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Reservoir Evaluation Tests On RRGE 1
And RRGE 2, Raft River Geothermal
Project, Idaho

T.N. Narasimhan and P.A. Witherspoon

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RESERVOIR EVALUATION TESTS ON RRGE 1 AND RRGE 2,
RAFT RIVER GEOTHERMAL PROJECT, IDAHO

by

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ABSTRACT

This report presents results of the production and interference tests conducted on the geothermal wells RRGE 1 and RRGE 2 in Raft River Valley, Idaho during September - November, 1975. In all, three tests were conducted, two of them being short-duration production tests and one, a long duration interference test. In addition to providing estimates on the permeability and storage parameters of the geothermal reservoir, the tests also indicated the possible existence of barrier boundaries. The data collected during the tests also indicated that the reservoir pressure varies systematically in response to the changes in the Earth's gravitational field caused by the passage of the sun and the moon. Overall, the results of the tests indicate that the geothermal reservoir in southern Raft River valley is fairly extensive and significantly permeable and merits further exploration.

INTRODUCTION

Between January and July, 1975, the Idaho National Engineering Laboratory (INEL) drilled two deep wells in the Known Geothermal Resource Area (KGRA) in southern Raft River Valley and successfully produced hot water at about 147°C (about 297°F) with free artesian flow of over 1500 liters (400 gallons) per minute. Upon completion of the wells, Dr. Jay Kunze, Director, Raft River Geothermal Project, requested the help of the Geothermal Group of Lawrence Berkeley Laboratory (LBL) to conduct appropriate reservoir tests on the two successful wells with a view to gaining as much knowledge as possible about the reservoir to guide further exploration and development. Accordingly, the LBL Geothermal Group carried out production as well as interference tests on the two geothermal wells during the last 3 weeks of September and the first week of November, 1975. The tests yielded useful data on the physical parameters of the geothermal reservoir in Raft River Valley as well as providing clues about the possible reservoir geometry. Based on these tests the drilling of a third well was commenced during April 1976.

The purpose of this progress report is to present the findings of the first reservoir evaluation tests.

GEOMORPHOLOGY, GEOLOGY AND STRUCTURE

The Raft River KGRA is located on a north trending intermontane valley which is bounded on the west (Fig. 1) by the Jim Sage and Cotterell mountains, on the south by the Raft River mountain range, and on the east by Black Pine and Sublett mountain ranges. The valley is about 38 miles long and about 12 to 15 miles wide and is drained

Fig. 1: Location map of the Raft River valley geothermal field, Idaho.

by the perennial Raft River, which flows into the Snake River to the north. The floor of the valley is at an average elevation of about 4600 feet while the surrounding hill ranges attain elevations of up to 9800 feet. The valley is relatively flat and slopes gently towards the north. At the southwestern extremity of the valley the Raft River flows through a gap (known as the "Narrows") between the north-south Jim Sage mountains and the east-west trending Raft River mountains. The latter reportedly forms one of the few east-west trending mountain ranges in the North American Cordillera (Williams et al., 1975).

The Raft River valley lies in a graben formed by down faulting in late Tertiary times (Williams et al., 1975). The basin lies in the northern part of the Basin and Range province near its structural junction with Snake River volcanic plains. The basin is filled with Tertiary and Pleistocene sediments to depths of about 5900 feet. The Jim Sage and Cotterell mountains on the west are made up of Tertiary volcanic rocks and sediments while the Black Pine and Sublett Ranges on the east are mainly made up of Paleozoic sediments. To the south, the Raft River mountains ex-

pose Precambrian adamellite (quartz monzonite), capped by Paleozoic metasediments (Williams et al., 1975). The two geothermal wells, RRGE 1 and RRGE 2, terminate in the adamellites indicating that the Precambrian rocks of the Raft River mountains form the floor of the Raft River basin.

A bulk of the sediments filling the basin belong to the Salt Lake formation of Mio-Pliocene age, attaining thicknesses of up to 5900 ft (Williams et al., 1975). The Salt Lake formation comprises tufaceous sandstone, siltstone and conglomerate. At the bottom, the Salt Lake formation is separated from the Adamellite basement by Paleozoic metamorphic rocks comprising quartzites and schists.

The Salt Lake formation is overlain by Pleistocene sand, gravel, silt and clay (the Raft River formation) which does not outcrop in the valley. The Raft River formation is in turn overlain by alluvial and pluvial sediments.

Structurally (Fig. 2), the Raft River basin is considerably faulted; by north-south faults at the base of the Jim Sage-Cotterell hills on the west and at the base of the Black Pine-Sublett ranges on the east and by east-west faults at the foot of the

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Fig. 2: Structural geology in and around the Raft River valley geothermal field (after Williams et al., 1975).

CORRELATION OF MAP UNITS

LIST OF MAP UNITS

SURFICIAL

Qa	Alluvium	
Qf	Fan gravels	
Qfy	Young	
Qfm	Middle	
Qfo	Old	
Qs	Silt	
Td	VOLCANIC DOME	
Twt	WELDED TUFF	
Ts	SALT LAKE FORMATION	
Tsu	Upper member	
Tsj	Volcanic member at Jim Sage Mountain	
Tsju	Upper Flow unit	Upper flow unit
Tsjb	Vitrophyre breccia unit	
Tsjl	Lower flow unit	
Tsl	Lower member	
Pz	PALEOZOIC ROCKS	

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Fig. 3: Geologic cross section across part of the Raft River valley (after Williams et al., 1975).

Raft River mountains on the south. All the fault planes apparently dip towards the basin, rendering the basin a complex graben. The "Narrows" structure, which has been picked up by geophysical measurements (Williams et al., 1975), is an incompletely understood structural lineament trending ENE at the SW corner of the basin and NE (Fig. 2) at the NE corner of the basin.

The most important structural element in the vicinity of RRGE 1 and RRGE 2 is the Bridge Fault, which seemingly outcrops 2250 feet west of RRGE 1 and trends north-south and dips east at approximately 60 degrees near the surface. The Bridge Fault was apparently intercepted at RRGE 1 at about 4200 feet. In Fig. 3 is reproduced a geological section prepared by Williams et al. (1975) along a WNW-ESE line passing just south of RRGE 1.

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Fig. 4: Profile showing completion details of geothermal well RRGE 1 (prepared by Aerojet Nuclear Company).

SUBSURFACE CORRELATION

The geothermal wells RRGE 1 and RRGE 2 are located in Section 23, Township 15S, Range 26E. The distance between the wells is approximately 4000 feet with RRGE 2 located towards NE from RRGE 1. The completion data for the two wells are summarized in Table 1, and the well profiles are sketched in Figs. 4 and 5.

Tentative correlation of the borehole logs of the two wells (Fig. 6) by the geologists of Aerojet Nuclear Company indicate that the sediments apparently dip towards RRGE 2. In particular, the correlation shows that the base of the Raft River formation is offset downward by about 200 feet toward RRGE 2, suggesting an apparent dip of about

Fig. 5: Profile showing completion details of geothermal well RRGE 2 (prepared by Aerojet Nuclear Company).

three degrees toward NE. With depth, the dips increase gradually and at about 4500 feet in RRGE 2, the deposits are about 500 feet deeper than the comparable sediments in RRGE 1, indicating an apparent dip of about seven degrees. The upper part of the Elba quartzite of Precambrian age, which underlies the Salt Lake formation in RRGE 1 and in

RRGE 2, is apparently almost horizontal between the two wells. While a prominent fault zone (Bridge fault?) was pierced in RRGE 1 between 3800 and 4500 feet, the borehole data from RRGE 2 failed to indicate the presence of any such pronounced fault zone.

Fig. 6:
Stratigraphic correlation of
geothermal wells RRGE 1 and
RRGE 2 (prepared by Aerojet
Nuclear Company).

TABLE 1

	RRGE 1	RRGE 2
Total depth, ft	4,989	5,988
Casing:		
Diameter, in	13-3/8	13-3/8
Depth, ft	3,624	4,227
Uncased hole:		
Diameter, in	20	12-1/4
Depth range, ft	3,624-4,989	4,227-5,988
Major production, depth range	3,624-4,200(?)	4,227-5,000(?)
Reservoir temperature, °F (°C)	≈ 294 (146)	≈ 294 (146)
Well head pressure, psi	≈ 150	≈ 150

RESERVOIR TESTS AND INSTRUMENTATION

The basic aims of the reservoir tests were to evaluate the permeability and storage parameters of the reservoir and to decipher reservoir geometry. The tests essentially consisted in producing fluid from one of the wells at controlled rates and over prolonged periods of time and observing the water pressure changes in the producing well itself or in the other well. Since the wells have positive well head pressures (artesian), controlled flow can be achieved by carefully opening the well head valve. Also, since the theory of the tests is based on a single, homogeneous fluid, the flow had to be so controlled that there can be no flashing or formation of a vapor phase within the well.

Since the wells are over 4000 feet apart, the pulse introduced at one well can create only very small pressure changes in the observation well. A key piece of equipment in the tests was therefore a very sensitive quartz crystal pressure gage which can be conveniently lowered into the well to any desired depth and which communicates with surface recording equipment through a conductor cable. The pressure gage has a resolution of 0.01 psi (over the range 0 - 10,000 psi) and can withstand temperatures of up to 300°F. Since the maximum reservoir temperatures recorded at RRGE 1 and RRGE 2 were only about 294°F, the aforesaid pressure gage was very well suited for monitoring pressure changes in an active producing well or in a quiet well.

During the tests, use was also made of a similar, but less expensive quartz pressure gage, which could measure pressure changes only at the well head. Since both RRGE 1 and RRGE 2 have positive well head pressures, this "surface pressure gage" was especially well suited for monitoring pressure changes in the observation well during the interference test.

In regard to instrumentation, one of the objectives of the tests was to evaluate the performance of the less expensive surface pressure gage in comparison to the more expensive downhole gage. Towards this end, both the instruments were installed in the same well (RRGE 1) during a long duration interference test and simultaneous pressure measurements were made, with the downhole gage set at approximately 1000 feet. The data so collected are presented in Plate 2. A comparison of the data from the instruments for the period from September 30 to October 6, 1975 shows that the pressure changes sensed by the two instruments agree reasonably well in general, except for the fact that the surface gage data tend to show somewhat enhanced peaks during the early afternoon periods (between 1200 and 1800 hours). It is worthwhile pointing out here that in setting up the surface gage, an air column was used as a buffer to protect the pressure sensing crystal from the water in the well. It seems reasonable to infer that the accentuated pressure readings indicated by the surface gage during the early afternoons are to be attributed to the expansion of the air column buffer due to the increased temperatures.

The experience gained in regard to the surface pressure gage has showed that the surface pressure gage is indeed a valuable, economical alternative to the considerably more expensive downhole gage whenever one is interested only in measuring transient well head pressure changes in observation wells. It is felt that the anomalous readings induced by the air column buffer due to its susceptibility to temperature changes can be minimized or even eliminated by replacing the air column by a buffer of an inert oil, such as silicone oil.

DESCRIPTION OF RESERVOIR TESTS

In all, three tests were conducted between September 12 and November 7, 1975. Two of these were production well tests in which the pressure gage was positioned in the production well within the producing interval. This was necessary in order to assure a fairly stable temperature environment for the pressure gage, which is temperature sensitive. The production well tests were both of short duration and lasted less than 30 hours. After shutting down production, pressure buildup within the well was monitored for less than 24 hours.

The third test was an interference test in which fluid was produced from RRGE 2 and the pressure changes were monitored in RRGE 1. Since the latter was quiet and fluid filled, it was not essential to position the instrument close to the bottom of the well. The interference test, which provides data on a large portion of the reservoir between the two wells, was of a long duration. During this test, RRGE 2 was flowed for approximately 26 days.

The specifications of the tests conducted are given in Table 2.

TABLE 2

Test No.	Description	Duration Hours	Production Well No. Flow Rate gpm	Pressure Gage in Well No. Depth, ft	Maximum Pressure Drop Well No. Δp , psi
1	Short term test on RRGE #2	15	RRGE #2 225	RRGE #2 5200	RRGE #2 39
2	Long term test on RRGE #2	615 $\frac{1}{2}$	RRGE #2 400	RRGE #1 1000	RRGE #1 3.6
3	Short term test on RRGE #1	30	RRGE #1 26	RRGE #1 4700	RRGE #1 1.1

INFLUENCE OF EARTH TIDES ON OBSERVED WATER PRESSURES

A significant phenomenon that came to light from the water pressure data collected during the long duration interference tests (Plate 2) and the short duration production test on RRGE 1 (Plate 3) was that the water pressure in the reservoir responds systematically to the changes in the earth's gravitational field induced by the paths of the moon and the sun. The field data indicated regular fluctuations in water pressures with wave lengths varying from 10 to 12 hours and with amplitudes of up to 0.1 psi about the mean.

For a proper evaluation of the pressure data, the gravitational changes at the location of RRGE 1 over the period of the tests was calculated by Dr. Howard Oliver of the U. S. Geological Survey, Menlo Park, California. Figure 7 shows a comparison between the calculated gravity variation and water pressure variation in RRGE 1 between September 28 and October 6, 1975. It can be seen from the figure that there is good correlation between gravity change and pressure change. A cross spectral analysis of the data showed that the troughs and crests of the water pressure wave tend to lead the corresponding features of the gravity wave by about 37 minutes. Due consideration had to be given to the tidal influence before the interference data could be analyzed.

THEORY OF PUMPING TESTS

Before we present and discuss the results, it is pertinent to briefly describe the theoretical basis of interpretation. The analytical model used for interpretation is that of transient potential distribution around a continuous line source (axisymmetric system) in an infinite, homogeneous, horizontal slab of finite thickness. By the principle of superposition and using image concepts, the model can be extended to non-infinite or bounded systems. Details of this interpretive technique can be found in Witherspoon et al., 1967, or Ferris et al., 1962. The aim of interpretation is to determine the reservoir kH , the reservoir storativity, ϕcH (where K is the permeability coefficient, H is reservoir thickness, ϕ is porosity and c reservoir compressibility) and decipher the existence of barriers or other boundaries. The

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Fig. 7: Correlation between variation in the earth's gravitational field and water pressure in RRGE 1 during the long-term interference test.

transient pressure change around a line source in an initially static system is given by the relation (often known as the Theis equation)

$$\Delta P = \frac{q\mu P_D}{(v)kH} \quad (1)$$

where ΔP is pressure change, q is constant flow rate, μ is fluid viscosity (assumed to 0.18 cp at 294°F and 2000 psi), P_D is dimensionless pressure and v is a constant depending on units used. Moreover, P_D is expressed as an integral of the dimensionless time t_D

$$P_D = 1/2 \int_u^\infty \frac{e^{-u}}{u} du \quad (2)$$

where $u = 1/4 t_D$. The dimensionless time t_D is given by

$$t_D = \frac{kt}{\phi\mu cr^2} \quad (3)$$

in which t is time and r is the radius to the point of observation. In order to evaluate kH and ϕcH using (1), (2) and (3) a technique of curve matching is conventionally used, by plotting the pressure drawdown data on a log-log graph paper. Or, for $t_D \gg 1$, an asymptotic approximation may be used in which drawdown is plotted as a function of the log of time. In addition to kH and ϕcH , the departure of the plotted data from the type curve in the log-log plot or the occurrence of breaks in the slopes of the straightline segments of the semi-log plot would indicate the presence of barrier or leaky boundaries in the system.

RESULTS OF TESTS AND INTERPRETATION

(1) Short term production test, RRGE 2: The short term production test on RRGE 2 was conducted between September 12 and 13, 1975. The data collected during this test is presented in Appendix 1 and the time history of pressure change is shown in Plate 1. During this test, the well was flowed at a near-constant rate of 225 gpm for 15 hours. After shutting down the flow, pressure buildup was observed for an additional 2.25 hours. The maximum pressure drawdown observed during the production period was approximately 37.5 psi. The total pressure recovery during the 2.25 hours of buildup observation was about 24.25 psi. During this test, the quartz pressure gage was installed at a depth of 5200 feet where the absolute static pressure was about 2261 psi.

A log-log plot of the pressure drawdown data collected from this short term test is presented in Fig. 8. It can be seen from the figure that between 15 and 600 seconds of the start of production, the drawdown data closely matches the Theis' type-curve. Computations based on this early drawdown data indicate the following parameters for the reservoir in the vicinity of RRGE 2: $kH = 47,600$ millidarcy-feet; $\phi cH = 2.91 \times 10^{-2}$ ft/psi, assuming an effective well radius of one foot. Since the exact production thickness of the reservoir is not known, the fundamental parameters, permeability and compressibility have not been computed.

Fig. 8: Short-term production test, RRGE 2: Log-log plot of drawdown versus time.

The data presented in Fig. 8 also show that after about 600 seconds, the drawdown data gradually departs from the Theis type-curve, showing larger drawdowns than those suggested by the type-curve. This kind of departure could normally be indicative of the presence of one or more barrier boundaries in the vicinity of RRGE 2. Figure 8 suggests that if indeed a barrier boundary exists near RRGE 2, it is equivalent to an "image" well located at a distance of between twenty and fifty times the effective radius of the well. However, it is possible that (H.J. Ramey, personal communication) the observed departure from the type-curve could have been caused by other factors such as gradual changes in production rates or commingling of different producing horizons.

A semi-log plot of the drawdown data is presented in Fig. 9. It is seen from this figure that the data within the first 800 seconds of production fall on a fairly well-defined straightline indicating a kH value of about 47,300 millidarcy-feet and a ϕcH value of 3.0×10^{-2} ft/psi assuming an effective well radius of one foot. It is interesting to note from this figure the drawdown data plot on three distinct line segments; the second and the third line segments may indicate the probable presence of more than one barrier boundary near RRGE 2.

A log-log plot of the pressure buildup data is presented in Fig. 10. The buildup plot is of considerable interest in gaining an insight as to whether the reservoir may or may not be fractured in the vicinity of RRGE 2. It is known from petroleum engineering literature that when pressure

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Fig. 10: Short-term production test, RRGE 2: Log-log plot of build up versus time.

buildup is plotted on a log-log graph paper, the presence of a unit slope in the early drawdown data is indicative of well-bore storage effects, while the existence of a half-slope is indicative of the presence of large, highly permeable fractures close to the well bore. It is very well seen from Fig. 10 that even within the first ten seconds of shutting down the flow, one fails to discern the presence of a unit slope or a half-slope, leading to the inference that for purposes of overall interpretation, one could effectively treat the reservoir as a porous medium.

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Fig. 9: Short-term production test, RRGE 2: Semi-log plot of drawdown versus time.

Fig. 11: Short-term production test, RRGE 2: Build up as a function of $\log t/t'$.

A plot of pressure buildup as a function of t/t' , where t is the time since flow started and t' is the time since flow stopped, is given in Fig. 11. Since we are aware of the possible presence of barrier boundaries from the drawdown history, the interpretation of the buildup data is rendered somewhat difficult. The drawdown data indicated that the first barrier boundary became noticeable after about 800 seconds of production. Figure 8 indicates a pronounced break in slope at $t/t' \approx 6 \times 10^1$, which corresponds to about 900 seconds. Thus for buildup analysis we fit a straight-line for $t/t' > 6 \times 10^1$ or $t' < 900$ seconds and obtain a kH of about 49,900 millidarcy-feet, which is in reasonable agreement with the kH values indicated by the drawdown data.

Computations in regard to skin effect according to the method of Matthews and Russell (1976) indicate that excess pressure drop due to skin effect is about 0.9 psi, being less than 3 per cent of the total drawdown of 37.5 psi and that the effective well bore radius is about 5.6 inches as compared with the actual radius of about 7 inches. This probably suggests that the borehole is not significantly damaged.

(2) **Long term interference test:** The long term interference test was conducted between September 20 and October 30, 1975, when RRGE 2 was flowed at a near constant discharge of 400 gpm and the water pressure changes were monitored in RRGE 1, 4000 feet away, which acted as the observation well. The production on RRGE 2 lasted for 615.5

hours, extending from 2230 hours on September 20 to 1400 hours on October 16, 1975.

During the course of the test water pressures were monitored in RRGE 1, both at the surface and downhole. The downhole measurements were made with the downhole gage located at approximately 575 psi. The static well head pressure was about 150 psi. The maximum pressure drawdown in RRGE 1 due to production from RRGE 2 was 3.6 psi. The data gathered from the two gages are presented in Appendix 2 and are graphically shown in Plate 2.

The downhole gage was available for use only for a limited period of time, from September 20 until October 6, 1975. Within this period, the performance of the downhole instrument was frequently interrupted by leakage of water through the cable head and consequent instrument malfunction. Such malfunctions occurred five times between September 20 and October 11, 1975 and on each of these occasions the instrument had to be removed from the well, repaired and relowered into the well. Each time the instrument was removed from its setting and repositioned, there was a change in the absolute pressures recorded, the magnitude of the shift being approximately about 1 psi. These shifts are to be attributed to the sensitivity of the instrument to perturbations in temperature and total pressure. However, these slight changes in absolute pressures had no effect on the recorded changes in pressure. It may be noted here that for reservoir interpretation, it is the pressure differentials that are critical and not the absolute pressures.

In preparing the graph of pressure history presented in Plate 2, appropriate adjustments were made in the aforesaid shifts in order to establish overall continuity.

The surface pressure gage was used throughout the period of test from September 20 to October 30, 1975. However, continuous recording equipment was not installed until September 30 and hence only sparse data could be collected during the first ten days of the test. The pressure transient data at RRGE 1, relating to the last ten days of the production period and the entire buildup to data, were collected exclusively from the surface instrument.

As seen from Plate 2, both the downhole and the surface data show the effect of earth tides superposed on the pressure transient caused by the producing well. For a proper interpretation of the interference effects, it was necessary to filter out the effects of the earth tides. In as much as the correlation between the water pressure data and the computed variation in gravity is extremely good (Plate 2), it was possible to eliminate earth tide effects from the fluid pressure data by simply considering (for purposes of interpretation) only the pressure data relating to those instants of time when the computed gravity variation was zero. This procedure was followed in carrying out the interpretation of the drawdown and the buildup data described below.

The interpretation of the drawdown data collected from the downhole instrument at a depth of 1000 feet is presented in Figs. 12 and 13. The log-log plot shown in Fig. 12 shows that the data collected closely match the Theis' type curve during the first 70 hours of drawdown history, suggesting the following parameters for the large portion of the reservoir between the wells: $kH =$

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Fig. 12: Long-term interference test: Log-log plot of drawdown versus time for RRGE 1.

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Fig. 13: Long-term interference test: Semi-log plot of drawdown versus time for RRGE 1.

228,000 millidarcy feet and $\phi cH = 1.19 \times 10^{-3}$ ft/psi. After about 70 hours, the observed drawdowns gradually depart from the type curve of Theis, indicating the presence of a barrier boundary. It is further seen from Fig. 12 that the data points roughly fall between the lines labeled $2R_D$ and $5R_D$ suggesting that the barrier boundary could be treated effectively equivalent to an "image well" located at a distance of approximately $3R_D$ from RRGE 1, where $R_D = 4000$ ft is the distance between the producing well RRGE 2 and the observation well RRGE 1. Theoretically, the barrier boundary should coincide with the perpendicular bisector between the producing well RRGE 2 and the image well. However, since we only have a two-well system, it is impossible to determine the orientation of the image well with reference to RRGE 1 and hence it is not possible to locate the barrier boundary accurately.

A semi-log plot of the drawdown data is presented in Fig. 13. The prominent break in the slope of the straight line at about 130 hours is also indicative of the effects of a barrier boundary. The early drawdown data in Fig. 9 suggest the following parameters for the reservoir: $kH = 228,000$ millidarcy feet, $\phi cH = 9.38 \times 10^{-4}$ ft/psi. Calculations based on the slope change after 130 hours suggest that the barrier boundary is equivalent to an image well located about 11,000 feet from RRGE 1 in an unknown direction.

As mentioned earlier, the pressure buildup data was collected exclusively from the surface instrument. The buildup data is interpreted graphically in Figs. 14 and 15. The pressure buildup values used in the interpretation are corrected buildup values, arrived at after removing the ef-

fects of the production well and its image from the actually observed values of buildup. The components of drawdown due to the production well and its image were in turn evaluated by extrapolating the drawdown curve into the buildup period.

A comparison of Figs. 14 and 12 and Figs. 15 and 13 indicate reasonable agreement in the reservoir behavior observed during production and buildup. In addition to confirming the presence of a barrier boundary, the early drawdown data from Fig. 14 suggest the following reservoir parameters: $kH = 192,800$ millidarcy feet; $\phi cH = 1.06 \times 10^{-3}$ ft/psi. Similarly, the semi-log plot in Fig. 15 indicates, for the reservoir, a kH value of 210,000 millidarcy feet and a ϕcH value of 8.20×10^{-4} ft/psi. Calculations based on the slope change seen in Fig. 11 indicate that the barrier boundary is effectively equivalent to an image well located about 8,500 feet away from RRGE 1.

(3) Short term production test, RRGE 1: The short term test on RRGE 1 was conducted between November 4 and November 7, 1975. After making observations on background reservoir pressure for about 18 hours, the well was flowed at an average discharge of 26.5 gpm for a period of 30 hours from 0845 hours on November 5 to 1445 hours on November 6, 1975. After shutting down flow, pressure buildup was monitored for approximately 19 hours. During the test, the downhole pressure instrument was positioned at a depth of 4700 feet within the well.

Fig. 14: Long-term interference test: Log-log plot of build up versus time for RRGE 1.

The pressure data collected during the test are summarized in Appendix 3 and the time history of pressure change is graphically presented in Plate 3. The maximum pressure drawdown at the end of 30 hours of production was approximately 1.1 psi.

Fig. 15: Long-term interference test: Semi-log plot of build up versus time for RRGE 1.

Fig. 16: Short-term production test, RRGE 1: Log-log plot of drawdown versus time.

Fig. 17: Short-term production test, RRGE 1: Semi-log plot of drawdown versus time.

It can be seen from Plate 3 that throughout the period of observation the observed pressure data indicate significant influence of earth tides. This is to be expected, since the maximum pressure due to well production is small, being only about 1.1 psi.

The interpretation of the pressure drawdown data is presented in Figs. 16 and 17. It should be pointed out here that the significant presence of earth tide effects has rendered the interpretation considerably difficult. Since the flow duration extended only for 30 hours and since during this 30-hour period zero-gravitational change occurred only twice (at 2200 hours on November 5 and 0625 hours on November 6) it was not possible to eliminate the earth tide effects by the same procedure that was employed in the interpretation of the interference test. Nor has it been possible to establish precise correlation coefficients between the tidal junction and the pressure variation. Under these conditions, the best that could be done was to interpret, in an average sense, the actual observed drawdown data. Thus, it is seen from Fig. 16 that matching against Theis' type curve yields a kH value of 105,000 millidarcy feet and a ϕcH value of 2.56×10^{-2} ft/psi, assuming an effective well radius of 1 foot. Again, as seen from Fig. 17, the semi-log plot of the time-drawdown relation suggests a kH value of 132,000 millidarcy feet and a ϕcH value of 7.2×10^{-3} ft/psi, assuming an effective well radius of one foot.

Figure 18 is a plot of the buildup pressures as a function of t/t' where t is the time since flow started and t' is the time since flow shut down. It is readily seen from the figure that there is more than one straight line segment discernible in the plot and it is difficult to conclude the correct one. Computations show that the first line segment indicates a kH of about 67,500 millidarcy feet, which appears somewhat low when compared with the drawdown interpretation. Similar calculations based on the slope of the second line segment indicate a kH value of 661,600 millidarcy feet which seems unreasonably high. The difficulty associated with the interpretation of the buildup data is to be attributed to the masking effects of earth tides.

(4) Summary of test results: The reservoir parameters, as computed from the different tests, are summarized in Table 3. As can be seen from the table, the long duration interference test has indicated a kH of approximately 225,000 millidarcy feet and a ϕcH of about 1×10^{-3} for the large portion of the reservoir included between the two wells RRGE 1 and RRGE 2. If we assume a compressibility value of 1×10^{-5} psi⁻¹ for the rock matrix and an overall porosity of 0.1, then the thickness of the producing horizon works out to about 1000 feet, which seems reasonable from available geological data. This would, in turn, imply an overall average permeability of about 225 millidarcy for the reservoir material which is a satisfactory value.

Fig. 18: Short-term production test, RRGE 1: Build up as a function of $\log t/t'$.

Both the short-term tests have indicated somewhat lower values of kH than the interference test. The computation of the storage parameter, ϕcH , from the short term tests has been rendered difficult due to lack of information on the effective well radius.

The short term test on RRGE 2 has indicated a fairly low value of kH ($\approx 50,000$ millidarcy feet), probably indicating a region of low permeability close to that well. The short term test on RRGE 1 has indicated a kH value ($\approx 130,000$ millidarcy feet) which is much closer to the interference test results, indicating that the reservoir material near that well is much closer to the overall reservoir in respect of permeability.

The interference test has definitely indicated that the reservoir has a barrier boundary that is effectively equivalent to an image well located 12,000 feet from RRGE 1. The precise determination of the location of a hydrological boundary is a problem of triangulation and hence, with only two wells available for testing, it is at present not possible to locate the position of the boundary.

The short term test on RRGE 2 has also indicated the presence of a barrier boundary (or boundaries?) very close to that well, possibly within a few hundred feet. Whether this boundary is indicative of the Bridge Fault which supposedly lies close to RRGE 2 at depth, is uncertain. Alternatively, the possibility exists that the departures observed from the ideal behavior in the short term test data may not be indicative of barrier boundary effects but may be due to other causes such as variation of discharge or commingling of different producing zones.

SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

The Raft River Valley geothermal field is located on a faulted graben filled with sediments ranging in age from Mio-Pliocene (the Salt Lake formation) to Pleistocene (the Raft River formation) with a total thickness of about 5000 feet. The sediments rest on a basement of Adamellite, with an intervening zone of metamorphic rocks, about 200 feet thick.

The successful geothermal wells, RRGE 1 and RRGE 2, have indicated that the geothermal reservoir occurs at the base of the Salt Lake formation and that the producing horizon is probably about 1000 feet thick, extending from about 3600 feet to about 4800 feet. The reservoir temperature is approximately 294°F (146°C).

Three hydraulic tests were conducted to estimate the production parameters of the reservoir. The primary task of these tests was the careful and accurate measurement of water pressure changes in the wells. Towards this end, successful use was made of a sensitive quartz pressure gage, capable of an accuracy of 0.01 psi over an absolute pressure range of 0 - 10,000 psi and with a temperature tolerance of up to 300°F. The tests also showed that a less expensive quartz pressure gage, capable of measuring only wellhead pressures, provides a useful alternative to the more expensive down-hole gage when one is interested only in accurately monitoring wellhead pressure changes in a shut-in observation well.

The data collected during the tests have revealed the interesting fact that the reservoir responds systematically to the small changes in the earth's gravitational field induced by the paths

TABLE 3

TEST		DRAWDOWN		BUILDUP
		Log-log plot	Semi-log plot	
Short term* production test, RRGE 2	kH md-feet	47,600	47,300	49,900
	ϕcH ft/psi	2.91×10^{-2} ($r_w = 1$ ft)	3.03×10^{-2} ($r_w = 1$ ft)	
Long term** interference test	kH md-feet	228,000	228,000	193,000 (210,000 by semi-log plot)
	ϕcH ft/psi	1.19×10^{-3}	9.38×10^{-4}	1.06×10^{-3} (8.20×10^{-4} by semi-log plot)
Short term production test, RRGE 1	kH md-feet	105,000	132,000	67,500 (?)
	ϕcH ft/psi	2.56×10^{-2} ($r_w = 1$ ft)	7.2×10^{-3} ($r_w = 1$ ft)	

* This test indicated the possible presence of a barrier boundary in the vicinity of RRGE 2.

** This test indicated the possible presence of a barrier boundary, equivalent to an image well located about 12,000 feet from RRGE 1.

of the sun and the moon. Appropriate corrections had to be made for these earth tide effects before one could interpret the pressure transient data for the reservoir production parameters.

The long duration interference test has shown that the geothermal reservoir at the Raft River site is in general highly transmissible, with a kH of about 225,000 millidarcy feet. Assuming a total thickness of 1000 feet for the reservoir, this suggests an average reservoir permeability of 225 millidarcy. The interference test has also shown that the geothermal reservoir is bounded in some direction. With only two wells available for testing, it is not at present possible to precisely locate this boundary.

The short duration production tests indicated that the reservoir is probably less permeable in the vicinity of RRGE 2 and that a barrier boundary (Bridge fault?) may be present within a few hundred feet of RRGE 2.

The reservoir tests so far conducted have definitely established that the geothermal reservoir in the Raft River valley is fairly extensive and significantly permeable. The reservoir, therefore, merits further exploration. From the point of view of reservoir assessment, an important question is that of reservoir geometry. In order to accurately determine the location of the barrier boundaries that have been indicated by the tests so far conducted, it is necessary to have additional wells. From available geological information, a favorable location for a third geothermal well would be a site one to two miles southeast of the existing wells, towards the center of the valley.

ACKNOWLEDGMENTS

Dr. Jay Kunz and Messrs. Lowell Miller, Roger Stoker, Gregg Mines, Don Suckling and Gary Cooper of the Idaho National Engineering Laboratory provided the necessary field assistance and facilities in the successful completion of the tests. During the early stages of the tests, Dr. George Miller, Oil Instruments Ltd., helped initiate the use of the downhole quartz pressure gauge. Ms. Jeanette Mullaney of Lawrence Berkeley Laboratory assisted with the processing of field data.

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APPENDIX 1

RRGE 2 SHORT-TERM TEST DATA.

RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

RICE 2 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE /	TIME /	/FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
H.P. GAGE SET AT 5200 FT					
09/12/75	200000		2298.19		
09/12/75	203000		2982.10		
09/12/75	204000		2982.20		
09/12/75	205000		2982.04		
09/12/75	205010		2982.00		
09/12/75	205030		2982.00		
09/12/75	205040		2981.98		
09/12/75	205050		2981.99		
09/12/75	205100		2981.99		
09/12/75	205110		2981.98		
09/12/75	205120		2981.98		
09/12/75	205130		2981.96		
09/12/75	205140		2981.99		
09/12/75	205150		2981.97		
09/12/75	205200		2981.98		
09/12/75	205210		2981.97		
09/12/75	205220		2981.96		
09/12/75	205230		2981.98		
09/12/75	205240		2981.98		
09/12/75	205250		2981.98		
09/12/75	205300		2981.98		
09/12/75	205310		2982.01		
09/12/75	205320		2982.01		
09/12/75	205330		2982.00		
09/12/75	205340		2982.01		
09/12/75	205350		2981.99		
09/12/75	205400		2982.01		
09/12/75	205410		2982.00		
09/12/75	205420		2982.01		
09/12/75	205430		2982.01		
09/12/75	205440		2982.03		
09/12/75	205450		2982.02		
09/12/75	205500		2982.04		
09/12/75	205510		2982.03		
09/12/75	205520		2982.01		
09/12/75	205530		2982.04		
09/12/75	205540		2982.02		
09/12/75	205550		2982.02		
09/12/75	205600		2982.05		
09/12/75	205610		2982.05		
09/12/75	205620		2081.22		
09/12/75	205630		2298.22		
09/12/75	205650		2298.23		
09/12/75	205720		2298.23		
09/12/75	205750		2298.22		
09/12/75	205820		2298.22		
09/12/75	205829		2298.23		
09/12/75	205830		2298.22		
09/12/75	205840		2298.24		
09/12/75	205850		2298.23		
09/12/75	205900		2298.23		
09/12/75	205910		2298.22		
09/12/75	205920		2298.23		
09/12/75	205930		2298.23		
09/12/75	205940		2298.22		
09/12/75	205950		2298.23		
09/12/75	210000		2298.22		
09/12/75	210010		2298.24		
09/12/75	210020		2298.22		
09/12/75	210030		2298.23		
09/12/75	210040		2298.24		
09/12/75	210050		2298.23		
09/12/75	210100		2298.24		
09/12/75	210110		2298.24		
09/12/75	210150		2298.23		
09/12/75	210200		2298.24		
09/12/75	210210		2298.23		
09/12/75	210220		2298.22		

DATE /	TIME /	/FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
09/12/75	210230		2298.23		
09/12/75	210240		2298.24		
09/12/75	210250		2298.22		
09/12/75	210300		2298.24		
09/12/75	210310		2298.24		
09/12/75	210320		2298.22		
09/12/75	210330		2298.25		
09/12/75	210340		2298.23		
09/12/75	210350		2298.22		
09/12/75	210400		2298.25		
09/12/75	210410		2298.23		
09/12/75	210420		2298.24		
09/12/75	210430		2298.24		
09/12/75	210440		2298.23		
09/12/75	210450		2298.23		
09/12/75	210500		2298.24		
09/12/75	210510		2298.23		
09/12/75	210520		2298.24		
09/12/75	210530		2298.22		
09/12/75	210540		2298.23		
09/12/75	210550		2298.24		
09/12/75	210600		2298.24		
09/12/75	210610		2298.22		
09/12/75	210620		2298.22		
09/12/75	210630		2298.24		
09/12/75	210640		2298.23		
09/12/75	210650		2298.22		
09/12/75	210700		2298.23		
09/12/75	210710		2298.22		
09/12/75	210720		2298.22		
09/12/75	210730		2298.22		
09/12/75	210740		2298.22		
09/12/75	210750		2298.22		
09/12/75	210800		2298.23		
09/12/75	210810		2298.22		
09/12/75	210820		2298.22		
09/12/75	210830		2298.22		
09/12/75	210840		2298.22		
09/12/75	210850		2298.23		
09/12/75	210900		2298.23		
09/12/75	210910		2298.23		
09/12/75	210920		2298.23		
09/12/75	210930		2298.23		
09/12/75	210940		2298.24		
09/12/75	210950		2298.23		
09/12/75	211000		2298.23		
09/12/75	211010		2298.24		
09/12/75	211020		2298.24		
09/12/75	211030		2298.24		
09/12/75	211040		2298.23		
09/12/75	211050		2298.24		
09/12/75	211100		2298.24		
09/12/75	211110		2298.24		
09/12/75	211120		2298.24		
09/12/75	211130		2298.23		
09/12/75	211140		2298.22		VALVE BRIEFLY OPENED AND THEN CLOSED.
09/12/75	211150		2298.24		
09/12/75	211200		2296.60		
09/12/75	211210		2291.97		
09/12/75	211220		2291.08		
09/12/75	211230		2296.38		
09/12/75	211240		2297.29		
09/12/75	211250		2297.69		
09/12/75	211300		2297.74		
09/12/75	211310		2297.85		
09/12/75	211320		2297.86		
09/12/75	211330		2297.93		
09/12/75	211340		2297.95		
09/12/75	211350		2297.97		

RICE 2 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
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09/12/75	211400		2297.97		
09/12/75	211410		2298.00		
09/12/75	211420		2298.01		
09/12/75	211430		2298.03		
09/12/75	211440		2298.01		

09/12/75	211450		2298.02		
09/12/75	211500		2298.02		
09/12/75	211600		2298.08		
09/12/75	211700		2298.08		
09/12/75	211800		2298.08		

09/12/75	211900		2298.11		
09/12/75	212000		2298.11		
09/12/75	212100		2298.12		
09/12/75	212200		2298.14		
09/12/75	212300		2298.14		

09/12/75	212343		2298.13		
09/12/75	212345		2298.13		
09/12/75	212346		2298.15		
09/12/75	212347		2298.13		
09/12/75	212348		2298.13		

09/12/75	212350		2298.14		
09/12/75	212351		2298.15		
09/12/75	212352		2298.13		
09/12/75	212353		2298.15		
09/12/75	212354		2298.13		

09/12/75	212355		2298.14		
09/12/75	212356		2298.15		
09/12/75	212358		2298.12		
09/12/75	212359		2298.14		
09/12/75	212400		2298.13		

09/12/75	212401		2298.13		
09/12/75	212402		2298.15		
09/12/75	212403		2298.12		
09/12/75	212404		2298.15		
09/12/75	212406		2298.14		

09/12/75	212407		2298.14		
09/12/75	212408		2298.14		
09/12/75	212409		2298.12		
09/12/75	212410		2298.15		
09/12/75	212411		2298.12		

09/12/75	212412		2298.14		
09/12/75	212414		2298.13		
09/12/75	212415		2298.13		
09/12/75	212416		2298.14		
09/12/75	212417		2298.12		

09/12/75	212418		2298.14		
09/12/75	212419		2298.13		
09/12/75	212420		2298.14		
09/12/75	212422		2298.14		
09/12/75	212423		2298.13		

09/12/75	212424		2298.14		
09/12/75	212425		2298.12		
09/12/75	212426		2298.15		
09/12/75	212427		2298.13		
09/12/75	212428		2298.13		

09/12/75	212430		2298.15		
09/12/75	212431		2298.14		
09/12/75	212432		2298.15		
09/12/75	212433		2298.13		
09/12/75	212434		2298.15		

09/12/75	212435		2298.14		
09/12/75	212436		2298.13		
09/12/75	212438		2298.15		
09/12/75	212439		2298.15		
09/12/75	212440		2298.13		

09/12/75	212441		2298.14		
09/12/75	212442		2298.14		
09/12/75	212443		2298.13		
09/12/75	212444		2298.14		
09/12/75	212446		2298.12		

DATE /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
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09/12/75	212447		2298.14		
09/12/75	212448		2298.14		
09/12/75	212449		2298.14		
09/12/75	212450		2298.14		
09/12/75	212451		2298.12		

09/12/75	212452		2298.14		
09/12/75	212454		2298.14		
09/12/75	212455		2298.14		
09/12/75	212456		2298.14		
09/12/75	212457		2298.13		

09/12/75	212458		2298.15		
09/12/75	212459		2298.13		
09/12/75	212500		2298.15		
09/12/75	212502		2298.14		

VALVE OPENED FOR PRODUCTION. FLOWRATE=210 GPM.

09/12/75	212503		2298.14		
09/12/75	212504		2298.15		
09/12/75	212505		2298.13		
09/12/75	212506		2298.15		
09/12/75	212507		2298.13		

09/12/75	212508		2298.15		
09/12/75	212510		2298.14		
09/12/75	212511		2298.14		
09/12/75	212512		2298.15		

ASSUMED ZERO TIME FOR PRESSURE DRAWDOWN.

09/12/75	212513		2298.12		
09/12/75	212514		2297.93		
09/12/75	212515		2298.20		
09/12/75	212516		2293.70		
09/12/75	212518		2293.73		

09/12/75	212519		2298.00		
09/12/75	212520		2298.00		
09/12/75	212521		2298.33		
09/12/75	212522		2298.73		
09/12/75	212523		2298.37		

09/12/75	212524		2298.02		
09/12/75	212526		2298.90		
09/12/75	212527		2298.09		
09/12/75	212528		2298.51		
09/12/75	212529		2298.40		

09/12/75	212530		2298.41		
09/12/75	212531		2298.23		
09/12/75	212532		2298.07		
09/12/75	212534		2298.01		
09/12/75	212535		2298.94		

09/12/75	212536		2298.78		
09/12/75	212537		2298.72		
09/12/75	212538		2298.66		
09/12/75	212539		2298.55		
09/12/75	212540		2298.48		

09/12/75	212542		2298.40		
09/12/75	212543		2298.35		
09/12/75	212544		2298.26		
09/12/75	212545		2298.19		
09/12/75	212546		2298.16		

09/12/75	212547		2298.07		
09/12/75	212548		2298.03		
09/12/75	212550		2289.97		
09/12/75	212551		2289.90		
09/12/75	212552		2289.80		

09/12/75	212553		2289.62		
09/12/75	212554		2289.56		
09/12/75	212555		2289.52		
09/12/75	212556		2289.42		
09/12/75	212558		2289.36		

09/12/75	212559		2289.33		
09/12/75	212600		2289.26		
09/12/75	212601		2289.20		
09/12/75	212602		2289.16		
09/12/75	212603		2289.09		

RRGE 2 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
03/12/75	212604		2269.07		
03/12/75	212606		2269.01		
03/12/75	212607		2268.96		
03/12/75	212608		2268.93		
03/12/75	212609		2268.87		
03/12/75	212610		2268.85		
03/12/75	212611		2268.80		
03/12/75	212612		2268.76		
03/12/75	212614		2268.73		
03/12/75	212615		2268.67		
03/12/75	212616		2268.66		
03/12/75	212617		2268.62		
03/12/75	212618		2268.58		
03/12/75	212619		2268.56		
03/12/75	212620		2268.51		
03/12/75	212622		2268.49		
03/12/75	212623		2268.46		
03/12/75	212624		2268.41		
03/12/75	212625		2268.40		
03/12/75	212626		2268.36		
03/12/75	212627		2268.33		
03/12/75	212628		2268.31		
03/12/75	212630		2268.27		
03/12/75	212631		2268.25		
03/12/75	212632		2268.21		
03/12/75	212633		2268.20		
03/12/75	212634		2268.17		
03/12/75	212635		2268.13		
03/12/75	212636		2268.14		
03/12/75	212638		2268.10		
03/12/75	212639		2268.07		
03/12/75	212640		2268.05		
03/12/75	212641		2268.02		
03/12/75	212642		2268.01		
03/12/75	212643		2267.97		
03/12/75	212644		2267.96		
03/12/75	212646		2267.94		
03/12/75	212647		2267.90		
03/12/75	212648		2267.89		
03/12/75	212649		2267.85		
03/12/75	212650		2267.85		
03/12/75	212651		2267.82		
03/12/75	212652		2267.79		
03/12/75	212654		2267.79		
03/12/75	212655		2267.74		
03/12/75	212656		2267.75		
03/12/75	212657		2267.72		
03/12/75	212658		2267.69		
03/12/75	212659		2267.68		
03/12/75	212700		2267.64		
03/12/75	212702		2267.64		
03/12/75	212703		2267.62		
03/12/75	212704		2267.60		
03/12/75	212705		2267.59		
03/12/75	212706		2267.56		
03/12/75	212707		2267.56		
03/12/75	212708		2267.53		
03/12/75	212710		2267.52		
03/12/75	212711		2267.51		
03/12/75	212712		2267.47		
03/12/75	212713		2267.47		
03/12/75	212714		2267.44		
03/12/75	212715		2267.43		
03/12/75	212716		2267.41		
03/12/75	212718		2267.38		
03/12/75	212719		2267.40		
03/12/75	212720		2267.34		
03/12/75	212721		2267.34		
03/12/75	212722		2267.34		
03/12/75	212723		2267.30		

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
03/12/75	212730		2267.23		
03/12/75	212740		2267.08		
03/12/75	212750		2266.97		
03/12/75	212800		2266.85		
03/12/75	212810		2266.76		
03/12/75	212820		2266.64		
03/12/75	212830		2266.52		
03/12/75	212840		2266.45		
03/12/75	212850		2266.37		
03/12/75	212900		2266.24		
03/12/75	212910		2266.18		
03/12/75	212920		2266.09		
03/12/75	212930		2266.00		
03/12/75	212940		2265.93		
03/12/75	212950		2265.86		
03/12/75	213000		2265.77		
03/12/75	213010		2265.68		
03/12/75	213020		2265.63		
03/12/75	213030		2265.54		
03/12/75	213040		2265.45		
03/12/75	213050		2265.40		
03/12/75	213100		2265.33		
03/12/75	213110		2265.25		
03/12/75	213120		2265.20		
03/12/75	213130		2265.12		
03/12/75	213140		2265.07		
03/12/75	213150		2265.00		
03/12/75	213200		2264.94		
03/12/75	213210		2264.86		
03/12/75	213220		2264.83		
03/12/75	213230		2264.79		
03/12/75	213240		2264.74		
03/12/75	213250		2264.70		
03/12/75	213300		2264.67		
03/12/75	213310		2264.62		
03/12/75	213320		2264.57		
03/12/75	213330		2264.52		
03/12/75	213340		2264.47		
03/12/75	213350		2264.43		
03/12/75	213400		2264.40		
03/12/75	213410		2264.36		
03/12/75	213420		2264.29		
03/12/75	213430		2264.25		
03/12/75	213440		2264.21		
03/12/75	213450		2264.16		
03/12/75	213500		2264.11		
03/12/75	213510		2264.08		
03/12/75	213520		2264.05		
03/12/75	213530		2264.00		
03/12/75	213540		2263.96		
03/12/75	213550		2263.91		
03/12/75	213600		2263.89		
03/12/75	213610		2263.85		
03/12/75	213620		2263.79		
03/12/75	213630		2263.74		
03/12/75	213640		2263.73		
03/12/75	213650		2263.69		
03/12/75	213700		2263.67		
03/12/75	213710		2263.61		
03/12/75	213720		2263.58		
03/12/75	213730		2263.56		
03/12/75	213740		2263.55		
03/12/75	213750		2263.52		
03/12/75	213800		2263.48		
03/12/75	213810		2263.46		
03/12/75	213820		2263.38		
03/12/75	213830		2263.38		
03/12/75	213840		2263.34		
03/12/75	213850		2263.29		
03/12/75	213900		2263.25		

RRGE 2 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
03/12/75	213910		2283.20		
03/12/75	213920		2283.16		
03/12/75	213930		2283.12		
03/12/75	213940		2283.06		
03/12/75	213950		2283.04		
03/12/75	214000		2283.02		
03/12/75	214010		2282.97		
03/12/75	214020		2282.93		
03/12/75	214030		2282.91		
03/12/75	214040		2282.88		
03/12/75	214050		2282.84		
03/12/75	214100		2282.80		
03/12/75	214110		2282.77		
03/12/75	214120		2282.73		
03/12/75	214130		2282.71		
03/12/75	214140		2282.67		
03/12/75	214150		2282.64		
03/12/75	214200		2282.61		
03/12/75	214210		2282.58		
03/12/75	214220		2282.53		
03/12/75	214230		2282.51		
03/12/75	214240		2282.47		
03/12/75	214250		2282.45		
03/12/75	214300		2282.42		
03/12/75	214310		2282.37		
03/12/75	214320		2282.35		
03/12/75	214330		2282.31		
03/12/75	214340		2282.28		
03/12/75	214350		2282.26		
03/12/75	214400		2282.24		
03/12/75	214410		2282.19		
03/12/75	214420		2282.16		
03/12/75	214430		2282.14		
03/12/75	214440		2282.09		
03/12/75	214450		2282.07		
03/12/75	214500		2282.04		
03/12/75	214510		2281.99		
03/12/75	214520		2281.95		
03/12/75	214530		2281.92		
03/12/75	214540		2281.86		
03/12/75	214545		2281.86		
03/12/75	214600		2281.82		
03/12/75	214700		2281.65		
03/12/75	214800		2281.48		
03/12/75	214900		2281.32		
03/12/75	215000		2281.16		
03/12/75	215100		2281.01		
03/12/75	215200		2280.85		
03/12/75	215300		2280.71		
03/12/75	215400		2280.55		
03/12/75	215500		2280.35		
03/12/75	215600		2280.22		
03/12/75	215700		2280.08		
03/12/75	215800		2279.96		
03/12/75	215900		2279.84		
03/12/75	220000		2279.67		
03/12/75	220100		2279.54		
03/12/75	220200		2279.41		
03/12/75	220300		2279.28		
03/12/75	220400		2279.16		
03/12/75	220500		2279.08		
03/12/75	220600		2278.95		
03/12/75	220700		2278.79		
03/12/75	220800		2278.69		
03/12/75	220900		2278.59		
03/12/75	221000		2278.48		
03/12/75	221100		2278.35		
03/12/75	221200		2278.23		
03/12/75	221300		2278.14		
03/12/75	221400		2278.01		

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
03/12/75	221500		2277.90		
03/12/75	221600		2277.79		
03/12/75	221700		2277.69		
03/12/75	221800		2277.50		
03/12/75	221900		2277.44		
03/12/75	222000		2277.32		
03/12/75	222100		2277.20		
03/12/75	222200		2277.10		
03/12/75	222300		2276.99		
03/12/75	222400		2276.89		
03/12/75	222500		2276.74		
03/12/75	222600		2276.64		
03/12/75	222700		2276.53		
03/12/75	222800		2276.46		
03/12/75	222900		2276.35		
03/12/75	223000		2276.24		
03/12/75	223100		2276.17		
03/12/75	223200		2276.09		
03/12/75	223300		2276.02		
03/12/75	223400		2275.92		
03/12/75	223500		2275.85		
03/12/75	223600		2275.80		
03/12/75	223700		2275.72		
03/12/75	223800		2275.60		
03/12/75	223900		2275.51		
03/12/75	224000		2275.41		
03/12/75	224100		2275.34		
03/12/75	224200		2275.30		
03/12/75	224300		2275.21		
03/12/75	224400		2275.15		
03/12/75	224500		2275.07		
03/12/75	224600		2275.01		
03/12/75	224700		2274.94		
03/12/75	224800		2274.87		
03/12/75	224900		2274.77		
03/12/75	225000		2274.73		
03/12/75	225100		2274.66		
03/12/75	225200		2274.61		
03/12/75	225300		2274.58		
03/12/75	225400		2274.51		
03/12/75	225500		2274.43		
03/12/75	225600		2274.37		
03/12/75	225700		2274.29		
03/12/75	225800		2274.24		
03/12/75	225900		2274.22		
03/12/75	230000		2274.08		
03/12/75	230100		2274.08		
03/12/75	230200		2274.03		
03/12/75	230300		2273.95		
03/12/75	230400		2273.93		
03/12/75	230500		2273.85		
03/12/75	230600		2273.79		
03/12/75	230700		2273.78		
03/12/75	230800		2273.71		
03/12/75	230900		2273.63		
03/12/75	231000		2273.63		
03/12/75	231100		2273.48		
03/12/75	231200		2273.46		
03/12/75	231300		2273.46		
03/12/75	231400		2273.42		
03/12/75	231500		2273.39		
03/12/75	231600		2273.33		
03/12/75	231649		2273.27		
03/12/75	232000		2273.15		
03/12/75	233000		2272.71		
03/12/75	234000		2272.31		
03/12/75	235000		2272.02		
03/13/75	000000		2271.63		
03/13/75	001000		2271.27		
03/13/75	002000		2271.01		

RRGE 2 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS	DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
09/13/75	003000		2278.82			09/13/75	121800		2261.378		
09/13/75	004000		2270.58			09/13/75	121721		2261.3		
09/13/75	005000		2270.42			09/13/75	121723		2261.2		
09/13/75	010000		2270.23			09/13/75	121724		2261.4		
09/13/75	011000		2270.06			09/13/75	121725		2261.3		
09/13/75	012000		2269.91			09/13/75	121726		2261.3		
09/13/75	013000		2269.75			09/13/75	121727		2261.4		
09/13/75	014000		2269.58			09/13/75	121728		2261.3		
09/13/75	015000		2269.32			09/13/75	121729		2261.3		
09/13/75	020000		2269.13			09/13/75	121730		2261.3		
09/13/75	021000		2269.88			09/13/75	121731		2261.4		
09/13/75	022000		2268.75			09/13/75	121732		2261.3		
09/13/75	023000		2268.45			09/13/75	121733		2261.3		
09/13/75	024000		2268.15			09/13/75	121734		2261.3		
09/13/75	025000		2267.93			09/13/75	121735		2261.2		
09/13/75	030000		2267.61			09/13/75	121736		2261.4		
09/13/75	031000		2267.56			09/13/75	121737		2261.1		
09/13/75	032000		2267.42			09/13/75	121738		2261.4		
09/13/75	033000		2266.29			09/13/75	121739		2261.2		
09/13/75	034000		2267.10			09/13/75	121740		2261.3		
09/13/75	035000		2266.88			09/13/75	121741		2261.1		
09/13/75	040000		2266.65			09/13/75	121742		2261.3		
09/13/75	041000		2266.41			09/13/75	121743		2261.2		
09/13/75	042000		2266.21			09/13/75	121744		2261.4		
09/13/75	043000		2265.99			09/13/75	121745		2261.2		
09/13/75	044000		2265.80			09/13/75	121746		2261.3		
09/13/75	045000		2265.62			09/13/75	121747		2261.2		
09/13/75	050000		2265.43			09/13/75	121748		2261.4		
09/13/75	051000		2265.18			09/13/75	121749		2261.2		
09/13/75	052000		2264.96			09/13/75	121750		2261.4		
09/13/75	053000		2264.52			09/13/75	121751		2261.2		
09/13/75	054000		2264.18			09/13/75	121752		2261.4		
09/13/75	055000		2263.96			09/13/75	121753		2261.2		
09/13/75	060000		2263.73			09/13/75	121754		2261.4		
09/13/75	061000		2263.57			09/13/75	121755		2261.2		
09/13/75	062000		2263.36			09/13/75	121756		2261.3		
09/13/75	063000		2263.27			09/13/75	121757		2261.2		
09/13/75	064000		2263.22			09/13/75	121758		2261.3		
09/13/75	065000		2263.11			09/13/75	121759		2261.2		
09/13/75	070000		2262.94			09/13/75	121800		2261.3		
09/13/75	071000		2262.85			09/13/75	121801		2261.2		
09/13/75	072000		2262.71			09/13/75	121802		2261.3		
09/13/75	073000		2262.59			09/13/75	121803		2261.2		
09/13/75	074000		2262.47			09/13/75	121804		2261.3		
09/13/75	075000		2262.29			09/13/75	121805		2261.1		
09/13/75	080000		2262.20			09/13/75	121806		2261.4		
09/13/75	081000		2262.07			09/13/75	121807		2261.2		
09/13/75	082000		2261.96			09/13/75	121808		2261.3		
09/13/75	083000		2262.07			09/13/75	121809		2261.2		
09/13/75	084000		2261.73			09/13/75	121810		2261.4		
09/13/75	085000		2261.34			09/13/75	121811		2261.1		
09/13/75	090000		2261.26			09/13/75	121812		2261.3		
09/13/75	091000		2261.14			09/13/75	121813		2261.1		
09/13/75	092000		2261.02			09/13/75	121814		2261.3		
09/13/75	093000		2260.89			09/13/75	121815		2261.1		
09/13/75	094000		2260.84			09/13/75	121816		2261.3		
09/13/75	095000		2260.75			09/13/75	121817		2261.2		
09/13/75	100000		2260.66		HYDRIL LEAKING BADLY.	09/13/75	121818		2261.4		
09/13/75	101000		2259.53		HYDRIL SHUT.	09/13/75	121819		2261.1		
09/13/75	102000		2260.24			09/13/75	121820		2261.3		
09/13/75	103000		2261.45			09/13/75	121821		2261.2		
09/13/75	104000		2261.56			09/13/75	121822		2261.3		
09/13/75	105000		2261.59			09/13/75	121823		2261.2		
09/13/75	110000		2261.599			09/13/75	121824		2261.3		
09/13/75	111000		2261.623			09/13/75	121825		2261.2		
09/13/75	112000		2261.590			09/13/75	121826		2261.4		
09/13/75	113000		2261.593			09/13/75	121827		2261.2		
09/13/75	114000		2261.525			09/13/75	121828		2261.3		
09/13/75	115000		2261.491			09/13/75	121829		2261.1		
09/13/75	120000		2261.445			09/13/75	121830		2261.4		

RRGE 2 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
09/13/75	121031		2261.1		
09/13/75	121032		2261.3		
09/13/75	121033		2261.2		
09/13/75	121034		2261.3		
09/13/75	121035		2261.1		
09/13/75	121036		2261.3		
09/13/75	121037		2261.1		
09/13/75	121038		2261.3		
09/13/75	121039		2261.1		
09/13/75	121040		2261.3		
09/13/75	121041		2261.2		
09/13/75	121042		2261.3		
09/13/75	122505		2261.2		
09/13/75	122506		2261.3		
09/13/75	122507		2261.2		
09/13/75	122508		2261.3		
09/13/75	122509		2261.1		
09/13/75	122510		2261.3		
09/13/75	122511		2261.1		
09/13/75	122512		2261.3		
09/13/75	122513		2261.2		
09/13/75	122514		2261.3		
09/13/75	122515		2261.2		FLOW SHUT IN.
09/13/75	122516		2261.5		
09/13/75	122517		2261.9		
09/13/75	122518		2262.9		
09/13/75	122519		2264.9		
09/13/75	122520		2266.3		
09/13/75	122521		2266.9		
09/13/75	122522		2267.3		
09/13/75	122523		2267.6		
09/13/75	122524		2267.8		
09/13/75	122525		2268.0		
09/13/75	122526		2268.2		
09/13/75	122527		2268.4		
09/13/75	122528		2268.5		
09/13/75	122529		2268.6		
09/13/75	122530		2268.7		
09/13/75	122531		2268.8		
09/13/75	122532		2268.9		
09/13/75	122533		2268.9		
09/13/75	122534		2269.0		
09/13/75	122535		2269.1		
09/13/75	122536		2269.1		
09/13/75	122537		2269.2		
09/13/75	122538		2269.3		
09/13/75	122539		2269.3		
09/13/75	122540		2269.4		
09/13/75	122541		2269.4		
09/13/75	122542		2269.5		
09/13/75	122543		2269.5		
09/13/75	122544		2269.6		
09/13/75	122545		2269.6		
09/13/75	122546		2269.7		
09/13/75	122547		2269.7		
09/13/75	122548		2269.7		
09/13/75	122549		2269.8		
09/13/75	122550		2269.8		
09/13/75	122551		2269.7		
09/13/75	122552		2270.0		
09/13/75	122553		2269.9		
09/13/75	122554		2270.0		
09/13/75	122555		2269.9		
09/13/75	122556		2270.1		
09/13/75	122557		2270.0		
09/13/75	122558		2270.2		
09/13/75	122559		2270.0		
09/13/75	122600		2270.2		
09/13/75	122601		2270.2		
09/13/75	122602		2270.3		

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
09/13/75	122603			2270.2	
09/13/75	122604			2270.4	
09/13/75	122605			2270.3	
09/13/75	122606			2270.4	
09/13/75	122607			2270.3	
09/13/75	122608			2270.6	
09/13/75	122609			2270.5	
09/13/75	122610			2270.6	
09/13/75	122611			2270.5	
09/13/75	122612			2270.6	
09/13/75	122613			2270.6	
09/13/75	122614			2270.7	
09/13/75	122615			2270.7	
09/13/75	122616			2270.8	
09/13/75	122617			2270.7	
09/13/75	122618			2270.9	
09/13/75	122619			2270.8	
09/13/75	122620			2270.6	
09/13/75	122621			2270.9	
09/13/75	122622			2270.7	
09/13/75	122623			2270.9	
09/13/75	122624			2270.7	
09/13/75	122625			2270.9	
09/13/75	122626			2270.8	
09/13/75	122627			2271.0	
09/13/75	122628			2270.9	
09/13/75	122629			2271.1	
09/13/75	122630			2270.9	
09/13/75	122631			2271.1	
09/13/75	122632			2270.9	
09/13/75	122633			2271.2	
09/13/75	122634			2271.0	
09/13/75	122635			2271.2	
09/13/75	122636			2271.0	
09/13/75	122637			2271.2	
09/13/75	122638			2271.1	
09/13/75	122639			2271.3	
09/13/75	122640			2271.1	
09/13/75	122641			2271.3	
09/13/75	122642			2271.2	
09/13/75	122643			2271.3	
09/13/75	122644			2271.4	
09/13/75	122645			2271.4	
09/13/75	122646			2271.5	
09/13/75	122647			2271.4	
09/13/75	122648			2271.4	
09/13/75	122649			2271.4	
09/13/75	122650			2271.5	
09/13/75	122651			2271.5	
09/13/75	122652			2271.5	
09/13/75	122653			2271.5	
09/13/75	122654			2271.6	
09/13/75	122655			2271.5	
09/13/75	122656			2271.6	
09/13/75	122657			2271.6	
09/13/75	122658			2271.7	
09/13/75	122659			2271.6	
09/13/75	122700			2271.7	
09/13/75	122710			2271.6	
09/13/75	122720			2271.8	
09/13/75	122730			2272.1	
09/13/75	122740			2272.1	
09/13/75	122750			2272.2	
09/13/75	122800			2272.3	
09/13/75	122810			2272.5	
09/13/75	122820			2280.66	
09/13/75	122830			2272.76	
09/13/75	122840			2272.86	
09/13/75	122850			2272.93	
09/13/75	122900			2273.03	

RAGE 2 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
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09/13/75	122910		2273.13		
09/13/75	122920		2273.21		
09/13/75	122930		2273.27		
09/13/75	122940		2273.38		
09/13/75	122950		2273.43		

09/13/75	123000		2273.54		
09/13/75	123010		2273.59		
09/13/75	123020		2273.68		
09/13/75	123030		2273.76		
09/13/75	123040		2273.82		

09/13/75	123050		2273.90		
09/13/75	123100		2273.96		
09/13/75	123104		2274.01		
09/13/75	123200		2274.37		
09/13/75	123300		2274.69		

09/13/75	123400		2275.82		
09/13/75	123500		2275.31		
09/13/75	123600		2275.52		
09/13/75	123700		2275.77		
09/13/75	123800		2276.02		

09/13/75	123900		2276.28		
09/13/75	124000		2276.40		
09/13/75	124100		2276.56		
09/13/75	124200		2276.78		
09/13/75	124300		2276.96		

09/13/75	124400		2277.13		
09/13/75	124600		2277.43		
09/13/75	124800		2277.78		
09/13/75	125000		2278.07		
09/13/75	125200		2278.36		

09/13/75	125400		2278.61		
09/13/75	125600		2278.88		
09/13/75	125800		2279.12		
09/13/75	130000		2279.36		
09/13/75	130100		2279.47		

09/13/75	130200		2279.59		
09/13/75	130300		2279.70		
09/13/75	130400		2279.82		
09/13/75	130500		2279.95		
09/13/75	130600		2280.04		

09/13/75	130700		2280.10		
09/13/75	130800		2280.22		
09/13/75	130900		2280.32		
09/13/75	131000		2280.40		
09/13/75	131100		2280.49		

09/13/75	131200		2280.56		
09/13/75	131300		2280.67		
09/13/75	131400		2280.77		
09/13/75	131500		2280.84		
09/13/75	131600		2280.94		

09/13/75	131700		2281.02		
09/13/75	131800		2281.10		
09/13/75	131900		2281.17		
09/13/75	132000		2281.24		
09/13/75	132100		2281.33		

09/13/75	132200		2281.43		
09/13/75	132300		2281.50		
09/13/75	132400		2281.57		
09/13/75	132500		2281.63		
09/13/75	132600		2281.70		

09/13/75	132700		2281.80		
09/13/75	132800		2281.88		
09/13/75	132900		2281.92		
09/13/75	133000		2282.01		
09/13/75	133100		2282.07		

09/13/75	133200		2282.14		
09/13/75	133300		2282.20		
09/13/75	133400		2282.24		
09/13/75	133500		2282.31		
09/13/75	133600		2282.39		

DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
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09/13/75	133700		2282.45		
09/13/75	133800		2282.53		
09/13/75	133900		2282.58		
09/13/75	134000		2282.62		
09/13/75	134100		2282.70		

09/13/75	134200		2282.76		
09/13/75	134300		2282.85		
09/13/75	134400		2282.88		
09/13/75	134500		2282.95		
09/13/75	134600		2283.00		

09/13/75	134700		2283.08		
09/13/75	134800		2283.12		
09/13/75	134900		2283.16		
09/13/75	135000		2283.21		
09/13/75	135100		2283.25		

09/13/75	135200		2283.31		
09/13/75	135300		2283.37		
09/13/75	135400		2283.43		
09/13/75	135500		2283.49		
09/13/75	135600		2283.52		

09/13/75	135700		2283.60		
09/13/75	135800		2283.63		
09/13/75	135900		2283.64		
09/13/75	140000		2283.68		
09/13/75	140100		2283.76		

09/13/75	140200		2283.81		
09/13/75	140300		2283.88		
09/13/75	140400		2283.92		
09/13/75	140441		2283.95		

END OF DATA

APPENDIX 2

RRGE 1 INTERFERENCE TEST DATA.

RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE	TIME	FLOW RATE (GPH)	DOWNHOLE PRESSURE (PSIA)	WELL HEAD PRESSURE (PSIA)	REMARKS
9/14/75	1720		575.872	150.465	
9/14/75	1730		575.865		
9/14/75	1740		575.868		
9/14/75	1750		575.862		
9/14/75	1800		575.855		
9/14/75	1810		575.854		
9/14/75	1820		575.846		
9/14/75	1830		575.845		
9/14/75	1840		575.843		
9/14/75	1850		575.833		
9/14/75	1900		575.820		
9/14/75	1910		575.829		
9/14/75	1920		575.825		
9/14/75	1920		.825		PRODUCTION STARTED AT
9/14/75	1930		575.822		
9/14/75	2000	916	575.815	.354	
9/14/75	2030	916	575.783		
9/14/75	2100	916	575.752		
9/14/75	2130	916	575.729		
9/14/75	2200	916	575.706		
9/14/75	2230	916	575.713		
9/14/75	2300	916	575.683		
9/14/75	2300		.683		AT 2310 HRS. LEAKAGE IN
9/14/75	2330	916	575.712		
9/15/75	0000	916	575.685	.232	
9/15/75	0030	916	575.659		
9/15/75	0100	916	575.646		
9/15/75	0130	916	575.639		
9/15/75	0200	916	575.622		
9/15/75	0230	916	575.608		
9/15/75	0300	916	575.593		
9/15/75	0330	916	575.581		
9/15/75	0400	916	575.565		
9/15/75	0430	916	575.545		
9/15/75	0500	916	575.518		
9/15/75	0530	916	575.493		
9/15/75	0600	916	575.471		
9/15/75	0630	916	575.439		
9/15/75	0700	916	575.480		
9/15/75	0730	808	575.387	149.951	
9/15/75	0800	808	575.354		
9/15/75	0830	808	575.337		
9/15/75	0900	808	575.308		
9/15/75	0930	808	575.283		
9/15/75	1000	808	575.263		
9/15/75	1030	808	575.249		
9/15/75	1100	808	575.236		
9/15/75	1130	808	575.224		
9/15/75	1200	836	575.216	.849	
9/15/75	1230	836	575.212		
9/15/75	1300	836	575.210		
9/15/75	1330	836	575.203		
9/15/75	1400	836	575.200		
9/15/75	1430	836	575.201		
9/15/75	1500	836	575.210		
9/15/75	1530	808	575.208		
9/15/75	1600	808	575.206	149.892	
9/15/75	1630	808	575.206		
9/15/75	1700	808	575.195		
9/15/75	1730	808	575.186		
9/15/75	1800	808	575.172		
9/15/75	1830	808	575.155		
9/15/75	1900	808	575.145		
9/15/75	1930	808	575.127		
9/15/75	2000	458	575.866	.757	
9/15/75	2030	458	575.874		
9/15/75	2100	458	575.863		

DATE	TIME	FLOW RATE (GPH)	DOWNHOLE PRESSURE (PSIA)	WELL HEAD PRESSURE (PSIA)	REMARKS
9/15/75	2130	458	575.836		
9/15/75	2200	458	575.824		
9/15/75	2230	458	575.817		
9/15/75	2300	458	575.		
9/15/75	2330	458	575.005		
9/16/75	0000	458	575.818	.681	
9/16/75	0030	458	575.806		
9/16/75	0100	458	575.811		
9/16/75	0130	458	575.802		
9/16/75	0200	458	575.801		
9/16/75	0230	458	575.805		
9/16/75	0300	458	575.810		
9/16/75	0330	458	575.814		
9/16/75	0400	458	575.809		
9/16/75	0430	458	574.985		
9/16/75	0500	458	574.986		
9/16/75	0530	458	574.972		
9/16/75	0600	458	574.956		
9/16/75	0630	458	574.932		
9/16/75	0700	458	574.906		
9/16/75	0730	458	574.890		
9/16/75	0800	453	574.861	.427	
9/16/75	0830	453	574.830		
9/16/75	0900	453	574.822		
9/16/75	0930	453	574.792		
9/16/75	1000	453	574.779		
9/16/75	1030	453	574.757	.368	
9/16/75	1100	453	574.747		
9/16/75	1130	453	574.734		
9/16/75	1200	453	574.737	.373	
9/16/75	1230	453	574.728		
9/16/75	1300	453	574.733	.449	
9/16/75	1330	453	574.733		
9/16/75	1400	453	574.732		
9/16/75	1430	453	574.746		
9/16/75	1500	453	574.751	.487	
9/16/75	1530	453	574.745		
9/16/75	1600	453	574.747	.492	
9/16/75	1630	453	574.752		
9/16/75	1700	447	574.759	149.465	
9/16/75	1730	447	574.754		
9/16/75	1800	447	574.732		
9/16/75	1830	447	574.730	.422	
9/16/75	1900	447	574.716		
9/16/75	1930	447	574.698		
9/16/75	2000	447	574.687		
9/16/75	2030	437	574.661	.314	
9/16/75	2100	437	574.642		
9/16/75	2130	437	574.628		
9/16/75	2200	442	574.614		
9/16/75	2230	442	574.602	.211	
9/16/75	2300	442	574.588		
9/16/75	2330	442	574.575	.146	
9/17/75	0000	442	574.562		
9/17/75	0030	442	574.577		
9/17/75	0100	442	574.580		
9/17/75	0130	442	574.587		
9/17/75	0200	442	574.584		
9/17/75	0230	442	574.587		
9/17/75	0300	442	574.590		
9/17/75	0330	442	574.588		
9/17/75	0400	442	574.591		
9/17/75	0430	442	574.594		
9/17/75	0500	442	574.588		
9/17/75	0530	442	574.584		
9/17/75	0600	442	574.562		
9/17/75	0630	442	574.559	.033	
9/17/75	0700	442	574.542		
9/17/75	0730	442	574.523		
9/17/75	0800	442	574.505	.849	

RRGE 1 INTERFERENCE TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS	DATE / /	TIME / /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
9/17/75	0830	442	574.472			9/17/75	2130	437	574.319		
9/17/75	0900	442	574.455			9/17/75	2140	437	574.318		
9/17/75	0930	437	574.429	.811		9/17/75	2150	437	574.322	148.941	
9/17/75	1000	437	574.399			9/17/75	2200	437	574.315		
9/17/75	1030	437	574.383			9/17/75	2210	437	574.308		
9/17/75	1100	437	574.360			9/17/75	2220	437	574.303		
9/17/75	1130	437	574.356			9/17/75	2230	437	574.295		
9/17/75	1200	437	574.351	148.979		9/17/75	2240	437	574.291		
9/17/75	1230	437	574.347			9/17/75	2250	437	574.287		
9/17/75	1300	437	574.344			9/17/75	2300	437	574.285	148.795	
9/17/75	1330	437	574.			9/17/75	2330	437	574.280		
9/17/75	1400	437	574.196	149.84		9/18/75	0000	437	574.284		
9/17/75	1430	437	574.363			9/18/75	0030	437	574.289		
9/17/75	1500	437	574.374			9/18/75	0100	437	574.305		
9/17/75	1530	437	574.384	.109		9/18/75	0130	437	574.318		
9/17/75	1600	437	574.393			9/18/75	0200	437	574.339		
9/17/75	1630	437	574.408	.114		9/18/75	0230	437	574.360		
9/17/75	1700	437	574.409	.109		9/18/75	0300	437	574.379		
9/17/75	1730	437	574.391	.098		9/18/75	0330	437	574.402		
9/17/75	1800	437	574.392	.082		9/18/75	0400	437	574.420		
	1800	437	.392	.082RRGE 2 SHUT IN. 20 SEC SHUT IN TIME.		9/18/75	0430	437	574.428		
9/17/75	1801	437	574.390			9/18/75	0500	437	574.435		
9/17/75	1802	437	574.391			9/18/75	0530	437	574.450		
9/17/75	1803	437	574.390			9/18/75	0600	437	574.447		
						9/18/75	0630	437	574.447		
9/17/75	1804	437	574.389			9/18/75	0700	437	574.441		
9/17/75	1805	437	574.388			9/18/75	0730	437	574.429		
9/17/75	1806	437	574.389			9/18/75	0800	437	574.418		
9/17/75	1807	437	574.386			9/18/75	0830	437	574.399		
9/17/75	1808	437	574.384			9/18/75	0900	437	574.391		
9/17/75	1809	437	574.385			9/18/75	0930	437	574.377	.995	
9/17/75	1810	437	574.385	149.076		9/18/75	1000	437	574.366	.930	
9/17/75	1811	437	574.388			9/18/75	1030	437	574.357	.963	
9/17/75	1812	437	574.388			9/18/75	1100	437	574.336	.963	
9/17/75	1813	437	574.388			9/18/75	1130	437	574.323	.968	
9/17/75	1814	437	574.387			9/18/75	1200	437	574.319	.984	
9/17/75	1815	437	574.386			9/18/75	1230	437	574.325	.979	
9/17/75	1816	437	574.385			9/18/75	1300	437	574.347		
9/17/75	1817	437	574.384			9/18/75	1330	437	574.356		
9/17/75	1818	437	574.380			9/18/75	1400	437	574.372		
9/17/75	1819	437	574.381			9/18/75	1430	437	574.379		
9/17/75	1820	437	574.381			9/18/75	1500	437	574.386	149.898	
9/17/75	1825	437	574.380			9/18/75	1530	437	574.448	.141	
9/17/75	1830	437	574.381						.448		FIRST DATA POINT AFTER HP GAGE WAS TURNED ON AFTER
9/17/75	1835	437	574.379	.055							
9/17/75	1840	437	574.384			9/18/75	1600	437	574.451		
9/17/75	1845	437	574.380			9/18/75	1630	437	574.480		
9/17/75	1850	437	574.376			9/18/75	1700	437	574.487		
9/17/75	1855	437	574.370			9/18/75	1730	437	574.499	.173	
9/17/75	1900	437	574.373								
9/17/75	1905	437	574.365			9/18/75	1800	437	574.509	.190	
9/17/75	1910	437	574.364			9/18/75	1830	437	574.517		
9/17/75	1915	437	574.367			9/18/75	1900	437	574.509		
9/17/75	1920	437	574.359			9/18/75	1930	437	574.510		
9/17/75	1925	437	574.362			9/18/75	2000	437	574.500		
9/17/75	1930	437	574.361			9/18/75	2030	437	574.483		
9/17/75	1935	437	574.363			9/18/75	2100	437	574.486	.071	
9/17/75	1940	437	574.359			9/18/75	2130	437	574.478	.033	
9/17/75	1945	437	574.360			9/18/75	2200	437	574.453	.038	
9/17/75	1950	437	574.354			9/18/75	2230	437	574.455	.076	
9/17/75	1955	437	574.351			9/18/75	2300	437	574.445		
9/17/75	2000	437	574.351			9/18/75	2330	437	574.445		
9/17/75	2010	437	574.347			9/19/75	0000	437	574.435	.849	
9/17/75	2020	437	574.345			9/19/75	0030	437	574.444		
9/17/75	2030	437	574.342			9/19/75	0100	437	574.462		
9/17/75	2040	437	574.329			9/19/75	0130	437	574.472		
9/17/75	2050	437	574.332			9/19/75	0200	437	574.489		
9/17/75	2100	437	574.329			9/19/75	0230	437	574.508		
9/17/75	2110	437	574.334			9/19/75	0300	437	574.517		
9/17/75	2120	437	574.323			9/19/75	0330	437	574.549		

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS	DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
9/19/75	0400	437	574.572			9/21/75	1800	432	574.141		RRGE 1. SET AT
9/19/75	0430	437	574.586			9/21/75	1830	432	574.124		1800 FT.
9/19/75	0500	437	574.598			9/21/75	1900	432	574.114	149.541	
9/19/75	0530	437	574.625			9/21/75	1930	374	574.099		
9/19/75	0600	437	574.634								
9/19/75	0630	437	574.641			9/21/75	2000	374	574.079		
9/19/75	0700	437	574.590			9/21/75	2030	374	574.062	.444	
9/19/75	0730	437	574.610			9/21/75	2100	374	574.039	.449	
9/19/75	0800	437	574.606	149.249		9/21/75	2130	374	574.003		
9/19/75	0830	437	574.611			9/21/75	2200	374	573.958		
9/19/75	0900	437	574.686			9/21/75	2230	374	573.918		
9/19/75	0930	437	574.585	.244		9/21/75	2300	374	573.883	.309	
9/19/75	1000	437	574.568			9/21/75	2330	374	573.848		
9/19/75	1030	437	574.562			9/22/75	0800	421	573.820	.389	
9/19/75	1100	437	574.552			9/22/75	0830	421	573.790		
9/19/75	1130	437	574.519	.288		9/22/75	0180	421	573.768		
9/19/75	1200	437	574.534	.222		9/22/75	0130	421	573.749		
9/19/75	1230	437	574.538	.265		9/22/75	0200	421	573.739		
9/19/75	1300	437	574.532	.276		9/22/75	0230	421	573.735		
9/19/75	1320	437	574.			9/22/75	0300	421	573.736		
1320					AT 1320 HRS COMMENCED LOWERING PROBE FROM 1800 TO 3700 FT IN RRGE 1. ELEV,FT TEMP,DEG F 1000 197.5	9/22/75	0330	421	573.741		
						9/22/75	0400	421	573.750		
						9/22/75	0430	421	573.760		
						9/22/75	0500	409	573.768	.260	
						9/22/75	0530	409	573.776		
						9/22/75	0600	409	573.787		
						9/22/75	0630	409	573.793		
						9/22/75	0700	409	573.801		
						9/22/75	0730	409	573.804		
						9/22/75	0800	409	573.795	.260	
						9/22/75	0830	409	573.790		
						9/22/75	0900	409	573.781		
						9/22/75	0930	409	573.769		
						9/22/75	1000	409	573.744		
						9/22/75	1030	409	573.721	.184	
						9/22/75	1100	421	573.781		
						9/22/75	1130	421	573.675		
						9/22/75	1200	421	573.651		
						9/22/75	1230	421	573.633		
9/20/75					LEAKAGE OF WATER IN PROBE SUSPECTED. 2230 TO 0100 HRS. PRESS. AND TEMP. GAGE PULLED OUT OF RRGE 1. 1030 TO 1150	9/22/75	1300	421	573.619	.195	
						9/22/75	1330	421	573.599		
						9/22/75	1400	421	573.605		
						9/22/75	1430	421	573.599		
						9/22/75	1500	421	573.602	.205	
						9/22/75	1530	421	573.606		
						9/22/75	1600	421	573.		
						9/22/75	1630	421	573.624		
						9/22/75	1700	409	573.625	.184	
						9/22/75	1740	409	573.645		
9/20/75	1800	437	573.783	.788		9/22/75	1800	409	573.639	.173	
9/20/75	1830	437	573.773								
9/20/75	1900	437	573.762	.788		9/22/75	1840	409	573.648		
9/20/75	1930	437	573.780			9/22/75	1900	409	573.654	.163	
9/20/75	1930		.780			9/22/75	1930	409	573.661		
9/20/75	2000		.810		MP GAGE CORRECTED FOR SLIGHT LEAKAGE AT STRIPPER.	9/22/75	2010	409	573.646	.114	
						9/22/75	2040	409	573.636		
9/20/75	2000	437	573.810			9/22/75	2110	409	573.622		
9/20/75	2030	437	573.880	.741		9/22/75	2140	409	573.599		
9/20/75	2100	437	573.880	.735		9/22/75	2210	409	573.582	148.925	
9/20/75	2130	437	573.864	.735		9/22/75	2240	409	573.593		
9/20/75	2200	437	573.859			9/22/75	2310	409	573.530		
9/20/75	2230	437	573.838			9/22/75	2340	386	573.583		
9/20/75	2230		.838		PRODUCTION STARTED AT RRGE 2. FLOW RATE 432 GPM	9/23/75	0810	386	573.489		
9/20/75	2300	437	573.779			9/23/75	0840	386	573.464		
9/20/75	2330	437	573.726	.735		9/23/75	0110	386	573.453		
						9/23/75	0140	386	573.449		
9/20/75	2350	432	573.			9/23/75	0210	386	573.447		
9/21/75					MP SIGNAL WENT DEAD. 0800 TO 1700 HRS. THE MP GAGE WAS PULLED OUT, CLEANED, TESTED AND RELOWERED INTO	9/23/75	0240	386	573.439		
						9/23/75	0310	386	573.447		
						9/23/75	0340	386	573.437		
						9/23/75	0410	386	573.445		

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

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9/23/75	0440	386	573.456			9/25/75	1150	398	573.796		
9/23/75	0510	386	573.476			9/25/75	1220	398	573.774		
9/23/75	0540	386	573.487			9/25/75	1250	386	573.771		.358
9/23/75	0610	386	573.498		.849	9/25/75	1320	386	573.751		
9/23/75	0640	386	573.505			9/25/75	1350	386	573.742		.341
9/23/75	0710	386	573.499			9/25/75	1420	386	573.732		
9/23/75	0740	386	573.513			9/25/75	1450	386	573.723		.352
9/23/75	0810	386	573.522		.871	9/25/75	1520	404	573.715		
9/23/75	0840	386	573.517			9/25/75	1550	404	573.711		.352
9/23/75	0910	386	573.486			9/25/75	1620	404	573.705		
9/23/75	0940	386	573.474			9/25/75	1650	404	573.711		
9/23/75	1010	386	573.430		.865	9/25/75	1720	398	573.705		.341
9/23/75	1040	386	573.435			9/25/75	1750	398	573.713		
9/23/75	1110	386	573.426			9/25/75	1820	398	573.716		
9/23/75	1140	386	573.			9/25/75	1850	398	573.725		.320
9/23/75	1210	386	573.388			9/25/75	1920	398	573.721		
9/23/75	1240	386	573.382		.855	9/25/75	1950	386	573.723		.293
9/23/75	1310	386	573.375			9/25/75	2020	386	573.724		.277
9/23/75	1340	386	573.345			9/25/75	2050	386	573.715		
9/23/75	1410	421	573.335		.876	9/25/75	2120	386	573.712		
9/23/75	1440	421	573.337			9/25/75	2150	386	573.710		.228
9/23/75	1510	421	573.336		.855	9/25/75	2220	404	573.698		
9/23/75	1540	421	573.334			9/25/75	2250	404	573.685		.163
9/23/75	1610	409	573.344		.865	9/25/75	2320	404	573.672		
9/23/75	1730	386	573.355		.860	9/25/75	2350	404	573.650		
9/23/75	1900	386	573.372		.860	9/26/75	0020	404	573.629		.125
9/23/75	1930	386	573.385		.844	9/26/75	0050	404	573.615		
9/23/75	2030	386	573.385			9/26/75	0120	404	573.589		
9/23/75	2220	380	573.351		.730	9/26/75	0150	404	573.579		
9/23/75	2243	380	573.308		.703	9/26/75	0220	404	573.567		148.061
	2243		.308		.703HP GAGE FAILED, PULLED OUT OF WELL FOR CHECKING AND REPAIR.	9/26/75	0250	404	573.558		
9/24/75	1400	409	574.514		.671	9/26/75	0320	404	573.544		
9/24/75	1400	409	574.514		.671HP GAGE LOWERED INTO RRGE	9/26/75	0350	404	573.539		
						9/26/75	0420	398	573.543		.012
						9/26/75	0450	398	573.531		
					1 AND SET AT 1000 FT.	9/26/75	0520	398	573.533		147.990
9/24/75	1430	409	574.043			9/26/75	0550	398	573.537		
9/24/75	1500	409	574.013			9/26/75	0620	398	573.544		
9/24/75	1530	409	574.003			9/26/75	0650	398	573.548		
9/24/75	1600	409	574.017			9/26/75	0720	398	573.570		
9/24/75	1630	409	573.990			9/26/75	0750	398	573.577		148.033
9/24/75	1700	409	573.993		.666	9/26/75	0820	398	573.587		.05
9/24/75	1750	404	574.011			9/26/75	0850	398	573.583		
9/24/75	1820	404	573.995			9/26/75	0920	398	573.588		.055
9/24/75	1900	404	573.999			9/26/75	0950	398	573.587		
9/24/75	1930	404	573.995		148.606	9/26/75	1020	398	573.585		
9/24/75	2000	404	574.002			9/26/75	1050	398	573.581		.066
9/24/75	2030	404	574.017			9/26/75	1120	398	573.576		
9/24/75	2100	404	574.048			9/26/75	1150	398	573.564		
9/24/75	2130	404	574.036			9/26/75	1220	404	573.559		.088
9/24/75	2200	404	574.073		.666	9/26/75	1250	404	573.553		
9/24/75	2230	404	574.175			9/26/75	1320	404	573.550		.077
9/24/75	2320	404	574.112			9/26/75	1350	404	573.532		
9/25/75	0020	404	573.975		.466	9/26/75	1420	404	573.513		.077
9/25/75	0120	404	573.933			9/26/75	1450	404	573.509		
9/25/75	0220	404	573.877			9/26/75	1520	404	573.498		.066
9/25/75	0320	404	573.845			9/26/75	1607	404	573.497		
9/25/75	0350	404	573.833			9/26/75	1620	404	573.492		.071
9/25/75	0420	404	573.857		.358	9/26/75	1650	404	573.492		
9/25/75	0520	404	573.841			9/26/75	1720	404	573.489		.061
9/25/75	0620	404	573.831		.347	9/26/75	1750	404	573.493		
9/25/75	0720	404	573.855			9/26/75	1820	404	573.489		.050
9/25/75	0750	404	573.857			9/26/75	1850	404	573.492		
9/25/75	0820	398	573.854		.368	9/26/75	1920	404	573.495		.028
9/25/75	0850	398	573.849			9/26/75	1950	404	573.497		
9/25/75	0920	398	573.846			9/26/75	2020	398	573.496		.017
9/25/75	0950	398	573.840			9/26/75	2050	398	573.500		
9/25/75	1020	398	573.831			9/26/75	2120	398	573.500		147.969
9/25/75	1050	398	573.822		.385	9/26/75	2150	409	573.495		
9/25/75	1120	398	573.806			9/26/75	2220	409	573.480		.942

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

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9/26/75	2250	409	573.470			9/28/75	1130	404	572.584	.753	
9/26/75	2300	409	573.471			9/28/75	1200	404	572.579		
9/26/75	2350	409	573.			9/28/75	1230	404	572.598		
9/27/75	0020	409	573.456	.915		9/28/75	1300	404	572.596		
9/27/75	0050	409	573.442			9/28/75	1330	404	572.591	147.601	
9/27/75	0120	409	573.421			9/28/75	1400	404	572.582		
9/27/75	0150	409	573.			9/28/75	1430	404	572.582		
9/27/75	0220	409	573.403			9/28/75	1500	404	572.577	.817	
9/27/75	0250	409	573.387			9/28/75	1530	404	572.567		
9/27/75	0320	409	573.	.834		9/28/75	1600	404	572.564		
9/27/75	0350	409	573.368			9/28/75	1630	404	572.553		
9/27/75	0420	409	573.368			9/28/75	1700	404	572.539		
9/27/75	0450	409	573.371			9/28/75	1730	404	572.531	.788	
9/27/75	0520	409	573.378	147.839		9/28/75	1800	404	572.529		
9/27/75	0550	409	573.400			9/28/75	1830	404	572.519		
9/27/75	0750	404	573.489	.909		9/28/75	1900	404	572.511		
9/27/75	0750	404	.409	.909	HP GAGE MALFUNCTION. REMOVED FROM WELL. INSTALLED NEW CROSSOVER FROM CABLE AND NEW	9/28/75	1930	404	572.509	.731	
					CONNECTION. HP GAGE RE- LOWEED AND SET AT 1000FT	9/28/75	2000	404	572.510		
9/27/75	1400	404	576.482	.942		9/28/75	2030	404	572.516		
9/27/75	1400	404	.482	.942	THE HP GAGE READINGS IN COLUMN 4 ARE THE CORRECT	9/28/75	2100	404	572.510		
					ED VALUES FOR THE TIME PERIOD 9/27/75 1400 HRS. TO 10/3/75 0950 HRS.	9/28/75	2130	404	572.510	.650	
9/27/75	1430	404	572.792			9/28/75	2200	404	572.514		
9/27/75	1500	404	572.746	.936		9/28/75	2230	404	572.508		
9/27/75	1530	404	572.735			9/28/75	2300	404	572.509	.612	
9/27/75	1600	404	572.722			9/28/75	2330	404	572.506		
9/27/75	1630	404	572.716			9/29/75	0000	404	572.505		
9/27/75	1700	404	572.708			9/29/75	0030	404	572.502		
9/27/75	1730	404	572.704	.690		9/29/75	0100	404	572.501	.596	
9/27/75	1800	404	572.693			9/29/75	0130	404	572.498		
9/27/75	1830	404	572.696			9/29/75	0200	404	572.484		
9/27/75	1900	404	572.691			9/29/75	0230	404	572.482		
9/27/75	1930	404	572.687	.861		9/29/75	0300	404	572.470		
9/27/75	2000	404	572.683			9/29/75	0330	404	572.457	.520	
9/27/75	2030	404	572.696			9/29/75	0400	404	572.442		
9/27/75	2100	404	572.780			9/29/75	0430	404	572.427		
9/27/75	2130	404	572.695			9/29/75	0500	404	572.419		
9/27/75	2200	404	572.699	.780		9/29/75	0530	398	572.482	.493	
9/27/75	2230	404	572.686			9/29/75	0600	398	572.390		
9/27/75	2300	404	572.667			9/29/75	0630	398	572.379		
9/27/75	2330	404	572.667			9/29/75	0700	398	572.370		
9/28/75	0000	404	572.692			9/29/75	0730	398	572.357		
9/28/75	0030	404	572.705	.769		9/29/75	0800	398	572.347	.420	
9/28/75	0100	404	572.712			9/29/75	0830	398	572.343		
9/28/75	0130	404	572.728			9/29/75	0900	398	572.346		
9/28/75	0200	404	572.707			9/29/75	0930	398	572.337		
9/28/75	0230	404	572.689			9/29/75	0950	398	572.342		
9/28/75	0300	404	572.735	.655		9/29/75	1020	398	572.342	.439	
9/28/75	0330	404	572.793			9/29/75	1050	398	572.350		
9/28/75	0400	404	572.706			9/29/75	1120	398	572.354	.472	
9/28/75	0430	404	572.679			9/29/75	1150	398	572.358		
9/28/75	0500	404	572.667	.758		9/29/75	1220	398	572.367	.509	
9/28/75	0530	404	572.649			9/29/75	1250	398	572.378		
9/28/75	0600	404	572.639			9/29/75	1320	398	572.386	.558	
9/28/75	0630	404	572.793			9/29/75	1350	398	572.394	.569	
9/28/75	0700	404	572.612			9/29/75	1420	404	572.396		
9/28/75	0730	404	572.622	.709		9/29/75	1450	404	572.398		
9/28/75	0800	404	572.592			9/29/75	1520	404	572.392	147.601	
9/28/75	0830	404	572.591			9/29/75	1550	404	572.389		
9/28/75	0830	404	572.595			9/29/75	1620	404	572.381		
9/28/75	0900	404	572.583	.784		9/29/75	1650	404	572.378	.580	
9/28/75	0930	404	572.588			9/29/75	1720	404	572.369		
9/28/75	1000	404	572.587			9/29/75	1750	404	572.361	.547	
9/28/75	1030	404	572.586			9/29/75	1820	404	572.362		
9/28/75	1100	404	572.584			9/29/75	1850	404	572.347		
						9/29/75	1920	404	572.337	.482	
						9/29/75	1950	404	572.337		
						9/29/75	2020	404	572.332	.450	
						9/29/75	2050	404	572.328		
						9/29/75	2120	404	572.326		
						9/29/75	2150	404	572.328		

RRGE 1 INTERFERENCE TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
9/29/75	2220	404	572.324	.305	
9/29/75	2250	404	572.320		
9/29/75	2320	404	572.331		
9/29/75	2350	404	572.331		
9/30/75	0020	404	572.335	.369	
9/30/75	0050	404	572.337		
9/30/75	0120	404	572.345		
9/30/75	0150	404	572.345		
9/30/75	0220	404	572.342	.347	
9/30/75	0250	404	572.337		
9/30/75	0320	404	572.340		
9/30/75	0350	404	572.325		
9/30/75	0420	404	572.316		
9/30/75	0450	404	572.306	.326	
9/30/75	0520	404	572.293		
9/30/75	0550	404	572.283		
9/30/75	0620	404	572.270	.304	
9/30/75	0650	398	572.247		
9/30/75	0720	398	572.237	.203	
9/30/75	0750	398	572.214		
9/30/75	0820	398	572.200		
9/30/75	0850	398	572.189		
9/30/75	0920	398	572.190		
9/30/75	0950	398	572.185	.180	
9/30/75	1020	398	572.184		
9/30/75	1050	404	572.184	.239	
9/30/75	1120	404	572.189		
9/30/75	1150	404	572.191	.208	
9/30/75	1220	404	572.211	.326	
9/30/75	1250	404	572.211	.353	
9/30/75	1320	404	572.220	.380	
9/30/75	1350	404	572.231	.445	
9/30/75	1420	404	572.226	.439	
9/30/75	1450	404	572.240	.423	
9/30/75	1520	404	572.244	.407	
9/30/75	1550	404	572.248	.385	
9/30/75	1620	404	572.253	.364	
9/30/75	1650	404	572.243	.347	
9/30/75	1720	404	572.235	.320	
9/30/75	1750	404	572.228		
9/30/75	1820	404	572.216		
9/30/75	1850	404	572.215		
9/30/75	1920	404	572.194		
9/30/75	1950	404	572.185	147.299	
9/30/75	2020	404	572.178	.277	
9/30/75	2050	404	572.163	.261	
9/30/75	2120	409	572.154	.239	
9/30/75	2150	409	572.137	.223	
9/30/75	2220	409	572.149	.212	
9/30/75	2250	409	572.150	.196	
9/30/75	2320	409	572.157		
9/30/75	2350	409	572.157	.180	
10/01/75	0050	409	572.176	.207	
10/01/75	0120	409	572.186	.202	
10/01/75	0150	409	572.191	.218	
10/01/75	0220	409	572.202	.229	
10/01/75	0250	409	572.195	.234	
10/01/75	0320	409	572.216	.234	
10/01/75	0350	409	572.203	.229	
10/01/75	0420	409	572.202	.223	
10/01/75	0450	409	572.205	.212	
10/01/75	0520	409	572.184	.202	
10/01/75	0550	409	572.166	.180	
10/01/75	0620	409	572.154	.164	
10/01/75	0650	409	572.130	.142	
10/01/75	0720	409	572.108	.120	
10/01/75	0750	409	572.098	.099	
10/01/75	0820	409	572.061	.077	
10/01/75	0850	409	572.050	.072	
10/01/75	0920	409	572.041	.066	

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/01/75	0950	409	572.031	.066	
10/01/75	1020	409	572.016	.083	
10/01/75	1050	409	572.020	.099	
10/01/75	1120	409	572.028	.126	
10/01/75	1150	409	572.022	.158	
10/01/75	1220	409	572.034	.180	
10/01/75	1250	409	572.039	.212	
10/01/75	1320	409	572.053	.234	
10/01/75	1350	409	572.075	.266	
10/01/75	1420	409	572.084	.293	
10/01/75	1450	409	572.091	.326	
10/01/75	1520	409	572.099	.342	
10/01/75	1550	409	572.106	.358	
10/01/75	1620	409	572.103	.358	
10/01/75	1650	409	572.106	.347	
10/01/75	1720	409	572.104	.331	
10/01/75	1750	409	572.090	.315	
10/01/75	1820	409	572.093	.283	
10/01/75	1850	415	572.070	.250	
10/01/75	1920	415	572.041	.218	
10/01/75	1950	415	572.046	.185	
10/01/75	2020	415	572.040	.153	
10/01/75	2050	415	572.023	.120	
10/01/75	2120	415	571.997	147.099	
10/01/75	2150	415	571.991	.072	
10/01/75	2220	409	571.992	.050	
10/01/75	2250	409	571.995	.029	
10/01/75	2320	409	571.999	.012	
10/01/75	2350	409	571.984	.007	
10/02/75	0020	409	572.001	.007	
10/02/75	0050	409	572.018	.023	
10/02/75	0120	409	572.026	.039	
10/02/75	0150	409	572.048	.039	
10/02/75	0220	409	572.034	.061	
10/02/75	0250	409	572.065	.072	
10/02/75	0320	409	572.067	.077	
10/02/75	0350	409	572.075	.088	
10/02/75	0420	409	572.076	.088	
10/02/75	0450	409	572.086	.093	
10/02/75	0520	409	572.081	.077	
10/02/75	0550	409	572.068	.061	
10/02/75	0620	409	572.049	.045	
10/02/75	0650	409	572.044	.034	
10/02/75	0720	409	572.019	.002	
10/02/75	0750	409	572.000	146.996	
10/02/75	0820	409	571.977	.964	
10/02/75	0850	409	571.932	.948	
10/02/75	0920	409	571.931	.937	
10/02/75	0950	409	571.923	.926	
10/02/75	1020	409	571.896	.926	
10/02/75	1050	409	571.903	.937	
10/02/75	1120	409	571.884	.953	
10/02/75	1150	409	571.869	.969	
10/02/75	1220	409	571.890	.996	
10/02/75	1250	409	571.899	147.018	
10/02/75	1320	409	571.913	.045	
10/02/75	1350	409	571.915	.061	
10/02/75	1420	409	571.937	.088	
10/02/75	1450	409	571.946	.115	
10/02/75	1520	409	571.956	.137	
10/02/75	1550	409	571.982	.142	
10/02/75	1620	409	571.982	.142	
10/02/75	1650	409	572.005	.137	
10/02/75	1720	409	571.989	.126	
10/02/75	1750	409	571.984	.110	
10/02/75	1820	409	571.991	.088	
10/02/75	1850	409	571.989	.061	
10/02/75	1920	409	571.952	.029	
10/02/75	1950	409	571.940	146.991	
10/02/75	2020	409	571.920	.964	

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/02/75	2050	409	571.903	.931	
10/02/75	2120	409	571.872	.899	
10/02/75	2150	409	571.864	.877	
10/02/75	2220	404	571.829	.850	
10/02/75	2250	404	571.835	.834	
10/02/75	2320	404	571.840	.823	
10/02/75	2350	404	571.820	.818	
10/03/75	0020	404	571.839	146.818	
10/03/75	0050	404	571.840	.834	
10/03/75	0120	404	571.855	.840	
10/03/75	0150	404	571.862	.856	
10/03/75	0220	409	571.886	.872	
10/03/75	0250	409	571.904	.894	
10/03/75	0320	409	571.910	.910	
10/03/75	0350	409	571.928	.931	
10/03/75	0420	404	571.954	.942	
10/03/75	0450	404	571.947	.953	
10/03/75	0520	404	571.951	.964	
10/03/75	0550	404	571.954	.948	
10/03/75	0620	404	571.963	.942	
10/03/75	0650	404	571.923	.926	
10/03/75	0720	404	571.919	.915	
10/03/75	0750	404	571.918	.894	
10/03/75	0820	404	571.877	.867	
10/03/75	0850	404	571.863	.845	
10/03/75	0920	404	571.838	.	
10/03/75	0950	404	571.811	.807	
10/03/75	1020	404	571.790	.796	
10/03/75	1050	404	571.	.796	
10/03/75	1120	404	571.757	.796	
10/03/75	1150	404	571.762	.802	
10/03/75	1220	404	571.747	.813	
10/03/75	1250	404	571.763	.840	
10/03/75	1320	404	571.763	.867	
10/03/75	1350	404	571.801	.888	
10/03/75	1420	404	571.784	.918	
10/03/75	1450	404	571.812	.942	
10/03/75	1520	404	571.824	.958	
10/03/75	1550	404	571.834	.975	
10/03/75	1620	404	571.881	.985	
10/03/75	1650	404	571.874	.980	
10/03/75	1720	404	571.866	.	
10/03/75	1750	404	571.874	.964	
10/03/75	1820	404	571.864	.953	
10/03/75	1850	404	571.856	.926	
10/03/75	1920	404	571.845	.904	
10/03/75	1950	404	571.814	.877	
10/03/75	2020	404	571.802	.850	
10/03/75	2050	404	571.787	.823	
10/03/75	2120	398	571.768	.796	
10/03/75	2150	398	571.754	.	
10/03/75	2220	398	571.724	.742	
10/03/75	2250	398	571.700	.721	
10/03/75	2320	398	571.684	.699	
10/03/75	2350	404	571.686	.888	
10/04/75	0020	404	571.667	.683	
10/04/75	0050	404	571.672	.883	
10/04/75	0120	404	571.692	.688	
10/04/75	0150	404	571.707	.694	
10/04/75	0220	404	571.698	.715	
10/04/75	0250	404	571.723	.726	
10/04/75	0320	404	571.744	146.748	
10/04/75	0350	404	571.777	.764	
10/04/75	0420	404	571.808	.780	
10/04/75	0450	404	571.849	.796	
10/04/75	0520	404	571.818	.807	
10/04/75	0550	404	571.849	.818	
10/04/75	0620	404	571.846	.829	
10/04/75	0650	404	571.847	.823	
10/04/75	0720	404	571.812	.813	

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/04/75	0750	404	571.831	.796	
10/04/75	0820	409	571.808	.788	
10/04/75	0850	409	571.776	.	
10/04/75	0920	409	571.762	.736	
10/04/75	0950	409	571.732	.715	
10/04/75	1020	409	571.720	.784	
10/04/75	1050	409	571.687	.699	
10/04/75	1120	409	571.657	.699	
10/04/75	1150	409	571.646	.694	
10/04/75	1220	409	571.665	.784	
10/04/75	1250	409	571.653	.715	
10/04/75	1320	409	571.633	.721	
10/04/75	1350	409	571.646	.742	
10/04/75	1420	409	571.658	.764	
10/04/75	1450	409	571.673	.791	
10/04/75	1520	409	571.687	.818	
10/04/75	1550	409	571.714	.845	
10/04/75	1620	409	571.716	.861	
10/04/75	1650	409	571.740	.877	
10/04/75	1720	409	571.760	.883	
10/04/75	1750	409	571.739	.888	
10/04/75	1820	409	571.758	.877	
10/04/75	1850	409	571.770	.861	
10/04/75	1920	409	571.757	.834	
10/04/75	1950	409	571.738	.813	
10/04/75	2020	409	571.718	.780	
10/04/75	2050	409	571.706	.	
10/04/75	2120	409	571.683	.784	
10/04/75	2150	409	571.643	.667	
10/04/75	2220	409	571.643	.629	
10/04/75	2250	409	571.596	.596	
10/04/75	2320	409	571.594	.510	
10/04/75	2350	409	571.572	.542	
10/05/75	0020	409	571.561	.526	
10/05/75	0050	409	571.547	.521	
10/05/75	0120	409	571.558	.521	
10/05/75	0150	409	571.573	.526	
10/05/75	0220	409	571.564	.548	
10/05/75	0250	409	571.599	.564	
10/05/75	0320	409	571.615	.580	
10/05/75	0350	409	571.619	.602	
10/05/75	0420	409	571.657	.634	
10/05/75	0450	409	571.682	.658	
10/05/75	0520	409	571.676	.667	
10/05/75	0550	409	571.683	.683	
10/05/75	0620	404	571.738	146.677	
10/05/75	0650	404	571.706	.694	
10/05/75	0720	404	571.735	.688	
10/05/75	0750	404	571.715	.683	
10/05/75	0820	404	571.687	.667	
10/05/75	0850	404	571.786	.661	
10/05/75	0920	404	571.682	.645	
10/05/75	0950	404	571.654	.634	
10/05/75	1020	404	571.658	.618	
10/05/75	1050	404	571.684	.613	
10/05/75	1120	404	571.599	.618	
10/05/75	1150	404	571.586	.618	
10/05/75	1220	404	571.559	.613	
10/05/75	1250	404	571.558	.623	
10/05/75	1320	404	571.544	.623	
10/05/75	1350	404	571.539	.634	
10/05/75	1420	404	571.542	.639	
10/05/75	1450	404	571.553	.650	
10/05/75	1520	404	571.570	.667	
10/05/75	1550	404	571.596	.677	
10/05/75	1620	404	571.686	.683	
10/05/75	1650	404	571.689	.710	
10/05/75	1720	404	571.594	.715	
10/05/75	1750	404	571.624	.715	
10/05/75	1820	404	571.643	.715	

RRGE 1 INTERFERENCE TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS	DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/05/75	1850	404	571.667	.710		10/07/75	0550	404	571.351	.326	
10/05/75	1920	404	571.631	.699		10/07/75	0620	404	571.374	.337	
10/05/75	1950	404	571.648	.683		10/07/75	0650	404	571.401	.348	
10/05/75	2020	404	571.617	.656		10/07/75	0720	404	571.404	.364	
10/05/75	2050	404	571.618	.634		10/07/75	0750	404	571.396	.391	
10/05/75	2120	404	571.566	.596		10/07/75	0820	404	571.405	.391	
10/05/75	2150	404	571.531	.559		10/07/75	0850	404	571.465	.386	
10/05/75	2220	404	571.527	.521		10/07/75	0920	404	571.397	.380	
10/05/75	2250	404	571.502	.391		10/07/75	0950	404	571.434	.370	
10/05/75	2320	404	571.478	.456		10/07/75	1020	404	584.752	.321	
10/05/75	2350	404	571.466	.429		10/07/75	1050	404	584.	.451	
10/06/75	0020	404	571.436	.413					.752		.321 FROM 1020 HRS TO 1150 HRS ON 10/7/75. THE HP GAGE WAS LOWERED FROM 1800 FT TO 4500 FT.
10/06/75	0050	404	571.427	.391							
10/06/75	0120	404	571.405	.386							
10/06/75	0150	404	571.406	.380							
10/06/75	0220	404	571.424	.386		10/07/75	1120	404	584.	.424	
10/06/75	0250	404	571.417	.397		10/07/75	1150	404	2003.763	.418	
10/06/75	0320	404	571.439	.413		10/07/75	1220	404	2003.720	146.402	
10/06/75	0350	404	571.454	.429		10/07/75	1250	404	2003.697	.397	
10/06/75	0420	404	571.475	.445		10/07/75	1320	404	2003.667	.375	
10/06/75	0450	404	571.522	.461		10/07/75	1350	404	2003.660	.375	
10/06/75	0520	404	571.524	.488		10/07/75	1420	404	2003.651	.359	
10/06/75	0550	404	571.534	.499		10/07/75	1450	404	2003.649	.348	
10/06/75	0620	404	571.553	.521		10/07/75	1520	404	2003.648	.353	
10/06/75	0650	404	571.560	.537		10/07/75	1550	404	2003.654	.380	
10/06/75	0720	404	571.570	.532		10/07/75	1620	404	2003.655	.386	
10/06/75	0750	404	571.598	.542		10/07/75	1650	404	2003.656	.391	
10/06/75	0820	392	571.967	.532		10/07/75	1720	404	2003.659	.397	
10/06/75	0850	404	571.598	.521		10/07/75	1750	404	2003.668	.397	
10/06/75	0920	404	571.565	146.516		10/07/75	1820	404	2003.669	.397	
10/06/75	0950	404	571.562	.505		10/07/75	1850	404	2003.682	.402	
10/06/75	1020	404	571.526	.494		10/07/75	1920	404	2003.679	.429	
10/06/75	1050	404	571.516	.483		10/07/75	1950	404	2003.675	.424	
10/06/75	1120	404	571.483	.472		10/07/75	2020	404	2003.666	.	
10/06/75	1150	404	571.464	.456		10/07/75	2050	404	2003.653	.191	
10/06/75	1220	404	571.436	.456		10/07/75	2150	404	2003.601	.375	
10/06/75	1250	404	571.438	.456		10/07/75	2220	404	2003.601	.353	
10/06/75	1320	404	571.408	.456		10/07/75	2250	404	2003.582	.326	
10/06/75	1350	404	571.420	.456		10/07/75	2320	404	2003.549	.310	
10/06/75	1420	404	571.438	.450		10/07/75	2350	404	2003.530	.283	
10/06/75	1450	404	571.432	.456		10/08/75	0020	404	2003.496	.256	
10/06/75	1520	404	571.421	.461		10/08/75	0050	404	2003.484	.234	
10/06/75	1550	404	571.432	.466			0050		.484		.234 HP GAGE MALFUNCTION.
10/06/75	1620	404	571.464	.478		10/09/75	1830	404	571.316		
10/06/75	1650	404	571.489	.488		10/09/75	1830	404	571.316		HP GAGE REPAIRED.
10/06/75	1720	404	571.461	.505		10/09/75	1920	404	571.391		
10/06/75	1750	404	571.478	.510		10/09/75	2000	404	571.336		
10/06/75	1820	404	571.498	.510		10/09/75	2050	404	571.362		
10/06/75	1850	404	571.523	.510		10/09/75	2140	404	571.330		
10/06/75	1920	404	571.509	.510		10/09/75	2220	404	571.320		
10/06/75	1950	404	571.471	.591		10/09/75	2250	404	571.326		
10/06/75	2020	404	571.487	.478		10/09/75	2320	404	571.279		
10/06/75	2050	404	571.456	.461		10/10/75	0000	404	571.195	.261	
10/06/75	2120	404	571.454	.429		10/10/75	0100	404	571.161	.251	
10/06/75	2150	404	571.418	.402		10/10/75	0200	404	571.199	.224	
10/06/75	2220	404	571.394	.375		10/10/75	0300	404	571.190	.202	
10/06/75	2250	404	571.364	.348		10/10/75	0400	404	571.199	.175	
10/06/75	2320	404	571.354	.321		10/10/75	0600	404	571.170	.175	
10/06/75	2350	404	571.318	.288		10/10/75	0700	404	571.161	.186	
10/07/75	0020	404	571.317	.267		10/10/75	0800	404	571.165	.207	
10/07/75	0050	404	571.291	.251		10/10/75	0900	404	571.148	.218	
10/07/75	0120	404	571.250	.240		10/10/75	1000	404	571.	.218	
10/07/75	0150	404	571.261	.213			1000				.218 H.P. GAGE MALFUNCTION
10/07/75	0220	404	571.284	.213		10/10/75	1600	404	571.291	.278	
10/07/75	0250	404	571.280	.218		10/10/75	1700	404	571.290	.256	
10/07/75	0320	404	571.281	.213		10/10/75	1800	404	571.277	.240	
10/07/75	0350	404	571.287	.256		10/10/75	1900	404	571.241	.229	
10/07/75	0420	404	571.307	.267		10/10/75	2000	404	571.209	.218	
10/07/75	0450	404	571.327	.278		10/10/75	2100	404	571.217	.207	
10/07/75	0520	404	571.326	.288		10/10/75	2300	404	571.150	.175	

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/10/75	2310	404	570.985	.175	
10/11/75	0000	404	571.171	.153	
10/11/75	0100	404	571.147	.132	
10/11/75	0200	404	571.085	146.894	
10/11/75	0300	404	571.089	.067	
10/11/75	0400	404	571.043	.029	
10/11/75	0500	404	571.041	.008	
10/11/75	0620	404	571.039	.008	
10/11/75	0700	404	571.013	.002	
10/11/75	0800	404	571.040	.013	
10/11/75	0900	404	571.114	.010	
10/11/75	1000	404	571.065	.045	
10/11/75	1200	404	571.126	.056	
10/11/75	1330	404	571.125	.056	
10/11/75	1510	404	571.053	.061	
10/11/75	1530	404	571.108	.051	
10/11/75	1640	404	571.032	.051	
10/11/75	1710	404	571.069	.045	
10/11/75	1730			.040	
10/11/75	1800			.040	
10/11/75	1830				
10/11/75	1900			.040	
10/11/75	1930			.020	
10/11/75	2000			.030	
10/11/75	2030			.020	
10/11/75	2100			.020	
10/11/75	2130			.020	
10/11/75	2200			.010	
10/11/75	2230			.020	
10/11/75	2300			.000	
10/11/75	2330			.010	
10/12/75	0000			.000	
10/12/75	0030			.000	
10/12/75	0100			.000	
10/12/75	0130			145.990	
10/12/75	0200			.990	
10/12/75	0230			.960	
10/12/75	0300			.960	
10/12/75	0330			.940	
10/12/75	0400			.950	
10/12/75	0430			.930	
10/12/75	0500			.930	
10/12/75	0530			.920	
10/12/75	0600			.900	
10/12/75	0630			.900	
10/12/75	0700			.870	
10/12/75	0730			.890	
10/12/75	0800				
10/12/75	0830			.890	
10/12/75	0900			.890	
10/12/75	0930			.890	
10/12/75	1000			.890	
10/12/75	1030			.890	
10/12/75	1100			.910	
10/12/75	1130			.900	
10/12/75	1200			.920	
10/12/75	1230			.930	
10/12/75	1300			145.920	
10/12/75	1330			.940	
10/12/75	1400			.930	
10/12/75	1430			.930	
10/12/75	1500			.930	
10/12/75	1530			.940	
10/12/75	1600			.930	
10/12/75	1600			145.930	
10/12/75	1630			.920	
10/12/75	1700			.930	
10/12/75	1730			.920	
10/12/75	1800			.900	
10/12/75	1830			.920	

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/12/75	1900				.940
10/12/75	1930				
10/12/75	2000				.930
10/12/75	2030				.930
10/12/75	2100				.920
10/12/75	2130				.930
10/12/75	2200				.900
10/12/75	2230				.930
10/12/75	2300				.900
10/12/75	2330				.920
10/13/75	0000				.920
10/13/75	0030				.930
10/13/75	0100				.920
10/13/75	0130				.920
10/13/75	0200				.920
10/13/75	0230				.920
10/13/75	0300				.910
10/13/75	0330				.910
10/13/75	0400				.890
10/13/75	0430				.890
10/13/75	0500				.880
10/13/75	0530				.870
10/13/75	0600				.860
10/13/75	0630				.850
10/13/75	0700				.840
10/13/75	0730				.830
10/13/75	0800				.820
10/13/75	0830				.830
10/13/75	0900				.820
10/13/75	0930				.820
10/13/75	1000				.820
10/13/75	1030				.820
10/13/75	1100				.840
10/13/75	1130				
10/13/75	1200				.870
10/13/75	1230				.880
10/13/75	1300				.890
10/13/75	1330				145.820
10/13/75	1400				.880
10/13/75	1430				.810
10/13/75	1500				.800
10/13/75	1530				145.990
10/13/75	1600				.980
10/13/75	1630				.980
10/13/75	1700				.960
10/13/75	1730				.960
10/13/75	1800				.950
10/13/75	1830				.930
10/13/75	1900				145.930
10/13/75	1930				.900
10/13/75	2000				.900
10/13/75	2030				.890
10/13/75	2100				.880
10/13/75	2130				.880
10/13/75	2200				.870
10/13/75	2230				.870
10/13/75	2300				.860
10/13/75	2330				.870
10/14/75	0000				.870
10/14/75	0030				.880
10/14/75	0100				.880
10/14/75	0130				.880
10/14/75	0200				.890
10/14/75	0230				.710
10/14/75	0300				.690
10/14/75	0330				.690
10/14/75	0400				.690
10/14/75	0430				.690
10/14/75	0500				.670
10/14/75	0530				.670

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/14/75	0600			.860	
10/14/75	0630			.850	
10/14/75	0700			.840	
10/14/75	0730			.810	
10/14/75	0800			.810	
10/14/75	0830			.790	
10/14/75	0900			.790	
10/14/75	0930			.780	
10/14/75	1000			.790	
10/14/75	1030			.790	
10/14/75	1100			.790	
10/14/75	1130			.790	
10/14/75	1200			.800	
10/14/75	1230			.800	
10/14/75	1300			.800	
10/14/75	1330			.810	
10/14/75	1400			.830	
10/14/75	1430			.860	
10/14/75	1500			.880	
10/14/75	1530			.890	
10/14/75	1600			.890	
10/14/75	1630			.890	
10/14/75	1700			.880	
10/14/75	1730			.870	
10/14/75	1800			.850	
10/14/75	1830			.820	
10/14/75	1900			.800	
10/14/75	1930			.790	
10/14/75	2000			.770	
10/14/75	2030			.770	
10/14/75	2100			.760	
10/14/75	2130			.740	
10/14/75	2200		145.750	.750	
10/14/75	2230			.750	
10/14/75	2300			.740	
10/14/75	2330			.740	
10/15/75	0000			.750	
10/15/75	0030			.750	
10/15/75	0100			.760	
10/15/75	0130			.760	
10/15/75	0200			.780	
10/15/75	0230			.780	
10/15/75	0300			.790	
10/15/75	0330			.790	
10/15/75	0400			.790	
10/15/75	0430			.790	
10/15/75	0500			.790	
10/15/75	0530			.760	
10/15/75	0600			.760	
10/15/75	0630			.760	
10/15/75	0700			.740	
10/15/75	0730			.730	
10/15/75	0800			.710	
10/15/75	0830			.700	
10/15/75	0900			.680	
10/15/75	0930			.680	
10/15/75	1000			.680	
10/15/75	1030			.680	
10/15/75	1100			.680	
10/15/75	1130			.690	
10/15/75	1200			.710	
10/15/75	1230			.730	
10/15/75	1300			.730	
10/15/75	1330			.750	
10/15/75	1400			.750	
10/15/75	1430			.770	
10/15/75	1500			.770	
10/15/75	1530			.760	
10/15/75	1600			.760	
10/15/75	1630			.750	

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/15/75	1700			.740	
10/15/75	1730			.730	
10/15/75	1800			.710	
10/15/75	1830			.780	
10/15/75	1900			.680	
10/15/75	1930			.660	
10/15/75	2000			.650	
10/15/75	2030			.650	
10/15/75	2100			.630	
10/15/75	2130			.610	
10/15/75	2200			.610	
10/15/75	2230			.600	
10/15/75	2300			.600	
10/15/75	2330			.610	
10/16/75	0000			.610	
10/16/75	0030			.620	
10/16/75	0100			145.630	
10/16/75	0130			.640	
10/16/75	0200			.670	
10/16/75	0230			.660	
10/16/75	0300			.680	
10/16/75	0330			.680	
10/16/75	0400			.690	
10/16/75	0430			.690	
10/16/75	0500			.780	
10/16/75	0530			.690	
10/16/75	0600			.690	
10/16/75	0630			.680	
10/16/75	0700			.670	
10/16/75	0730			.670	
10/16/75	0800			.640	
10/16/75	0830			.620	
10/16/75	0900			.650	
10/16/75	0930			.600	
10/16/75	1000				
10/16/75	1030				
10/16/75	1100				
10/16/75	1130				
10/16/75	1200				
10/16/75	1230			.790	
10/16/75	1300			.820	
10/16/75	1330			.850	
10/16/75	1400			.880	
10/16/75	1430			.880RRGE 2 SHUT IN	
10/16/75	1500			.940	
10/16/75	1530			.950	
10/16/75	1600			.930	
10/16/75	1630			.980	
10/16/75	1700			.880	
10/16/75	1730			.870	
10/16/75	1800			.880	
10/16/75	1830			.860	
10/16/75	1900			.930	
10/16/75	1930			.980	
10/16/75	2000			.870	
10/16/75	2030			.850	
10/16/75	2100			.850	
10/16/75	2130			.820	
10/16/75	2200			.810	
10/16/75	2230			.810	
10/16/75	2300			.800	
10/16/75	2330			.780	
10/17/75	0000			.810	
10/17/75	0030			.880	
10/17/75	0100			.820	
10/17/75	0130			.840	
10/17/75	0200			.850	
10/17/75	0230			.880	
10/17/75	0300			.890	

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS	DATE / /	TIME /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/17/75	0330			.910		10/18/75	1430			.420	
10/17/75	0400			145.920		10/18/75	1500			.430	
10/17/75	0430			.940		10/18/75	1530			.460	
10/17/75	0500			.940		10/18/75	1600			.470	
10/17/75	0530			.950		10/18/75	1630			.470	
10/17/75	0600			.950		10/18/75	1700			.480	
10/17/75	0630			.950		10/18/75	1730			.480	
10/17/75	0700			.940		10/18/75	1800			.480	
10/17/75	0730			.940		10/18/75	1830			.480	
10/17/75	0800			.930		10/18/75	1900			.470	
10/17/75	0830			.920		10/18/75	1930			.460	
10/17/75	0900			.920		10/18/75	2000			.430	
10/17/75	0930			.920		10/18/75	2030			.410	
10/17/75	1000			.920		10/18/75	2100			.480	
10/17/75	1030			.920		10/18/75	2130			.370	
10/17/75	1100			.930		10/18/75	2200			.370	
10/17/75	1130			.930		10/18/75	2230			.360	
10/17/75	1200			.950		10/18/75	2300			.340	
10/17/75	1230			.960		10/18/75	2330			.350	
10/17/75	1300			.980		10/19/75	0000			.360	
10/17/75	1330			146.000		10/19/75	0030			.350	
10/17/75	1400			.040		10/19/75	0100			.380	
10/17/75	1430			.060		10/19/75	0130			.400	
10/17/75	1500			.080		10/19/75	0200			.410	
10/17/75	1530			.100		10/19/75	0230			.450	
10/17/75	1600			.120		10/19/75	0300			.460	
10/17/75	1630			.120		10/19/75	0330			.490	
10/17/75	1700			.130		10/19/75	0400			.510	
10/17/75	1730			.130		10/19/75	0430			.550	
10/17/75	1800			.130		10/19/75	0500			.570	
10/17/75	1830			.120		10/19/75	0530			.590	
10/17/75	1900			.100		10/19/75	0600			.610	
10/17/75	1930			.080		10/19/75	0630			.620	
10/17/75	2000			.040		10/19/75	0700			.630	
10/17/75	2030			.050		10/19/75	0730			.630	
10/17/75	2100			.020		10/19/75	0800			.630	
10/17/75	2130			.000		10/19/75	0830			.620	
10/17/75	2200			.010		10/19/75	0900			.620	
10/17/75	2230			.000		10/19/75	0930			.620	
10/17/75	2300			145.990		10/19/75	1000			146.620	
10/17/75	2330			146.000		10/19/75	1030			.620	
10/18/75	0000			.000		10/19/75	1100			.620	
10/18/75	0030			.010		10/19/75	1130			.640	
10/18/75	0100			.030		10/19/75	1200			.660	
10/18/75	0130			.050		10/19/75	1230			.680	
10/18/75	0200			.070		10/19/75	1300			.700	
10/18/75	0230			.090		10/19/75	1330			.770	
10/18/75	0300			.120		10/19/75	1400			.770	
10/18/75	0330			.150		10/19/75	1430			.800	
10/18/75	0400			.160		10/19/75	1500			.820	
10/18/75	0430			.200		10/19/75	1530			.830	
10/18/75	0500			.210		10/19/75	1600			.840	
10/18/75	0530			.230		10/19/75	1630			.850	
10/18/75	0600			.240		10/19/75	1700			.850	
10/18/75	0630			.260		10/19/75	1730			.850	
10/18/75	0700			146.250		10/19/75	1800			.850	
10/18/75	0730			.260		10/19/75	1830			.850	
10/18/75	0800			.250		10/19/75	1900			.830	
10/18/75	0830			.250		10/19/75	1930			.820	
10/18/75	0900			.230		10/19/75	2000			.800	
10/18/75	0930			.240		10/19/75	2030			.770	
10/18/75	1000			.240		10/19/75	2100			.680	
10/18/75	1030			.250		10/19/75	2130			.720	
10/18/75	1100			.250		10/19/75	2200			.760	
10/18/75	1130			.270		10/19/75	2230			.780	
10/18/75	1200			.270		10/19/75	2300			.690	
10/18/75	1230			.300		10/19/75	2330			.670	
10/18/75	1300			.330		10/20/75	0000			.680	
10/18/75	1330			.360		10/20/75	0030			.670	
10/18/75	1400			.390		10/20/75	0100			.680	

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/20/75	0130			.690	
10/20/75	0200			.710	
10/20/75	0230			.730	
10/20/75	0300			.760	
10/20/75	0330			.780	
10/20/75	0400			.810	
10/20/75	0430			.830	
10/20/75	0500			.870	
10/20/75	0530			.890	
10/20/75	0600			.910	
10/20/75	0630			.930	
10/20/75	0700			.940	
10/20/75	0730			.950	
10/20/75	0800			.950	
10/20/75	0830			.950	
10/20/75	0900			.950	
10/20/75	0930			.940	
10/20/75	1000			.940	
10/20/75	1030			.940	
10/20/75	1100				
10/20/75	1130			.960	
10/20/75	1200			.970	
10/20/75	1230			.970	
10/20/75	1300		146.	.970	
10/20/75	1330			.980	
10/20/75	1400			.990	
10/20/75	1430		147.	.000	
10/20/75	1500			.020	
10/20/75	1530			.040	
10/20/75	1600			.070	
10/20/75	1630			.080	
10/20/75	1700			.090	
10/20/75	1730			.100	
10/20/75	1800			.110	
10/20/75	1830			.110	
10/20/75	1900			.100	
10/20/75	1930			.090	
10/20/75	2000			.070	
10/20/75	2030			.040	
10/20/75	2100			.030	
10/20/75	2130			.010	
10/20/75	2200			.000	
10/20/75	2230		146.	.990	
10/20/75	2300			.990	
10/20/75	2330			.950	
10/21/75	0000			.950	
10/21/75	0030			.910	
10/21/75	0100			.940	
10/21/75	0130			.940	
10/21/75	0200			.960	
10/21/75	0230			.970	
10/21/75	0300		147.	.000	
10/21/75	0330			.010	
10/21/75	0400			.040	
10/21/75	0430			.060	
10/21/75	0500			.100	
10/21/75	0530			.060	
10/21/75	0600			.150	
10/21/75	0630			.170	
10/21/75	0700			.190	
10/21/75	0730			.200	
10/21/75	0800			.190	
10/21/75	0830				
10/21/75	0900				
10/21/75	0930				
10/21/75	1000			.200	
10/21/75	1030			.190	
10/21/75	1100			.170	
10/21/75	1130			.170	
10/21/75	1200			.170	

DATE /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/21/75	1230			.180	
10/21/75	1300			.190	
10/21/75	1330			.190	
10/21/75	1400			.210	
10/21/75	1430			.220	
10/21/75	1500			.240	
10/21/75	1530			.260	
10/21/75	1600			147.	.280
10/21/75	1630			.290	
10/21/75	1700			.310	
10/21/75	1730			.320	
10/21/75	1800			.330	
10/21/75	1830			.330	
10/21/75	1900			.340	
10/21/75	1930			.320	
10/21/75	2000			.310	
10/21/75	2030			.290	
10/21/75	2100			.270	
10/21/75	2130			.240	
10/21/75	2200			.220	
10/21/75	2230			.210	
10/21/75	2300			.190	
10/21/75	2330			.170	
10/22/75	0000			.170	
10/22/75	0030			.160	
10/22/75	0100			.160	
10/22/75	0130			.150	
10/22/75	0200			.150	
10/22/75	0230			.160	
10/22/75	0300			.170	
10/22/75	0330			.210	
10/22/75	0400			.230	
10/22/75	0430			.260	
10/22/75	0500			.280	
10/22/75	0530			.310	
10/22/75	0600			.330	
10/22/75	0630			.350	
10/22/75	0700			.370	
10/22/75	0730			.390	
10/22/75	0800			.390	
10/22/75	0830			.400	
10/22/75	0900			.400	
10/22/75	0930			.400	
10/22/75	1000			.420	
10/22/75	1030			.420	
10/22/75	1100			.410	
10/22/75	1130			.400	
10/22/75	1200			.390	
10/22/75	1230			.390	
10/22/75	1300			.380	
10/22/75	1330			.380	
10/22/75	1400			.390	
10/22/75	1430			.400	
10/22/75	1500			.420	
10/22/75	1530			.430	
10/22/75	1600			.450	
10/22/75	1630			.460	
10/22/75	1700			.480	
10/22/75	1730			.510	
10/22/75	1800			.530	
10/22/75	1830			.540	
10/22/75	1900			147.	.540
10/22/75	1930			.540	
10/22/75	2000			.540	
10/22/75	2030			.530	
10/22/75	2100			.540	
10/22/75	2130			.510	
10/22/75	2200			.500	
10/22/75	2230			.480	
10/22/75	2300			.470	

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE	TIME	FLCM RATE (GPH)	DOWNHOLE PRESSURE (PSIA)	WELL HEAD PRESSURE (PSIA)	REMARKS
10/22/75	2330		.450		
10/23/75	0000		.450		
10/23/75	0030		.440		
10/23/75	0100		.430		
10/23/75	0130		.430		
10/23/75	0200		.430		
10/23/75	0230		.430		
10/23/75	0300		.430		
10/23/75	0330		.450		
10/23/75	0400		.450		
10/23/75	0430		.480		
10/23/75	0500		.500		
10/23/75	0530		.530		
10/23/75	0600		.550		
10/23/75	0630		.560		
10/23/75	0700		.580		
10/23/75	0730		.600		
10/23/75	0800		.620		
10/23/75	0830		.620		
10/23/75	0900		.630		
10/23/75	0930		.640		
10/23/75	1000		.640		
10/23/75	1030		.640		
10/23/75	1100		.640		
10/23/75	1130		.640		
10/23/75	1200		.640		
10/23/75	1230		.640		
10/23/75	1300		.630		
10/23/75	1330				
10/23/75	1400		147.630		
10/23/75	1430		.630		
10/23/75	1500		.590		
10/23/75	1530		.640		
10/23/75	1600		.660		
10/23/75	1630		.660		
10/23/75	1700		.680		
10/23/75	1730		.690		
10/23/75	1800		.710		
10/23/75	1830		.720		
10/23/75	1900		.730		
10/23/75	1930		.740		
10/23/75	2000		.740		
10/23/75	2030		.750		
10/23/75	2100		.740		
10/23/75	2130				
10/23/75	2200		147.740		
10/23/75	2230		.720		
10/23/75	2300		.700		
10/23/75	2330		.690		
10/24/75	0000		.680		
10/24/75	0030		.660		
10/24/75	0100		.650		
10/24/75	0130		.640		
10/24/75	0200		.630		
10/24/75	0230		.630		
10/24/75	0300		.630		
10/24/75	0330		.640		
10/24/75	0400		.650		
10/24/75	0430		.670		
10/24/75	0500				
10/24/75	0530				
10/24/75	0600				
10/24/75	0630				
10/24/75	0700				
10/24/75	0730				
10/24/75	0800				
10/24/75	0830				
10/24/75	0900				
10/24/75	0930				
10/24/75	1000				

DATE	TIME	FLCM RATE (GPH)	DOWNHOLE PRESSURE (PSIA)	WELL HEAD PRESSURE (PSIA)	REMARKS
10/24/75	1030				
10/24/75	1100			.860	
10/24/75	1130			.870	
10/24/75	1200			.860	
10/24/75	1230			.880	
10/24/75	1300			.880	
10/24/75	1330			.880	
10/24/75	1400			.870	
10/24/75	1430			.870	
10/24/75	1500			.870	
10/24/75	1530			.870	
10/24/75	1600			.870	
10/24/75	1630			.870	
10/24/75	1700			.870	
10/24/75	1730			.880	
10/24/75	1800			.890	
10/24/75	1830			.920	
10/24/75	1900			.930	
10/24/75	1930			.940	
10/24/75	2000			.940	
10/24/75	2030			.950	
10/24/75	2100			.950	
10/24/75	2130			.950	
10/24/75	2200			.940	
10/24/75	2230			.940	
10/24/75	2300			.930	
10/24/75	2330			.910	
10/25/75	0000			.910	
10/25/75	0030			.880	
10/25/75	0100			147.870	
10/25/75	0130			.870	
10/25/75	0200			.850	
10/25/75	0230			.850	
10/25/75	0300			.840	
10/25/75	0330			.840	
10/25/75	0400			.850	
10/25/75	0430			.850	
10/25/75	0500			.860	
10/25/75	0530			.870	
10/25/75	0600			.880	
10/25/75	0630			.900	
10/25/75	0700			.910	
10/25/75	0730			.930	
10/25/75	0800			.940	
10/25/75	0830			.960	
10/25/75	0900			.970	
10/25/75	0930			.970	
10/25/75	1000			.980	
10/25/75	1030			148.000	
10/25/75	1100			.910	
10/25/75	1130			.910	
10/25/75	1200			.920	
10/25/75	1230			.910	
10/25/75	1300			.920	
10/25/75	1330			.910	
10/25/75	1400			.910	
10/25/75	1430			.920	
10/25/75	1500			.900	
10/25/75	1530			.910	
10/25/75	1600			.900	
10/25/75	1630			.910	
10/25/75	1700			.900	
10/25/75	1730			.920	
10/25/75	1800			.920	
10/25/75	1830			.940	
10/25/75	1900			.940	
10/25/75	1930			.950	
10/25/75	2000			.950	
10/25/75	2030			.970	
10/25/75	2100			.960	

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/25/75	2130			.880	
10/25/75	2200			.840	
10/25/75	2230				
10/25/75	2300		148.880		
10/25/75	2330			.870	
10/26/75	0000			.860	
10/26/75	0030			.823	
10/26/75	0100			.807	
10/26/75	0130			.801	
10/26/75	0200		147.985		
10/26/75	0230			.985	
10/26/75	0300			.969	
10/26/75	0330			.969	
10/26/75	0400		147.958		
10/26/75	0430			.963	
10/26/75	0500			.958	
10/26/75	0530			.963	
10/26/75	0600			.963	
10/26/75	0630			.970	
10/26/75	0700			.990	
10/26/75	0730			.996	
10/26/75	0800	148.007			
10/26/75	0830			.034	
10/26/75	0900			.044	
10/26/75	0930			.061	
10/26/75	1000			.071	
10/26/75	1030			.088	
10/26/75	1100			.098	
10/26/75	1130			.109	
10/26/75	1200			.115	
10/26/75	1230			.131	
10/26/75	1300			.136	
10/26/75	1330			.142	
10/26/75	1400			.147	
10/26/75	1430			.147	
10/26/75	1500			.142	
10/26/75	1530			.147	
10/26/75	1600			.142	
10/26/75	1630			.147	
10/26/75	1700			.142	
10/26/75	1730			.147	
10/26/75	1800			.152	
10/26/75	1830			.152	
10/26/75	1900			.159	
10/26/75	1930			.174	
10/26/75	2000			.174	
10/26/75	2030				
10/26/75	2100			.185	
10/26/75	2130				
10/26/75	2200			.201	
10/26/75	2230			.206	
10/26/75	2300			.201	
10/26/75	2330			.206	
10/27/75	0000			.201	
10/27/75	0030			.206	
10/27/75	0100			.201	
10/27/75	0130			.190	
10/27/75	0200			.185	
10/27/75	0230			.174	
10/27/75	0300			.169	
10/27/75	0330			.158	
10/27/75	0400			.158	
10/27/75	0430			.152	
10/27/75	0500				
10/27/75	0530			.147	
10/27/75	0600			.152	
10/27/75	0630			.147	
10/27/75	0700	148.163			
10/27/75	0730			.169	
10/27/75	0800			.179	

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/27/75	0830			.190	
10/27/75	0900			.206	
10/27/75	0930			.233	
10/27/75	1000			.239	
10/27/75	1030			.250	
10/27/75	1100			.277	
10/27/75	1130			.277	
10/27/75	1200			.287	
10/27/75	1230			.298	
10/27/75	1300			.320	
10/27/75	1330			.331	
10/27/75	1400			.325	
10/27/75	1430			.336	
10/27/75	1500			.336	
10/27/75	1530			.325	
10/27/75	1600			.331	
10/27/75	1630			.328	
10/27/75	1700			.336	
10/27/75	1730			.320	
10/27/75	1800			.325	
10/27/75	1830			.325	
10/27/75	1900			.325	
10/27/75	1930			.325	
10/27/75	2000			.336	
10/27/75	2030			.336	
10/27/75	2100			.347	
10/27/75	2130			.347	
10/27/75	2200			.363	
10/27/75	2230			.368	
10/27/75	2300			.374	
10/27/75	2330			.385	
10/28/75	0000				
10/28/75	0030			.401	
10/28/75	0100			.396	
10/28/75	0130			.401	
10/28/75	0200			.401	
10/28/75	0230			.396	
10/28/75	0300			.396	
10/28/75	0330			.385	
10/28/75	0400			.385	
10/28/75	0430			.388	
10/28/75	0500			.368	
10/28/75	0530			.363	
10/28/75	0600			.358	
10/28/75	0630			.358	
10/28/75	0700			.347	
10/28/75	0730			.347	
10/28/75	0800			.358	
10/28/75	0830			.358	
10/28/75	0900			.374	
10/28/75	0930			.385	
10/28/75	1000		148.406		
10/28/75	1030			.423	
10/28/75	1100			.444	
10/28/75	1130			.477	
10/28/75	1200			.504	
10/28/75	1230			.531	
10/28/75	1300			.547	
10/28/75	1330			.563	
10/28/75	1400			.568	
10/28/75	1430			.574	
10/28/75	1500			.585	
10/28/75	1530			.579	
10/28/75	1600			.579	
10/28/75	1630			.552	
10/28/75	1700			.536	
10/28/75	1730			.525	
10/28/75	1800			.509	
10/28/75	1830			.487	
10/28/75	1900			.477	

RRGE 1 INTERFERENCE TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/26/75	1930			.471	
10/26/75	2000			.482	
10/26/75	2030			.471	
10/26/75	2100			.482	
10/26/75	2130			.482	
10/28/75	2200			.493	
10/28/75	2230			.504	
10/28/75	2300			.504	
10/28/75	2330			.510	
10/29/75	0000			.525	
10/29/75	0030			.547	
10/29/75	0100			.547	
10/29/75	0130			.563	
10/29/75	0200			.563	
10/29/75	0230			.568	
10/29/75	0300			.574	
10/29/75	0330			.568	
10/29/75	0400			.568	
10/29/75	0430			.550	
10/29/75	0500			.552	
10/29/75	0530				
10/29/75	0600			.520	
10/29/75	0630			.520	
10/29/75	0700			.504	
10/29/75	0730			.504	
10/29/75	0800			.493	
10/29/75	0830			.493	
10/29/75	0900			.493	
10/29/75	0930			.504	
10/29/75	1000			.509	
10/29/75	1030			.531	
10/29/75	1100			.547	
10/29/75	1130			.563	
10/29/75	1200			.585	
10/29/75	1230			.606	
10/29/75	1300		146.633		
10/29/75	1330		.655		
10/29/75	1400		.671		
10/29/75	1430		.687		
10/29/75	1500		.682		
10/29/75	1530		.676		
10/29/75	1600		.671		
10/29/75	1630		.666		
10/29/75	1700		.620		
10/29/75	1730		.606		
10/29/75	1800		.585		
10/29/75	1830		.574		
10/29/75	1900		.579		
10/29/75	1930		.568		
10/29/75	2000		.558		
10/29/75	2030		.552		
10/29/75	2100		.568		
10/29/75	2130		.563		
10/29/75	2200		.574		
10/29/75	2230		.579		
10/29/75	2300		.595		
10/29/75	2330		.595		
10/30/75	0000		.622		
10/30/75	0030		.633		
10/30/75	0100		.649		
10/30/75	0130		.660		
10/30/75	0200		.676		
10/30/75	0230		.671		
10/30/75	0300		.671		
10/30/75	0330		.676		
10/30/75	0400		.687		
10/30/75	0430		.666		
10/30/75	0500		.649		
10/30/75	0530		.639		
10/30/75	0600		.633		

DATE / /	TIME / /	FLOW RATE / (GPH) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
10/30/75	0630			.612	
10/30/75	0700			.601	
10/30/75	0730			.585	
10/30/75	0800			.574	
10/30/75	0830			.579	
10/30/75	0900			.590	
10/30/75	0930			.585	
10/30/75	1000			.590	
10/30/75	1030			.601	
10/30/75	1100			.628	
10/30/75	1130			.649	
10/30/75	1130			.649	POWER OUT.
10/30/75	2330			.752	
10/31/75	0000			.757	
10/31/75	0030			.817	
10/31/75	0100			.839	
10/31/75	0130			.860	
10/31/75	0200			.882	
10/31/75	0230			.898	
10/31/75	0300			148.898	
10/31/75	0330			.914	
10/31/75	0400			.909	
10/31/75	0430			.903	
10/31/75	0500			.898	
10/31/75	0530			.893	
10/31/75	0600			.887	
10/31/75	0630			.866	
10/31/75	0700			.849	
10/31/75	0730			.833	
10/31/75	0800			.828	
10/31/75	0830			.812	
10/31/75	1300			149.384	
10/31/75	1330			.873	
10/31/75	1400			.852	
10/31/75	1430			.838	
10/31/75	1500			.814	
10/31/75	1530			.292	
10/31/75	1600			.276	
10/31/75	1630			.249	
10/31/75	1700			.222	
10/31/75	1730			.187	
10/31/75	1800			.173	
10/31/75	1830			.065	
10/31/75	1900			.183	
10/31/75	1930			.076	
10/31/75	2000			.071	
10/31/75	2030			.817	
10/31/75	2100			.806	
10/31/75	2130			148.979	
10/31/75	2200			.984	
10/31/75	2230			149.817	
10/31/75	2300			148.979	
10/31/75	2330			149.822	
11/01/75	0000			148.990	
11/01/75	0030			149.849	
11/01/75	0100			.838	

END OF DATA

APPENDIX 3

RRGE 1 SHORT-TERM TEST DATA.

RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

RRGE 1 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
11/04/75	170000		2082.392		
11/04/75	171000		2082.394		
11/04/75	172000		2082.395		
11/04/75	173000		2082.379		
11/04/75	174000		2082.373		
11/04/75	175000		2082.399		
11/04/75	180000		2082.395		
11/04/75	181000		2082.417		
11/04/75	182000		2082.395		
11/04/75	183000		2082.380		
11/04/75	184000		2082.389		
11/04/75	185000		2082.403		
11/04/75	190000		2082.409		
11/04/75	191000		2082.387		
11/04/75	192000		2082.419		
11/04/75	193000		2082.413		
11/04/75	194000		2082.389		
11/04/75	195000		2082.355		
11/04/75	200000		2082.323		
11/04/75	201000		2082.363		
11/04/75	202000		2082.390		
11/04/75	203000		2082.331		
11/04/75	204000		2082.342		
11/04/75	205000		2082.331		
11/04/75	210000		2082.341		
11/04/75	211000		2082.333		
11/04/75	212000		2082.324		
11/04/75	213000		2082.337		
11/04/75	214000		2082.285		
11/04/75	215000		2082.267		
11/04/75	220000		2082.297		
11/04/75	221000		2082.258		
11/04/75	222000		2082.295		
11/04/75	223000		2082.234		
11/04/75	224000		2082.284		
11/04/75	225000		2082.244		
11/04/75	230000		2082.215		
11/04/75	231000		2082.213		
11/04/75	232000		2082.212		
11/04/75	233000		2082.236		
11/04/75	234000		2082.177		
11/04/75	235000		2082.189		
11/05/75	000000		2082.246		
11/05/75	001000		2082.239		
11/05/75	002000		2082.229		
11/05/75	003000		2082.201		
11/05/75	004000		2082.192		
11/05/75	005000		2082.264		
11/05/75	010000		2082.169		
11/05/75	011000		2082.208		
11/05/75	012000		2082.197		
11/05/75	013000		2082.202		
11/05/75	014000		2082.223		
11/05/75	015000		2082.200		
11/05/75	020000		2082.248		
11/05/75	021000		2082.241		
11/05/75	022000		2082.251		
11/05/75	023000		2082.233		
11/05/75	024000		2082.239		
11/05/75	025000		2082.244		
11/05/75	030000		2082.273		
11/05/75	031000		2082.247		
11/05/75	032000		2082.289		
11/05/75	033000		2082.269		
11/05/75	034000		2082.272		
11/05/75	035000		2082.288		
11/05/75	040000		2082.279		
11/05/75	041000		2082.281		
11/05/75	042000		2082.336		

DATE / /	TIME / /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
11/05/75	043000		2082.305		
11/05/75	044000		2082.343		
11/05/75	045000		2082.349		
11/05/75	050000		2082.344		
11/05/75	051000		2082.328		
11/05/75	052000		2082.371		
11/05/75	053000		2082.396		
11/05/75	054000		2082.416		
11/05/75	055000		2082.394		
11/05/75	060000		2082.382		
11/05/75	061000		2082.392		
11/05/75	062000		2082.368		
11/05/75	063000		2082.381		
11/05/75	064000		2082.423		
11/05/75	065000		2082.419		
11/05/75	070000		2082.429		
11/05/75	071000		2082.408		
11/05/75	072000		2082.414		
11/05/75	073000		2082.417		
11/05/75	074000		2082.420		
11/05/75	075000		2082.404		
11/05/75	080000		2082.468		
11/05/75	081000		2082.425		
11/05/75	082000		2082.410		
11/05/75	083000		2082.429		
11/05/75	084000		2082.424		
11/05/75	084100		2082.421		
11/05/75	084110		2082.421		
11/05/75	084120		2082.421		
11/05/75	084130		2082.417		
11/05/75	084140		2082.416		
11/05/75	084150		2082.416		
11/05/75	084200		2082.413		
11/05/75	084210		2082.413		
11/05/75	084220		2082.411		
11/05/75	084230		2082.412		
11/05/75	084240		2082.409		
11/05/75	084250		2082.409		
11/05/75	084300		2082.407		
11/05/75	084310		2082.408		
11/05/75	084320		2082.490		
11/05/75	084330		2082.408		
11/05/75	084340		2082.413		
11/05/75	084350		2082.413		
11/05/75	084400		2082.417		
11/05/75	084410		2082.419		
11/05/75	084420		2082.421		
11/05/75	084430		2082.422		
11/05/75	084440		2082.423		
11/05/75	084450		2082.428		
11/05/75	084500		2082.403		
11/05/75	084510		2081.032		
11/05/75	084520		2081.883		
11/05/75	084530		2081.816		
11/05/75	084540		2081.768		
11/05/75	084550		2081.733		
11/05/75	084600		2081.708		
11/05/75	084610		2081.685		
11/05/75	084620		2081.667		
11/05/75	084630		2081.653		
11/05/75	084640		2081.643		
11/05/75	084650		2081.632		
11/05/75	084700		2081.622		
11/05/75	084710		2081.613		
11/05/75	084720		2081.606		
11/05/75	084730		2081.598		
11/05/75	084740		2081.591		
11/05/75	084750		2081.583		
11/05/75	084800		2081.578		
11/05/75	084810		2081.573		

FLOW COMMENCED

ARGE 1 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS	DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
11/05/75	084820		2081.567			11/05/75	090000		2081.462		
11/05/75	084830		2081.564			11/05/75	090200		2081.452		
11/05/75	084840		2081.557			11/05/75	090100		2081.463		
11/05/75	084850		2081.556			11/05/75	090300		2081.447		
11/05/75	084900		2081.622			11/05/75	090400		2081.439		
11/05/75	084910		2081.546			11/05/75	090500		2081.435		
11/05/75	084920		2081.542			11/05/75	090600		2081.424		
11/05/75	084930		2081.538			11/05/75	090700		2081.411		
11/05/75	084940		2081.537			11/05/75	090800		2081.415		
11/05/75	084950		2081.533			11/05/75	090900		2081.419		
11/05/75	085000		2081.532			11/05/75	091000		2081.415		
11/05/75	085010		2081.530			11/05/75	091100		2081.407		
11/05/75	085020		2081.529			11/05/75	091200		2081.403		
11/05/75	085030		2081.528			11/05/75	091300		2081.397		
11/05/75	085040		2081.527			11/05/75	091400		2081.398		
11/05/75	085050		2081.525			11/05/75	091500		2081.400		
11/05/75	085100		2081.524			11/05/75	091600		2081.400		
11/05/75	085110		2081.521			11/05/75	091700		2081.401		
11/05/75	085120		2081.517			11/05/75	091800		2081.395		
11/05/75	085130		2081.515			11/05/75	091900		2081.402		
11/05/75	085140		2081.515			11/05/75	092000		2081.407		
11/05/75	085150		2081.515			11/05/75	092100		2081.401		
11/05/75	085200		2081.513			11/05/75	092200		2081.402		
11/05/75	085210		2081.511			11/05/75	092300		2081.406		
11/05/75	085220		2081.505			11/05/75	092400		2081.411		
11/05/75	085230		2081.500			11/05/75	092500		2081.421		
11/05/75	085240		2081.495			11/05/75	092600		2081.414		
11/05/75	085250		2081.491			11/05/75	092700		2081.412		
11/05/75	085300		2081.492			11/05/75	092800		2081.408		
11/05/75	085310		2081.493			11/05/75	092900		2081.398		
11/05/75	085320		2081.494			11/05/75	093000		2081.377		
11/05/75	085330		2081.497			11/05/75	093100		2081.376		
11/05/75	085340		2081.500			11/05/75	093200		2081.379		
11/05/75	085350		2081.500			11/05/75	093300		2081.377		
11/05/75	085400		2081.503			11/05/75	093400		2081.368		
11/05/75	085410		2081.503			11/05/75	093500		2081.362		
11/05/75	085420		2081.503			11/05/75	093600		2081.374		
11/05/75	085430		2081.504			11/05/75	093700		2081.373		
11/05/75	085440		2081.503			11/05/75	093800		2081.372		
11/05/75	085450		2081.500			11/05/75	093900		2081.381		
11/05/75	085500		2081.497			11/05/75	094000		2081.380		
11/05/75	085510		2081.500			11/05/75	094100		2081.377		
11/05/75	085520		2081.499			11/05/75	094200		2081.368		
11/05/75	085530		2081.496			11/05/75	094300		2081.377		
11/05/75	085540		2081.494			11/05/75	094400		2081.391		
11/05/75	085550		2081.494			11/05/75	094500		2081.406		
11/05/75	085600		2081.494			11/05/75	094600		2081.406		
11/05/75	085610		2081.491			11/05/75	094700		2081.394		
11/05/75	085620		2081.491			11/05/75	094800		2081.390		
11/05/75	085630		2081.490			11/05/75	094900		2081.383		
11/05/75	085640		2081.488			11/05/75	095000		2081.372		
11/05/75	085650		2081.485			11/05/75	095100		2081.359		
11/05/75	085700		2081.484			11/05/75	095200		2081.345		
11/05/75	085710		2081.485			11/05/75	095300		2081.333		
11/05/75	085720		2081.485			11/05/75	095400		2081.340		
11/05/75	085730		2081.481			11/05/75	095500		2081.342		
11/05/75	085740		2081.479			11/05/75	095600		2081.339		
11/05/75	085750		2081.478			11/05/75	095700		2081.329		
11/05/75	085800		2081.472			11/05/75	095800		2081.322		
11/05/75	085810		2081.471			11/05/75	095900		2081.320		
11/05/75	085820		2081.473			11/05/75	100000		2081.320		
11/05/75	085830		2081.469			11/05/75	100100		2081.328		
11/05/75	085840		2081.469			11/05/75	100200		2081.311		
11/05/75	085850		2081.470			11/05/75	100300		2081.311		
11/05/75	085900		2081.467			11/05/75	100400		2081.306		
11/05/75	085910		2081.466			11/05/75	100500		2081.306		
11/05/75	085920		2081.465			11/05/75	100600		2081.303		
11/05/75	085930		2081.464			11/05/75	100700		2081.300		
11/05/75	085940		2081.465			11/05/75	100800		2081.292		
11/05/75	085950		2081.464			11/05/75	100900		2081.297		

RRGE 1 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
11/05/75	101000		2081.297		
11/05/75	101100		2081.304		
11/05/75	101200		2081.315		
11/05/75	101300		2081.314		
11/05/75	101400		2081.317		
11/05/75	101500		2081.327		
11/05/75	101600		2081.327		
11/05/75	101700		2081.321		
11/05/75	101800		2081.317		
11/05/75	101900		2081.307		
11/05/75	102000		2081.320		
11/05/75	102100		2081.334		
11/05/75	102200		2081.340		
11/05/75	102300		2081.341		
11/05/75	102400		2081.333		
11/05/75	102500		2081.320		
11/05/75	102600		2081.322		
11/05/75	102700		2081.324		
11/05/75	102800		2081.316		
11/05/75	102900		2081.329		
11/05/75	103000		2081.320		
11/05/75	104000		2081.281		
11/05/75	105000		2081.261		
11/05/75	110000		2081.261		
11/05/75	111000		2081.253		
11/05/75	112000		2081.268		
11/05/75	113000		2081.268		
11/05/75	114000		2081.298		
11/05/75	115000		2081.268		
11/05/75	120000		2081.264		
11/05/75	121000		2081.270		
11/05/75	122000		2081.261		
11/05/75	123000		2081.229		
11/05/75	124000		2081.294		
11/05/75	125000		2081.258		
11/05/75	130000		2081.255		
11/05/75	131000		2081.233		
11/05/75	132000		2081.262		
11/05/75	133000		2081.232		
11/05/75	134000		2081.220		
11/05/75	135000		2081.246		
11/05/75	140000		2081.193		
11/05/75	141000		2081.213		
11/05/75	142000		2081.217		
11/05/75	143000		2081.256		
11/05/75	144000		2081.235		
11/05/75	145000		2081.238		
11/05/75	150000		2081.208		
11/05/75	151000		2081.187		
11/05/75	152000		2081.227		
11/05/75	153000		2081.197		
11/05/75	154000		2081.233		
11/05/75	155000		2081.222		
11/05/75	160000		2081.217		
11/05/75	161000		2081.210		
11/05/75	162000		2081.232		
11/05/75	163000		2081.180		
11/05/75	164000		2081.221		
11/05/75	165000		2081.175		
11/05/75	170000		2081.250		
11/05/75	171000		2081.275		
11/05/75	172000		2081.234		
11/05/75	173000		2081.236		
11/05/75	174000		2081.254		
11/05/75	175000		2081.263		
11/05/75	180000		2081.237		
11/05/75	181000		2081.256		
11/05/75	182000		2081.227		
11/05/75	183000		2081.271		
11/05/75	184000		2081.216		

DATE / /	TIME / /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
11/05/75	185000		2081.196		
11/05/75	190000		2081.226		
11/05/75	191000		2081.168		
11/05/75	192000		2081.183		
11/05/75	193000		2081.194		
11/05/75	194000		2081.255		
11/05/75	195000		2081.223		
11/05/75	200000		2081.225		
11/05/75	201000		2081.246		
11/05/75	202000		2081.208		
11/05/75	203000		2081.202		
11/05/75	204000		2081.224		
11/05/75	205000		2081.194		
11/05/75	210000		2081.201		
11/05/75	211000		2081.101		
11/05/75	212000		2081.173		
11/05/75	213000		2081.184		
11/05/75	214000		2081.122		
11/05/75	215000		2081.186		
11/05/75	220000		2081.148		
11/05/75	221000		2081.143		
11/05/75	222000		2081.129		
11/05/75	223000		2081.087		
11/05/75	224000		2081.105		
11/05/75	225000		2081.131		
11/05/75	230000		2081.084		
11/05/75	231000		2081.118		
11/05/75	232000		2081.111		
11/05/75	233000		2081.049		
11/05/75	234000		2081.056		
11/05/75	235000		2081.326		
11/06/75	000000		2081.048		
11/06/75	001000		2081.070		
11/06/75	002000		2081.328		
11/06/75	003000		2081.021		
11/06/75	004000		2081.003		
11/06/75	005000		2081.073		
11/06/75	010000		2081.063		
11/06/75	012000		2081.070		
11/06/75	013000		2081.013		
11/06/75	014000		2081.079		
11/06/75	015000		2081.000		
11/06/75	020000		2081.015		
11/06/75	021000		2081.068		
11/06/75	022000		2081.000		
11/06/75	023000		2081.038		
11/06/75	024000		2081.001		
11/06/75	025000		2081.062		
11/06/75	030000		2081.333		
11/06/75	031000		2081.058		
11/06/75	032000		2081.057		
11/06/75	033000		2081.075		
11/06/75	034000		2081.091		
11/06/75	035000		2081.093		
11/06/75	040000		2081.043		
11/06/75	041000		2081.053		
11/06/75	042000		2081.033		
11/06/75	043000		2081.129		
11/06/75	044000		2081.104		
11/06/75	045000		2081.132		
11/06/75	050000		2081.154		
11/06/75	051000		2081.151		
11/06/75	052000		2081.101		
11/06/75	053000		2081.150		
11/06/75	054000		2081.167		
11/06/75	055000		2081.133		
11/06/75	060000		2081.159		
11/06/75	061000		2081.169		
11/06/75	062000		2081.178		
11/06/75	063000		2081.130		

RRGE 1 SHORT-TERM TEST DATA, RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME / /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
11/06/75	064000		2081.200		
11/06/75	065000		2081.202		
11/06/75	070000		2081.201		
11/06/75	071000		2081.109		
11/06/75	072000		2081.212		
11/06/75	073000		2081.213		
11/06/75	074000		2081.185		
11/06/75	075000		2081.225		
11/06/75	080000		2081.205		
11/06/75	081000		2081.208		
11/06/75	082000		2081.162		
11/06/75	083000		2081.276		
11/06/75	084000		2081.268		
11/06/75	085000		2081.214		
11/06/75	090000		2081.197		
11/06/75	091000		2081.206		
11/06/75	092000		2081.245		
11/06/75	093000		2081.211		
11/06/75	094000		2081.245		
11/06/75	095000		2081.228		
11/06/75	100000		2081.196		
11/06/75	101000		2081.215		
11/06/75	102000		2081.257		
11/06/75	103000		2081.248		
11/06/75	104000		2081.209		
11/06/75	105000		2081.206		
11/06/75	110000		2081.160		
11/06/75	111000		2081.181		
11/06/75	112000		2081.164		
11/06/75	113000		2081.206		
11/06/75	114000		2081.267		
11/06/75	115000		2081.208		
11/06/75	120000		2081.217		
11/06/75	121000		2081.268		
11/06/75	122000		2081.124		
11/06/75	123000		2081.164		
11/06/75	124000		2081.146		
11/06/75	125000		2081.139		
11/06/75	130000		2081.144		
11/06/75	131000		2081.108		
11/06/75	132000		2081.076		
11/06/75	133000		2081.188		
11/06/75	134000		2081.185		
11/06/75	135000		2081.188		
11/06/75	140000		2081.120		
11/06/75	141000		2081.207		
11/06/75	142000		2081.127		
11/06/75	143000		2081.09		
11/06/75	143600		2081.11		
11/06/75	143700		2081.13		
11/06/75	143800		2081.15		
11/06/75	143900		2081.14		
11/06/75	144000		2081.13		
11/06/75	144100		2081.13		
11/06/75	144259		2081.15		
11/06/75	144301		2081.14		
11/06/75	144302		2081.14		
11/06/75	144303		2081.15		
11/06/75	144304		2081.14		
11/06/75	144305		2081.13		
11/06/75	144306		2081.14		
11/06/75	144308		2081.15		
11/06/75	144310		2081.14		
11/06/75	144311		2081.14		
11/06/75	144312		2081.13		
11/06/75	144313		2081.15		
11/06/75	144314		2081.15		
11/06/75	144315		2081.14		
11/06/75	144316		2081.14		
11/06/75	144318		2081.14		

DATE / /	TIME / /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
11/06/75	144319			2081.14	
11/06/75	144320			2081.14	
11/06/75	144321			2081.13	
11/06/75	144322			2081.13	
11/06/75	144323			2081.13	
11/06/75	144324			2081.14	
11/06/75	144325			2081.14	
11/06/75	144326			2081.14	
11/06/75	144327			2081.14	
11/06/75	144328			2081.14	
11/06/75	144329			2081.14	
11/06/75	144330			2081.15	
11/06/75	144331			2081.14	
11/06/75	144332			2081.13	
11/06/75	144334			2081.14	
11/06/75	144335			2081.14	
11/06/75	144336			2081.14	
11/06/75	144337			2081.14	
11/06/75	144338			2081.15	
11/06/75	144339			2081.15	
11/06/75	144340			2081.14	
11/06/75	144342			2081.14	
11/06/75	144343			2081.15	
11/06/75	144344			2081.14	
11/06/75	144345			2081.14	
11/06/75	144346			2081.15	
11/06/75	144347			2081.15	
11/06/75	144348			2081.15	
11/06/75	144350			2081.15	
11/06/75	144351			2081.14	
11/06/75	144352			2081.15	
11/06/75	144353			2081.15	
11/06/75	144354			2081.15	
11/06/75	144355			2081.14	
11/06/75	144356			2081.15	
11/06/75	144358			2081.16	
11/06/75	144359			2081.15	
11/06/75	144400			2081.15	
11/06/75	144401			2081.17	
11/06/75	144402			2081.15	
11/06/75	144403			2081.15	
11/06/75	144404			2081.15	
11/06/75	144406			2081.16	
11/06/75	144407			2081.16	
11/06/75	144408			2081.15	
11/06/75	144409			2081.15	
11/06/75	144410			2081.15	
11/06/75	144411			2081.16	
11/06/75	144412			2081.15	
11/06/75	144414			2081.15	
11/06/75	144415			2081.16	
11/06/75	144416			2081.15	
11/06/75	144417			2081.16	
11/06/75	144418			2081.16	
11/06/75	144419			2081.17	
11/06/75	144420			2081.16	
11/06/75	144422			2081.16	
11/06/75	144423			2081.17	
11/06/75	144424			2081.16	
11/06/75	144425			2081.15	
11/06/75	144426			2081.16	
11/06/75	144427			2081.17	
11/06/75	144428			2081.16	
11/06/75	144430			2081.15	
11/06/75	144431			2081.17	
11/06/75	144432			2081.16	
11/06/75	144433			2081.16	
11/06/75	144434			2081.16	
11/06/75	144435			2081.17	
11/06/75	144436			2081.16	

RRGE 1 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
11/06/75	144438		2081.16		
11/06/75	144439		2081.17		
11/06/75	144440		2081.17		
11/06/75	144441		2081.16		
11/06/75	144442		2081.16		
11/06/75	144443		2081.17		
11/06/75	144444		2081.17		
11/06/75	144446		2081.16		
11/06/75	144447		2081.18		
11/06/75	144447		2081.18		
11/06/75	144448		2081.17		
11/06/75	144449		2081.17		
11/06/75	144450		2081.17		
11/06/75	144451		2081.17		
11/06/75	144452		2081.17		
11/06/75	144454		2081.17		
11/06/75	144455		2081.18		
11/06/75	144456		2081.17		
11/06/75	144457		2081.17		
11/06/75	144458		2081.17		
11/06/75	144459		2081.17		
11/06/75	144500		2081.17		FLOW SHUT IN. ASSUME ZERO TIME FOR BUILD UP
11/06/75	144502		2081.18		
11/06/75	144503		2081.19		
11/06/75	144504		2081.28		
11/06/75	144505		2081.40		
11/06/75	144506		2081.53		
11/06/75	144507		2081.57		
11/06/75	144508		2081.58		
11/06/75	144510		2081.66		
11/06/75	144511		2081.67		
11/06/75	144512		2081.67		
11/06/75	144513		2081.74		
11/06/75	144514		2081.75		
11/06/75	144515		2081.75		
11/06/75	144516		2081.78		
11/06/75	144518		2081.79		
11/06/75	144519		2081.80		
11/06/75	144520		2081.83		
11/06/75	144521		2081.83		
11/06/75	144522		2081.85		
11/06/75	144523		2081.86		
11/06/75	144524		2081.86		
11/06/75	144526		2081.88		
11/06/75	144527		2081.88		
11/06/75	144528		2081.88		
11/06/75	144529		2081.90		
11/06/75	144530		2081.92		
11/06/75	144531		2081.91		
11/06/75	144532		2081.92		
11/06/75	144534		2081.94		
11/06/75	144535		2081.93		
11/06/75	144536		2081.94		
11/06/75	144537		2081.95		
11/06/75	144538		2081.95		
11/06/75	144539		2081.95		
11/06/75	144540		2081.95		
11/06/75	144542		2081.97		
11/06/75	144543		2081.97		
11/06/75	144544		2081.97		
11/06/75	144545		2081.98		
11/06/75	144546		2081.98		
11/06/75	144547		2081.98		
11/06/75	144548		2081.99		
11/06/75	144550		2082.00		
11/06/75	144551		2082.00		
11/06/75	144552		2082.00		
11/06/75	144553		2082.00		
11/06/75	144554		2082.00		

DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
11/06/75	144555		2082.01		
11/06/75	144556		2082.01		
11/06/75	144558		2082.01		
11/06/75	144559		2082.02		
11/06/75	144600		2082.02		
11/06/75	144601		2082.02		
11/06/75	144602		2082.03		
11/06/75	144603		2082.03		
11/06/75	144604		2082.03		
11/06/75	144606		2082.03		
11/06/75	144607		2082.04		
11/06/75	144608		2082.03		
11/06/75	144609		2082.03		
11/06/75	144610		2082.04		
11/06/75	144611		2082.04		
11/06/75	144612		2082.04		
11/06/75	144614		2082.05		
11/06/75	144615		2082.05		
11/06/75	144616		2082.05		
11/06/75	144617		2082.05		
11/06/75	144618		2082.06		
11/06/75	144619		2082.05		
11/06/75	144620		2082.06		
11/06/75	144622		2082.06		
11/06/75	144623		2082.07		
11/06/75	144624		2082.06		
11/06/75	144625		2082.07		
11/06/75	144626		2082.07		
11/06/75	144627		2082.07		
11/06/75	144628		2082.07		
11/06/75	144630		2082.07		
11/06/75	144631		2082.08		
11/06/75	144632		2082.07		
11/06/75	144633		2082.08		
11/06/75	144634		2082.09		
11/06/75	144635		2082.09		
11/06/75	144636		2082.08		
11/06/75	144638		2082.09		
11/06/75	144639		2082.09		
11/06/75	144640		2082.09		
11/06/75	144641		2082.09		
11/06/75	144642		2082.11		
11/06/75	144643		2082.09		
11/06/75	144644		2082.09		
11/06/75	144646		2082.09		
11/06/75	144647		2082.10		
11/06/75	144648		2082.10		
11/06/75	144649		2082.10		
11/06/75	144650		2082.11		
11/06/75	144651		2082.11		
11/06/75	144652		2082.10		
11/06/75	144654		2082.11		
11/06/75	144655		2082.11		
11/06/75	144656		2082.10		
11/06/75	144657		2082.11		
11/06/75	144658		2082.12		
11/06/75	144659		2082.11		
11/06/75	144700		2082.11		
11/06/75	144702		2082.12		
11/06/75	144703		2082.12		
11/06/75	144704		2082.11		
11/06/75	144705		2082.11		
11/06/75	144706		2082.13		
11/06/75	144707		2082.12		
11/06/75	144708		2082.12		
11/06/75	144710		2082.12		
11/06/75	144711		2082.13		
11/06/75	144712		2082.12		
11/06/75	144713		2082.13		
11/06/75	144714		2082.14		

RAGE 1 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
11/06/75	144715		2082.13		
11/06/75	144716		2082.13		
11/06/75	144718		2082.13		
11/06/75	144719		2082.13		
11/06/75	144720		2082.13		
11/06/75	144721		2082.13		
11/06/75	144722		2082.14		
11/06/75	144723		2082.13		
11/06/75	144724		2082.13		
11/06/75	144726		2082.13		
11/06/75	144727		2082.13		
11/06/75	144728		2082.13		
11/06/75	144729		2082.14		
11/06/75	144730		2082.15		
11/06/75	144731		2082.14		
11/06/75	144732		2082.14		
11/06/75	144734		2082.15		
11/06/75	144735		2082.14		
11/06/75	144736		2082.14		
11/06/75	144737		2082.14		
11/06/75	144738		2082.15		
11/06/75	144739		2082.15		
11/06/75	144740		2082.15		
11/06/75	144742		2082.15		
11/06/75	144743		2082.15		
11/06/75	144744		2082.15		
11/06/75	144745		2082.15		
11/06/75	144746		2082.16		
11/06/75	144747		2082.15		
11/06/75	144748		2082.15		
11/06/75	144750		2082.16		
11/06/75	144751		2082.15		
11/06/75	144752		2082.15		
11/06/75	144753		2082.15		
11/06/75	144754		2082.16		
11/06/75	144755		2082.16		
11/06/75	144756		2082.16		
11/06/75	144758		2082.16		
11/06/75	144759		2082.16		
11/06/75	144800		2082.17		
11/06/75	144801		2082.16		
11/06/75	144802		2082.16		
11/06/75	144803		2082.16		
11/06/75	144804		2082.17		
11/06/75	144806		2082.16		
11/06/75	144807		2082.17		
11/06/75	144808		2082.17		
11/06/75	144809		2082.17		
11/06/75	144810		2082.16		
11/06/75	144811		2082.16		
11/06/75	144812		2082.17		
11/06/75	144814		2082.17		
11/06/75	144815		2082.16		
11/06/75	144816		2082.17		
11/06/75	144817		2082.16		
11/06/75	144818		2082.16		
11/06/75	144819		2082.17		
11/06/75	144820		2082.18		
11/06/75	144822		2082.17		
11/06/75	144823		2082.17		
11/06/75	144824		2082.16		
11/06/75	144825		2082.16		
11/06/75	144826		2082.17		
11/06/75	144827		2082.17		
11/06/75	144828		2082.16		
11/06/75	144830		2082.16		
11/06/75	144831		2082.17		
11/06/75	144832		2082.16		
11/06/75	144833		2082.17		
11/06/75	144834		2082.18		

DATE / /	TIME /	FLOW RATE / (GPM) /	DOWNHOLE / PRESSURE / (PSIA) /	WELL HEAD / PRESSURE / (PSIA) /	REMARKS
11/06/75	144835		2082.16		
11/06/75	144836		2082.17		
11/06/75	144838		2082.17		
11/06/75	144839		2082.16		
11/06/75	144840		2082.17		
11/06/75	144841		2082.17		
11/06/75	144842		2082.17		
11/06/75	144843		2082.17		
11/06/75	144844		2082.18		
11/06/75	144846		2082.17		
11/06/75	144847		2082.17		
11/06/75	144848		2082.18		
11/06/75	144849		2082.17		
11/06/75	144850		2082.16		
11/06/75	144851		2082.17		
11/06/75	144852		2082.17		
11/06/75	144854		2082.17		
11/06/75	144855		2082.17		
11/06/75	144856		2082.18		
11/06/75	144857		2082.17		
11/06/75	144858		2082.16		
11/06/75	144859		2082.17		
11/06/75	144900		2082.18		
11/06/75	144902		2082.17		
11/06/75	144903		2082.17		
11/06/75	144904		2082.18		
11/06/75	144905		2082.17		
11/06/75	144906		2082.16		
11/06/75	144907		2082.17		
11/06/75	144908		2082.18		
11/06/75	144910		2082.17		
11/06/75	144911		2082.17		
11/06/75	144912		2082.18		
11/06/75	144913		2082.17		
11/06/75	144914		2082.17		
11/06/75	144915		2082.17		
11/06/75	144916		2082.18		
11/06/75	144918		2082.17		
11/06/75	144919		2082.17		
11/06/75	144920		2082.18		
11/06/75	144921		2082.17		
11/06/75	144922		2082.17		
11/06/75	144923		2082.17		
11/06/75	144924		2082.18		
11/06/75	144926		2082.17		
11/06/75	144927		2082.18		
11/06/75	144928		2082.18		
11/06/75	144929		2082.17		
11/06/75	144930		2082.17		
11/06/75	144931		2082.17		
11/06/75	144932		2082.18		
11/06/75	144934		2082.18		
11/06/75	144935		2082.17		
11/06/75	144936		2082.18		
11/06/75	144937		2082.18		
11/06/75	144938		2082.17		
11/06/75	144939		2082.17		
11/06/75	144940		2082.17		
11/06/75	144942		2082.18		
11/06/75	144943		2082.17		
11/06/75	144944		2082.17		
11/06/75	144945		2082.18		
11/06/75	144946		2082.18		
11/06/75	144947		2082.17		
11/06/75	144948		2082.17		
11/06/75	144950		2082.17		
11/06/75	144951		2082.17		
11/06/75	144952		2082.17		
11/06/75	144953		2082.17		
11/06/75	144954		2082.18		

DATE	TIME	FLOW RATE/ (GPM)	WELL HEAD/ PRESSURE/ (PSIA)	REMARKS
11/07/75	023000		2082.196	
11/07/75	024000		2082.208	
11/07/75	025000		2082.201	
11/07/75	030000		2082.213	
11/07/75	031000		2082.241	
11/07/75	032000		2082.212	
11/07/75	033000		2082.190	
11/07/75	034000		2082.226	
11/07/75	035000		2082.209	
11/07/75	040000		2082.206	
11/07/75	041000		2082.209	
11/07/75	042000		2082.226	
11/07/75	043000		2082.255	
11/07/75	044000		2082.280	
11/07/75	045000		2082.265	
11/07/75	050000		2082.237	
11/07/75	051000		2082.275	
11/07/75	052000		2082.289	
11/07/75	053000		2082.303	
11/07/75	054000		2082.308	
11/07/75	055000		2082.270	
11/07/75	060000		2082.311	
11/07/75	061000		2082.299	
11/07/75	062000		2082.282	
11/07/75	063000		2082.308	
11/07/75	064000		2082.327	
11/07/75	065000		2082.312	
11/07/75	070000		2082.313	
11/07/75	071000		2082.330	
11/07/75	072000		2082.327	
11/07/75	073000		2082.355	
11/07/75	074000		2082.317	
11/07/75	075000		2082.355	
11/07/75	080000		2082.387	
11/07/75	081000		2082.361	
11/07/75	082000		2082.363	
11/07/75	083000		2082.392	
11/07/75	084000		2082.369	
11/07/75	085000		2082.350	
11/07/75	090000		2082.335	
11/07/75	091000		2082.361	
11/07/75	092000		2082.403	

END OF DATA

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၁၁၁၁၁၁၁၁.၁၁၁၁၁၁၁၁.၁၁၁၁၀၀၀၀.၀၀၀၀၀၀၀၀.၀၀၀၀၀၀၁၁.၁၁၁၁၁၁၀၀.၀၀၀၀၀၀၀၀.၀၀၁၁၁၁၁၁

LOAD MAP.

LINK - SKY 6000/7000

FL REQUIRED TO LOAD 20600
FL REQUIRED TO RUN 10100
INITIAL TRANSFER TO COPYIT - 101

BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE
COPYIT	100	4352	L60
/QSYSCON/	4452	20	
ENDP	4472	31	SYSLIB
/ABCDUF/	4523	231	
INPUTC	4754	117	SYSLIB
/QLNLMT/	5073	1	
OUTPTC	5074	75	SYSLIB
/QASAFGL/	5171	1	
/QFILEAD/	5172	1	
/QJOESFL/	5173	2	
QENTRY	5175	90	SYSLIB
/EZOSC/	5245	30	
KODER	5275	1242	SYSLIB
KRAKER	6537	747	SYSLIB
QREADST	7506	23	SYSLIB
QSYS	7531	25	SYSLIB
QTRACED	7556	21	SYSLIB
QWRITES	7577	43	SYSLIB
SYSTEM*	7642	133	SYSLIB
QFILEND	7775	12	SYSLIB
QFNDFET	10067	51	SYSLIB
REMARK	10060	13	SYSLIB

RRGE 1 SHORT-TERM TEST DATA. RAFT RIVER VALLEY GEOTHERMAL FIELD, IDAHO

DATE / /	TIME /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS	DATE / /	TIME /	FLOW RATE/ (GPM) /	DOWNHOLE/ PRESSURE/ (PSIA) /	WELL HEAD/ PRESSURE/ (PSIA) /	REMARKS
11/06/75	144955		2082.17			11/06/75	152600		2082.192		
11/06/75	144956		2082.16			11/06/75	152700		2082.192		
11/06/75	144958		2082.17			11/06/75	152800		2082.187		
11/06/75	144959		2082.17			11/06/75	152900		2082.195		
11/06/75	145000		2082.17			11/06/75	153000		2082.193		
11/06/75	145010		2082.18			11/06/75	154000		2082.171		
11/06/75	145020		2082.17			11/06/75	155000		2082.228		
11/06/75	145030		2082.17			11/06/75	160000		2082.206		
11/06/75	145040		2082.17			11/06/75	161000		2082.248		
11/06/75	145050		2082.17			11/06/75	162000		2082.281		
11/06/75	145100		2082.17			11/06/75	163000		2082.284		
11/06/75	145110		2082.17			11/06/75	164000		2082.256		
11/06/75	145120		2082.17			11/06/75	165000		2082.258		
11/06/75	145130		2082.18			11/06/75	170000		2082.264		
11/06/75	145140		2082.18			11/06/75	171000		2082.288		
11/06/75	145150		2082.18			11/06/75	172000		2082.274		
11/06/75	145200		2082.17			11/06/75	173000		2082.322		
11/06/75	145210		2082.16			11/06/75	174000		2082.317		
11/06/75	145220		2082.16			11/06/75	175000		2082.303		
11/06/75	145230		2082.17			11/06/75	180000		2082.306		
11/06/75	145240		2082.16			11/06/75	181000		2082.301		
11/06/75	145250		2082.15			11/06/75	182000		2082.278		
11/06/75	145300		2082.17			11/06/75	183000		2082.318		
11/06/75	145310		2082.16			11/06/75	184000		2082.273		
11/06/75	145320		2082.17			11/06/75	185000		2082.328		
11/06/75	145330		2082.16			11/06/75	190000		2082.323		
11/06/75	145340		2082.15			11/06/75	191000		2082.363		
11/06/75	145350		2082.15			11/06/75	192000		2082.333		
11/06/75	145400		2082.15			11/06/75	193000		2082.314		
11/06/75	145410		2082.16			11/06/75	194000		2082.333		
11/06/75	145420		2082.15			11/06/75	195000		2082.362		
11/06/75	145430		2082.15			11/06/75	200000		2082.355		
11/06/75	145440		2082.14			11/06/75	201000		2082.342		
11/06/75	145450		2082.14			11/06/75	202000		2082.305		
11/06/75	145500		2082.14			11/06/75	203000		2082.341		
11/06/75	145530		2082.15			11/06/75	204000		2082.341		
11/06/75	145600		2082.15			11/06/75	205000		2082.329		
11/06/75	145630		2082.17			11/06/75	210000		2082.292		
11/06/75	145700		2082.17			11/06/75	211000		2082.319		
11/06/75	145730		2082.18			11/06/75	212000		2082.293		
11/06/75	145800		2082.18			11/06/75	213000		2082.317		
11/06/75	145830		2082.18			11/06/75	214000		2082.321		
11/06/75	145900		2082.19			11/06/75	215000		2082.279		
11/06/75	145930		2082.20			11/06/75	220000		2082.305		
11/06/75	150000		2082.122			11/06/75	221000		2082.294		
11/06/75	150100		2082.198			11/06/75	222000		2082.289		
11/06/75	150200		2082.187			11/06/75	223000		2082.266		
11/06/75	150300		2082.188			11/06/75	224000		2082.291		
11/06/75	150400		2082.187			11/06/75	225000		2082.288		
11/06/75	150500		2082.140			11/06/75	230000		2082.247		
11/06/75	150600		2082.129			11/06/75	231000		2082.261		
11/06/75	150700		2082.142			11/06/75	232000		2082.237		
11/06/75	150800		2082.157			11/06/75	233000		2082.219		
11/06/75	150900		2082.157			11/06/75	234000		2082.223		
11/06/75	151000		2082.161			11/06/75	235000		2082.248		
11/06/75	151100		2082.160			11/07/75	000000		2082.199		
11/06/75	151200		2082.171			11/07/75	001000		2082.239		
11/06/75	151300		2082.193			11/07/75	002000		2082.198		
11/06/75	151400		2082.192			11/07/75	003000		2082.228		
11/06/75	151500		2082.195			11/07/75	004000		2082.216		
11/06/75	151600		2082.191			11/07/75	005000		2082.204		
11/06/75	151700		2082.183			11/07/75	010000		2082.189		
11/06/75	151800		2082.173			11/07/75	011000		2082.179		
11/06/75	151900		2082.171			11/07/75	012000		2082.201		
11/06/75	152000		2082.167			11/07/75	013000		2082.214		
11/06/75	152100		2082.164			11/07/75	014000		2082.207		
11/06/75	152200		2082.172			11/07/75	015000		2082.191		
11/06/75	152300		2082.181			11/07/75	020000		2082.243		
11/06/75	152400		2082.193			11/07/75	021000		2082.162		
11/06/75	152500		2082.186			11/07/75	022000		2082.198		

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