Operating Experience with High Beta Superconducting RF Cavities

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Operating Experience with High Beta Superconducting RF Cavities*

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Abstract

The number of installed and operational $\beta=1$ superconducting rf cavities has grown significantly over the last two years in accelerator laboratories in Europe, Japan and the U.S. The total installed acceleration capability as of mid-1993 is approximately 1 GeV at nominal gradients. Major installations at CERN, DESY, KEK and CEBAF have provided large increments to the installed base and valuable operational experience. A selection of test data and operational experience theretofore to date is reviewed.

I. INTRODUCTION

Superconducting Radio-Frequency (SRF) cavities for speed of light particles ($\beta=1$) are playing an increasing role in high energy and nuclear physics accelerators worldwide. As more cavities are manufactured, tested, and put into service, the breadth and depth of operational experience is growing. Installed acceleration capacity is approximately 1 GeV and a total of about $10^6$ cavity-hours of operation has been accumulated. Figure 1 shows the time history of installed SRF acceleration capacity.

![Figure 1. History of installed SRF acceleration capacity.](image)

The range of parameters spanned by the cavities in use is substantial. Cavities are constructed either of solid niobium or niobium sputtered onto formed copper. They are operated between 1.8 K and 4.5 K. Frequencies range from 352 MHz to 3000 MHz. Beam currents range up to 70 mA. Gradients in laboratory tests of production cavities range from 5 to 20 MV/m. Once these cavities are installed in cryostat systems, additional constraints due to the system interlocks and the interfaces result in system gradients ranging from 3 to 12 MV/m.

Several accelerator SRF projects are complete and operational: Stanford's HEPL, KEK's TRISTAN, Darmstadt's S-Dalinac, DESY's HERA, and CERN's SPS. Accelerator projects using SRF that are under construction and have some operational experience are CEBAF, CERN's LEP, Saclay, and Frascati. Possible future applications include TESLA [13], spallation neutron sources and FEL drivers. See also Table 1.

This paper presents a summary of present performance and experience of the installations worldwide. Topics include operational aspects of the cavities and their peripheral hardware. Particular emphasis is placed on CEBAF's experience with SRF cavities because the authors are closest to it and because the number of units at CEBAF is about 80% of those now installed worldwide.

II. OPERATIONAL EXPERIENCE WITH SRF

A. Tristan (KEK)

This system comprises thirty-two 508 MHz cavities installed in pairs in 16 cryostats and operated at 4.5K.[1] Total active length is 47.2 m. In pre-operational testing, the average gradient was 7 MV/m, while in operation this drops to 3.2–4.7 MV/m. 400,000 cavity-hours of operation with beam have been accumulated. Operational problems at startup included vacuum leaks at beam pipe indium joints, since solved, and coaxial coupler ceramic punch throughs. There have been some difficulties with the piezoelectric devices used to tune the cavity frequency within the cryostat. One cavity experienced heating due to synchrotron radiation and so did not perform as anticipated until an intercept was installed.

B. DESY

The HERA electron ring includes sixteen, 500 MHz cavities in eight cryostats, totaling 19.2 active meters. The operating temperature is 4.4 K. In pre-operational testing, the average gradient was 6 MV/m, while in operation this drops to 4 MV/m. 160,000 cavity-hours of operation with beam have been accumulated. Operational problems at startup included Q degradation with slow cooldown.[2] This "Q-disease" was determined to be due to hydride formation in the temperature range 70–170 K. A fast cooldown from 170 K to below 70 K eliminates the difficulty, but this can be difficult for some machines due to cryogenic system limitations. [3] Raising the temperature to 200 K for two hours redistributes the hydrogen and Q is often restored. [4] High temperature heat treatment above 1200 °C eliminates the problem and in laboratory experiments anodization of the niobium surface considerably reduced the Q-degradation.[3, 5]

C. Darmstadt

S-Dalinac includes ten and one quarter 3000 MHz 20-cell cavities in two cryostats, totaling 10.25 active meters.[6] (Fractional cavities have fewer than the standard number of cells for a given machine.) The operating temperature is 1.8 K. In operation, the average gradient is 5.6 MV/m.

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43,000 cavity-hours of operation with beam have been accumulated. Some of the cavities have lower Q than expected. This, coupled with refrigeration limitations, has led the system to be operated at less than design energies. Replacement cavities are due to be installed shortly.

D. Saclay

MACSE includes five 1500 MHz cavities in two and a half cryostats, totaling 2.5 active meters, operating at 1.8 K.[7] (Fractional cryostats have fewer than the usual number of cavities for a given machine.) In operation the average gradient is 12 MV/m. Operational problems at startup included a cold sapphire rf window failure.

Saclay has made great strides in closed loop chemical treatment and cleaning systems for SRF cavities. Results have been excellent, with gradients on test cavities ranging to 28 MV/m.[8]

E. CERN

LEP 200 is the on-going upgrade of the LEP accelerator system with SRF cavities to double the available particle energy. The installation will consist of 192 cavities in 48 cryostats operating at 352 MHz.[9] The operating temperature is 4.5 K. As of May 1993, twelve cavities in three cryostats have been installed and operated with beam. This represents 20.4 m of active length, about 6% of the total planned (326 m). In pre-operational testing, the average gradients were 5–6 MV/m, while in operation this drops to 3.5–5.5 MV/m. By contract, the vendors are allowed 20% maximum degradation between vertical test and tunnel horizontal cryostat test results.

30,000 cavity-hours of operation with beam have been accumulated. Startup problems include difficulties with coaxial input power couplers and HOM output couplers.

F. CEBAF

CEBAF now has 113 active meters installed for operation at 2K; upon completion in December 1993 it will comprise 169 active meters. The machine will include 338 cavities operating at 1497 MHz in 42 1/4 cryostats. In pre-operational testing, the average gradients at field emission onset are 7.5–10 MV/m, while in operation in the horizontal cryostat usable gradient is 5–7.5 MV/m. 140,000 cavity-hours of operation with beam have been accumulated.[10] One cryomodule was pushed to an average gradient of 8 MV/m with beam. Operational problems at startup include system performance limited by refrigeration capacity until the 2K cold compressor system functions (expected in late 1993). It appears that consistent system operation above 7.5 MV/m will require rf conditioning of the waveguide transition from room temperature to 2 K and better understanding of the interactions among the hardware interlocks monitoring performance.

III. CURRENT STATE OF THE ART

Significant advances are being made in pushing cavity performance, as reported in several papers at this conference. Proch reviewed this area in these proceedings, [11], so only highlights will be given here. More work is needed: the usable gradient assumed for the contemplated European Electron Machine is 10 MV/m at Q ≥ 4 × 10^9.[12] The usable gradient goal for the cavities being fabricated for the TESLA Test Facility is 15 MV/m at Q ≥ 5 × 10^9. TESLA itself will require a usable gradient of 25 MV/m at the same Q.[13]

The best production (5-cell) cavity at CEBAF reached 20 MV/m gradient in the vertical test dewar. No special care was taken in preparing this cavity; it represents the outlier of the distribution. This result is shown in Figure 2. One cavity in the CEBAF production run was specially treated, and achieved 20.5 MV/m. On initial testing (standard processing) this latter cavity reached 16 MV/m without field emission.

It was subsequently annealed at 1400°C in an UHV furnace with titanium as a solid state getter, chemically etched and rinsed with water at moderate pressure (10 MPa). [14] Cornell reported at this conference results on a 9 cell cavity at 3 GHz which achieved 30 MV/m.[15] For CEBAF, the surface field is 2.56 times the accelerating field, while the ratio is 2.1:1 for the Cornell cavity.

![Figure 2. Performance of two CEBAF cavities](image)

IV. CEBAF CAVITY TESTING

At CEBAF, the basic unit of the accelerating structure is a hermetically sealed pair of cavities. The cavities are chemically etched, rinsed with high purity water and alcohol (isopropanol or methanol), assembled in a class 100 clean room with the necessary auxiliary hardware, and evacuated; all within a five hour period. The cavity pairs remain under vacuum thereafter. Each cavity pair is hung from a dewar lid, connected to variable coaxial couplers, and subjected to a full rf performance test at 2 K in a vertical dewar. This has proved advantageous compared to procedures during which cavities have to be exposed to atmosphere after initial testing, raising the chances of introduction of particulate contamination.

As of May 1, 1993, 250 cavities had been assembled into pairs and tested. CEBAF defines usable gradient as the lower of the gradient with 1 W of field emission dissipation or the quench gradient less 1 MV/m. Using this definition, the average usable gradient achieved was 9.4 MV/m at Q = 7 × 10^9 versus 5 MV/m at 2.4 × 10^9 specified. In vertical test, gradient was limited by the following mechanisms: 5% quench without any field emission, 35% quench with field emission and 60% field emission sufficient to exceed
available rf power (80 W) or a self-imposed radiation limit. In Figure 2 we show the Q versus E plots of two cavities, a typical unit with field emission loading at moderate gradients and the best production cavity to date, with field emission beginning at 12 MV/m and a thermal-magnetic quench at 20.1 MV/m with 46 W power dissipation, about half in field emission. In Figure 3 we show field emission onset gradients versus time. It is noteworthy that the standard deviation of the field emission onset gradient and usable gradients has not changed since production began: $\sigma \approx 3$ MV/m has remained constant while the average gradients increased by 50%. The source of this performance spread is not understood. A cavity fabrication and performance database is being assembled for further trending and feedback to cavity performance, but no variable examined to date has correlated well with the width of the distribution. This effort will continue after the cavity pair production is complete to provide information to the accelerator community.

![Graph of field emission onset gradients versus time for CEBAF cavity production](image)

Figure 3. Gradient at field emission onset versus time for CEBAF cavity production.

The cavities which did quench without field emission did so with a spread in gradients of 8 to 18 MV/m. This is sufficient data to indicate that the niobium used in the CEBAF cavities, with RRR=250 as supplied and RRR=200 as welded, does not yet provide the thermal stability needed for $E_{\text{acc}} > 15$ MV/m as desired for future accelerators. Even the titanium gettered cavity cited above, with an RRR>800, was limited to 20.5 MV/m. More work on the basic materials used in cavities is clearly needed.

V. SRF CAVITY FIELD EMISSION LIMITATION

As mentioned above, only about 5% of the CEBAF cavities show no field emission loading, i.e., have a flat Q profile until quench. There are two types of electron loading in cavities, resonant (multiacting) and non-resonant (field emission). The first is reasonably well understood and can be eliminated by proper cavity shaping.[16] Non-resonant electron loading is due to both intrinsic and extrinsic impurities of the niobium surface. Field emission loading needs to be limited to minimize radiation damage to coupler ceramics which can result in vacuum leaks and to minimize radiation damage to the niobium itself.

CEBAF has steadily improved its average gradient at field emission onset over time by careful rinsing and attention to clean assembly techniques. The data shows that much improvement is still possible, and many techniques are being investigated in labs around the world. High pressure (10 MPa) water rinsing has shown great promise at CERN [17] and CEBAF [14]. Cornell has also successfully applied high power pulsed processing to eliminate (by explosion) field emission sites.[18] Cornell [19] and Wupertal [20] have shown that heat treatment in a UHV furnace above 1200 °C can also reduce field emission. Of these techniques, the high pressure rinsing is the easiest to implement and therefore the most likely to enter manufacturing service soon.

VI. SRF PERFORMANCE LIMITATIONS IN ACCELERATORS

One has to make a clear distinction between the fundamental capability of the SRF cavity technology and its practical application in an accelerator environment. For the group of people dealing with cavities alone, it is important to stretch the performance of a cavity to its limit. The results of such tests, generally done under well controlled conditions in a vertical configuration without beam, point towards fundamental performance limitations: anomalous losses caused by defects, thermal-magnetic breakdown, or field emission loading. In the accelerator environment, often the prior performance of the cavities cannot be repeated due to external constraints which are not present in the well controlled vertical tests. Among these are power handling problems (rf heating and outgassing) in external waveguides (CEBAF), rf power limitations due to low Q external (CEBAF), insufficient masking of synchrotron radiation (KEK), limitations in cryogenics due to high rf losses (Q-disease, HERA) and non-performing (incomplete) cryo-systems (CEBAF).

At CEBAF, there are several interlocks installed in the cavity cryostats to protect the system. At the present time, since there is little operating experience, these are set very conservatively. Most of these monitor the waveguide between the warm and cold rf windows. There is a phototube which senses the light from arcs in the waveguide. If light is seen for more than 50 μs, the rf is shut off. There is a thermopile which monitors the IR radiation in the waveguide. If this sensor goes above a set point which corresponds to about 50 °C on a warm polyethylene window, the rf is shut off. The ion pump on this waveguide section is monitored and the rf shut off if the pressure exceeds $10^{-7}$ torr. Finally, the cavity is administratively limited to 1 W of field emission loading as measured calorimetrically. With all these constraints, the first 12 cryomodules at CEBAF (96 cavities) averaged 7.2 MV/m usable gradient versus a specification of 5 MV/m. Within the allowed dynamic heat load of 45 W, the average gradient is 6.5 MV/m. Cavity performance has continued to improve and these values are expected to increase for the entire machine when installed and commissioned. Further increases are expected as the waveguide is conditioned and the machine is better understood, allowing some interlocks to be relaxed.
Net performance of a cavity necessarily diminishes as more and more requirements and support equipment are considered. This has little to do with actual degradation of the cavity, and more to do with the fact that a chain is only as strong as its weakest link. We note in passing that the design specification for CEBAF cavity operation is 5 MV/m with Qo\geq2.4 \times 10^9, and that neither typical cavities nor their supporting hardware has any problems operating at that level. Subsystems and infrastructure start to show their limits when asked to perform at 150% of specifications and higher, although the CEBAF cavities (on average) are capable of operation at about 200% of specifications. In Figure 4 we compare vertical test performance with tunnel commissioning performance for 125 cavities, while in Figure 5 we remove the 47 cavities constrained in the tunnel by interlocks from the comparison.

VII. HIGHER ORDER MODE POWER EXTRACTION

Higher order modes (HOMs) must be adequately damped to prevent various forms of beam breakup. Different accelerators have different requirements, and the problems increase with increasing beam current, decreasing rf bucket length, increasing number of passes, and decreasing time between bunches.

High current machines such as storage rings generate large amounts of HOM power. TRISTAN, in fact, has problems with power handling on the HOM output coupler, and has had to replace the couplers. Low current machines like CEBAF, on the other hand, will only dissipate a fraction of a watt of HOM power (0.25 W per 5-cell cavity at a beam current of 1 mA). The heat load involved in couplers to take this power out to room temperature or even a thermal shield at 40–80K would exceed the power in the modes themselves, and therefore CEBAF has HOM loads inside the cryostat at 2 K. Materials requirements for these loads were themselves something of a challenge.

Operational measurements of the damping of HOMs in CEBAF cavities with beam indicate that the beam breakup (BBU) threshold is about 14 ma, which is 70 times the design current. Future SRF accelerator projects, such as CERN LEP-II, Cornell B-factory, and FEL drivers, will have HOM damping and power handling requirements more severe than those of accelerators in operation today, and research to advance the technology is underway.

VIII. COUPLER CERAMICS

As mentioned above, several laboratories have had trouble with arcing and breakdown of coupler ceramics, leading to reduced power handling limits or vacuum leaks through the ceramics. As a result, many laboratories are contributing to the knowledge base on breakdown properties of ceramics, in particular high purity alumina. There are at least two distinct phenomena related to the interaction of ionizing radiation with the ceramics. Glass (SiOₓ) impurities must be minimized because radiation dosage leads to decomposition and formation of vacuoles which increase permeation rates and can eventually link up to form a true leak. Ionizing radiation can also cause surface flashover. The second phenomenon has been seen at CEBAF. These phenomena may be the cause of small (\sim 10^{-8} \text{ atm-cc/s}) vacuum leaks which are infrequently found in the CEBAF cold rf window ceramic after vertical test.

Multipacting has been identified as a source of rf window failure and antimultipacting coatings, such as TiN, TiO₂ or Cr₂O₃, are routinely applied to ceramic rf windows. Coatings with controlled resistivity, designed to provide some charge drainage while minimizing rf loss in the coating, are under development. Gold and other impurity dispersions in the antimultipacting coatings cited appear promising.

Above all, good surface preparation, cleaning and handling procedures are mandatory.
IX. CAVITY VACUUM INTEGRITY

Cavity vacuum integrity has been a problem for the field because of the sensitivity of the indium sealed niobium flanges to surface preparation. A recent technique developed at CEBAF has increased the sensitivity for measuring the vacuum integrity of cavity assemblies.[26,27] Since the cavity pairs are submerged in liquid helium for roughly a day, an integrated leak test provides great sensitivity. In the CEBAF cavity pairs there are 16 indium joints (4.75m) and 4 copper knife edge seals. The average integrated leak rate for 80 pairs was 5.8 x 10^-11 atm-cc/s.

X. SUMMARY

Superconducting rf technology is finally maturing as a reliable and cost effective means of accelerating high quality particle beams. Significant operational experience is being clocked now and will double in the next year. Performance is also improving, with production cavity gradients of 10-20 MV/m in vertical test and 5-12 MV/m when installed in accelerators and subject to additional systems requirements. Significant progress has been made on key technical issues which can limit performance and reliability, including HOM power extraction, cavity assembly vacuum integrity, and power input couplers. Additional work is needed on the last item as power handling requirements increase to the MW level.

XI. ACKNOWLEDGMENTS

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XII. REFERENCES

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[10] A. Hutton, these proceedings.
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Table 1 - Machine Parameters

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