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Dr. # 979

TREE-NUREG-1052

for U.S. Nuclear Regulatory Commission

**EXPERIMENT DATA REPORT FOR SEMISCALE MOD-1
TEST S-05-3
(ALTERNATE ECC INJECTION TEST)**

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March 1977

MASTER

EG&G Idaho, Inc.

IDAHO NATIONAL ENGINEERING LABORATORY

ENERGY RESEARCH AND DEVELOPMENT ADMINISTRATION

IDAHO OPERATIONS OFFICE UNDER CONTRACT EY-76-C-07-1570

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TREE-NUREG-1052

EXPERIMENT DATA REPORT FOR SEMISCALE MOD-1

TEST S-05-3

(ALTERNATE ECC INJECTION TEST)

Approved:

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Semiscale Program

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TEST S-05-3

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by

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EG&G IDAHO, INC.

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PREPARED FOR THE
U.S. NUCLEAR REGULATORY COMMISSION
AND
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ABSTRACT

Recorded test data are presented for Test S-05-3 of the Semiscale Mod-1 alternate ECC injection test series. These tests are among several Semiscale Mod-1 experiments conducted to investigate the thermal and hydraulic phenomena accompanying a hypothesized loss-of-coolant accident in a pressurized water reactor (PWR) system.

Test S-05-3 was conducted from initial conditions of 2263 psia and 545°F to investigate the response of the Semiscale Mod-1 system to a depressurization and reflood transient following a simulated double-ended offset shear of the cold leg broken loop piping. During the test, cooling water was injected into the cold leg sides of the intact and broken loops and into the vessel upper plenum to simulate emergency core coolant injection in a PWR. For Test S-05-3, specifically the effects of upper plenum coolant injection on core thermal and system response were being investigated.

- The purpose of this report is to make available the uninterpreted data from Test S-05-3 for future data analysis and test results reporting activities. The data, presented in the form of graphs in engineering units, have been analyzed only to the extent necessary to assure that they are reasonable and consistent.

SUMMARY

Test S-05-3 was performed as part of the Semiscale Mod-1 portion of the Semiscale Program conducted by EG&G Idaho, Inc., for the United States Government. This test was part of the alternate ECC injection test series (Test Series 5) performed to investigate the response of the Mod-1 system to specific variations in coolant injection location. The test objective specific to Test S-05-3 was to provide data which can be used to assess the influence of upper plenum injection on the core and system response. Hardware configuration and test parameters were selected to yield a system response that simulates the response of a pressurized water reactor (PWR) to a hypothesized loss-of-coolant accident (LOCA) with subsequent refill and reflood.

Test S-05-3 utilized the Semiscale Mod-1 system equipped with a pressure vessel with a 40-rod electrically heated core; an intact loop with pump, steam generator, and pressurizer; a broken loop with simulated pump, simulated steam generator, and rupture assemblies; and a pressure suppression system with header, pressure suppression tank, and a heated steam supply system. High and low pressure coolant injection pumps and a coolant injection accumulator were provided for each system loop. An additional coolant injection accumulator was provided for the vessel upper plenum. Upper plenum injection flow rate was set to extend the time that coolant was injected. In addition, for Test S-05-3, four heater rods were intentionally unpowered to simulate the effects of control rod guide tubes and the power in three heater rods was increased to produce a slightly peaked profile.

The test was conducted from initial conditions of 2263 psia and 545°F (at the intact loop cold leg vessel inlet) with a simulated full size (200%) double-ended offset shear of the cold leg broken loop piping at an initial core power level of 1.49 MW, and an initial core inlet flow rate of 145 gpm. The instantaneous offset shear of the broken loop cold leg piping was simulated by simultaneous (within 10 msec) actuation of the rupture assemblies. After initiation of blowdown, power to the heated core was reduced to simulate the predicted heat flux response of nuclear fuel rods during a LOCA. Blowdown was accompanied by simulated emergency core coolant injected into the cold legs of the intact and broken loops and the vessel upper plenum.

Test S-05-3 was generally conducted as specified. Conditions which did not conform to the specified test configuration were considered acceptable for analysis purposes within the test objectives. The instrumentation used generally functioned as intended. Of 220 measurements taken, 218 produced usable data.

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EXPERIMENT DATA REPORT FOR SEMISCALE MOD-1

TEST S-05-3

(ALTERNATE ECC INJECTION TEST)

I. INTRODUCTION

The Semiscale Mod-1 experiments represent the current phase of the Semiscale Program conducted by EG&G Idaho, Inc., for the United States Government. The program, which is sponsored by the Nuclear Regulatory Commission through the Energy Research and Development Administration, is part of the overall program designed to investigate the response of a pressurized water reactor system to a hypothesized loss-of-coolant accident (LOCA). The underlying objectives of the Semiscale program are to quantify the physical processes controlling system behavior during a LOCA and to provide an experimental data base for assessing reactor safety evaluation models. The Semiscale Mod-1 program has the further objective of providing support to other experimental programs in the form of instrumentation assessment, optimization of test series, selection of test parameters, and evaluation of test results.

Test S-05-3 was conducted December 1, 1976 in the Semiscale Mod-1 system as part of the alternate ECC injection test series, (Test Series 5) which was designed to obtain thermal-hydraulic response data from blowdown, refill, and reflood transients in a simulated nuclear reactor with a heated core, to study system response to change in ECC injection location.

The purpose of this report is to present the test data in an uninterpreted but readily usable form for use by the nuclear community in advance of detailed analysis and interpretation. Section II briefly describes the system configuration, procedures, initial test conditions, and events that are applicable to Test S-05-3; Section III presents the data graphs and provides comments and supporting information necessary for interpretation of the data. A description of the overall Semiscale Program and test series, a more detailed description of the Semiscale Mod-1 system, and a description of the measurement and data processing techniques and uncertainties can be found in Reference 1.

II. SYSTEM, PROCEDURES, CONDITIONS, AND EVENTS FOR TEST S-05-3

The following system configuration, procedures, initial test conditions, and events are specific to Test S-05-3 as indicated.

1. SYSTEM CONFIGURATION AND TEST PROCEDURES

The Semiscale Mod-1 system used for this test consisted of a pressure vessel with internals, including a 40-rod core with 36 electrically heated rods; an intact loop with steam generator, pump, and pressurizer; a broken loop with simulated steam generator, simulated pump, and two rupture assemblies; coolant injection accumulators for the intact loop, the broken loop, and the vessel upper plenum; high and low-pressure injection pumps for each of the system loops; and a pressure suppression system with a suppression tank, header, and a heated steam supply system. For Test S-05-3, the volume of the lower plenum was reduced to 0.529 ft³ by the addition of a metal filler piece. The Semiscale Mod-1 experimental system configuration is described further in Reference 1. Figures 1 and 2 provide the system configuration for Test S-05-3.

For Test S-05-3, 33 rods of the 40-rod electrically heated core were operated at a peak power density of approximately 11.5 kW/ft, three rods (Rods D-4, E-4, and E-5) were operated at a peak power density of 12.1 kW/ft to yield a slightly peaked power profile, and four rods (Rods C-3, D-5, F-3, and F-6) were unpowered to simulate the effect of control rod guide tubes. The resulting total core power was approximately 1.49 MW.

In preparation for the test, the accumulators were filled with treated demineralized water, drained to the specified initial levels, and pressurized with nitrogen to 600 psig (300 psig for vessel accumulator). The system was filled with treated demineralized water and vented at strategic points to assure a liquid full system. Prior to warmup the system was pressurized to check for leakage, system instrumentation was checked, and transducer readings were initialized. Warmup to initial test conditions was accomplished with the heaters in the vessel core. Heatup of the broken loop piping was accomplished with bypass lines which served to allow circulation through the broken loop. During warmup, the purification and sampling systems were valved into the primary system to maintain water chemistry requirements and to provide a water sample at system conditions for subsequent analysis. At 100-°F temperature intervals during warmup, detector readings were sampled to allow the integrity of the measurement instrumentation and the operability of the data acquisition system to be checked.

Prior to the initial core power level being established, the pressure suppression system was pressurized to 35 psia with saturated steam from the steam supply system. After the core power was increased to 1.49 MW, initial test conditions were held for 10 minutes to establish equilibrium in the system. At the end of this period all auxiliary systems including the bypass lines were isolated to prevent blowdown through those systems.

Fig. 1 Semiscale Mod-1 system for cold leg break configuration -- schematic.

Fig. 2 Cross section of vessel with lower plenum filler.

The system was successfully subjected to a simulated double-ended cold leg break through two rupture assemblies and two blowdown nozzles, each having a break area of 0.00262 ft². Pressure to operate the rupture assemblies and initiate blowdown was taken from an accumulator system filled with water and pressurized to 2250 psig with gaseous nitrogen. Immediately (within 0.02 sec) after initiation of blowdown, the lines to the accumulator were again isolated. The effluent from the primary system was ejected into the pressure suppression system which was vented to maintain a constant pressure of 35 psia. At blowdown, power to the primary coolant circulation pump was reduced and the pump was allowed to coast down to a speed of 1640 rpm which was maintained for the duration of the test. During the blowdown transient, power to the electrically heated core was automatically controlled to simulate the thermal response of nuclear heated fuel rods.

For Test S-05-3, the coolant injection systems were arranged to discharge into both system loops at the cold leg injection points (Spool 14 and Spool 42) and into the vessel upper plenum at a point 13.5 in. above the cold leg centerline. The high pressure coolant injection pumps were started immediately after initiation of blowdown (0 sec) and continued to the end of the test (300 sec). Low pressure coolant injection was initiated 26 sec after blowdown at a system pressure of 150 psig and continued until test termination (300 sec). Coolant injection from the intact loop accumulator started 17 sec after blowdown, and nitrogen discharge began 65 sec after rupture and was terminated 98 sec after blowdown. The broken loop accumulator began injection 3.6 sec after blowdown and continued to exhaustion (70 sec). The vessel accumulator began injection at 22 sec and at a system pressure of 300 psig and was emptied 162 sec after blowdown initiation.

2. INITIAL TEST CONDITIONS AND SEQUENCE OF EVENTS

Conditions in the Semiscale Mod-1 system at initiation of blowdown are given in Tables I and II; the primary system water chemistry prior to blowdown is given in Table III; and the sequence of events relative to rupture is given in Table IV.

TABLE I
CONDITIONS AT BLOWDOWN INITIATION

	Test S-05-3	
	Measured ^[a]	Specified
Core power (MW)	1.486	1.444 $\pm$ 0.03
Intact loop cold leg fluid temperature (°F)	545	544 $\pm$ 2
Hot leg to cold leg temperature differential (°F)	66	66 $\pm$ 1
Pressurizer pressure (psia)	2263	2263 $\pm$ 25
Pressurizer water level (in.) ^[b]	24.1 ^[c]	27.1
Steam generator feedwater temperature (°F)	440	435 $\pm$ 10
Steam generator liquid level (from bottom of tube sheet) (in.)	111	116 $\pm$ 2
Fluid temperature in broken loop (pump side) (°F)	572	Not Specified
Fluid temperature in broken loop (vessel side) (°F)	542 ^[d]	Not Specified
Intact loop cold leg flow (gpm)	145	[e]
Pressure suppression tank water level (in.)	47.5	47.5 $\pm$ 1
Pressure suppression tank pressure (psia)	35	35
Pressure suppression tank water temperature (°F) ^[e]	60	Ambient

[a] Measured initial conditions are taken from process instrumentation read just prior to blowdown. Those measured conditions which did not meet the specified initial conditions were considered acceptable for analysis purposes within the test objectives.

[b] Pressurizer water level measured down from inside of top head. Level was specified in terms of differential pressure in the liquid level measuring system.

[c] Level shown corresponds to a pressurizer system volume of 0.61 ft³ (including surge line).

[d] Process instrumentation not used. Data taken from last digital scan 212 sec prior to blowdown initiation.

[e] Flow is not specified, since it must be adjusted to achieve the required differential temperature across the core.

TABLE II

PRIMARY COOLANT TEMPERATURE DISTRIBUTION PRIOR TO RUPTURE^[a]

	<u>Test S-05-3</u>	
	<u>Detector</u>	<u>Temperature (°F)</u>
Vessel lower plenum (upper portion above filler block)	TFV-LP-7	545
Intact loop hot leg (near vessel)	RBU-2	609
Intact loop cold leg (near pump inlet)	TFU-10	543
Intact loop cold leg (near vessel)	RBU-14A	542
Broken loop cold leg (near nozzle)	TFB-23	542
Broken loop hot leg (near vessel)	TFB-30	607
Broken loop cold leg (near nozzle)	TFB-42	600

[a] Data taken from final digital scan 212 sec before blowdown.

TABLE III
WATER CHEMISTRY PRIOR TO BLOWDOWN^[a]

	<u>Test S-05-3</u>
pH	9.30
Conductivity (μmho/cm)	162
Lithium (ppm)	10
Chlorides (ppm)	2.8
Fluorides (ppm)	0.52
Oxygen (ppm)	0.05
Total gas (cc/l)	209.3
Suspended solids (ppm)	1.4

[a] Water sample taken at a system pressure of about 2250 psia and a system temperature of about 540°F (cold leg).

TABLE IV
SEQUENCE OF EVENTS DURING TEST^[a]

Event	Time Relative To Rupture
Core power level established (min)	-6
Bypass lines valved out of system (sec)	-2.5
Blowdown initiated (sec)	0
Pump power reduced (sec)	0
High pressure injection system pumps started (sec) ^[b]	0
Steam generator feedwater and discharge valves closed (sec)	1
Core power decay transient started (sec)	2.7
Broken loop ECC accumulator valved in (sec) ^[b]	3.6
Intact loop ECC accumulator valved in (sec) ^[b]	17
Vessel ECC accumulator valved in (sec) ^[b]	22
Low pressure injection system pumps started (sec) ^[b]	26
Intact loop accumulator injection terminated (sec)	98
Vessel accumulator injection terminated (sec)	162
Core power tripped off (sec) ^[c]	300

[a] A time-controlled sequencer was used to control critical events during the test.

[b] Injection from ECC accumulators and high and low pressure injection system pumps does not start until system pressure drops below accumulator or pump pressure, respectively.

[c] Core power tripped manually at termination of test.

III. DATA PRESENTATION

The data from Semiscale Mod-1 Test S-05-3 are presented with brief comment. Processing analysis has been performed only to the extent necessary to obtain appropriate engineering units and to assure that the data are reasonable and consistent. In all cases, in converting transducer output to engineering units, a homogeneous fluid was assumed. Further interpretation and analysis should consider that sudden decompression processes such as those occurring during blowdown may have subjected the measurement devices to nonhomogeneous fluid conditions.

The performance of the system during Test S-05-3 was monitored by 220 detectors. The data obtained were recorded on both digital and analog data acquisition systems. The digital system was used to process the data presented in this report. The digital data were recorded at a sample rate of 57.5 points per sec. Long term plots (-20 to 300 sec) were compressed at a 20 to 1 ratio giving an effective sample rate of 2.875 points per sec. Short term plots (-6 to 42 sec) were compressed at a 3 to 1 ratio giving an effective sample rate of 19.17 points per sec. The analog system was used to provide better resolution capability (needed as input to various data analysis codes) and to provide redundancy.

The data are presented, in some instances, in the form of composite graphs to facilitate comparison of the values of given variables at several locations. The scales selected for the graphs do not reflect the obtainable resolution of the data. (The data processing techniques are described further in Reference 1.)

Figures 3 through 8 and Table V provide supporting information for interpretation of the data graphs shown in Figures 9 through 324, and provide relative locations of all detectors used during Test S-05-3. Table V groups the measurements according to measurement type; identifies the specific measurement location and the range of the detector and actual recording range of the data acquisition system; provides brief comments regarding the data; and references the measurements and comments to the corresponding figure. Figures 9 through 324 present all the blowdown and reflood data obtained. Time zero on the graphs is the time of rupture initiation. Appendix A provides information explaining posttest data processing for data conversion into engineering units and data adjustments.

Fig. 3 Semiscale Mod-1 system and instrumentation for cold leg break configuration -- isometric.

Fig. 6 Semiscale Mod-1 pressure vessel isometric showing instrumentation.

Fig. 7 Semiscale Mod-1 pressure vessel -- penetrations and instrumentation.

Fig. 8 Semiscale Mod-1 heated core -- plan view.

TABLE V
DATA PRESENTATION FOR SEMISCALE MOD-1 TEST S-05-3

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
FLUID TEMPERATURE					
	Chromel-Alumel thermocouples unless specified otherwise.				
<u>Intact Loop</u>		0 to 2300°F	0 to 591°F		
RBU-2	Hot leg, Spool 2, 46 in. from vessel center (platinum resistance bulb).	0 to 1000°F	0 to 1000°F	9, 10	
TFU-10	Cold leg, Spool 10, 144 in. from vessel center.			11, 12	
RBU-14A	Cold leg, Spool 14, 43 in. from vessel center, upstream of cold leg injection port (platinum resistance bulb).	0 to 1000°F	0 to 1000°F	11, 12	
TFU-14B	Cold leg, Spool 14, 39 in. from vessel center, downstream of cold leg injection port.			11, 12	
<u>Broken Loop</u>		0 to 2300°F	0 to 1017°F		
TFB-20	Cold leg, Spool 20, 21 in. from vessel center.			13, 14	
TFB-23	Cold leg, Spool 23, 91 in. from vessel center, upstream of vessel-side nozzle.			13, 14	
TFB-30	Hot leg, Spool 30, 16 in. from vessel center.			15, 16	
TFB-37	Cold leg, Spool 37, 276 in. from vessel center along hot leg, discharge of simulated steam generator.			15, 16	
TFB-42	Cold leg, Spool 42, 414 in. from vessel center along hot leg, upstream of pump-side nozzle.			15, 16	
<u>Inlet Annulus</u>	4 in. below cold leg centerline, 0.2 in. from vessel wall, Type J iron-constantan thermocouples.	0 to 1400°F	0 to 803°F		
TFV-ANN-4A	0°.				Thermocouple failed.
TFV-ANN-4M	180°.			17, 18	
<u>Downcomer Annulus</u>	Centered in annulus, Type J iron-constantan thermocouples.	0 to 1400°F	0 to 803°F		
TFV-ANN-35A	35 in. below cold leg centerline, 0°.			19, 20	
TFV-ANN-70A	70 in. below cold leg centerline, 0°.			19, 20	
TFV-ANN-115A	115 in. below cold leg centerline, 0°.			19, 20	
TFV-ANN-156A	156 in. below cold leg centerline, 0°. Type K.	0 to 2300°F	0 to 591°F	19, 20	
<u>Upper Plenum</u>		0 to 2300°F	0 to 1017°F		
TFV-UP-13	In upper plenum, 13.5 in. above cold leg centerline at 180°.			21, 22	
<u>Lower Plenum</u>	On fluid thermocouple rack, 1 in. from vessel center, 45° filler.	0 to 2300°F	0 to 1017°F		
TFV-LP-4	4.0 in. above top of lower plenum filler.			23, 24	
TFV-LP-7	7.0 in. above top of lower plenum filler.			23, 24	
<u>Core</u>					
TFV-CORE-IN	In core flow mixer box, 150 in. below cold leg centerline (a part of FDV-CORE-IN).	0 to 2300°F	0 to 1017°F	25, 26	

TABLE V (continued)

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
<u>Core Grid Spacers</u>					
<u>Grid Spacer 5</u>	55 in. below cold leg centerline, 21.5 in. above top of heated length.	0 to 2300°F	0 to 2382°F		
TFG-5CD-45	Thermocouple in space defined by Columns C and D, Rows 4 and 5.			27, 28	
<u>Grid Spacer 6</u>	76 in. below cold leg centerline, 1/2 in. above top of heated length.				
TFG-6AB-45	Thermocouple in space defined by Columns A and B, Rows 4 and 5.			29, 30	
TFG-6CD-45	Thermocouple in space defined by Columns C and D, Rows 4 and 5.			29, 30	
<u>Core Barrel Insulation Gap</u>					
TFV-LIG-UA	70 in. below cold leg centerline, 0°.	0 to 1400°F	0 to 803°F	31, 32	
<u>Vessel Filler Insulation Gap</u>					
TFV-FIG-156A	156 in. below cold leg centerline, 0°.	0 to 2300°F	0 to 1017°F	33, 34	
<u>ECC System</u>					
TFU-ECC-14	In ECC line leading to intact loop Spool 14.	0 to 2300°F	0 to 591°F	35, 36	
TFB-ECC-42	In ECC line leading to broken loop Spool 42.			37, 38	
TFV-ECC+13	In ECC line leading to vessel 13.5 in. above cold leg centerline.			39, 40	
<u>Steam Generator</u>					
TFU-SGFV	In feedwater line leading to steam generator.	0 to 2300°F	0 to 591°F	41, 42	
TFU-SG1	Secondary side, 12 in. above bottom of tube sheet.			43, 44	
TFU-SG2	Secondary side, 24 in. above bottom of tube sheet.			43, 44	Data have uncertain offset probably due to formation of secondary thermocouple junctions.
TFU-SG3	Secondary side, 40 in. above bottom of tube sheet.			43, 44	
<u>Pressurizer</u>					
TFU-PRI-Z	In surge line, near pressurizer exit, between turbine flowmeter and pressurizer.	0 to 2300°F	0 to 1017°F	45, 46	
<u>Pressure Suppression System</u>					
TF-PSS-33	33 in. from bottom of tank.	0 to 2300°F	0 to 591°F	47, 48	
TF-PSS-130	130 in. from bottom of tank.			47, 48	
<u>MATERIAL TEMPERATURE</u>					
<u>Intact Loop</u>					
TMU-15T16	Hot leg, Spool 1, top, 1/16 in. from pipe ID, 29 in. from vessel center.	0 to 2300°F	0 to 591°F	49, 50	
TMU-15T16	Cold leg, Spool 15, top, 1/16 in. from pipe ID, 17 in. from vessel center.		0 to 1017°F	49, 50	
<u>Broken Loop</u>					
TMB-20B16	Cold leg, Spool 20, bottom, 1/16 in. from pipe ID, 21 in. from vessel center.	0 to 2300°F	0 to 591°F	51, 52	
TMB-30T16	Hot leg, Spool 30, top, 1/16 in. from pipe ID, 16 in. from vessel center.		0 to 1017°F	51, 52	

TABLE V (continued)

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
<u>Vessel Filler</u>	Type J iron-constantan.	0 to 1400°F	0 to 803°F		
TMV-FI-4M	4 in. below cold leg centerline, 1/16 in. from filler ID, 180°.			53, 54	
TMV-FI-15A	15 in. below cold leg centerline, 1/16 in. from filler ID, 0°.			53, 54	
TMV-FI-35A	35 in. below cold leg centerline, 1/16 in. from filler ID, 0°.			53, 54	
TMV-FI-115A	115 in. below cold leg centerline, 1/16 in. from filler ID, 0°.			55, 56	
TMV-FI-156A	156 in. below cold leg centerline, 1/16 in. from filler ID, 0°.	0 to 2300°F	0 to 1017°F	55, 56	
TMV-FO-156A	156 in. below cold leg centerline, 0.65 in. from filler OD, 0°.	0 to 2300°F	0 to 1017°F	57, 58	
<u>Vessel Filler Insulator</u>	Outer surface of insulator, Type J iron-constantan thermocouples.	0 to 1400°F	0 to 803°F		
TIV-FO-35A	35 in. below cold leg centerline, 0°.			59, 60	
TIV-FO-35M	35 in. below cold leg centerline, 0°.			59, 60	
TIV-FO-70A	70 in. below cold leg centerline, 0°.			59, 60	
TIV-FO-115A	115 in. below cold leg centerline, 0°.			59, 60	
<u>Core Barrel</u>	Type J iron-constantan thermocouples	0 to 1400°F	0 to 803°F		
TMV-CI-70A	70 in. below cold leg centerline, 1/16 in. from core barrel ID, 0°.			61, 62	
TMV-CI-115A	115 in. below cold leg centerline, 1/16 in. from core barrel ID, 0°.			61, 62	
TMV-CO-70A	70 in. below cold leg centerline, 1/16 in. from core barrel OD, 0°.			63, 64	
TMV-CO-115A	115 in. below cold leg centerline, 1/16 in. from core barrel OD, 0°.			63, 64	
<u>Core Housing Filler</u>		0 to 2300°F	0 to 1017°F		
TMV-HF-115W	On core housing filler, 115 in. below cold leg centerline, 0.20 in. from outer surface, 315°.			65, 66	
TMV-HF-138W	On core housing filler, 138 in. below cold leg centerline, 0.20 in. from outer surface, 315°.			65, 66	
<u>Steam Generator</u>		0 to 2300°F	0 to 591°F		
TMU-SG1	On a steam generator tube, 12 in. above bottom of tube sheet, on tube OD.			67, 68	
TMU-SG2	On a steam generator tube, 24 in. above bottom of tube sheet, on tube OD.			67, 68	
TMU-SG3	On a steam generator tube, 48 in. above bottom of tube sheet, on tube OD.			67, 68	
<u>CORE HEATER CLADDING TEMPERATURES</u>	Chromel-Alumel thermocouples.				
<u>High Power Heaters</u>		0 to 2300°F	0 to 2382°F		
TH-D4-14 TH-D4-29	Heater at Column D, Row 4. Thermocouples 14 in. (270°) and 29 in. (315°) above bottom of core.			69, 70	
TH-D5-29	Heater at Column D, Row 5. Thermocouple 29 in. (225°) above bottom of core.			71, 72	
TH-E4-09 TH-E4-20 TH-E4-55	Heater at Column E, Row 4. Thermocouples 9 in. (180°), 28 in. (90°), and 55 in. (0°) above bottom of core.			73, 74	
TH-E5-25	Heater at Column E, Row 5. Thermocouple 25 in. (90°) above bottom of core.			75, 76	

TABLE V (continued)

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
Low Power Heaters		0 to 2300°F	0 to 2382°F		
TH-A4-09 TH-A4-29 TH-A4-39	Heater at Column A, Row 4. Thermo- couples 9 in. (105°), 29 in. (240°) and 39 in. (300°) above bottom of core.			77, 78	
TH-A5-29 TH-A5-45	Heater at Column A, Row 5. Thermo- couples 29 in. (180°) and 45 in. (255°) above bottom of core.			79, 80	
TH-B3-32	Heater at Column B, Row 3. Thermo- couple 32 in. (135°) above bottom of core.			81, 82	
TH-B5-29 TH-B5-33	Heater at Column B, Row 5. Thermo- couples 29 in. (150°) and 33 in. (45°) above bottom of core.			83, 84	
TH-B6-29	Heater at Column B, Row 6. Thermo- couple 29 in. (45°) above bottom of core.			85, 86	
TH-C2-38	Heater at Column C, Row 2. Thermo- couple 38 in. (225°) above bottom of core.			87, 88	
TH-C4-26 TH-C4-53	Heater at Column C, Row 4. Thermo- couples 26 in. (75°) and 53 in. (300°) above bottom of core.			89, 90	
TH-C5-28	Heater at Column C, Row 5. Thermo- couple 28 in. (315°) above bottom of core.			91, 92	
TH-C7-07 TH-C7-15	Heater at Column C, Row 7. Thermo- couples 7 in. (345°) and 15 in. (255°) above bottom of core.			93, 94	
TH-D1-21	Heater at Column D, Row 1. Thermo- couple 21 in. (330°) above bottom of core.			95, 96	
TH-D2-14 TH-D2-61	Heater at Column D, Row 2. Thermo- couple 14 in. (0°) and 61 in. (270°) above bottom of core.			97, 98	
TH-D3-29 TH-D3-39	Heater at Column D, Row 3. Thermo- couples 29 in. (150°) and 39 in. (210°) above bottom of core.			99, 100	
TH-D6-15 TH-D6-25	Heater at Column D, Row 6. Thermo- couples 15 in. (90°) and 25 in. (255°) above bottom of core.			101, 102	
TH-D7-20	Heater at Column D, Row 7. Thermo- couple 20 in. (60°) above bottom of core.			103, 104	
TH-D8-27 TH-D8-57	Heater at Column D, Row 8. Thermo- couples 27 in. (180°) and 57 in. (15°) above bottom of core.			105, 106	
TH-E1-33	Heater at Column E, Row 1. Thermo- couple 33 in. (60°) above bottom of core.			107, 108	
TH-E2-20 TH-E2-33	Heater at Column E, Row 2. Thermo- couples 20 in. (210°) and 33 in. (315°) above bottom of core.			109, 110	
TH-E3-05 TH-E3-20 TH-E3-24	Heater at Column E, Row 3. Thermo- couples 5 in. (15°), 20 in. (165°), and 24 in. (75°) above bottom of core.			111, 112	
TH-E6-00 TH-E6-28 TH-E6-37	Heater at Column E, Row 6. Thermo- couples 8 in. (150°), 28 in. (285°), and 37 in. (330°) above bottom of core.			113, 114	
TH-E7-44	Heater at Column E, Row 7. Thermo- couple 44 in. (195°) above bottom of core.			115, 116	
TH-E8-14 TH-E8-29 TH-E8-45	Heater at Column E, Row 8. Thermo- couples 14 in. (150°), 29 in. (225°), and 45 in. (300°) above bottom of core.			117, 118	
TH-F2-07 TH-F2-22 TH-F2-25	Heater at Column F, Row 2. Thermo- couples 7 in. (255°), 22 in. (105°), and 25 in. (0°) above bottom of core.			119, 120	
TH-F4-14 TH-F4-29 TH-F4-44	Heater at Column F, Row 4. Thermo- couples 14 in. (90°), 29 in. (165°), and 44 in. (210°) above bottom of core.			121, 122	TH-F4-44 failed.

TABLE V (continued)

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
<u>Low Power Heaters (continued)</u>		0 to 2300°F	0 to 2382°F		
TH-F5-20 TH-F5-26 TH-F5-33 TH-F5-53	Heater at Column F, Row 5. Thermocouples 20 in. (255°), 26 in. (165°), 33 in. (315°), and 53 in. (30°) above bottom of core.			123, 124	
TH-G3-13	Heater at Column G, Row 3. Thermocouple 13 in. (150°) above bottom of core.			125, 126	
TH-G4-29 TH-G4-33 TH-G4-38	Heater at Column G, Row 4. Thermocouples 29 in. (300°), 33 in. (225°), and 38 in. (30°) above bottom of core.			127, 128	
TH-G5-14 TH-G5-24	Heater at Column G, Row 5. Thermocouples 14 in. (45°) and 24 in. (330°) above bottom of core.			129, 130	
TH-H5-32	Heater at Column H, Row 5. Thermocouple 32 in. (45°) above bottom of core.			131, 132	
<u>PRESSURE</u>					
<u>Intact Loop</u>		0 to 3000 psi			
PU-13	Cold leg, Spool 13, 54 in. from vessel center.		0 to 4571 psia	133, 134	
PU-15L	Cold leg, Spool 15, 16 in. from vessel center, to atmosphere (low range).	0 to 500 psi	0 to 553 psia	135, 136	
<u>Broken Loop</u>		0 to 3,000 psi			
PB-23	Cold leg, Spool 23, 92 in. from vessel center, upstream of nozzle (tee off DP tap).		0 to 4364 psia	137, 138	
PB-37	Cold leg, Spool 37, 282 in. from vessel center along hot leg.		0 to 4402 psia	139, 140	
PB-42	Cold leg, Spool 42, 415 in. from vessel center along hot leg, upstream of pump-side nozzle (tee off DP tap).		0 to 4832 psia	139, 140	
PB-HN1	Pump-side nozzle, nozzle throat, 419 in. from vessel center along hot leg (tee off DP tap).		0 to 4666 psia	141, 142	
PB-CN1	Cold leg, Spool 23, vessel-side nozzle, nozzle throat, 96 in. from vessel center along cold leg, 45°.		0 to 2462 psia	143, 144	
<u>Vessel</u>					
PV-UP+10	In upper plenum, 10 in. above cold leg centerline, mounted on standoff, 20°.	0 to 2500 psi	0 to 3110 psia	145, 146	
PV-LP-166	In upper part of lower plenum, 166 in. below cold leg centerline, mounted on standoff, 225°.	0 to 3000 psi	0 to 2503 psia	145, 146	
<u>ECC System</u>		0 to 750 psi			
PU-ACC	In intact loop accumulator.		0 to 773 psia	147, 148	
PB-ACC	In broken loop accumulator.		0 to 746 psia	149, 150	
PV-ACC	In vessel accumulator.		0 to 742 psia	151, 152	
<u>Steam Generator</u>					
PU-SGSD	Secondary side steam dome.	0 to 3000 psi	0 to 2053 psia	153, 154	
<u>Pressurizer</u>					
PU-PRIZE	Pressurizer steam dome.	0 to 2500 psi	0 to 3171 psia	155, 156	
<u>Pressure Suppression System</u>					
P-PSS	Suppression tank top.	0 to 250 psi	0 to 347 psia	157, 158	

TABLE V (continued)

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
DIFFERENTIAL PRESSURE					
Elevation difference between transducer taps is zero unless otherwise specified.					
<u>Intact Loop</u>					
DPU-UP-3	Upper plenum 10.5 in. above cold leg centerline at 30° to hot leg, Spool 3, 62 in. from vessel center. Upper plenum tap is approximately 2 in. above Spool 3 tap.	+50 in. water	+4.9 psid	159, 160	Data acquisition system or detector saturated near t=0 sec.
DPU-3-7	Across steam generator, hot leg Spool 3, 62 in. from vessel center to cold leg Spool 7, 231 in. from vessel center. Spool 3 tap is approximately 10 in. above Spool 7 tap.	+500 in. water	+25 psid	161, 162	
DPU 7-10	Steam generator outlet to pump inlet, cold leg Spool 7, 231 in. from vessel center, to cold leg Spool 10, 141 in. from vessel center.	+50 in. water	+4.4 psid	163, 164	
DPU-12-10	Pump outlet to pump inlet, cold leg Spool 10, 75 in. from vessel center, to cold leg Spool 10, 141 in. from vessel center. Spool 10 tap is 10 in. below Spool 12 tap.	160 psi	150 psid	165, 166	
DPU-12-10L	Pump outlet to pump inlet, cold leg Spool 12, 75 in. from vessel center, to cold leg Spool 10, 141 in. from vessel center. Spool 10 tap is 10 in. below Spool 12 tap (low range).	+100 in. water	+4.9 psid	167, 168	Data acquisition system saturated to t=7 sec.
DPU-12-15	Across cold leg injection point, cold leg Spool 12, 75 in. from vessel center, to cold leg Spool 15, 16 in. from vessel center.	+100 in. water	+4.8 psid	169, 170	
DPU-15-1	Cold leg to hot leg; cold leg Spool 15, 16 in. from vessel center, to hot leg Spool 1, 31 in. from vessel center. Spool 15 tap is 8.5 in. below Spool 1 tap.	+500 in. water	+25 psid	171, 172	
DPU-15-1L	Cold leg to hot leg; cold leg Spool 15, 16 in. from vessel center, to hot leg Spool 1, 31 in. from vessel center. Spool 15 tap is 8.5 in. below Spool 1 tap (low range).	+100 in. water	+4.8 psid	173, 174	Data acquisition system saturated prior to t=0 sec.
DPU-15-1ANN	Cold leg Spool 15, 16 in. from vessel center, to inlet annulus, 9 in. below cold leg centerline at 225°. Spool 15 tap is 9 in. above inlet annulus tap.	+100 in. water	+4.9 psid	175, 176	
DPU-PRESLL	Pressurizer water level. Elevation difference between taps is 53 in. Lower tap is 3.5 in. above pressurizer exit.	+50 in. water	+2.5 psid	177, 178	
DPU-PR-4	Pressurizer bottom to Spool 4. Elevation difference between taps is 62 in. Spool 4 tap is 55 in. below pressurizer exit.	+1000 psi	+1357 psid	179, 180	
<u>Broken Loop</u>					
DPB-UP-30	Vessel upper plenum, 10.5 in. above cold leg centerline at 30°, to hot leg Spool 20, 18 in. from vessel center. Upper plenum tap is 2 in. above Spool 30 tap.	+100 in. water	+9.6 psid	181, 182	
DPB-21-1ANN	Cold leg Spool 21, 49 in. from vessel center, to vessel inlet annulus, 9 in. below cold leg centerline at 225°. Inlet annulus tap is 9 in. below Spool 21 tap.	+100 in. water	+4.8 psid	183, 184	
DPB-30-36L	Across entire simulated steam generator assembly, hot leg Spool 30, 18 in. from vessel center, to cold leg Spool 36 lower tap, 242 in. from vessel center. Spool 30 tap is 19 in. below Spool 36 lower tap.	+500 psi	+500 psid	185, 186	

TABLE V (continued)

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
Broken Loop (continued)					
DPB-32U-36L	Across simulated steam generator orifice assembly, hot leg Spool 32 upper tap, 73 in. from vessel center, to Spool 36 lower tap, 242 in. from vessel center. Spool 32 upper tap is 16 in. above Spool 36 lower tap.	±500 psi	±500 psid	187, 188	
DPB-36L-37	Across nozzle assembly, Spool 36 lower tap, 242 in. from vessel center along hot leg, to Spool 37, 282 in. from vessel center along hot leg. Spool 37 tap is 40 in. below Spool 36 lower tap.	±50 psi	±50 psid	189, 190	
DPB-37-38	Across turbine flowmeter and drag disc, cold leg Spool 37, 282 in. from vessel center along hot leg, to cold leg Spool 38, 305 in. from vessel center along hot leg. Spool 37 tap is 23 in. above Spool 38 tap.	±50 in. water	±5.1 psid	191, 192	
DPB-38-40	Across simulated pump, cold leg Spool 38, 305 in. from vessel center along hot leg, to cold leg Spool 40, 365 in. from vessel center along hot leg.	±1000 psi	±1353 psid	193, 194	
DPB-40-42	Across elbow leading to spool upstream of pump-side nozzle. Cold leg Spool 40, 365 in. from vessel center along hot leg, to Spool 42, 415 in. from vessel center along hot leg. Spool 40 tap is 40 in. below Spool 42 tap.	±50 in. water	±4.7 psid	195, 196	Physical conditions exceeded detector measurement capability from t=0 to t=1 sec
Vessel					
DPV-UP-1ANN	Upper plenum, 10.5 in. above cold leg centerline at 30° to inlet annulus, 9 in. below cold leg centerline at 225°. Elevation difference between taps is 19 in.	±300 in. water	±14.7 psid	197, 198	
DPV-0-96Q	Inlet annulus cold leg centerline at 90°, to 9 in. below cold leg centerline at 225°. Elevation difference between taps is 9 in.	±50 in. water	±2.6 psid	199, 200	
DPV-9-26QQ	Inlet annulus, 9 in. below cold leg centerline at 225°, to downcomer gap, 26 in. below cold leg centerline at 225°. Elevation difference between taps is 17 in.	±50 in. water	±2.4 psid	201, 202	
DPV-9-166QQ	Inlet annulus, 9 in. below cold leg centerline at 225°, to lower plenum, 166 in. below cold leg centerline at 225°. Elevation difference between taps is 157 in.	±300 in. water	±14.5 psid	203, 202	
DPV-26-55QM	Across part of downcomer, 26 in. (225°), to 55 in. (180°), below cold leg centerline. Elevation difference between taps is 29 in.	±50 in. water	±5.6 psid	205, 206	
DPV-55-110MM	Across part of downcomer, 55 in. (180°), to 110 in. (180°), below cold leg centerline. Elevation difference between taps is 55 in.	±100 in. water	±4.9 psid	207, 208	
DPV-110-156MQ	Across part of downcomer, 110 in. (180°), to 156 in. (225°), below cold leg centerline. Elevation difference between taps is 46 in.	±100 in. water	±4.9 psid	209, 210	
DPV-166-173QQ	Across part of lower plenum, 166 in. (225°), to 173 in. (225°), below cold leg centerline. Elevation difference between taps is 7 in.	±20 in. water	±0.98 psid	211, 212	
DPV-166Q-UP	Lower plenum, 166 in. below cold leg centerline at 225°, to upper plenum, 10.5 in. above cold leg centerline at 30°. Elevation difference between taps is 177 in.	±300 in. water	±14.7 psid	213, 214	

TABLE V (continued)

Measurement	Location and Comments ^[a]	Detector	Range ^[a]	Figure ^[a]	Measurement Comments ^[b]
			Data Acquisition System		
<u>Vessel (continued)</u>					
DPU-UP-3	Vessel upper plenum, 10.5 in. above cold leg centerline at 30°, to intact loop hot leg Spool 3, 62 in. from vessel center. Upper plenum tap is ~2 in. above Spool 3 tap.	+50 in. water	+4.9 psid	159, 160	
DPB-21-IANN	Cold leg Spool 21, 49 in. from vessel center, to vessel inlet annulus, 9 in. below cold leg centerline at 225°. Inlet annulus tap is 9 in. below Spool 21 tap.	+100 in. water	+4.8 psid	183, 184	
<u>Vessel Core</u>					
DPVC-89W-UP	Upper segment of active core region, 89 in. below cold leg centerline (315°), to upper plenum core tube, 10.5 in. above cold leg centerline (30°). Elevation difference between taps is 100 in.	+500 in. water	+24.3 psid	215, 216	Liquid may have boiled from sense lines; questionable data.
DPVC-89-106WQ	In active core region, upper segment, 89 in. below cold leg centerline (315°), to 106 in. below cold leg centerline (225°). Elevation difference between taps is 17 in.	+50 in. water	+5.0 psid	217, 218	
<u>CCC SYSTEM</u>					
DPU-ACC-TB	Top to bottom of intact loop accumulator. Elevation difference between taps is 108 in.	+500 in. water	+25 psid		Measurement failed due to air in sense lines.
DPB-ACC-TB	Top to bottom of broken loop accumulator tank. Elevation difference between taps is 84 in.	+50 in. water	+5.3 psid	219, 220	
DPV-ACC-TB	Top to bottom of vessel accumulator. Elevation difference between taps is 117 in.	+500 in. water	+2.5 psid	221, 222	
<u>Steam Generator</u>					
DPU-SG-SEC	Secondary side, differential pressure taps at 45 in. and 126 in. above bottom of tube sheet. Elevation difference between taps is 81 in.	+100 in. water	+12.8 psid	223, 224	
DPU-SG-DISC	Across venturi tube, 66 in. downstream from steam generator discharge.	+500 in. water	+24.5 psid	225, 226	
VOLUMETRIC FLOW RATE	Turbine flowmeter, bidirectional.				Data acquisition system range may exceed rated detector range; however, turbine response is linear to flow rates well beyond the rated range.
<u>Intact Loop</u>					
FTU-1	Hot leg, Spool 1, 18 in. from vessel center.	+20 to +400 gpm	+1200 gpm	227, 228	
FTU-9	Cold leg, Spool 9, 134 in. from vessel center.	+20 to +800 gpm	+1200 gpm	227, 228	
FTU-13	Cold leg, Spool 13, 64 in. from vessel center.	+20 to +800 gpm	+1200 gpm	229, 230	
FTU-15	Cold leg, Spool 15, 29 in. from vessel center.	+20 to +800 gpm	+1000 gpm	231, 232	
<u>Broken Loop</u>					
FTB-21	Cold leg, Spool 21, 58 in. from vessel center; 3-in. pipe.	+20 to +400 gpm	+1200 gpm	233, 234	
FTB-30	Hot leg, Spool 30, 25 in. from vessel center; 3-in. pipe.	+20 to +400 gpm	+800 gpm	235, 236	
FTB-37	Cold leg, Spool 37, 290 in. from vessel center along hot leg; 2-in. pipe.	+20 to +800 gpm	+800 gpm	235, 236	

TABLE V (continued)

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
<u>Core</u>					
FTV-CORE-IN	Entrance to core, ~158 in. below cold leg centerline.	+20 to +200 gpm	+900 gpm	237, 238	Data acquisition system saturated intermittently from t=25 to t=56 sec.
<u>ECC System</u>					
FTU-HPIS	In line immediately after HPIS pump for intact loop, 1/2-in. line.	+0.75 to +7.5 gpm	+2 gpm	239, 240	Noise signals prior to t=0 sec. Data between t=2 and t=29 sec are 60 cycle noise pickup except for data transients greater or smaller than the approximate 0.3 are gpm noise signal.
FTB-HPIS	In line immediately after HPIS pump for broken loop, 1/2-in. line.	+0.75 to +7.5 gpm	+2 gpm	241, 242	
FTU-LPIS	In line leading from LPIS pump for intact loop, 1/2-in. line.	+0.75 to +7.5 gpm	+10 gpm	243, 244	
FTB-LPIS	In line leading from LPIS pump for broken loop, 3/4-in. line.	+0.75 to +7.5 gpm	+2 gpm	245, 246	
FTU-ACC	In line leading from intact loop accumulator, 1-in. line.	+5 to +50 gpm	+75 gpm	247, 248	Data acquisition system saturated from t=74 to t=86 sec.
FTB-ACC	In line leading from broken loop accumulator, 1-in. line.	+2 to +20 gpm	+25 gpm	249, 250	
FTV-ACC	In line leading from vessel accumulator, 1-in. line.	+5 to +50 gpm	+50 gpm	251, 252	
<u>Pressurizer</u>					
FTU-PRIZE	Surge line.	+5 to +50 gpm	+100 gpm	253, 254	Apparent sticking of turbine bearings caused excessive and uncertain dead band.
<u>FLUID VELOCITY</u>					
<u>Downcomer</u>					
FTV-40A	40 in. below cold leg centerline, 0°.	+2.5 to 50 ft/sec	+50 ft/sec	255, 256	Apparent sticking of turbine bearings caused excessive and uncertain dead band.
FTV-40M	40 in. below cold leg centerline, 180°.	+2.5 to 50 ft/sec	+50 ft/sec	257, 258	Turbine bearings were stuck prior to blowdown initiation.
<u>MOMENTUM FLUX</u>					
	Drag disc, bidirectional.				Momentum flux reported only for -6 to 42 sec, except as noted. Drag disc data may exhibit significant temperature dependence. Drag disc data should be used only for short-term transient response.
<u>Intact Loop</u>					
FDU-1	Hot leg, Spool 1, 29 in. from vessel center; target size 0.875 in.	+200 to +11,500 lbm/ft-sec ²	+17,800 lbm/ft-sec ²	259	
FDU-5	Hot leg, Spool 5, 100 in. from vessel center; target size 1.0 in.	+1 to +2000 lbm/ft-sec ²	+4700 lbm/ft-sec ²	260	Detector saturated prior to t=0 sec.
FDU-10	Cold leg, Spool 10, 137 in. from vessel center; target size 0.875 in.	+200 to +104,000 lbm/ft-sec ²	+23,750 lbm/ft-sec ²	261	
FDU-13	Cold leg, Spool 13, 54 in. from vessel center; target size 0.875 in.	+200 to +14,800 lbm/ft-sec ²	+19,170 lbm/ft-sec ²	262	
FDU-15	Cold leg, Spool 15, 19 in. from vessel center; target size 0.875 in.	+200 to +14,500 lbm/ft-sec ²	+20,700 lbm/ft-sec ²	263	
<u>Broken Loop</u>					
FDB-21	Cold leg, Spool 21, 53 in. from vessel center, 3-in. pipe; target size 0.875 in.	+200 to +170,500 lbm/ft-sec ²	+125,000 lbm/ft-sec ²	264	Flow indicated prior to t=0 sec is not representative of physical conditions and should be zero; data after t=0 sec appears not to be offset.
FDB-23	Cold leg, Spool 23, 93 in. from vessel center, upstream of vessel side nozzle, 2-in. pipe; target size 0.406 in.	+200 to +121,000 lbm/ft-sec ²	+144,030 lbm/ft-sec ²	265	

TABLE V (continued)

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
Broken Loop (continued)					
FDB-30	Hot leg, Spool 30, 21 in. from vessel center, 3-in. pipe; target size 0.656 in.	+200 to +60,000 lbm/ft-sec ²	+47,500 lbm/ft-sec ²	266	
FDB-37	Cold leg, Spool 37, 284 in. from vessel center along hot leg, steam generator outlet, vertical pipe, 2-in. pipe; target size 0.406 in.	+200 to +121,000 lbm/ft-sec ²	+248,000 lbm/ft-sec ²	267	
FDB-42	Cold leg, Spool 42, 416 in. from vessel center along hot leg, upstream of pump-side nozzle, downstream of injection point, 2-in. pipe; target size 0.406 in.	+200 to +116,000 lbm/ft-sec ²	+100,500 lbm/ft-sec ²	268	
Vessel					
FDV-CORE 1H	In core flow mixer box 150 in. below cold leg centerline; target size 1.0 in.	+1 to +1125 lbm/ft-sec ²	+2000 lbm/ft-sec ²	269, 270	Figure 269 is long-term (-20 to 300 sec) plot; detector overranged near t=0 sec.
DENSITY					
Intact Loop					
		0.1 to 100 lbm/ft ³	0 to 100 lbm/ft ³		
GU-1VR	Hot leg, Spool 1, 24 in. from vessel center, vertical.			271, 272	
GU-1HZ	Hot leg, Spool 1, 26 in. from vessel center, horizontal.			271, 272	
GU-5VR	Hot leg, Spool 5, 96 in. from vessel center, vertical.			273, 274	
GU-10VR	Cold leg, Spool 10, 141 in. from vessel center, vertical.			273, 274	
GU-13VR	Cold leg, Spool 13, 59 in. from vessel center, vertical.			275, 276	Data values above 62.4 lbm/ft ³ do not reflect actual system density and were the result of detector photomultiplier tube nonlinearity.
GU-15VR	Cold leg, Spool 15, 23 in. from vessel center, vertical.			277, 278	
GU-15HZ	Cold leg, Spool 15, 20 in. from vessel center, horizontal.			277, 278	Data values above 62.4 lbm/ft ³ do not reflect actual system density and were the result of detector photomultiplier tube nonlinearity.
Broken Loop					
		0.1 to 100 lbm/ft ³	0 to 100 lbm/ft ³		
GB-21VR	Cold leg, Spool 21, 49 in. from vessel center, vertical.			279, 280	
GB-23VR	Cold leg, Spool 23, 92 in. from vessel center, vertical.			279, 280	
GB-30VR	Hot leg, Spool 30, 18 in. from vessel center, vertical.			281, 282	
GB-42VR	Cold leg, Spool 42, 415 in. from vessel center along hot leg, vertical.			281, 282	
Vessel					
		0.1 to 100 lbm/ft ³	0 to 100 lbm/ft ³		
GV-COR-150HZ	Core flow mixer box, 152 in. below cold leg centerline, horizontal, 0 to 180°.			283, 284	
GVLP-165HZ	Upper part of lower plenum, 165 in. below cold leg centerline, 1.724 in. below downcomer exit, horizontal, 0 to 180°.			285, 286	
GVLP-172HZ	Lower plenum, 172 in. below cold leg centerline, 8.729 in. below downcomer exit, horizontal, 90 to 270°.			285, 286	
Pressurizer					
GU-PRIZE	Surge line.	0.1 to 100 lbm/ft ³	0 to 100 lbm/ft ³	287, 288	

TABLE V (continued)

Measurement	Location and Comments ^[a]	Range ^[a]		Figure ^[a]	Measurement Comments ^[b]
		Detector	Data Acquisition System		
MASS FLOW RATE	Mass flow rate obtained by combining density (gamma attenuation technique) with volumetric flow rate (turbine flowmeter) or momentum flux (drag disc).	Range for mass flow is determined from range of individual detectors used in calculation.			Mass flow rate reported only for -6 to 42 sec for all drag discs except FDV-CORE-IN.
<u>Intact Loop</u>					
FDU-1, GU-1VR FTU-1, GU-1VR	Hot leg, Spool 1.			289 290, 291	
FDU-5, GU-5VR	Hot leg, Spool 5.			292	The drag disc transducer saturated prior to t=0 sec.
FTU-9, GU-10VR	Cold leg, Spool 9.			293, 294	
FDU-10, GU-10VR	Cold leg, Spool 10.			295	
FDU-13, GU-13VR FTU-13, GU-13VR	Cold leg, Spool 13.			296 297, 298	Nonlinearity in the density detector system caused density data near 62.4 lbm/ft ³ to be greater than 62.4 lbm/ft ³ .
FDU-15, GU-15VR FTU-15, GU-15VR	Cold leg, Spool 15.			299 300, 301	
<u>Broken Loop</u>					
FDB-21, GB-21VR FTB-21, GB-21VR	Cold leg, Spool 21.			302 303, 304	Flow prior to t=0 sec should be zero. Flow indicated by FDB-21 prior to t=0 is not representative of system physical conditions. Data after t=0 sec appear not to be offset.
FDB-23, GB-23VR	Cold leg, Spool 23			305	
FDB-30, GB-30VR FTB-30, GB-30VR	Hot leg, Spool 30.			306 307, 308	
FDB-42, GB-42VR	Cold leg, Spool 42.			309	
<u>Vessel</u>					
FDV-CORE-IN. GV-COR-150HZ	Entrance to core.			310, 311	Long-term (-20 to 300 sec) plots are also included for vessel core mass flow measurements. Detector FDV-CORE-IN overranged near t=0 sec.
FTV-CORE-IN. GV-COR-150HZ	Entrance to core.			312, 313	Data acquisition for FTV-CORE-IN saturated intermittently from t=25 to t=56 sec.
<u>Pressurizer</u>					
FTU-PRIZE GU-PRIZE	Pressurizer surge line.			314	Apparent sticking of turbine bearings caused excessive and uncertain dead band.
CORE CHARACTERISTICS					
PWRCOR T-1	Core power.		1600 kW	315, 316	
PWRCOR T-2	Core power.		1600 kW	315, 316	
VOLTCOR-T	Core voltage.		0 to 200 Vdc	317, 318	
AMPCOR-T	Core current.		0 to 10,000 A	319, 320	
PUMP CHARACTERISTICS					
PUMPU-CUR	Pump current.		0 to 25 A	321, 322	
PUMPU-RPM	Pump speed.		0 to 3600 rpm	323, 324	

[a] Statements at the beginning of a measurement category regarding location and comments, range, and figure apply to all subsequent measurements within the given category unless specified otherwise.

[b] Detectors which were subjected to overrange conditions during portions of the test were capable of withstanding these conditions without change in operating or measuring characteristics when the physical conditions were again within the detector range.

Fig. 9 Fluid temperature in intact loop hot leg (RBU-2), from -20 to 300 sec.

Fig. 10 Fluid temperature in intact loop hot leg (RBU-2), from -6 to 42 sec.

Fig. 11 Fluid temperature in intact loop cold leg (TFU-10, RBU-14A, TFU-14B), from -20 to 300 sec.

Fig. 12 Fluid temperature in intact loop cold leg (TFU-10, RBU-14A, TFU-14B), from -6 to 42 sec.

Fig. 13 Fluid temperature in broken loop, vessel side (TFB-20 and TFB-23), from -20 to 300 sec.

Fig. 14 Fluid temperature in broken loop, vessel side (TFB-20 and TFB-23), from -6 to 42 sec.

Fig. 15 Fluid temperature in broken loop, pump side (TFB-30, TFB-37, TFB-42), from -20 to 300 sec.

Fig. 16 Fluid temperature in broken loop, pump side (TFB-30, TFB-37, TFB-42), from -6 to 42 sec.

Fig. 17 Fluid temperature in downcomer annulus (TFV-ANN-4M), from -20 to 300 sec.

Fig. 18 Fluid temperature in downcomer annulus (TFV-ANN-4M), from -6 to 42 sec.

Fig. 19 Fluid temperature in downcomer annulus (TFV-ANN-35A, TFV-ANN-70A, TFV-ANN-115A, TFV-ANN-156A), from -20 to 300 sec.

Fig. 20 Fluid temperature in downcomer annulus (TFV-ANN-35A, TFV-ANN-70A, TFV-ANN-115A, TFV-ANN-156A), from -6 to 42 sec.

Fig. 21 Fluid temperature in upper plenum (TFV-UP+13), from -20 to 300 sec.

Fig. 22 Fluid temperature in upper plenum (TFV-UP+13), from -6 to 42 sec.

Fig. 23 Fluid temperature in lower plenum (TFV-LP-2, TFV-LP-4, TFV-LP-7), from -20 to 300 sec.

Fig. 24 Fluid temperature in lower plenum (TFV-LP-2, TFV-LP-4, TFV-LP-7), from -6 to 42 sec.

Fig. 25 Fluid temperature in core inlet (TFV-CORE-IN), from -20 to 300 sec.

Fig. 26 Fluid temperature in core inlet (TFV-CORE-IN), from -6 to 42 sec.

Fig. 27 Fluid temperature in core, Grid Spacer 5 (TFG-5CD-45), from -20 to 300 sec.

Fig. 28 Fluid temperature in core, Grid Spacer 5 (TFG-5CD-45), from -6 to 42 sec.

Fig. 29 Fluid temperature in core, Grid Spacer 6 (TFG-6AB-45 and TFG-6CD-45), from -20 to 300 sec.

Fig. 30 Fluid temperature in core, Grid Spacer 6 (TFG-6AB-45 and TFG-6CD-45), from -6 to 42 sec.

Fig. 31 Fluid temperature in core barrel insulation gap (TFV-CIG-70A), from -20 to 300 sec.

Fig. 32 Fluid temperature in core barrel insulation gap (TFV-CIG-70A), from -6 to 42 sec.

Fig. 33 Fluid temperature in filler insulation gap (TFV-FIG-156A); from -20 to 300 sec.

Fig. 34 Fluid temperature in filler insulation gap (TFV-FIG-156A), from -6 to 42 sec.

Fig. 35 Fluid temperature in intact loop ECC injection line (TFU-ECC-14), from -20 to 300 sec.

Fig. 36 Fluid temperature in intact loop ECC injection line (TFU-ECC-14), from -6 to 42 sec.

Fig. 37 Fluid temperature in broken loop ECC injection line (TFB-ECC-42), from -20 to 300 sec.

Fig. 38 Fluid temperature in broken loop ECC injection line (TFB-ECC-42), from -6 to 42 sec.

Fig. 39 Fluid temperature in vessel ECC injection line (TFV-ECC+13), from -20 to 300 sec.

Fig. 40 Fluid temperature in vessel ECC injection line (TFV-ECC+13), from -6 to 42 sec.

Fig. 41 Fluid temperature in steam generator feedwater line (TFU-SGFW), from -20 to 300 sec.

Fig. 42 Fluid temperature in steam generator feedwater line (TFU-SGFW), from -6 to 42 sec.

Fig. 43 Fluid temperature in steam generator secondary (TFU-SG1, TFU-SG2, TFU-SG3), from -20 to 300 sec.

Fig. 44 Fluid temperature in steam generator secondary (TFU-SG1, TFU-SG2, TFU-SG3), from -6 to 42 sec.

Fig. 45 Fluid temperature in pressurizer surge line (TFU-PRIZE), from -20 to 300 sec.

Fig. 46 Fluid temperature in pressurizer surge line (TFU-PRIZE), from -6 to 42 sec.

Fig. 47 Fluid temperature in pressure suppression tank (TF-PSS-33 and TF-PSS-130), from -20 to 300 sec.

Fig. 48 Fluid temperature in pressure suppression tank (TF-PSS-33 and TF-PSS-130), from -6 to 42 sec.

Fig. 49 Material temperature in intact loop (TMU-1T16 and TMU-15T16), from -20 to 300 sec.

Fig. 50 Material temperature in intact loop (TMU-1T16 and TMU-15T16), from -6 to 42 sec.

Fig. 51 Material temperature in broken loop (TMB-20B16 and TMB-30T16), from -20 to 300 sec.

Fig. 52 Material temperature in broken loop (TMB-20B16 and TMB-30T16), from -6 to 42 sec.

Fig. 53 Material temperature in vessel filler (TMV-FI-4M, TMV-FI-15A, TMV-FI-35A), from -20 to 300 sec.

Fig. 54 Material temperature in vessel filler (TMV-FI-4M, TMV-FI-15A, TMV-FI-35A), from -6 to 42 sec.

Fig. 55 Material temperature in vessel filler insulator (TMV-FI-115A and TMV-FI-156A), from -20 to 300 sec.

Fig. 56 Material temperature in vessel filler insulator (TMV-FI-115A and TMV-FI-156A), from -6 to 42 sec.

Fig. 57 Material temperature in vessel filler (TMV-F0-156A), from -20 to 300 sec.

Fig. 58 Material temperature in vessel filler (TMV-F0-156A), from -6 to 42 sec.

Fig. 59 Material temperature in vessel filler insulator (TIV-F0-35A, TIV-F0-35M, TIV-F0-70A, TIV-F0-115A), from -20 to 300 sec.

Fig. 60 Material temperature in vessel filler insulator (TIV-F0-35A, TIV-F0-35M, TIV-F0-70A, TIV-F0-115A), from -6 to 42 sec.

Fig. 61 Material temperature in core barrel (TMV-CI-70A and TMV-CI-115A), from -20 to 300 sec.

Fig. 62 Material temperature in core barrel (TMV-CI-70A and TMV-CI-115A), from -6 to 42 sec.

Fig. 63 Material temperature in core barrel (TMV-CO-70A and TMV-CO-115A), from -20 to 300 sec.

Fig. 64 Material temperature in core barrel (TMV-CO-70A and TMV-CO-115A), from -6 to 42 sec.

Fig. 65 Material temperature on core housing filler (TMV-HF-115W and TMV-HF-138W), from -20 to 300 sec.

Fig. 66 Material temperature on core housing filler (TMV-HF-115W and TMV-HF-138W), from -6 to 42 sec.

Fig. 67 Material temperature in steam generator (TMU-SG1, TMU-SG2, TMU-SG3), from -20 to 300 sec.

Fig. 68 Material temperature in steam generator (TMU-SG1, TMU-SG2, TMU-SG3), from -6 to 42 sec.

Fig. 69 Core heater temperature, Rod D-4 (TH-D4-14 and TH-D4-29), from -20 to 300 sec.

Fig. 70 Core heater temperature, Rod D-4 (TH-D4-14 and TH-D4-29), from -6 to 42 sec.

Fig. 71 Core heater temperature, Rod D-5 (TH-D5-29), from -20 to 300 sec.

Fig. 72 Core heater temperature, Rod D-5 (TH-D5-29), from -6 to 42 sec.

Fig. 73 Core heater temperature, Rod E-4 (TH-E4-09, TH-E4-28, TH-E4-55), from -20 to 300 sec.

Fig. 74 Core heater temperature, Rod E-4 (TH-E4-09, TH-E4-28, TH-E4-55), from -6 to 42 sec.

Fig. 75 Core heater temperature, Rod E-5 (TH-E5-25), from -20 to 300 sec.

Fig. 76 Core heater temperature, Rod E-5 (TH-E5-25), from -6 to 42 sec.

Fig. 77 Core heater temperature, Rod A-4 (TH-A4-09, TH-A4-29, TH-A4-39), from -20 to 300 sec.

Fig. 78 Core heater temperature, Rod A-4 (TH-A4-09, TH-A4-29, TH-A4-39), from -6 to 42 sec.

Fig. 79 Core heater temperature, Rod A-5 (TH-A5-29 and TH-A5-45), from -20 to 300 sec.

Fig. 80 Core heater temperature, Rod A-5 (TH-A5-29 and TH-A5-45), from -6 to 42 sec.

Fig. 81 Core heater temperature, Rod B-3 (TH-B3-32), from -20 to 300 sec.

Fig. 82 Core heater temperature, Rod B-3 (TH-B3-32), from -6 to 42 sec.

Fig. 83 Core heater temperature, Rod B-5 (TH-B5-29 and TH-B5-33), from -20 to 300 sec.

Fig. 84 Core heater temperature, Rod B-5 (TH-B5-29 and TH-B5-33), from -6 to 42 sec.

Fig. 85 Core heater temperature, Rod B-6 (TH-B6-29), from -20 to 300 sec.

Fig. 86 Core heater temperature, Rod B-6 (TH-B6-29), from -6 to 42 sec.

Fig. 87 Core heater temperature, Rod C-2 (TH-C2-38), from -20 to 300 sec.

Fig. 88 Core heater temperature, Rod C-2 (TH-C2-38), from -6 to 42 sec.

Fig. 89 Core heater temperature, Rod C-4 (TH-C4-26 and TH-C4-53), from -20 to 300 sec.

Fig. 90 Core heater temperature, Rod C-4 (TH-C4-26 and TH-C4-53), from -6 to 42 sec.

Fig. 91 Core heater temperature, Rod C-5 (TH-C5-28), from -20 to 300 sec.

Fig. 92 Core heater temperature, Rod C-5 (TH-C5-28), from -6 to 42 sec.

Fig. 93 Core heater temperature, Rod C-7 (TH-C7-07 and TH-C7-15), from -20 to 300 sec.

Fig. 94 Core heater temperature, Rod C-7 (TH-C7-07 and TH-C7-15), from -6 to 42 sec.

Fig. 95 Core heater temperature, Rod D-1 (TH-D1-21), from -20 to 300 sec.

Fig. 96 Core heater temperature, Rod D-1 (TH-D1-21), from -6 to 42 sec.

Fig. 97 Core heater temperature, Rod D-2 (TH-D2-14 and TH-D2-61), from -20 to 300 sec.

Fig. 98 Core heater temperature, Rod D-2 (TH-D2-14 and TH-D2-61), from -6 to 42 sec.

Fig. 99 Core heater temperature, Rod D-3 (TH-D3-29 and TH-D3-39), from -20 to 300 sec.

Fig. 100 Core heater temperature, Rod D-3 (TH-D3-29 and TH-D3-39), from -6 to 42 sec.

Fig. 101 Core heater temperature, Rod D-6 (TH-D6-15 and TH-D6-25), from -20 to 300 sec.

Fig. 102 Core heater temperature, Rod D-6 (TH-D6-15 and TH-D6-25), from -6 to 42 sec.

Fig. 103 Core heater temperature, Rod D-7 (TH-D7-20), from -20 to 300 sec.

Fig. 104 Core heater temperature, Rod D-7 (TH-D7-20), from -6 to 42 sec.

Fig. 105 Core heater temperature, Rod D-8 (TH-D8-27 and TH-D8-57), from -20 to 300 sec.

Fig. 106 Core heater temperature, Rod D-8 (TH-D8-27 and TH-D8-57), from -6 to 42 sec.

Fig. 107 Core heater temperature, Rod E-1 (TH-E1-33), from -20 to 300 sec.

Fig. 108 Core heater temperature, Rod E-1 (TH-E1-33), from -6 to 42 sec.

Fig. 109 Core heater temperature, Rod E-2 (TH-E2-20 and TH-E2-33), from -20 to 300 sec.

Fig. 110 Core heater temperature, Rod E-2 (TH-E2-20 and TH-E2-33), from -6 to 42 sec.

Fig. 111 Core heater temperature, Rod E-3 (TH-E3-05, TH-E3-20, TH-E3-24), from -20 to 300 sec.

Fig. 112 Core heater temperature, Rod E-3 (TH-E3-05, TH-E3-20, TH-E3-24), from -6 to 42 sec.

Fig. 113 Core heater temperature, Rod E-6 (TH-E6-08, TH-E6-28, TH-E6-37), from -20 to 300 sec.

Fig. 114 Core heater temperature, Rod E-6 (TH-E6-08, TH-E6-28, TH-E6-37), from -6 to 42 sec.

Fig. 115 Core heater temperature, Rod E-7 (TH-E7-44), from -20 to 300 sec.

Fig. 116 Core heater temperature, Rod E-7 (TH-E7-44), from -6 to 42 sec.

Fig. 117 Core heater temperature, Rod E-8 (TH-E8-14, TH-E8-29, TH-E8-45), from -20 to 300 sec.

Fig. 118 Core heater temperature, Rod E-8 (TH-E8-14, TH-E8-29, TH-E8-45), from -6 to 42 sec.

Fig. 119 Core heater temperature, Rod F-2 (TH-F2-07, TH-F2-22, TH-F2-25), from -20 to 300 sec.

Fig. 120 Core heater temperature, Rod F-2 (TH-F2-07, TH-F2-22, TH-F2-25), from -6 to 42 sec.

Fig. 121 Core heater temperature, Rod F-4 (TH-F4-14 and TH-F4-29), from -20 to 300 sec.

Fig. 122 Core heater temperature, Rod F-4 (TH-F4-14 and TH-F4-29), from -6 to 42 sec.

Fig. 123 Core heater temperature, Rod F-5 (TH-F5-20, TH-F5-26, TH-F5-33, TH-F5-53), from -20 to 300 sec.

Fig. 124 Core heater temperature, Rod F-5 (TH-F5-20, TH-F5-26, TH-F5-33, TH-F5-53), from -6 to 42 sec.

Fig. 125 Core heater temperature, Rod G-3 (TH-G3-13), from -20 to 300 sec.

Fig. 126 Core heater temperature, Rod G-3 (TH-G3-13), from -6 to 42 sec.

Fig. 127 Core heater temperature, Rod G-4 (TH-G4-29, TH-G4-33, TH-G4-38), from -20 to 300 sec.

Fig. 128 Core heater temperature, Rod G-4 (TH-G4-29, TH-G4-33, TH-G4-38), from -6 to 42 sec.

Fig. 129 Core heater temperature, Rod G-5 (TH-G5-14 and TH-G5-24), from -20 to 300 sec.

Fig. 130 Core heater temperature, Rod G-5 (TH-G5-14 and TH-G5-24), from -6 to 42 sec.

Fig. 131 Core heater temperature, Rod H-5 (TH-H5-32), from -20 to 300 sec.

Fig. 132 Core heater temperature, Rod H-5 (TH-H5-32), from -6 to 42 sec.

Fig. 133 Pressure in intact loop, Spool 13 (PU-13), from -20 to 300 sec.

Fig. 134 Pressure in intact loop, Spool 13 (PU-13), from -6 to 42 sec.

Fig. 135 Pressure in intact loop, Spool 15, low range (PU-15L), from -20 to 300 sec.

Fig. 136 Pressure in intact loop, Spool 15, low range (PU-15L), from -6 to 42 sec.

Fig. 137 Pressure in broken loop, Spool 23 (PB-23), from -20 to 300 sec.

Fig. 138 Pressure in broken loop, Spool 23 (PB-23), from -6 to 42 sec.

Fig. 139 Pressure in broken loop, near break (PB-37 and PB-42), from -20 to 300 sec.

Fig. 140 Pressure in broken loop, near break (PB-37 and PB-42), from -6 to 42 sec.

Fig. 141 Pressure in broken loop, pump-side nozzle (PB-HN1), from -20 to 300 sec.

Fig. 142 Pressure in broken loop, pump-side nozzle (PB-HN1), from -6 to 42 sec.

Fig. 143 Pressure in broken loop, vessel-side nozzle (PB-CN1), from -20 to 300 sec.

Fig. 144 Pressure in broken loop, vessel-side nozzle (PB-CN1), from -6 to 42 sec.

Fig. 145 Pressure in vessel (PV-UP+10 and PV-LP-166), from -20 to 300 sec.

Fig. 146 Pressure in vessel (PV-UP+10 and PV-LP-166), from -6 to 42 sec.

Fig. 147 Pressure in intact loop accumulator (PU-ACC), from -20 to 300 sec.

Fig. 148 Pressure in intact loop accumulator (PU-ACC), from -6 to 42 sec.

Fig. 149 Pressure in broken loop accumulator (PB-ACC), from -20 to 300 sec:

Fig. 150 Pressure in broken loop accumulator (PB-ACC), from -6 to 42 sec.

Fig. 151 Pressure in vessel accumulator (PV-ACC), from -20 to 300 sec.

Fig. 152 Pressure in vessel accumulator (PV-ACC), from -6 to 42 sec.

Fig. 153: Pressure in steam generator, secondary side (PU-SGSD), from -20 to 300 sec.

Fig. 154: Pressure in steam generator, secondary side (PU-SGSD), from -6 to 42 sec.

Fig. 155 Pressure in pressurizer (PU-PRIZE), from -20 to 300 sec.

Fig. 156 Pressure in pressurizer (PU-PRIZE), from -6 to 42 sec.

Fig. 157 Pressure in pressure suppression tank (P-PSS), from -20 to 300 sec.

Fig. 158 Pressure in pressure suppression tank (P-PSS), from -6 to 42 sec.

Fig. 159 Differential pressure in intact loop (DPU-UP-3), from -20 to 300 sec.

Fig. 160 Differential pressure in intact loop (DPU-UP-3), from -6 to 42 sec.

Fig. 161 Differential pressure in intact loop (DPU-3-7), from -20 to 300 sec.

Fig. 162 Differential pressure in intact loop (DPU-3-7), from -6 to 42 sec.

Fig. 163 Differential pressure in intact loop (DPU-7-10), from -20 to 300 sec.

Fig. 164 Differential pressure in intact loop (DPU-7-10), from -6 to 42 sec.

Fig. 165 Differential pressure in intact loop (DPU-12-10), from -20 to 300 sec.

Fig. 166 Differential pressure in intact loop (DPU-12-10), from -6 to 42 sec.

Fig. 167 Differential pressure in intact loop, low range (DPU-12-10L), from -20 to 300 sec.

Fig. 168 Differential pressure in intact loop, low range (DPU-12-10L), from -6 to 42 sec.

Fig. 169 Differential pressure in intact loop (DPU-12-15), from -20 to 300 sec.

Fig. 170 Differential pressure in intact loop (DPU-12-15), from -6 to 42 sec.

Fig. 171 Differential pressure in intact loop (DPU-15-1), from -20 to 300 sec.

Fig. 172 Differential pressure in intact loop (DPU-15-1), from -6 to 42 sec.

Fig. 173 Differential pressure in intact loop, low range (DPU-15-1L), from -20 to 300 sec.

Fig. 174 Differential pressure in intact loop, low range (DPU-15-1L), from -6 to 42 sec.

Fig. 175 Differential pressure in intact loop (DPU-15-IANN), from -20 to 300 sec.

Fig. 176 Differential pressure in intact loop (DPU-15-IANN), from -6 to 42 sec.

Fig. 177 Differential pressure in intact loop (DPU-PRESLL), from -20 to 300 sec.

Fig. 178 Differential pressure in intact loop (DPU-PRESLL), from -6 to 42 sec.

Fig. 179 Differential pressure in intact loop (DPU-PR-4), from -20 to 300 sec.

Fig. 180 Differential pressure in intact loop (DPU-PR-4), from -6 to 42 sec.

Fig. 181 Differential pressure in broken loop (DPB-UP-30), from -20 to 300 sec.

Fig. 182 Differential pressure in broken loop (DPB-UP-30), from -6 to 42 sec.

Fig. 183 Differential pressure in broken loop (DPB-21-IANN), from -20 to 300 sec.

Fig. 184 Differential pressure in broken loop (DPB-21-IANN), from -6 to 42 sec.

Fig. 185 Differential pressure in broken loop (DPB-30-36L), from -20 to 300 sec.

Fig. 186 Differential pressure in broken loop (DPB-30-36L), from -6 to 42 sec.

Fig. 187 Differential pressure in broken loop (DPB-32U-36L), from -20 to 300 sec.

Fig. 188 Differential pressure in broken loop (DPB-32U-36L), from -6 to 42 sec.

Fig. 189 Differential pressure in broken loop (DPB-36L-37), from -20 to 300 sec.

Fig. 190 Differential pressure in broken loop (DPB-36L-37), from -6 to 42 sec.

Fig. 191 Differential pressure in broken loop (DPB-37-38), from -20 to 300 sec.

Fig. 192 Differential pressure in broken loop (DPB-37-38), from -6 to 42 sec.

Fig. 193 Differential pressure in broken loop (DPB-38-40), from -20 to 300 sec.

Fig. 194 Differential pressure in broken loop (DPB-38-40), from -6 to 42 sec.

Fig. 195 Differential pressure in broken loop (DPB-40-42), from -20 to 300 sec.

Fig. 196 Differential pressure in broken loop (DPB-40-42), from -6 to 42 sec.

Fig. 197 Differential pressure in vessel (DPV-UP-IANN), from -20 to 300 sec.

Fig. 198 Differential pressure in vessel (DPV-UP-IANN), from -6 to 42 sec.

Fig. 199 Differential pressure in vessel (DPV-0-9GQ), from -20 to 300 sec.

Fig. 200 Differential pressure in vessel (DPV-0-9GQ), from -6 to 42 sec.

Fig. 201 Differential pressure in vessel (DPV-9-2600), from -20 to 300 sec.

Fig. 202 Differential pressure in vessel (DPV-9-2600), from -6 to 42 sec.

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Fig. 204 Differential pressure in vessel (DPV-9-166QQ), from -6 to 42 sec.

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Fig. 206 Differential pressure in vessel (DPV-26-55QM), from -6 to 42 sec.

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Fig. 208 Differential pressure in vessel (DPV-55-110MM), from -6 to 42 sec.

Fig. 209 Differential pressure in vessel (DPV-110-156M), from -20 to 300 sec.

Fig. 210 Differential pressure in vessel (DPV-110-156M), from -6 to 42 sec.

Fig. 211 Differential pressure in vessel (DPV-166-173QQ), from -20 to 300 sec.

Fig. 212 Differential pressure in vessel (DPV-166-173QQ), from -6 to 42 sec.

Fig. 213 Differential pressure in vessel (DPV-166Q-UP), from -20 to 300 sec.

Fig. 214 Differential pressure in vessel (DPV-166Q-UP), from -6 to 42 sec.

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Fig. 216 Differential pressure in vessel core (DPVC-89W-UP), from -6 to 42 sec.

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Fig. 218 Differential pressure in vessel core (DPVC-89-106WQ), from -6 to 42 sec.

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Fig. 221 Differential pressure in vessel accumulator (DPV-ACC-TB), from -20 to 300 sec.

Fig. 222 Differential pressure in vessel accumulator (DPV-ACC-TB), from -6 to 42 sec.

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Fig. 224 Differential pressure in steam generator secondary (DPU-SG-SEC), from -6 to 42 sec.

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Fig. 226 Differential pressure across steam generator outlet orifice (DPU-SG-DISC), from -6 to 42 sec.

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Fig. 228 Volumetric flow in intact loop (FTU-1 and FTU-9), from -6 to 42 sec.

Fig. 229 Volumetric flow in intact loop (FTU-13), from -20 to 300 sec.

Fig. 230 Volumetric flow in intact loop (FTU-13), from -6 to 42 sec.

Fig. 231 Volumetric flow in intact loop (FTU-15), from -20 to 300 sec.

Fig. 232 Volumetric flow in intact loop (FTU-15), from -6 to 42 sec.

Fig. 233 Volumetric flow in broken loop (FTB-21), from -20 to 300 sec.

Fig. 234 Volumetric flow in broken loop (FTB-21), from -6 to 42 sec.

Fig. 235 Volumetric flow in broken loop (FTB-30 and FTB-37), from -20 to 300 sec.

Fig. 236 Volumetric flow in broken loop (FTB-30 and FTB-37), from -6 to 42 sec.

Fig. 237 Volumetric flow in core entrance (FTV-CORE-IN), from -20 to 300 sec.

Fig. 238 Volumetric flow in core entrance (FTV-CORE-IN), from -6 to 42 sec.

Fig. 239 Volumetric flow in intact loop high pressure injection line (FTU-HPIS), from -20 to 300 sec.

Fig. 240 Volumetric flow in intact loop high pressure injection line (FTU-HPIS), from -6 to 42 sec.

Fig. 241 Volumetric flow in broken loop high pressure injection line (FTB-HPIS), from -20 to 300 sec.

Fig. 242 Volumetric flow in broken loop high pressure injection line (FTB-HPIS), from -6 to 42 sec.

Fig. 243 Volumetric flow in intact loop low pressure injection line (FTU-LPIS), from -20 to 300 sec.

Fig. 244 Volumetric flow in intact loop low pressure injection line (FTU-LPIS), from -6 to 42 sec.

Fig. 245 Volumetric flow in broken loop low pressure injection line (FTB-LPIS), from -20 to 300 sec.

Fig. 246 Volumetric flow in broken loop low pressure injection line (FTB-LPIS), from -6 to 42 sec.

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Fig. 250 Volumetric flow in broken loop accumulator discharge line (FTB-ACC), from -6 to 42 sec.

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Fig. 252 Volumetric flow in vessel accumulator discharge line (FTV-ACC), from -6 to 42 sec.

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Fig. 256 Fluid velocity in vessel (FTV-40A), from -6 to 42 sec.

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Fig. 261 Momentum flux in intact loop (FDU-10), from -6 to 42 sec.

Fig. 262 Momentum flux in intact loop (FDU-13), from -6 to 42 sec.

Fig. 263 Momentum flux in intact loop (FDU-15), from -6 to 42 sec.

Fig. 264 Momentum flux in broken loop (FDB-21), from -6 to 42 sec.

Fig. 265 Momentum flux in broken loop (FDB-23), from -6 to 42 sec.

Fig. 266 Momentum flux in broken loop (FDB-30), from -6 to 42 sec.

Fig. 267 Momentum flux in broken loop (FDB-37), from -6 to 42 sec.

Fig. 268 Momentum flux in broken loop (FDB-42), from -6 to 42 sec.

Fig. 269 Momentum flux in core entrance (FDV-CORE-IN), from -20 to 300 sec.

Fig. 270 Momentum flux in core entrance (FDV-CORE-IN), from -6 to 42 sec.

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Fig. 272 Density in intact loop (GU-1VR and GU-1HZ), from -6 to 42 sec.

Fig. 273 Density in intact loop (GU-5VR and GU-10VR), from -20 to 300 sec.

Fig. 274 Density in intact loop (GU-5VR and GU-10VR), from -6 to 42 sec.

Fig. 275 Density in intact loop (GU-13VR), from -20 to 300 sec.

Fig. 276 Density in intact loop (GU-13VR), from -6 to 42 sec.

Fig. 277 Density in intact loop (GU-15VR and GU-15HZ), from -20 to 300 sec.

Fig. 278 Density in intact loop (GU-15VR and GU-15HZ), from -6 to 42 sec.

Fig. 279 Density in broken loop (GB-21VR and GB-23VR), from -20 to 300 sec.

Fig. 280 Density in broken loop (GB-21VR and GB-23VR), from -6 to 42 sec.

Fig. 281 Density in broken loop (GB-30VR and GB-42VR), from -20 to 300 sec.

Fig. 282 Density in broken loop (GB-30VR and GB-42VR), from -6 to 42 sec.

Fig. 283 Density in vessel (GV-COR-150HZ), from -20 to 300 sec.

Fig. 284 Density in vessel (GV-COR-150HZ), from -6 to 42 sec.

Fig. 285 Density in vessel (GVLP-165HZ and GVLP-172HZ), from -20 to 300 sec.

Fig. 286 Density in vessel (GVLP-165HZ and GVLP-172HZ), from -6 to 42 sec.

Fig. 287 Density in pressurizer (GU-PRIZE), from -20 to 300 sec.

Fig. 288 Density in pressurizer (GU-PRIZE), from -6 to 42 sec.

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Fig. 291 Mass flow in intact loop (FTU-1 and GU-1VR), from -6 to 42 sec.

Fig. 292 Mass flow in intact loop (FDU-5 and GU-5VR), from -6 to 42 sec.

Fig. 293 Mass flow in intact loop (FTU-9 and GU-10VR), from -20 to 300 sec.

Fig. 294 Mass flow in intact loop (FTU-9 and GU-10VR), from -6 to 42 sec.

Fig. 295 Mass flow in intact loop (FDU-10 and GU-10VR), from -6 to 42 sec.

Fig. 296 Mass flow in intact loop (FDU-13 and GU-13VR), from -6 to 42 sec.

Fig. 297 Mass flow in intact loop (FTU-13 and GU-13VR), from -20 to 300 sec.

Fig. 298 Mass flow in intact loop (FTU-13 and GU-13VR), from -6 to 42 sec.

Fig. 299 Mass flow in intact loop (FDU-15 and GU-15VR), from -6 to 42 sec.

Fig. 300 Mass flow in intact loop (FTU-15 and GU-15VR), from -20 to 300 sec.

Fig. 301 Mass flow in intact loop (FTU-15 and GU-15VR), from -6 to 42 sec.

Fig. 302 Mass flow in broken loop (FDB-21 and GB-21VR), from -6 to 42 sec.

Fig. 303 Mass flow in broken loop (FTB-21 and GB-21VR), from -20 to 300 sec.

Fig. 304 Mass flow in broken loop (FTB-21 and GB-21VR), from -6 to 42 sec.

Fig. 305 Mass flow in broken loop (FDB-23 and GB-23VR), from -6 to 42 sec.

Fig. 306 Mass flow in broken loop (FDB-30 and GB-30VR), from -6 to 42 sec.

Fig. 307 Mass flow in broken loop (FTB-30 and GB-30VR), from -20 to 300 sec.

Fig. 308 Mass flow in broken loop (FTB-30 and GB-30VR), from -6 to 42 sec.

Fig. 309 Mass flow in broken loop (FDB-42 and GB-42VR), from -6 to 42 sec.

Fig. 310 Mass flow in vessel (FDV-CORE-IN and GV-COR-150HZ), from -20 to 300 sec.

Fig. 311 Mass flow in vessel (FDV-CORE-IN and GV-COR-150HZ), from -6 to 42 sec.

Fig. 312 Mass flow in vessel (FTV-CORE-IN and GV-COR-150HZ), from -20 to 300 sec.

Fig. 313 Mass flow in vessel (FTV-CORE-IN and GV-COR-150HZ), from -6 to 42 sec.

Fig. 314 Mass flow in pressurizer surge line (FTU-PRIZE and GU-PRIZE), from -6 to 42 sec.

Fig. 315 Core heater rod total power (PWRCOR T-1 and PWRCOR T-2), from -20 to 300 sec.

Fig. 316 Core heater rod total power (PWRCOR T-1 and PWRCOR T-2), from -6 to 42 sec.

Fig. 317 Core heater voltage (VOLT COR-T), from -20 to 300 sec.

Fig. 318 Core heater voltage (VOLT COR-T), from -6 to 42 sec.

Fig. 319 Core heater total current (AMPCOR-T), from -20 to 300 sec.

Fig. 320 Core heater total current (AMPCOR-T), from -6 to 42 sec.

Fig. 321 Primary pump current (PUMPU-CUR), from -20 to 300 sec.

Fig. 322 Primary pump current (PUMPU-CUR), from -6 to 42 sec.

Fig. 323 Primary pump speed (PUMPU-RPM), from -20 to 300 sec.

Fig. 324 Primary pump speed (PUMPU-RPM), from -6 to 42 sec.

IV. REFERENCE

1. E. M. Feldman and D. J. Olson, *Semiscale Mod-1 Program and System Description for the Blowdown Heat Transfer Tests (Test Series 2)*, ANCR-1230 (August 1975).

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APPENDIX A

POSTTEST ADJUSTMENTS TO DATA FROM SEMISCALE MOD-1 TEST S-05-3

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APPENDIX A

POSTTEST ADJUSTMENTS TO DATA FROM SEMISCALE MOD-1 TEST S-05-3

Many of the transducers used in the Semiscale Mod-1 system exhibit significant sensitivity to one or more spurious inputs. Strain gage bridge circuits used in pressure transducers, differential pressure transducers, and drag discs are sensitive to changes in ambient temperature. Differential pressure cells are also sensitive to changes in system pressure. Photomultiplier tubes used as gamma ray detectors in the density transducers are sensitive to temperature changes, as well as to random variations in the locations of the radiation sources. Core power measurements depend on a calibrated resistor, which changes in value as a function of time and power level as it heats up.

Although the errors introduced into the data by spurious secondary inputs generally do not exceed the specified error ranges of the transducers, significant improvement in measurement accuracy can be achieved if the secondary sensitivity can be identified and removed. In the case of the drag discs, corrections are absolutely necessary since the signal due to temperature fluctuations can exceed that due to flow by several hundred percent. Since the exact values of the spurious inputs to which different transducers might be sensitive cannot often be easily predicted and are sometimes inconvenient to measure, secondary effects have been accounted for by correcting the data after the test rather than by using elaborate real time programs in the data acquisition system computer. The methods and results of the posttest data correction analysis for Test S-05-3 are presented in the following paragraphs and tables.

1. PRESSURE MEASUREMENTS

Corrections to pressure transducer measurements in the main system loop are based on data taken from the standard reference (Heise) gauge at Spool 4, taken 15 sec before initiation of blowdown and at 300 sec after initiation of blowdown. The pressure readings are adjusted to account for pressure variations around the main loop, using the readings of nearby differential pressure cells. A linear correction is then applied to the pressure data to match the data to the calculated reference data at the two specified time points.

Correction of the steam generator secondary pressure (PU-SGSD) measurement is done in the same manner as for the main loop pressures using a Heise gauge installed expressly for this purpose. The data from the pressure transducer for the pressure suppression system (P-PSS) are corrected to match the process instrumentation at preblowdown conditions.

Pressure measurement corrections are performed using the data acquisition system (DAS) computer using the following equation:

$$F'(t) = C_0 + C_1 [F(t)]$$

where:

$F'(t)$ = corrected data

$F(t)$ = raw data

C_0 = offset

C_1 = scaling factor

The exact values of C_0 and C_1 are given in Table A-1.

TABLE A-1

CONSTANTS FOR PRESSURE MEASUREMENT
CORRECTIONS (TEST S-05-3)

<u>Detector Identification:</u>	<u>C_0</u>	<u>C_1</u>
PB-ACC	138	1
PV-ACC	-10	1
PU-13	57.7	1.0057
PU-SGSD	68	0.9861
PV-UP+10	20.3	0.9987
PU-PRIZE	22.6	1.0031
PB-CNI	23.5	0.9869
PB-23	24.4	0.9895
PB-42	22.3	0.9907
PB-HNI	33.3	0.9908
P-PSS	-2.5	1
PB-37	25.7	0.9898
PV-166	12.6	0.9955

2. DIFFERENTIAL PRESSURE MEASUREMENTS

Pressure sensitivity in the differential pressure cells in the main system loop is determined from the pretest system pressure check. Digital data are recorded for all measurements at ambient temperature, with no system flow, at pressures of ambient, 200, 500, 1000, 1500, 2000, and 2250 psig. The output of the differential pressure cells is plotted against system pressure, with the resulting plots used to describe the pressure response of the transducers.

The response of the differential pressure cells due to ambient temperature is determined from a digital data scan taken at 500°F and 1750 psig, with no system flow. The measured transducer outputs are corrected for pressure and compared with the values calculated due only to the density difference between the water inside the loop (500°F) and outside the loop in the sense lines (80 to 100°F).

The difference between the measured pressure corrected value and the calculated value is the thermal drift. After the data scan at 500°F is made, no more opportunities exist to obtain data with the pump stopped and the system full of liquid; therefore, for lack of later data, the thermal drift calculated from the 500°F data is assumed to be constant throughout the test.

For some differential pressure measurements, the data scan at 500°F cannot be used as a reference for thermal drift; so other references are used. The liquid level measurements in the vessel accumulator (DPV-ACC-TB) and pressurizer (DPU-PRESLL) are referenced to calculated values based on geometrical considerations at the time when gas flow from the respective vessel is first noted. The reading from the steam generator discharge venturi (DPU-SGDISC) is shifted to read zero after flow is stopped. The steam generator secondary liquid level measurement (DPU-SG-SEC) is shifted to match the output of the process instrumentation prior to blowdown.

In correcting differential pressure data for pressure sensitivity, the corrections are calculated for various times during the test by referring to nearby system pressure transducers. The thermal drift correction is then added to each pressure sensitivity correction and the combined value is added to the raw data using a computer program that linearly interpolates the corrections between the specified time points. The corrections are performed according to the following equations:

$$F'(t) = KF(t) + C_1 \text{ for } t < t_1 \text{ or when no } t_i \text{ are listed.}$$

For time points t , where $t_1 \leq t \leq t_n$

$$F'(t) = KF(t) + C_i + \frac{t-t_i}{t_{i+1}-t_i} (C_{i+1} - C_i) \text{ for } t_i \leq t \leq t_{i+1}$$

where i takes on value 1 to $n-1$

$$F'(t) = KF(t) + C_n \text{ for } t > t_n$$

where

t = time

$F'(t)$ = corrected data

$F(t)$ = raw data

K = scaling factor

C_i and t_i = corrections and time points

The exact values of the constants are given in Table A-II.

TABLE A-II

CONSTANTS FOR DIFFERENTIAL PRESSURE
MEASUREMENT CORRECTIONS (TEST S-05-3)

Detector Identification	K	c_1	t_1	c_2	t_2	c_3	t_3
DPV-ACC-TB	1	0.45					
DPU-30-36L	1	2.39	0	1.19	0.01	-2.01	30
DPU-SG-SEC	-1 ^[a]						
DPB-32U-36L	1	3.13	0	1.33	0.01	-1.67	30
DPB-36L-37	1	-0.724	0	-0.674	0.01	-0.559	30
DPU-15-1	1	0.461	0	0.386	0.01	0.251	30
DPU-15-1L	1	-0.112	0	-0.090	0.01	-0.043	30
DPB-UP-30	2 ^[b]	0.86	0	0	0.01		
DPU-SG-SEC	1.0	-0.6 ^[c]					
DPB-38-40	-1 ^[d]	-6.29	0	-4.79	0.01	-2.34	30
DPB-40-42	1	-0.071	0	-0.058	0.01	-0.032	30
DPV-26-55QM	1	-0.081	0	-0.011	0.01	0.139	30
DPU-7-10	1	0.043	0	0.053	0.01	0.075	30
DPVC-89W-UP	1	0.84	0	0.73	0.01	0.50	30
DPVC-9-166QQ	1	0.29	0	0.18	0.01	-0.14	30
DPVC-89-106WQ	1	0.091	0	0.098	0.01	-0.022	30
DPV-UP-IANN	1	-4.8	0	0.101	0.01	-0.066	30
DPV-166-UP	1	-0.418	0	-0.446	0.01		

[a] Transducer output was inverted to show liquid level.

[b] Electronic gain off by a factor of two.

[c] Data corrected to agree with more stable process instrumentation.

[d] Patch panel connections were reversed.

3. MOMENTUM FLUX MEASUREMENTS

The temperature sensitivity of drag discs is determined from pretest warmup data taken at 200 and 500°F with no system flow. The temperature sensitivity is removed before the data are converted to momentum flux. The temperature of each transducer is taken from the signal of a nearby fluid or metal temperature thermocouple. Slight corrections for errors in setting the transducer output to zero at ambient conditions are also made at this time. Corrections are made using the following equation:

$$F'(t) = F(t) + D_0 - D_1 T(t)$$

where

$F'(t)$ = corrected data

$F(t)$ = raw data

$T(t)$ = temperature data from the transducer used for temperature correction sensitivity

D_0 = ambient offset

D_1 = temperature sensitivity.

Values of the constants are given in Table A-III.

TABLE A-III
CONSTANTS FOR MOMENTUM FLUX
MEASUREMENT CORRECTIONS (TEST S-05-3)

<u>Detector Identification</u>	<u>D₀</u>	<u>D₁</u>	<u>T(t)^[a]</u>
FDU-5	0	-0.000156	TMU-1T16
FDU-10	0	0.000219	TMU-1T16
FDU-13	0	0.000380	TMU-15B16
FDB-30	-0.094	-0.000762	TFB-30
FDB-21	-0.123	-0.000683	TMB-20B16
FDB-23	-0.094	0.000677	TMB-20B16
FDB-37	0	0.000417	TMB-37
FDB-42	-0.061	0.000747	TFB-42
FDU-1	0	-0.000701	TMU-1T16
FDU-15	0	-0.001207	TMU-15T16

[a] T(t) is the temperature data used for temperature sensitivity correction. The symbols listed identify the thermocouples from which the data were obtained.

4. DENSITY MEASUREMENTS

Density calculations are based on the voltage output of the photomultiplier tubes in the gamma-attenuation densitometer assemblies. The equation used for converting voltage to density is as follows:

$$\rho = (1/C) \ln \{D / [A F(t) + B]\}$$

where

ρ = the density in lbm/ft³

C = a constant based on the length of the gamma beam path

D = a theoretical voltage for zero attenuation inside the vessel

A = an amplification factor

B = a biasing factor

F(t) = the transducer voltage output.

Constants A and B are adjusted to match the final data to density values calculated from measured pressure and temperature values at the preblowdown and postdrain conditions, effectively giving the data an in-place calibration. The values of the constants for various transducers are given in Table A-IV.

TABLE A-IV
CONSTANTS FOR DENSITY MEASUREMENT
CONVERSIONS TO ENGINEERING UNITS (TEST S-05-3)

<u>Detector Identification</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>
GV-COR-150HZ	1.003	0.012	0.014	3.49
GB-30VR	1.096	-0.588	0.0095	6.49
GB-42VR	1.043	-0.224	-0.006	5.55
GU-1VR	1.077	-0.239	0.0095	3.34
GU-1HZ	1.336	-1.658	0.0095	5.03
GU-5VR	1.107	-0.616	0.0095	6.00
GU-10VR	1.071	-0.452	0.0095	7.02
GU-13VR	1.279	-0.738	0.0095	2.72
GU-15VR	1.086	-0.578	0.0095	7.23
GU-15HZ	1.111	-0.182	0.0095	1.71
GU-21VR	1.016	-0.054	0.0095	4.72
GU-23VR	0.980	0.173	0.0095	6.95
GU-PRIZE	1.136	-0.172	0.0095	1.34
GV-LP-165HZ	0.743	2.045	0.014	7.72

The density measurement GVLP-172HZ uses an amplifier which precalculates the logarithm function, and hence has a simpler conversion formula:

$$\rho = 1.604 F(t) - 43.6$$

5. CORE POWER MEASUREMENTS

Corrections to core power readings are determined from the core voltage and core current readings, with a slight adjustment for the power lost in setting the core radial peaking factor. The adjustments are as follows:

$$\text{PWRCOR T-1: } F'(t) = 0.9829 F(t) - 0.34 = [(\text{voltage}) (\text{current}) (0.974)]$$

$$\text{PWRCOR T-2: } F'(t) = 0.9917 F(t) + 4.87 = [(\text{voltage}) (\text{current}) (0.974)]$$

where

$F'(t)$ = core power in kilowatts

$F(t)$ = the raw core power reading.

6. VOLUMETRIC FLOW MEASUREMENTS

The turbine flowmeter in the vessel accumulator discharge line (FTV-ACC) was affected by 60 Hz interference, giving a false indication of 1.59 gpm under no-flow conditions. The false indication was removed using a time-dependent correction, as described in Section 2 and shown in Table A-V.

TABLE A-V
CONSTANTS FOR CORRECTION OF TURBINE FLOWMETER
FTV-ACC, TEST S-05-3

<u>K</u>	<u>i</u>	<u>C_i</u>	<u>t_i</u>
1	1	-1.59	3.29
	2	0	3.34
	3	0	6.68
	4	-1.59	6.83
	5	-1.59	22.17
	6	0	22.23
	7	0	164.0
	8	-1.59	164.35

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