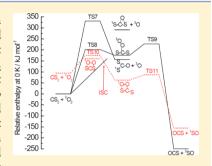
Oxidation of Reduced Sulfur Species: Carbon Disulfide

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Supporting Information

ABSTRACT: A detailed chemical kinetic model for oxidation of CS_2 has been developed, on the basis of ab initio calculations for key reactions, including $CS_2 + O_2$ and $CS + O_2$, and data from literature. The mechanism has been evaluated against experimental results from static reactors, flow reactors, and shock tubes. The $CS_2 + O_2$ reaction forms OCS + SO, with the lowest energy path involving crossing from the triplet to the singlet surface. For $CS + O_2$, which yields OCS + O, we found a high barrier to reaction, causing this step to be important only at elevated temperatures. The model predicts low temperature ignition delays and explosion limits accurately, whereas at higher temperatures it appears to overpredict both the induction time for CS_2 oxidation and the formation rate of OS_2 upon ignition. The predictive capability of the model depends on the accuracy of the rate constant for the initiation step $CS_2 + O_2$, which is



difficult to calculate due to the intersystem crossing, and the branching fraction for $CS_2 + O$, which is measured only at low temperatures. The governing reaction mechanisms are outlined on the basis of calculations with the kinetic model.

■ INTRODUCTION

Off-gases containing carbon disulfide (CS₂) are produced together with other sulfur containing compounds such as H2S from a range of industrial processes, including the Claus process¹⁻³ and production of viscous fibers,⁴ and in gasification of coal⁵ and biomass.⁶ Similar to H₂S and the oxidation product SO₂, carbon disulfide is toxic and harmful to the environment. Efficient treatment of the sulfur containing off gases becomes a bottleneck in these processes as strict emission requirements must be met. Hence, knowledge of the CS₂ oxidation mechanism is important. Investigations have shown that CS₂/ O2 mixtures are able to autoignite at low temperature and low pressure⁷⁻¹³ under conditions of negligible self-heating. Two explosion limits have been reported in the literature, 7 studies have been carried out to determine the effect upon the limits with a change in surface conditions and addition of inert gases. The induction times range from a few seconds to several minutes.^{9,11,14} At higher temperatures, CS₂ oxidation has been investigated in flow reactors, ^{2,15} shock tubes, ^{16–18} and laminar premixed flames.^{19–23} Much of the high-temperature work has been motivated by interest in the CO laser. CS₂/O₂ flames form CO with its vibrational population inverted, facilitating production of a CO flame laser.

Previous studies of the reaction mechanism of carbon disulfide oxidation have mostly been restricted to fuel-lean, dry conditions. ^{17,18,20,24,25} No reported chemical kinetic models are found to satisfactory describe experimental data across a wider range of mixture composition, temperature, and pressure

as the mechanism is complex and accurate kinetic data have been unavailable for several important reactions. The objective of the present study is to develop a detailed chemical kinetic model for oxidation of CS_2 and evaluate it over a broad range of conditions. The work is a continuation of a recent study by Glarborg and Marshall²⁶ on the oxidation chemistry of carbonyl sulfide. Rate constants for reactions CS_2 with O_2 and SO_2 and for CS with O_2 and SO_2 and so are calculated from ab initio theory. The mechanism aims at describing moist as well as dry oxidation conditions and includes reactions with hydrogencontaining radicals such as H, OH, HO₂, and SH. The resulting model is evaluated by comparing predictions with reported experimental results from static reactors, flow reactors, and shock tubes.

■ DETAILED KINETIC MODEL

In the present study, the starting mechanism and corresponding thermodynamic properties were drawn from earlier work on oxidation of ${\rm CO/H_2}^{27,28}$ and on sulfur chemistry. ^{29–34} The ${\rm CS_2}$ oxidation subset of the mechanism was developed in the present work, whereas reactions of OCS were drawn from recent work of the authors. ²⁶ An ozone subset was compiled from the evaluation of Atkinson et al. ³⁵ The thermodynamic properties for selected species in the sulfur subset are shown in

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Table 1. Thermodynamic Properties of Selected Species in the Reaction Mechanism^a

species	H_{298}	S_{298}	$C_{p,300}$	$C_{p,400}$	$C_{p,500}$	$C_{p,600}$	$C_{p,800}$	$C_{p,1000}$	$C_{p,1500}$	ref
CS_3	264.5	291.8	62.64	68.50	72.48	75.12	78.05	79.68	81.61	36, pw
CS_2	116.8	238.0	45.60	49.62	52.34	54.31	57.19	58.87	61.00	37
CS	278.7	210.7	29.85	30.94	32.16	33.25	34.75	35.67	36.76	37
OCS	-141.8	231.8	41.66	45.89	48.90	51.17	54.52	56.78	59.75	37
OCS_2	25.8	279.9	58.74	64.69	68.79	71.68	75.24	77.46	80.35	26, 38
SO	5.02	222.1	30.19	31.61	32.83	33.83	35.26	36.09	37.47	37
SO_2	-297.0	248.3	39.94	43.55	46.60	49.07	52.46	54.52	56.99	37
S	277.1	167.9	23.70	23.32	22.78	22.28	21.81	21.48	21.19	37
SH	143.1	195.9	32.45	31.86	31.36	31.15	31.86	32.78	34.92	37
S_2	128.5	228.4	32.53	34.00	35.00	35.67	36.47	37.31	38.90	37
S_2O	-57.7	266.5	43.88	47.44	50.04	51.88	54.22	55.52	56.94	34

 a Units are kJ mol $^{-1}$ for H and J mol $^{-1}$ K $^{-1}$ for S and C_p . The temperatures for C_p are in K.

Table 1. The data are mostly drawn from the database of Goos, Burcat, and Ruscic.³⁷

Table 2 lists the key reactions in the CS_2 oxidation scheme with the rate coefficients used in the present work. The full mechanism is available as Supporting Information. The CS_2 oxidation subset mostly relies on rate constants obtained from literature or estimated by analogy. However, in the present work we characterize the key reactions of CS_2 and CS with O_2 , as well as the minor steps $CS_2 + SO_2$ and CS + SO which have been proposed in prior modeling, by ab initio calculations.

Available experimental data on CS₂ oxidation from the literature are largely obtained under conditions with at most trace concentrations of water vapor. For this reason, the important radicals are O, CS, S, and SO, whereas chain carriers such as H, OH, HO₂, and SH have at most a minor influence. In industrial processes, however, CS₂ is typically present together with H₂S and water vapor, and we have chosen to include in the mechanism also species and chain carriers involving hydrogen.

Ab Initio Calculations. A key reaction in oxidation of carbon disulfide is $CS + O_2$. Three product channels have been proposed for this reaction:

$$CS + O_2 \Rightarrow OCS + O$$
 (R16)

$$CS + O_2 \rightleftharpoons CO + SO$$
 (R16')

$$CS + O_2 \rightleftharpoons CO_2 + S$$
 (R16")

The reaction numbering refers to the listing in Table 2. Both the overall rate constant and the products of reaction are in discussion. Atkinson et al. based their recommendation for the overall rate constant on the work of Black et al. at 298 K. However, the reaction is slow at this temperature and difficult to quantify. Results from photochemical and explosion limit studies had a comparable importance of channels R16 and R16′, but in the more direct flow system study of Richardson, had been smaller than k_{16} . In a more recent high-temperature shock tube study, Murakami et al. considered only channel R16 as a plausible path for the CS + O2 reaction and measured the value of k_{16} to be $(6.1 \pm 0.6) \times 10^{12} \exp(-(6140 \pm 8150)/T)$ cm mol⁻¹ s⁻¹ in the 2000–2900 K range. Note the substantial uncertainty in the activation energy.

The potential energy surface for $CS + O_2$ (R16) was explored using density functional theory (DFT) and QCISD theory. No four-center R16' or complex bond rearrangement R16" pathways were found and accordingly we consider it unlikely that product channels other than OCS + O R16 are

active. The abstraction path leading to OCS + O was characterized using the W1U method 43 as implemented in the Gaussian 09 program. 44 We modified this method to base it on geometry optimization and vibrational frequencies at the QCISD/6-311G(2d,d,p) level of theory, followed by several component steps that are combined to yield an approximate coupled cluster (CCSD(T)) energy at the infinite basis set limit, with corrections for core-valence electron correlation and scalar relativistic effects. The resulting potential energy diagram (PED) is shown in Figure 1. Reaction proceeds via addition over a 119 kJ mol⁻¹ barrier to form an SCOO adduct that then dissociates over a lower barrier (100 kJ mol⁻¹ relative to CS + O₂) to yield OCS + O. There are trans and cis pathways, with the former having a marginally lower entrance barrier, by 1.7 kJ mol⁻¹. Using DFT, the corresponding cis adduct is not bound and therefore was not explored further. The overall 0 K reaction enthalpy is computed at -176 kJ mol^{-1} (cf. a literature value of -175 kJ mol^{-1} depending on the source of the thermo data). The cis/trans reaction path degeneracy is taken into account by a symmetry factor of 2 for the hindered torsion in the trans entrance transition state (TS), which has a frequency of 78 cm⁻¹. The detailed Cartesian coordinates, vibrational frequencies, and energies are listed in the Supporting Information. These data are employed in canonical transition state theory (TST) as implemented in Multiwell, 45 along with the assumption that the first barrier is rate determining, to obtain the rate constant $1.3 \times 10^7 T^{1.97}$ $\exp(-14140/T)$ cm³ mol⁻¹ s⁻¹, for T = 500-2500 K. Although the exit barrier from the adduct is ~20 kJ mol⁻¹ below the entrance barrier, this transition state is also tighter. The computed A factor at 1000 K for adduct dissociation to OCS + O is 2.2×10^{13} s⁻¹ at the high-pressure limit, 6.7 times smaller than that for dissociation back to CS + O2. This would suggest that above ~1400 K it is the second barrier that becomes rate limiting. However, because the cis pathway appears to have no barrier, in fact rapid rotation allows for fast overall dissociation limited by the initial rate of adduct formation. For comparison, computed pathways for CO + O2 abstraction proceed via similar TSs but without subsequent bound adducts, and the cis and trans barriers are higher at 260 and 318 kJ mol⁻¹, respectively.46

Figure 2 shows an Arrhenius plot for the reaction of CS with O_2 . The calculated activation energy is consistent with the wide range of values quoted for the valence iso-electronic reaction $CO + O_2$, but it makes $CS + O_2$ too slow to be consistent with the low temperature observations of Black et al. ⁴¹ and Richardson. ²¹ It is larger than the value derived by Murakami

Table 2. Reaction Subset for Carbon Disulfide Oxidation^a

		$A \left[\text{cm mol}^{-1} \text{ s}^{-1} \right]$	β	$E_{\rm a}/R~[{ m K}]$	source
1.	$CS + S(+M) \rightleftharpoons CS_2(+M)$	1.9×10^{26}	-4.300	0	39
	low pressure limit:	6.2×10^{23}	-2.420	0	
2.	$CS + SH \rightleftharpoons CS_2 + H$	1.2×10^{13}	0.000	0	see text
3.	$CS_2 + O \rightleftharpoons CS + SO$	3.2×10^{13}	0.000	820	see text
4.	$CS_2 + O \Rightarrow OCS + S$	2.9×10^{12}	0.000	820	see text
5.	$CS_2 + O \rightleftharpoons CO + S_2$	1.6×10^{12}	0.000	820	see text
6.	$CS_2 + OH(+M) \rightarrow HOCS_2(+M)$	4.8×10^{12}	0.000	0	35
	low pressure limit:	2.9×10^{17}	0.000	0	00
	$HOCS_2(+M) \rightarrow CS_2 + OH(+M)$	1.6×10^{13}	0.000	5159	35
	low pressure limit:	9.6×10^{17}	0.000	5159	(Fc = 0.8)
7.	$CS_2 + O_2 \rightleftharpoons OCS + SO$	1.6×10^{13}	0.000	31000	pw
8.	$CS_2 + O_2 \rightleftharpoons OCS + {}^1SO$	3.6×10^{11}	0.000	17900	pw
9.	$CS_2 + S(+M) \Rightarrow CS_3(+M)$	1.3×10^{12}	0.000	0	36
<i>,</i> ,	low pressure limit:	2.5×10^{21}	-1.600	0	00
10.	$CS_2 + S \rightleftharpoons CS + S_2$	6.9×10^{13}	0.000	4447	36
11.	$CS_2 + SO \rightleftharpoons CS + S_2O$	1.0×10^{12}	0.000	5030	est
12.	$CS_2 + SO_2 = CS + S_2O$ $CS_2 + SO_2 = OCS + S_2O$	7.8×10^{12}	0.000	24460	pw
13.	$CS_2 + SC_2 \leftarrow CCS + S_2C$ $CS + O \rightleftharpoons CO + S$	1.6×10^{14}	0.000	760	35
14.	$CS + OH \Rightarrow OCS + H$	1.0×10^{14}	0.000	0	40, est
15.	$CS + OH \rightleftharpoons CO + SH$	2.0×10^{13}	0.000	0	40, est
16.	$CS + O_2 \rightleftharpoons CCS + O$	1.3×10^{7}	1.970	14140	pw
17.	$CS + O_2 \leftarrow CCS + CC$ $CS + OCS \rightleftharpoons CS_2 + CC$	2.0×10^{12}	0.000	18970	est as OCS + SO
18.	$CS + SO \Rightarrow CS_2 + CS$ $CS + SO \Rightarrow CS + S$	3.6×10^{5}	2.193	1744	pw
19.	$CS + SO_2 \rightleftharpoons OCS + SO$	2.7×10^{12}	0.000	12230	est as CO + SO ₂
20.	$OCS + M \rightleftharpoons CO + S + M$	2.7×10^{14} 2.5×10^{14}	0.000	30900	26
21.	$OCS + M \leftarrow CO + S + M$ $OCS + H \rightleftharpoons CO + SH$	2.2×10^{11}	1.022	2810	26
22.	$OCS + O \rightleftharpoons CO + SO$	4.7×10^{13}	0.000	2617	26, b
22.	063 + 0 = 60 + 30	-2.0×10^{13}	0.000	3717	20, 0
23.	$OCS + O \rightleftharpoons CO_2 + S$	-2.0×10^{13} 2.0×10^{13}	0.000	3717	26
24.	$OCS + OL = CO_2 + SH$ $OCS + OH = CO_2 + SH$	4.6×10^{11}	0.000	8072	26
25.	$OCS + O11 \leftarrow CO_2 + S11$ $OCS + O_2 \rightleftharpoons CO + SO_2$	1.0×10^{12}	0.000	16100	26
26.	$OCS + S \rightleftharpoons CO + S_2$ $OCS + S \rightleftharpoons CO + S_2$	4.0×10^4	2.570	1180	26
27.	$OCS + S \rightleftharpoons OCS_2$ $OCS + S \rightleftharpoons OCS_2$	4.6×10^{33}	-8.220	4769	$0.066 \text{ atm}^{26,b}$
2/.	$OC3 + 3 \rightleftharpoons OC3_2$	1.1×10^{31}	-6.980	4206	0.066 atm
		2.4×10^{34}	-8.220	4769	0.66 atm
		5.7×10^{31}	-6.980	4206	0.66 atm
20	$OCS + SH \rightleftharpoons CS_2 + OH$	1.2×10^{12}	0.000		
28.	$OCS + SO \Rightarrow CO + S_2O$	1.2×10^{12} 2.0×10^{12}		25670	est
29. 30.	$CS_3 + O \rightleftharpoons CS_2 + SO$ $CS_3 + O \rightleftharpoons CS_2 + SO$	6.0×10^{13}	0.000	18970 0	26
		6.0×10^{13}			est
31. 32.	$CS_3 + S \rightleftharpoons CS_2 + S_2$ $OCS_2 + O \rightleftharpoons OCS + SO$	6.0×10^{13}	0.000	0	est 26
32.	$OCS_2 + O = OCS + SO$ $OCS_2 + S = OCS + S_2$	6.0×10^{13}	0.000	0	26 26
		1.0×10^{12}		0	
34.	$OCS_2 + O_2 \Rightarrow OCS + SO_2$ $HOCS_2 + O_2 \rightarrow OCS + HOSO$	1.0×10^{10} 1.4×10^{10}	0.000		est
35. 27			0.000	0	35
37.	$HOCS_2 + O_2 \rightarrow HCO + SO_2 + S$	0.3×10^{10}	0.000	720	35
38.	$S + O_2 \rightleftharpoons SO + O$	5.4×10^5	2.110	-730	53
39.	$SO + O_2 \Rightarrow SO_2 + O$	7.6×10^3	2.370	1495	54
40.	$O + O_2 + M \rightleftharpoons O_3 + M$	5.6×10^{20}	-2.600	0	35
41.	$O_3 + O \rightleftharpoons O_2 + O_2$	4.8×10^{12}	0.000	2060	35
42.	$O_3 + OH \Rightarrow O_2 + HO_2$	1.0×10^{12}	0.000	936	35
43.	$O_3 + HO_2 \rightleftharpoons O_2 + O_2 + OH$	5.8×10^{-4}	4.570	-693	35
44.	$CS + O_3 \rightleftharpoons OCS + O_2$	4.5×10^{12}	0.000	3020	35, est
45.	$S + O_3 \rightleftharpoons O_2 + SO$	7.2×10^{12}	0.000	0	35
46.	$SO + O_3 \rightleftharpoons O_2 + SO_2$	2.7×10^{12}	0.000	1170	35

^aParameters for use in the modified Arrhenius expression $k = AT^{\beta} \exp(-E_a/[RT])$. Units are mol, cm, s, K. ^bDuplicate reaction; the rate constant is calculated by adding the two Arrhenius expressions.

et al. 25 from shock tube experiments, but within their reported uncertainty. The calculated value of k_{16} is in agreement with the scattered data reported by Murakami et al., at least in the upper

part of their temperature range. Two critical reviews of this reaction in the context of low temperature chemistry ^{35,47} accepted the measurements at room temperature but, because

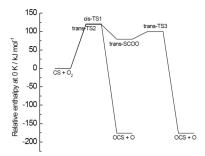


Figure 1. Potential energy diagram for CS + O₂ based on W1U results.

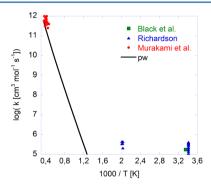


Figure 2. Arrhenius plot for the reaction CS + O_2 . Experimental results (symbols) from Black et al., ⁴¹ Richardson, ²¹ and Murakami et al. ²⁵ The solid line denotes the rate constant calculated in the present work.

the data of Richardson et al. imply an almost zero activation energy and an extraordinarily small A factor, made no recommendation concerning the temperature dependence. The present computations might not contradict the measured rate constants below 600 K if there is a further channel other than O atom abstraction from O_2 . However, one should be mindful of the great difficulty of isolating very slow processes from interference by impurities or secondary chemistry. The $CS + O_2$ reaction deserves further investigation, especially above 600 K.

Other processes were investigated using the lower-cost CBS-QB3 approximation, ⁴⁸ which begins with B3LYP/6-311G-(2d,d,p) geometries and frequencies followed by several steps that are combined to approximate the CCSD(T) energy at the infinite basis set limit. Chernysheva et al.²⁴ included the reaction of CS with SO, assuming two product channels,

$$CS + SO \Rightarrow OCS + S$$
 (R18)

$$CS + SO \rightleftharpoons CO + S_2$$
 (R18')

Reaction R18' is a four-center reaction, and the occurrence of this step is not supported by our ab initio calculations.

Figure 3 shows the PED for CS + SO R18, which, like the oxygen analog R16, proceeds via an addition/dissociation path, but with much lower barriers. TST was applied to the initial, higher barrier at TS4 to determine the rate constant. For reaction R18, our calculated rate constant is considerably smaller than the value proposed by Chernysheva et al. at low temperatures but faster above 1000 K. We also looked at the reaction of CS_2 with SO_2 ,

$$CS_2 + SO_2 \rightleftharpoons OCS + S_2O$$
 (R12)

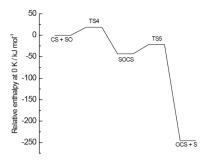


Figure 3. Potential energy diagram for CS + SO based on CBS-QB3 results.

The simple PED for atom exchange between CS_2 and SO_2 is shown in Figure 4. As expected, the reaction is slow, with a calculated activation energy of 203 kJ mol⁻¹.

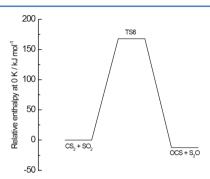


Figure 4. Potential energy diagram for CS₂ + SO₂ based on CBS-QB3 results.

The reaction of CS_2 with O_2 is important for initiation of CS_2 oxidation at higher temperatures. It was investigated by Saito et al. ¹⁸ in a shock tube study of CS_2 oxidation under conditions with a large excess of O_2 and Ar. Saito et al. assumed that the major product channel led to formation of CS and SO_2 and derived a rate constant for this step from simulations with a complex mechanism. However, the activation energy derived by Saito et al. of 134 kJ mol⁻¹ for $CS_2 + O_2$ is significantly lower than the computed barrier of 247 kJ mol⁻¹ for addition of O_2 to CS_2 , ⁴⁹ indicating that more work is required on this reaction.

We investigated a number of pathways for the reaction between CS_2 and O_2 , as shown on Figure 5. The highest energy path is abstraction by the central carbon atom to yield $CS_2O + O$, which with a barrier of 332 kJ mol⁻¹ will be too slow to be significant under most combustion conditions. The most favorable spin-allowed pathway involves addition over a barrier

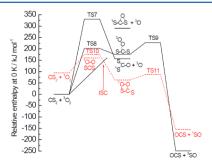


Figure 5. Potential energy diagram for $CS_2 + O_2$ based on CBS-QB3 results.

of 202 kJ mol⁻¹ to make a triplet CS_2OO adduct, followed by dissociation over a second, slightly higher barrier of 227 kJ mol⁻¹ (relative to the reactants) to form OCS + SO,

$$CS_2 + O_2 \rightleftharpoons OCS + SO$$
 (R7)

The second barrier, TS9, is also tighter than the first, TS8. For example, at 1000 K the A factors at the high-pressure limit for dissociation of the triplet CS_2O_2 adduct via TS8 and TS9 are 3×10^{13} and 8×10^{12} s⁻¹, respectively. Thus, at all temperatures passage through TS9 will be rate-limiting, and the corresponding rate constant for channel R7 is listed in Table 2.

There is also a possible singlet reaction path,

$$CS_2 + O_2 \rightleftharpoons OCS + {}^1SO$$
 (R8

Singlet oxygen can add to CS2 to make a singlet adduct with a four-membered ring. The high barrier for this step is consistent with the very low reactivity of CS₂ toward $O_2(^1\Delta)$. This adduct can also be accessed by CS₂ + ³O₂ via intersystem crossing. By application of the algorithm of Harvey,⁵¹ we have located a minimum-energy crossing point (MECP) that lies 81 kJ mol⁻¹, at the B3LYP/6-311G(2d,d,p) level of theory, above the singlet four-membered ring species. This places the MECP ~145 kJ mol⁻¹ above that for $\overline{CS}_2 + O_2$. Because the singlet four-membered ring is formed with more energy than necessary to overcome the barrier to OCS + ¹SO, this dissociation will be fast and we adopt 145 kJ mol⁻¹ as the activation energy for CS₂ $+ O_2 \rightleftharpoons OCS + {}^1SO$. The A factor incorporates the probability of intersystem crossing and is presumably smaller than a typical collision rate. We set it equal to the value measured for the spin-forbidden O + SO₂ addition, $3.6 \times 10^{11} \text{ cm}^3 \text{ mol}^{-1} \text{ s}^{-1.52}$ This is a crude estimate and might be uncertain perhaps by an order of magnitude.

Other singlet CS_2O_2 species, with five- and three-membered rings, have also been characterized. These have energies rather higher than the four-membered ring (Figure 5) and so probably play little role in the kinetics of the $CS_2 + O_2$ reaction.

The activation energies calculated for channels R8, R12, R16, and R18 are probably accurate to within about 8 kJ mol⁻¹. This corresponds to an uncertainty in the rate constant of about a factor of 3. For k_8 the uncertainty is larger, due to the crude estimate of the A-factor for this reaction.

Reaction Mechanism. The CS_2 oxidation subset involves a number of other reactions, in addition to those characterized from ab initio calculations. The thermal dissociation of CS_2 ,

$$CS_2(+M) \rightleftharpoons CS + S(+M)$$
 (R1b)

has been investigated in high temperature shock tube experiments. $^{25,55-64}$ In most of the earlier work, the decay of CS₂ was monitored, 58,60,62,63 whereas the more recent study of Murakami et al. 25 involved measuring the time profile of S atoms using atomic resonance spectroscopy. Direct extrapolation of the reported data yields rate constants at low temperature for the reverse step, CS + S + M \rightleftharpoons CS₂ + M (R1), that are much too fast to be feasible. For this reason, Troe et al. 39 recently re-evaluated the available experimental data for thermal dissociation of CS₂ to improve values for the low-pressure limit (based on refs 25, 58, 60, 61, 63, and 64) and the high-pressure limit (based on data from ref 62). We have adopted their recommended rate coefficients for (R1) that we believe to be reliable over a wider range of temperature and pressure than previous evaluations.

The reaction of CS₂ with atomic hydrogen,

$$CS_2 + H \rightleftharpoons CS + SH$$
 (R2b)

has been studied by Woiki and Roth, 65 who used time-resolved atomic resonance absorption spectroscopy (ARAS) measurements of H atoms in a shock tube to determine the rate constant. The reverse reaction of CS + SH (R2) is exothermic and we expect it to proceed without a barrier. We include the reaction in the exothermic direction, deriving the rate constant $k_2 = 1.2 \times 10^{13} \text{ cm}^3 \text{ mol}^{-1} \text{ s}^{-1}$ from the measurements of Woiki and Roth of k_{2b} in the 1170-1830 K range.

Among reactions of CS_2 with the O/H radical pool, CS_2 + O is generally the most important. This reaction is known to have three product channels:

$$CS_2 + O \rightleftharpoons CS + SO$$
 (R3)

$$CS_2 + O \rightleftharpoons OCS + S$$
 (R4)

$$CS_2 + O \rightleftharpoons CO + S_2$$
 (R5)

The main product channel is (R3), whereas channels R4 and R5 are minor, at least at low temperature. Data for the total reaction rate of CS_2 + O are in good agreement and are described well by the rate constant recommended by Singleton and Cvetanovic. Measurements of the product distribution at low temperatures indicate values of $k_4/k_{\rm tot}$ of $8-10\%^{67-69}$ whereas $k_5/k_{\rm tot}$ appears to be in the range 1-5%. The distribution of $k_4/k_{\rm tot}$ in the 250–500 K range and at 1100 K⁷¹ indicate that the branching fraction decreases slightly with temperature but differences may be within experimental uncertainty. We assume that the branching fraction for CS_2 + O is independent of temperature and combine the overall rate constant from Singleton and Cvetanovic and the product distribution from the low temperature work to obtain values for k_3 , k_4 , and k_5 .

On the basis of a theoretical study, Saheb⁷² recently concluded that channels R4 and R5 could both be disregarded, but this result is not supported by the experimental evidence. Saheb's work was focused on triplet stationary points on the O + CS₂ potential energy surface, with correspondingly high barriers to the minor but crucial product channels OCS + S and CO + S₂, which led him to argue against a significant role for these pathways in O + CS₂ kinetics. Some 18 years earlier, Froese and Goddard⁷³ investigated the possibilities of both singlet and triplet potential surfaces and commented on the possibility of intersystem crossing (ISC) between them. Our initial exploration at the B3LYP/6-311G(2d,d,p) level of density functional theory yields a minimum energy ISC point close to the geometry of cis-OSCS, 100 kJ mol⁻¹ below that of O + CS₂. This opens the possibility that a small fraction of triplet O + CS₂ trajectories, having passed over a minor barrier, 72 cross to the lower-lying singlet OSCS structure. This may undergo a series of rearrangements or dissociation via barriers that are significantly lower relative to the reactants than those on the triplet surface.⁷³ Because the branching fraction for CS₂ + O is very important for the generation of chain carriers in CS2 oxidation, more work on this reaction is required.

The reaction of CS₂ with OH is important in the atmosphere and has been studied at low temperatures, where it proceeds through addition:

$$CS_2 + OH(+M) \rightleftharpoons HOCS_2(+M)$$
 (R6)

Because of the low thermal stability of HOCS₂, redissociation of the adduct is fast even at low temperatures. We have adopted

the recommendation of Atkinson et al. 35 for the rate constant, but the value is not important for the modeling predictions in the present work. A possible secondary product channel for CS_2 + OH to form OCS + SH is apparently slow, with a measured upper limit of approximately 10^9 cm 3 mol $^{-1}$ s $^{-1}$ at 298 K. 35

The reaction of CS₂ with atomic sulfur has two possible product channels:

$$CS_2 + S(+M) \rightleftharpoons CS_3(+M)$$
 (R9)

$$CS_2 + S \rightleftharpoons CS + S_2$$
 (R10)

Gao and Marshall³⁶ investigated the reaction combining pulsed laser photolysis and resonance fluorescence over the temperature range 290–1040 K. Over 290–770 K, they observed pressure-dependent kinetics, which were attributed to the recombination channel R9. This is in agreement with the early reports of Basco and Pearson.⁷⁴ At the intermediate temperatures of 690 < T < 770 K, reaction R9 was reversible; i.e., the time scale for decomposition of CS₃ to CS₂ + S was similar to that for addition.³⁶ At 690–1040 K, Gao and Marshall observed a change in mechanism to the pressure-independent channel R10. Their value of k_{10} agrees well with the shock tube results of Woiki and Roth,⁷⁵ obtained in the 1260–1820 K range. For both channels R9 and R10, we adopt the rate constants measured by Gao and Marshall. For the low pressure limit, we fit their data to an $A \cdot T^{\beta}$ expression to obtain a format that is compatible with CHEMKIN.

The reaction $CS_2 + SO$ is not well characterized. Wood and Heicklen⁹ investigated the explosion limits of CS_2/O_2 mixtures at temperatures of 341–415 K and found that their results were sensitive to the competition between $CS_2 + O_2$ and $CS_2 + SO$, assuming the products of the latter reaction to be OCS + S_2 . We consider S abstraction to form CS and S_2O to be more likely,

$$CS_2 + SO \rightleftharpoons CS + S_2O$$
 (R11)

and include this step with an estimated rate constant.

Among the reactions of CS with the O/H radical pool, CS + O and CS + OH are believed to be fast. The CS radical may recombine with atomic hydrogen to form HCS, but this step was not included in the present mechanism. The reaction of CS with atomic oxygen are expected to yield CO and S as the only products:

$$CS + O \rightleftharpoons CO + S$$
 (R13)

Only limited experimental investigations have been made to determine the rate expression of channel R13, but reported low-temperature data are in good agreement. The recommendations of Singleton and Cvetanovic and Atkinson et al. for k_{13} are based on the study by Lilenfeld and Richardson.

There are no experimental data for the reaction of CS with OH. Ab initio calculations 78,79 indicate that the reaction has no barrier, and Loison et al. 40 report it to be fast, with OCS + H being the major product channel,

$$CS + OH \Rightarrow OCS + H$$
 (R14)

and a minor (20%) contribution from formation of CO and SH,

$$CS + OH \rightleftharpoons CO + SH$$
 (R15)

In addition to CS + SO discussed above, Chernysheva et al.²⁴ included reactions of CS with OCS and SO₂,

$$CS + OCS \rightleftharpoons CS_2 + CO$$
 (R17)

$$CS + SO_2 \rightleftharpoons OCS + SO$$
 (R19)

We consider these steps plausible and include them with estimated rate constants. However, with the current rate constants, which are considerably smaller than the values proposed by Chernysheva et al., they are too slow to influence modeling predictions.

Reactions of ozone have been proposed to play a role in chain termination at low temperatures for the CS_2/O_2 system. For this reason, we include an O_3 reaction subset with rate constants from Atkinson et al. For the reaction of CS with O_3 , the rate constant was based on room temperature data and an assumed activation energy.

■ RESULTS AND DISCUSSION

Experimental results for oxidation of CS_2 have been obtained in batch reactors, $^{7-13}$ flow reactors, 2,15 shock tubes, $^{16-18}$ and laminar premixed flames. $^{19-23}$ For evaluation of the model, we have selected experimental data obtained in batch and flow reactors, as well as in shock tubes. Most of the reported experiments were conducted under conditions with only trace amounts of water vapor. Clarke et al. 2 conducted flow reactor experiments on CS_2 conversion to CO and CS in the presence of CS_2 conversion to CS_3 unfortunately, the results reported for the CS_2/H_2O mixture were all obtained at close to full conversion of CS_3 and these data were not used for model validation.

Explosion Limits and Low Temperature Induction Times. To evaluate the performance of the chemical kinetic model at low temperatures, predictions have been compared to measured explosion limits in batch reactors at temperatures between 350 and 520 K. The experimental data were taken from Voronkov and Semenov,⁷ and Myerson and Taylor.^{8,14} These data sets were obtained in an overlapping temperature and pressure range but under conditions of low (300 ppm⁷) and high (25%^{8,14}) concentrations of CS₂, respectively.

Figure 6 compares the measured and calculated explosion limits. Both sets of explosion limits exhibit the characteristic peninsula-shape, involving a lower as well as an upper limiting pressure in a certain temperature range. Batch reactor results for CS_2 oxidation have been reported to depend on the surface

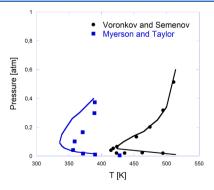


Figure 6. Comparison of experimental and predicted explosion limits for CS_2 in a batch reactor. The experimental data are taken from Voronkov and Semenov⁷ and Myerson and Taylor.^{8,14} The symbols mark experimental data, and solid lines denote model predictions. Inlet composition for Voronkov and Semenov experiments: 300 ppm of CS_2 , 21% O_2 , and 79% N_2 . Inlet composition for Myerson and Taylor experiments: 25% CS_2 and 75% O_2 .

to volume ratio of the reactor^{8,9,14} and the first (lower) explosion limit is controlled mainly by competition between a gas-phase chain branching reaction sequence and termination of radicals at the wall of the reactor. In the modeling, we did not include a wall termination reaction; instead explosion had to occur within a set induction time to be acknowledged. The limiting induction time was somewhat arbitrarily set to 10 s; the use of a different value would affect the predicted explosion limits but not the overall trends.

The experimental results indicate that the lower explosion limit is only slightly dependent on temperature, whereas the upper limit exhibits a stronger temperature dependence. Similar to the first limit, the second limit is controlled by a competition between chain branching and chain terminating reactions, but the second limit is expected to be independent of surface reactions.

The agreement between the reported observations and the calculations is very good, in particular for the dilute mixture of Voronkov and Semenov. The model predicts correctly that the lower limit pressure at which explosion occurs has only a small dependence on temperature in the investigated range and it captures well the secondary explosion limits for both mixtures. Also the low temperature limits for explosion, which according to the reported data are approximately 350 and 410 K, respectively, are predicted satisfactorily.

Induction times for the CS₂/O₂ system at low temperatures have been reported by several groups. ^{9,11,14} Depending on temperature, pressure, and mixture composition, the time for ignition may vary from a few seconds to several minutes. For model validation purposes, the shorter induction time data are preferable, as they are less prone to be affected by loss of radicals on the reactor walls. Figure 7 compares the induction

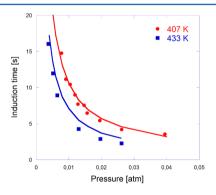


Figure 7. Comparison of experimental and predicted induction times as a function of pressure and temperature for CS_2 in a batch reactor. The experimental data are taken from Taylor and Myerson. ¹⁴ The symbols mark experimental data, and solid lines denote model predictions. Inlet composition: 25% CS_2 and 75% O_2 .

times reported by Taylor and Myerson¹⁴ for a mixture of 25% CS_2 and 75% O_2 at temperatures of 407 and 433 K and varying pressure with modeling predictions. Again, the agreement between observed and calculated data is good, indicating that the low temperature chain branching chemistry of CS_2 under oxidizing conditions is described well by the model.

Oxidation in a Flow Reactor. Homann et al.¹⁵ reported detailed species measurements as a function of time (distance) from oxidation of CS₂ in a low-pressure flow reactor. The data were obtained by molecular beam mass spectrometry. Homann et al. measured concentrations of CS₂, OCS, CO, CO₂, SO, and SO₂, as well as a number of minor species, at a pressure of

0.0395 atm and temperatures of 1200 and 1360 K, respectively. For the purpose of evaluating the model, we have chosen the 1200 K data, which were obtained at more dilute and well-controlled conditions. The 1360 K experiments were conducted with 4 times higher CS_2 inlet concentrations, resulting in an adiabatic temperature increase for complete oxidation of several hundred degrees.

The experimental results are compared with modeling predictions in Figure 8. In addition to the sulfur species

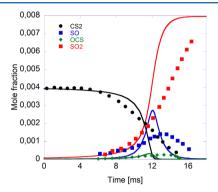


Figure 8. Comparison of experimental and predicted mole fractions for oxidation of CS_2 in a flow reactor at low pressure. The experimental data are taken from Homann et al. The symbols mark experimental data, and solid lines denote model predictions. Modeling predictions are shifted 39 ms to match the experimental time for 50% conversion of CS_2 . Conditions: T = 1200 K, P = 0.0395 atm, inlet composition is 0.4% CS_2 , 8.0% O_2 , balance Ar.

shown, also S, S_2 , S_2O , and S_2O_2 were detected in small quantities. The measured induction time (about 8 ms) is significantly shorter than the calculated value; the predicted profiles have been shifted approximately 40 ms to lower values to match the observed time for 50% conversion of CS_2 . Once reaction has started, the model predicts a consumption rate for CS_2 , which is faster than observed. The overprediction of the oxidation rate for CS_2 after onset of reaction, facilitated by a sequence of chain-branching reactions discussed below, has the consequence that also the peaks of SO and OCS become too narrow, and the SO_2 formation rate is larger than observed. The maximum concentration of SO is predicted within a factor of 2, whereas the peak concentration of OCS is calculated quite accurately.

Both Homann et al. 15 and Howgate and Barr, 20 who previously modeled these data, pointed out that the observed induction time in the flow reactor was possibly affected by experimental artifacts. In the experiments, the reactants CS_2 and O_2 were preheated separately and mixed at the entrance to the reaction zone. Atomic oxygen, formed from O_2 at the heating elements in the preheating oven, was suggested to promote onset of reaction. Also, the induction time could conceivably be affected by the mixing process at the reaction zone inlet and/or by reactions at the reactor surface, facilitated by fast diffusion to the wall at the low pressure. However, it is noteworthy that in their modeling of OCS oxidation in the same reactor setup, Glarborg and Marshall 26 found no indication that the induction time was affected by experimental artifacts.

The oxidation rate of CS₂ upon initiation of reaction was modeled satisfactorily by both Homann et al. and Howgate and Barr. They obtained a slower oxidation rate than in the present work by introducing loss of atomic oxygen on the reactor

surface and by using a fast rate constant for $CS_2 + S$ to yield $CS + S_2$; a value that is not supported by more recent direct measurements. Some loss of oxygen atoms through a heterogeneous reaction at the reactor wall is plausible; however, such a reaction was not taken into consideration in the present modeling.

Oxidation in a Shock Tube. CS₂ ignition and oxidation have been investigated in shock tubes at high temperature. ^{16–18} We believe that the most reliable data are those of Saito et al., ¹⁸ who used very dilute mixtures and monitored the concentration of atomic oxygen by ARAS. Figure 9 compares experimental

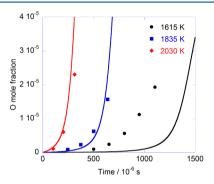


Figure 9. Comparison of experimental and predicted mole fractions of atomic oxygen for oxidation of CS_2 in a shock tube. The experimental data are taken from Saito et al.¹⁸ The symbols mark experimental data, and solid lines denote model predictions. Conditions: T = 1615, 1835, and 2035 K. The total concentration $[M] = 1.8 \times 10^{-5}$ mol cm⁻³. The inlet composition is 50 ppm of CS_2 , 0.2% O_2 (1615 K) or 100 ppm of CS_2 , 0.1% O_2 (1835 and 2030 K); balance Ar.

and predicted concentrations of O as a function of time at three selected temperatures (1615, 1835, and 2030 K). In the calculations the total concentration [M] is assumed to be 1.8 \times 10^{-5} mol cm $^{-3}$, similar to other CS $_2$ oxidation experiments reported in the paper. However, neither the gas density nor the pressure was reported by Saito et al. for the data sets chosen for analysis in the present work and this introduces an uncertainty in the modeling interpretation.

The comparison in Figure 9 shows that the O atom profiles are predicted accurately at the higher temperatures, 1835 and 2030 K. However, at 1615 K both the induction time for CS_2 and the formation rate of [O] upon ignition are overpredicted. This discrepancy is similar to the one discussed above for the flow reactor results of Homann et al. at 1200 K. It indicates that

the balance between initiation and chain branching in the model at higher temperatures is not correct. This is discussed in more detail in the next section.

Reaction Paths and Bottlenecks. In this section, we discuss the oxidation pathways for CS_2 and identify the reactions that are rate limiting for the oxidation rate. Figure 10 shows the results of a sensitivity analysis for selected experimental conditions. Table 3 provides an uncertainty estimate for the rate constants of the key reactions.

Analysis of the calculations with the model shows that roughly the same set of key reactions plays an important role over the range of conditions investigated, from the low temperature batch reactor experiments to the high temperature shock tube experiments. Reaction is initiated by thermal dissociation of CS₂,

$$CS_2(+M) \rightleftharpoons CS + S(+M)$$
 (R1b)

or by reaction of CS2 with O2,

$$CS_2 + O_2 \rightleftharpoons OCS + {}^{1}SO$$
 (R8)

After initiation, the generation of chain carriers in the system is controlled by the competition between chain branching and chain terminating reaction sequences. Sequence A,

$$CS_2 + O \rightleftharpoons CS + SO$$
 (R3)

$$SO + O_2 \rightleftharpoons SO_2 + O$$

$$\overline{CS_2 + O_2} \rightleftharpoons \overline{CS + SO_2}$$
(R39)

is chain propagating at low to medium temperatures where the CS radical is comparatively unreactive toward stable species. At high temperatures, CS may react with O_2 to yield atomic oxygen R16 and (A) becomes chain branching. Sequence B,

$$CS_2 + O \rightleftharpoons OCS + S$$
 (R4)

$$S + O_2 \rightleftharpoons SO + O \tag{R38}$$

$$SO + O_2 \rightleftharpoons SO_2 + O \tag{R39}$$

$$\overline{\text{CS}_2 + 2\text{O}_2} \rightleftharpoons \overline{\text{OCS} + \text{SO}_2 + \overline{\text{O}}}$$

is a chain branching sequence. The propagating and branching sequences compete with terminating steps, mainly the reaction

$$CS_2 + O \rightleftharpoons CO + S_2$$
 (R5)

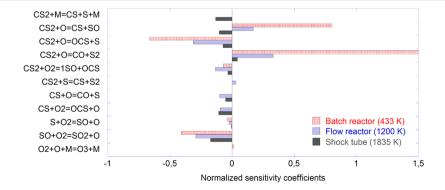


Figure 10. Sensitivity coefficients for the induction time at different reaction conditions. The coefficients show the relative change in the predicted induction time caused by a factor of 2 increase in the rate constant of the specific reaction. Conditions correspond to those of the experiments conducted in batch reactor (Figure 7, 433 K, 0.01 atm), flow reactor (Figure 8, 1200 K, 0.0395 atm), and shock tube (Figure 9, 1835 K, 2.9 atm).

Table 3. Uncertainty Evaluation for Key Reactions in the CS₂ Oxidation Subset

		method ^a	uncertainty ⁶	comment
1.	$CS + S(+M) \rightleftharpoons CS_2(+M)$			
	high pressure limit k_{∞} :	review, theory	UF = 3 (300-2000 K)	с
	low pressure limit k_0 :	review, theory	UF = 2 (300-2000 K)	с
3-5.	$CS_2 + O \Rightarrow products$	review	UF = 1.5 (218-920 K)	d
3.	$CS_2 + O \rightleftharpoons CS + SO$	review	UF = 1.5 (218-920 K)	d
4.	$CS_2 + O \rightleftharpoons OCS + S$	review	UF = 2 (250-500 K)	d, e
5.	$CS_2 + O \rightleftharpoons CO + S_2$	review	UF = 3 (298 K)	d, e
8.	$CS_2 + O_2 \rightleftharpoons OCS + {}^1SO$	theory	UF = 10	f
13.	$CS + O \rightleftharpoons CO + S$	review	UF = 1.25 (150 - 300 K)	g
16.	$CS + O_2 \rightleftharpoons OCS + O$	theory	UF = 3 (1000 K)	h

"Method of deriving the rate constant used in the present mechanism. b The uncertainty is given as an uncertainty factor (UF). Uncertainty evaluation from ref 39. Uncertainty evaluation from ref 66. The branching fraction for the $CS_2 + O$ reaction has only been measured directly at low temperature, and the uncertainty increases with temperature. The factor of 10 uncertainty in the rate constant relates to the difficulty of calculating the A-factor for a spin-forbidden reaction. In addition there is a $\pm 8 \text{ kJ mol}^{-1}$ uncertainty in the activation energy. Uncertainty evaluation from ref 35. The reaction is fast, and the uncertainty factor is not expected to increase above 2 with temperature. The uncertainty relates to a $\pm 8 \text{ kJ mol}^{-1}$ uncertainty in the activation energy.

Other termination steps may also be active, dependent on the type of reactor and the temperature/pressure range of the experiment.

The chemistry responsible for the CS_2 explosion limits has been discussed in a series of papers by Azatyan and coworkers. ^{13,80,81} Their findings are largely in agreement with the present analysis. Under the conditions of the batch reactor experiments (350–520 K), the $CS_2 + O_2$ reaction R8 is the initiating step. The ignition delay and explosion limits are controlled by the competition of the chain branching sequence (B), which promotes reaction, and the terminating reaction R5. Under these conditions, sequence A acts in effect as a terminating sequence, with positive sensitivity coefficients for reaction R3. Some additional termination steps may be active, depending on the pressure. At the lower limiting pressure, termination is dominated by radical diffusion to the wall and subsequent deactivation:

$$O \xrightarrow{+wall} inert$$

At increased pressure, the second explosion limit is controlled by (R5), together with the gas-phase termination sequence:

$$O_2 + O + M \rightleftharpoons O_3 + M$$

$$O_3 + O \rightleftharpoons O_2 + O_2$$

Only the first of these steps, the O_2 + O recombination, shows up in the sensitivity analysis, as the O_3 + O reaction is fast. Reactions of S and SO with CS_2 (R9)–(R11) could act as chain terminating steps, but under the investigated conditions, they cannot compete with S + O_2 and SO + O_2 .

The predicted ignition delay times and explosion limits depend strongly on the product branching fraction of the CS_2 + O reactions R3, R4, and R5. The good agreement between experimental results and modeling predictions support the accuracy of the low temperature measurements of the relative importance of channels R4 and R5.^{67–69} As pointed out by Azatyan et al.,⁸¹ reaction R4 is required to supply the necessary chain branching; without this step the CS_2/O_2 system would be nonexplosive at these temperatures.

For the flow reactor conditions (Figure 8), both the initiation reaction $(CS_2 + O_2)$ and the mechanisms of radical formation and termination are similar to those of the batch reactor

experiments. The chain branching sequence (B) competes with the propagating sequence (A) and the terminating reaction (R5). At the elevated temperature (1200 K) and increased radical levels, also reactions of CS with O (R13) and O_2 (R16) act to promote oxidation, whereas CS_2 + S reaction R10 inhibits oxidation.

Under the conditions of the high temperature shock tube experiments, thermal dissociation of CS_2 (R1b) becomes the most important initiation step. The $CS + O_2$ reaction (R16) is here sufficiently fast to contribute to radical generation, causing sequence A to become chain branching, along with sequence B. Reaction R5 is still the controlling terminating step.

The results of Figures 6-9 indicate that the modeling predictions are most accurate at low temperatures where calculated ignition delays and explosion limits are in good agreement with observed values. The predictive capability of the model under these conditions is facilitated by the knowledge of the low temperature branching fraction for CS₂ + O. At the higher temperatures of the flow reactor and shock tube experiments, the model appears to overpredict both the induction time for CS2 and the formation rate of [O] upon ignition. As discussed above, this indicates that the balance between initiation and chain branching in the model at higher temperatures is not correct. The rate constant for $CS_2 + O_2 R8$, which is a major initiation step, is quite uncertain because the reaction involves intersystem crossing from the triplet to the singlet surface. Also the CS₂ + O branching fraction, which is controlling the chain branching rate, is quite uncertain at elevated temperatures. It is unlikely, as assumed in the model, that the branching fraction is independent of temperature. Available data in the 250-500 K range⁶⁸ and at 1100 K⁷¹ indicate that the $k_4/k_{\rm tot}$ ratio decreases slightly with temperature. This would slow down the predicted formation rate of atomic oxygen, consistent with the high temperature results, but more work is needed to confirm this.

CONCLUSIONS

A detailed chemical kinetic model for oxidation of CS_2 has been developed and evaluated against experimental results from batch reactors, flow reactors, and shock tubes. Rate constants and product channels for a number of key reactions, i.e., $CS_2 + O_2$, $CS_2 + SO_2$, $CS + O_2$, and CS + SO, were determined through ab initio calculations. The $CS_2 + O_2$ reaction forms

OCS + SO, with the lowest energy barrier involving crossing from the triplet to the singlet surface. For CS + O_2 , which yields OCS + O, we found a high barrier to reaction, causing this step to be important only at elevated temperatures. The model predicts low temperature ignition delays and explosion limits quite accurately, whereas at higher temperatures the model appears to overpredict both the induction time for CS_2 oxidation and the formation rate of [O] upon ignition. The predictive capability of the model depends on the accuracy of the rate constant for the initiation step $CS_2 + O_2$, which is difficult to calculate due to the intersystem crossing, and the branching fraction for $CS_2 + O$, which is measured only at low temperatures. More work on these important reactions is desirable.

ASSOCIATED CONTENT

Supporting Information

Computed results for stationary points on the potential energy surfaces for the reactions $CS + O_2$, CS + SO, $CS_2 + SO_2$ and $CS_2 + O_2$ (geometries, rotational constants, frequencies, and energies) at the W1U or CBS-QB3 levels of theory. Thermodynamic data and reaction mechanism in Chemkin input format. This material is available free of charge via the Internet at http://pubs.acs.org

AUTHOR INFORMATION

Notes

The authors declare no competing financial interest.

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