TRACKING TESTS FOR THE SNS FAST INJECTION BUMP POWER SUPPLY*

W.Eng (BNL), R.Cutler (SNS), S.Dewan (DPS), R.Holmes (IE), R.Lambiase (BNL), Y.Y.Lee (BNL), W.McGahern (BNL), C.Pai (BNL), S.Peng (SNS), K.Rust (SNS), J.Sandberg (BNL), J.Smith (BNL), A.Soukas (BNL), J.Wei (BNL), B.Weng (BNL), S.Wong (UOT), J.Zeng (UOT), BNL, Upton, NY 11973 USA

Abstract

The tracking requirement of the SNS Fast Injection Bump power supplies is described. In addition to the usual tracking between the load current and the input reference of a power supply, these power supplies must also track between pairs of units under slightly different loads. This paper describes the use of a current-null test to measure tracking performances. For the actual tests, a single dummy magnet load was used to measure the tracking between the first two production units at the manufacturer's facility. Using the Yokogawa WE7000 PC-based measurement instrument, input and output waveforms are digitized and stored in data files. A program written for this application is then used to extract data from these files to construct, analyze the waveforms and characterize the power supply performance. Results of the measurements of two SNS Fast Injection Bump power supplies will be presented in this paper.

INTRODUCTION

The SNS Fast Injection Bump switch mode power supplies are pulsed current-regulated. In order to meet current tracking and current ripple requirements, the supply has an outer current loop bandwidth of about 2 kHz and an inner voltage loop bandwidth of 100 kHz. These two quadrant power supplies are peak rated at 1.12 MVA, +1400A, and +/-800V[1].

Two reference functions are used for testing the tracking performance of the power supplies. Both waveforms have the same rise and flat top of 2 millisecc and 1 millisecc respectively. The fall time, on the other hand, is 1 millisecc for one and 250 microsecc for the other. Within the pulse duration, besides the basic requirement of having the load current of individual power supply tracked the reference, load currents of pairs of power supplies must also track. In this case, because of the complex tasks involved in verifying tracking performance, a test system has been developed to gather, process, and analyze test data.

BASIC TEST SYSTEM

Figures 1 and 2 show the conceptual tracking tests based on signal-null.

For the reference vs. current tracking test, a WFG (Waveform Generator) feeds a pulse to the power supply and a programmable delay circuit. Signal picked up by the current detector is subtracted from a time-delayed version of the reference pulse to generate a tracking error waveform.

For the dual supplies tracking test, the WFG feeds both power supplies. In this case, signals from two current

detectors are subtracted from one another to get the error waveform.

Fig. 1 Reference vs. current tracking test

Fig. 2 Tracking between power supplies

Fig. 3 shows the basic elements of a practical test system, which consist of two programmable waveform generators and a 2-channel waveform digitizer.

Fig. 3 Injection Bump P. S. tracking test system

For the reference vs. current tracking test, load current signal from the current detector is fed into one of the digitizers and, an identical but time-delayed version of the reference pulse is fed into the other. A tester can look at the real-time digitizer outputs, readjust the time delay of the WFG2 waveform if needed, and save the outputs to a file. A waveform-viewing program is then used to generate the tracking error based on the two data streams in the file. For the dual supplies tracking test, it is just a

In this system, the matching of identical functions generated by the waveform function generators are within 0.1%. The A/D resolution of the digitizers is equivalent to 14 bits.

Finally, to obtain a simplified error profile in the reference vs. current or current vs. current null, the tester is allowed to delay one of the waveforms by whatever amount needed to get the best result. This, in effect, should eliminate the tracking error due to the inherent time delay produced by the power supply.

The reference vs. load current error without delay correction is shown in the bottom window of Fig. 4, which also depicts the graphic user interface of the Waveform Viewer program used by the tester to check that proper waveforms have been captured. Since a large portion of this error is caused by the time delay of the power supply, applying a proper time delay to the reference pulse minimizes it.

For unit 1, though tested on a slightly different load, it can duplicate the tracking performance exhibited by the reference unit with a current-loop gain change. Comparing to Fig. 6, the error profile in Fig. 7 looks almost identical.

Fig. 6 Tracking error profile for reference unit

Fig. 7 Tracking error profile for unit 1

The reference unit has been tested with a load of 13 mOhm + 170 uH. For unit 1, the same load has its inductance increased to 180 uH.

To maintain the same tracking as the reference unit, however, a 10.7% increase in gain is needed for unit 1 to compensate for this load change. The tracking of load currents between the first two production units is shown in Fig. 8.

Fig. 8 Tracking between two power supplies

The tracking error between supplies lies within +0.5% and -0.2%.

Now, for the pulse with 1millisec fall, the power supplies are expected to track the reference better. This is shown in Fig. 9.

Fig. 9 Tracking error for unit 1

The tracking between supplies remains almost the same regardless of the change in fall time. This is shown in Fig. 10.

Fig. 10 Dual supplies tracking error profile

CONCLUSIONS

The use of two test functions and a PC-based measuring system has sped and simplified the verification of the tracking performance of the SNS Fast Injection Bump power supplies. The general tracking ability of the power supplies is checked with a pulse having a 1millisec fall. The worst case tracking is checked with a pulse having a 250microsec fall. The tracking results indicate that the first two production units satisfy SNS application requirements.

REFERENCES

- [1] S. Dewan, et. al., "1.12 MVA Peak Two Quadrant Pulse Switch Mode Power Supply for SNS Injection Bump Magnet", Proceedings of EPA2002, Paris, France.

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