A Machine Approach for Field Weakening of Permanent-Magnet Motors

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ABSTRACT
The commonly known technology of field weakening for permanent-magnet (PM) motors is achieved by controlling the direct-axis current component through an inverter. Without using mechanical variation of the air gap, a new machine approach for field weakening of PM machines by direct control of air-gap fluxes is introduced. The demagnetization situation due to field weakening is not an issue with this new method. In fact, the PMs are strengthened at field weakening. The field-weakening ratio can reach 10:1 or higher. This technology is particularly useful for the PM generators and electric vehicle drives.

INTRODUCTION
When a vehicle is cruising at high speed, the required torque is normally low, and the supply voltage to the motor has a certain limit. Therefore, field weakening is an essential requirement for motors used for electric vehicle drive. The field weakening can be obtained easily for an induction motor when its supply frequency is increased without proportionally increasing the motor terminal voltage. On the contrary, from the word "permanent," the motor terminal voltage may not easily be reduced when the supply frequency goes up. The field weakening is not an inherent property of PM motors. Various relatively complex approaches for obtaining field weakening of PM motors exist. For PM generators, if their field can be controlled, the need of using a buck-boost converter to control the generator output voltage measured at the direct current (DC) link and then using the inverter to change back to alternating current could be eliminated.

There are ideas on adjusting the air gap mechanically for field weakening of PM motors, however, their mechanical instability may cause a certain concern. Chan et al. [1] introduced the use of transformer electromotive force (emf) to oppose the rotational emf by purposely producing a slope on the armature current. Certain torque ripples would be generated.

Sebastian and Slemon proposed that with optimum alignment of the stator and magnet fields, maximum torque per ampere is achieved up to a break-point speed [2]. Operation at higher speeds with reduced torque is achieved by adjustment of the current angle to reduce the effective magnet flux (i.e., the equivalent of field weakening).

Sozer and Torrey [3] presented an approach for adaptive control of the surface mount PM motor over its entire speed range. The adaptive flux-weakening scheme is able to determine the right amount of direct-axis current at any operating condition.

Namuduri and Murty [4] focused their discussion on the pulse-width-modulation (PWM) strategy and the microcontroller system that implements the phase-angle control scheme. The authors concluded that though the PM motors were not designed for field weakening by phase-angle control, experiments showed that the torque at no-load speed can be increased significantly with phase advance, at the expense of increased motor losses.

Soong and Miller [5] based their study on the work by Morimoto et al. [6] for the maximum torque field-weakening control. They concluded that the optimal high-saliency interior PM motor design is the most promising for applications requiring a wide field-weakening range.
ION-BEAM-INDUCED DEFECTS AND DEFECT INTERACTIONS IN PEROVSKITE-STRUCTURE TITANATES

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Abstract

Ion-beam irradiation of perovskite structures results in the production and accumulation of defects. Below a critical temperature, irradiation also leads to a crystalline-to-amorphous transformation. The critical temperature for amorphization under 800 keV Kr⁺ ion irradiation is 425, 440 and 550 K for SrTiO₃, CaTiO₃ and BaTiO₃, respectively. The results of ion-channeling studies on SrTiO₃ irradiated with 1.0 MeV Au²⁺ ions suggest that the crystalline-to-amorphous transformation is dominated by the accumulation and interaction of irradiation-induced defects. In SrTiO₃ irradiated with He⁺ and O⁺ ions at 180 K, isochronal annealing studies indicate that there is significant recovery of defects on both the oxygen and cation sublattices between 200 and 400 K. These results suggest that defect recovery processes may control the kinetics of amorphization. A fit of the direct-impact/defect-stimulated model to the data for SrTiO₃ suggests that the kinetics of amorphization are controlled by both a nearly athermal irradiation-assisted recovery process with an activation energy of 0.1 ± 0.05 eV and a thermal defect recovery process with an activation energy of 0.6 ± 0.1 eV. In SrTiO₃ implanted with 40 keV H⁺ to 5.0 x 10¹⁶ and 1.0 x 10¹⁷ ions/cm², annealing at 470 K increases the backscattering yield from Sr and Ti and is mostly likely due to the coalescence of H₂ into bubble nuclei. Annealing at 570 K and higher results in the formation of blisters or large cleaved areas.

1. Introduction

Compounds with the perovskite structure represent a rich class of materials with potential applications ranging from electronic and optoelectronic devices to the immobilization of nuclear wastes. Irradiation with energetic ions can be used to modify the surface and near-surface properties of such materials, introduce new elements and defects, induce phase transformations, and study irradiation effects. Subsequent thermal annealing can lead to full or partial recovery, evolution of new microstructures, and the
determination of activation energies associated with various recovery stages. Consequently, irradiation with energetic ions and subsequent thermal annealing can be used to induce and study a rich set of defects and transformation processes in perovskite structures that could lead to technological advances.

Many oxides with the perovskite structure undergo an irradiation-induced crystalline-to-amorphous phase transition [1-10]; however, the mechanism for this irradiation-induced amorphization has not yet been identified. In several of these studies, thermal annealing was utilized to study the epitaxial regrowth of the ion-beam-induced amorphized layers [1-6,8]. The activation energies for epitaxial regrowth have been determined to be 0.95 and 1.85 eV for SrTiO₃ [4] and CaTiO₃ [8], respectively, in moist (H₂O) atmospheres. In dry atmospheres, the activation energies for epitaxial regrowth have been determined to increase to 1.2 and 3.9 eV for SrTiO₃ [4] and CaTiO₃ [8], respectively. Several perovskite-structure oxides also undergo one or more displacive phase transitions at temperatures below the critical temperature for amorphization; however, no significant effects of this transition on amorphization have been observed [9].

In the present study, the results for ion-beam-induced disordering in CaTiO₃, SrTiO₃, and BaTiO₃ are reviewed, and new results are presented. In addition, the results from thermal annealing of ion-beam-induced damage in SrTiO₃ are reported. Some of these results have been reported previously [9-11].

2. Experimental procedures

As described previously [9], the single crystals of CaTiO₃ and BaTiO₃ used in the studies conducted by Oak Ridge National Laboratory (ORNL) were grown by a flux technique, while the SrTiO₃ single crystals were grown by flame fusion. Specimens for transmission electron microscopy (TEM) were prepared by hand polishing and then ion milling at 77 K with 4 keV Ar⁺ ions. The specimens were irradiated at the HVEM-Tandem facility (i.e., in vacuum) at Argonne National Laboratory (ANL) using either 0.8 MeV Kr⁺ or 0.8 MeV Xe⁺ at an ion flux of 1.7 x 10¹⁴ ions/cm²/s. The irradiation-induced amorphization was monitored in situ, using electron diffraction techniques, as a function of temperature. To facilitate comparisons of dose dependence, the ion fluence for complete amorphization was normalized to an equivalent displacement dose in displacements per atom (dpa) using TRIM 97 and a displacement energy of 25 eV.

The SrTiO₃ single crystals used in the studies at the Pacific Northwest National Laboratory (PNNL) were obtained from Commercial Crystal Laboratories, Inc. and were oriented along the [100] axis. Both the accumulation of disorder and subsequent thermal recovery were followed in situ using 2 MeV He⁺ Rutherford Backscattering Spectroscopy in channeling geometry (RBS/C), as described previously [10]. The single crystals were irradiated at 180 to 200 K with 410 keV He⁺, 400 keV O⁺ or 1.0 MeV Au⁺ ions at an incident angle of 60°, which produced near-surface damage that could be probed by RBS/C methods. The irradiation and in situ ion-beam analysis were carried out using the accelerator facility at the Environmental Molecular Sciences Laboratory at PNNL. Single crystals of SrTiO₃ were also implanted at 120 K with 40 keV H⁺ ions by Implant Sciences Corporation to ion fluences of 5.0 x 10¹⁶ and 1.0 x
Figure 1. Relative disorder at the damage peak in SrTiO\textsubscript{3} irradiated at 200 K with 1.0 MeV Au\textsuperscript{2+} ions. Also shown is a fit of Eq. (1) to the data.

10\textsuperscript{17} ions/cm\textsuperscript{2} [11]. These hydrogen-implanted samples were subsequently characterized and subjected to a thermal annealing study at PNNL. Isochronal annealing on all these samples was performed in situ (i.e., in vacuum) at temperatures ranging from 300 to 870 K for time periods of 20 minutes. After each annealing step, the sample was cooled down, and the RBS/C measurements were performed at 300 K. In the case of the hydrogen-implanted samples, hydrogen nuclear reaction analysis (NRA) was also carried out, using the resonant \textsuperscript{1}H(\textsuperscript{19}F,\textsuperscript{7}Li)\textsuperscript{16}O reaction, to monitor the hydrogen profile. The sample was in random orientation during the hydrogen profile measurements, and Mylar film was used for hydrogen calibration.

3. Results and discussions

3.1. DAMAGE ACCUMULATION

The accumulation of relative disorder as a function of dose (dpa) in SrTiO\textsubscript{3} irradiated at 200 K with 1.0 MeV Au\textsuperscript{2+} ions is shown in Figure 1. The relative disorder shows a very strong sigmoidal dependence on dose, and the results indicate that the random level (or amorphous state) is reached at a dose of about 1.0 dpa. As discussed elsewhere [12], several models of amorphization can be used to describe the sigmoidal behavior shown in Figure 1. One model that has proven useful is the direct-impact/defect-stimulated (DI/DS) model for amorphization [12]. In the absence of any recovery processes, the amorphous fraction, \( f_a \), in this model is given by the following expression:

\[
    f_a = 1 - (\sigma_a + \sigma_0) / (\sigma_a + \sigma_0 \exp[(\sigma_a + \sigma_0)D]), \tag{1}
\]
where $\sigma_d$ and $\sigma_i$ are effective cross sections for direct-impact and defect-stimulated amorphization, respectively, and D is the dose. A fit of this model to the data is shown in Figure 1 and yields a value of about 300 for $\sigma_d/\sigma_i$, which is the largest value of this ratio measured to date in this laboratory. This large value for $\sigma_d/\sigma_i$ indicates the strong dominance of defect accumulation in the amorphization process. At low doses (<0.3 dpa), both amorphization and interstitial defects contribute to the relative disorder, which may explain why the relative disorder is slightly higher than that indicated by the model fit in this dose range.

3.2. DAMAGE RECOVERY

The specimens irradiated with 1.0 MeV Au$^{2+}$ ions (Figure 1) were subsequently annealed at 300 K for 13 hours in order to investigate the amount of recovery for a given level of disorder. The amount of recovered disorder as a function of pre-existing, irradiation-induced disorder is shown in Figure 2 and should be proportional to the relative contribution of interstitial defects to the measured disorder. The results indicate that the maximum recovery probably occurs between 40% and 80% disorder, which is where the product of the crystalline fraction, $1-f_a$, and the concentration of irradiation-induced point defects in the residual crystalline phase reaches a maximum. The relative recovery at a pre-existing disorder of 1.0 decreases with dose, indicating some continued defect contribution to the disorder as it initially reaches the random level.

Single crystals of SrTiO$_3$ were irradiated at 180 K to low doses with 410 keV He$^+$ or 400 keV O$^+$ to produce a partially damaged state (<25% disorder at the damage peak) consisting primarily of point defects. The recovery of defects in these samples was studied by isochronal annealing. The recovery behavior for disorder on the oxygen sublattice at the damage peak is shown in Figure 3 for SrTiO$_3$ irradiated with 400 keV
Figure 3. Isochronal recovery on the oxygen sublattice at the damage peak for SrTiO$_3$ irradiated with 400 keV O$^+$ ions at 180 K.

O$^+$ ions. The results indicate that thermal recovery processes on the oxygen sublattice are complete after annealing at 475 K for this sample and these irradiation conditions. The results also suggest the presence of two recovery stages on the oxygen sublattice, with peak recoveries at about 200 and 300 K, respectively. Based on experimental studies [13,14] the activation energy for migration of oxygen vacancies in single crystal SrTiO$_3$ is on the order of 0.98 to 1.3 eV, and a computer simulation study of defects in SrTiO$_3$ [15] indicates that the oxygen vacancy has a minimum migration energy of 0.65 eV. More recently, computer simulation studies at PNNL indicate that the minimum migration energy for the oxygen interstitial in SrTiO$_3$ is about 0.2 eV, and further computer simulation studies are in progress. These activation energies for migration of point defects on the oxygen sublattice are consistent with the recovery behavior observed in Figure 3.

Thermal recovery of the disorder on the cation sublattice at the damage peak is shown in Figure 4 for SrTiO$_3$ single crystals irradiated with either 410 keV He$^+$ ions or 400 keV O$^+$ ions. The results show a single recovery stage between 200 and 400 K, and gradual recovery at higher temperatures, which is similar to the recovery behavior previously observed in SrTiO$_3$ irradiated with 1.0 MeV Au$^{3+}$ [10] to low ion fluences. Complete recovery on the cation sublattice occurs at temperatures above 900 K. Based on computer simulations [15], the cation vacancy migration energies are 2.52 and 11.6 eV for Sr and Ti, respectively, which suggests these defects are relatively immobile during irradiation and thermal annealing. The results of preliminary computer simulations at PNNL indicate that long-range migration of Sr and Ti interstitials require activation energies of 4.34 and 3.33 eV, respectively; however, short-range migration pathways also exist for Sr and Ti interstitials with activation energies of 0.96 and 0.87 eV, respectively. Such short-range migrations would produce only partial recovery from the recombination of close-pairs, which is consistent with the behavior observed.
in Figure 4. Furthermore, oxygen defects will induce minor displacements of neighboring cations, which will contribute somewhat to the observed disorder on the cation sublattice. Consequently, the recovery of defects on the oxygen sublattice should also relieve some local displacive disorder on the cation sublattice.

3.3. TEMPERATURE DEPENDENCE OF AMORPHIZATION

The temperature dependence of the dose necessary to achieve the amorphous state, as determined by TEM techniques, in SrTiO₃, CaTiO₃, and BaTiO₃ irradiated with 800 keV Kr⁺ ions has been reported previously [9], and the results are summarized in Figure 5. (Note: the dose in Figure 5 has been renormalized based on a displacement energy of 25 eV.) As discussed previously [9], the amorphization dose is not noticeably affected by the displacive phase transition at 108 K in SrTiO₃; in the case of BaTiO₃, however, the displacive phase transition at 393 K results in a minor decrease in amorphization dose with increasing temperature. The critical temperature, Tc, above which the TEM-amorphous state cannot be produced under these irradiation conditions, increases from 425 K for SrTiO₃ to 550 K for BaTiO₃. The critical temperatures are summarized in Table 1, along with the temperature, Tn, for thermal epitaxial recrystallization of amorphous layers in these materials [1,4,8,16]. If a thermal recovery process controls the critical temperature for amorphization, then Tc will generally exceed the temperature at which the thermal recovery process is normally active (in the absence of irradiation) because the rate of thermal recovery must balance the damage production rate [12]. It is clear that thermal epitaxy occurs at temperatures much higher than the critical temperature for amorphization. Consequently, processes other than thermal epitaxy should control the critical temperature for amorphization in these materials. In the case of SrTiO₃, the thermal defect recovery stages that are observed at 300 K for
Figure 5. Temperature dependence of dose to reach TEM amorphous state in SrTiO₃, CaTiO₃, and BaTiO₃ irradiated with 800 keV Kr⁺ (adapted from Meldrum et al. [9])

The dose necessary to achieve the TEM amorphous state in SrTiO₃ irradiated with 800 keV Kr⁺ or 800 keV Xe⁺ ions is shown in Figure 6 as a function of temperature. The amorphization dose in SrTiO₃ is relatively independent of irradiation temperature below 200 K. Above this temperature, the amorphization dose increases with temperature. This onset for an observable effect of temperature on amorphization is consistent with the onset of thermal defect recovery processes in Figures 3 and 4. The temperature dependence of the amorphization dose shows only a weak dependence on the damage-energy density (i.e., ion mass) for these ions and is mostly within experimental error. The critical temperature under Kr⁺ irradiation may be slightly lower (QO K) than under Xe⁺ irradiation, and this is consistent with a slightly lower damage production rate for Kr⁺ relative to Xe⁺. The weak dependence of Tc on damage-energy density in Figure 6 is consistent with the critical temperature being controlled by a

<table>
<thead>
<tr>
<th>Material</th>
<th>Tc (K)</th>
<th>Tr (K)</th>
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<tbody>
<tr>
<td>SrTiO₃</td>
<td>425</td>
<td>575 [1,4]</td>
</tr>
<tr>
<td>CaTiO₃</td>
<td>440</td>
<td>685 [8]</td>
</tr>
<tr>
<td>BaTiO₃</td>
<td>550</td>
<td>&lt;1375 [16]</td>
</tr>
</tbody>
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Figure 6. Temperature dependence of dose to reach the TEM amorphous state in SrTiO$_3$ irradiated with 800 keV Kr$^+$ or 800 keV Xe$^+$ ions.

thermal recovery process, as described previously [12]. However, irradiation with lighter ions (lower energy density) may exhibit a decrease in $T_c$ as irradiation-assisted recovery processes become dominant [12].

A relationship between dose and temperature to achieve a specific amorphous state has been recently derived based on the kinetic direct-impact/defect-stimulated model for amorphization [12], which considers both epitaxial recrystallization, $K_d(T)$, and defect recombination/annihilation, $K_d(T)$, rates. Since epitaxial recrystallization does not appear to play a significant role in the temperature dependence of amorphization in SrTiO$_3$, the dose to achieve a specific amorphous state in this material is given by the expression [12]:

$$D = [D_0 + A \phi \ln(1 - AK_d(T)[1 - \exp(-D_0/\phi A)])] / [1 - AK_d(T)]$$

(2)

where $A = \{ \phi (\sigma_a + \sigma_r) \}^{-1}$, $\phi$ is the ion flux, and $D_0$ is the dose to achieve the specific amorphous state at 0 K. Furthermore, as noted elsewhere [12], the recovery rate in Eq. (2) is the sum of temperature-dependent rate constants for both irradiation-assisted and thermal annealing processes (i.e., $K_d(T) = K_{irr}(T) + K_{th}(T)$), each with its own effective jump frequency and activation energy. The irradiation-assisted recovery processes may be nearly athermal with low activation energies. The result of an iterative fit of Eq. (2) to the data is shown in Figure 6 and yields activation energies of 0.1 ± 0.05 eV and 0.6 ± 0.1 eV for irradiation-assisted and thermal recovery processes, respectively. The activation energy of 0.6 ± 0.1 eV for the thermal recovery process is consistent with the thermal recovery processes in Figures 3 and 4 and with the calculated activation energy for oxygen vacancy migration [15].
3.4. EFFECTS OF HYDROGEN IMPLANTATION

The channeling spectra from the irradiated and virgin regions are presented as a function of annealing temperature, along with the random spectrum, in Figure 7 for an ion fluence of $5.0 \times 10^{16}$ ions/cm$^2$. Only the RBS/C spectra from the irradiated region after isochronal annealing at 300, 470 and 570 K are shown to minimize the overlap of different spectra. As expected, the irradiation-induced disorder (300 K spectrum) on both the Ti and Sr sublattices is rather dilute. The as-implanted hydrogen concentration profile and several profiles after annealing are shown in Figure 8. The as-implanted hydrogen concentration profile (300 K) shows a broad profile due to diffusion and a maximum at about 300 nm, which according to TRIM calculations is where the peak of the implanted hydrogen profile should occur. The measurements indicate that the total amount of hydrogen within the analyzed region is $4.43 \times 10^{16}$ H/cm$^2$, which indicates that some hydrogen has diffused to the surface or beyond the analyzed region. Annealing the sample to 370 K resulted in a slight increase in the backscattering yield from the Sr and Ti sublattices (not shown) suggesting that there is some increased disordering due to annealing, perhaps as a result of hydrogen coalescence. The maximum in the hydrogen profile after annealing at 370 K shifts to a depth of 275 nm, which is coincident with the damage peak predicted by TRIM. Furthermore, the hydrogen profile sharpens somewhat after annealing at 370 K, and the total amount of hydrogen in the analyzed region is reduced slightly to $4.26 \times 10^{16}$ H/cm$^2$.

The local disorder generated on the Sr and Ti sublattices is significantly increased near the damaged peak position after annealing at 470 K (Figure 7). The local disorder
on these two sublattices is well separated in the spectrum and is very prominent compared to the disorder generated from implantation damage. The total amount of hydrogen after annealing at 470 K remains unchanged (4.26 x 10^{16} \text{H/cm}^2). The hydrogen profile indicates some diffusion towards the surface; however, the peak in the profile at 275 nm becomes more pronounced. Since scanning electron microscopy (SEM) results indicate the presence of hydrogen blisters at higher annealing temperatures [11], the increase in backscattering yield at the damage peak is believed to be caused by the nucleation of H₂ bubbles, which locally distort the structure and provide new scattering surfaces. The shift in the peak of the hydrogen profile to coincidence with the peak in the damage profile indicates diffusion and trapping of the hydrogen at irradiation-induced defects. Annealing at 570 K results in a significant decrease in the RBS/C backscattering yield from the peak damage region, an increase in the backscattering yield from the surface peak region, and a slight increase in the backscattering from the region between the surface peak and the damage peak. The hydrogen profile after annealing at 570 K indicates a significant loss of hydrogen from the implanted region. SEM results indicate that large cleaved areas exist after annealing this sample. This behavior is similar to the so-called "smart cutting" observed in Si [17], which suggests that it may be possible to produce large cleaved single crystals of titanate perovskites with a controlled thickness on the order of 50 nm to several hundred nanometers for research or device applications.

Similar RBS/C and hydrogen profiles have been obtained for an ion fluence of 1.0 \times 10^{17} \text{H/cm}^2. In these samples, annealing at 570 K results in a much larger increase in the RBS/C backscattering yield across the penetration depth of the implanted hydrogen. The hydrogen profile after annealing at 570 K indicates an increase in the hydrogen

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**Figure 8.** Hydrogen profile, based on nuclear reaction analysis, in SrTiO₃ after hydrogen implantation to 5.0 x 10^{16} ions/cm² and after isochronal annealing.
concentration near the surface region and a decrease in the total amount of hydrogen within the analyzed region, but not a complete loss of hydrogen as observed for $5.0 \times 10^{16}$ H$^+$ cm$^{-2}$. The sudden increase in the backscattering yield across the penetration depth is caused by the deformation of the surface region due to the formation of large hydrogen blisters, which are large enough to misorient the blister surface relative to the substrate. Annealing at 670 K reduces the total amount of hydrogen, as the blisters begin to burst, and after annealing at 770 K, the hydrogen is nearly completely lost. This behavior is due to the blisters bursting and releasing H$_2$ gas, which leads to both exfoliated blister surfaces and blister caps, as shown by SEM [11].

4. Conclusions

Ion-beam irradiation of SrTiO$_3$, CaTiO$_3$, and BaTiO$_3$ results in a crystalline-to-amorphous transformation below a critical temperature. In the case of irradiation with 800 keV Kr$^+$ ions, this critical temperature is 425, 440 and 550 K for SrTiO$_3$, CaTiO$_3$, and BaTiO$_3$, respectively. Ion-channeling studies of damage accumulation in SrTiO$_3$ irradiated with 1.0 MeV Au$^{2+}$ ions suggest that the crystalline-to-amorphous transformation is dominated by the accumulation and interaction of irradiation-induced defects. In SrTiO$_3$ irradiated with He$^+$ and O$^+$ ions at 180 K, isochronal annealing studies indicate that there is significant recovery of defects on both the oxygen and cation sublattices between 200 and 400 K. These defect recovery processes may control the kinetics of amorphization. A fit of the direct-impact/defect-stimulated model to the data for SrTiO$_3$ suggests that the kinetics of amorphization are controlled by both a nearly athermal irradiation-assisted recovery process with an activation energy of 0.1 $\pm$ 0.05 eV and a thermal defect recovery process with an activation energy of 0.6 $\pm$ 0.1 eV. In SrTiO$_3$ implanted with 40 keV H$^+$, annealing at 470 K results in increased backscattering from Sr and Ti in the damage peak due to the nucleation of H$_2$ bubbles; annealing at 570 K and higher results in the formation of blisters or large cleaved areas.

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