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QUARTERLY REPORT
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**NUMERICAL STUDY OF THE FLOW OF
GRANULAR MATERIALS DOWN AN INCLINED
PLANE USING A MODEL BASED ON A KINETIC
THEORY APPROACH**

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SUMMARY

In the previous report the linearized stability results for the flow of granular materials down an inclined plane, modeled by a constitutive theory based on the kinetic theory approach [cf. Richman & Marciniec (1990)] were presented. In this report, we derive the governing equations for the flow of granular materials down an inclined plane, modeled by the constitutive theory proposed by Boyle and Massoudi (1990). The governing equations obtained will be solved numerically to obtain the basic solutions.

INTRODUCTION

Kinetic theory approaches in the formulation of rapid flows of granular materials have attracted considerable attention in recent years. There are several models which have been suggested to describe the rapid flow of granular materials which are derived using a statistical approach. Boyle and Massoudi (1989) have written comprehensive survey article of the constitutive equations and the laws governing the flow of granular material. A major difference between the continuum theories discussed previously and the theories based on a statistical approach is the concept of "granular temperature" which is introduced in the latter approach. Granular temperature describes the fluctuating velocity of the flow of granular solids and in this sense is similar to the temperature in a gas due to fluctuating motion of the gas particles. However, it is not clear how this quantity can be measured. Several models have been proposed by various investigators using ideas of kinetic theory.

GOVERNING EQUATIONS

Boyle and Massoudi (1990) proposed a model which can exhibit normal-stress effects by including the effects of the gradient of the volume distribution function, which is the noticeable difference between the model proposed by Lun, Savage and co-workers (1984).

The granular stress tensor \mathbf{T} is the sum of the two terms, reflecting that momentum can be transported by the uninterrupted streaming of granules \mathbf{T}_k and by the essentially instantaneous transport from one center to another during a collision \mathbf{T}_c . The granular stress tensor \mathbf{T} follows from that of Lun et al. (1984), but there is an additional contribution to \mathbf{T} that is given by

$$\mathbf{T}_m = \frac{4}{5} \eta g_0 \rho \theta v \frac{V_0^{*2} \bar{\sigma}^2}{(1 - v V_0)^2} (2 \mathbf{M} + \pi \mathbf{M} \mathbf{1}) \quad (1)$$

The stress tensor for a rapidly sheared granular material is found by summing the above individual contributions, which is given by

$$\begin{aligned}
\mathbf{T} = & \left\{ \rho \theta (1 + 4 \eta v g_0) + \left(\frac{2 \mu}{3 \eta (2 - \eta) g_0} (1 + \frac{8}{5} \eta v g_0) \right. \right. \\
& \left. \left. \left\{ 1 + \frac{8}{5} \eta (3 \eta - 2) v g_0 \right\} - \frac{3}{5} \mu_b \eta \right) \nabla \cdot \mathbf{u} \right. \\
& \left. + \frac{4}{5} \eta v g_0 \rho \theta \frac{V_0^{*2} \bar{\sigma}^2}{(1 - v V_0^*)^2} \pi \mathbf{M} \right\} \mathbf{1} \\
& - \left\{ \frac{2 \mu}{\eta (2 - \eta) g_0} (1 + \frac{8}{5} \eta v g_0) \left[1 + \frac{8}{5} \eta (3 \eta - 2) v g_0 \right] + \frac{6}{5} \mu_b \eta \right\} \mathbf{D} \\
& + \frac{8}{5} \eta g_0 \rho \theta v \frac{V_0^{*2} \bar{\sigma}^2}{(1 - v V_0^*)^2} \mathbf{M}
\end{aligned} \tag{2}$$

$$\text{where, } \mu_b = \frac{256 \mu v^2 g_0}{5 \pi}$$

$$\mu = \frac{5 m}{16 \bar{\sigma}^2}$$

$$V_0^* = \frac{6 V_0}{\pi \bar{\sigma}^3}$$

$$\mathbf{M} = \nabla \mathbf{v} \otimes \nabla \mathbf{v}$$

$$\eta = \frac{1}{2} (1 + e)$$

$$g_0 = \frac{V_0^*}{4(1 - v V_0^*)}$$

V_0 represents the volume per neighboring particle, and \mathbf{D} is the stretching tensor. Also ρ is the bulk density, v is the volume fraction, θ is the granular temperature, e is the coefficient of restitution, $\bar{\sigma}$ is the diameter of the spherical particles and m is the mass.

Consider the flow of granular materials modeled by the above model down an inclined plane (cf. Figure 1) due to the action of gravity [Savage (1979), Johnson and Jackson (1987), Johnson, et al. (1990), Hui, et al. (1984), Richman and Marciniak (1990),

Hutter, et al. (1986a, b)]. In this problem we consider steady one dimensional flow of incompressible granular materials (*i.e.* $\rho_p = \text{constant}$) down an inclined plane, where the angle of inclination is α . The governing equations of motion are the conservation of mass and momentum. We assume that the granular temperature is constant and the volume fraction, velocity to be of the form

$$\begin{aligned} v &= v(y) \\ u &= U(y)i \end{aligned} \quad (3)$$

For the above flow field, the conservation of mass is automatically satisfied. From the balance of linear momentum we have

$$\begin{aligned} \frac{6 E_6 V_0^* v^2}{(1-v V_0^*)^3} \frac{dv}{dy} \frac{d^2v}{dy^2} + \frac{3 E_6 V_0^* v (2+v V_0^*)}{(1-v V_0^*)^4} \left\{ \frac{dv}{dy} \right\}^3 \\ \left\{ E_1 + \frac{E_2 V_0^* v (2-v V_0^*)}{(1-v V_0^*)^2} \right\} \frac{dv}{dy} = -\gamma g v \cos \alpha \end{aligned} \quad (4)$$

$$\begin{aligned} \left\{ \frac{6 E_3 (1-v V_0^*)}{V_0^*} + \frac{3 E_4 v}{2} + \frac{E_7 V_0^* v^2}{8 (1-v V_0^*)} \right\} \frac{d^2U}{dy^2} + \left\{ \left(\frac{3 E_4}{2} - 6 E_3 \right) \right. \\ \left. + \frac{E_7 V_0^* v (2-v V_0^*)}{4 (1-v V_0^*)^2} \right\} \frac{dv}{dy} \frac{dU}{dy} = -\gamma g v \sin \alpha \end{aligned} \quad (5)$$

The equations (4) and (5) are to be solved subject to appropriate boundary conditions. for this problem, they are:

$$U = 0 \quad \text{at } y = 0 \text{ (on the inclined plane)} \quad (6)$$

$$Q_3 = \int_0^L v \, dy \quad (7)$$

and,

$$\frac{dU}{dy} = 0 \quad (8)$$

$$v = 0 \quad \text{at } y = L \text{ (at the free surface)} \quad (9)$$

The system of equations subject to the boundary conditions are non-dimensionalized by

$$\bar{y} = \frac{y}{L}; \quad \bar{U} = \frac{U}{u_0} \quad (10)$$

where L is the characteristic length and u_0 is the reference velocity. Now, the above system equations reduces to

$$\begin{aligned} \frac{2 D_3 v^2}{(1-vV_0^*)^3} \frac{dv}{d\bar{y}} \frac{d^2 v}{d\bar{y}^2} + \frac{D_3 v (2+v V_0^*)}{(1-vV_0^*)^4} \left\{ \frac{dv}{d\bar{y}} \right\}^3 \\ + \left\{ D_1 + \frac{D_2 v (2-vV_0^*)}{(1-vV_0^*)^2} \right\} \frac{dv}{d\bar{y}} = -v \cos \alpha \end{aligned} \quad (11)$$

$$\begin{aligned} \left\{ D_4 (1-vV_0^*) + D_5 v + \frac{D_6 v^2}{(1-vV_0^*)} \right\} \frac{d^2 \bar{U}}{d\bar{y}^2} \\ + \left\{ D_5 - D_4 V_0^* + \frac{D_6 v (2-vV_0^*)}{(1-vV_0^*)^2} \right\} \frac{dv}{d\bar{y}} \frac{d\bar{U}}{d\bar{y}} = -v \sin \alpha \end{aligned} \quad (12)$$

and the boundary conditions become

$$\bar{U} = 0 \quad \text{at } \bar{y} = 1 \text{ (on the inclined plane)} \quad (13)$$

$$N = \int_0^1 v d\bar{y} \quad (14)$$

and,

$$\frac{d\bar{U}}{d\bar{y}} = 0 \quad (15)$$

$$v = 0 \quad \text{at } \bar{y} = 1 \text{ (at the free surface)} \quad (16)$$

$$\begin{aligned} D_1 = \frac{E_1}{L \gamma g}; \quad D_2 = \frac{E_2 V_0^*}{L \gamma g}; \quad D_3 = \frac{3 E_6 V_0^*}{L^3 \gamma g} \\ D_4 = \frac{6 E_3 u_0}{L^2 \gamma g V_0^*}; \quad D_5 = \frac{3 E_4 u_0}{2 L^2 \gamma g}; \quad D_6 = \frac{E_7 u_0 V_0^*}{8 L^2 \gamma g} \end{aligned} \quad (17)$$

where,

$$\begin{aligned}
E_1 &= \gamma \theta, & E_2 &= \gamma \theta \eta \\
E_3 &= \frac{2 \mu}{3 \eta (2-\eta)}, & E_4 &= \frac{16 \mu (3\eta-1)}{15 (2-\eta)} \\
E_5 &= \mu \eta \left\{ \frac{128 (3\eta-2)}{75 (2-\eta)} - \frac{768}{25 \pi} \right\} \\
E_6 &= \frac{4}{5} \gamma \theta \eta \bar{\sigma}^2 V_0^2 \\
E_7 &= \mu \eta \left\{ \frac{128 (3\eta-2)}{25 (2-\eta)} + \frac{1536}{25 \pi} \right\}
\end{aligned} \tag{18}$$

Results and Discussion

The system of equations (11) and (12), with the boundary conditions (13), (14), (15) and (16) will be solved numerically using a collocation code COLSYS [cf. Ascher et al. (1981)]. A parametric study for the volume fraction and velocity profiles will be carried out for the base solution and the results will be presented in the next report.

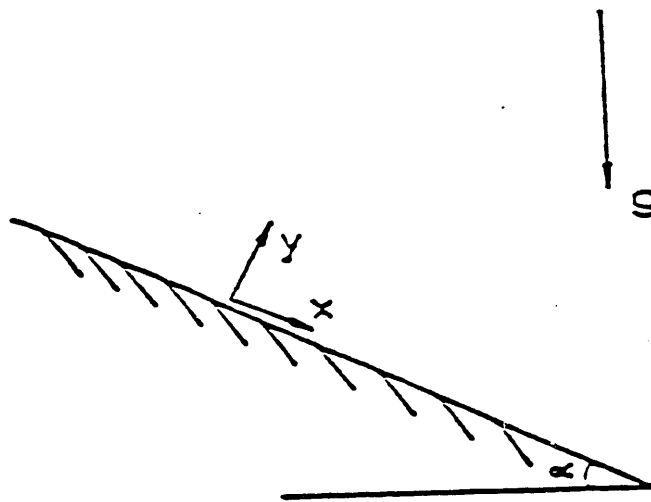


Figure 1. Flow Down An Inclined Plane

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