Simultaneous Removal of H$_2$S and NH$_3$ in Coal Gasification Processes

CONTRACT INFORMATION

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OBJECTIVES

The objective of this study is to develop advanced high-temperature coal gas desulfurization mixed-metal oxide sorbents with stable ammonia decomposition materials at 550-800° C (1022-1472° F). The specific objectives of the project are to:

(i) Develop a combined sorbent-catalyst materials shall be capable of removing hydrogen sulfide to less than 20 ppmv and ammonia by at least 90 percent.

(ii) Carry out comparative fixed-bed studies of absorption and regeneration with various formulations of sorbent-catalyst systems and select most promising sorbent-catalyst type.

(iii) Conduct long-term (at least 30 cycles) durability and chemical reactivity in the fixed-bed with the superior sorbent-catalyst.

BACKGROUND INFORMATION

Nitrogen (N$_2$) occurs in coal in the form of tightly bound organic ring compounds, typically at levels of 1 to 2 wt% on a dry-ash-free basis. During coal gasification, this fuel-
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bound nitrogen is released principally as ammonia and nitrogen, with smaller levels of HCN. The formation of \(\text{NH}_3\) in a coal gasification processes is a function of the fuel gas composition and the gasifier operating conditions. During the use of coal gas to generate electricity in gas-fired turbines, fuel bound\(\text{(N}_2\)) is converted to nitrogen oxides\((\text{NO}_x)\), which are difficult to remove and are highly undesirable as atmospheric pollutants. Recent results indicate that while the efficiency of molten carbonate fuel cell (MCFC) anodes is not effected by exposure to \(\text{NH}_3\), \(\text{NO}_x\) is generated during combustion of the anode exhaust gas. Thus, \(\text{NH}_3\) must be removed from the coal gas before it is used in IGCC or MCFC applications.

The product stream from a high temperature, oxygen-blown gasifier, such as Texaco, contains about 2000 ppmv of \(\text{NH}_3\), where higher concentrations (about 5000 ppmv) occur when the gasification is conducted at lower temperatures, such as in the Lurgi or GE air-blown gasifier. A range of 1500 to 3000 ppmv is considered for this study.

Removal of \(\text{H}_2\text{S}\) using zinc-based sorbents, particularly zinc titanate, to < 20 ppmv levels has been well established (Lew et al., 1989; Jothimurugesan and Harrison, 1990; Woods et al., 1990; Gupta and Gangwal, 1993). Previous literature study indicated that catalyst have high activities for \(\text{NH}_3\) decomposition (Krishnan et al., 1988). If desulfurization sorbents such as zinc titanate could be used along with the \(\text{NH}_3\) decomposition catalysts to decompose ammonia present in hot coal gas, then the number of unit processes necessary to clean hot coal gas could be reduced by one.

The objective of this project is to develop successful combination of an \(\text{NH}_3\) decomposition catalyst with the mixed-metal oxide sorbent so that the sorbent-catalyst activity remains stable for \(\text{NH}_3\) decomposition in addition to \(\text{H}_2\text{S}\) removal under cyclic sulfidation-regeneration conditions in the temperature range of 550-800° C (1022-1472° F) and pressures up to 20 atm.
PROJECT DESCRIPTION/RESULTS AND ACCOMPLISHMENTS

The project consists of three major experimental tasks (Tasks 1-3) addressing the contract objectives described above.

Task 1: Sorbent - Catalyst Preparation and Characterization

Task 2: Experimental Testing

Task 3: Cyclic Testing

**Task 2: Experimental Testing**

The activities of the HART 39 and HART40 sorbent-catalysts were tested at 700°C using simulated coal gas. The H$_2$S removal ability is Figures 1&2 and its ammonia decomposition activity is shown in Figures 3&4. Figures 1& 2 shows the H$_2$S breakthrough profiles as a function of time. The pre-breakthrough H$_2$S level was below 100 ppm. Nearly complete sorbent conversion (100%) was observed at breakthrough.

The HART 39 and HART 40 sorbent-catalysts showed moderate catalytic activity (39% average conversion for HART39; 46% average conversion for HART 40)for ammonia decomposition as shown in Figures 3&4.

**FUTURE WORK**

Additional sorbent-catalysts containing Mo and W will be prepared and then it will be tested in the fixed bed reactor.

**REFERENCES**


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HART-39
P=1 atm, S.V. = 2500 h⁻¹
T_s = 700°C (C-1 To C-5), C=Cycle NO
Inlet Gas Molar Composition
H₂S=1%, NH₃=0.18%, H₂=10%, CO₂=5%
CO=15%, H₂O=15%, N₂=Bal
T_{REGEN}=750°C (With N₂/Air=90/10)
t* = 347 min

Figure 1. H₂S Breakthrough Curves in Successive Sulfidation Cycles of Sorbent-Catalyst HART-39
HART-40
P=1 atm, S.V.= 2500 h⁻¹
t₂ = 700°C (C-1 To C-5), C=Cycle NO
Inlet Gas Molar Composition
H₂S=1%, NH₃=0.18%, H₂=10%, CO₂=5%
CO=15%, H₂O=15%, N₂=Bal
T_REGEN=750°C (With N₂/Air=90/10)
t* = 358 min

Figure 2. H₂S Breakthrough Curves in Successive Sulfidation Cycles of Sorbent-Catalyst HART-40
Figure 3. Conversion of ammonia on HART 39 catalyst-sorbents at 700°C.

HART 39
P=1 atm, S.V.= 2500 h⁻¹
Tₜ= 700°C (C-2To C-5), C=Cycle NO
Inlet Gas Molar Composition
H₂S=1%, NH₃=0.18%, H₂=10%, CO₂=5%
CO=15%, H₂O=15%, N₂=Bal
Tᵣₑₜₜₑₜ=750°C (With N₂/Air=90/10)
Figure 4. Conversion of ammonia on HART-40 catalyst-sorbents at 700°C.