hydrogen bonds, whereas the atomic layers are widely spaced (i.e., 0.318 nm) and held together by weak forces, e.g., van der Waals (Fig. 4). In a sense, the layered-crystal structure of boric acid resembles those of  $\text{MoS}_2$ , graphite, and hexagonal boron nitride which are well established as lamellar solid lubricants. Therefore, we believe that the ultralow friction behavior of the flash-annealed  $\text{VB}_2$  surfaces is associated with the formation of a thin boric acid film that has a layered crystal structure. Mechanistically, we propose that under shear forces, atomic layers of boric acid crystal align themselves parallel to the direction of relative motion; once so aligned, they can slide over one another with relative ease to provide the low friction coefficient shown in Fig. 1.

## SUMMARY

In this study, we demonstrated that ultralow friction coefficients can be achieved on  $\text{VB}_2$  surfaces after short-duration annealing. We believe that the sequential formation of first a boric oxide layer during annealing at  $800^\circ\text{C}$  and then a boric acid film during cooling on  $\text{VB}_2$  surface are the main reason for low friction properties. The boric acid film formed on the surface has a layered crystal structure. Boron, oxygen, and hydrogen atoms making up the layers are closely packed and strongly bonded to each other, while the layers themselves are relatively apart and bonded together with weak van der Waals forces. When present at a sliding surface, the layers can shear

easily, thus providing low friction. The findings of this study suggest that other transition metal diborides, such as  $TiB_2$  and  $ZrB_2$  can also be made slippery by performing a similar annealing procedure at elevated temperatures.

#### ACKNOWLEDGMENTS

This work was supported by the U.S. Department of Energy under Contract W-31-109-Eng-38.

#### REFERENCES

1. Boron, Metallo-boron Compounds and Boranes, R. M. Adams, Interscience Publ., New York, 1964, pp. 335-364.
2. R. A. Cutler, Engineering Properties of Borides, Engineered Materials Handbook Vol. 4, Ceramics and Glasses, S. J. Schneider, Jr., (Ed, chairman), ASM International, Metals Park, OH., 1991, pp. 787-803
3. C. H. McMurtry, W. D. G. Boecker, S. G. Seshadry, J. S. Zanghi, and J. E. Garnier, "Microstructure and Material Properties of SiC- $TiB_2$  Particulate Composites," Ceram. Bull., 66(1987) pp. 325-329
4. W. Herr, B. Matthes, E. Broszeit, and K. H. Kloos, "Fundamental properties of wear resistance of r.f. sputtered  $TiB_2$  and Ti(B,N) coatings," Mat. Sci. Eng., A140(1991) pp. 616-624.

5. H. Deng, J. Chen, R. B. Inturi, J. A. Barnard, "Structure, mechanical and Tribological properties of d.c. magnetron sputtered  $TiB_2$  and  $TiB_2(N)$  thin films, Surf. Coat. Technol., 76-77(1995) pp. 609-614.
6. C. Bindal and A. Erdemir, "Ultralow friction behavior of borided steel surfaces after flash annealing," Appl. Phys. Lett., 68 (1996), pp. 923-925.
7. A. Erdemir, C. Bindal, and G. R. Fenske, "Formation of ultralow friction surface films on boron carbide," Appl. Phys. Lett., 68 (1996), pp. 1637-1639.
8. R. Janda and G. Heller, "IR- und Ramanspectren isotop markerter Tetra- und Pentaborate," Spectrochim. Acta, A., 36, 997 (1981).
9. A. Erdemir, G. R. Fenske, and R. A. Erck, "A Study of the Formation and Self-lubricating Mechanisms of Boric Acid Films on Boric Oxide Coatings," Surf. Coat. Technol., Volume 43/44 (1990) pp. 588-596.
10. C. E. Wicks and F. E. Block, "Thermodynamic Properties of 65 Elements-Their Oxides, Halides, Carbides, and Nitrides," U.S. Bureau of Mines, Bulletin # 605, pages 22 and 131 (1963).
11. A. Erdemir, G. R. Fenske, R. A. Erck, F. A. Nichols, and D. E. Busch, "Tribological Properties of Boric Acid and Boric-Acid-Forming Surfaces. Part II. Mechanisms of Formation and Self-Lubrication of Boric Acid Films on Boron- and Boric Oxide-Containing Surfaces," Lubr. Eng., 47 (1991) 179 - 183.
12. A. Erdemir, "Tribological Properties of Boric Acid and Boric-Acid-Forming Surfaces. Part I: Crystal Chemistry and Mechanism of Self-lubrication of Boric Acid," Lubr. Eng., 47 (1991), 168-178.

**FIGURE CAPTIONS:**

Fig. 1. Variation of friction coefficients of 440C steel pins during sliding against as-received and flash-annealed  $\text{VB}_2$ .

Fig. 2. Raman spectra of (a) as-received and flash-annealed  $\text{VB}_2$  and (b) standard  $\text{H}_3\text{BO}_3$  samples.

Fig. 3. Schematic illustration of formation of  $\text{B}_2\text{O}_3$  and  $\text{H}_3\text{BO}_3$  films on  $\text{VB}_2$  surfaces.

Fig. 4. Layered triclinic crystal structure of  $\text{H}_3\text{BO}_3$ .

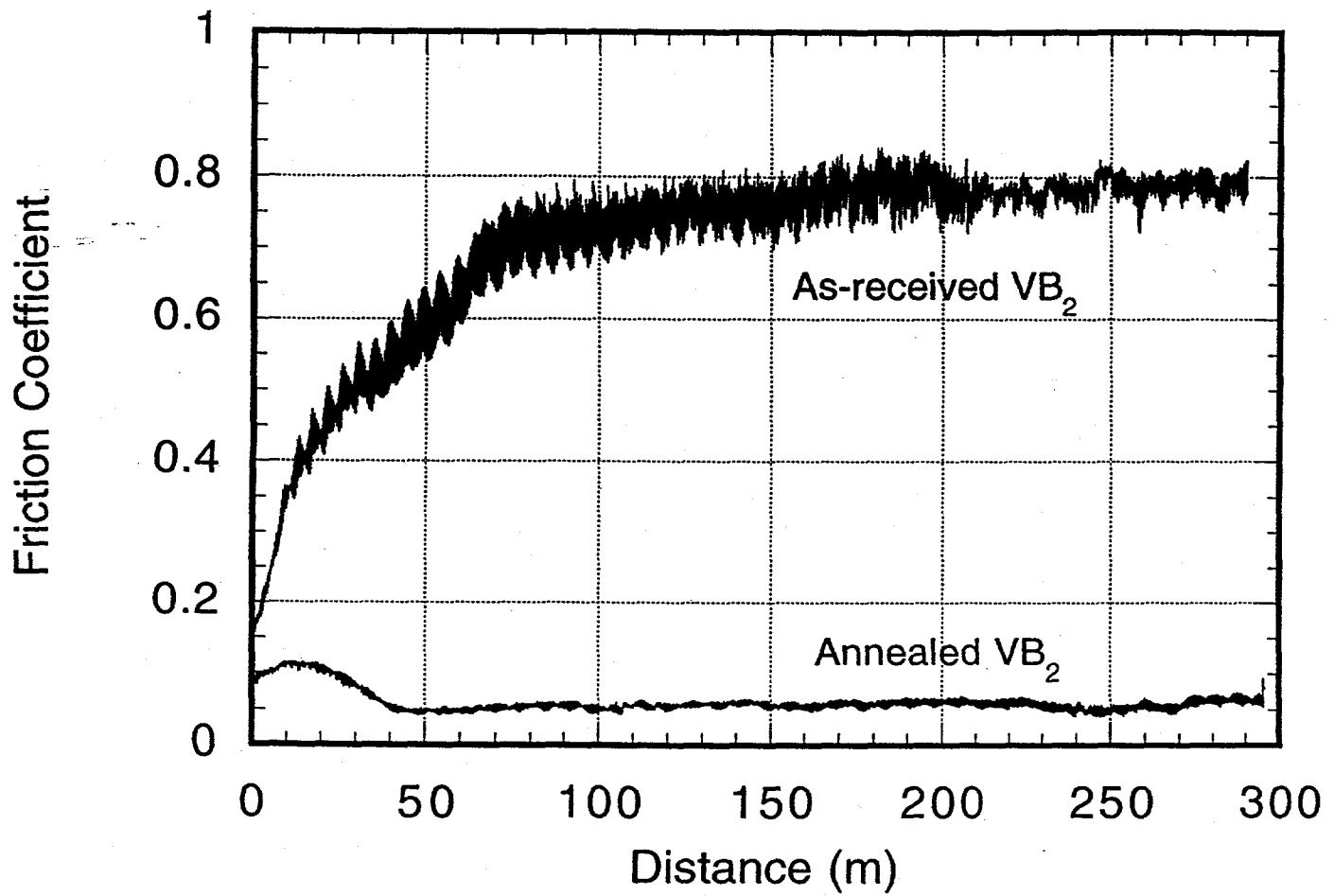
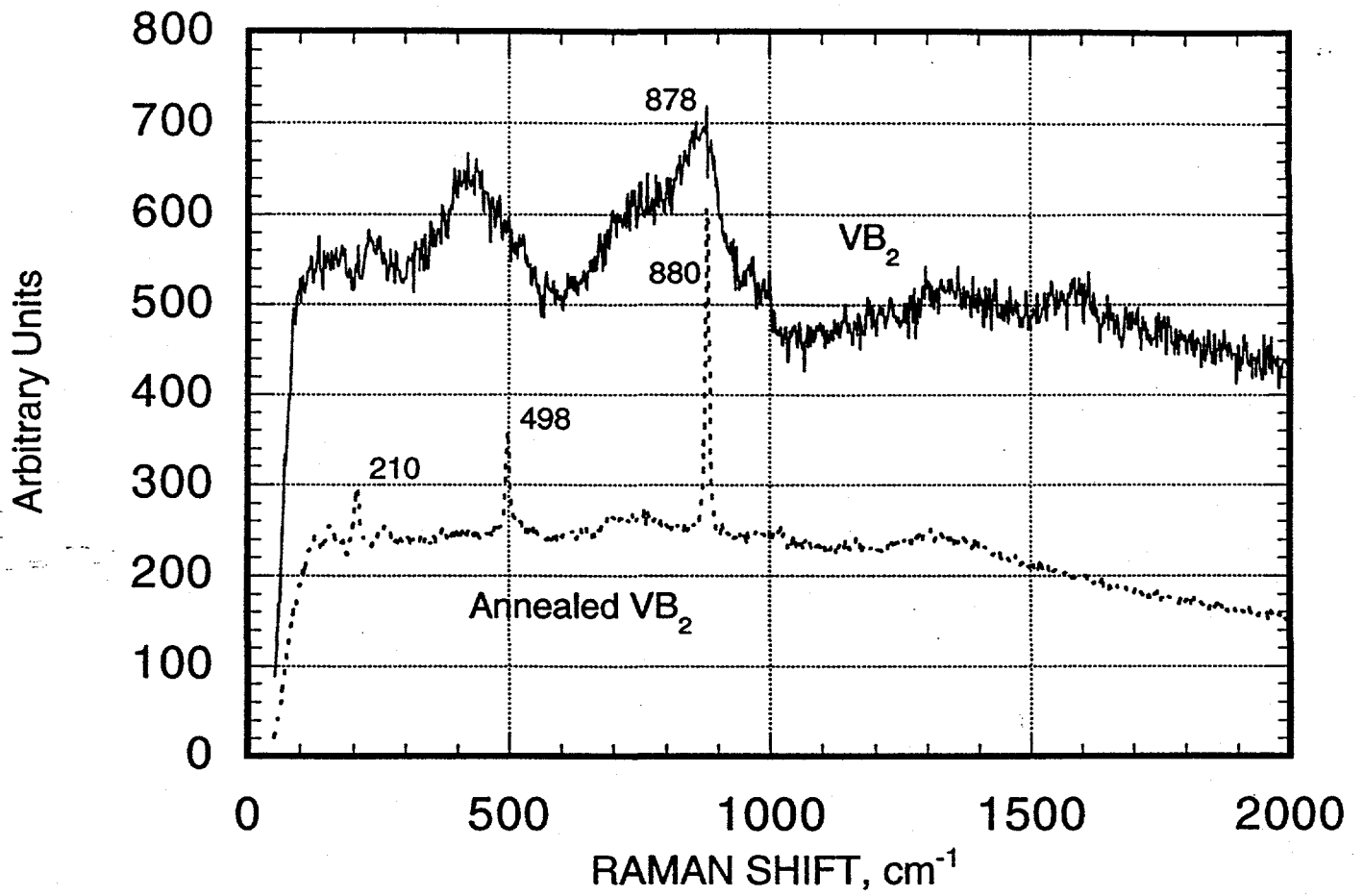
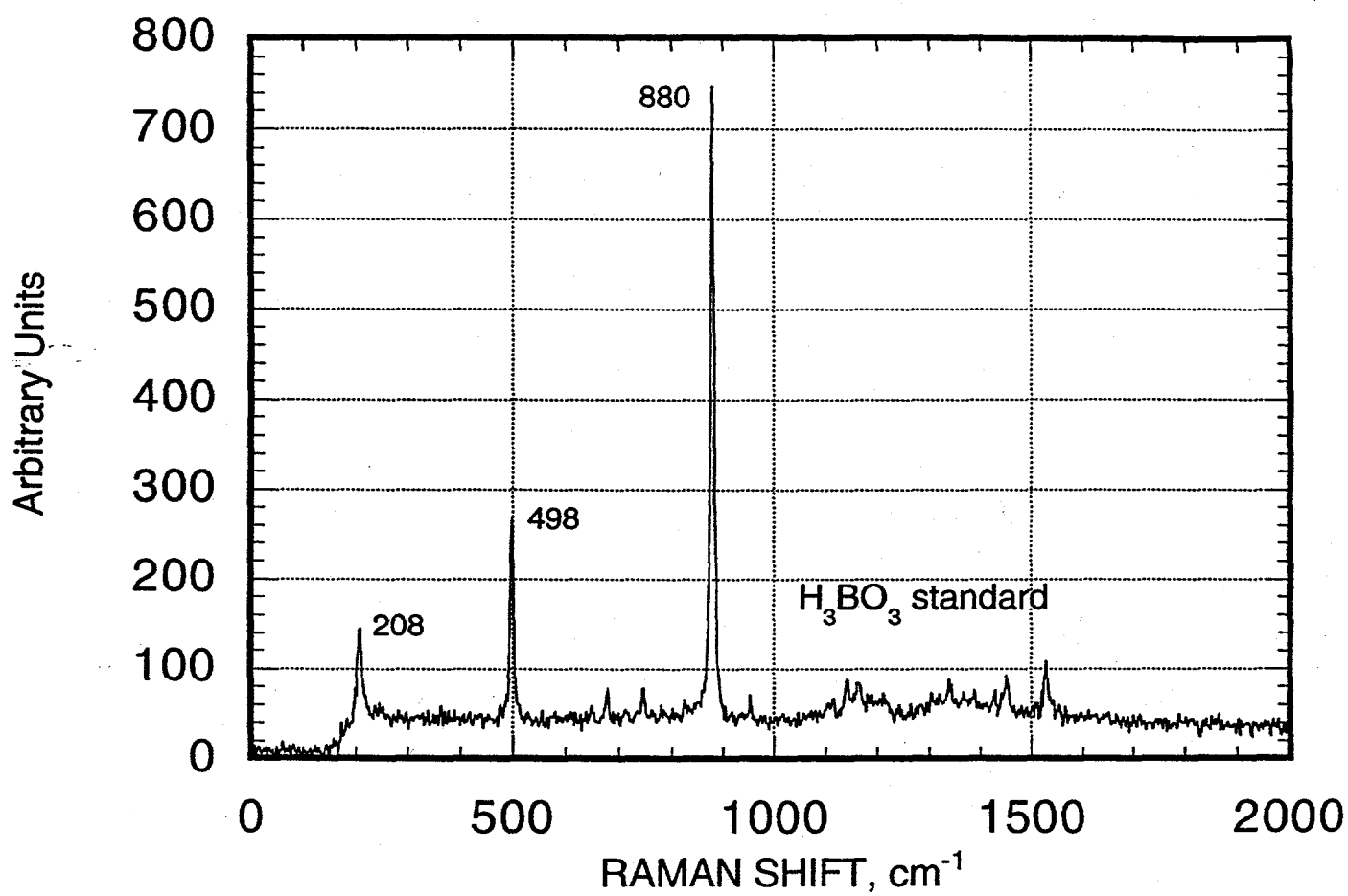


Fig. 1. Variation of friction coefficients of 440C steel pins during sliding against as-received and flash-annealed VB<sub>2</sub>.



(a)



(b)

Fig. 2. Raman spectra of (a) as-received and flash-annealed  $VB_2$  and (b) standard  $H_3BO_3$  samples.



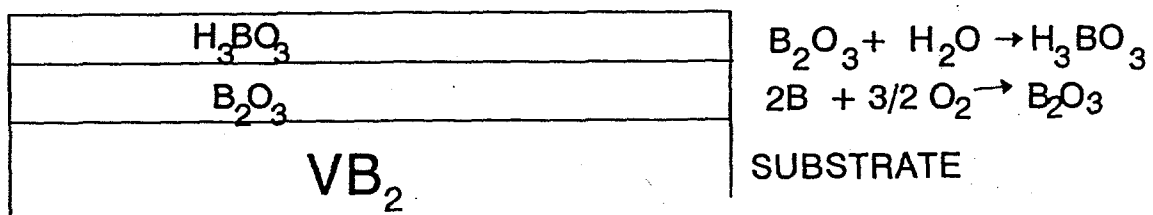
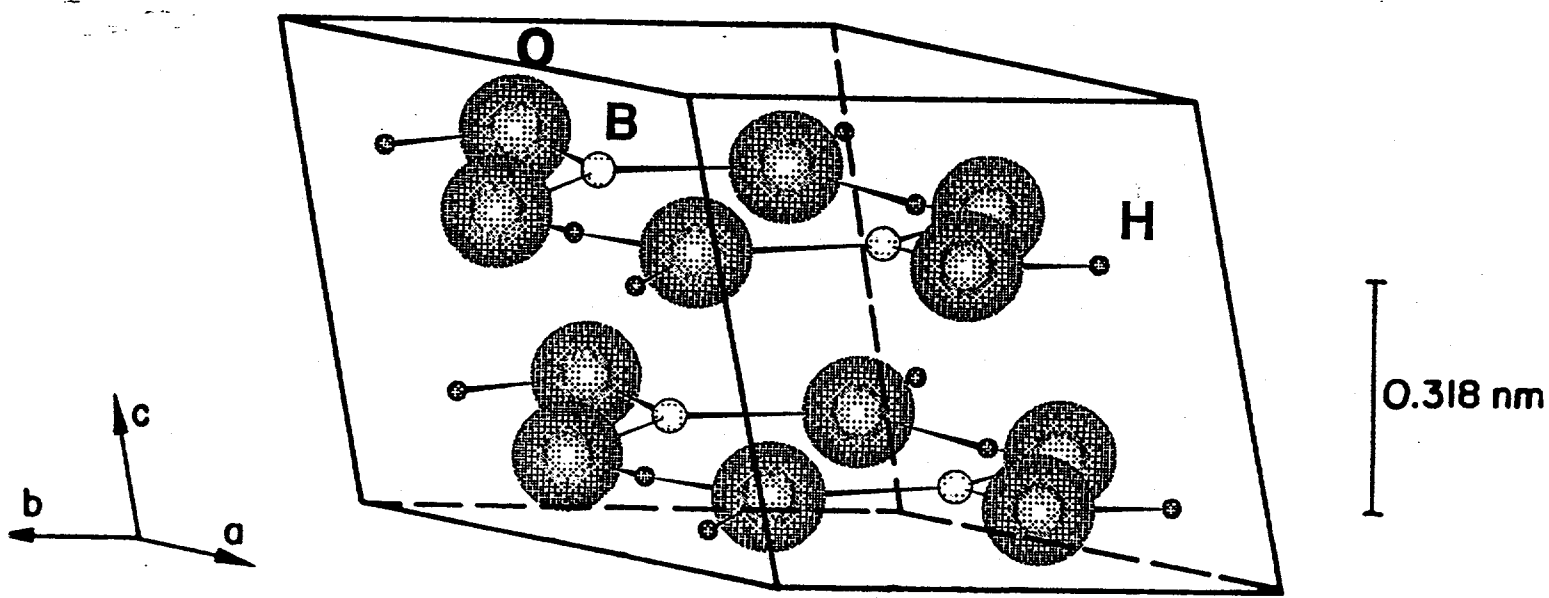


Fig. 3. Schematic illustration of formation of  $B_2O_3$  and  $H_3BO_3$  films on  $VB_2$  surfaces.



INTERLAYER BONDING : van der Waals

$\alpha = 92.58^\circ$	$a = 0.7039 \text{ nm}$
$\beta = 101.17^\circ$	$b = 0.7053 \text{ nm}$
$\gamma = 119.83^\circ$	$c = 0.6578 \text{ nm}$

Fig. 4. Layered triclinic crystal structure of  $\text{H}_3\text{BO}_3$ .