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PRATT & WHITNEY AIRCRAFT DIVISION
CONNECTICUT OPERATIONS - CANEL
WELDING & BRAZING DEVELOPMENT GROUP
ADVANCED TOOL ENGINEERING

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02

Interim Report - Project 1047

June 17, 1959

Bonding of Tantalum

Object:

This investigation was undertaken to determine the necessary requirements for obtaining sound bonded joints on tantalum.

Equipment:

- P & H 300 amp Arc Welder - TIG
- Sciaky 50 KVA Resistance Welder
- Vacuum Chamber
- Plastic Bag Chambers
- Tantalum Sheet - XM-238A - 1/16" Thick

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Summary:

Corrosion and Mass Transfer Loops LTM 237A and 427 called for fabrication of 430 stainless steel clad tantalum tubing. Since there was little or no experience at welding this material at CANEL, specimens were welded using vacuum chambers and plastic chambers as normally used for loop fabrication. XM-238A material was used for this work, which was vacuum arc cast and cold rolled from three inch minimum diameter ingots.

Tantalum, like other refractories, has a strong affinity for oxygen, nitrogen, the halogens, carbon monoxide and water vapor at temperatures between 600°F and 2200°F. Degasing can be accomplished at temperatures above 3300°F in vacuo. Hydrogen causes embrittlement. It is soluble in hydrofluoric acid, strong alkalis and solutions containing free sulfur trioxide.

Carbon arc welding under a liquid cover of carbon tetrachloride is described in literature, however, attempts to reproduce this method at CANEL were unsuccessful. The main reason being that the liquid rapidly clouds up to the extent that the joint cannot be followed. Adequate ventilation must be provided to carry off the noxious fumes produced by this process.

Resistance welding was performed without the use of a special atmosphere producing sound bonds. See Fig. III.

TABLE I

<u>Spec.</u>	<u>Joint</u>	<u>Weld Method</u>	<u>Remarks</u>
4	Lap - 1/16 Sheet	Spot Weld 50 KVA - 65% Phase Shift Cool Cycles 3 Heat Cycles 10 Squeeze Cycles 3 Impulses 3 600# Constant High Pressure	Diffusion Type Bond Grain Size Base - Cold Worked Structure Nugget - ASTM 5-6
5	Lap - 1/16 Sheet	Same as above	Shear Strength - 51,000 PSI

Butt joints were fusion welded both in vacuum chambers and plastic bags. Specimens were degreased and pickled for six minutes in a solution of 16% hydrofluoric and 20% nitric acids, prior to welding. Specimens were then X-Rayed and metallurgically examined. See Fig. I and II.

TABLE II

<u>Spec.</u>	<u>Joint</u>	<u>Weld Chamber</u>	<u>X-Ray</u>	<u>Remarks</u>									
6	1/16 Sheet Butt	Vacuum-Argon	No Defects	Incomplete penetration									
7	"	"	"	"									
8	"	"	"	"									
9	1/16 Sheet Butt .020 Filler	Plastic-Argon	No Defects										
10	1/16 Sheet Butt .032 Filler	Plastic-Argon	No Defects	Weld sound and clean - small amount of second phase in spheroidal form dispersed through matrix of weld. Grain Size <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td>Base</td><td>HAZ</td><td>Weld</td></tr><tr><td>Cold worked</td><td>2 to >1</td><td>>1</td></tr></table> Hardness-DPH <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td>219</td><td>146</td><td>142</td></tr></table>	Base	HAZ	Weld	Cold worked	2 to >1	>1	219	146	142
Base	HAZ	Weld											
Cold worked	2 to >1	>1											
219	146	142											
11	1/16 Sheet Butt	Plastic-Argon	No Defects										
12	1/16 Sheet Butt Welded both sides	Vacuum-Argon	No Defects										
13	"	"	Poor Fusion										
14	1/16 Sheet Butt Braided 1/64 Filler both sides	"	Porosity	A few small voids									
15	1/16 Sheet Butt Braided 1/64 Filler	"	No Defects	Machined weld was bent through 180° flat against itself									
16	1/16 Sheet 1/32 Filler Welded both sides	"	No Defects	Same as Spec. #10 Grain Size <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td>Base</td><td>HAZ</td><td>Weld</td></tr><tr><td>Cold worked</td><td>4 to >1</td><td>>1</td></tr></table> Hardness-DPH <table border="1" style="display: inline-table; vertical-align: middle;"><tr><td>219</td><td>149</td><td>130</td></tr></table>	Base	HAZ	Weld	Cold worked	4 to >1	>1	219	149	130
Base	HAZ	Weld											
Cold worked	4 to >1	>1											
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17	"	"	No Defects	Tensile Tested 62,000 PSI									

Specimens were brazed with Coast Metals #52 and Microbraz 130 in helium. Flow with Microbraz 130 was poor while Coast Metals 52 produced a sound joint although ductility was poor.

TABLE III

"T" Joint	Pickle	Braze Filler	Braze Temp.	Time at Temp.	Atmos.	Results
1	16 HF 20 HNO ₃ 64 H ₂ O	NR 130	1925	10 min.	He	Poor flow, very brittle.
2	"	"	"	15 min.	He	Poor flow, braze very porous. Brittle.
3	"	CM 52	"	15 min.	He	Fair to good flow. Sound strong joint. Good Fillet. Poor ductility. Max. dilution 1 1/2 Mils

Physical Data:

Melting Point 5425° F
 Annealing temperature above 1920° F in vacuo
 Outgassing temperature above 3300° F in vacuo
 Thermal expansion 3.6 x 10⁻⁶ in/in/°F
 Tensile Strength
 Sheet, annealed 50,000 PSI
 Sheet, worked 110,000 "

Chemical Specifications - XH-238A
 Carbon 200 PPM Hydrogen 10 PPM Iron 50 PPM
 Oxygen 100 " Nitrogen 30 " Tantalum Bal.

Conclusions:

No difficulties are anticipated in tantalum to itself in loop applications. Atmosphere purity precautions similar to those currently employed when welding other refractory metals should be adhered to. Chill bars can be used to advantage to reduce grain growth and the extent of heat affected zones. This is demonstrated by comparing Figures I and II where the latter specimen utilized chill bars. There was no appreciable difference between welds made in vacuum chambers and plastic chambers. The main fault in weld joints was the frequent lack of complete penetration, attributable to the operators inexperience with this high melting metal.

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TANTALUM
BUTT WELDED IN PLASTIC CHAMBER
0.062 SHEET



MAGNIFIED: 16X

PROJ. 1047
FIG. 1

2

4

5

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TANTALUM
BUTT WELDED BOTH SIDES IN VACUUM CHAMBER
0.062 SHEET

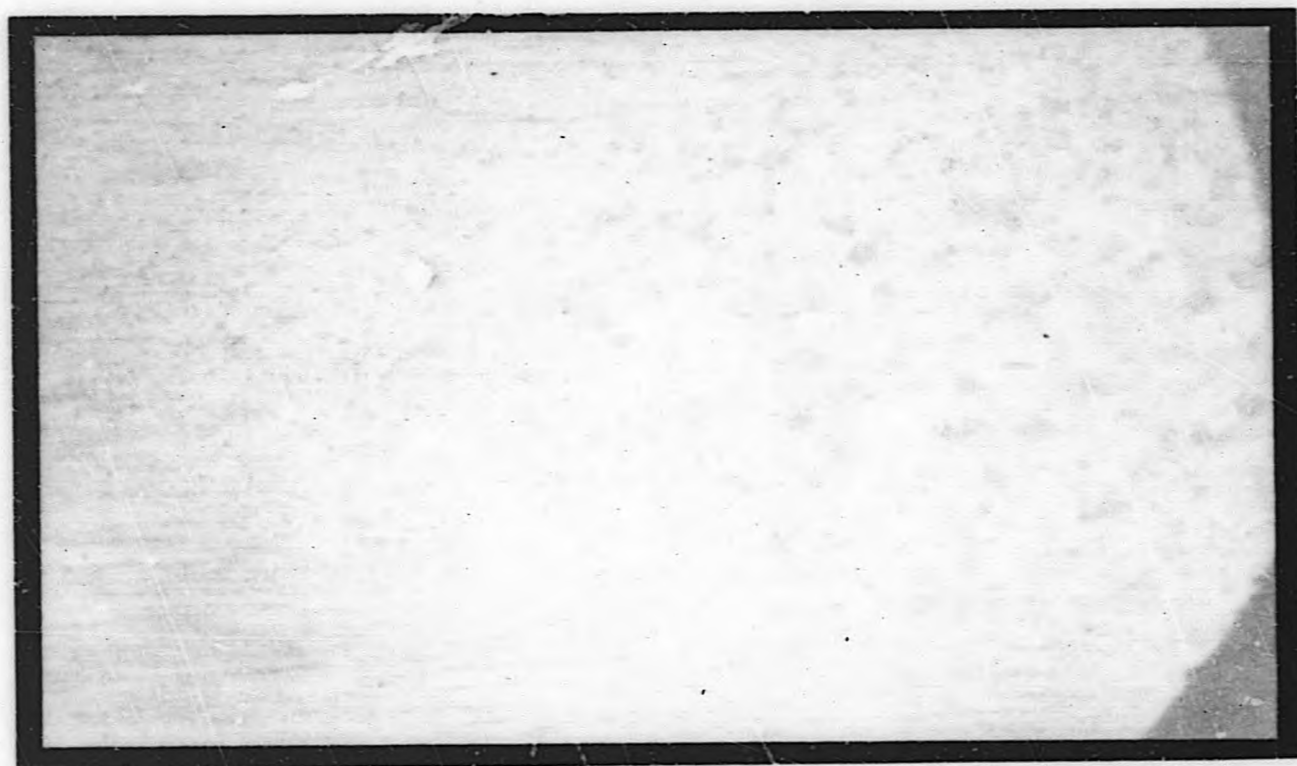


MAGNIFIED: 16X

PROJ. 1047
FIG 2

2
4
6

TANTALUM SPOT WELD - 0.062 SHEET



MAGNIFIED: 50X

PROJ - 1047
FIG 3

C-19-2

2
7

END