NENORATORI LABORATORI

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SUBJ BOT :	Accuracy of	Relater	tion	

We consider here the accuracy of relexation lengths measured during the vater-uranium lattice experiments. Since such an analysis for all measurements would take a great deal of time, we have applied it to just one lattice. This one (2:1 water-to-metal ratio) was aboven completely at rendom.

We define three separate measures of the error in an individual relaxation length. These are:

> The probable error associated with the least squares fit of an exponential to the measured fluxes. We call this SL.

- (2) The probable error as derived from statistical considerations of the accuracy to which foils were counted. This we call ΔL.
- (3) The standard deviations of the measured relaxation lengths from the values predicted by least-squares fits to B² and A. These we term dL.

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If the major contribution to the size of δL comes from the statistics of flux measurements, we should expect that δL and ΔL will be comparable. In other words, the quantity

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SL - AL

should be negative about as often as it is positive. An example of a seuse which would upset this belance is changing counter consitivities during foil counting. Another cause might be improper taking into account of end corrections during calculation of L from the flux levels.

(1)

(2)

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dL is a measure of another kind of error. For instance, in our analysis loading to values of B^2 and λ_r we assume that we can replace any geometrical loading shape used by an "equivalent cylinder" having the same total area. If this assumption is poor, we may expect that the quantity

SL - dL

is more often negative then positive. Another cause of such deviation of the sign of (2) from randomness might be a changing reflector savings with loading. Other causes could be varying enrichments or sizes of fuel rods, contamination of the water by neutron absorbers, plating out of cadmium on rods, sto.

In Table I we give the values of \$L, AL, and dL for the relaxation lengths measured with the 2sl lattice. Inspection shows that quantity (1) is positive in eleven cases, and is negative in thirteen cases. I think it can be concluded from this good agreement that our values of L are as good or we have been trying to make them.

On the other hand, the quantity (2) is negative in fifteen instances, and positive in just seven. One would hope for a more equitable distribution.

We have evidence that some at least of this effect derives from our essump tion that any loading can be replaced by its equivalent cylinder. The first

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such evidence appeared strongly during the relaxation length measurements on the 211 lattice. Least squares fits of the L's to B² and λ were consistently poor, the trouble being alsorly associated with the relaxation lengths measured at loadings of 271, 277, and 283 rods. Rerunning these measurements confirmed their L's, which still deviated from the expected values by about two contineters. We then decided to find out if the difficulty was related to the hexagonal 271 rod loading. The relaxation length of the latter was remeasured, with the uranium having a more cylindrical loading. The results were:

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Geometry	
Hexagon	42.998 m
Better cylinder	43-496 m

Remeasurement of the relaxation length of the 283 rod loading in a better cylindrical geometry gave the even more striking results:

Geometrz			
Hexagon + 2 on each side	61.589 m		
Better cylinder	62-605 m		

These changes were so great that we dedided not to use the three loadings involved in the B² determinations.

Inspection of other relexation length measurements" for all lettices shows consistently large values of [dL] for measurements made with hexagonal loadings. As a result, we are not longer using hexagonal shapes, and are in-

"See for instance the memorandum from Chernick to Kaplan, "Analysis of the Clean Bucklings of 1.3 per cent Enriched Uranium-Water Lattices", HML Log No. 0-7027, April 6, 1953.

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stead rounding out all loadings as much as geometry permits.

These geometrical effects are of course understandable. The six corner rods in a hexagonal or nearly hexagonal loading are farther from the center of the loading than are other perimeter rods. Too, they have less uranium near them than do other rods. Thus they contribute less to the reactivity.

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It does not follow that the equivalent cylinder assumption necessarily causes all the excessive negative values of (2). We find conscionally (by remeasurement of suspicious values of L) cases in which apparently too many or too few fuel rods were loaded during a given run, and this must be added as a partial cause. It is known that fuel rod diameters do not vary appreciably, and analysis makes variation of the enrichment factor unlikely. We have looked for plating out of cadmium in the past but have not seen any. Evidence indicates that the water does not become noticeably poisoned with use.

In an attempt to discover how much of the departure from randomness is due to geometrical effects, we have redone the B^2 , λ calculation, leaving out the rod loadings at hexagons and within six rods of hexagons. The improvement in securacy of the least squares fits were marked, the new values being

B² - 61.58 ± .37 x 10-4 cm-2

λ = 6.97 = .07 m

The residuals from this lesst squares fit are shown in Table II. These values lead to four cases with (2) negative, seven with (2) positive, and three cases in which ΔL and |dL| are equal within the securacy of the analysis. Such a distribution is not too unlikely; in fact, it has a P of .27.

Use of the ΔL in Table II leads to expected securacies in B² and λ of # .30 x 10⁻⁴ cm⁻² and .06 cm, respectively. Thus the securacy of the buckling

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fits is quite closely what is expected, when allowance is made for gapmetrical effects.

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The analysis does not seen to lead to discovery of any factors offer than geometrical ones exusing departures from randomness in the least squares fits.

	Table I			
Rota.	-	-SIL	AL	
283 201	62.595 50.860	-175 -152	-544	
201	42.998	-109	.212	208
259 253	37-475 34-586	.321	.218	250
247	32.466	-327	.162	+.016
235 229	28.340 26.944	-105	.125	+.010
223	25.657 23.924	-095	.091	+.144
211 205	23.177	-096	.089	042
199	21.415	-063	.059	+.186
187	19.685	-046	.066	081
175	18.301	-035	.055	+.126
163	16.844	-040	.060	062
145	15.301	-107	.075	+.089
133	14.308	-044	.059	+.113

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