Improved Real Gas Routines for Sandia's NASA Ames Flow Field Program

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IMPROVED REAL GAS ROUTINES FOR SANDIA'S NASA AMES FLOW FIELD PROGRAM

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ABSTRACT

The real gas subroutines in Sandia's version of the NASA Ames flow field code have been extensively revised. Using these modifications the required computer run time for a difficult high Mach number case has been reduced from 1330 seconds to 151 seconds.

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IMPROVED REAL GAS ROUTINES FOR SANDIA'S NASA AMES FLOW FIELD PROGRAM

INTRODUCTION

Sandia's version of the NASA Ames flow field code continues to be used extensively for calculating inviscid gas flow fields along bodies at zero angle of attack. This code in its original form requires extremely large amounts of computer time when calculating with the real equilibrium gas model. Over thirteen hundred seconds of CDC 6600 computer time are required to calculate the flow over a blunted 6° cone for a length of 60 nose radii when $M_\infty = 22$ and the altitude, h , is 30 km. This difficult case requires only 24 seconds using an ideal gas model. A less difficult case for the same geometry and using the real gas model for $M_\infty = 8$ and $h = 0.3$ km requires 530 seconds.

With a moderate amount of modifying subroutines RGAS, SERCH and ISENC these same real gas cases can now be computed in 152 seconds and 109 seconds, respectively. The modified code is 5 to 8 times faster than the original code. The time of computation for the original code was strongly dependent on the size of the compressibility factor Z in the equation of state ($p = Z\rho RT$). Some of these calculations have Z larger than 3 when total isentropic properties are being calculated. Ideal gas equations are used as a first approximation to the equilibrium gas solution. The real solution is then obtained using an iterative procedure. The ideal gas equations are not accurate for large Z , thus many iterations must be completed to obtain satisfactory real gas values. In the modified code, the methods used to iterate have been greatly improved.

This report discusses the function of the three subroutines listed above and outlines the recommended changes that must be incorporated into the original code to obtain the reduction in computing time described above.

SUBROUTINE RGAS

The function of the RGAS subroutine is to supply thermodynamic state properties for a gas in chemical equilibrium. Given two state properties the remaining properties

are calculated using the spline fit coefficients which are stored on Tape 9 (hereafter identified as RGAS data or RGAS Tables). If pressure and density are provided, the look up procedure is direct. If pressure and entropy are provided, the look up procedure is iterative. In this latter case the pressure and entropy are used to estimate density which in turn is used with pressure to determine entropy from the tables. This entropy is then compared with the given entropy. The density is incremented and an iteration procedure is followed until the given and calculated values of entropy agree satisfactorily. The final density and given pressure are then used to determine the remaining state properties; enthalpy, temperature, and sonic velocity.

Due to the general use of the RGAS subroutine in this program, a sample problem, a detailed outline and a FORTRAN listing are given in Appendix A, B and C. Prior to studying these Appendices it is important to understand how the spline fit data (Tape 9) is stored, retrieved and used. An outline of this concept follows.

Groups of spline fit coefficients for the four variables and their associated indexing parameters can be thought of as being contained in boxes. There are eleven boxes which are indexed by powers of density.

Sketch 1. Groups of Spline Coefficients

The process of obtaining real gas thermodynamic state properties for a given pressure and density using the information in these boxes can be divided into three general steps.

Step 1

Step one is to locate the two storage boxes that contain coefficients for the densities which bracket the given density. We are now interested only in these two boxes.

Step 2

Both of these boxes contain a complete range of coefficients for the four state variables. In order to isolate the sets of coefficients which are the most closely associated with the given pressure and density, a quantity F is calculated. F is a function of pressure, density and several constants, Figure 1. For each of the four state properties the indexing parameters (see Sketch 2) are searched to find the one that is closest to, but smaller than F .

Sketch 2. Details of Any One of the Boxes Shown in Sketch 1.

These four sets of spline fit coefficients and F are then used to calculate the state properties as follows.

$$Y = a_i + b_i F + c_i F^2 + d_i F^3$$

$$\text{where } Y = \begin{cases} \text{Sonic Velocity} & i = 1 \\ \text{Enthalpy} & i = 2 \\ \text{Temperature} & i = 3 \\ \text{Entropy} & i = 4 \end{cases}$$

and a_i , b_i , c_i and d_i are the spline fit coefficients for the cubic spline.

Step 3

Two values, one from each of the two boxes, have been obtained for each of the four state properties. The final values of the real gas thermodynamic state properties are obtained by interpolating between these boxes.

Several modifications have been made to RGAS. The logic flow has been revised. It is more readable and several of the multiple recalculations of branching variables have been eliminated. Originally numerous calls were made to SERCH for the polynomial coefficient values for F equal zero. Since these values never change, the revised program obtains these values once and stores them in an array for retrieval when needed.

The most significant improvement to RGAS is the reduction in the number of iterations of density when the input is pressure and entropy. This is accomplished by starting the iteration with the density obtained at the previous mesh point along the characteristic line.

SUBROUTINE SERCH

This subroutine searches the arrays filled from the RGAS tape to find the coefficients which correspond with the index F calculated in subroutine RGAS. The original technique, which is valid for data in random order, has been modified to take advantage of the fact that the tables are stored in monotonic order. The original Do Loop required searching through all data points. The revised program, lines 5-8

of Appendix D, uses the monotonic order to exit from the loop immediately after passing the desired value. This Do Loop has been shortened. It now fits "IN STACK"* which saves computer time.

The second time saving improvement consists of replacing the parameter list with a common block. In addition the coding now brackets the midpoint (NER) upon initially entering the subroutine. Consequently, no more than half of the table needs to be examined for each entry into SERCH. The most significant improvement is obtained with the first two revisions.

The third statement of the subroutine sets NOUT equal to 70,000. This is done in order to help debug the program in the event that the subroutine is called with a value of F less than the first position in the RGAS Table (zero for air). In case of this event the program is returned to subroutine RGAS and the calculations fail with a mode one type error on the CDC 6600.

SUBROUTINE ISENC

Subroutine ISENC contains an iteration scheme which is used to obtain state properties at point 2 given entropy (S) at points 1 and 2 and enthalpy (H) at point 1. Points 1 and 2 are adjoining points along a characteristic line. Since RGAS will not use S and H directly the pressure is approximated using an ideal gas equation. P and S are then used in RGAS to obtain the remaining state properties. Next an iteration procedure is used on pressure until the enthalpy calculated in RGAS agrees within a given tolerance to the given enthalpy.

The original subroutine is excessively time consuming; particularly when total isentropic state properties being calculated are quite different from ideal gas approximations. In these cases the ideal gas equations which are used for first

* Computer programmed instructions are stored in an instruction stack capable of holding eight 60-bit words. Instructions for inner "Do Loops" which can be contained within eight words fit "IN STACK" and are the fastest executing loops.

approximations are not accurate for real equilibrium gas, consequently many iterations must be performed.

In order to describe the improvements made to this program an outline of the original scheme will be given followed by an outline of the modifications made.

Original Subroutine Outline

1. Entropy and enthalpy are known.
2. Pressure (P) is estimated using pressure and Mach number at point 1 and the ideal gas equation.
3. Subroutine RGAS is called with P and S to get remaining state properties.
4. The H from RGAS is compared with given H. If not within given tolerance, P is improved as outlined below.
5. P_{initial} is decreased by a factor $Z\text{ROOT} = 0.97$ (Figure 2). Steps 3 and 4 are redone. Checks to see if P was changed in proper direction.
6. If change was in right direction and not too large (doesn't overshoot answer), another increment is taken ($P_{\text{initial}} \times 0.97 \times 0.97$).
7. If change is in wrong direction, P_{initial} is multiplied by $Z\text{ROOT} = 1.03$ (Figure 3). The process of using RGAS to obtain remaining state properties is repeated.
8. New P values are obtained using $P_{\text{initial}} \times Z\text{ROOT}^n$ until given H is passed.
9. When answer is bracketed between steps n and n + 1, the properties at the intermediate 1/3 intervals are calculated.
10. Using the four points obtained in Step 9 an interpolation scheme is used in subroutine INTER to calculate the final pressure. RGAS is then used to obtain the final state properties.

Improvements Made to Subroutine ISENC

In situations where the real gas answer differs appreciably from the initial ideal gas estimate the above technique consumes computer time excessively. In some

extreme cases the P had to be incremented in the order of 10^2 times by the factor (ZROOT = 0.97 or ZROOT = 1.03) before the convergence criterion was met. Consequently, the subroutine ISENC has been rewritten to change the convergence technique as follows. Step 1 through 7 given above remain the same. Step 8 is the same the first time through the subroutine. At this point the program stores the final n so that the next time the subroutine is used for a similar type calculation the stored value of n can be used to "jump" (n-3) intermediate steps. See Figure 4 for a typical case. If the "jump" passes the correct P then the subroutine automatically reduces the size of n to reduce the size of the next jump. This technique appreciably reduces the amount of computer time required. See section on results and conclusions.

A brief flow diagram is in Appendix E and a computer listing of this subroutine is given in Appendix F.

RESULTS AND CONCLUSIONS

In order to calculate the amount of computer time which can be saved by the various changes incorporated into the program, four runs were made for a short sphere-cone body in $M_\infty = 22$ flow. Initially the program was run to $X_{\max} = 2$ nose radii using the original program. Secondly the improvements made in subroutine ISENC were added and the program rerun. This reduces the required run time from 246.1 seconds to 158.6 seconds as shown in Table 1. Then corrections in SERCH were included and rerun. An additional 92 seconds of run time (Table 1) were saved. Finally the program was run with all improvements including those in RGAS. The percentages given in Table 1 are based on the current run compared with the previous run. Comparing the final run time with the original program, a savings of 79% in computer time is realized. Considering a longer body ($X_{\max} = 60$) a savings of 89% is realized. Results obtained with the improved method were identical to those obtained with the original program.

Therefore, it is of great importance that the original subroutines be modified if the program is to be used to obtain real equilibrium gas flow fields.

TABLE 1

Computer Times Required for the Program in Various
Stages of Improvement. ($X_{\max} = 2$, $M_{\infty} = 22$)

<u>Type of Program</u>	<u>Time (sec)</u>	<u>Time Saving (sec)</u>	<u>%</u>
Original Program	246.1	-	-
Improved ISENC Sub.	158.6	87.5	36%
Improved ISENC and SERCH Sub.	66.4	92.2	58%
Improved ISENC, SERCH and RGAS Sub.	51.2	15.2	23%

Figure 1. Function F Determined from Pressure and Density.

Figure 2. Iterative Sequence for P_{initial} Larger than P_{final} .

Figure 3. Iterative Sequence for P_{initial} Smaller than P_{final} .

Figure 4. Sequence for P_{initial} Smaller than P_{final} and (n - 3) Steps Skipped.

REFERENCES

1. Eaton, R. R. and Larson, D. E., "A Description of the Sandia version of the NASA-Ames Flow Field Code. Input-Output and Storage Locations," Sandia Laboratories, Albuquerque, New Mexico, SAND74-0096, November 1974.

APPENDIX A

SAMPLE CASE ILLUSTRATING OPERATION OF RGAS

The mechanics of subroutine RGAS are illustrated through the use of a sample case. It is assumed that the subroutine is entered with a pressure of 18599.449 psfa and density of 0.0005689099724 slugs/ft³, and the property index NUMX is equal to 4. Base 10 logarithms of normalized pressure (51)* and density (73) are used in RGAS. The applicable normalizing parameters are listed in Appendix B under line numbers 35-50. Thus, P equals .943984427646 and R is -0.6409352834.

Array TH consists of a series of "boxes" containing the desired coefficients for all four output variables. The specific set of coefficients is located by comparing F(89) with the indexing parameters in the corresponding boxes of the TH5 array. Arrays NDL and NDU define the beginning and end position respectively of each box in TH and TH5. Table A1 lists the directory information contained in NDL and NDU for each of the four output variables. The NR + 8 position is determined by the value of R which spans the range of $-7 < R < 3$. Table A2 contains a listing of the beginning portion of TH and TH5.

For the sample case NR(79-86) equals -1. The calculated value of F, 1.595155586, is used to search TH5 from 120 to 129 for sonic velocity data. This search, which is done in SERCH, can be verified by comparing the value of F against those in Table A2 from TH5(120) to TH5(129). The value nearest to but less than F is 1.3687 which means NOUT is 125. Thus the polynomial coefficients are TH(1,125), TH(2,125), TH(3,125) and TH(4,125). The resulting polynomial is solved as a function of F to give Y1 equal to 6.749088. The Do Loop which enters the final answer in AN(N1) is from line 97 to 109. The normalized values of the state properties, which were described in the body of the report as lying between two boxes, are calculated linearly a DX(87) distance between Y1 and Y2 (108). Results for this case and the remaining three output variables are listed in Table A3. Further insight can be obtained from Figure A1 which is a plot

* Numbers in the () refer to specific Fortran logic statements in Appendix C.

of the two boxes involved for the sonic speed property. The solutions for F are shown at Y1 and Y2 with the solution of AN(1) (not shown) located at 6.66 between them. Final answers are obtained from the intermediate results by using the dimensionalizing constants given from statement numbers 114 to 117.

Figure A1. Calculated Y Curves for Sonic Speed (Air) Using TH Coefficients Obtained from Table 2A.

Table A1

Directory Information, in Arrays NDL and NDU, Used to
Address Sets of Real Gas Data in Array TH

(NR + 8)	N1 = 1 Sonic Velocity		N1 = 2 Enthalpy		N1 = 3 Temperature		N1 = 4 Entropy	
	NDL	NDU	NDL	NDU	NDL	NDU	NDL	NDU
1	1	26	156	177	300	314	422	434
2	27	49	178	196	315	328	435	446
3	50	68	197	212	329	341	447	457
4	69	88	213	227	342	353	458	468
5	89	105	228	241	354	366	469	478
6	106	119	242	253	367	378	479	487
7	120	129	254	264	379	389	488	494
8	130	137	265	274	390	399	495	500
9	138	144	275	284	400	408	501	505
10	145	150	285	292	409	415	506	509
11	151	155	293	299	416	421	510	512

Table A2

Polynomial Coefficients, Stored in TH Array, for Spline Fits of the
Real Gas Properties; Sonic Velocity, Enthalpy, Temperature and Entropy

Spline Fit Coefficients (TH Array)					Index Parameters (TH5)	Spline Fit Coefficients (TH Array)					Index Parameters (TH5)
1.1358E+00	1.4134E+00	9.3266E-01	2.1549E-01	0.	1	1.5821E+00	-6.2785E-02	1.7530E+00	9.2478E-01	5.3228E-01	2
-1.9072E+00	9.6979E+00	-2.0497E+00	-3.6998E+00	6.0833E-01	3	-4.3795E+01	1.9088E+02	-2.6315E+02	1.2166E+02	7.0971E-01	4
2.2244E+01	-6.9682E+01	7.9186E+01	-2.8116E+01	7.8575E-01	5	-8.0921E+02	2.7478E+03	-3.1033E+03	1.1701E+03	8.8714E-01	6
8.0561E+02	-2.5685E+03	2.7308E+03	-9.6395E+02	9.1249E-01	7	-8.1065E+02	2.3678E+03	-2.2944E+03	7.4120E+02	9.8853E-01	8
-6.7693E+01	2.2380E+02	-2.3202E+02	7.9910E+01	1.0392E+00	9	2.4001E+01	-5.1546E+01	4.0595E+01	-9.2608E+00	1.1153E+00	10
-4.2154E+02	9.7038E+02	-7.4061E+02	1.8977E+02	1.2927E+00	11	-3.2843E+03	7.2720E+03	-5.3644E+03	1.3206E+03	1.3687E+00	12
6.6843E+03	-1.4201E+04	1.0054E+04	-2.3696E+03	1.3941E+00	13	-6.2203E+03	1.2546E+04	-8.4254E+03	1.8861E+03	1.4448E+00	14
9.0455E+02	-1.6845E+03	1.0485E+03	-2.1629E+02	1.4955E+00	15	-2.3185E+01	5.0234E+01	-3.2526E+01	8.2605E+00	1.6222E+00	16
-3.1055E+03	5.0163E+03	-2.6994E+03	4.8564E+02	1.8503E+00	17	7.1096E+02	-7.5966E+02	2.1195E+02	-3.0861E+00	1.9264E+00	18
1.9712E+04	-2.9777E+04	1.4982E+04	-2.5090E+03	1.9771E+00	19	-3.4509E+04	4.9232E+04	-2.3393E+04	3.7041E+03	2.0531E+00	20
-4.8051E+04	6.8701E+04	-3.2723E+04	5.1941E+03	2.1038E+00	21	2.0116E+04	-2.7513E+04	1.2544E+04	-1.9049E+03	2.1291E+00	22
-2.9384E+02	4.2735E+02	-2.0544E+02	3.4261E+01	2.2052E+00	23	-2.3071E+04	2.9518E+04	-1.2590E+04	1.7918E+03	2.3573E+00	24
3.3482E+04	-4.1066E+04	1.6771E+04	-2.2789E+03	2.4333E+00	25	-9.2285E+02	1.1023E+03	-4.5316E+02	6.5821E+01	2.4840E+00	26
1.1356E+00	1.4092E+00	8.6545E-01	3.2943E-01	0.	27	1.8593E+00	-2.5097E+00	7.8784E+00	-3.8100E+00	5.0694E-01	28
6.9568E+00	-3.5601E+01	7.1932E+01	-4.2656E+01	6.8437E-01	29	-3.7151E+01	1.6111E+02	-2.1838E+02	9.9291E+01	7.3506E-01	30
-1.1152E+01	5.0841E+01	-6.5047E+01	2.9130E+01	8.1110E-01	31	-3.9118E+02	1.2830E+03	-1.3965E+03	5.0862E+02	9.3783E-01	32
1.0025E+03	-3.0653E+03	3.1258E+03	-1.0591E+03	9.6318E-01	33	-7.7662E+02	2.1857E+03	-2.0402E+03	6.3499E+02	1.0139E+00	34
1.2564E+02	-3.0337E+02	2.4861E+02	-6.6554E+01	1.0899E+00	35	-4.7799E+01	1.1795E+02	-9.2529E+01	2.5515E+01	1.2420E+00	36
-1.0620E+03	2.3368E+03	-1.7102E+03	4.1854E+02	1.3941E+00	37	5.3184E+03	-1.0980E+04	7.5549E+03	-1.7300E+03	1.4448E+00	38
-6.1052E+03	1.1971E+04	-7.8163E+03	1.7014E+03	1.6955E+00	39	7.3953E+02	-1.3330E+03	8.0367E+02	-1.6024E+02	1.5462E+00	40
-3.2477E+01	6.5584E+01	-4.0824E+01	9.7124E+00	1.6729E+00	41	-2.5909E+03	4.0837E+03	-2.1444E+03	3.7678E+02	1.9010E+00	42
-1.9036E+03	3.1475E+03	-1.7247E+03	3.1512E+02	1.9771E+00	43	2.5708E+04	-3.7735E+04	1.8453E+04	-3.0043E+03	2.0278E+00	44
-4.3186E+04	6.0334E+04	-2.8080E+04	4.3554E+03	2.1038E+00	45	1.7491E+04	-2.3352E+04	1.0393E+04	-1.5403E+03	2.1798E+00	46
-7.5463E+02	1.0224E+03	-4.6085E+02	7.0678E+01	2.2559E+00	47	-2.9994E+04	3.7380E+04	-1.5530E+04	2.1527E+03	2.4080E+00	48
1.3718E+03	-1.0168E+03	1.3480E+02	2.2691E+01	2.4840E+00	49	1.1356E+00	1.3984E+00	8.4610E-01	3.3178E-01	0.	50
1.1096E+00	1.6035E+00	3.5060E-01	7.1110E-01	5.3228E-01	51	-6.4230E+00	2.7481E+01	-2.7024E+01	8.9609E+00	6.8437E-01	52
-6.6956E+00	3.8159E+01	-5.2880E+01	2.5133E+01	7.8575E-01	53	-5.5643E+01	1.9335E+02	-2.1617E+02	8.2111E+01	8.8714E-01	54
6.9473E+02	-2.0453E+03	2.0094E+03	-6.5518E+02	9.8853E-01	55	-7.5756E+02	2.0475E+03	-1.8353E+03	5.4871E+02	1.0646E+00	56
1.2199E+02	-2.8345E+02	2.2369E+02	-5.7520E+01	1.1406E+00	57	-6.7208E+01	1.5771E+02	-1.1919E+02	3.1307E+01	1.2927E+00	58
-5.4576E+02	1.1882E+03	-8.5797E+02	2.0764E+02	1.4448E+00	59	4.3793E+03	-8.7473E+03	5.8230E+03	-1.2898E+03	1.4955E+00	60
-3.6533E+03	6.9016E+03	-4.3391E+03	9.0986E+02	1.5462E+00	61	2.7973E+02	-4.6819E+02	2.6331E+02	-4.8059E+01	1.6222E+00	62
-1.9182E+02	3.2399E+02	-1.7843E+02	3.4644E+01	1.7996E+00	63	-2.8969E+03	4.4194E+03	-2.2465E+03	3.8212E+02	2.0024E+00	64
2.5449E+04	-3.6203E+04	1.7150E+04	-2.7877E+03	2.1038E+00	65	-4.9908E+04	6.7782E+04	-3.8676E+04	4.6270E+03	2.1798E+00	66
1.2484E+04	-1.6131E+04	6.9403E+03	-8.9612E+02	2.2385E+00	67	-1.1897E+03	1.4467E+03	-6.2824E+02	9.2411E+01	2.3319E+00	68

Table A2 (Con't)

Spline Fit Coefficients (TH Array)				Index Parameters (TH5)		Spline Fit Coefficients (TH Array)				Index Parameters (TH5)	
1.1356E+00	1.7827E+00	8.3940E-01	2.9771E-01	0.	69	2.0111E+00	-3.0448E+00	8.2052E+00	-3.7188E+00	5.3228E-01	70
1.2093E+01	-4.6748E+01	7.1137E+01	-3.3833E+01	7.7506E-01	71	-1.8905E+01	7.8286E+01	-9.5816E+01	4.0039E+01	8.1110E-01	72
-5.1456E+00	2.7823E+01	-3.4787E+01	1.5653E+01	9.1249E-01	73	1.8272E+01	-4.2710E+00	-1.6472E+01	1.4017E+01	1.0139E+00	74
6.9352E+02	-1.9465E+03	1.8238E+03	-5.6717E+02	1.0646E+00	75	-6.8626E+02	1.7753E+03	-1.5225E+03	4.3575E+02	1.1153E+00	76
1.1273E+02	-2.5062E+02	1.8963E+02	-4.6566E+01	1.1913E+00	77	-5.7284E+01	1.3091E+02	-9.5761E+01	2.4593E+01	1.3434E+00	78
4.7416E+02	-8.8794E+02	5.5392E+02	-1.1317E+02	1.4955E+00	79	1.1796E+03	-2.3430E+03	1.5488E+03	-3.3883E+02	1.5715E+00	80
-1.9126E+03	3.4742E+03	-2.0981E+03	4.2306E+02	1.4222E+00	81	1.4129E+02	-2.1728E+02	1.1289E+02	-1.8236E+01	1.6982E+00	82
-5.0501E+02	7.8253E+02	-4.0264E+02	7.0367E+01	1.9264E+00	83	-1.8152E+03	2.7218E+03	-1.3581E+03	2.2710E+02	2.1038E+00	84
2.5456E+04	-3.4917E+04	1.5958E+04	-2.4283E+03	2.1798E+00	85	-4.7283E+04	6.2085E+04	-2.7162E+04	3.9608E+03	2.2559E+00	86
1.0499E+04	-1.3361E+04	5.5615E+03	-7.7020E+02	2.1066E+00	87	5.1241E+02	-5.8495E+02	2.2089E+02	-2.6063E+01	2.4080E+00	88
1.1356E+00	1.3622E+00	8.2095E-01	2.7503E-01	0.	89	1.5681E+00	-7.5440E-01	4.1948E+00	-1.4604E+00	5.3228E-01	90
-4.2729E+00	1.8509E+01	-1.6167E+01	5.2861E+00	7.4041E-01	91	3.1203E+00	2.2250E+00	-7.6370E+00	5.7730E+00	8.8714E-01	92
1.9811E+02	-5.2795E+02	4.7225E+02	-1.3881E+02	1.0646E+00	93	-2.0334E+02	4.8287E+02	-3.7447E+02	9.7095E+01	1.1406E+00	94
3.2411E+01	-5.6555E+01	3.4478E+01	-5.5157E+00	1.2167E+00	95	-1.1412E+01	3.2213E+01	-2.4830E+01	7.5206E+00	1.3434E+00	96
-3.5144E+02	7.0062E+02	-4.6272E+02	1.0313E+02	1.5462E+00	97	1.6675E+03	-3.0823E+03	1.8995E+03	-3.8848E+02	1.6222E+00	98
-8.8781E+02	1.5413E+03	-8.8754E+02	1.7121E+02	1.6982E+00	99	4.4429E+01	-5.4331E+01	2.2225E+01	-1.5774E+00	1.7996E+00	100
-1.1741E+03	1.6913E+03	-8.1126E+02	1.3107E+02	2.0784E+00	101	1.1597E+04	-1.5312E+04	6.7334E+03	-9.8474E+02	2.2305E+00	102
3.6931E+03	-5.3381E+03	2.5481E+03	-3.9994E+02	2.1066E+00	103	-2.1165E+04	2.6683E+04	-1.1204E+04	1.5686E+03	2.3573E+00	104
9.6358E+02	-1.0785E+03	4.0134E+02	-4.8213E+01	2.4333E+00	105	1.1356E+00	1.3375E+00	7.8091E-01	2.7970E-01	0.	106
1.8198E+00	-1.0854E+00	5.9047E+00	-2.2839E+00	5.5763E-01	107	-1.8855E+01	6.7569E+01	-7.1669E+01	2.6406E+01	8.3645E-01	108
-3.2257E-01	1.1715E+01	-1.5655E+01	7.7121E+00	1.0392E+00	109	1.2696E+02	-3.3661E+02	3.0007E+02	-8.7157E+01	1.1913E+00	110
-1.7550E+02	4.1330E+02	-3.1842E+02	8.2559E+01	1.2673E+00	111	1.9108E+01	-2.9778E+01	1.7363E+01	-2.1573E+00	1.3687E+00	112
-1.8328E+01	5.2306E+01	-4.1401E+01	1.1645E+01	1.5969E+00	113	2.2121E+02	-4.3413E+02	2.8115E+02	-5.8534E+01	1.7236E+00	114
-1.5298E+02	2.6403E+02	-1.4813E+02	2.8635E+01	1.7996E+00	115	-6.8124E+01	1.1391E+02	-6.1128E+01	1.2054E+01	1.9517E+00	116
-7.8028E+02	1.0810E+03	-4.9867E+02	7.8014E+01	2.2559E+00	117	8.7647E+03	-1.1124E+04	4.7020E+03	-6.6052E+02	2.3826E+00	118
8.1918E+03	-1.0113E+04	4.1641E+03	-5.7041E+02	2.4586E+00	119	1.1356E+00	1.3080E+00	7.5597E-01	2.4676E-01	0.	120
1.5388E+00	-5.3265E-01	3.4681E+00	-1.0226E+00	5.5763E-01	121	-1.2616E+01	4.4373E+01	-4.3814E+01	1.5489E+01	8.8714E-01	122
3.0230E+01	-6.7511E+01	5.3570E+01	-1.2763E+01	1.1406E+00	123	-5.4371E+01	1.0950E+02	-6.7747E+01	1.4319E+01	1.2673E+00	124
1.8504E+01	-2.6110E+01	1.3703E+01	-1.2254E+00	1.3687E+00	125	3.2510E+01	-4.0236E+01	1.5770E+01	-4.0391E-01	1.6982E+00	126
-4.1489E+02	6.3528E+02	-3.2153E+02	5.5203E+01	1.8250E+00	127	1.7644E+01	-8.3872E+00	-2.5911E+00	2.5866E+00	1.9517E+00	128
-2.4394E+02	3.4091E+02	-1.5786E+02	2.5564E+01	2.1319E+00	129	1.1357E+00	1.2742E+00	7.1082E-01	2.3965E-01	0.	130
1.4474E+00	-6.7854E-02	2.5629E+00	-5.6200E-01	5.8298E-01	131	8.4285E+02	7.3994E+00	-7.8574E+00	3.7672E+00	1.0646E+00	132
6.2493E+01	-1.4225E+02	1.1145E+02	-2.7964E+01	1.3180E+00	133	-1.7960E+01	4.4220E+01	-3.1054E+01	8.1141E+00	1.4448E+00	134

Table A2 (Con't)

Spline Fit Coefficients (TH Array)				Index Parameters (TH5)		Spline Fit Coefficients (TH Array)				Index Parameters (TH5)	
-2.0474E+01	4.4816E+01	-2.8558E+01	7.0308E+00	1.4475E+00	135	-2.7403E+02	3.9393E+02	-1.8694E+02	3.0580E+01	1.9517E+00	136
-3.6211E+01	6.1931E+01	-3.2646E+01	6.7081E+00	2.7305E+00	137	1.1357E+00	1.2356E+00	6.6545E-01	2.2471E-01	0.	138
1.1671E+00	1.1576E+00	6.6750E-01	2.9269E-01	6.0833E-01	139	7.9766E-01	4.3401E+00	-4.0610E+00	2.2410E+00	1.1406E+00	140
1.1223E+01	-2.4150E+01	2.0719E+01	-4.7227E+00	1.3941E+00	141	-6.1021E+00	1.9135E+01	-1.3323E+01	3.8763E+00	1.5715E+00	142
1.8340E+02	-2.5972E+02	1.2341E+02	-1.8466E+01	2.0024E+00	143	-1.0019E+00	1.2382E+01	-9.1194E+00	2.8781E+00	2.2559E+00	144
1.1358E+00	1.1916E+00	6.2948E-01	1.8882E-01	0.	145	1.0524E+00	1.6076E+00	-6.2208E-02	5.7208E-01	6.0833E-01	146
1.0444E+00	2.5866E+00	-1.7240E+00	1.2822E+00	1.1660E+00	147	-1.8154E+01	3.5454E+01	-1.9927E+01	4.4983E+00	1.4955E+00	148
-7.3124E+00	2.0120E+01	-1.3025E+01	3.5382E+00	1.7489E+00	149	-1.1616E+02	1.4226E+02	-5.7552E+01	8.7554E+00	2.3066E+00	150
1.1357E+00	1.1445E+00	5.9747E-01	1.3866E-01	0.	151	1.0851E+00	1.4289E+00	6.8842E-02	4.6426E-01	5.0298E-01	152
1.4368E+00	1.2174E+00	-3.7138E-01	7.7574E-01	1.1406E+00	153	-2.0074E+01	3.7402E+01	-2.0384E+01	4.4008E+00	1.5969E+00	154
-8.3614E+00	2.1246E+01	-1.3030E+01	3.2986E+00	1.0771E+00	155	3.2035E+00	8.0853E+00	9.8407E+00	1.5976E+01	0.	156
2.1484E+00	1.8003E+01	-2.1161E+01	4.8192E+01	3.0416E-01	157	-7.4954E+01	3.9292E+02	-6.2677E+02	3.7303E+02	5.0298E-01	158
-6.9152E+02	3.2112E+03	-4.9209E+03	2.5539E+03	6.5902E-01	159	-1.3936E+03	6.1523E+03	-9.0250E+03	4.4617E+03	7.3506E-01	160
3.0934E+03	-1.0961E+04	1.2731E+04	-4.7579E+03	7.8575E-01	161	5.1151E+03	-1.8496E+04	2.2080E+04	-8.6188E+03	8.3645E-01	162
-9.7540E+03	2.9786E+04	-3.0168E+04	1.0224E+04	9.3783E-01	163	-1.5073E+04	4.5087E+04	-4.4028E+04	1.4901E+04	1.0139E+00	164
1.1425E+04	-2.7995E+04	2.2360E+04	-5.6880E+03	1.0899E+00	165	2.0165E+04	-4.8235E+04	3.7955E+04	-9.6853E+03	1.2420E+00	166
4.9501E+04	-1.1561E+05	8.9487E+04	-2.2815E+04	1.3434E+00	167	-1.2784E+05	2.6493E+05	-1.8264E+05	4.2036E+04	1.4194E+00	168
4.6061E+04	-7.9285E+04	4.4473E+04	-7.9113E+03	1.5208E+00	169	7.8894E+04	-1.3375E+05	7.4514E+04	-1.3420E+04	1.7236E+00	170
2.6760E+05	-4.4340E+05	2.4377E+05	-4.4242E+04	1.8757E+00	171	-4.3710E+05	6.4501E+05	-3.1640E+05	5.1833E+04	1.9771E+00	172
-1.8333E+06	2.6704E+06	-1.2957E+06	2.0967E+05	2.0784E+00	173	1.1172E+06	-1.4836E+06	6.5348E+05	-9.5170E+04	2.1545E+00	174
1.2164E+06	-1.5981E+06	6.9671E+05	-1.0047E+05	2.2812E+00	175	-6.9833E+05	7.5775E+05	-2.6899E+05	3.1406E+04	2.3826E+00	176
-1.7952E+06	2.1511E+06	-8.5808E+05	1.1430E+05	2.4586E+00	177	3.2035E+00	8.0599E+00	9.7527E+00	1.5594E+01	0.	178
2.2466E+00	1.7135E+01	-1.8892E+01	4.5678E+01	3.0416E-01	179	-5.1932E+01	2.7915E+02	-4.4109E+02	2.7236E+02	6.0833E-01	180
-1.5297E+03	6.5345E+03	-9.2674E+03	4.4237E+03	7.0971E-01	181	1.1324E+03	-3.6370E+03	3.6871E+03	-1.0760E+03	7.8575E-01	182
6.6038E+03	-2.2680E+04	2.5780E+04	-9.6198E+03	8.6179E-01	183	-1.3678E+03	2.7648E+03	-1.2925E+03	-1.8365E+01	9.3783E-01	184
-1.0401E+04	3.0634E+04	-2.9943E+04	9.7974E+03	9.8853E-01	185	1.1593E+03	-3.2860E+02	-2.3233E+03	1.5912E+03	1.0899E+00	186
1.0561E+04	-2.4994E+04	1.9238E+04	-4.6893E+03	1.1660E+00	187	6.7902E+04	-1.5127E+05	1.1194E+05	-2.7371E+04	1.3687E+00	188
-1.4744E+05	2.9670E+05	-1.9870E+05	4.4429E+04	1.4448E+00	189	3.8159E+04	-6.3039E+04	3.3721E+04	-5.6249E+03	1.5462E+00	190
2.8257E+05	-4.5245E+05	2.4053E+05	-4.4235E+04	1.8757E+00	191	-5.6359E+05	8.1082E+05	-3.8809E+05	6.2026E+04	2.0278E+00	192
-1.4925E+06	2.1354E+06	-1.0176E+06	1.6173E+05	2.1291E+00	193	1.0490E+06	-1.3590E+06	5.8381E+05	-8.2864E+04	2.2052E+00	194
1.6715E+06	-2.0863E+06	8.8618E+05	-1.2473E+05	2.3319E+00	195	-1.6732E+05	9.0103E+04	8.4966E+03	-6.7539E+03	2.4586E+00	196
3.2035E+00	7.9970E+00	9.6216E+00	1.5158E+01	0.	197	2.2934E+00	1.6641E+01	-1.7709E+01	4.3915E+01	3.0416E-01	198
-4.4969E+01	2.4148E+02	-3.7378E+02	2.3160E+02	6.0833E-01	199	-1.0157E+03	4.2257E+03	-5.8245E+03	2.7171E+03	7.3506E-01	200

Table A3

Data Extracted from Tables A1 and A2 to Obtain Intermediate Results for Sample Case

	NR + 8 = 7				NR + 9 = 8			Intermediate Results
	N1	NL = NDL(N1,7)	NU = NDU(N1,7)	Y1	NL = NDL(N1,8)	NU = NDU(N1,8)	Y2	AN(N1)
Normalized Sonic = AN(1) Velocity	1	120	129	6.749088	130	137	6.495157	6.657908
Normalized Enthalpy = AN(2)	2	254	264	293.914313	265	274	223.05058	268.4696
Temperature = AN(3)	3	379	389	7236.71625	390	399	7429.264	7305.85335
Entropy = AN(4)	4	488	494	44.6211646	495	500	38.90891	42.57009

APPENDIX B

FUNCTIONAL DESCRIPTION OF RGAS BY LINE NUMBERS

Line No.

10-14 Local variables are set equal to subroutine input parameters. NUM(NUMX) is either 4 and NUM5 is -1 with density and pressure input or NUM = 5 and NUM5 = 0 for pressure and entropy (S) input.

15 NTEST is negative for real gas. If zero or positive, ideal equations are used from Line 233, to the end. Real gas calculations are from 16 to 232.

16-50 Real gas data read in once, and many parameters initialized.

19-21 Read in from real gas tape (Tape 9) NDL, equivalence NDU, TH, WTMIX and C(1)-C(7).

23-24 Find and store the midpoint location between each NDL and NDU set in MIDL. This revision in SERCH allows a maximum of only half the distance from NDU to NDL to be searched in SERCH.

25-27 TH(5,N) data is stored in TH5(N), against which F is searched in SERCH. This single dimensioned array permits a faster more direct solution than the original method.

28-34 This coding originally was at 220 and is used whenever $F \leq 0.0$. The constant coefficients for each of the 4 variables, which is the solution for Y at $F = 0$, need to be determined only once and are stored in SAVFO for use at 220.

35-50 Many parameters are initialized here. To aid the discussion of the sample case (page 18) the significant variables will be identified for air, which is file 2 of Table 1, page 15, of Ref. 1.

Line No.

CONC = .99629144514 (air)

PO = 2116. Normalizing parameter for pressure

RO = .002488736 (air) Normalizing parameter for density

B = -.037985802 (air)

E = -.02828552 (air)

D = -.0017838726 (air)

FM = 2.508714 (air) Maximum value of F

51 Base 10 logarithm of input pressure normalized by PO is the value of P.

52 Branch on (NUM-5): For NUM = 4, to 73-77; for NUM = 5, to 53-72; for
NUM = 6 (impossible branch), terminate at 205.

53-72 NUM = 5 branch. P and S input provided.

53-55 RGAS will solve for correct R (normalized logarithm of density). Initial R
is calculated at 55. Solving Do Loop 97-109 for entropy and iterating on
incremented values of R, the proper solution is obtained when the cal-
culated entropy (119-120) matches input entropy, REAL, (normalized entropy,
S/RRR).

56-58 When RGAS is called from a subroutine which is iterating to the solution
of some variable, R converges with fewer iterations if the solution is
initiated using R from the previous call (stored in RLAST, 127) to RGAS
instead of the calculated R(55). This is normally the case if the cal-
culated value of R varies less than 10% from the calculated value on the
previous call and R is set to equal RLAST. If more than 10% variation
exists, the calculated value is used to begin the solution.

59-65 The minimum (RH) and maximum (RL) allowable range for R is established.
RH is calculated at 60-61. The maximum value of RL(59) is calculated by
solving the equation of F(59) for R with F = 0 (see Figure 1). RH, RL
and R must be within the range of -7.0 to 3.0.

66-72 Integer flags are set including NUMM = 5, NUMM9P = NUMM - 9 + NUM = 1,
NBOT = 4 and NUP = 4. The last two provide that the calculating Do 17
Loop, 97-109, only calculates entropy until final value of R is achieved.

Line No.

73-77 NUM = 4 branch. P and R input provided. The logarithm of the input density normalized by R0 is the value of R. NUMM = 5 and NUM9P = NUMM - 9 + NUM = 0, which will solve for all 4 variables (NBOT = 1 to NUP = 4) at one pass.

78-86 NR is determined from R. If R is positive, NR is integer value of R. Otherwise, NR = R - 1.0. $-7 \leq NR \leq 2$.

87-89 DX is the difference between R and NR. This is used to linearly interpolate between Y1 and Y2 which is calculated for F from coefficients from NR and NR + 1 respectively (108).

NR = NR + 8, provides positive integers 1-10 which can be used to address arrays NDL and NDU.

F is the variable used to search the TH5 RGAS data and is a function of variables P and R and constants B, E and D. See Figure 1 for the relationship of P, R, NR and F.

90 For F zero or positive go to 92.

91 For negative F, test that the value is nearly zero and if the absolute value is less than 10^{-8} , set F = 0.

94 Test NUMM9P. If $\neq 0$, go to 97. This branch is taken only for NUM = 5 when iterating to the solution of R.

95-96 Branch here for NUMM9P = 0. Always branch here for NUM = 4 and for NUM = 5 after final value of R is obtained. These tests determine if F is within the proper limits. If $F \leq 0$, branching is to 207 for the calculation of the 4 output variables. If F is too large, that is greater than FM(45), branching is to 186 for error message and termination.

97-109 This is the heart of RGAS which solves for up to 4 output variables and stores the normalized results in array AN.

AN(1) Normalized sonic velocity

AN(2) Normalized enthalpy, H

Line No.

AN(3) Temperature $^{\circ}\text{K}$

AN(4) Normalized entropy, S

Refer to the preceeding discussion for details (page 18). Subroutine SERCH searches RGAS data from TH5(NL) to TH5(NU) (also stored and used in Q) for the location exceeding or equal to F(89). The coefficients for the preceeding position (NOUT) are used to solve the third degree polynomial for Y1 at F. Y2 is found in the same manner using NDL(NL, NR+1) and NDU(NL, NR+1) for NL and NU. The answer is obtained by linearly interpolating between Y1 and Y2 and is placed in AN(NL) (108,87).

110 Branch on NUM-5. For NUM = 4 go to 113, leave RX unchanged, and output final answers.

111 Branch to here for NUM = 5. If still iterating on R(NUMM9P $\neq$ 0) go to 119 to test again on entropy.

112 Branch here for NUM = 5 and final R found and calculate density from R.

113-118 Calculate final values of sonic velocity, enthalpy, temperature ($^{\circ}\text{R}$) and entropy and exit from RGAS.

119-120 Calculate (percentage) difference between input entropy and calculated value and determine if within tolerance (10^{-4}), then branch to 122 or 129.

122-128 Branch here when difference is within tolerance and prepare for one final pass through (97-109) Do Loop to calculate AN(1)-AN(3). AN(4) is supplied with normalized input S, and RLAST is set equal to final R.

129-185 Branch here when convergence not obtained and calculate a new value of R.

131 Convergence must be obtained within 20 iterations or branch to 186, print error message, and exit from RGAS.

132-185 Value of R is adjusted by adding .3, -.3, or linearly interpolating between solutions of the last two iterations (151,155). R is always kept within the limits of RH to RL(59-65).

186-206 This point is entered from 96 to 131 for error message and exit from RGAS. However, if F is negative or zero, branching will go to 207 for calculation of 4 output variables and density. For positive F an error message with the values of some of the variables are printed.

Line No.

200-206 A maximum of nine calls to RGAS can pass through this error message and
exit RGAS without changing the values of any of the output variables.
On the tenth time the program will be terminated by a CALL EXIT.

207-232 Solution for F zero or negative called from 95 and 186. The RGAS
coefficients are solved once for $R = 0$ (28-34), stored in SAVFO, the
output variables placed in BN(1)-BN(4) and ANR array positions calculated.
Branching is next to the ideal gas solution (242-264) but for the ANR
positions with $L = 8$.

233-241 Begin ideal gas solution called from 15 using parameter list input
conditions, γ and density. Solutions of ANR positions are begun with
 $L = 0$.

242-264 Ideal gas solution is concluded here.

265-268 Normal exit from RGAS.

Appendix C. RGAS Fortran Listing

SUBROUTINE RGAS		CDC 6600 FTN V3.0-V34A OPT=1	03/10/75	11.37.59.	PAGE	1
	SUBROUTINE RGAS(PX,RX,AX,HX,TX, SX,RRX,GX,NTEST,NUMX,NGAS)	COUNT	90			
	CRGASR WALKER TEMP CONVERTED TO RANKINE	COUNT	91			
	DIMENSION TH(5,600),NDL(4,11),NDU(4,11),AN(4),C(7),ANR(17),BN(4)	COUNT	92			
	EQUIVALENCE(NDL(45),NDU)	COUNT	93			
5	COMMON /CSERCH/ F, TH5(600), NL, NU, NOUT, NER	COUNT	94			
	DIMENSION MIDL(4,11), SAVF0(4)	COUNT	95			
	DATA IFO / 0 /	COUNT	96			
	C	COUNT	97			
	C	COUNT	98			
10	P=PX	COUNT	99			
	S= SX	COUNT	100			
	R=RX	COUNT	101			
	NUM=NUMX	COUNT	102			
	NUM5 = NUM - 5	COUNT	103			
15	3 IF (NTEST) 7,8,8	COUNT	104			
	7 IF (NFIRST-NGAS) 10,9,10	COUNT	105			
	10 NFIRST=NGAS	COUNT	106			
	CALL LOCATE(NGAS,9)	COUNT	107			
	READ (9) (NDL(N),N=1,89)	COUNT	108			
20	NMM =NDL(89)	COUNT	109			
	READ (9) (TH(N),N=1,NMM),WTMIX,(C(N),N=1,7)	COUNT	110			
	REWIND 9	COUNT	111			
	DO 115 N=1,44	COUNT	112			
25	115 MIDL(N) = (NDL(N)+NDU(N))/2	COUNT	113			
	NDUMX = NDU(44)	COUNT	114			
	DO 120 N=1,NDUMX	COUNT	115			
	120 TH5(N) = TH(5,N)	COUNT	116			
	F=0.	COUNT	117			
	DO 21 N1=1,4	COUNT	118			
30	NL=NDL(N1,1)	COUNT	119			
	NU=NDU(N1,1)	COUNT	120			
	NER = MIDL(N1,1)	COUNT	121			
	CALL SERCH	COUNT	122			
35	21 SAVF0(N1) = TH(1,NOUT)	COUNT	123			
	CONC=WTMIX/28.966	COUNT	124			
	P0=2116.	COUNT	125			
	R0=.002498*CONC	COUNT	126			
	RRR=1716./CONC	COUNT	127			
	RRX=RRR	COUNT	128			
40	RT0=RRR*493.635	COUNT	129			
	SQPOR0 = SQRT(R0/P0)	COUNT	130			
	B=TH(NMM-2)	COUNT	131			
	E=TH(NMM-1)	COUNT	132			
	D=TH(NMM)	COUNT	133			
45	FM=2.1632+.3468*CONC	COUNT	134			
	AA=D*FM	COUNT	135			
	BB=E*FM*.1.	COUNT	136			
	CCC=B*FM	COUNT	137			
	RLAST = 0.0	COUNT	138			
50	RSTART = 100.0	COUNT	139			
	9 P =ALOG(P/P0)/2.3025851	COUNT	140			
	IF (NUM5)40,31,70	COUNT	141			
	31 REAL=S/RRR	COUNT	142			
	GG=(REAL-C(1)-C(2)*P)/(C(3)+P*(C(4)+P*C(5)))	COUNT	143			
55	R=C(6)+GG*C(7)*P	COUNT	144			

Appendix C (Continued)

SUBROUTINE	RGAS	CDC 4600 FTN V3.0-V34A OPT=1	03/10/75	11.37.59.	PAGE	2
	PER = ABS((RSTART - R) / R)	COUNT	145			
	RSTART = R	COUNT	146			
	IF (PFR.LT. 0.1) R = RLAST	COUNT	147			
	RL=P-R	COUNT	148			
60	CC=CCC-P	COUNT	149			
	RH=-CC*(1.+AA*CC/(BB*HB))/HB+.005	COUNT	150			
	IF(RH .LT. -7.) RH = -7.0	COUNT	151			
	IF (R .LT. RH) R = RH	COUNT	152			
65	IF(RL.GT.3.0) RL = 3.0	COUNT	153			
	IF(RL .LT.R) R = RL	COUNT	154			
	NUMB=0	COUNT	155			
	NIMX=0	COUNT	156			
	NUMM=5	COUNT	157			
	NUMM9P = NUMM - 9 + NUM	COUNT	158			
70	NBOT = 4	COUNT	159			
	NUP = 4	COUNT	160			
	GO TO 42	COUNT	161			
40	R = ALOG(R/R0)/2.3025851	COUNT	162			
	NUMM=5	COUNT	163			
75	NUMM9P = NUMM - 9 + NUM	COUNT	164			
	NBOT=1	COUNT	165			
	NUP=NUM	COUNT	166			
42	CONTINUE	COUNT	167			
	IF(R)11,12,13	COUNT	168			
80	11 NR = R - 1.0	COUNT	169			
	IF (NR .LT.-7) NR= -7	COUNT	170			
	GO TO 15	COUNT	171			
	12 NR = -1.0	COUNT	172			
	GO TO 15	COUNT	173			
85	13 NR = R	COUNT	174			
	IF(NR.GT.2) NR = 2	COUNT	175			
15	DX=R-FLOAT(NR)	COUNT	176			
	NR=NR+8	COUNT	177			
	F=(P-R-B)/(1.+R*(E+D*R))	COUNT	178			
90	IF(F)158,160,160	COUNT	179			
	158 IF (F .GT. -1.0E-08) F = 0.0	COUNT	180			
	160 CONTINUE	COUNT	181			
C	IF (NUMM-9+NUM) 22,162,22 ----- IF (NUMM9P)	COUNT	182			
	IF (NUMM9P)22,162,22	COUNT	183			
95	162 IF(F-.000001) 27,161,161	COUNT	184			
	161 IF(FM .LT. F) GO TO 44	COUNT	185			
	22 DO 17 N1=NBOT,NUP	COUNT	186			
	36 NL=NDL(N1,NR)	COUNT	187			
	NU=NDU(N1,NR)	COUNT	188			
100	NER = MIDL(N1,NR)	COUNT	189			
	CALL SERCH	COUNT	190			
	Y1 = TH(1,NOUT) +F*(TH(2,NOUT)+F*(TH(3,NOUT)+F*TH(4,NOUT)))	COUNT	191			
	NL=NDL(N1,NR+1)	COUNT	192			
	NU=NDU(N1,NR+1)	COUNT	193			
105	NER = MIDL(N1,NR+1)	COUNT	194			
	CALL SERCH	COUNT	195			
	Y2 = TH(1,NOUT) +F*(TH(2,NOUT)+F*(TH(3,NOUT)+F*TH(4,NOUT)))	COUNT	196			
	AN(N1)=Y1-DX*(Y2-Y1)	COUNT	197			
17	CONTINUE	COUNT	198			
110	IF (NUM5) 51,52,52	COUNT	199			

Appendix C (Continued)

SUBROUTINE RGAS		CDC 6600 FTM V3.0-V34A OPT=1		03/10/75	11:37.59.	PAGE	3
	52 IF(NUMM9P)39,108,39				COUNT	200	
	108 RX=R0*10.**R				COUNT	201	
	51 GO TO (121,122,123,124,124),NUM				COUNT	202	
	124 SX=AN(4)*RRR				COUNT	203	
115	123 TX= AN(3)*1.8				COUNT	204	
	122 HX=AN(2)*RT0				COUNT	205	
	121 AX=AN(1)/SQP0R0				COUNT	206	
	GO TO 109				COUNT	207	
	39 DIFF=ABS((REAL-AN(NUP))/REAL)				COUNT	208	
120	IF(DIFF-.0001) 37,37,38				COUNT	209	
	C NUMM9P = NUMM - 9 * NUM = 0				COUNT	210	
	37 NUMM9P = 0				COUNT	211	
	NUMM = 9 - NUM				COUNT	212	
	NBOT=1				COUNT	213	
125	NUP=3				COUNT	214	
	AN(4) = REAL				COUNT	215	
	RLAST = R				COUNT	216	
	GO TO 42				COUNT	217	
	38 NUMB=NUMB+1				COUNT	218	
130	NIMX=NIMX+1				COUNT	219	
	IF (NIMX .GT. 20) GO TO 44				COUNT	220	
	43 IF(NUMB-2)82,83,84				COUNT	221	
	82 IF(REAL-AN(NUP)) 85,37,86				COUNT	222	
	85 R1=R				COUNT	223	
135	S1=AN(NUP)				COUNT	224	
	R=R+.3				COUNT	225	
	IF (RL.LT.R) R = RL				COUNT	226	
	R2=R				COUNT	227	
	L = 0				COUNT	228	
140	GO TO 42				COUNT	229	
	86 R2=R				COUNT	230	
	S2=AN(NUP)				COUNT	231	
	R=R-.3				COUNT	232	
	IF (R.LT.RH) R=RH				COUNT	233	
145	R1 = R				COUNT	234	
	L=1				COUNT	235	
	GO TO 42				COUNT	236	
	83 IF(L) 91,90,91				COUNT	237	
	90 S2=AN(NUP)				COUNT	238	
150	R=R2				COUNT	239	
	IF(S1.NE.S2) R=R2-(S2-REAL)/(S2-S1)*(R2-R1)				COUNT	240	
	IF (RL.LT.R) R=RL				COUNT	241	
	GO TO 93				COUNT	242	
	91 S1=AN(NUP)				COUNT	243	
155	R=(REAL-S1)/(S2-S1)*(R2-R1)+R1				COUNT	244	
	IF (R.LT.RH) R=RH				COUNT	245	
	93 IF(R2-R) 104,37,105				COUNT	246	
	104 NUMB=1				COUNT	247	
	R1=R2				COUNT	248	
160	S1=S2				COUNT	249	
	L=0				COUNT	250	
	IF(R2+.3-RL) 210,211,211				COUNT	251	
	211 R2=RL				COUNT	252	
	R=R2				COUNT	253	
165	GO TO 42				COUNT	254	

Appendix C (Continued)

SUBROUTINE	RGAS	CDC 6600 FTN V3.0-V34A OPT=1	03/10/75	11.37.59.	PAGE	4
	210 R2=R2+.3			COUNT	255	
	R=R2			COUNT	256	
	GO TO 42			COUNT	257	
170	105 IF(R-R1) 106,37,42			COUNT	258	
	106 NUMB=1			COUNT	259	
	R2=R1			COUNT	260	
	S2=S1			COUNT	261	
	L=1			COUNT	262	
	IF(RH-R1+.3) 212,213,213			COUNT	263	
175	213 R1=RH			COUNT	264	
	R=R1			COUNT	265	
	GO TO 42			COUNT	266	
	212 R1=R1-.3			COUNT	267	
	R=R1			COUNT	268	
180	GO TO 42			COUNT	269	
	84 IF(REAL-AN(NUP)) 87,87,88			COUNT	270	
	87 R1=R			COUNT	271	
	GO TO 91			COUNT	272	
	88 R2=R			COUNT	273	
185	GO TO 90			COUNT	274	
	44 IF(F=.000001) 27,444,444			COUNT	275	
	444 NTIMES=NTIMES+1			COUNT	276	
	WRITE (6,190)			COUNT	277	
	190 FORMAT(1H0,10X,36HOUTSIDE TABLES IN RGAS ENTERING WITH)			COUNT	278	
190	WRITE (6,191) PX			COUNT	279	
	191 FORMAT(11X,2HP=,E13.6)			COUNT	280	
	IF(NUMS) 192,193,193			COUNT	281	
	192 CONTINUE			COUNT	282	
	WRITE (6,194) RX			COUNT	283	
195	194 FORMAT(11X,2HR=E13.6)			COUNT	284	
	GO TO 196			COUNT	285	
	193 CONTINUE			COUNT	286	
	WRITE (6,195) SX			COUNT	287	
	195 FORMAT(11X,2HS=,E13.6)			COUNT	288	
200	196 IF(NTIMES=10) 109,197,197			COUNT	289	
	197 CONTINUE			COUNT	290	
	WRITE (6,198)			COUNT	291	
	198 FORMAT(20X,28HEXIT CALLED ON TENTH FAILURE)			COUNT	292	
	GO TO 25			COUNT	293	
205	70 Z = Z*SQRT(-1.0)			COUNT	294	
	25 CALL EXIT			COUNT	295	
	27 L=8			COUNT	296	
	P=PX			COUNT	297	
	R=RX			COUNT	298	
210	IF (GTEST.EQ.GX) GO TO 440			COUNT	299	
	24 GTEST= GX			COUNT	300	
	L1=9			COUNT	301	
	Z2=R0/10.**7			COUNT	302	
	PR=-7.**8			COUNT	303	
215	PR=P0*10.**PR			COUNT	304	
	Z1=PR			COUNT	305	
	IF0 = IF0 + 1			COUNT	306	
	F = 0.0			COUNT	307	
	DO 23 N1=1,4			COUNT	308	
220	23 RN(N1) = SAVF0(N1)			COUNT	309	

Appendix C (Continued)

SUBROUTINE	RGAS	CDC 6600 FTN V3.0-V34A OPT=1	03/10/75	11.37.59.	PAGE	5
		BN(1)=BN(1)/SQP0R0		COUNT	310	
		BN(2)=BN(2)*RT0		COUNT	311	
		BN(3)=BN(3)*1.8		COUNT	312	
		BN(4)=BN(4)*RRR		COUNT	313	
225		ANR(9)=PR/(Z2 *BN(3))		COUNT	314	
		RRX=ANR(9)		COUNT	315	
		ANR(12)=BN(2)/BN (3)		COUNT	316	
		ANR(10)=1.+ANR(9)/(ANR(12)-ANR(9))		COUNT	317	
		ANR(11)=ANR(12)/ANR(10)		COUNT	318	
230		ANR(17)=BN(1)*BN(1)*Z2/Z1		COUNT	319	
		ANR(16)=BN(4)-ANR(11)*ALOG(Z1/Z2**ANR(10))		COUNT	320	
		GO TO 26		COUNT	321	
	8	L=0		COUNT	322	
		IF (GTEST.EQ.GX) GO TO 440		COUNT	323	
235	64	GTEST= GX		COUNT	324	
		L1=2		COUNT	325	
		ANR(1)=RRX		COUNT	326	
		ANR(2)=GX		COUNT	327	
		ANR(3)=ANR(1)/(ANR(2)-1.)		COUNT	328	
240		ANR(4)=ANR(1)+ANR(3)		COUNT	329	
		ANR(8)=49008.609-ANR(3)*ALOG(171.6/.0001**ANR(2))		COUNT	330	
	26	ANR(L+5)=1./ANR(L+2)		COUNT	331	
		ANR(L+6)=ANR(L+4)/ANR(L+1)		COUNT	332	
		ANR(L+7)=ANR(L+6)/ANR(L+2)		COUNT	333	
245		IF (NUM5)440,69,70		COUNT	334	
	440	QUOD=P/R**ANR(L+2)		COUNT	335	
		QUOT=P/R		COUNT	336	
		GO TO(65,66,67,68,69).NUM		COUNT	337	
	69	EX=S-ANR(L+8)		COUNT	338	
250		EX=EXP(EX/ANR(L+3))		COUNT	339	
		R=(P/EX)**ANR(L+5)		COUNT	340	
		QUOD=P/R**ANR(L+2)		COUNT	341	
		QUOT=P/R		COUNT	342	
		GO TO 67		COUNT	343	
255	68	S=ANR(L+8)+ANR(L+3)*ALOG(QUOD)		COUNT	344	
	67	T=QUOT/ANR(L+1)		COUNT	345	
	66	H=QUOT*ANR(L+6)		COUNT	346	
	65	LL=L+L1		COUNT	347	
		A=SQRT(ANR(LL)*QUOT)		COUNT	348	
260	30	AX=A		COUNT	349	
		HX=H		COUNT	350	
		TX= T		COUNT	351	
		SX=S		COUNT	352	
		RX=R		COUNT	353	
265	109	CONTINUE		COUNT	354	
		GTEST=-1.0E+30		COUNT	355	
		RETURN		COUNT	356	
		END		COUNT	357	

Appendix D. SERCH Fortran Listing

SUBROUTINE	SERCH	CDC 6600 FTN V3.0-V34A OPT=1	03/10/75	11.37.59.	PAGE	1
	SUBROUTINE SERCH				COUNT	358
	COMMON /CSERCH/ X, Q(600), NL, NU, NOUT, NER				COUNT	359
	NOUT = 70000				COUNT	360
5	IF (X.GE. Q(NER)) NL=NER				COUNT	361
	DO 10 I=NL,NU				COUNT	362
	IF(X.LT. Q(I)) RETURN				COUNT	363
	NOUT = I				SERCH	11
10	CONTINUE				SERCH	12
	RETURN				COUNT	364
10	END				COUNT	365

Appendix E

Subroutine ISENC Flow Diagram

(56) The difference of the calculated enthalpy (H2) and the known enthalpy (line 17) is stored in PROOTY

(59) The choices for the subscript I578 are as follows: I578 = 5 when the P is being iterated upon in the main Do Loop; I578 = 7 when the correct pressure has been bracketed and $n + 1/3$ n step to be calculated; I578 = 8 indicates the $n + 2/3$ n step is to be calculated

Appendix F. ISENC Fortran Listing

SUBROUTINE ISENC		CDC 6600 FTN V3.0-V34A OPT=1 03/10/75 11.37.59.		PAGE	1
	SUBROUTINE ISENC(P1,S1X,V1,V2,P2,RX,GX,NTESTX,NGASX,ER)	ISENC	2		
	CISENC LOMAX	ISENC	3		
	DIMENSION PROOT(10)	ISENC	4		
5	DATA NFSAV / 1 /	COUNT	1		
	DATA LIM1, LIM, LIM1 / 6, 5, 4 /	COUNT	2		
	DATA ZROOTL / .97 /	COUNT	3		
	DATA ZROOTH / 1.03 /	COUNT	4		
	C	ISENC	5		
10	ER=0.0	ISENC	6		
	R=RX	ISENC	8		
	G=GX	ISENC	9		
	NTEST=NTESTX	ISENC	10		
	NGAS=NGASX	ISENC	11		
	S1=S1X	ISENC	12		
15	CALL RGAS(P1,R1,A1,H1,T1,S1,R,G,NTEST,5,NGAS)	ISENC	13		
	HT=H1*.5*V1**2	ISENC	14		
	HTMV2=HT-.5*V2**2	ISENC	15		
	IF(HTMV2) 3,3,4	ISENC	16		
20	3 ER=-1.0	ISENC	17		
	GO TO 5	ISENC	18		
	4 IF(NTEST) 6,7,7	ISENC	19		
	7 PROOT(1)=G/(G-1.)	ISENC	20		
	PROOT(2)=(V1/A1)**2	ISENC	21		
	PROOT(3)=(V2/A1)**2	ISENC	22		
25	PROOT(4)=PROOT(2)-PROOT(3)	ISENC	23		
	PROOT(5)=(G-1.0)/2.0	ISENC	24		
	P2=P1*(1.0+(PROOT(5)*PROOT(4)))*PROOT(1)	ISENC	25		
	GO TO 5	ISENC	26		
30	6 PROOTX = P2	COUNT	5		
	IF(PROOTX) 1,1,2	ISENC	30		
	1 PROOTX=P1	ISENC	31		
	2 CONTINUE	ISENC	32		
	C	ISENC	33		
35	C PROOTX GUESSED VALUE OF ROOT	ISENC	34		
	C ZROOTH AND ZROOTL PERCENT INCREMENTS	ISENC	35		
	C	ISENC	36		
	NROOT=0	COUNT	6		
	ZROOT =ZROOTL	COUNT	7		
40	PROOT(9)=0.0	COUNT	8		
	MROOT = -1	COUNT	9		
	NFCHK = NFSAV	COUNT	10		
	NF = 1	COUNT	11		
	IS78 = 5	COUNT	12		
	PROOT(1)=PROOTX/ZROOT	COUNT	13		
45	DO 100 NROOT1=1,200	COUNT	14		
	PROOT(1) = PROOT(1)*ZROOT**NF	COUNT	15		
	PROOTZ=PROOT(1)	COUNT	16		
114	CONTINUE	COUNT	17		
	C	COUNT	18		
50	C INSERT EQUATION FOR ROOT	COUNT	19		
	C PROOTZ = FUNCTION	COUNT	20		
	C PROOTY IS ZERO FOR TRUE ROOT	COUNT	21		
	JISENC = JISENC + 1	COUNT	22		
	C	COUNT	23		
55	CALL RGAS(PROOTZ,R2,A2,H2,T2,S1,R,G,NTEST,5,NGAS)	COUNT	24		

Appendix F (Continued)

SUBROUTINE ISENC		CDC 6600 FTN V3.0-V34A OPT=1	03/10/75	11.37.59.	PAGE	2
	PROOTY=HTMV2-H2			COUNT	25	
	C			COUNT	26	
	C	END OF EQUATION FOR ROOT		COUNT	27	
	112	PROOT(1578) = PROOTY		COUNT	28	
60	C			COUNT	29	
	104	IF(NROOT) 102,101,125		COUNT	30	
	101	NROOT= -1		COUNT	31	
		GO TO 103		COUNT	32	
	108	ZROOT = ZROOTH		COUNT	33	
65		PROOT(1)=PROOTX/ZROOT		COUNT	34	
		GO TO 103		COUNT	35	
	107	IF(NF.EQ.1) GO TO 127		COUNT	36	
		NF = NF- 2		COUNT	37	
		IF (NF .LT. 1) NF=1		COUNT	38	
70		PROOT(1) = PROOT(2)		COUNT	39	
		NFCHK = NF		COUNT	40	
		GO TO 100		COUNT	41	
	127	NROOT=(PROOT(2)-PROOT(1))/3.		COUNT	42	
		PROOT(3)=PROOT(1)+DROOT		COUNT	43	
75		PROOT(4)=PROOT(3)+DROOT		COUNT	44	
		PROOTZ=PROOT(3)		COUNT	45	
		MROOT = 0		COUNT	46	
		NROOT=1		COUNT	47	
		I578 = 7		COUNT	48	
80		GO TO 114		COUNT	49	
	125	IF(MROOT)131,113,115		COUNT	50	
	113	PROOTZ=PROOT(4)		COUNT	51	
	C	PROOT(7)=PROOTY		COUNT	52	
		MROOT = 1		COUNT	53	
85		I578 = 8		COUNT	54	
		GO TO 114		COUNT	55	
	102	IF (SIGN(PROOT(6),PROOT(5))-PROOT(6)) 107,106,107		COUNT	56	
	106	IF (ARS(PROOT(5)) - ABS(PROOT(6)))103,103,108		COUNT	57	
	103	IF(PROOT(5))124,105,124		COUNT	58	
90	105	PROOT(10)=PROOT(1)		COUNT	59	
		GO TO 110		COUNT	60	
	124	PROOT(2)=PROOT(1)		COUNT	61	
		PROOT(6)=PROOT(5)		COUNT	62	
		NF=1		COUNT	63	
95		IF (NROOT1 .EQ.2) NF=NFSAV		COUNT	64	
	100	CONTINUE		COUNT	65	
	131	WRITE (6,111) PROOT(1), PROOT(2), PROOT(5), PROOT(		COUNT	66	
		16),PROOTX		COUNT	67	
	111	FORMAT(13H0 ER ISENC P1=E14.6+4H P2=E14.6+4H P5=E14.6+4H P6=E14.6+4		COUNT	68	
100		1H PG=E14.6)		COUNT	69	
		CALL ODD(9)		COUNT	70	
	C	PROOT(8)=PROOTY		COUNT	71	
	115	CALL NTERP(1,1,PROOT)		COUNT	72	
		IF (NFSAV .GT. 1) GO TO 220		COUNT	73	
105		IF(NROOT1 .LE.LIM) GO TO 220		COUNT	74	
		NFSAV=NROOT1 - LIM1		COUNT	75	
	C	PRINT 225, NFSAV		COUNT	76	
	225	FORMAT (* NEW LIMIT NF=* 14)		COUNT	77	
		GO TO 250		COUNT	78	
110	220	IF (NFSAV .GT. NFCHK) GO TO 240		COUNT	79	

Appendix F (Continued)

SUBROUTINE	ISENC	CDC 6600 FTN V3.0-V34A OPT=1	03/10/75	11.37.59.	PAGE	3
	IF (NROOT1-LIMP1)248,248,235			COUNT	80	
	235 NF=NFSAV			COUNT	81	
	NFSAV = (NROOT1 -LIMP1) + NFSAV			COUNT	82	
	C PRINT 238, NF, NFSAV			COUNT	83	
115	238 FORMAT (* INCREASE LIMIT FROM* I4 * TO*I4)			COUNT	84	
	GO TO 250			COUNT	85	
	248 IF (NROOT1 .GT. LIM1) GO TO 250			COUNT	86	
	NFCHK = NFSAV-1			COUNT	87	
120	240 NFSAV = NFCHK			COUNT	88	
	250 CONTINUE			COUNT	89	
	110 PROOTX=PROOT(10)			ISENC	90	
	C			ISENC	91	
	C PROOTX FINAL VALUE OF ROOT			ISENC	92	
	C			ISENC	93	
125	P2=PROOTX			ISENC	94	
	5 RETURN			ISENC	95	
	END			ISENC	96	

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