The Electric Energy Savings from New Technologies

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January 1986

**Prepared for the U.S. Department of Energy
under Contract DE-AC06-76RLO 1830**

**Pacific Northwest Laboratory
Operated for the U.S. Department of Energy
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PACIFIC NORTHWEST LABORATORY
operated by
BATTELLE
for the
UNITED STATES DEPARTMENT OF ENERGY
under Contract DE-AC06-76RLO 1830

Printed in the United States of America
Available from
National Technical Information Service
United States Department of Commerce
5285 Port Royal Road
Springfield, Virginia 22161

NTIS Price Codes
Microfiche A01

Printed Copy

Pages	Price Codes
001-025	A02
026-050	A03
051-075	A04
076-100	A05
101-125	A06
126-150	A07
151-175	A08
176-200	A09
201-225	A010
226-250	A011
251-275	A012
276-300	A013

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ABSTRACT

This report was prepared by Pacific Northwest Laboratory for the Office of Coal and Electricity Policy (OCEP), U.S. Department of Energy. The purpose of the report is to provide information about the electricity-saving potential of new technologies to OCEP that it can use in developing alternative long-term projections of U.S. electricity consumption. Low-, base-, and high-case scenarios of the electricity savings for ten technologies were prepared. The total projected annual savings for the year 2000 for all ten technologies were 137 billion kilowatt hours (BkWh), 279 BkWh, and 470 BkWh, respectively, for the three cases.

The magnitude of these savings projections can be gauged by comparing them to the Department's reference case projection for the 1985 National Energy Policy Plan. In the Department's reference case, total consumption in 2000 is projected to be 3319 BkWh. Thus, the savings projected here represent between 4 percent and 14 percent of total consumption projected for 2000. Because approximately 75 percent of the base-case estimate of savings are already incorporated into the reference forecast, reducing projected electricity consumption from what it otherwise would have been, the savings estimated here should not be directly subtracted from the reference forecast.

EXECUTIVE SUMMARY

This report was prepared by Pacific Northwest Laboratory (PNL) for the Office of Coal and Electricity Policy (OCEP), U.S. Department of Energy. The purpose of the study was to provide information about new electricity-saving technologies to the OCEP that it can use in the development of alternative forecasts of U.S. electricity consumption for the fifth National Energy Policy Plan (NEPP).

The project had three specific objectives. The first objective was to collect information about the technical characteristics and costs of ten important new electricity-saving technologies. The second objective was to estimate base, low, and high scenarios of the future potential market, market penetration rate, and impact on aggregate U.S. electricity consumption of each of the ten technologies. These projections were intended to be first-cut or approximate estimates of the potential magnitude of the impacts of these technologies. The third objective was to generate approximate estimates of the average levelized cost per kilowatt hour saved by each technology. These estimates were to be compared to published estimates of the cost of new generating capacity to determine if utility efforts to facilitate penetration of any of the technologies might be a cost-effective alternative to construction of new generating capacity.

These objectives were accomplished by performing three tasks. The first task was to select the ten technologies for detailed analysis. This task was performed in four steps. First, a list of potential electricity-saving technologies for analysis was prepared. Amory Lovins, an international authority on energy-saving technologies, provided a list of some 27 candidate technologies. To his list seven other technologies were added based on a review of the literature on conservation technologies and conversations with a number of experts around the country.

Second, criteria for selecting ten technologies for further analysis from the list of 34 were established. The primary criterion for selection was the electricity-saving potential of the technology, based on previous estimates of potential savings. For each of the three electricity-consuming sectors

(residential, commercial, industrial), only the top five in savings potential were considered for further analysis. The second primary criterion was that the technology be commercially available or expected to be commercially available in the near future. Technologies still in the formulation stage were excluded from further consideration based on this criterion. The third primary criterion was that the technology not yet have a high market penetration. This criterion was imposed because technologies with a high penetration rate would likely already be included in the NEPP forecasting models, and special measures to ensure their consideration to the NEPP forecasts would therefore not be necessary.

The third step of the task was to collect preliminary information related to these criteria about each of the 34 technologies. Most of the required information was obtained from books and reports published by Lovins, DOE, and other energy organizations.

Finally, the fourth step of the selection task was to apply the criteria to the 34 technologies and select ten for further analysis. Four technologies were selected from the residential sector and three each from the commercial and industrial sectors. The ten selected technologies, together with previously published estimates of their electricity saving potential, are listed in Table ES.1. Based on these previous estimates, the total long-term annual savings potential of these ten technologies is 727 BkWh--approximately 22 percent of DOE's NEPP reference case projection of total electricity use in 2000.

The second task was to develop a methodology for projecting the future base-case market potential, market penetration rate, and electricity savings of each of the ten technologies. The methodology was developed based on a review of the technology assessment and market analysis literatures. It is a variant of a method frequently used to project potential sales of a product still in the development stage. The base-case methodology consists of six steps. First, the potential market is estimated. This is defined as the total potential market adjusted to reflect technical limitations of the new technology. Typically, the total potential market is the total projected sales of the

TABLE ES.1. Technologies Selected for Detailed Analysis and Previously
Estimated Electricity Savings

<u>Technology</u>	<u>Previously Estimated Long-Term Potential Annual Savings (BkWh)</u>
<u>Residential</u>	
Advanced Heat Pumps	152
Advanced Thermal Insulation and Anti-Infiltration Devices	96
Solar Water Heaters	57
High-Efficiency Appliances	<u>32</u>
Subtotal	337
<u>Commercial</u>	
Advanced Lighting	69
Glazings and Other Window Technologies	44
Heat and Cool Storage	<u>80</u>
Subtotal	193
<u>Industrial</u>	
Adjustable-Speed Motors	139
High-Efficiency Motors	35
Advanced Electrolytic Techniques	<u>23</u>
Subtotal	<u>197</u>
Total	727

generic product class to which the technology belongs. The total potential market for high-efficiency fluorescent light bulbs, for example, is defined as the total sales of all types of light bulbs. The total potential market is usually estimated separately for new, normal replacement, and retrofit/accelerated replacement. After estimating the total potential market, the actual potential market is estimated by taking technical limitations of the new

technology into account. The actual market potential of water-to-air heat pumps is smaller than its total potential market (which is sales of electric heating/cooling equipment), for example, because access to a lake or pond is required.

Second, the payback period of purchasing the new technology instead of 1) a competitive technology (in the new and replacement cases) or 2) retaining the existing technology (in the retrofit/accelerated replacement case) is calculated. The payback period represents the number of years required for an investment to "pay for itself", and is equal to the incremental capital costs (the new technology is expected to have a higher purchase price) divided by the annual operating cost savings. The third step is to use the payback period to project the maximum or eventual market penetration rate. The latter rate represents the percentage of the potential market that the new technology will capture when it is mature. In the methodology employed in this study, the relationship between this rate and the payback period is taken from a set of sector-specific tables developed for the office of Buildings Energy Research and Development (BERD), U.S. Department of Energy. In these tables, the lower the payback period, the higher the maximum market penetration rate.

The fourth step of the methodology is to estimate the year-by-year penetration rate of the new technology, from its commercial introduction through maturation. This is done by multiplying the estimated maximum market penetration rate by the values of an "S-curve." This curve demonstrates how the market penetration of a new technology increases from zero at the time of its introduction to its maximum rate. The S-curve used in this analysis is an adaptation of one developed for BERD. In the fifth step, the actual potential market computed in the first step is multiplied year-by-year by the actual penetration rates computed in the fourth step to estimate the annual sales of the new technology. In the final step of the base-case methodology, the annual sales are accumulated over time to calculate the number of units in use in any given year, and this is multiplied by the per-unit electricity savings of the technology (vis-a-vis its competitor) to estimate total electricity savings.

As part of task two, methodologies for projecting the low-case and high-case scenarios were also developed. For the low-case projections two modifications to the base-case were made. First, the maximum market penetration rates were divided by two. Second, the S-curve was adjusted so that the maximum rate was approached more slowly over time. For the high-case projections, the maximum penetration was doubled (up to a maximum of 90 percent) and the S-curve was adjusted to accelerate the approach to the maximum penetration rate.

The third task was to assess the characteristics and estimate the potential market, annual market penetration rates, electricity savings, and levelized cost per kWh saved of each technology. This task was performed by collecting information about each technology from published sources and then applying the task two methodology.

Tables ES.2 through ES.6 summarize the quantitative findings of this task. Tables ES.2, ES.3, and ES.4 display the base-case, low-case, and high-case projections of electricity savings for each technology respectively, for each of the years 1985, 1990, 1995, and 2000. Total projected savings in the base case increase from 21.4 BkWh in 1985 to 63.4 BkWh in 1990, 162.1 BkWh in 1995, and 279.3 BkWh in 2000. The three commercial technologies account for approximately half of these projected savings, with the major portion of that contribution coming from advanced lighting technologies. Advanced heat pumps is the largest electricity saver in the residential sector, and adjustable speed drive (ASD) motors is the largest saver in the industrial sector. In the low-case scenario, total projected savings in 2000 are 137.1 BkWh. Advanced lighting, ASD motors, and heat pumps remain the largest contributors to this total. In the high-case scenario, total projected savings in 2000 are 470.5 BkWh. Glazings, ASD motors, lighting, and heat pumps account for 84 percent of these total savings.

Table ES.5 shows the year 2000 projected savings for each of the three cases and ten technologies as a percentage of the corresponding previous estimate of potential savings presented in Table ES.1. The table shows that for the ten technologies combined, the year 2000 projected savings are 19 percent, 35 percent, and 65 percent, in the low, base, and high scenarios, respectively,

TABLE ES.2. Base-Case Projections of Electricity Savings (BkWh)

	<u>1985</u>	<u>1990</u>	<u>1995</u>	<u>2000</u>
<u>Residential</u>				
Advanced Heat Pumps	1.69	7.43	28.34	60.84
Advanced Thermal Insulation and Anti-Infiltration Devices	1.82	4.90	12.51	15.69
Solar Water Heaters	0.85	1.61	3.20	4.27
High-Efficiency Appliances	<u>0.04</u>	<u>0.20</u>	<u>0.87</u>	<u>4.78</u>
Subtotal	4.40	14.14	44.92	85.58
<u>Commercial</u>				
Glazings and Other Window Technologies	5.23	15.65	35.15	49.01
Advanced Lighting Technologies	2.17	13.42	40.01	79.23
Heat and Cool Storage	<u>0.34</u>	<u>1.57</u>	<u>4.11</u>	<u>7.75</u>
Subtotal	7.74	30.64	79.27	135.99
<u>Industrial</u>				
High-Efficiency Motors	0.39	1.61	3.57	6.19
Adjustable-Speed-Drive Motors	8.88	17.02	34.17	51.22
Advanced Electrolytic Techniques	<u>0</u>	<u>0</u>	<u>0.21</u>	<u>0.33</u>
Subtotal	<u>9.27</u>	<u>18.63</u>	<u>37.95</u>	<u>57.74</u>
Total	21.41	63.41	162.14	279.31

of the total previously projected potential savings of 727 BkWh cited in Table ES.1. In the base case, only the glazing and lighting technologies savings estimates exceed 50 percent, suggesting that the potential savings estimates are severe overestimates of likely savings. If these two technologies are removed from the calculation, the total percentage estimates fall to 13, 25, and 42 percent, respectively. Thus, the estimates of savings appear optimistic, even in comparison to our high-case estimates.

TABLE ES.3. Low-Case Projections of Electricity Savings (BkWh)

	<u>1985</u>	<u>1990</u>	<u>1995</u>	<u>2000</u>
<u>Residential</u>				
Advanced Heat Pumps	0.90	3.61	14.10	30.41
Advanced Thermal Insulation and Anti-Infiltration Devices	1.48	2.48	3.70	5.95
Solar Water Heaters	0.42	0.78	1.36	1.64
High-Efficiency Appliances	<u>0.04</u>	<u>0.17</u>	<u>0.60</u>	<u>2.72</u>
Subtotal	2.84	7.04	19.76	40.72
<u>Commercial</u>				
Glazings and Other Window Technologies	3.69	7.59	13.33	18.96
Advanced Lighting Technologies	1.35	7.13	18.84	36.23
Heat and Cool Storage	<u>0.32</u>	<u>1.13</u>	<u>2.23</u>	<u>3.62</u>
Subtotal	5.36	15.85	34.40	58.81
<u>Industrial</u>				
High-Efficiency Motors	0.25	0.94	1.83	2.52
Adjustable-Speed-Drive Motors	7.25	12.65	19.77	34.92
Advanced Electrolytic Techniques	<u>0</u>	<u>0</u>	<u>0.08</u>	<u>0.17</u>
Subtotal	<u>7.50</u>	<u>13.59</u>	<u>21.68</u>	<u>37.61</u>
Total	15.70	36.48	75.84	137.14

Table ES.6 summarizes the findings regarding the levelized cost of the various technologies. According to Energy Information Administration publications, the levelized cost of new generating capacity varied from 4.24 cents per kWh in the North Central OOE region to 6.30 cents per kWh in New England;

TABLE ES.4. High-Case Projections of Electricity Savings

	<u>1985</u>	<u>1990</u>	<u>1995</u>	<u>2000</u>
<u>Residential</u>				
Advanced Heat Pump	1.92	11.43	40.53	77.50
Advanced Thermal Insulation and Anti-Infiltration Devices	2.89	16.26	30.59	32.16
Solar Water Heaters	0.92	3.90	8.08	8.67
High-Efficiency Appliance	<u>0.05</u>	<u>0.48</u>	<u>2.56</u>	<u>11.49</u>
Subtotal	5.78	32.07	81.76	129.82
<u>Commercial</u>				
Glazings and Other Window Technologies	5.78	38.27	99.29	115.52
Advanced Lighting Technologies	1.92	14.02	48.65	95.57
Heat and Cool Storage	<u>0.35</u>	<u>1.96</u>	<u>5.16</u>	<u>8.98</u>
Subtotal	8.05	54.25	153.10	220.07
<u>Industrial</u>				
High-Efficiency Motors	0.39	2.15	7.24	12.11
Adjustable-Speed-Drive Motors	8.99	29.86	82.66	107.86
Advanced Electrolytic Techniques	<u>0</u>	<u>0.09</u>	<u>0.40</u>	<u>0.64</u>
Subtotal	<u>9.38</u>	<u>32.10</u>	<u>90.30</u>	<u>120.61</u>
Total	23.21	118.42	325.16	470.50

the median cost for the ten DOE regions was 5.89 cents per kWh. Table ES.6 exhibits which technologies have a lower levelized cost than this median generating cost in 1) new and normal replacement applications and 2) retrofit/accelerated replacement applications. The table shows that nearly all of the

TABLE ES.5. Year 2000 Estimated Savings as Percentage of Previous Projections of Potential Savings

	<u>Low Case</u>	<u>Base Case</u>	<u>High Case</u>
<u>Residential</u>			
Advanced Heat Pump	20	40	51
Advanced Thermal Insulation and Anti-Infiltration Devices	6	16	34
Solar Water Heater	3	7	15
High-Efficiency Appliances	<u>8</u>	<u>15</u>	<u>36</u>
Subtotal	12	25	38
<u>Commercial</u>			
Glazing and Other Window Technologies	43	111	262
Advanced Lighting Technologies	52	114	138
Heat and Cool Storage	4	<u>10</u>	<u>11</u>
Subtotal	30	70	114
<u>Industrial</u>			
High-Efficiency Motors	7	18	35
Adjustable-Speed-Drive Motors	25	37	78
Advanced Electrolytic Techniques	<u>1</u>	<u>1</u>	<u>3</u>
Subtotal	<u>19</u>	<u>29</u>	<u>61</u>
Total	19	38	65

technologies have a levelized cost per kilowatt hour saved that is less than the national average cost of electricity from new generating capacity, in both types of applications.

In addition to the quantitative results of task three that are summarized in Tables ES.2 through ES.6, there were a number of other interesting, important findings of this task, of both a general and technology-specific nature.

TABLE ES.6. Levelized Cost per kWh Saved Versus National Average
Projected Cost per kWh from New Generating Capacity

	<u>New/ Replacement</u>	<u>Retrofit/ Accelerated Replacement</u>
<u>Residential</u>		
Advanced Heat Pump	L	H
Advanced Thermal Insulation and Anti-Infiltration Devices	L	L
Solar Water Heaters	H	NA
High-Efficiency Appliances	L(a)	H
<u>Commercial</u>		
Glazings and Other Window Technologies	L	L
Advanced Lighting Technologies	L	L
11 at and Cool Storage	L	NA
<u>Industrial</u>		
High-Efficiency Motors	L	NA
Adjustable-Speed-Drive Motors	L(b)	L(b)
Advanced Electrolytic Technologies	NA	L

Key: L = Technology cost lower than cost of new generating capacity.
H = Technology cost higher than cost of new generating capacity.
NA = Not applicable or not analyzed.
(a) Three appliances were analyzed. One had lower cost.
(b) ASD motors were divided into five categories, based on horsepower.
Only the largest two categories representing motors over 50 hp, had costs lower than the cost of generating capacity.

The reader is referred to the individual chapter discussing each technology for a discussion of the technology-specific findings. The most important general finding is that only a few of the ten technologies selected for detailed analysis are new enough and radically different enough from existing technologies already in use that their availability is probably not reflected in the models

used to generate the NEPP forecasts. These technologies are water-to-air and natural gas-fired heat pumps, the two sub-technologies considered in the heat pump technology area; heat and cool storage in commercial buildings; and new electrolytic techniques in the aluminum industry. The base-case projection of the year 2000 electricity savings associated with these technologies is approximately 69 BkWh, approximately 25 percent of the corresponding total projection for all ten technologies. The detailed analysis in task three resulted in the conclusion that the other technologies examined are either 1) discrete technologies that have been available for a long enough period of time that their availability is also reflected in the NEPP models; or 2) are refinements, extensions, or enhancements of existing technologies whose availability is reflected in the models. The technologies of the second type, for example, are associated with adding additional insulation of the type most residences already have, not the development of a new type of insulation. Since insulation is a technology whose availability is reflected in the NEPP models, by definition the addition of insulation is available and will take place in the models if it is economically feasible. Included in the first category are electronic adjustable speed drive motors, solar water heaters, and high-efficiency freezers and refrigerators. Included in the second category are thermal insulation and anti-infiltration devices, glazings and other window technologies, high-efficiency fluorescent light bulbs and ballasts, and high-efficiency electric motors.

The analysis and, therefore, the electricity savings estimates generated in the study, are subject to several caveats. These caveats result from the inherent uncertainty in such projections, as well as from the time and resource constraints of the project. First, the estimates are based on a purely economic approach. The estimated penetration rate of each technology is based on a comparison of its capital and operating costs to those of its competitor technologies. To the extent that they are considered at all, consumer behavior and attitudes are assumed to be incorporated in the penetration rate/payback and S-curve relationships, and do not vary from technology to technology. The methodology employed is fairly simple, and is based on a small number of case studies. It has not been tested for application to other technologies. In utilizing the methodology, it was assumed (with one exception) that the only

operating cost savings of the new technology were due to reduced electricity consumption. Finally, it was assumed in the base case that the S-curves were shaped so that the maximum market penetration rate was just realized in the year 2000.

Second, the analysis was performed at the national, not the regional, level. National electricity prices, national estimates of consumption by end use, and national climate data were used. Estimates of the savings for those technologies whose adoption may vary significantly across regions (such as solar water heaters) may therefore be inaccurate.

Third, in the analysis of each technology a large number of assumptions had to be made. Estimates of future electricity prices in each sector were required, as were estimates of future residential and commercial building stocks (and their characteristics), the future stock of electric motors (by horsepower class), and future U.S. production of aluminum. Assumptions about these variables, though laden with uncertainty, were fairly straightforward to develop, as the associated data is readily available. More difficult to develop were technology-specific assumptions, such as the number of residences with access to low-cost water (e.g., rivers, streams, lakes). Because the savings estimates are based on such assumptions, they are also laden with uncertainty. In most cases in which accurate, unbiased estimates (such as forecasts from DOE) could not be used, assumptions were made conservatively, i.e., were made so that the resulting savings estimates would be higher than is probably actually the case. Therefore, the base case estimates probably slightly overestimate the true savings. The low-case estimates probably represent a lower bound, while the high-case estimates represent an upper bound.

Finally, the impacts of the ten technologies on load shapes were not considered. Because the value to utilities of energy savings depends on the season and time of day that the impact (saving) occurs, this analysis does not directly yield estimates of the value of the estimated energy savings to utilities.

Because of these caveats, the electricity savings estimates developed in this study should be interpreted as first-cut or approximate estimates that

provide information about the potential magnitudes of the actual savings and also point to further areas of investigation. For purposes other than the development of alternative forecasts of electricity consumption, the savings estimates should be used with caution.

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1.0 INTRODUCTION

This research was performed by Pacific Northwest Laboratory (PNL) for the Office of Coal and Electricity Policy (OCEP), U.S. Department of Energy. The focus of the project was on new technologies that may reduce future electricity consumption.

1.1 BACKGROUND

In the base case forecasts of the Fourth National Energy Policy Plan (NEPP-IV), aggregate U.S. electricity consumption was forecast to grow during the next 20 years at approximately the same rate as the real gross national product (GNP). Recent aggregate trends support this association between electricity consumption and economic growth, and it is likely that the NEPP-V base case forecasts of electricity demand and GNP currently being prepared will be similarly related.

However, several phenomena that have not yet begun to affect aggregate U.S. electricity consumption, and thus are not yet part of the recent trends upon which these forecasts are based, may break or at least weaken the relationship between future electricity consumption growth and GNP growth. In particular, several technologies and/or products that may replace more electricity-intensive technologies have been developed and commercialized in the past 5 to 10 years, and many more can be expected to become commercially available in the next 5 to 10 years. Several analysts believe that these technologies will significantly reduce future U.S. electricity consumption, and, therefore, indirectly weaken the relationship between consumption growth and GNP growth. Amory Lovins, for example, has suggested in his publications, correspondence, and public testimony that such technologies could potentially reduce future electricity consumption to 25 percent of its current value, which would result in a savings of more than 1700 billion kilowatt hours.

Because some of these technologies may not yet have been adequately incorporated into the models used to generate the NEPP electricity consumption

forecasts, the resulting forecasts may overpredict future U.S. electricity consumption. The OCEP has initiated this study to provide information that it can use to insure that its projections of U.S. electricity consumption reflect the availability of these new technologies.

1.2 OBJECTIVES

The objectives of this study are three-fold:

- to collect information about the technical characteristics costs of new electricity saving technologies
- to estimate base, low, and high scenarios of the future potential market, market penetration rate, and impact on aggregate electricity consumption of ten of these technologies
- to estimate the national average levelized cost per kilowatt hour saved by each of the ten technologies.

1.3 OVERVIEW OF REPORT

To achieve these objectives, three tasks were performed:

- selection of ten technologies for detailed analysis
- development of a methodology for estimating the potential market, market penetration electricity savings, and levelized cost of each technology
- assessment of the characteristics and estimate the potential market, market penetration, electricity savings, and levelized cost (per kWh saved) of each technology.

The remainder of this report is divided into 13 chapters. Chapter 2.0 presents the conclusions and recommendations generated from performing these three tasks. Chapter 3.0 describes the methods used and results of the technology selection task. Chapter 4.0 discusses the methodology developed for estimating the future potential market, market penetration, electricity savings, and

levelized cost per kWh saved of each technology. Chapters 5.0 through 14.0 present detailed analyses of each of the ten technologies. Each analysis includes a description of the technology; base-, low-, and high-scenario projections of the future potential market, market penetration rate, and electricity consumption impacts of the technology; and an estimate of the levelized cost per kilowatt hour saved by the technology. Chapters 5.0-8.0 cover technologies affecting the residential sector; chapters 9.0-11.0, the commercial sector; and chapters 12.0-14.0 the industrial sector.

2.0 CONCLUSIONS

In brief, the study yielded the following conclusions:

- At least 30 technologies or products developed in the past five-ten years or expected to be developed in the next five-ten years are discussed in the open literature as having the potential to significantly reduce future U.S. electricity consumption. Amory Lovins has stated that these and other emerging products could reduce future consumption by more than 1700 billion kilowatt hours (BkWh). Ten of these technologies were selected for more detailed analysis in this study. Previous estimates of the potential electricity savings associated with these ten technologies suggest that they could save approximately 725 BkWh of electricity, or about 40 percent of Lovins' total estimate of potential savings.
- A relatively simple, straightforward methodology for projecting future potential markets and market penetration rates based on capital and operating costs exists in the literature and can be used to generate approximate, first-cut estimates of these parameters.
- Of the ten technologies selected for detailed analysis, several are new enough and radically different enough from existing technologies in use that their commercial availability is probably not reflected in the models used to generate the National Energy Policy Plan (NEPP) forecasts. These technologies include water-to-air heat pumps, natural gas-fired heat pumps, heat and cool storage in commercial buildings, and new electrolytic techniques in the aluminum industry. Base-case projections of the year 2000 electricity savings associated with these technologies are approximately 69 BkWh. The other technologies examined are either discrete technologies that have been available for a long enough period of time that they are appropriately represented in the NEPP models or are refinements of existing technologies whose availability is reflected in the models. Included in the former category, we believe, are solar water heaters,

American-made high-efficiency freezers and refrigerators, and electronic adjustable-speed-drive motors. Included in the latter category are thermal insulation and anti-infiltration devices, glazings and other window technologies, high-efficiency fluorescent light bulbs and ballasts, and high-efficiency electric motors.

- High-, base-, and low-case projections of the electricity savings associated with the ten technologies are (in BkWh):

	<u>1985</u>	<u>1990</u>	<u>1995</u>	<u>2000</u>
High Case	23	118	325	470
Base Case	21	63	162	279
Low Case	16	36	76	137

For the year 2000, these projections represent 65, 38, and 19 percent, respectively, of the 725 BkWh potential savings estimate derived from previous studies. This suggests that previous estimates of potential savings substantially overstate projected likely savings.

- Base-case projections of electricity savings for the year 2000 are (in BkWh):
 - Residential, 86
 - heat pumps, 61
 - Thermal insulation and anti-infiltration devices, 16
 - Solar water heaters, 4
 - High-efficiency appliances, 5
 - Commercial, 136
 - Glazings and other window technologies, 49
 - Lighting technologies, 79
 - Heat and cool storage, 8
 - Industrial, 58
 - High-efficiency motors, 6
 - Adjustable-speed-drive motors, 51
 - Electrolytic techniques, 0.3

- The levelized cost per kWh saved of most of the technologies analyzed is less than the cost per kWh of new generating capacity in several regions of the United States. Utilities facing capacity constraints who are considering building new generating capacity may therefore wish to consider facilitating the penetration of one or more of these technologies instead, since they may reduce future costs by doing so.
- The projections generated in this study are subject to several important caveats due to the inherent uncertainties in such projections and to the time and resource constraints of the study. The base-case projections tend to be overestimates of the likely savings, as an attempt was made to be "conservative" in making assumptions. The low-scenario projections, however, probably bound the actual estimates from below. The projections are based almost solely on information in the open literature, as original data collection on such items as consumer acceptance of each technology was beyond the scope of the study. The methodology employed in the study, although utilized by a number of Federal agencies is based on a small number of case studies and has not been empirically validated. In applying this methodology to each technology, a number of simplifying assumptions had to be made. For example, the projections are based entirely on economic and climatic characteristics of the nation as a whole, as a region-by-region analysis was beyond the scope of the study. Because of these and other limitations of the analysis, we believe the projections should be interpreted as first-cut or approximate estimates that provide information about the potential magnitudes of the savings associated with these technologies, and not as precise estimates of the actual savings.

3.D SELECTION OF CONSERVATION TECHNOLOGIES FOR DETAILED MARKET ANALYSES

There are many conservation technologies that could produce future electrical energy savings. The first task in this analysis was to develop a list of the conservation technologies that could potentially be implemented in the residential, commercial, and industrial sectors.

The initial list of prospective conservation technologies was too large to permit detailed analyses of the market penetration and energy-savings potential of all of them. Accordingly, a decision was made to select and focus upon ten that appeared especially promising or potentially important. To complete this task, a set of technology selection criteria was developed. Data on each technology on the list was collected from various sources, and each technology was evaluated to determine how well it met the specified criteria. If a technology did not meet a specified criterion to some degree, it was rejected from the selected set of technologies until ten technologies that fit all of the specified criteria were identified.

In this chapter, the criteria used in the selection process are described. Evaluations of the degree to which each of the conservation technologies in the residential, commercial, and industrial sectors meet the selection criteria are also presented. The chapter concludes with a summary of the results of the selection process.

3.1 ELECTRICITY CONSERVATION TECHNOLOGIES

There are many new and newly developing electrical energy savings technologies that could be used in different applications in the near future. Thus, the first step in this analysis was to identify those technologies that have the potential to be major contributors to future electrical energy savings. An initial list of these potentially "major contributors" is presented in Table 3.1. This list is primarily a modification and extension of a similar listing that had been suggested by Amory Lovins.^(a) Lovins' list was generally

(a) Unpublished letter from Amory Lovins, Director of Research, Rocky Mountain Institute, Snowmass, Colorado, to David Meyer, Office of Coal and Electricity Policy, U.S. Department of Energy, Washington, D.C.

TABLE 3.1. List of Electricity Conservation Technologies

Technology Name	Sector(s)	End Use
1. Advanced thermal insulation and anti-infiltration technologies	residential/commercial	space conditioning
2. Advanced heat pump technologies	residential/commercial	space conditioning
3. Hybrid passive space heating	residential/commercial	space heating
4. Passive space heating	residential/commercial	space heating
5. Hybrid passive space cooling	residential/commercial	space cooling
6. Passive space cooling	residential/commercial	space cooling
7. Air-to-air heat exchangers	residential/commercial	space conditioning
8. Energy management control systems	residential/commercial/ industrial	general use
9. Evaporative cooling	residential/commercial	space cooling
10. Desiccant dehumidification and cooling	residential/commercial	space cooling
11. Window glazings and other window technologies	residential/commercial	space conditioning
12. Solar water heaters	residential	water heating
13. Heat pump water heaters	residential	water heating
14. High-efficiency electrical appliances	residential	appliances
15. High-efficiency gas appliances	residential	appliances
16. Advanced lighting technologies	residential/commercial/ industrial	lighting
17. Daylighting technologies	residential/commercial/ industrial	lighting
18. Heat/cool storage in floor slabs	commercial	space conditioning
19. High-efficiency office equipment	commercial	office operation
20. Variable-speed motor controllers	industrial	motor drive
21. High-efficiency motors	industrial	motor drive
22. Motor resizing, clutched flywheels, etc.	industrial	motor drive
23. Hydraulic/direct industrial drive to replace electric drive	industrial	motor drive
24. High-efficiency electrolytic process	industrial	electrolysis
25. Displacement of steel and aluminum with graphite fibers	industrial	electrolysis/process heating
26. Increase charging of steel scrap	industrial	process heating
27. Fluidized-bed heat treatment	industrial	process heating

complete but it did not include some important measures. The technologies added to his list were:

- energy control management systems
- air-to-air heat pumps
- water-to-air heat pumps
- variable-speed motor drives
- heat-pump water heaters
- heat/cool storage for commercial buildings
- energy-efficient motors.

3.2 SELECTION CRITERIA

The objective of developing selection criteria for use in this study was to provide a methodology for selecting ten conservation technologies for detailed study that could be consistently applied across all the technologies listed in Table 3.1. The criteria were formulated so that the ten technologies that are readily identifiable as being the most likely to have a significant impact upon future electricity demands would be selected from among those listed. The criteria were exclusionary in the sense that, if a technology did not fulfill each of the selection criteria to at least a moderate degree, it was excluded from the selected technology set, until only those ten technologies that fit all of the selection criteria remained.

The first selection criterion is that the selected technologies should represent a cross-section of those available in the residential, industrial, and commercial sectors. The residential sector appeared to offer more potential for electrical energy savings than the other sectors because of a larger number of available conservation technologies and greater electrical energy use (DOE 1984). Four technologies were therefore selected from the residential sector and three each from the commercial the industrial sectors.

Additional criteria were then specified for selecting technologies from among those available within each sector. A summary of the specified criteria is presented in Table 3.2.

The first criterion listed in Table 3.2 is that the technology be among the top five in its sector in terms of potential electricity savings. It is

TABLE 3.2. Criteria Used in Selecting Conservation Technologies

1. The technology is among the top 5 in terms of estimated potential electricity savings from among those available in each of the electricity-consuming sectors (residential, commercial and industrial).
2. The technology is commercially available or is likely to become commercially available in the near future.
3. The technology has not reached high levels of market penetration that would preclude the potential for obtaining additional market share in the future.
4. Unbiased experts and published literature indicate that the potential for growth in the use of the technology is promising.
5. The technology is clearly identifiable as a relatively distinct technology that will allow for projections of its market penetration and energy-savings potentials to be developed.
6. Penetration of the technology will not require radical changes in existing modes of operation.
7. The technology appears, on the basis of published information, to be cost effective.

the most important criterion, and most of the available technologies were excluded or included in the selected technology set based on this criterion. If a technology does not have a large potential for producing electrical energy savings relative to other available technologies in its sector, it was excluded from further analyses. For some technologies, published estimates of the potential energy savings were available. In other cases, estimates of potential energy savings for the technologies were derived using published data on the amount of electricity used in a particular sector's end use (lighting, heating, etc.) and assumptions about the percentage reduction in energy use that a particular conservation technology would produce in this end use. In many cases, the relative amount of electricity used for a given end use was so small that the technologies that might impact upon this end use could be excluded on this basis alone from the selected set of technologies.

The second criterion is that the technology be commercially available or expected to soon become commercially available. It was used to eliminate technologies that are in the basic research and development stage. For such technologies, analyzing the potential energy savings and market penetration of

the technologies would be speculative at best. Very few of the listed technologies were eliminated from further consideration using this criterion.

The third criterion, that the technology has not yet attained a high degree of market penetration (significantly above 10 percent), was used to exclude technologies for which future increases in market penetration and energy savings possibilities are limited. This criterion was employed for two reasons. First, a high degree of current market penetration reduces the possibility for large future increases in penetration. Consequently, the potential for significant future additional energy savings would be modest. Second, the energy from high current penetration would also have been (implicitly) accounted for in present energy forecast modeling efforts. Several technologies from each sector were excluded from further analysis on the basis of this criterion.

The fourth criterion was used to eliminate technologies that conservation experts contacted at Pacific Northwest Laboratory and elsewhere felt had little potential for market penetration growth. In addition, those technologies for which little or no information was identified in the published literature available to us were eliminated using this criterion. If available expert opinion and published literature are currently unable to provide a positive assessment of a conservation technology, it was assumed to be unlikely that the technology will be implemented on a widespread basis in the future.

The fifth criterion is that the technology be relatively distinct. This criterion was used to eliminate technologies for which the definition of the technology is so broad that analyzing the market penetration and energy-saving potential of it would be difficult. For example, a passive solar cooling technology can include anything from shade trees to window glazing. The definition of a passive solar technology is not standardized enough to allow for a market analysis to be performed. Several other examples of technologies that were not clearly identifiable were noted.

The sixth criterion was used to eliminate technologies that require radical changes in existing operations and behavior. Such technologies are less likely to be implemented than technologies that do not require behavioral changes. In addition, the energy savings of technologies that require behavior changes are more uncertain, because the changes in behavior may be short lived. Only a small number of the available technologies appeared to require radical changes

in existing behavior and modes of operation, but these were eliminated from further consideration.

The seventh criterion, that the technology appears to be cost effective, was used to eliminate technologies only when they were obviously too expensive to be cost effective. Relatively few technologies fell into this category.

After having clearly specified the criteria for the technology-selection process, the necessary data to evaluate the technologies according to the criteria were collected and the selection process was performed. The data collected for the evaluation were obtained from various sources, including articles and papers from Arthur D. Little, Inc. (ADL), the Alliance to Save Energy (ASE), the U.S. Department of Energy (DOE), the Electric Power Research Institute (EPRI), the Lawrence Berkeley Laboratory (LBL), the Office of Technology Assessment (OTA), and others. A great deal of emphasis was placed on verifying that data used were consistent with Fifth National Energy Policy Plan (NEPP-V) data and projections. As a backup, consistency was further checked using the estimated sectoral end-use data of DOE's 1984 Energy Conservation Multi-year Plan, FY 1986-FY 1990 (DOE 1984).

The technology-selection process was performed by evaluating each measure according to how well the measure met the specified selection criteria. Whenever it was determined that a technology did not meet any one of the criteria to at least a moderate degree, that technology was evaluated as not suitable for selection. In most cases, the estimated potential electricity savings of each technology was stressed as the most critical criterion. Evaluations of each of the technologies listed in Table 3.1 are presented by sector in the next three sections of this chapter.

3.3 RESIDENTIAL TECHNOLOGY EVALUATIONS

In this section, 17 residential electricity conservation technologies for different end uses are evaluated as to how well they meet the selection criteria. Table 3.3 provides an overview of the results of the selection and evaluation analysis. Note from Table 3.3 that the technologies of thermal insulation and anti-infiltration devices, advanced heat pumps, solar water heaters, and high-efficiency electric appliances were evaluated as meeting all of the selection criteria and, thus, were selected to be included in the

TABLE 3.3. Evaluation of Residential Electricity Conservation Technologies

Technology Name	End Use	1. High Potential Energy Savings	2. Cost Effective	3. Commercially Available	4. Potential Market Penetration	5. Expert Opinion	6. Distinct Technology	7. No Radical Change
*Thermal Insulation and Anti-Infiltration	Space conditioning	Yes	Yes	Yes	Yes	Yes	Yes	Yes
*Advanced Heat Pump Technologies	Space conditioning	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Hybrid Passive Space Heating	Space conditioning	Some	Some	Yes	Yes	Some	No	No
Passive Space Heating	Space conditioning	Some	Some	Yes	Some	Some	No	No
Hybrid Passive Space Cooling	Space conditioning	Some	Yes	Yes	Yes	Yes	No	No
Passive Space Cooling	Space conditioning	Some	Some	Yes	Yes	Some	No	No
Air-to-Air Heat Exchangers	Space conditioning	No	Some	Yes	Some	No	Yes	Yes
Energy Management Control Systems	General use	Some	Yes	Yes	No	Some	Yes	Some
Evaporative Cooling	Space conditioning	No	Some	No	Yes	Some	No	Some
Desiccant Dehumidification and Cooling	Space conditioning	No	Yes	Yes	No	No	Yes	Some
Window Glazings and Other Window Technologies	Space conditioning	Some	Yes	Yes	Some	Some	No	Some
*Solar Water Heaters	Water heating	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Heat Pump Water Heaters	Water heating	Some	Yes	Yes	Yes	Yes	Yes	Yes
*High-Efficiency Electrical Appliances	Appliances	Yes	Yes	Yes	Yes	Yes	Yes	Yes
High-Efficiency Gas Appliances	Appliances	No	Some	No	Yes	Some	Yes	Some
Advanced Lighting Technologies	Lighting	Some	Yes	Yes	Yes	Yes	Yes	Yes
Daylighting	Lighting	No	Yes	Yes	Some	Some	Yes	Some

* Selected technologies.

final technology set.

The remainder of this section presents a description of the evaluation process for the residential sector conservation technologies. The evaluation begins (in Section 3.3.1) with a brief summary of the present levels of electricity consumption for different end uses in the residential sector. This information is important because the potential for future electrical energy savings from each technology is directly related to present consumption. Section 3.3.2 presents brief descriptions of the four residential technologies that were selected for more detailed analysis while Section 3.3.3 provides information about the residential technologies listed in Table 3.1 that were not selected.

3.3.1 Present Residential Electricity Consumption, by End Use

Space conditioning is the single largest end use of electricity in the residential sector. In 1984, approximately 117 Billion kilo-watt hours (BkWh) out of a total of 780 BkWh of residentially consumed electricity was utilized for the purpose of space heating. In addition, residential space cooling consumed an estimated 167 BkWh (DOE 1985). Because more than 1/3 of the total residential electrical energy consumption is used for space conditioning, reductions in electricity consumed for this purpose have the potential to produce relatively large electricity savings.

In 1983, electrical consumption for refrigeration alone was estimated to be in the range of 111 BkWh (DOE 1985). When refrigerators are considered in combination with freezers (41 BkWh), cooking and drying equipment (50 BkWh), and "other" appliances such as washers, toasters, etc. (126 BkWh), it becomes apparent that the potential for future electrical savings from more efficient appliances is also large.

Water heating is the third largest use of electricity consumption in the residential sector. In 1984, residential use of electricity for water heating was an estimated 85 BkWh of electrical consumption, which was approximately about 11 percent of total residential electrical consumption (DOE 1985).

Residential electricity use for lighting was approximately 80 BkWh in 1984. This was approximately 10 percent of total residential electricity consumption.

3.3.2 Selected Residential Technologies

The technologies selected for the residential sector have the potential to impact upon the electricity consumed in all of the major end uses listed above. Evaluations of each of the selected technologies are presented below.

Advanced Thermal Insulation and Anti-Infiltration Technologies

Thermal insulation reduces the amount of thermal transmission through walls, ceilings and floors and, thus, can reduce the energy used in both heating and cooling buildings. Anti-infiltration technologies (such as vapor barriers) reduce the amount of air exchange in buildings, thereby resulting in decreased heating and cooling energy usage and reduced moisture infiltration.

These measures clearly remain among the most important technologies in terms of their untapped potential for additional and significant electrical energy savings. New, technologically superior, safer, and more cost-effective insulation retrofit measures in combination with newly developed and developing anti-infiltration retrofit devices have the potential to reduce electricity use for space heating in existing homes by as much as 50 percent (OTA). Furthermore, these measures also have the potential to further reduce electrical consumption for space cooling in existing homes by more than 10 percent (OTA). Even greater energy savings could be attained if new high insulation and low infiltration building practices become more common for new residential structures. Based on the current amount of electricity used for space conditioning in the residential sector, achieving these potential reductions could reduce residential electricity consumption by 95 BkWh. Because of their high savings potential and because these technologies appear to meet all the other selection criteria, they have been selected for more detailed analysis in later chapters.

Advanced Heat Pump Technologies

Heat pumps are devices that can, under many conditions, heat and cool buildings more efficiently than conventional HVAC systems. When heating, a heat pump's refrigerant takes available heat from outside air or water, compresses it, and distributes it throughout a building through a forced air system. When cooling, the cycle is reversed. Several different types of

heat pumps, including electric air-to-air and water-to-air models and gas models, fit within the general category of heat pump technologies.

The air-to-air electric heat pump has made significant gains in the residential space-conditioning market during the past several years. However, future market growth for heat pumps is likely to be comprised primarily of the expanded use of electric water-to-air models and gas models.

Several gas-fired heat pump technologies are currently receiving large expenditures for development and, if they are perfected and aggressively marketed, they could be commercially available and competitive by the late 1980s or early 1990s. Gas-fired heat pumps differ from electric heat pump systems because the motor driven compressor operates on gas power rather than electric power (see Chapter 6). The gas-fired motors now being developed are likely to be significantly improved over existing models. This technical advance, in combination with the fact that gas power is less expensive per unit of power output than electricity, suggests that the gas-fired heat pump is likely to become an important space heating technology. Specifically, the anticipated market potential for gas-fired heat pump systems ranges from a competitive share to a complete domination of the market (Itteilag and Swanson 1984).

Because the energy efficiency of water-to-air heat pumps is significantly higher than that of either electric HVAC systems or the more conventional air-to-air electric heat pumps, they also have considerable potential to improve on the present electrical demands of those systems. In combination with other new heat pump space-conditioning systems (i.e., gas heat pumps), water-to-air heat pumps form a category/technological area that deserves to be considered among the most promising of the new residential energy savings technologies.

Every gas-fired heat pump that penetrates the electric space-conditioning market obviously displaces 100 percent of the electrical alternative's electrical consumption with gas consumption. Assuming that water-to-air heat pumps compete for market share only with other electric HVAC systems, each such system will also contribute to a reduction in electricity demand. For example, depending on the climate conditions of the installation, water-to-air heat pumps can reduce the electrical consumption of air-to-air heat pumps by as much as 25 percent (McGuigan 1982). Hence, the potential exists for

additional reductions in electrical energy use, beyond those that have been achieved using air-to-air heat pumps, through the use of advanced heat pump technologies. Because of the remaining large potential for energy savings from the use of advanced heat pump technologies and because heat pump technologies appear to meet all of the other selection criteria, they have also been included for intensive study.

High-Efficiency Electrical Appliances

The potential electrical consumption savings of advanced insulation for appliances has been reported to be in the range of 32 BkWh by the year 2000 (DOE/BERD 1984). For refrigerators and freezers alone the savings could be in the range of 23 BkWh by the year 2000, depending on the degree of market penetration of these technologically advanced appliances. In addition, high-efficiency electrical appliances generally are out of the research and development stage, would not require major changes in behavior, and appear to be cost effective. Because high-efficiency appliances appear to meet all of the selection criteria, they have been selected for intensive study.

Solar Water Heaters

Mechanically, solar water heaters for the home are not very different from gas or electric water heaters. Solar collectors absorb solar radiation and convert it to usable heat. Solar energy actually serves to preheat the household hot water and must typically be used in combination with a conventional gas or electric water heater. The reduction in household electricity use for water heating attributable to use of a solar water heater depends on the climate, the site, and the surface area of solar panels that are installed.

Solar water heaters now appear to be economically competitive with electric water heaters in many parts of the country. In addition, solar water heaters appear to have a relatively large energy-savings potential. Depending on the location and the number of square feet of solar panels installed, 30 percent to 75 percent of a household's energy demand for water heating can be met by a solar water heater (HUD/DOE 1980). Assuming that an energy savings of 50 percent is a representative average, the potential electricity savings of solar hot water heaters could be as great as 42 BkWh. Solar water heaters

appear to have great potential for significant future penetration in the market for water heaters. In summary, this technology appears to meet all of the selection criteria, and is therefore selected for intensive study.

3.3.3 Residential Technologies Considered But Not Selected

Each of the technologies discussed in this section failed to adequately meet at least one of the specified selection criteria.

Hybrid Passive Space Heating

Hybrid passive heating applications include the heating of building areas with only minimal use of low-power fans or pumps. Primary methods include employing external structural devices to capture heat from sunlight and to diffuse that heat to the building proper by means of radiance, convection, conduction, fan, or pump. Specific systems include the trombe wall, the stagnating trombe wall, the water wall, the sunspace or greenhouse, roof pond systems, and the thermosiphon.

Although the future electrical energy savings of this technology are potentially substantial, it has a relatively high initial installation cost with a consequent long pay-back period. As such, it is likely to remain a less desirable alternative than the insulating and/or heat pump technologies.

Therefore, this technology is not recommended for inclusion in our final selected set of technologies because:

- 1) It would, to be widely effective, require extensive refitting of existing homes and/or radical changes in the manner in which new houses are designed and built, so its cost effectiveness is uncertain; and
- 2) is not clear that, as a system, it could be readily analyzed as a distinct technology.

Passive Space Heating

Passive space heating is, the heating of building areas without the use of any mechanical or external storage/collection devices. Primary methods include allowing sunlight to warm building areas through south-facing windows and allowing the natural distribution of that warmth by means of convection, conduction, or radiation from south-facing solar-warmed walls next to living space.

The potential electrical energy savings of this technology are moderate as compared to the insulating and heat pump technologies. Passive space heating is primarily limited to improvements in the architectural design of new buildings because effective savings from the implementation of these systems into existing buildings can only be gained at a relatively high cost. Specifically, this technology is not recommended for further study because:

- 1) Its contribution to future electrical energy savings is likely to be only moderate in comparison to the potential contributions of other conservation measures;
- 2) has a probable rate of market penetration that is strongly dependent upon the number of new houses that are built, and is generally not applicable to existing buildings; and
- 3) is not clear that, as a system, it could be readily analyzed as a distinct technology.

Hybrid Passive Space Cooling

Hybrid passive space cooling is the cooling of building areas with only minimal use of mechanical or external devices. Primary methods include cooling by evaporation, ventilation, dehumidification, convection, conduction, and/or radiation reduction. Examples include air-wash evaporative cooling devices, low-power ventilation fans or pumps, dehumidifiers, and mechanized venetian-type blinds that automatically adjust the solar radiation permitted to enter the work space to the most desirable level.

The electrical energy savings of these measures are potentially substantial. However, hybrid passive space cooling is not a single technology but rather a family of related technologies, some of which would require significant behavioral adjustments to be implemented. As such, this technology does not meet the selection criteria of being a distinct technology nor that of requiring no radical changes in behavior.

Passive Space Cooling

Passive space cooling is the cooling of building areas without the use of any mechanical or external storage/collection devices. Primary methods include shading of building areas from exposure to the summer sun and allowing

ventilation to reduce internal heat and humidity. Examples include external shading from trees, awnings, and overhangs; window glazings and/or venetian-type blinds; earth sheltering; and daytime/nighttime "modulated" ventilation procedures.

The potential electrical energy savings of these measures is low to moderate, depending on the climate which they are to be applied. This category is also better described as a family of related technologies and depends heavily upon significant behavioral adjustments in their most effective implementation. For these reasons, passive space cooling is not recommended for inclusion in the group of technologies selected for intensive study.

Air-to-Air Heat Exchangers

An air-to-air heat exchanger is a device for mitigating reductions in indoor air quality resulting from building tightening. Air-to-air heat exchangers mix the heat of outgoing indoor air with incoming outdoor air to result in less heat loss than would occur if air were allowed to be exchanged through walls, windows, and other parts of a building. Thus, the exchangers allow for acceptable levels of indoor air quality to be achieved while at the same time preserving much of the energy-conserving potential of the building.

Further analysis of this technology is not recommended because:

- 1) It compares unfavorably with other residential technological systems in terms of its potential for significantly affecting the future consumption of electrical energy; and
- 2) It has a probable rate of market penetration that is strongly dependent on the degree to which the insulating and anti-infiltration technologies are adopted. In fact, this technology by itself does not save energy but rather contributes to the energy savings of other technologies by reducing heat loss while alleviating an undesirable air-quality side effect that typically occurs with high levels of insulation.

Energy Management Control Systems

In recent years, a variety of control systems have been developed to more efficiently manage the energy use of a building. Examples of these controls include night setback thermostats, automated lighting controls, and

electric demand data recording systems. These controls either provide automated control of energy-consuming systems or provide residents data that allows them to better manage their energy consumption processes.

This technology has already achieved a relatively high level of market penetration. Therefore, although such systems have saved a significant amount of electrical energy to date, it seems likely that future savings attributable to these systems have already been accounted for in projections of residential sector demand. Accordingly, they are not included in the selected technology set.

Evaporative Space Cooling

Evaporative cooling occurs when heat energy in the air or on a roof is "consumed" or converted into water vapor by evaporation. Although the creation of water vapor increases the ambient humidity, in dry climates that increase combines with the coinciding reduction in air temperature to provide greater comfort. Primary methods include the addition of bodies of water (pools or fountains) or of moisture (atriums) to cool the living/working space or, alternatively, the spraying of roof tops with water to cool the ceiling surface below. Some other methods include employing mechanical evaporative devices to pre-cool air before it enters various types of conventional air coolers to reduce the energy demand of those systems.

Applications of the evaporative cooling methodologies are only reasonably effective in hot/arid climates where water for cooling is plentiful. In less arid regions, utilization of evaporative space-cooling methods is less beneficial because these systems tend to produce an undesirable increase in the ambient humidity. Most importantly, in almost all applications, the potential electrical energy savings of these systems is relatively small. As such, they would have to be used in combination with alternative cooling equipment to ensure reasonable occupant comfort. Finally, the more advanced system designs of this technology are still in the basic research and development stage. Because of the above factors, this technology is not selected for further study.

Desiccant Dehumidification and Cooling

Desiccant cooling is the drying of very humid air, which helps to promote natural cooling (by evaporation of sweat) and to reduce the formation of frost and condensation on refrigeration units (allowing them to work more efficiently). In climates that experience high humidity levels, the dehumidification effectively reduces electrical demand for air conditioning and refrigeration. The use of desiccant salts (which absorb moisture from air), solar dehumidification systems, or mechanical dehumidifiers are all methods of desiccant cooling. Desiccant salts eventually become saturated with moisture and require (solar or gas) energy for drying out; specific systems have been and continue to be developed for this purpose.

This technology is not recommended for inclusion in the final technology set primarily because its contribution to potential future electrical energy savings is not likely to be large. Most forms of this technology have been around a long time and are only effective in climatic regions that experience high levels of humidity or in typically humid buildings such as those that are passively cooled. In addition, desiccant salt solar systems are still in the development stage and remain a technological challenge.

Window Glazings and Other Window Technologies

Glazings are materials that are either translucent or transparent to solar radiation. By regulating the intensity of sunlight allowed to pass through a glazed surface, the natural warming and lighting effects of sunlight can be either permitted or inhibited. Glazings also have the quality of increasing the insulation R-value of treated windows. Other window technologies include various types of window shades or energy-efficient venetian-type blinds that automatically adjust to regulate the solar radiation permitted to enter the living/working space.

The potential contribution of future electrical energy savings of this technology in the residential sector is only moderate. Therefore, it is not recommended for inclusion in the selected set of residential conservation technologies. However, the contribution to commercial electrical savings is potentially quite large for these technologies, and they will be highly recommended for further analysis in that application.

Heat Pump Water Heating Systems

Heat-pump water heaters incorporate the general principles of heat pump technology in heating water. Heat is drawn from the air, condensed, and then transferred to water. The ideal location for a heat-pump water heater is in a partially conditioned location where the air temperature is normally between 45°F and 95°F. In summer, a water heat pump that is located indoors can reduce cooling loads by transferring heat from indoor air. However, in winter the same heat pump could increase space heating demands. For this reason and others, it is normally recommended that heat-pump water heaters be placed in areas that are normally unoccupied.

Water heating heat pumps are estimated to be about 50 percent more energy efficient than electric resistance water heaters (EPRI 1984) but, depending on the climate, typically less energy efficient than solar water heaters. In addition, determining the potential energy savings of heat pump water heaters is difficult because their effectiveness is dependent upon their location within a residence. If they are located inside a residence that uses electric space heating or outside a residence located in a cold climate, their energy-savings potential is marginal. Thus, even though the capital costs of heat pump water heaters are generally lower than solar water heaters, it is recommended that they not be included in the selected technology set because of lower potential energy savings considerations.

High-Efficiency Light Bulbs

High-efficiency light bulbs are simply light bulbs that perform the same function as conventional light bulbs while using less energy. Estimates of the potential savings in future electrical consumption from highly efficient lighting technologies in the residential sector were not identified during this study. However, it appears that a very high percentage efficiency improvement would be necessary in order for these light bulbs to be competitive with the selected technologies in terms of their expected electrical consumption savings, and they are not recommended for inclusion in the selected technology set on this basis.

Daylighting

Daylighting is a technology whereby buildings are designed to capture natural light for internal building use by utilizing proper window spacing, window angles, and other techniques. The use of natural light will obviously reduce the amount of electricity used in providing artificial light. However, properly designed daylighting systems can also reduce cooling electrical demands because of the lower heat content of natural light compared to artificial light.

The potential energy savings of daylighting in the residential sector appear to be very small because the technology will generally be cost effective only on new buildings, and even in these buildings the savings of the increased use of natural light in residences are likely to be minor. Based on these considerations, daylighting is not recommended for inclusion among the selected set of technologies.

High Efficiency Gas Appliances

High efficiency gas appliances include gas refrigeration and air conditioning. At present high efficiency products employing these technologies are not being produced in significant numbers and have achieved only negligible market penetration. Although this is an area of keen interest on the parts of both the American Gas Association and the Gas Research Institute, our preliminary findings indicate that products employing this technology would be configured so differently from standard appliances that their adoption and use would require substantial changes in consumer behavior. Subsequently, this technology has not been selected for further study.

3.4 COMMERCIAL TECHNOLOGY EVALUATIONS

Evaluations of the degree to which 15 commercial electricity conservation technologies meet the specified selection criteria are discussed in this section. A summary of the results of these evaluations is shown in Table 3.4. Again, in that table a Yes implies that a conservation technology fully met the corresponding selection criterion; a Some implies that a technology at least moderately met the corresponding selection criterion; a No implies that a technology did not meet the corresponding selection criterion. Note that the selected technologies (i.e., those identified in Table 3.4 by o) of advanced lighting systems, window glazings and other window technologies, and

TABLE 3.4. Evaluation of Commercial Electricity Conservation Technologies

Technology Name	End Use	1. High Potential Energy Savings	2. Cost Effective	3. Commercially Available	4. Potential Market Penetration	5. Expert Opinion	6. Distinct Technology	7. No Radical Change
*Advanced Lighting Systems	Lighting	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Daylighting	Lighting	Some	No ^(a)	Yes	Yes	Yes	Yes	Yes
*Window Glazings and Other Window Technologies	Space cooling and lighting	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Hybrid Passive Cooling	Space cooling	Some	Yes	Yes	Yes	Yes	No	No
Passive Cooling	Space cooling	Some	Some	Yes	Yes	Some	No	No
Evaporative Cooling	Space cooling	No	Some	No	Yes	Some	No	Some
Desiccant Dehumidification and Cooling	Space cooling	No	Yes	Yes	No	No	Yes	Some
*Heat/Cool Storage in Building Structure	Space conditioning	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Building Shell Tightening	Space conditioning	No	Yes	Yes	No	Yes	Yes	Yes
Advanced Heat Pump Technologies	Space conditioning	No ^(b)	Yes	Yes	Yes	Some	Yes	Yes
Hybrid Passive Heating	Space heating	Some	Some	Yes	Yes	Some	No	No
Passive Heating	Space heating	Some	Some	Yes	Some	Some	No	No
Air-to-Air Heat Exchangers	Space heating	No	Some	Yes	Some	No	Yes	Yes
High-Efficiency Office Equipment	Office operations	No	Some	Yes	Yes	No	No	Yes
Energy Management Control Systems	General use	Some	Yes	Yes	No	Some	Yes	Some

(a) The primary reason for the non-cost-effectiveness of the daylighting technologies is that, to be effective, they frequently require costly structural changes to be made on existing buildings.

(b) Heat pump's main contribution to efficiency is in its applications as a space heater. Commercial space heating is a relatively small end-use category; hence, the low subjective rating for heat pump savings in this application.

* Selected technologies.

heat/cool storage in building structures were evaluated as fully meeting all of the selection criteria.

3.4.1 Present Commercial Electricity Consumption by End Use

The lighting of commercial buildings is by far the largest of the electricity consuming end-use categories in the commercial sector. In 1984, an estimated 237.38 BkWh out of a total 656.5 BkWh of commercial electricity use was consumed for lighting purposes in the commercial sector (DOE 1985). Consequently, improvements over present lighting technologies could dramatically affect total future electrical consumption.

Space cooling is the second largest electrical energy user of the commercial end-use categories. In 1984, an estimated 193.4 BkWh of commercially consumed electricity was utilized for the purpose of space cooling (DOE 1985). Potential future reductions in electricity utilized for this purpose would significantly contribute toward influencing total electrical energy savings by the year 2000.

The electrical requirement for heating purposes in commercial buildings is at most only one-greater of that required for cooling purposes. In 1984, an estimated 43.9 BkWh of electricity was consumed commercially for the purpose of space heating (DOE 1985). During the week, the working space of a commercial building is warmed to a great degree by the heat produced from the operation of lights, office machines, and from body heat. Therefore, commercial buildings typically produce an excess of heat during the working week. However, over the weekends during the colder months the internal activities of the building can not meet the heating requirements and the heating system must typically be turned on.

3.4.2 Selected Commercial Technologies

The selected technologies of advanced lighting systems, window glazings and other window technologies, and heat and cool storage in the building mass could have significant impacts upon the electricity used in the three major end-use categories of the commercial sector. In addition, they were determined to have fully met all of the selection criteria. An explanation of why each of these technologies was selected for further analysis is presented below.

Advanced Lighting Systems

Ballasts are devices for starting voltage and limiting lamp current in all gas-discharge lamps. High-frequency ballasts perform these functions more efficiently. The lower power input requirements of high-frequency ballasts reduce the heat retention in a light fixture. Thus, both lighting and cooling electricity demands can be reduced by using high-frequency ballasts. SL/PL bulbs are simply light bulbs that require less electricity input to produce light output than the standard incandescent bulbs in widespread use today.

High-frequency ballasts, more efficient fluorescent tubes, and more efficient light bulbs all have significant potential for reducing future electrical energy consumption. It has been estimated that approximately 68.8 BkWh of electricity could be saved annually by the year 2000 by using more efficient lighting technologies (DOE/BERD 1984). These technologies are commercially available, to a limited degree, and should not require major changes in existing behavior. Advanced lighting technologies have the potential to produce large energy savings and also appear to fulfill the other selection criteria. Thus, it is recommended that they be included in the selected set of technologies.

Window Glazings and Other Window Technologies

Glazings and other window technologies were described in Section 3.3. However, the potential electrical energy savings of implementing these technologies are significantly greater in the commercial sector than they are in the residential sector.

Replacing clear glass office windows with windows that are properly glazed, or installing light filtering film over existent windows, could reduce commercial electrical consumption for cooling by up to 22 percent providing a potential for savings of about 44 BkWh. Glazings also have the ability to increase the insulation R-value of treated windows, and they allow for more widespread use of daylighting technologies. Additional energy savings can be gained by further regulating the solar radiation that enters the work space with various types of window shades and energy-efficient venetian-type blinds. This technology appears to fulfill all of the technology selection criteria and, thus, is recommended for inclusion in the selected technology set.

Heat and Cool Storage in the Building Structure

HVAC units, regardless of the type, work far more efficiently when they are used for cooling pre-cooled air. Because night air, depending on the location, is typically much cooler than mid-day air, HVAC systems operating at night can save up to 30 percent on their energy intake (Anderson et al. 1979). Therefore, if night-time cool air can be stored in the building structure and released when needed during the heat of the day, substantial energy savings can be realized.

Furthermore, during the winter months, commercial buildings typically have to be heated only on Monday mornings for a few hours or until the activities that take place within the buildings are well underway. This is because, even during the winter months, commercial buildings typically acquire substantial amounts of excess heat from the operation of lights, office machines, and from body heat. When this excess heat is directed into the building's structure rather than discarded to the outside, it can be released again as needed over the weekend to help maintain building temperature without turning up the furnace. It has been estimated that up to 50 percent of a commercial building's demand for heat can be met by employing this method (Anderson et al. 1979).

The combined heating and cooling savings that could be realized by more widespread application of these methods appear large, and the technology appears to fulfill all of the other selection criteria. Thus, it is retained for more in-depth analysis.

3.4.3 Commercial Technologies Considered But Not Selected

The following commentaries offer explanations for not selecting other technologies for further study. Note that insofar as these technologies have already been described in their applications to the residential sector, they are not described again below.

Daylighting

This technology is likely to significantly reduce commercial lighting demand for electricity in new commercial buildings. However, its application to existing buildings is in most cases not cost effective. The potential electrical energy savings directly attributable to daylighting technologies

have been estimated to be only about one-fourth of the potential savings attributable to advanced lighting technologies (DOE/BERD 1984). Because of the apparent lack of cost effectiveness of daylighting on existing buildings and its low potential for savings relative to advanced lighting technologies, it is not included in the set for intensive study.

Hybrid Passive Cooling

This technology is not a single technology but rather a family of related technologies, some of which are likely to be major contributors to future electrical savings and some of which will have a much smaller impact on those savings. The major contributors (i.e., window glazings and blinds, and heat and cool storage in floor slabs) will be treated in this analysis as two distinct technologies. The remaining contribution of other hybrid passive cooling technologies to electrical savings is not large enough to warrant further analysis here.

Passive Cooling

The anticipated future electrical savings of this technology are moderate when the impact of window glazings is treated as a separate technology. Other forms of passive cooling either are not cost effective or would require significant behavioral adjustments in their application. For these reasons, passive cooling is not suitable for additional research.

Evaporative Cooling

Applications of the evaporative cooling methodologies are cost effective and have a large impact on electrical consumption only in hot/arid climates where water for cooling is plentiful. In humid climates, these systems are inappropriate because they elevate the level of humidity, which is, of course, undesirable. The potential for electrical energy savings of these systems is relatively small, and they have not been selected for further study.

Desiccant Dehumidification and Cooling

The likely contribution of these methodologies to reduce future electrical energy demand is modest. For the most part, this is not a new technology, but newer systems are being developed (e.g., desiccant salt solar systems). In almost all applications, these systems would have to be used in combination with other cooling measures to ensure reasonable comfort. Finally, these

systems are only applicable to humid climates or to structures that are typically humid, such as those that are passively cooled.

Advanced Insulation and Anti-Infiltration Technologies

Most of the more modern commercial buildings are already fairly well constructed in terms of their inherent levels of insulation and their incorporation of anti-infiltration measures. Because of this and because heating is not nearly as large a commercial electrical end use as either the lighting or the space-cooling categories, the potential for substantial future electrical savings from building-shell tightening is comparatively small. Hence, this technology is an attractive candidate for further study.

Advanced Heat Pump Technologies

In terms of electrical energy savings, the main contribution of advanced heat pumps is in space heating. Since the commercial end use of space heating is small relative to the lighting and space-cooling end-use categories, the anticipated future electrical savings due to the application of heat pump technologies in the commercial sector are comparatively small. This technology is not included in the set selected for further study.

Hybrid Passive Heating

Hybrid passive heating is actually not a single technology but rather is several different technologies under a broad heading. The more important of these various specific types of hybrid passive heating are treated independently for their specific contributions. The combined contribution to future electrical savings of the lesser hybrid passive technologies is likely to be modest.

Passive Heating

Like the other passive technologies, this alternative has major and minor specific technologies which are better considered individually. The anticipated future electrical savings of the minor passive heating technologies are not likely to make a significant contribution to future electrical energy savings. In addition, many of them do not appear to be cost effective or would require adjustments in behavior. This technology is not selected for further study.

Air-to-Air Heat Exchangers

This technology compares unfavorably with other commercial alternatives in terms of its potential for significant contributions to future electricity consumption reductions. The system's primary contribution is that it reduces heat loss while bringing in fresh air for ventilation purposes and it only saves energy when used in concert with building tightening measures. Thus, it is not even an energy conservation technology when considered as a stand-alone measure, and it is recommended that it is not an attractive candidate for further analysis.

High-Efficiency Office Equipment

Besides lighting and space conditioning, all other end uses of electricity combined in the commercial sector utilize only 92 BkWh, or 14 percent, of total commercial electricity use (DOE 1984). Because of the relatively small electrical consumption of commercial office equipment, the potential savings resulting from major technological improvements in their efficiency is likely to be small compared to those that can be realized by using lighting and space-cooling conservation technologies. Therefore, this category is not suitable for an in-depth analysis into its electricity savings potential.

Energy Management Control Systems

These systems have been commercially available for several years and are already widely used in the commercial sector. A recent survey conducted by the association of energy engineers found that 62 percent of commercially active companies are currently using energy management systems and that an additional 32 percent are planning to install such systems in the near future (Association of Energy Engineers 1984). Therefore, although this technology has saved large amounts of electricity to date, it seems likely that future savings from these systems will not change significantly from present levels. Therefore, it is not considered further here as a potential major new electricity energy savings technology.

3.5 INDUSTRIAL TECHNOLOGY EVALUATIONS

The evaluations and discussions of 11 industrial electricity-saving technologies are presented in this section. As before, a summary of the basic results of these evaluations (presented in Table 3.5) precedes the more detailed

TABLE 3.5. Evaluation of Industrial Electricity Conservation Technologies

Technology Name	End Use	1. High Potential Energy Savings	2. Cost Effective	3. Commercially Available	4. Potential Market Penetration	5. Expert Opinion	6. Distinct Technology	7. No Radical Change
*Variable-Speed Motor Controllers	Motor drive	Yes	Yes	Yes	Yes	Yes	Yes	Yes
*High-Efficiency Motors	Motor drive	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Motor Resizing, Clutched Flywheels, etc.	Motor drive	Some	NA	NA	NA	No	Yes	NA
Hydraulic/Direct Industrial Drive To Replace Electric Drive	Motor drive	Some	NA	Yes	Yes	No	Yes	No
*High-Efficiency Electrolytic Processes	Electrolysis	Yes	Some	Yes	Yes	Yes	Some	Yes
Displacement of Steel and Aluminum with Graphite Fibers	Electrolysis and process heating	Some	NA	Yes	Yes	No	No	No
Increase Charging of Steel Scrap	Process heating	No	Yes	Yes	No	Yes	Yes	Yes
Fluidized-Bed Heat Treatment	Process heating	No	Yes	Yes	Yes	Yes	Yes	Yes
Advanced Lighting Concepts	Lighting	No	Yes	Yes	Yes	Yes	Yes	Yes
Daylighting	Lighting	No	Yes	Yes	Yes	Yes	Yes	Yes
Energy Management Control Systems	General use	No	Yes	Yes	No	Yes	Yes	Yes

* Selected technologies.

discussions. Note that the selected technologies of variable-speed motor controllers, high-efficiency motors, and high-efficiency electrolytic processes (identified in Table 3.5 by * were evaluated as having met all of the selection criteria to at least a moderate degree.

3.5.1 Present Industrial Electricity Consumption by End Use

In 1984, approximately 899 BkWh of electricity was consumed in the industrial sector, according to a recent estimate (DOE 1985). The major end-use applications for this electricity were for motor drives and electrolytic processes.

Electric motors use by far the largest share of total electrical energy use in the industrial sector. In 1984, 656 BkWh was consumed for motor-drive end uses (DOE 1985). This comprised 68 percent of industrial electricity end usage. Obviously, if even small percentage changes in electrical energy use in this sector are achieved, the total savings could be relatively large.

Electrolytic processes are the second largest end use of electricity in the industrial sector, consuming about 114 BkWh in 1984 (DOE 1985). Almost 70 percent of this electricity is consumed in the primary metals industry, and most of the other 30 percent is used in the chemical and allied products industry.

3.5.2 Selected Industrial Technologies

The three technologies selected for further study could have major impacts on the electric energy used by motor drives and electrolytic processes. These selected technologies have the combined potential to annually save in excess of an estimated 197 BkWh electrical energy by the year 2000. Discussions of these technologies are presented below.

Variable-Speed Motor Controllers

Variable-speed drives allow electric motors to operate at varied speeds so as to match varying load requirements. The resulting closer match of motor output and load requirements reduces the electricity used in powering electric motors. Variable-speed drives are seeing increasing use in industries in which processes require speed control, where load requirements vary substantially over time and where soft-starting may reduce wear and tear on components. Several different types of power semiconductors and circuits may

be used to accomplish variable-speed control, but the most common technique is to use variable-frequency controllers.

Variable-speed motor controllers can save energy by reducing the throttling losses associated with varying motor load requirements. The typical net energy savings that can be expected from the use of variable-speed motor controllers are on the order of 25-30 percent (Hane et al. 1982). Thus, the potential energy savings of variable-speed motors could be as high as 139 BkWh.

Variable-speed motor controllers are commercially available and are generally regarded as being cost-effective in many industrial applications. The Electric Power Research Institute (EPRI) believes the potential for variable speed electric motor controllers to capture a significant part of the future industrial electric motor drive market is so great that they have initiated an entire research program to study the technology. In addition, the technology is distinct and readily identifiable. In summary, it appears that variable-speed electric motor controllers meet all of the selection criteria and consequently it is included in the selected set of technologies.

High-Efficiency Electric Motors

Energy-efficient electric motors are motors designed to minimize internal motor losses from such sources as stator winding resistance, rotor slip, bearing friction and stray load losses. The technology of energy-efficient motors incorporates only internal motor design changes that reduce internal motor energy losses. The reduction in electricity use that will result from the use of energy-efficient motors will depend upon the size of the motor. In general, the greatest reductions will occur in motor sizes from 5 to 50 horsepower, while the smallest reductions will occur in motors greater than 125 horsepower.

High-efficiency electric motors are motors that minimize the internal electrical losses of an electric motor. They can be used in association with either variable-speed or constant-speed motor drives. The energy savings of more efficient electric motors will generally range from 5 to 12 percent (ADL 1976). According to one estimate, the likely level of savings for energy-efficient motors by the year 2000 is approximately 35 BkWh (ADL 1976).

Energy-efficient electric motors are commercially available and, in many cases,

may be more cost effective than variable-speed controllers. In addition, energy-efficient motors are a distinct technology. In summary, energy-efficient motors seem to meet all of the selection criteria, and this technology has been selected for further study.

High-Efficiency Electrolytic Processes

An electrolytic process is basically a purification process that involves the application of an electric current to a substance to separate it into relatively pure components (i.e., into a pure gas or a pure solid deposit).

Several technologies are currently available for producing improvements in the energy efficiency of electrolytic processes. For example, efficiency improvements of 20 percent are achievable in existing aluminum plants using currently available technology (Alliance to Save Energy 1984).

The sources of improvements are numerous and include:

- improved cell design
- improved carbon electrodes
- changes in the chemical bath in which reduction takes place.

A 20 percent decrease in the electricity used in electrolytic processes could result in potential electricity savings of about 22 BkWh. Although these savings are relatively small compared to the potential savings in electric motors, they are relatively large compared to the potential savings in other industrial electricity end uses, such as process heating. In addition, the Department of Energy is currently sponsoring research to improve the efficiency of electrolytic processes that has the potential to produce even greater savings (DOE 1984).

More efficient electrolytic processes will not require major changes in current industrial modes of operation. Because more efficient electrolytic processes appear to meet all of the selection criteria, this technology has been selected for further study.

3.5.3 Industrial Technologies Considered But Not Selected

Explanations of why several other industrial conservation technologies were not selected for further study are presented below.

Industrial Motor Resizing, Clutched Flywheels, Torque Converters, ACS Chips

The technologies of industrial motor resizing and ACS chips save energy by more closely matching motor output to load requirements. They therefore compete with variable-speed motor controllers, and much of the electrical energy savings that may be available from these technologies may already be captured in our analysis of variable-speed motor controllers. Clutched flywheels and torque converters do not compete directly with variable-speed motor controllers. However, contacts with available experts and a review of available literature did not provide any information on these technologies. This indicates that their potential energy savings are likely to be small. Because some of the above technologies compete with variable-speed motor controllers and because the level of their potential energy savings appears to be small, they were not selected for further study.

Hydraulic or Direct Industrial Drive to Replace Electric Drive

This technology also competes directly with variable-speed electric motors at the end-use application level. However, because the use of this technology would involve significantly greater changes in industrial modes of operation than would the use of variable-speed drives, it appears that variable-speed drives offer greater market penetration potential. In addition, some experts^(a) question whether the energy-savings potential of hydraulic drive motors would be significant. One available study indicated that for the specific application of powered hand tools, the energy consumption of hydraulically powered hand tools could actually be greater than that of electrically powered tools (DOE/OIP 1977). In summary, it appears that the potential energy savings levels and market potential of hydraulic and direct industrial drives are too small relative to variable-speed motor controllers to be included in the group of technologies selected for further study.

Displacement of Steel and Aluminum by Composites Containing Graphite Fibers

The production of graphite fibers is likely to require less electrical energy than the production of steel and aluminum. Thus, if graphite fibers can replace steel and aluminum, the amount of electricity used in the industrial

(a) Personal communication with Ray Watts, mechanical engineer with Pacific Northwest Laboratory, October 1984.

sector will be reduced. However, replacement of steel and aluminum with graphite would likely require significant changes in existing industrial and commercial modes of operation. For this reason, this technology was not selected for further study.

Fluidized-Bed and Other Advanced Heat Treatment of Metal Parts

Use of a fluidized bed of chemicals in the heat treating of metal parts can reduce the amount of electricity used in this industrial process by facilitating more efficient heat transfer. However, because the total electricity used in the heat treating of metal parts is only 26 BkWh (DOE 1985), it appears that the potential energy savings of fluidized-bed heat treating processes are small. Even if fluidized-bed furnaces reduced electrical heat treating usage by 50 percent, the savings would be small relative to those that could be obtained for electric motor and electrolytic process end uses. Accordingly, this technology has not been selected for further analysis.

Advanced Lighting Technologies for the Industrial Sector

Lighting, space conditioning, and other end uses of electricity in the industrial sector consumed approximately 77 BkWh of electricity (DOE 1985). This total is only 17 percent of industrial electric use for motor drives and 75 percent of industrial electricity use in electrolytic processes. Obviously, very large improvements in the efficiency of these end uses would be necessary before the total electricity savings would compare to small improvements in the efficiency of other industrial end uses of electricity.

Advanced lighting technologies, such as high-frequency ballasts and more efficient fluorescent tubes, are discussed in detail in Section 3.4. Lighting technologies have not been selected for more detailed study here because of their small potential for electricity savings in this sector.

Daylighting

Daylighting, which involves the replacement of artificial light with natural light, could potentially be used to reduce energy use for lighting in the industrial sector. However, as discussed previously, the electric energy used for lighting in the industrial sector is relatively small. Thus, the potential energy savings from daylighting are likely to be small. The potential savings from daylighting are also limited by the fact that it is likely to

be cost effective only on new industrial structures. For these reasons, daylighting has not been selected for further study.

Energy Management Control Systems

Energy management control systems have the potential to save electrical energy in all industrial end uses by improving the efficiency and coordination of energy-consuming industrial processes. However, additional future energy savings from the use of energy management control systems are likely to be relatively small. This conclusion arises from the fact that energy management control systems are already used on a relatively widespread basis in industry. That is, the potential for future significant additions to the market penetration of energy management control systems is relatively small.

3.6 SUMMARY OF RESULTS

The ten technologies selected for a more extensive market analysis are summarized in Table 3.6. Only technologies that were not evaluated as having a "no" response for any of the selection criteria were selected. The total estimated long-term potential annual electricity savings for the ten selected technologies, based upon currently available estimates, is 727 BkWh. In the chapters to follow, detailed estimates are developed, technology by technology, which imply that most of the previous estimates of potential substantially overstate likely savings.

By comparison, Amory Lovin has estimated that over several decades, U.S. electricity consumption could potentially be reduced to one quarter of its present level through the full use of presently available, cost-effective energy-saving technologies (Lovins 1984). At current consumption levels, these potential savings exceed 1700 BkWh. Thus, the estimated potential electricity savings for the ten selected technologies could provide 40 percent of the potential savings estimated by Lovins.

TABLE 3.6. Conservation Technologies Selected for Market Analyses

<u>Electricity Consumption Sector</u>	<u>Selected Technology</u>	<u>Estimated Maximum Potential Electricity Savings(a) (BkWh) in 2000</u>
Residential	Advanced heat pumps	152
	Advanced insulation and anti-infiltration devices	96
	Solar water heaters	57
	High-efficiency appliances	32
Commercial	Advanced lighting	69
	Glazings/blinds	44
	Storage of heat and cool in the building structure	80
Industrial	Variable-speed motor controllers	139
	High-efficiency electric motors	35
	High-efficiency electrolytic processes	23
Total Estimated Electricity Savings	Ten selected technologies	727

(a) Estimates provided in literature obtained from various sources including DOE/BERD 1984) and (EPRI 1984).

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4.0 MARKET PENETRATION AND ENERGY SAVINGS ESTIMATION METHODOLOGY

This chapter describes the methodology used in the study to 1) estimate the likely energy savings associated with each of the ten technologies selected for further analysis and 2) compare the cost per kilowatt hour saved by each technology to the cost of new electrical generating plants.

An overview of the methodology for estimating future energy savings is provided in Figure 4.1. The four elements of Figure 4.1 are described in Sections 4.1-4.4.

FIGURE 4.1. Flow Diagram of Electrical Savings Estimation Methodology Employed in this Study

In Section 4.1, the methodology used in the study for estimating the maximum market penetration potential of conservation technologies is described. The general methodology for estimating the market sizes of the various conservation technologies is described in Section 4.2. Section 4.3 describes the method used to derive estimates of the energy savings potential of the various technologies. Section 4.4 describes the elements of a sensitivity analysis of the impacts of a low market penetration scenario and a high market penetration scenario on conservation technology energy savings. Section 4.5 discusses assumptions and data sources used in the market analysis. The chapter concludes (in Section 4.6) with a discussion of the methodology used to compare the costs of energy savings from the various conservation technologies to the energy costs of new electrical generating plants. Note that the analysis that the analysis considers only energy savings; because the load shape impacts of the technologies were not addressed this study we are not able to estimate the value of these savings to utilities.

4.1 MARKET PENETRATION ESTIMATION METHODOLOGY

As illustrated in Figure 4.1, the market penetration rates of the conservation technologies analyzed in this study are estimated as a function of their maximum market penetration potential and their likely rates of market adoption (i.e., the rate at which they reach the maximum overtime). This section describes how the "most likely" market penetration rates are derived; the methods used to derive the low and high market penetration estimates are presented in Section 4.4. A number of assumptions were necessary to derive estimates of the market penetration rates and some of these assumptions are described in this section. However, the specific data assumptions used in the study are described as part of the individual market analyses of each of the conservation technologies.

4.1.1 Maximum Potential Market Penetration Estimation

The maximum potential market penetration of a technology represents the highest percentage of the total market a technology is likely to ever achieve. Thus, as defined in this study, maximum potential market penetration estimates do not incorporate a time dimension. Most studies of the potential market

penetration of a technology in a given application have found that the most important factor determining this potential is the cost-effectiveness of the technology (e.g. Mansfield 1961; Fliegal and Kivlin 1966). There are various methods of measuring this cost-effectiveness, including net present value, internal rate of return, simple payback and incremental first cost.

Although discounted cash flow methods, such as net present value, are preferable in a theoretical sense, many studies have shown that a majority of potential purchasers of conservation technologies still behave as if they use simple payback to determine whether they will undertake a conservation investment (Moore 1983 and Kastovich et al. 1982). In reference to conservation technologies, simple payback is the length of time required for the technologies to return their capital investment through energy cost savings. Many potential investors will not purchase conservation technologies unless the payback period on their investment is less than three years (Moore 1983).

Various studies have shown that incremental first cost, as well as payback period, are important in determining the potential market for conservation technologies in the commercial and industrial sectors (Alliance To Save Energy 1984 and DOE/BERD 1984). Incremental first cost can be interpreted as the percentage increase in initial capital costs required for the purchase of a conservation technology rather than a conventional technology. Decision makers in the commercial and industrial sectors often indicate that, as a method of capital rationing, they will not purchase a conservation technology with significantly higher first costs than a conventional technology regardless of the length of the payback period for the conservation technology (Garrett-Price 1984).

In this study, the potential market penetration of the various conservation technologies are determined as a function of the payback period for each residential sector technology and percentage incremental first cost and payback period for each commercial and industrial sector technology. The equations used to calculate payback period and incremental first cost for the conservation technologies were the following:

$$CAP = (CV - CN) / CN \quad (4.1)$$

$$PB = (CV - CN) / (PES \times AEU \times EP) \quad (4.2)$$

where

CAP = Percentage incremental capital cost (including installation costs) of the conservation technology compared to the existing technology

CV = Capital cost of the conservation technology

CN = Capital cost of the conventional technology that the conservation technology could potentially replace

PB = Payback period in years for the conservation technology

PES = Percentage electricity savings of the new technology compared to the existing technology in decimal form

AEU = Annual electricity use in kWh of the existing technology that the conservation technology would replace

EP = Electricity price per kWh

The numerator in both of the equations described above is the incremental capital cost of the conservation technology. This numerator will vary depending on whether the conservation technology is used in a new application, a retirement application, or a retrofit application. To facilitate understanding of the differences between these applications, they are briefly described below.

For purposes of this study, a new application of a conservation technology is defined as an addition to the existing stock of the technology, while a retirement application represents a replacement of an existing technology that no longer operates properly. For example, an addition to the residential housing stock is treated as a potential new application of an advanced heat pump technology, while the replacement of a conventional HVAC system that no longer operates properly is treated as a potential retirement application. A retrofit application of a conservation technology is defined as the replacement of a conventional technology that is still operating properly with a conservation technology.

In both new and retirement applications of a technology, it is assumed that the choice faced by a potential purchaser of a conservation technology is whether to purchase a conservation technology or purchase a conventional technology. Thus, the payback period estimate for both new and retirement applications is based on the difference in capital costs between the two technologies. For example, if a conservation technology has an initial capital cost of \$500 and the conventional technology has an initial capital cost of \$300, then the numerator in the payback period and incremental first cost equations for new and retirement applications of the conservation technology would be \$200.

In retrofit applications, calculation of the payback period is based on an assumption that the initial capital cost of the conventional technology is zero because it is a cost that has already been incurred. Thus, the numerator of the payback period and incremental first cost equations is equal to the total initial capital cost of the conservation technology. In the example described above, the numerator would be \$500 for all retrofit applications of the conservation technology. Note that because CN is zero in retrofit applications, it is not possible to calculate incremental capital cost using equation 4.1. In the chapters that follow, where retrofitting is technically possible, we substituted an estimate of incremental capital cost for new/retirement applications for this incalculable variable.

The denominator for all of the potential applications of the conservation technology is the estimated annual energy cost savings in dollars. Thus, because the numerator used in calculating payback period and incremental first cost for new and retirement applications is smaller than that used for retrofit applications, the payback period for retrofit applications will be longer.

This study will rely on the results of an empirical study that identified residential consumer payback period requirements (Kastovich et al. 1982) as the basis for deriving maximum potential market penetration estimates. In Kastovich's study, several hundred residential home builders and owners were interviewed concerning whether they would purchase a conservation technology if the technology had a payback period equal to a specified number of years.

The interview results were compiled and percentages of builders and owners who stated they would purchase a conservation technology at various payback periods were calculated (e.g., 90 percent of home owners said they would purchase a heat pump if the payback period were one year or less). These percentages were used to represent the maximum potential market penetration that a conservation technology could achieve.

The market penetration results obtained in Kastovich's study are shown in Table 4.1. These results are used directly in estimating the baseline maximum potential market penetration that the four residential conservation technologies selected for analysis in this study are likely to achieve. To account for potential variance around the baseline maximum potential market penetration estimates shown in Table 4.1, a sensitivity analysis of the impacts

TABLE 4.1. Maximum Potential Market Penetration of Residential Conservation Technologies Estimated as a Function of Simple Payback(a)

Simple Payback, Years	Maximum Potential Market New Installations(%)	Penetration(b)
		Retrofit/Retirement Installations %
1	70	90
2	40	75
3	10	60
4		45
5		30
6		20
7		15
8		10
9		7.5
10		7.5
>10		5

(a) Source: Calculated directly from results of interviews of home builders and homeowners (Kastovich et al. 1982).

(b) Example interpretation of table is that if a residential conservation technology has a simple payback period of one year in new and retirement applications and three years in retrofit applications, its maximum potential market penetration will be 70 percent in new applications, 90 percent in retirement applications, and 60 percent in retrofit applications.

on conservation technology energy savings of modifying the estimates shown in Table 4.1 was performed. The major elements of the sensitivity analysis are described in Section 4.4.

The results shown in the second column of Table 4.1 are based upon the minimum payback requirements of new home builders. Thus, they are only applied to new applications of residential conservation technologies. The results shown in the third column of Table 4.1 are based on the minimum payback period requirements of existing home owners. Therefore, these results are applied to both retirement and retrofit applications of the conservation technologies. For example, if the calculated payback period for a residential technology is one year in new and retirement applications and three years in retrofit applications, then the maximum potential market penetration the technology would ever achieve is 70 percent in new applications, 90 percent in retirement applications and 60 percent in retrofit applications.

As stated above empirical evidence suggests that incremental first cost, as well as payback period, are important in determining the potential market for conservation technologies in the commercial and industrial sectors. In a study performed for DOE/BERD, estimates of the interaction between incremental first cost and payback period in determining maximum potential market penetration were presented (DOE/BERD 1984). These estimates are shown in Table 4.2.

The estimates shown in Table 4.2 are used directly in specifying the baseline maximum potential market penetration of the commercial and industrial conservation technologies analyzed in this study. For example, if the percentage incremental first cost of a commercial conservation technology is 10 percent and the payback period is one year in new and retirement applications, then the maximum potential market penetration of the technology in these applications would achieve is 75 percent. A sensitivity analysis of the impacts on industrial and commercial conservation technology energy savings of varying the baseline maximum potential market penetration estimates was also performed. The major elements of this analysis are described in Section 4.4.

TABLE 4.2. Maximum Potential Market Penetration^(a) of Commercial and Industrial Conservation Technologies Estimated as a Function of Percent Incremental First Cost and Simple Payback^(b)

First Cost Percentage Increase (%)	Simple Payback, Years				
	1	2	3	4	4
10	75%	65%	50%	45%	20%
20	50%	45%	40%	30%	10%
30	35%	30%	25%	20%	5%
40	30%	25%	15%	10%	0%
50	25%	15%	10%	5%	0%

(a) Source: Taken directly from results presented by DOE/BERD 1984.

(b) Example interpretation of table is that if a commercial or industrial conservation technology has a first cost percentage increase of 10 percent and a simple payback of one year, then its maximum potential market penetration will be 75 percent in both new and retirement installations.

The estimates presented in Tables 4.1 and 4.2 are based solely on economic considerations, without regard for technical limitations that may preclude certain applications of a technology. An example of such a technical limitation is that storage of heating and cooling in commercial building masses is only feasible in hollow-core buildings. Thus, commercial buildings that are not hollow-core should be excluded from the population of buildings that could potentially use this conservation technology.

The maximum potential market penetration for each conservation technology was estimated in this study using the following equation:

$$\text{MAXP} = \text{MPEN} \times (1 - \text{TL}) \quad (4.3)$$

where

MAXP = Maximum market penetration of each technology

MPEN = Maximum market penetration (in decimal form) obtained from Tables 4.1 and 4.2 as a function of payback period and (for the commercial and industrial sectors) incremental first cost

TL = Percentage of applications (in decimal form) where the use of a conservation technology would be technically infeasible

It should be noted that only in cases where there was a strong basis for applying technical limits were such limits applied. Thus, the technical limits parameter (TL) was zero for many of the conservation technologies.

4.1.2 Estimation of Market Adoption Rates

The market penetration of a conservation technology is a time dependent parameter. No conservation technology is likely to reach its maximum potential market penetration in a period as short as one year. The speed at which a conservation technology reaches its maximum market penetration can be defined as its market adoption rate, and this rate is dependent upon many factors.

E. M. Rogers, a rural sociologist, hypothesized that the rate of market adoption of a new technology is dependent upon: 1) its relative advantage compared to a conventional technology, 2) its compatibility with existing methods, 3) its divisibility into small units, 4) its ease of communication, and 5) its complexity (Rogers 1962). Economists, including Mansfield (1961) and Griliches (1958), have identified several variables likely to influence the rate of market adoption including: 1) profitability, 2) costs relative to other alternatives, 3) risk (both economic and technical), and 4) size of initial investment relative to the average value of assets of firms in the industry.

It was not possible within the scope of this study to evaluate how the factors listed above might apply to the rate of market adoption of the various conservation technologies, except in a subjective fashion. However, it was possible to make use of empirical studies that demonstrate that an S-shaped curve will generally reflect the rate of market adoption of a conservation technology more accurately than other types of functions (Blackman 1972). An illustration of such an S-shaped curve is shown in Figure 4.2.

In this study, the market adoption rates for the various technologies will be assumed to reflect an S-shaped curve. Thus, the fastest growth in market penetration is assumed to occur in the middle years between the point of technology introduction and maximum market potential. In the early years of product introduction and in the later years when the maximum rate of market penetration is approached, market adoption is assumed to occur at a slower rate.

FIGURE 4.2. S Shaped Market Adoption Curve

It is also assumed in the baseline analysis of this study that all of the conservation technologies will reach their maximum potential market penetration within 16 years, so that a technology that is currently available will reach its maximum potential market penetration by 2000. This assumption is consistent with several empirical studies of the rates of market adoption for various technologies (Blackman 1972). It is also consistent with assumptions used by BERD in forecasting the energy savings that will result from the use of conservation technologies (DOE/BERD 1984). However, to account for potential variations in the rates of market adoption of conservation technologies, a sensitivity analysis (described in Section 4.4) of the impacts on technology energy savings of varying these rates was performed.

Using the empirically based assumption of an S-shaped market adoption curve and the baseline analysis assumption that the maximum potential market penetration of conservation technologies would be reached by the year 2000 for all currently available technologies, the usage of conservation technologies was phased in over time. This procedure was performed by interpolating, using

an S-shaped function similar to the one illustrated in Figure 4.2, between the estimated level of the current market penetration of a conservation technology and the maximum potential market penetration estimated from Equation 4.3. For example, suppose the current market penetration of a conservation technology is estimated to be one percent and its maximum market penetration was estimated from Equation 4.3 to be five percent. The penetration rate would therefore increase four percent between 1984 and 2000. The market penetration of the technology would then be assumed to grow at a rate of .2 percent a year during the first five years (to 2.0 percent in 1989), .3 percent a year during the next three years (to 2.9 percent in 1992), .4 percent during the next three years (to 4.1 percent in 1995), .2 percent during the next three years (to 4.7 percent in 1998), and .15 percent during the last two years (to 5.0 percent in 2000). The specific levels of market penetration assumed for the conservation technologies in all years of the forecast period (1984 to 2000) are presented in tables in each of the chapters of this report.

4.2 MARKET SIZE ESTIMATION METHODOLOGY

Estimation of the size of the market in which each of the conservation technologies would be applied was performed using estimates of the existing stock of the conventional technology, forecasts of the future stock of the conventional technology, and assumed retirement rates for the conventional technology. Each of these elements are described in this section.

4.2.1 Existing Stock Estimation

In this study, existing stocks of conventional electricity consuming technologies are calculated using published estimates of the number of units of the conventional technology that currently exist and estimates of the percentages of these units that use electricity. Thus, the equation used to derive estimates of the existing stock of the conventional technology was the following:

$$EXS = POP \times PE \quad (4.4)$$

where

EXS = Existing stock of conventional technology that uses electricity

POP = Published estimate of the total number of existing units of the conventional technology

PE = Percentage of the total number of units of the conventional technology that use electricity

An example of an estimate used to represent the total number of units of a conventional technology (POP) is the number of single-family residences. This estimate is used to represent the variable POP for all of the residential conservation technologies. An example of an estimate used to represent the percentage of the total number of units that use electricity (PE) is the percentage of single-family residences that use electric water heaters. Because the estimates used in Equation 4.4 vary from one conservation technology to another, they are discussed in detail in the market analysis of each of the individual technologies. The sources of the estimates are also discussed as part of the market analyses.

4.2.2 New Stock Estimation

New stocks of the conventional electricity consuming technology are also derived from published estimates. Estimation of new stocks of the conventional technology was performed using the following equation:

$$NWS_i = FOR_i \times PE \quad (4.5)$$

where

NWS_i = New stock of conventional technology that uses electricity in year i , where $i = 1984$ to 2000

FOR_i = Published forecast of the total number of additions to the stock of the conventional technology in year i

An example of the variable FOR_i is a published estimate of additions to the residential housing stock in 1985. Note that the variable PE in Equation 4.5 is the same one used in Equation 4.4. Thus, in this study, it is assumed that the percentages of the total forecast number of new conventional technologies that use electricity are fixed at current estimated levels.

4.2.3 Retirement Stock Estimation

Retirement stocks are estimated as a function of the total number of existing units of a conventional technology, the percentage of these units that use electricity, and the expected lifetime of the conservation technology. The equation used to calculate retirement stocks is the following:

$$RS_i = (EXS / EL) \times PE \quad (4.6)$$

where

RS_i = Number of units of the conventional technology that use electricity retired in year i , where $i = 1984-2000$

EL = Expected life of the conventional technology obtained from published studies

For conservation technologies that represent an add-on rather than a replacement of a conventional technology (i.e. solar water heating systems), the retirement of the conventional technology should not affect the rate of usage of the conservation technology. Thus, for add-on technologies, the net retirements of the conventional technology were assumed to be zero.

4.2.4 Forecasting the Number of Units of the New Technology

In this study, forecasts of the number of units of the new technology that will be in use in future years are obtained by integrating the likely market penetration rates for the new technology with estimates of the stocks of the conventional technology. The following three equations were used to develop these forecasts:

$$ANU = \sum_{i=1}^n NWS_i \times MPN_i \quad (4.7)$$

$$ARU = \sum_{i=1}^n RS_i \times MPR_i \quad (4.8)$$

$$EU = (ES - ARU) \times MPE_i \quad (4.9)$$

where

ANU_n = Aggregate number of units of a conservation technology that will be installed in new applications in forecast year n , where $n = 1985, 1990, 1995$ and 2000

MPN_i = Likely level of market penetration of a conservation technology in new applications in year i , where $i = 1984$ to 2000

ARU_n = Aggregate number of units of a conservation technology that will be installed in retirement applications in forecast year n , where $n = 1985, 1990, 1995$ and 2000

MPR_i = Likely level of market penetration of a conservation technology in retirement applications in year i , where $i = 1984$ to 2000

EU_n = Number of units of a conservation technology that will be installed in retrofit applications in forecast year n , where $n = 1985, 1990, 1995$ and 2000

MPE_i = Likely level of market penetration of a conservation technology in retrofit applications in year i , where $i = 1984$ to 2000

The market penetration variables used in the above equations obtained by integrating the results derived from Equation 4.3 with information about the likely rate of market adoption for each of the conservation technologies. Note that because the number of new and retirement applications are changing every year, it is necessary to aggregate the annual unit estimates to obtain an estimate of the total number of units that will utilize the technology in new and retirement applications between the beginning of the current year (1984) and the selected forecast years.

When an existing unit of a conventional technology is assumed to be retired because it is no longer operable, it is subtracted from the existing stock of the technology and added to the retirement stock. This does not change the total number of applications that the conservation technology could potentially be applied in. However, it does allow for a different rate of market penetration to be applied to situations where the existing conventional technology is retired compared to situations where retrofitting is being considered for reasons of energy cost savings alone.

4.3 ENERGY SAVINGS ESTIMATION METHODOLOGY

Once forecasts of the number of units that would use the conservation technologies in the various forecast years were obtained, the energy savings potentials of the technologies were calculated using the following equation:

$$ESV_n = (ANU_n + ARU_n + EU_n) \times (PES \times AEU) \quad (4.10)$$

where

n = Forecast energy savings for a conservation technology in forecast year n, n = 1985, 1990, 1995 and 2000

PES = Percentage electricity savings of the new technology compared to the existing technology in decimal form

AEU = Annual electricity use in kWh of the existing technology that the conservation technology would replace

A number of assumptions were necessary to forecast energy savings potential using the Equations 4.1 to 4.10. These assumptions are described as part of the individual market analyses of the conservation technologies.

4.4 SENSITIVITY ANALYSIS OF ESTIMATED ENERGY SAVINGS

As indicated in the information presented elsewhere in this chapter, a number of factors will influence the electrical energy savings that are likely to be obtained from the use of conservation technologies. Among these factors are the capital and operating costs of the technologies, their energy savings abilities, the maximum market penetration they will achieve, and the rate at which they will reach their maximum market penetration. All of the factors that could influence the energy savings of the various conservation technologies are subject to significant uncertainty. Two of the most important and most uncertain factors appear to be the level of the maximum market penetration the technologies will achieve and the rate at which this maximum is reached. Thus, these two factors were selected to be incorporated in performing a sensitivity analysis of the estimated energy savings that are available from the various conservation technologies.

The major elements of the sensitivity analysis performed on the various conservation technologies were the following:

- a low scenario was implemented, which assumed that the maximum potential market penetration of each conservation technology was half of the value obtained from Table 4.1 or 4.2 and that a slower rate of market adoption would result in only 75 percent of the maximum potential market penetration being reached by 2000;
- a high scenario was implemented, which assumed that the maximum potential market penetration of each conservation technology was twice as large as the value obtained from Table 4.1 or 4.2 and that a faster rate of market adoption would result in the maximum potential market penetration being reached by 1995.

For some of the conservation technologies, the elements of the sensitivity analysis were modified from those listed above to account for such factors as technical limitations to the widespread use of a technology, the late introduction of the technology several years into the forecast period, and maximum potential market penetration rates that when doubled would exceed 100 percent. These modifications are described in more detail in the chapters of this report that present the results of the sensitivity analysis for each of the selected conservation technologies.

4.5 INPUT ASSUMPTIONS AND DATA SOURCES

In order to estimate likely energy savings attributable to technologies addressed in this study, it was necessary to make assumptions about several key input. This section discusses general input assumptions used along with their sources and reasons they were chosen. More specific input assumptions, relevant only to one or two conservation technologies, are not included here, but are discussed in the individual market analyses of each technology. Table 4.3 summarizes the common input assumptions and their sources.

4.5.1 Electricity Prices

The principle motivating factor for the adoption and installation of produces incorporating energy conservation technologies is to save money. The level of expected savings is a key factor in an end users decision on

TABLE 4.3. Common Input Assumptions

<u>Assumption</u>	<u>Source</u>	<u>Comments</u>
Electricity Price	<u>Annual Energy Review 1983</u> (DOE 1984)	Residential 7.18 cents/kWh Commercial 7.01 cent/kWh Industrial 4.97 cents/kWh
Housing Stock	<u>Energy Projections to the Year 2000</u> (DOE 1983)	Estimates provided for 1985, 1990, 1995 and 2000. Estimates derived using assumed 2% annual growth rate.
Commercial Floorspace	<u>Annual Energy Outlook 1983</u> (DOE 1984)	Floorspace estimate in square footage provided for 1983-1990 and for 1995. Estimates for other years derived using an assumed 2% annual growth rate.
Motor Populations	<u>Classification and Evaluation of Electric Motors and Pumps</u> (ANL 1980)	Estimates presented for 1978. Estimates for study time frame derived assuming constant annual motors additions and retirement.

whether or not to invest in a conservation technology. As the level of savings is directly related to the price of the energy saved, it was important to choose representative electricity prices.

Prices of 7.84 ¢/kWh for the residential sectors, 7.01 ¢/kWh for the commercial sector, and 4.97 ¢/kWh for the industrial sector from the Annual Energy Review 1983 (DOE 1984) were chosen as being the most reliable. These represent the average price of electricity sold by the electric utility industry for 1983. Prices for 1983 were used since they were the most current during the time this study was undertaken.

Real prices for electricity are assumed to remain constant for the 1984-2000 timeframe. This is consistent with the projections EIA has published the Annual Energy Outlook for 1984 (EIA 1985). Their findings indicate that real electricity prices are expected to remain stable or decline slightly throughout the forecast period. Except as noted all prices other than those for electricity quoted in this study are in 1984 dollars.

4.5.2 Residential Sector Assumptions

A good indication of residential energy use activity is projected housing stock. Estimates of residential housing stock are based on NEPP data published in Energy Projections to the Year 2010 (DOE 1983). Based on the point estimates given for the years 1985, 1990, 1995 and 2000, projections were interpolated for other years within the study timeframe using the 2 percent annual housing growth rate cited in that report.

Within our analysis, new housing is assumed to be equivalent to the incremental difference between the current year's housing stock and the previous year's housing stock. There is assumed to be no housing stock retirement.

Estimates of household fuel shares for specific uses and percentages of households employing certain appliances were derived from the 1982 Residential Energy Consumption Survey (DOE 1983). The estimates derived from the survey are further assumed to remain constant through the year 2000.

4.5.3 Commercial Sector Assumptions

Due to the great variance in the size and type of commercial buildings, actual population figures alone may not be sufficient to give a clear indication of the level of commercial activity. Subsequently a better indication of commercial activity, total commercial floorspace, was chosen. Projections of total commercial floorspace are based on estimates reported in the Annual Energy Outlook 1983 (DOE 1984). Using the estimates provided for the years 1983-1990 and 1995, estimates were interpolated for 1991-1994 and extrapolated to 2000 assuming a 2 percent annual growth rate. New commercial floorspace is estimated as the incremental difference between estimates for consecutive years. Floorspace retirement is assumed to be zero.

4.5.4 Industrial Sector Assumptions

Population estimates for electric motors used in analysis of high efficiency motors and alternate speed motor drives were taken from data prepared by Argonne National Laboratory (ANL) for DOE in 1980. These estimates are based on motor populations for 1978. In our analysis we assume that there

has been no growth between the 1978 and 1984 motor populations and that for the years 1985 and 2000, new additions and unit retirement occur at a fixed annual amounts.

Detailed information on input assumptions and data sources used for our market analysis of electrolytic processes is presented in the chapter devoted to that topic.

4.6 ENERGY COST ESTIMATION METHODOLOGY

The demand for electrical energy is expected to grow in the future. To meet that growth in demand, there are two primary utility investment alternatives that have been receiving consideration. One alternative is for utilities to invest in new electricity-generating capacity. The other alternative is for utilities to invest in (i.e., subsidize the installation of) conservation measures so as to make better use of the electricity-generating capacity that already exists. This section is a description of the methodology used to compare these alternatives on the basis of their respective levelized cost per kWh of electricity either produced or saved.

4.6.1 Cost per kWh of New Electricity Generating Capacity

The principal types of new electricity-generating units scheduled to become operational over the next ten years are nuclear and coal-fired power plants (Smolen et al. 1983). The estimated costs to the consumer of the electricity produced by such power plants is presented in Table 4.4. In general, these costs are calculated by estimating the levelized (i.e., discounted) annual capital costs associated with the power plants, adding these costs to the estimated annual variable costs of the power plants (i.e., fuel, labor, etc.) and dividing the sum of the two costs by the expected annual kWh production of the plants. The wide variation in the cost estimates across the ten DOE regions (see Figure 4.3) as well as between the nuclear and coal-fired type units should be noted.

4.6.2 Cost per kWh of New Conservation Technologies

Each of the ten conservation technologies discussed in Chapters 5.0 through 14.0 is an investment in reducing future electricity consumption. Therefore,

TABLE 4.4. Regional Costs of New Power (cents/kWh, constant 1982 dollars)

Region	1 Northeast	2 NY-NJ	3 South Mid-Atlantic	4 Atlantic	5 Midwest	6 Southwest	7 Central	8 North Central	9 West	10 Northwest	National Average ^(c)
Nuclear											
Capital(a)	3.75	3.89	3.45	3.34	3.67	3.49	3.56	3.49	4.04	3.78	3.59
O&N(a)	0.57	0.57	0.57	0.57	0.57	0.57	0.57	0.57	0.57	0.57	0.57
Decommissioning(a)	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.04
Fuel(a)	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11	1.11
Transmission and Distribution(b)	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
Total	5.97	6.11	5.67	5.56	5.89	5.71	5.78	5.71	6.26	6.00	5.81
Coal											
Capital(a)	2.42	2.42	2.23	2.16	2.33	2.26	2.26	2.23	2.58	2.40	2.30
O&N(a)	0.46	0.46	0.46	0.46	0.46	0.34	0.46	0.34	0.34	0.34	0.42
Fuel(a)	2.92	2.57	2.28	3.02	2.23	3.01	1.98	1.17	2.81	2.91	2.60
Transmission and Distribution(b)	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
Total	6.30	5.95	5.47	6.14	5.52	6.11	5.30	4.24	6.23	6.15	5.82

(a) DOE/ORNL 1983

(b) DOE 1983

(c) National averages are weighted average values based on projected regional electricity generation levels in 1995.

Source: 1981 Annual Report to Congress, DOE/EIA-0173(81)/3(S-2), pp. 345-356.

FIGURE 4.3. The Ten DOE Regions of the United States

it is possible to estimate the levelized cost per kWh of electricity saved by such investments. To do this, the incremental capital cost of each technology is converted to a discounted annual cost and then divided by the annual kWh savings expected to be obtained from the technology.

$$C_j = \left[(CV_j - CN_i) \left(\frac{d(1+d)^n}{(1+d)^n - 1} \right) \right] / ESA_j \quad (4.11)$$

where

CN_i = the capital cost of the conventional technology i that the conservation technology j would replace

ESA_j = the electricity saved annually by conservation technology j

d = the real discount rate used to levelized the incremental capital costs of conservation technology j

n = the useful lifetime in years of conservation technology j ;

The term in brackets in the equation presented above is a method for converting the present value of the incremental capital costs of the conservation technologies to a discounted stream of annual payments. In principle, these payments can be regarded as being similar to equal mortgage payments that are used to amortize the debt on a home or other type of property. Use of the above equation allows for the cost per kWh saved by conservation technologies and the costs per kWh produced by new generating plants to be compared on a consistent basis.

An eight percent real discount rate was selected for computing the discounted, levelized cost per kWh saved for the various conservation technologies. This discount rate was computed by subtracting an estimated average future inflation rate of five percent from a representative long-term utility bond interest rate of 13 percent (Wall Street Journal 1985).

4.6.3 Cost Comparisons: New Generation Capacity versus Conservation Measures

Following estimation of the nationally representative cost per kWh saved for each technology, a direct comparison can be made between those costs and either the regional costs or the national average cost per kWh of new generating capacity. For conservation technologies that on either a regional or national basis are less costly than new power plants, it is feasible for utilities to invest in the technologies to save power rather than investing in power plants to produce electricity. Note, however, that an estimate of a conservation technology's nationally representative cost per kWh saved may be significantly different from an estimate of the cost per kWh saved in the utility service area. Such differences are especially likely for the residential and commercial space heating and cooling technologies, since heating and cooling energy use loads vary considerably from region to region. Much analysis at the utility level will be required to identify an economically optimal portfolio of utility investments.

The estimated cost per kWh saved should serve as a general guide. Actual costs saved per kWh by the technologies evaluated in specific applications could vary considerably from the values estimated. As there is some uncertainty

as to the actual kWh cost savings that will result from the adoption of these technologies, further work might concentrate on better identifying the range of values that specific technology cost saving can take on.

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5.0 ADVANCED HEAT PUMP TECHNOLOGIES

The intent of this chapter is to estimate the potential national electrical energy savings that could occur in the years 1985 to 2000 as a result of recent technological improvements in residential space conditioning heat pump (HP) systems. Of specific interest is the estimate of the potential electrical energy savings that could result from the new high efficiency electric water-to-air and gas-fired heat pump heating, ventilating, and air conditioning (HVAC) systems.

In terms of their efficiency of energy input utilization and of their cost-effectiveness, these "advanced" heat pumps have emerged as a reasonable alternative in the residential HVAC market. They typically use 50 to 75 percent less electrical energy than conventional electric resistance (ER) HVAC systems use to produce the same annual output of heating and cooling services. In addition, these "advanced" HPs achieve the efficiency gains that they do at low enough purchase and installation costs to be considered as economically viable alternatives in the residential HVAC market. Hence, to the degree that these advanced HPs could be assumed to capture some share of the HVAC market by some future date, they will contribute toward the conservation of electrical energy.

The analysis begins with a review of the technical background of heat pump systems in Section 5.1. Section 5.2 describes the present and the expected future conditions of the residential HVAC market. Section 5.3 deals with the issues of cost-effectiveness and of estimating the potential for new heat pump systems to penetrate the HVAC market. In Section 5.4., the market penetration estimates of Section 5.3 are applied to housing stock data and forecasts to obtain estimates of future yearly installations of new-technology heat pumps. Section 5.5 presents the estimates of the maximum likely potential for annual electrical energy savings due to the implementation of new residential heat pump technologies by the years 1990, 1995, and 2000, along with a brief discussion of those results. Section 5.6 is an analysis of the sensitivity of the energy savings results to changes in the market penetration scenarios.

Finally, Section 5.7 presents the estimated cost per kWh saved by the new heat pump systems and discusses how those costs compare with the cost per kWh of new electrical generating capacity.

5.1 TECHNICAL BACKGROUND

The history of heat pump technology begins in 1850 with an Irishman by the name of Lord Kelvin. By combining and applying several different but related physical principles he developed what he was to call a "heat multiplier." That system was to become the forerunner of the heat pump systems of today.

To understand how heat pump systems work to save energy one must first understand those same basic physical principles put to use by Lord Kelvin. Those principles are 1) some heat exists in any matter until it reaches the ultimate low temperature of -460°F or -273°C , 2) heat always flows from a warmer element to a cooler element, 3) compressing a gas causes its temperature to rise while expanding it causes it to cool, 4) heat is absorbed when a liquid evaporates and is released again upon condensation of the vapor, and 5) both temperature and pressure influence whether a refrigerant (i.e., a liquid that boils at a "low" temperature) is in its liquid or gas phase.^(a)

Accordingly, Lord Kelvin's "heat multiplier" and modern heat pump systems work by circulating a refrigerant continuously in a closed cycle while alternately and strategically compressing and expanding it. The expanded and cooled refrigerant picks up heat from a source (typically air or water) via an evaporator and then, when compressed, releases that captured heat to a more desired location via a condenser. Note that neither gas-fired nor electric heat pumps "produce" heat as conventional HVAC systems do but rather they "pump" existing heat from a less desired location to a more desired location. Also note that the only energy input for heat pump systems is that which is used to operate a motor driven fan and a compressor. The compressor both propels the refrigerant through the system and creates pressure changes to either enhance the evaporation or the condensation of the refrigerant. Such systems are entirely reversible so that heat can either be pumped indoors during winter or outdoors

(a) See McGuigan 1982, Nesbit 1984, and OECD 1982.

during summer. In essence heat pumps use less energy than conventional electric resistance HVACs because they typically require less energy to move a given amount of heat than is required by a conventional HVAC to create that same amount of heat.

At present, the most common heat pump HVAC system is the electric air-to-air type system. Such systems are now capturing about 50 percent of the market for new electric installations and have already captured up to 25 percent of the total residential electric HVAC market (DOE 1984 and Cairns 1984).

The new water-to-air heat pump models are commonly more than 25 percent more efficient than the more common air-to-air units (McGuigan 1982). The efficiency difference is due to the fact that a water source (i.e., water from a well, lake, river, ocean, or municipal water system) usually has a higher temperature than winter air and a lower temperature than summer air, so it can better serve as a source or as a receptor of heat. That is, water-to-air HPs pump heat into and out of residences more efficiently because a water source makes it easier for the system to collect or to reject heat so that more heat can be pumped with less system effort.

The gas-fired heat pump models that are currently under development are different from electric models because the motor that drives the compressor operates on gas rather than electric power. Again, the gas fuel is not burned to "produce" heat for direct use but rather to power a motor that "pumps" heat from one location to another. Such systems are likely to become popular primarily because they are expected to be cheaper to operate than electrically powered models. They will be cheaper to operate because gas is about one-third the cost of electricity per unit of equivalent energy delivered to the compressor motor.^(a) Hence, even though gas-fired HPs are expected to be somewhat

(a) The present national average price for natural gas is about 63 cents per therm of energy (DOE 1984) which when converted into an energy equivalent number of kWhs, is comparable to about 2.4 cents per kWh. This compares to the current national average residential electricity price of 7.18 cents per kWh.

less efficient than electric models in an energy input-per-unit-of motor output sense, they are still likely to be less expensive to operate due to the difference in fuel input costs.

5.2 CURRENT MARKET SITUATION

Heat pumps first became commercially available during the 1950's and the early 1960's. Those years proved to be a period of initial market popularity for HP systems. By the mid 1960's, however, it became apparent that these "first generation" HPs were plagued with problems and design flaws and that the industry lacked the trained personnel to service them. The electric resistance type HVAC therefore systems captured the major market share. By the mid-1970's, the energy saving potential of HP systems became an important economic consideration in residential space conditioning system choice. Also, by that time the design flaws of the earlier HP models had been remedied in a "second generation" of better designed and more reliable HP systems. Consequently, as has been mentioned above, the "second generation" electric air-to-air HPs have made significant gains in the residential space conditioning market during the past several years.

Of the "third generation" of heat pump technologies (i.e., the electric water-to-air and the gas-fired models), only the electric water-to-air systems are presently being actively marketed. An estimated 115,000 water-to-air type systems are currently in use, which is less than one percent of the residential electric HVAC market.^(a) However, these advanced HP systems appear to be becoming more popular.^(b)

Gas-fired heat pump technologies are not currently commercially available in the United States. They are, however, receiving large expenditures for development.^(c) They could be commercially available and competitive by the

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- (a) Estimates were obtained via a phone conversation with a representative of the Air-Conditioning Research Institute.
 - (b) See McGuigan, 1982 and according to phone conversations with representatives of the Singer Company - Climate Control Division and others.
 - (c) See Chan 1984, Hlawiczka 1984, Kawamoto 1984, Nakatani 1984, and Tanaka 1984.

late 1980s or early 1990s. Specifically, the anticipated market potential for gas-fired heat pump systems ranges from a moderate market share to a near domination of the market by the year 2000 (GRID 1983).

5.3 COST EFFECTIVENESS AND MARKET PENETRATION

In this section, the cost effectiveness of the new electric water-to-air and gas-fired heat pump technologies will be estimated. An analysis such as this is basically a cost comparison between competing alternatives, similar to the sort of comparison a typical consumer would consider before deciding which of several alternatives to buy. The underlying presumption is, of course, that market penetration depends on consumer acceptance and choice. As an extension of the cost-effectiveness analysis, a forecast of the likely market share of each alternative at a given point in time can be obtained (see Chapter 4). Such forecasts ought to be considered as a rough appraisal of what might be the case given a specific economic scenario.

5.3.1 Cost Effectiveness

The primary market competitors of the new HP technologies are electric resistance (ER) HVAC systems and electric air-to-air (ATA) HP systems. At present, the existing electric HVAC stock (i.e., in existing homes) is about 75 percent ER-type systems and about 25 percent ATA heat pump systems. The new installation electric HVAC market mix is about 50 percent ER systems and 50 percent ATA heat pump systems. The ATA heat pump systems typically have a somewhat higher initial capital cost and a somewhat lower cost of operation than ER type systems. Appropriate consideration must be given to these facts when a scenario of representative initial capital and operation cost figures are selected for a base case "conventional" HVAC unit. In light of this, a reasonably representative figure for the installed capital cost of a base case conventional HVAC unit is assumed to be \$2900. Likewise, the installed capital

cost figures selected to be representative of the electric water-to-air with an available water supply and the gas-fired heat pump systems were, respectively, \$4100 and \$4200.^(a)

The achievable efficiency gain from employing the new technology can be determined by comparing the "seasonal performance factor" (SPF) of the new technology to that of the conventional technology. The SPF is a measure specifically designed for such direct comparisons. That is, because HVAC energy efficiency comparisons are typically made against a standard conventional HVAC type system, the SPF was defined to equal 1.0 for those systems. Hence, if an alternative system had a SPF of 2.0, that system would use just half of the energy required by a conventional unit to produce the same output of heating or cooling services.

The SPF measure employs the word "seasonal" because HVAC efficiencies vary from season to season as well as from region to region. Accounting for all such variations in efficiency levels is beyond the scope of the present analysis, so that it will be assumed that there is only one average or representative national SPF for each of the technologies. The national SPF value selected to be representative electric water-to-air heat pump systems is 3.0 in both heating and cooling modes of their application. This value was chosen based on the approximate average of values reported by major U.S. manufacturers.^(b) For the gas-fired heat pump units, that figure is 1.5 for heating and 1.0 for cooling (but recall that gas provides the same energy input at one-third the cost of electricity at present prices).^(c)

The consumption of electricity for home heating and cooling purposes varies greatly from region to region. Attempting to account for all such variations in this analysis would be prohibitively costly. Again, represen-

(a) The figures for the conventional HVAC unit and for the electric water-to-air heat pump were obtained from (McGuigan 1982). The acceptability of those figures was confirmed via several informal telephone conversations with relevant market vendors. The figure for the gas-fired heat pump unit was obtained from Itteilag and Swanson (1984).

(b) See the "Manufacturers Index" of McGuigan (1982).

(c) For the SPF estimates of a representative gas-fired heat pump system, see the "intermediate case" in Itteilag and Swanson (1984).

tative national average figures were employed here for analytical simplicity. Specifically, it will be assumed that the average electrically heated home uses approximately 5900 kWh per year for heating and that the average electrically cooled home uses approximately 2300 kWh per year for cooling.^(a) Using these figures and the national average price of electricity for 1983 of 7.18 cents per kWh (DOE 1984), the average electrically space-conditioned household which uses the conventional HVAC technology would (on average) spend approximately \$420 per year on electricity for heating and about \$165 per year on electricity for cooling.

In a new house or for the replacement of a worn-out HVAC system (i.e., in a retirement application), the installation of an electric water-to-air heat pump system in lieu of a conventional HVAC will initially cost the purchaser an additional \$1200.^(b) However, a water-to-air heat pump uses only about one-third of the electricity that a conventional HVAC system would use. Because of its greater efficiency, the water-to-air heat pump system would save approximately \$280 per year in electrical heating costs and approximately \$110 per year in electrical cooling costs for an average annual electricity cost savings of approximately \$390. Therefore, the estimated payback period for the purchase of an electric water-to-air heat pump system installed in a new house assuming cost-less access to an existing water supply (i.e., a private well or a lake or stream) is a little more than 3 years.^(c)

If a consumer was to consider the benefits of retrofitting an existing conventional HVAC system (i.e., one that still has its original value and service-producing potential) with an electric water-to-air heat pump system, the incremental capital cost would be \$4100. This implies that the consumer could expect the system to pay for itself in approximately 10.5 years (i.e., \$4100 divided by \$390 per year).

The actual number of properties with nearly cost-less access to a water supply is unknown but clearly it would be significantly less in both the new

(a) The rounded figures very closely approximate an average figure computed from residential energy consumption information found in DOE/EIA (1984).

(b) \$4100 minus \$2900.

(c) \$1200 divided by \$390 per year.

and the existing home markets than the total number of homes. That is, in some (unknown) number of cases, a new well may have to be dug at an additional cost of \$3,000 to \$4,000, or the water to be used in the system may have to be purchased from a municipal supply system at some additional cost to the consumer. Water-use costs such as these would be expected to be highly variable from municipality to municipality and therefore would be difficult to quantify in a representative fashion. Because of this and because the number of such cases is unknown, these cases were not differentiated from the base-case (i.e., cost-less access to water) set of cost assumptions. Hence, the base-case scenario is optimistic in its cost assumptions and, consequently, in its market penetration potential.

The installation of a gas-fired heat pump system in a new house or for the replacement of a broken or worn-out system will initially cost the purchaser approximately \$1300 more than a conventional electric resistance HVAC system. However, because the assumed representative SPF in the heating phase of a gas-fired heat pump system is 1.5, that implies that they are about 33 percent more energy efficient for heating. As mentioned above gas is about 70 percent less expensive to use per unit of output than electricity. Hence, the average annual savings on the typical fuel bill for heating for a representative gas-fired heat pump heating system would be approximately \$335 per year.

For cooling, a gas-fired heat pump system would likely not be any more energy efficient than the conventional electrical HVAC system but the fuel cost for gas power is much less than that for electrical power. Because of this price-of-power differential, the fuel cost for cooling the average household would be approximately \$115 per year less for the gas-fired heat pump system than for the conventional alternative.

The annual energy cost savings for the average household would, under the above specified conditions, sum to approximately \$450 per year for heating and cooling with a representative gas-fired heat pump system. These savings imply a simple payback period of less than 3 years in a new housing installation (\$1300 incremental capital cost divided by \$450 in savings per year) and of a little more than 9 years if purchased as a retrofit system (\$4200 divided by \$450 in savings per year). These results are summarized in Table 5.1.

5.3.2 Market Penetration

The estimated rate of market penetration of each of the new heat pump technologies depends on many factors. Among the most important of these factors are 1) the initial incremental capital costs of the new technology, 2) the simple payback period, 3) whether the technology is being considered as a new installation or as a retrofit installation, 4) the size of the new and the retrofit markets, and 5) whatever technical limitations there may be to the effective implementation of the technology. The capital costs and the payback periods are reported in Table 5.1. Note that our estimated payback periods are for residences that are both heated and cooled electrically. We have not estimated separate payback periods (and thus market penetrations) for electricity cooled only and electrically heated and cooled residences. One would expect that the payback period for electrically cooled only residences would be longer than for those both heated and cooled electrically because the annual fuel-bill savings would be smaller. However, an examination of this phenomenon was not performed in this analysis due to time and resource constraints.

The market penetration analysis is further complicated by the likelihood that the two new-technology HP systems will, in fact, be competing against each other for HVAC market share as well as against the conventional technology. To the degree that this occurs, the market penetration estimates presented below could be overstated, since we do not account for this in our analysis.

There are some technical constraints to the implementation of each of the new heat pump technologies. For example, the water-to-air heat pump system is an economically reasonable HVAC alternative only in those instances for which the consumer would have low-cost access to a sufficient water supply (i.e., a lake, river, or well). In fact, about 11.5 million homes have access to their own well, about 60 percent of which have sufficient flow capacity to accommodate the return flow of a water-to-air heat pump.^(a) More importantly, properties with low-cost access to an alternative water source would be expected to be numerous since many communities are located close to either a

(a) This information was obtained via a telephone conversation with John Voztek, National Water Well Association, November 21, 1984.

TABLE 5.1. Heat Pump Space Conditioner Simple Pay-Back Calculations

	Conventional Electric HVAC	Electric Water-to-Air Heat Pump	Gas-Fired Heat Pump
Capital Cost (\$)	2900	4100	4200
Seasonal Performance Factor (SPF)			
Heating	1.0	3.0	1.5
Cooling	1.0	3.0	1.0
Annual Household Energy Consumption			
Heating (kWh)	5900	1950	3950 ^(a)
Cooling (kWh)	2300	760	2300
Total (kWh)	8200	2710	6250
Energy Cost (cents per kWh)	7.18	7.18	2.14
Annual Fuel Bill (\$)			
Heating	420	140	85
Cooling	165	55	50
Total	585	195	135
Annual Savings on Fuel Bill (\$)	--	390	450
Incremental Capital Cost (\$)			
New Housing	--	1200	1300
Retrofit	--	4100	4200
Retirement	--	1200	1300
Pay-Back Period (yrs)			
New Housing	--	3	3
Retrofit	--	10	9
Retirement	--	3	3
Maximum Market Penetration (Percent)			
New Housing	--	10	10
Retrofit	--	5	7.5
Retirement	--	45	45

(a) kWh are energy equivalents.

lake or river. However, some (unknown number of) properties do not have low cost access to water. Those properties could still buy water from a municipal source, drill a new well, or install a technically advanced "closed-loop" type water system but only at considerably higher operation or installation cost. Hence, in those instances electric water-to-air HP systems are likely to be considered uneconomical and as such they are not explicitly considered in this analysis. To the degree that the housing stock figures used in this analysis are not net of this (unknown) number of properties inappropriate for the technology, our results overstate what would be the anticipated market penetration of water-to-air HP systems in the residential HVAC market, since we do not account for this in our analysis either.

The most apparent drawback to the immediate implementation of the gas-fired heat pump systems is that they are not likely to be actively marketed in the United States until about 1990. Another important consideration regarding the likelihood of their implementation would be the degree of availability and the relative per-unit energy cost of gas as opposed to electricity across the nation.

Mindful of these limitations, the reader is referred to Table 4.1, which relates the simple payback period for new and for retrofit installations to the percent rate of market penetration. From that table we see that the estimated market penetration of the electric water-to-air HP systems into the electric HVAC market is 10 percent (due to an estimated 3 year payback) of the new housing market, 45 percent (3 year payback) of the retired units market, and 5 percent (10 year payback) of the retrofit market. The estimates for gas-fired HP systems are 10 percent (3 year payback) of the new housing market, 45 percent (3 year payback) of the retired units market, and 7.5 percent (9 year payback) of the retrofit market. These results are summarized at the bottom of Table 5.1.

5.4 HOUSING STOCK PROJECTIONS AND MARKET SHARE ESTIMATES

Tables 5.2 through 5.5 present projections of housing stock and market share percentages at yearly intervals to the year 2000. The housing stock projections are based on estimates used by the DOE for computations in the

TABLE 5.2. Housing Stock Projections and Electric Water-to-Air Heat Pump Market Share Estimates for Electrically Heated and Cooled Residences

Year	Total Residences (a) (10 ⁶)	Retrofit Market (b) (10 ⁶)	Retired Units Market (c) (10 ⁶)	New Market Additions (a) (10 ⁶)	Residences Electrically Heated and Cooled (d) (Percent)	Retrofit Market Share (e)	Retired Units Market Share (e)	New Market Additions Share (e)	Annual Additions of New Technology Heating and Cooling Units (f)	Cumulative New Technology Heating and Cooling Units (g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units (h) (BkWh)
1984	90.6	90.6	--	1.9	14	0.01	0.02	0.01	129,500	139,500	0.77
1985	92.5	86.1	4.5	1.7	14	0.011	0.04	0.014	34,300	163,800	0.90
1986	94.2	81.6	4.5	1.7	14	0.012	0.06	0.018	46,600	210,400	1.16
1987	95.9	77.1	4.5	1.7	14	0.013	0.08	0.022	58,900	269,200	1.48
1988	97.6	72.6	4.5	1.7	14	0.015	0.11	0.027	87,900	357,000	1.96
1989	99.3	68.1	4.5	1.7	14	0.017	0.14	0.032	105,400	462,500	2.54
1990	101.0	63.6	4.5	1.6	14	0.02	0.18	0.038	137,900	600,400	3.30
1991	102.6	59.1	4.5	1.6	14	0.023	0.22	0.044	160,720	761,100	4.18
1992	104.2	54.6	4.5	1.6	14	0.027	0.26	0.051	191,300	952,400	5.23
1993	105.8	50.1	4.5	1.6	14	0.031	0.30	0.058	213,000	1,165,000	6.40
1994	107.4	45.6	4.5	1.6	14	0.035	0.34	0.066	235,000	1,400,500	7.69
1995	109.0	41.1	4.5	1.6	14	0.039	0.37	0.073	250,400	1,650,900	9.06
1996	110.4	36.6	4.5	1.4	14	0.043	0.40	0.08	263,600	1,914,500	10.51
1997	111.8	32.1	4.5	1.4	14	0.045	0.42	0.086	263,400	2,177,800	11.96
1998	113.2	27.6	4.5	1.4	14	0.047	0.43	0.092	268,300	2,466,200	13.42
1999	114.6	23.1	4.5	1.4	14	0.049	0.44	0.097	273,000	2,719,200	14.93
2000	116.0	18.6	4.5	1.4	14	0.05	0.45	0.1	274,800	2,994,000	16.44

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock (existed in 1984) - Stock which has been previously retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Market Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: $(\text{Cumulative New Technology Heating and Cooling Units}) \times (5490 \text{ kWh/year})$

TABLE 5.3. Housing Stock Projections and Electric Water-to-Air Heat Pump Market Share Estimates for Electrically Cooled Only Residences

Year	Total Residences (a) (10 ⁶)	Retrofit Market (b) (10 ⁶)	Retired Units Market (c) (10 ⁶)	New Market Additions (a) (10 ⁶)	Residences Electrically		Retired Units Market Share (e)	New Market Additions Share (e)	Annual Additions of New Technology Heating and Cooling Units (f)	Cumulative New Technology Heating and Cooling Units (g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units (h)
					Heated and Cooled (d) (Percent)	Retrofit Market Share (e)					(BkWh)
1984	90.6	90.6	0	1.9	42	0.01	0.02	0.01	--	388,500	0.59
1985	92.5	84.6	6	1.7	42	0.011	0.04	0.014	121,100	509,600	0.78
1986	94.2	78.6	6	1.7	42	0.012	0.06	0.018	169,300	678,900	1.05
1987	95.9	72.6	6	1.7	42	0.013	0.08	0.022	217,600	896,500	1.38
1988	97.6	66.6	6	1.7	42	0.015	0.11	0.027	319,700	1,216,200	1.87
1989	99.3	60.6	6	1.7	42	0.017	0.14	0.032	388,800	1,604,900	2.47
1990	101.0	54.6	6	1.6	42	0.02	0.18	0.038	505,100	2,110,000	3.25
1991	102.6	48.6	6	1.6	42	0.023	0.22	0.044	594,800	2,704,800	4.17
1992	104.2	42.6	6	1.6	42	0.027	0.26	0.051	703,100	3,407,900	5.25
1993	105.8	36.6	6	1.6	42	0.031	0.3	0.058	788,400	4,196,346	6.46
1994	107.4	30.6	6	1.6	42	0.035	0.34	0.066	874,000	5,070,800	7.81
1995	109.0	24.6	6	1.6	42	0.039	0.37	0.073	934,600	6,005,400	9.25
1996	110.4	18.6	6	1.4	42	0.043	0.4	0.08	988,000	6,993,400	10.77
1997	111.8	12.6	6	1.4	42	0.045	0.42	0.086	1,011,200	8,005,400	12.33
1998	113.2	6.6	6	1.4	42	0.047	0.43	0.092	1,029,800	9,034,400	13.91
1999	114.6	0.6	6	1.4	42	0.049	0.44	0.097	1,047,900	10,082,300	15.53
2000	116.0	0	0.6	1.4	42	0.05	0.45	0.10	46,400	10,128,700	15.60

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which has been previously retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Market Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: $(\text{Cumulative New Technology Cooling Units}) \times (1540 \text{ kWh})$

TABLE 5.4. Housing Stock Projects and Gas-Fired Heat Pump Market Share Estimates for Electrically Heated and Cooled Residences

Year	Total Residences (a) (10 ⁶)	Retrofit Market (b) (10 ⁶)	Retired Units Market (c) (10 ⁶)	New Market Additions (d) (10 ⁶)	Residences Electrically Heated and Cooled (e) (Percent)	Retrofit Market Share (f) (Percent)	Retired Units Market Share (g) (Percent)	New Market Additions Share (h) (Percent)	Annual Additions of New Technology Heating and Cooling Units (i)	Cumulative New Technology Heating and Cooling Units (j)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units (k) (BkWh)
1984	--	--	--	--	--	--	--	--	--	--	--
1985	--	--	--	--	--	--	--	--	--	--	--
1986	--	--	--	--	--	--	--	--	--	--	--
1987	--	--	--	--	--	--	--	--	--	--	--
1988	--	--	--	--	--	--	--	--	--	--	--
1989	--	--	--	--	--	--	--	--	--	--	--
1990	101.0	101.0	4.5	1.6	14	0.002	0.005	0.004	32,300	32,300	0.26
1991	102.6	96.5	4.5	1.6	14	0.005	0.02	0.009	53,800	86,200	0.71
1992	104.2	92.0	4.5	1.6	14	0.009	0.045	0.014	79,800	166,100	1.36
1993	105.8	87.5	4.5	1.6	14	0.014	0.07	0.02	104,200	270,200	2.22
1994	107.4	83.0	4.5	1.6	14	0.019	0.105	0.027	121,500	391,700	3.21
1995	109.0	78.5	4.5	1.6	14	0.025	0.145	0.034	152,900	544,600	4.47
1996	110.4	74.0	4.5	1.4	14	0.031	0.195	0.041	177,300	721,900	5.92
1997	111.8	69.5	4.5	1.4	14	0.037	0.25	0.049	205,900	927,900	7.61
1998	113.2	65.0	4.5	1.4	14	0.043	0.32	0.057	244,100	1,171,900	9.61
1999	114.6	60.5	4.5	1.4	14	0.049	0.39	0.066	282,400	1,454,400	11.93
2000	116.0	56.0	4.5	1.4	14	0.055	0.45	0.075	314,400	1,768,700	14.50

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: (Cumulative New Technology Heating and Cooling Units) x (8200 kWh)

TABLE 5.5. Housing Stock Projections and Gas-Fired Heat Pump Market Share Estimates for Electrically Cooled Only Residences

Year	Total Residences (10 ⁶) (a)	Retrofit Market (10 ⁶) (b)	Retired Units Market (10 ⁶) (c)	New Market Additions (10 ⁶) (a)	Residences Electrically Heated and Cooled (d) (Percent)	Retrofit Market Share (e)	Retired Units Market Share (e)	New Market Additions Share (e)	Annual Additions of New Technology Heating and Cooling Units (f)	Cumulative New Technology Heating and Cooling Units (g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units (h) (BkWh)
1984	--	--	--	--	--	--	--	--	--	--	--
1985	--	--	--	--	--	--	--	--	--	--	--
1986	--	--	--	--	--	--	--	--	--	--	--
1987	--	--	--	--	--	--	--	--	--	--	--
1988	--	--	--	--	--	--	--	--	--	--	--
1989	--	--	--	--	--	--	--	--	--	--	--
1990	101	101	6	1.6	42	0.002	0.005	0.004	100,100	100,100	0.23
1991	102.6	95	6	1.6	42	0.005	0.02	0.009	171,100	271,200	0.62
1992	104.2	89	6	1.6	42	0.009	0.045	0.014	259,700	530,900	1.22
1993	105.8	83	6	1.6	42	0.014	0.07	0.02	341,500	872,400	2.01
1994	107.4	77	6	1.6	42	0.019	0.105	0.027	409,200	1,281,600	2.95
1995	109	71	6	1.6	42	0.025	0.145	0.034	519,300	1,800,900	4.14
1996	110.4	65	6	1.4	42	0.031	0.195	0.041	616,300	2,417,200	5.56
1997	111.8	59	6	1.4	42	0.037	0.25	0.049	729,400	3,146,600	7.24
1998	113.2	53	6	1.4	42	0.043	0.32	0.057	880,200	4,026,800	9.26
1999	114.6	47	6	1.4	42	0.049	0.39	0.066	1,031,700	5,058,500	11.63
2000	116	41	6	1.4	42	0.055	0.45	0.075	1,157,900	6,216,400	14.30

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock (existed in 1990) - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: $(\text{Cumulative New Technology Cooling Units}) \times (2300 \text{ kWh})$.

National Energy Policy Plan (DOE 1983). The percentage of houses that use electricity for both heating and cooling purposes and for cooling only are calculated from estimates published in the 1982 Residential Energy Consumption Survey (DOE/EIA 1984). The market share estimates are derived as described in Chapter 4.0 and are based on the payback period and market penetration estimates presented in Table 5.1.

5.5 ENERGY SAVINGS COMPUTATIONS AND RESULTS

In this section, expected national electrical energy savings from the new heat pump technologies are estimated for the years 1990, 1995, and 2000. These estimates are based on the average annual electrical energy savings in a representative electrically space-conditioned home and the expected rate of market penetration of the new heat pump technologies. To use these representative savings and market penetration estimates to obtain a national savings estimate, they are applied to the data and forecasts presented in Tables 5.2 through 5.5 that characterize the size, composition, and expected changes over time of the space conditioning market.

The representative household that chooses to install an electric water-to-air heat pump over a conventional electric HVAC system will save an estimated 3950 kWh per year for heating and 1540 kWh per year for cooling.^(a) The total annual savings are therefore estimated to be 5490 kWh for a home that is both electrically heated and cooled.

The gas-fired heat pump system uses gas to circulate the refrigerant and to power the compressor but it also uses some electricity to power a fan. To simplify the analysis it will be assumed that the fan uses a negligible amount of electricity. Therefore, every gas-fired heat pump that is installed in lieu

(a) See the "Annual Household Energy Consumption" estimates that are presented in Table 5.1 and subtract the electric water-to-air heat pumps estimated consumption from that of the conventional HVAC system to obtain these per representative household annual energy savings estimates.

of a conventional electric HVAC system will save virtually all of the electricity that system would have otherwise consumed. As indicated in Table 5.1, that has been estimated to be 8200 kWh for homes that are both heated and cooled electrically. Savings for cooling only would be an estimated 2300 kWh.

The final electrical energy savings results were calculated by taking the estimated number of new technology units (found in Tables 5.2 through 5.5 above) installed by a given year and multiplying those estimates by the above described estimates of the per unit annual electrical energy savings (in kWh's). The resulting electricity saving estimates appear in the final column of each of those four tables. A summary of the electricity savings estimates is presented in Table 5.6.

Most of the information necessary to perform this analysis was found to be readily available from related sources in the literature as well as from market agents. However, the reader should be aware that portions of the analysis were treated in a highly simplistic fashion for the sake of analytical convenience. More specifically, these results depend critically on a specific scenario of assumed future prices, market penetration rates, housing stock changes, and "representative technology units." Such assumptions, forecasts, and other simplifications, no matter how well represented, should be interpreted as only approximate estimates. The results of this analysis should therefore be regarded in a similar fashion.

Table 5.6 shows that the two technologies considered in this chapter could save an estimated 61 BkWh in the year 2000. Current (1984) electricity use for space conditioning is approximately 284 BkWh. Although this latter figure is forecast to grow between now and 2000, the savings estimated here are a sizable portion of projected future electricity use for space conditioning. Hence, to the degree that the energy savings potential of these new heat pump technologies has not been accounted for in the most recent electricity consumption forecasts, those forecasts could be overstating residential space conditioning electrical energy demand by up to approximately 20 percent.

TABLE 5.6. Estimated National Annual Electrical Savings
from New Heat Pump Technologies BkWh

<u>Year</u>	<u>Electric Water-to-Air Heating and Cooling</u>	<u>Electric Water-to-Air Cooling Only</u>	<u>Gas-Fired Heating and Cooling</u>	<u>Gas-Fired Cooling Only</u>	<u>Total Savings</u>
1985	.90	.78	0	0	1.69
1990	3.30	3.25	.26	.62	7.43
1995	9.06	9.25	4.47	5.56	28.34
2000	16.48	15.60	15.50	14.30	60.84

5.6 SENSITIVITY ANALYSIS

This section is an analysis of the sensitivity of the aggregate energy savings results presented in Section 5.5 to alterations in the market penetration scenario. The analysis may serve to indicate a maximum/minimum range within which the actual energy savings could be expected to occur. Alternatively, the analysis may be helpful as an indicator of what the potential energy savings benefit could be from the institution of programs or policies designed to increase the private utilization of the new energy saving technologies.

5.6.1 Low Market Penetration Scenarios

It is possible that the new heat pump technologies will not penetrate the residential HVAC market as quickly or completely as indicated in Tables 5.2 through 5.5. For example, if the future cost of electricity to the consumer is perceived to be low relative to the cost of the new technologies, then the consumer's incentive to invest in such conservation technologies will not be strong. Alternatively, if technical limitations become a serious constraint to a new technology's acceptability to the consumer, then the technology's rate of market penetration will be dampened. The degree to which such potentialities may occur is a matter of conjecture. However, reasonable bounds can be postulated and examined for their implications.

In that regard, the low market penetration scenarios for the new electric water-to-air heat pump technology assume that the maximum level of market penetration reaches only half that of our previous estimates for all three

markets. The maximum market penetration rates were therefore estimated to be 2.5 percent in the retrofit market, 22.5 percent in the retirement market, and 5 percent in the new market. Furthermore, we lowered the entire S-curve (see Figure 4.1), assuming that only 75 percent of that new maximum penetration potential will be achieved by the year 2000.

The low market penetration scenarios for the new gas-fired heat pump technology assume that the penetration reaches only half of what the year 2000 base case was for all three markets. Due to the late market entry date of these systems, further limitations on their penetration were not assumed. The details of the analysis for the low market penetration scenarios are presented in Tables 5.7 through 5.10. A summary of national annual electrical energy savings estimates for the low-market penetration scenario of the new heat pump technologies is presented in Table 5.11. These results could be interpreted as being indicative of a reasonable minimum for the expected electrical energy savings from the new heat pump technologies market would also double (i.e., from 45 percent to 90 percent), the maximum level of penetration in that market is assumed to remain the same but it is to be achieved in 1995 rather than in 2000.

5.6.2 High Market Penetration Scenarios

The high market penetration scenarios for the gas-fired heat pump assumes a doubling of the penetration achieved in the base case by the year 2000 for the new installation and the retrofit markets. Due to the relatively high penetration in the base case retirement market (i.e., 45 percent) and due to the late market entry date of this technology, the assumed penetration for that market does not change from the base case. The specifics of these scenarios are detailed in Tables 5.12 through 5.15. A summary of the national annual electrical energy savings estimates for the high market penetration scenario of the advanced heat pump systems are displayed in Table 5.16. These estimates represent a reasonable maximum for the expected electrical energy savings from the advanced heat pump technologies.

TABLE 5.7. Electric Water-to-Air Heat Pump Low-Market Penetration Scenario for Electrically Heated and Cooled Residences

Year	Total Residences (a) (10 ⁶)	Retrofit Market (b) (10 ⁶)	Retired Units Market (c) (10 ⁶)	New Market Additions (d) (10 ⁶)	Residences Electrically Heated and Cooled (e) (Percent)	Retrofit Market Share (e)	Retired Units Market Share (e)	New Market Additions Share (e)	Annual Additions of New Technology Heating and Cooling Units (f)	Cumulative New Technology Heating and Cooling Units (g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units (h) (BkWh)
1984	90.6	90.6	--	1.9	14	0.005	0.02	0.01	66,100	66,100	0.36
1985	92.5	86.1	4.5	1.7	14	0.0055	0.025	0.011	21,200	87,400	0.48
1986	94.2	81.6	4.5	1.7	14	0.006	0.03	0.012	24,000	111,300	0.61
1987	95.9	77.1	4.5	1.7	14	0.0065	0.04	0.013	29,900	141,200	0.78
1988	97.6	72.6	4.5	1.7	14	0.007	0.05	0.015	36,000	177,300	0.97
1989	99.3	68.1	4.5	1.7	14	0.008	0.065	0.017	50,100	227,400	1.25
1990	101	63.6	4.5	1.6	14	0.009	0.08	0.019	58,500	285,900	1.57
1991	102.6	59.1	4.5	1.6	14	0.011	0.1	0.022	78,800	364,700	2.00
1992	104.2	54.6	4.5	1.6	14	0.013	0.12	0.025	89,600	454,300	2.49
1993	105.8	50.1	4.5	1.6	14	0.014	0.13	0.027	86,700	541,072	2.97
1994	107.4	45.6	4.5	1.6	14	0.015	0.14	0.029	92,300	633,300	3.48
1995	109	41.1	4.5	1.6	14	0.016	0.148	0.031	96,500	729,800	4.01
1996	110.4	36.6	4.5	1.4	14	0.017	0.155	0.0325	98,000	827,800	4.54
1997	111.8	32.1	4.5	1.4	14	0.018	0.16	0.034	100,000	927,800	5.09
1998	113.2	27.6	4.5	1.4	14	0.018	0.164	0.0355	101,200	1,029,400	5.65
1999	114.6	23.1	4.5	1.4	14	0.019	0.167	0.0365	102,600	1,131,700	6.21
2000	116	18.6	4.5	1.4	14	0.019	0.169	0.0375	102,900	1,234,700	6.78

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i)] + [(\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i)] + [(\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: $(\text{Cumulative New Technology Cooling Units}) \times (5490 \text{ kWh})$

TABLE 5.8. Electric Water-to-Air Heat Pump Low-Market Penetration Scenario for Electrically Cooled Only Residences

Year	Total Residences ^(a) (10 ⁶)	Retrofit Market ^(b) (10 ⁶)	Retired Units Market ^(c) (10 ⁶)	New Market Additions ^(a) (10 ⁶)	Residences Electrically Heated and Cooled ^(d) (Percent)	Retrofit Market Share ^(e)	Retired Units Market Share ^(e)	New Market Additions Share ^(e)	Annual Additions of New Technology Heating and Cooling Units ^(f)	Cumulative New Technology Heating and Cooling Units ^(g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units ^(h) (BkWh)
1984	90.6	90.6	0	1.9	42	0.005	0.02	0.01	198,200	198,200	0.31
1985	92.5	84.6	6	1.7	42	0.0055	0.025	0.011	76,000	274,300	0.42
1986	94.2	78.6	6	1.7	42	0.006	0.03	0.012	86,800	361,000	0.55
1987	95.9	72.6	6	1.7	42	0.0065	0.04	0.013	110,200	471,300	0.73
1988	97.6	66.6	6	1.7	42	0.007	0.05	0.015	134,300	605,600	0.93
1989	99.3	60.6	6	1.7	42	0.008	0.065	0.017	183,800	789,300	1.22
1990	101.0	54.6	6	1.6	42	0.009	0.08	0.019	217,100	1,006,500	1.55
1991	102.6	48.6	6	1.6	42	0.011	0.1	0.022	284,900	1,291,400	1.99
1992	104.2	42.6	6	1.6	42	0.013	0.12	0.025	327,200	1,618,700	2.49
1993	105.8	36.6	6	1.6	42	0.014	0.13	0.027	328,300	1,947,000	2.99
1994	107.4	30.6	6	1.6	42	0.015	0.14	0.029	349,800	2,296,900	3.54
1995	109.0	24.6	6	1.6	42	0.016	0.148	0.031	366,300	2,663,200	4.10
1996	110.4	18.6	6	1.4	42	0.0168	0.15	0.0325	363,000	3,026,300	4.66
1997	111.8	12.6	6	1.4	42	0.0175	0.16	0.034	384,600	3,410,800	5.25
1998	113.2	6.6	6	1.4	42	0.018	0.164	0.0355	391,400	3,802,300	5.86
1999	114.6	0.6	6	1.4	42	0.0185	0.167	0.0365	397,000	4,199,300	6.47
2000	116.0	0.0	0.6	1.4	42	0.0188	0.169	0.0375	17,400	4,216,700	6.49

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimate from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: $(\text{Cumulative New Technology Cooling Units}) \times (1540 \text{ kWh})$

**TABLE 5.9. Gas-Fired Heat Pump Low-Market Penetration Scenario
for Electrically Heated and Cooled Residences**

Year	Total Residences (a) (10 ⁶)	Retrofit Market (b) (10 ⁶)	Retired Units Market (c) (10 ⁶)	New Market Additions (d) (10 ⁶)	Residences Electrically Heated and Cooled (d) (Percent)	Retrofit Market Share (e)	Retired Units Market Share (e)	New Market Additions Share (e)	Annual Additions of New Technology Heating and Cooling Units (f)	Cumulative New Technology Heating and Cooling Units (g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units (h) (BkWh)
1984	--	--	--	--	--	--	--	--	--	--	--
1985	--	--	--	--	--	--	--	--	--	--	--
1986	--	--	--	--	--	--	--	--	--	--	--
1987	--	--	--	--	--	--	--	--	--	--	--
1988	--	--	--	--	--	--	--	--	--	--	--
1989	--	--	--	--	--	--	--	--	--	--	--
1990	101.0	101.0	4.5	1.6	14	0.002	0.005	0.004	32,300	32,300	0.26
1991	102.6	96.5	4.5	1.6	14	0.003	0.015	0.006	23,000	55,400	0.45
1992	104.2	92.0	4.5	1.6	14	0.005	0.03	0.008	44,600	99,900	0.82
1993	105.8	87.5	4.5	1.6	14	0.008	0.05	0.011	67,600	167,500	1.37
1994	107.4	83.0	4.5	1.6	14	0.012	0.08	0.015	45,200	262,700	2.15
1995	109.0	78.5	4.5	1.6	14	0.016	0.115	0.02	113,300	376,000	3.08
1996	110.4	74.0	4.5	1.4	14	0.019	0.145	0.025	117,300	493,300	4.05
1997	111.8	69.5	4.5	1.4	14	0.022	0.17	0.029	130,000	623,800	4.91
1998	113.2	65.0	4.5	1.4	14	0.024	0.19	0.032	130,300	754,100	4.39
1999	114.6	60.5	4.5	1.4	14	0.026	0.21	0.036	141,200	895,300	7.77
2000	116.0	56.0	4.5	1.4	14	0.028	0.225	0.038	148,500	1,043,800	8.56

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: $(\text{Cumulative New Technology Heating and Cooling Units}) \times (8200 \text{ kWh})$

TABLE 5.10. Gas-Fired Heat Pump Low-Market Penetration Scenario
for Electrically Cooled Only Residences

Year	Total Residences ^(a) (10 ⁶)	Retrofit Market ^(b) (10 ⁶)	Retired Units Market ^(c) (10 ⁶)	New Market Additions ^(d) (10 ⁶)	Residences Electrically Heated and Cooled ^(d) (Percent)	Retrofit Market Share ^(e)	Retired Units Market Share ^(e)	New Market Additions Share ^(e)	Annual Additions of New Technology Heating and Cooling Units ^(f)	Cumulative New Technology Heating and Cooling Units ^(g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units ^(h) (BkWh)
1984	--	--	--	--	--	--	--	--	--	--	--
1985	--	--	--	--	--	--	--	--	--	--	--
1986	--	--	--	--	--	--	--	--	--	--	--
1987	--	--	--	--	--	--	--	--	--	--	--
1988	--	--	--	--	--	--	--	--	--	--	--
1989	--	--	--	--	--	--	--	--	--	--	--
1990	101.0	101	6	1.6	42	0.002	0.005	0.004	100,100	100,100	0.23
1991	102.6	95	6	1.6	42	0.003	0.015	0.006	76,700	176,800	0.41
1992	104.2	89	6	1.6	42	0.005	0.03	0.008	148,200	325,000	0.75
1993	105.8	83	6	1.6	42	0.008	0.05	0.011	225,400	550,400	1.27
1994	107.4	77	6	1.6	42	0.012	0.08	0.015	320,700	871,250	2.00
1995	109.0	71	6	1.6	42	0.016	0.115	0.02	392,300	1,263,500	2.91
1996	110.4	65	6	1.4	42	0.019	0.145	0.025	421,700	1,685,200	3.88
1997	111.8	59	6	1.4	42	0.022	0.17	0.029	471,900	2,157,100	4.96
1998	113.2	53	6	1.4	42	0.024	0.19	0.032	486,700	2,643,800	6.08
1999	114.6	47	6	1.4	42	0.026	0.21	0.036	529,400	3,173,200	7.30
2000	116.0	41	6	1.4	42	0.028	0.225	0.038	558,300	3,731,450	8.58

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: $(\text{Cumulative New Technology Cooling Units}) \times (2300 \text{ kWh})$

Table 5.11. National Annual Electrical Savings Estimates From the Low Market Penetration Scenario for the New Heat Pump Technologies (BkWh)

<u>Year</u>	<u>Water-to-Air Heating and Cooling</u>	<u>Water-to-Air Cooling Only</u>	<u>Gas-Fired Heating and Cooling</u>	<u>Gas-Fired Cooling Only</u>	<u>Total Savings</u>
1985	.48	.42	0	0	.90
1990	1.57	1.55	.26	.23	3.61
1995	4.01	4.10	3.08	2.91	14.10
2000	6.78	6.49	8.56	8.58	30.41

5.7 COST PER KWH OF ENERGY SAVED CALCULATIONS AND COMPARISONS TO THE COST PER KWH OF PRODUCING NEW GENERATING CAPACITY

The new heat pump technologies may be considered as investments that have a return to the investor in the form of future reductions in the amount of energy that must be purchased for space conditioning. To the degree that the cost per kWh of those energy savings is less than the cost per kWh of producing that power utilities may choose to invest in technologies instead of new generating capacity.

In that regard, the cost per kWh saved calculations for each space conditioning application of the new heat pump technologies are displayed in Tables 5.17 and 5.18 and compared with estimated national average cost per kWh of new power from a new coal-fired generating plant of about 5.82¢/kWh.

The results of this analysis indicate that the costs per kWh saved for new and retirement market installations of both the electric water-to-air (2.55¢/kWh) and the gas-fired HPs (1.85¢/kWh) are significantly less than the estimated 5.82¢/kWh cost of new power. On the other hand, the analysis indicates that the 8.73¢/kWh cost for energy saved by replacing existing conventional electric HVACs with electric water-to-air type systems would not be a good investment for utilities and the cost of replacing an existing HVAC with a gas-fired HP system (5.98¢/kWh) would, at best, be only comparable to the cost of generating new power.

TABLE 5.12. Electric Water-to-Air Heat Pump High-Market Penetration Scenario for Electrically Heated and Cooled Residences

Year	Total Residences (a) (10 ⁶)	Retrofit Market (b) (10 ⁶)	Retired Units Market (c) (10 ⁶)	New Market Additions (d) (10 ⁶)	Residences Electrically Heated and Cooled (e) (Percent)	Retrofit Market Share (e)	Retired Units Market Share (e)	New Market Additions Share (e)	Annual Additions of New Technology Heating and Cooling Units (f)	Cumulative New Technology Heating and Cooling Units (g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units (h) (BkWh)
1984	90.6	90.6	--	1.9	14	0.01	0.02	0.01	129,500	129,500	0.56
1985	92.5	86.1	4.5	1.7	14	0.013	0.04	0.015	58,600	188,100	1.03
1986	94.2	81.6	4.5	1.7	14	0.017	0.07	0.023	87,100	275,200	1.51
1987	95.9	77.1	4.5	1.7	14	0.022	0.1	0.033	114,100	389,300	2.14
1988	97.6	72.6	4.5	1.7	14	0.03	0.14	0.05	167,500	556,900	3.06
1989	99.3	68.1	4.5	1.7	14	0.04	0.2	0.07	219,100	775,000	4.25
1990	101.0	63.6	4.5	1.6	14	0.05	0.27	0.1	256,300	1,032,300	5.67
1991	102.6	59.1	4.5	1.6	14	0.065	0.35	0.13	342,200	1,374,600	7.55
1992	104.2	54.6	4.5	1.6	14	0.077	0.4	0.16	336,600	1,713,200	9.41
1993	105.8	50.1	4.5	1.6	14	0.087	0.43	0.18	328,900	2,046,000	11.23
1994	107.4	45.6	4.5	1.6	14	0.095	0.44	0.19	316,000	2,362,038	12.97
1995	109.0	41.1	4.5	1.6	14	0.1	0.45	0.2	297,200	2,659,258	14.60
1996	110.4	36.6	4.5	1.4	14	0.1	0.45	0.2	259,700	2,918,000	16.03
1997	111.8	32.1	4.5	1.4	14	0.1	0.45	0.2	259,700	3,178,700	17.45
1998	113.2	27.6	4.5	1.4	14	0.1	0.45	0.2	259,700	3,438,400	18.88
1999	114.6	23.1	4.5	1.4	14	0.1	0.45	0.2	259,700	3,698,100	20.30
2000	116.0	18.6	4.5	1.4	14	0.1	0.45	0.2	259,700	3,957,800	21.73

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: (Cumulative New Technology Heating and Cooling Units) x (5490 kWh)

TABLE 5.13. Electric Water-to-Air Heat Pump High Market Penetration Scenario for Electrically Cooled Only Residences

Year	Total Residences ^(a) (10 ⁶)	Retrofit Market ^(b) (10 ⁶)	Retired Units Market ^(c) (10 ⁶)	New Market Additions ^(d) (10 ⁶)	Residences Electrically Heated and Cooled ^(d) (Percent)	Retrofit Market Share ^(e)	Retired Units Market Share ^(e)	New Market Additions Share ^(e)	Annual Additions of New Technology Heating and Cooling Units ^(f)	Cumulative New Technology Heating and Cooling Units ^(g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units ^(h) (BkWh)
1984	90.6	90.6	0	1.9	42	0.01	0.02	0.01	388,500	388,500	0.60
1985	92.5	84.6	6	1.7	42	0.013	0.04	0.015	192,900	581,400	0.89
1986	94.2	78.6	6	1.7	42	0.017	0.07	0.023	292,100	873,500	1.35
1987	95.9	72.6	6	1.7	42	0.022	0.1	0.033	385,200	1,258,700	1.94
1988	97.6	66.6	6	1.7	42	0.03	0.14	0.05	556,800	1,815,500	2.79
1989	99.3	60.6	6	1.7	42	0.04	0.2	0.07	732,900	2,548,400	3.92
1990	101.0	54.6	6	1.6	42	0.05	0.27	0.1	876,100	3,424,600	5.27
1991	102.6	48.6	6	1.6	42	0.065	0.35	0.13	1,150,500	4,578,400	7.04
1992	104.2	42.6	6	1.6	42	0.077	0.4	0.16	1,166,400	5,740,500	8.84
1993	105.8	36.6	6	1.6	42	0.087	0.43	0.18	1,164,200	6,904,800	10.63
1994	107.4	30.6	6	1.6	42	0.095	0.44	0.19	1,120,100	8,024,800	12.36
1995	109.0	24.6	6	1.6	42	0.1	0.45	0.2	1,080,700	9,105,500	14.02
1996	110.4	18.6	6	1.4	42	0.1	0.45	0.2	999,700	10,105,100	15.56
1997	111.8	12.6	6	1.4	42	0.1	0.45	0.2	999,700	11,104,700	17.10
1998	113.2	6.6	6	1.4	42	0.1	0.45	0.2	999,700	12,104,300	18.64
1999	114.6	0.6	6	1.4	42	0.1	0.45	0.2	999,700	13,103,900	20.18
2000	116.0	0	0.6	1.4	42	0.1	0.45	0.2	92,400	13,196,300	20.32

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: $(\text{Cumulative New Technology Cooling Units}) \times (1540 \text{ kWh})$

TABLE 5.14. Gas-Fired Heat Pump High-Market Penetration Scenario
for Electrically Heated and Cooled Residences

Year	Total Residences ^(a) (10 ⁶)	Retrofit Market ^(b) (10 ⁶)	Retired Units Market ^(c) (10 ⁶)	New Market Additions ^(d) (10 ⁶)	Residences Electrically Heated and Cooled ^(d) (Percent)	Retrofit Market Share ^(e)	Retired Units Market Share ^(e)	New Market Additions Share ^(e)	Annual Additions of New Technology Heating and Cooling Units ^(f)	Cumulative New Technology Heating and Cooling Units ^(g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units ^(h) (BkWh)
1984	--	--	--	--	--	--	--	--	--	--	--
1985	--	--	--	--	--	--	--	--	--	--	--
1986	--	--	--	--	--	--	--	--	--	--	--
1987	--	--	--	--	--	--	--	--	--	--	--
1988	--	--	--	--	--	--	--	--	--	--	--
1989	--	--	--	--	--	--	--	--	--	--	--
1990	101.0	101.0	4.5	1.6	14	0.002	0.005	0.004	32,300	32,300	0.26
1991	102.6	96.5	4.5	1.6	14	0.006	0.02	0.01	67,600	100,000	0.82
1992	104.2	92.0	4.5	1.6	14	0.011	0.045	0.018	93,000	193,000	1.58
1993	105.8	87.5	4.5	1.6	14	0.018	0.07	0.027	128,000	322,200	2.64
1994	107.4	83.0	4.5	1.6	14	0.03	0.105	0.037	202,500	524,500	4.30
1995	109.0	78.5	4.5	1.6	14	0.045	0.145	0.05	248,500	773,000	6.34
1996	110.4	74.0	4.5	1.4	14	0.065	0.195	0.07	315,400	1,088,400	8.92
1997	111.8	69.5	4.5	1.4	14	0.085	0.25	0.09	328,800	1,417,200	11.62
1998	113.2	65.0	4.5	1.4	14	0.095	0.32	0.115	261,600	1,678,800	13.77
1999	114.6	60.5	4.5	1.4	14	0.105	0.39	0.135	297,000	1,975,800	16.20
2000	116.0	56.0	4.5	1.4	14	0.11	0.45	0.15	285,000	2,261,700	18.55

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: $(\text{Cumulative New Technology Heating and Cooling Units}) \times (8200 \text{ kWh})$

TABLE 5.15. Gas-Fired Heat Pump High-Market Penetration Scenario
for Electrically Cooled Only Residences

Year	Total Residences (a) (10 ⁶)	Retrofit Market (b) (10 ⁶)	Retired Units Market (c) (10 ⁶)	New Market Additions (d) (10 ⁶)	Residences Electrically Heated and Cooled (e) (Percent)	Retrofit Market Share (f) (e)	Retired Units Market Share (g) (e)	New Market Additions Share (h) (e)	Annual Additions of New Technology Heating and Cooling Units (i) (f)	Cumulative New Technology Heating and Cooling Units (j) (g)	Annual Energy Savings From Cumulative New Technology Heating and Cooling Units (k) (BkWh)
1984	--	--	--	--	--	--	--	--	--	--	--
1985	--	--	--	--	--	--	--	--	--	--	--
1986	--	--	--	--	--	--	--	--	--	--	--
1987	--	--	--	--	--	--	--	--	--	--	--
1988	--	--	--	--	--	--	--	--	--	--	--
1989	--	--	--	--	--	--	--	--	--	--	--
1990	101.0	101	6	1.6	42	0.002	0.005	0.004	100,100	100,100	0.23
1991	102.6	95	6	1.6	42	0.006	0.02	0.01	211,700	311,800	0.72
1992	104.2	89	6	1.6	42	0.011	0.045	0.018	297,300	609,100	1.40
1993	105.8	83	6	1.6	42	0.018	0.07	0.027	410,800	1,019,900	2.35
1994	107.4	77	6	1.6	42	0.03	0.105	0.037	632,200	1,652,100	3.80
1995	109.0	71	6	1.6	42	0.045	0.145	0.05	770,700	2,422,800	5.57
1996	110.4	65	6	1.4	42	0.065	0.195	0.07	965,200	3,388,000	7.79
1997	111.8	59	6	1.4	42	0.085	0.25	0.09	1,014,700	4,402,700	10.13
1998	113.2	53	6	1.4	42	0.095	0.32	0.115	882,400	5,285,100	12.16
1999	114.6	47	6	1.4	42	0.105	0.39	0.135	1,020,200	6,305,300	14.50
2000	116.0	41	6	1.4	42	0.11	0.45	0.15	1,043,700	7,349,000	16.90

(a) Source: NEPP Forecasts

(b) Retrofit Market = Existing Old Stock - Stock which is retired

(c) Source: BPA 1981

(d) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(e) See Chapter 4.0.

(f) Calculated by: $[(\text{Retrofit Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i) + (\text{Retired Units Market in Year } i) \times (\text{Percent Electric}) \times (\text{Retired Units Share in Year } i) + (\text{New Market Additions in Year } i) \times (\text{Percent Electric}) \times (\text{New Additions Share in Year } i)] - [(\text{Retrofit Market in Year } i-1) \times (\text{Percent Electric}) \times (\text{Retrofit Share in Year } i-1)]$

(g) Calculated by summing each years additional new technology units to the cumulative number of units from the previous year.

(h) Calculated by: (Cumulative New Technology Cooling Units) x (2300 kWh)

These estimates are based on the assumption that the typical residence is both heated and cooled with electricity. The analysis also provides estimates of costs per kWh saved for heating only and for cooling only applications even though the typical HP system is designed to be used in both applications. For residences that are only cooled electrically, the cost of both water-to-air heat pumps (9.1¢/kWh) and gas heat pumps (6.6¢/kWh) exceed the national average cost of new generating plant additions (both for new and retirement markets).

TABLE 5.16. National Annual Electrical Savings Estimates from the High Market Penetration Scenarios for the New Heat Pump Technologies (BkWh)

<u>Year</u>	<u>Electric Water-to-Air Heating and Cooling</u>	<u>Electric Water-to-Air Cooling Only</u>	<u>Gas-Fired Heating and Cooling</u>	<u>Gas-Fired Cooling Only</u>	<u>Total Savings</u>
1985	1.03	.89	0	0	1.92
1990	5.67	5.27	.26	.23	11.43
1995	14.60	14.02	6.34	5.57	40.53
2000	21.13	20.32	18.55	16.90	77.50

TABLE 5.17. Cost per kWh Saved Calculations for Electric Water-to-Air Heat Pumps

Incremental Capital Cost (\$) ^(a)	
Installation	= 1,200
Replacement Installation	= 4,100
Levelized Capital Cost (\$/yr) ^(b)	
New/Retirement Installation	= 140.20
Replacement Installation	= 479.00
Annual Energy Savings (kWh/yr) ^(a)	
Heating	= 5,900 - 1,950 = 3,950
Cooling	= 2,300 - 760 = 1,540
Heating and Cooling	= 8,200 - 2,710 = 5,490
New/Retirement Installation Cost per kWh (¢/kWh) ^(c)	
Heating	= 14,020/3,950 = 3.55
Cooling	= 14,020/1,540 = 9.10
Heating and Cooling	= 14,020/5,490 = 2.55
Replacement Installation Cost per kWh (¢/kWh) ^(c)	
Heating	= 47,900/3,950 = 12.13
Cooling	= 47,900/1,540 = 31.10
Heating and Cooling	= 47,900/5,490 = 8.73

(a) See Table 5.1.

(b) The level stream of annual payments the present value of which would equal the investment's incremental capital cost. Assumes a 15 year useful lifetime of the investment and an 8 percent rate of interest compounded annually. See Equation 4.11 above.

(c) Levelized Capital Cost (x 100/\$)/Annual Energy Savings.

TABLE 5.18. Cost per kWh Saved Calculations for Gas-Fired Heat Pumps

Incremental Capital Cost (\$) ^(a)	
Installation	= 1,300
Replacement Installation	= 4,200
Levelized Capital Cost (\$/yr) ^(b)	
New/Retirement Installation	= 151.88
Replacement Installation	= 490.68
Annual Energy Savings (kWh/yr) ^(a)	
Heating	= 5,900
Cooling	= 2,300
Heating and Cooling	= 8,200
New/Retirement Installation Cost per kWh (¢/kWh) ^(c)	
Heating	= 15,188/5,900 = 2.57
Cooling	= 15,188/2,300 = 6.60
Heating and Cooling	= 15,188/8,200 = 1.85
Replacement Installation Cost per kWh (¢/kWh) ^(c)	
Heating	= 49,068/5,900 = 8.32
Cooling	= 49,068/2,300 = 21.33
Heating and Cooling	= 49,068/8,200 = 5.98

(a) See Table 5.1.

(b) The level stream of annual payments the present value of which would equal the investment's incremental capital cost. Assumes a 15 year useful lifetime of the investment and an 8 percent rate of interest compounded annually. See Equation 4.11 above.

(c) Levelized Capital Cost (x 100/\$)/Annual Energy Savings.

5.8 REFERENCES FOR CHAPTER 5.0

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6.0 ADVANCED THERMAL INSULATION AND ANTI-INFILTRATION TECHNIQUES

This chapter is directed toward estimating the potential national electrical energy savings in the years 1990, 1995, and 2000 from improvements in the thermal efficiency of residential structures. A thermally efficient residential building is, in actuality, a package of interrelated conservation measures. Among the most important of those measures are ceiling, wall, and floor insulation and anti-infiltration (or anti-air leakage) techniques.

Section 6.1 is a technical review of insulation and anti-infiltration methods and of how those methods contribute to household energy savings. Typical insulation levels in new and existing homes and recent trends in those levels are discussed in Section 6.2. Section 6.3 describes estimates of the purchase and installation costs, the energy savings, and the market penetration of specific insulation improvements. In Section 6.4 the market penetration estimates of Section 6.3 are applied to housing stock data and to housing stock forecasts to obtain an approximation of future yearly insulation and anti-infiltration installations. Section 6.5 presents of the results of the analysis. Section 6.6 is an analysis of the sensitivity of the energy savings results to changes in the market penetration scenarios. Finally, Section 6.7 presents the estimated cost per kWh saved by improved thermal efficiency measures and discusses how those costs compare with the cost per kWh of new electrical generating capacity.

6.1 TECHNICAL BACKGROUND

Insulation conserves energy by reducing the loss (gain) of heat by conduction through ceilings, walls, floors, and--to a lesser degree--doors and windows. The more common of the insulating materials are: fiberglass, rock wool, cellulose, cellular plastics, perlite, vermiculite, and various types of reflective surfaces. A number of physical properties influence the ability of an insulating material to restrict heat flow. That ability is expressed in terms of "thermal resistance" (R-value). The higher the R-value of the application, the lower the heat flow through the insulating material. At a given thickness of application, different insulation types have different R-values.

However, the thicker the application of insulating material (regardless of type), the higher the effective R-value of that application. In fact, improved insulation (higher R-value) is usually accomplished not by changing insulation materials but rather by simply applying a thicker layer of insulating material to the desired space. Consequently, insulation materials are sold by volume (i.e., number of inches deep over a specified area of ceiling, wall, or floor) typically in the form of blankets or loose-fill that can be blown into spaces.

Anti-infiltration measures contribute toward more energy efficient buildings by reducing direct air flows between the inside and the outside of buildings. That is, such measures save energy by reducing the loss of heated (cooled) air to outside the building's "thermal envelope." Less heat (cooling) must therefore be produced by the home's heating (cooling) system for a given level of comfort. The major areas of air leakage through the building envelope are between the soleplate and the foundation, through or around electrical wall outlets, ventilation duct systems, exterior windows and doors, and up various ceiling vents and fireplace chimneys (see Figures 6.1 and 6.2). The soleplate (i.e., the joint between the exterior wall and the building's foundation) is especially prone to air leakage because if it is not properly caulked or sealed it allows air to leak freely around the entire perimeter of the structure. Wall outlets are a particular problem because they essentially provide holes in walls through which air can pass almost unimpeded. Hence, any device or measure taken to reduce such leakage can lead to energy savings. Some anti-infiltration measures include caulking, weatherstripping, new air-tight window and door sills, fireplace doors and inserts, closeable shutters, special plastic coverings over wall outlets, and "tighter" building practices.

Infiltration is measured in terms of "air changes per hour" (ach) which is the number of times per hour that the entire volume of inside air is replaced with outside air. The lower the ach, the more air-tight and energy efficient the building is. The rate of air changes per hour depends not only on the air-tightness of the building but also on the wind speed and the differential between indoor and outdoor temperatures.

FIGURE 6.1. Air Leakage Spots in Conventional Construction
Source: PNL, 1981, p. 8.

FIGURE 6.2. Air Leakage Test Results for Average Home of 1,780 Sq. Ft. Source: Texas Power and Light Company, Residential Air Infiltration. November 1977.

6.2 CURRENT MARKET SITUATION

The best available source regarding the insulation of existing homes is the Residential Energy Consumption Survey: Housing Characteristics 1982 (EIA1984). That publication reports on the number/percent of homes with

various types of insulation, but it does not report on nation-wide levels of insulation of existing homes. In fact, an alternative source for national average insulation levels of existing homes could not be found. Table 6.1 summarizes the information that is available on the insulation of ceilings and walls of existing residential buildings, while Table 6.2 summarizes recent trends in insulation and anti-infiltration related home improvements. The information in these tables was used along with a set of regional estimates (NPPC 1983) and expert opinion^(a) to construct a set of assumptions about insulation and anti-infiltration levels, in a prototypical (i.e., representative of the national average) existing home. These existing-home base-case assumptions are presented in the first column of Table 6.3. As the reader will note, they are R19 for ceilings, R11 for walls, R7 for floors, and 0.6 ach for infiltration.

TABLE 6.1. Single-Family Homes with Selected Types of Insulation
1978 and 1980-1982 (Percent)

Type of Insulation	1978	1980	1981	1982
Roof/Ceiling Insulation				
Yes	75.6	76.8	77.6	79.0
No	17.2	14.5	13.8	13.3
Unknown	7.2	8.7	8.6	7.7
Wall Insulation				
Yes	53.2	64.4	61.4	61.2
All Walls	NA	52.6	51.3	50.7
Some Walls	NA	11.8	10.1	10.6
No	28.7	20.5	21.6	22.2
Unknown	18.1	15.1	17.0	16.6

NA = not asked.

Note: For 1979, not asked.

Source: Energy Information Administration, 1978 through
1982 Residential Energy Consumption Surveys.

(a) Personal communication on December 7, 1984 with Arthur Johnson of the National Association of Home Builders (NAHB) Research Foundation, Inc., Rockville, Maryland.

TABLE 6.2. Single-Family Homes Making Conservation Improvements 1978-1982 (Percent)

<u>Conservation Improvements</u>	<u>1978</u>	<u>1979</u>	<u>1980</u>	<u>1981</u>	<u>1982</u>
Caulking	18.6	(a)	19.1	10.8	10.7
Weatherstripping	7.6	(a)	13.6	6.1	5.8
Closeable Shutters, Reflective Film, Plastic Coverings, or Insulating Drapes ^(b)	8.3	(a)	9.6	4.3	5.0
Roof/Ceiling Insulation	5.1	5.8	6.1	3.9	2.6
Storm Doors	4.4	6.3 ^(c)	5.8	4.0	3.8
Storm Windows	4.3	(c)	4.3	3.1	3.0
Wall Insulation	2.6	2.9	3.5	2.3	1.7
Basement/Crawl Space Insulation	2.1	(a)	1.6	0.9	0.9

(a) Not asked.

(b) This category did not include film or drapes in 1978 or film in 1980.

(c) Storm doors and storm windows were combined into one category in the 1979 survey.

Note: The 1979 Screener Survey collected very limited data on conservation improvements.

Source: Energy Information Administration, 1978 through 1982 Residential Energy Consumption Surveys.

The information for new housing insulation levels was obtained from recent surveys performed by the National Association of Home Builders (NAHB). According to that source,^(a) the national averages for R-value insulation levels in new residential buildings for 1982 were R25.3 for ceilings, R11.9 for walls, and R7.8 for floors. Unfortunately, the typical air change rate for new homes was not available from the NAHB. However, a commonly used figure in

(a) Personal communication on December 7, 1984 with Arthur Johnson of the NAHB Research Foundation, Inc., Rockville, Maryland.

TABLE 6.3. Insulation and Anti-Infiltration Improvements for Residential Homes Base Case and Efficient Home Assumptions

	Base Case Assumptions	Efficient House Assumptions	Purchase and Installation Cost Assumptions(a) (1984 \$)	Heating Percent Savings Assumptions(b)	Cooling Percent Savings Assumptions(c)
<u>Existing Homes</u>					
Ceiling	R19	R38	500	7.7%	0.1%
Walls	R11	R11	(d)	0.0%	0.0%
Floors	R7	R19	500	9.7%	0.1%
Infiltration	0.6 ach	0.4 ach	<u>550</u>	<u>30.0%</u>	<u>30.0%</u>
Totals			1550	47.4%	30.2%
<u>New Homes</u>					
Ceiling	R30	R49	400	2.9%	0.1%
Walls	R11	R31	1000	35.0%	13.0%
Floors	R11	R30	575	5.2%	0.1%
Infiltration	0.6 ach	0.4 ach	<u>550</u>	<u>30.0%</u>	<u>30.0%</u>
Totals			2525	73.1%	43.2%

(a) Based on information gathered from the following sources: 1) NPPC 1983, p. K-32 through K-12, 2) Palmiter 1984, p. 6, 3) Personal Communication with several unnamed market vendors over the week of December 3-7, 1984.

(b) NPPC 1983, p. K-3 through K-12.

(c) PNL, 1981, P. B.4 through B.9.

(d) Assumed too costly to retrofit.

alternative studies (Palmiter 1984) estimates that value to be approximately 0.6 ach. Again, the reader will note that the assumed base case values for new homes, also presented in the first column of Table 6.3, have been rounded to more "standard" values.

6.3 COST EFFECTIVENESS AND MARKET PENETRATION

In this section, the assumed costs, expected energy and dollar savings, and consequent cost-effectiveness of higher levels of insulation/anti-infiltration measures are presented and discussed. These results are then used to estimate the degree to which such measures will be implemented in the housing market between the present year and the year 2000.

6.3.1 Cost Effectiveness

In order to make the task of obtaining cost estimates more manageable, it was necessary to explicitly define a specific set of "thermally efficient house" assumptions for existing and new residential homes.^(a) These assumptions are presented the second column in Table 6.3. The assumed "efficient" scenarios of R-values and ach levels presented here were selected not so much because they represent "ideal" improvements but rather because, given the published costs and energy savings estimates for various sets of specific home improvements (NPPC 1983 and Palmiter 1984), they are representative alternatives to present standards. The R-values and the infiltration rates for the "thermally efficient" existing home differ from those of the "thermally efficient" new home primarily because it is usually far more costly to install higher levels of insulation in older homes. This is because older homes were rarely constructed with energy efficiency in mind and typically have less space, especially between the inside and outside walls, to fill with insulation. To make more space for insulation, such homes would have to be remodeled with a 2" x 6" outer wall frame to replace the less spacious and more

(a) The critical dimensions of such a home are; ceiling space requiring insulation equaling approximately 1200 sq. ft., wall space to the outside equaling approximately 2000 sq. ft., floor space requiring insulation equaling approximately 1200 sq. ft., with "average numbers" of doors, window, electrical outlets, etc.

prevalent 2" x 4" type outer wall frame. Obviously, such remodeling would be far more costly than simply filling a pre-existing space with insulation. On the other hand, building a new home with a 2 x 6 outer wall frame with special insulation siding material is not nearly as costly and can provide substantial energy savings.

Estimates of average national costs of increasing R-values and decreasing infiltration rates from the "base case" to the "efficient house" levels could not be found. Therefore, the purchase and installation cost assumptions presented in the third column of Table 6.3 are based on regional approximations (NPPC 1983 and Palmiter 1984) and substantiated by personal communication with market vendors.

The percent heating and cooling energy savings assumptions presented in columns four and five of Table 6.3 were also difficult to quantify on a national level. Such figures are typically climate specific and climates vary considerably from region to region. Therefore, the sources (PNL 1981, NPPC 1983, and Palmiter 1984) which reported such energy savings estimates did so only for specific insulation level changes in specific regions. Because of this regional variation, the energy savings assumptions listed in Table 6.3 are only potentially "representative" for the nation as a whole.

Note that the percent heating savings assumptions exceed those for cooling for the same improvement in insulation. This is primarily because the rate of loss of heat or cooling by conduction through ceilings, walls, and floors to the buildings exterior depends on the indoor-outdoor temperature differential. The greater the indoor-outdoor temperature differential, the higher the rate of heat transfer. Hence, because the indoor-outdoor temperature differential is typically greater (both in terms of size and of duration) during the heating season, there is a greater potential for energy savings for heating as compared to cooling.

6.3.2 Market Penetration

The degree to which higher levels of insulation are likely to be installed depends on several factors. Some of the more important factors are: 1) the initial incremental capital cost of the "thermal efficiency" measures, 2) the

simple payback period, 3) whether the efficiency measures are being applied to new or to previously existing homes, 4) the number of existing homes and the number of new homes being built each year, and 5) technical limitations that may exist to the effective installation of such measures. The capital costs and the payback periods are reported in Table 6.4, as are the expected maximum market penetration rates.

The only readily apparent technical limitations to the implementation of these efficiency measures is the problem of retrofitting existing buildings, as well as problems of reduced indoor air quality. As infiltration is reduced below 0.2 ach there may be a significant deterioration of interior air conditions. These conditions can be remedied by installing an air-to-air heat ventilation while losing less than 15 percent of the heat that would otherwise be lost through ordinary infiltration (PNL 1981). In the present case, such devices would not be required because the infiltration rate is assumed to be higher than 0.2 ach (i.e., 0.4 ach).

6.4 HOUSING STOCK PROJECTIONS AND MARKET SHARE ESTIMATES

Tables 6.5 and 6.6 present scenarios of housing stock projections and market share percentages at yearly intervals up to the year 2000. The housing stock projections are based on estimates used by the DOE for computations in The National Energy Policy Plan (DOE 1983). The percentage of houses that use 1984). Note that separate calculations were performed for electrically cooled homes, although the payback periods and maximum market penetration rates were calculated for a "typical" residence that is both heated and cooled electrically. Varying these assumptions was not performed in the analysis due to the time and budget constraints. The percentage of market share estimates are derived as described in Chapter 4.0 and are based on the payback period and market penetration estimates presented in Table 6.4.

6.5 ENERGY SAVINGS COMPUTATIONS AND RESULTS

Tables 6.5 and 6.6 also present estimates of the expected national electrical energy savings from improvements in the thermal efficiency of residential buildings for the years 1984-2000. These estimates are based on the

TABLE 6.4. Insulation and Anti-Infiltration Space Conditioning
Simple Pay-Back Calculations

	Existing Home Base Case	Efficient Existing Home	New Home Base Case	Efficient New Home
Incremental Capital Cost (\$) ^(a)	--	1550	--	2525
Percent Savings ^(a)				
Heating --	47.4	--	73.1	
Cooling --	30.2	--	43.2	
Annual Household Energy Consumption ^(b)				
Heating (kWh)	5900	3103	5600	1506
Cooling (kWh)	<u>2300</u>	<u>1605</u>	<u>2275</u>	<u>1292</u>
Total Heating and Cooling (kWh)	8200	4708	7875	2798
Energy Cost (cents per kWh) ^(b)	7.18	7.18	7.18	7.18
Annual Fuel Bill (\$) ^(c)				
Heating (\$)	420	223	402	108
Cooling (\$)	<u>165</u>	<u>115</u>	<u>163</u>	<u>93</u>
Total Heating and Cooling (\$)	585	338	565	201
Annual Savings on Fuel Bill (\$) ^(d)	--	247	--	364
Simple Pay-Back Period (yrs) ^(e)	--	6	--	7
Maximum Market Penetration (percent) ^(f)		20		10

- (a) Based on information gathered from the following sources: 1) NPPC 1983, p. K-3 through K-12, 2) Palmiter 1984, p. 6, 3) personal communication with several unnamed market vendors over the week of December 3-7, 1984.
- (b) These rounded figures very closely approximate and average figure computed from residential energy consumption information found in the Residential Energy Consumption Survey: Housing Characteristics 1982 (DOE/EIA 1984).
- (c) Calculated at \$7.18¢/kWh.
- (d) Calculated by subtracting the total annual base case fuel bills from their respective total annual "efficient" home fuel bills.
- (e) Calculated by dividing the incremental capital costs of the home improvements by the calculated annual dollar savings on the "efficient" homes fuel bill.
- (f) See Chapter 4.0 and Table 4.1 above for a description of the methodology used to calculate these maximum market penetration rates from the above calculated simple payback period.

TABLE 6.5. Housing Stock Projections and Market Share Estimates of Thermal Efficiency Measures for Electrically Heated Residences

Year	Total Residences ^(a) (10 ⁶)	Retrofit Market ^(b) (10 ⁶)	Additional New Residences Market ^(a) (10 ⁶)	Residences Electrically Heated ^(c) (Percent)	Retrofit Market Share ^(d)	New Market Additions Share ^(d)	Thermally Efficient Retrofitted Existing Housing Units ^(e)	Additional Thermally Efficient New Housing Units ^(f)	Cumulative Thermally Efficient New Housing Units ^(g)	Annual Energy Savings From Cumulative Efficient Housing Units ^(h)
1984	90.6	90.6	1.9	14	0.02	0.01	0.25	0.003	0.003	0.72
1985	92.5	90.6	1.7	14	0.025	0.014	0.32	0.003	0.006	0.91
1986	94.2	90.6	1.7	14	0.03	0.018	0.38	0.004	0.010	1.11
1987	95.9	90.6	1.7	14	0.037	0.022	0.47	0.005	0.016	1.38
1988	97.6	90.6	1.7	14	0.045	0.027	0.57	0.006	0.022	1.69
1989	99.3	90.6	1.7	14	0.055	0.032	0.70	0.008	0.030	2.07
1990	101	90.6	1.6	14	0.065	0.038	0.82	0.009	0.038	2.46
1991	102.6	90.6	1.6	14	0.085	0.044	1.08	0.010	0.048	3.21
1992	104.2	90.6	1.6	14	0.105	0.051	1.33	0.011	0.059	3.97
1993	105.8	90.6	1.6	14	0.13	0.058	1.65	0.013	0.072	4.91
1994	107.4	90.6	1.6	14	0.155	0.066	1.97	0.015	0.087	5.86
1995	109	90.6	1.6	14	0.165	0.073	2.09	0.016	0.103	6.28
1996	110.4	90.6	1.4	14	0.172	0.08	2.18	0.016	0.119	6.59
1997	111.8	90.6	1.4	14	0.18	0.086	2.28	0.017	0.136	6.94
1998	113.2	90.6	1.4	14	0.187	0.092	2.37	0.018	0.154	7.26
1999	114.6	90.6	1.4	14	0.194	0.097	2.46	0.019	0.173	7.59
2000	116	90.6	1.4	14	0.2	0.1	2.54	0.020	0.193	7.88

(a) Source: NEPP forecasts.

(b) Retrofit Market = Existing Stock as of 1984.

(c) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984).

(d) See Chapter 4.0.

(e) Calculated by: (Retrofit Market) x (Percent Electric) x (Retrofit Share).

(f) Calculated by: (New Market Additions) x (Percent Electric) x (New Additions Share).

(g) Calculated by: summing each years, additional thermally efficient new units to the cumulative numbers of the previous year.

(h) Calculated by: [(Cumulative Retrofitted Thermally Efficient Units) x (2797 kWh) + (Cumulative New Thermally Efficient Housing Units) x (4094 kWh)].

TABLE 6.6. Housing Stock Projections and Market Share Estimates of Thermal Efficiency Measures for Electrically Cooled Residences

Year	Total Residences ^(a) (10 ⁶)	Retrofit Market ^(b) (10 ⁶)	Additional New Residences Market ^(a) (10 ⁶)	Residences Electrically Heated ^(c) (Percent)	Retrofit Market Share ^(d)	New Market Additions Share ^(d)	Cumulative Thermal Efficient Retrofitted Existing Housing Units ^(10⁶)	Additional Thermally Efficient New Housing Units ^(10⁶)	Cumulative Thermally Efficient New Housing Units ^(10⁶)	Annual Energy Savings From Cumulative Efficient Housing Units ^(h) (BkWh)
1984	90.6	90.6	1.9	56	0.02	0.01	1.01	0.011	0.011	0.72
1985	92.5	90.6	1.7	56	0.025	0.014	1.27	0.013	0.024	0.91
1986	94.2	90.6	1.7	56	0.3	0.018	1.52	0.017	0.041	1.10
1987	95.9	90.6	1.7	56	0.037	0.022	1.88	0.021	0.062	1.37
1988	97.6	90.6	1.7	56	0.045	0.027	2.28	0.026	0.088	1.67
1989	99.3	90.6	1.7	56	0.055	0.032	2.79	0.030	0.118	2.06
1990	101	90.6	1.6	56	0.065	0.038	3.30	0.034	0.152	2.44
1991	102.6	90.6	1.6	56	0.085	0.044	4.31	0.039	0.192	3.19
1992	104.2	90.6	1.6	56	0.105	0.051	5.33	0.046	0.237	3.94
1993	105.8	90.6	1.6	56	0.13	0.058	6.60	0.052	0.289	4.87
1994	107.4	90.6	1.6	56	0.155	0.066	7.86	0.059	0.348	5.81
1995	109	90.6	1.6	56	0.165	0.073	8.37	0.065	0.414	6.23
1996	110.4	90.6	1.4	56	0.172	0.08	8.73	0.063	0.477	6.53
1997	111.8	90.6	1.4	56	0.18	0.086	9.13	0.067	0.544	6.88
1998	113.2	90.6	1.4	56	0.187	0.092	9.49	0.072	0.616	7.20
1999	114.6	90.6	1.4	56	0.194	0.097	9.84	0.076	0.692	7.52
2000	116	90.6	1.4	56	0.2	0.1	10.15	0.078	0.771	7.81

(a) Source: NEPP Forecasts.

(b) Retrofit Market = Existing Stock as of 1984.

(c) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984).

(d) See Chapter 4.0.

(e) Calculated by: (Retrofit Market) x (Percent Electric) x (Retrofit Share).

(f) Calculated by: (New Market Additions) x (Percent Electric) x (New Additions Share).

(g) Calculated by: summing each years additional thermally efficient new units to the cumulative number of the previous year.

(h) Calculated by: [Cumulative Retrofitted Thermally Efficient Units) x (695kWh) + (Cumulative New Thermally Efficient Housing Units) x (983 kWh)].

average annual electrical energy savings in a representative electrically space conditioned home and the expected rate of market penetration of the thermal efficiency measures. To use these savings and market penetration estimates to obtain a national savings estimate, they are applied to the data and forecasts presented in Tables 6.5 and 6.6 that characterize the size, composition, and expected changes over time of the insulation/anti-infiltration markets.

6.5.1 Electrical Energy Savings Computations

The representative existing households that choose to install the selected set of thermal efficiency measures could save an estimated 2797 kWh per year per residence for heating and 695 kWh per year per residence for cooling.^(a) For new housing, the selected set of thermal efficiency measures could save an estimated 4094 kWh per year per residence for heating and 983 kWh per year per residence for cooling.

6.5.2 Aggregate Electrical Energy Savings Results

The results of the foregoing analysis are summarized in Table 6.7. The table shows that adoption of new insulation and anti-infiltration technologies in residential sector between 1984 and 2000 will reduce residential space conditioning electricity use by an estimated 15.7 BkWh in 2000.

The reader should be aware that portions of the analysis were treated in a somewhat simplistic fashion for the sake of analytical convenience. More specifically, these results depend critically on a specific scenario of assumed future prices, market penetration rates, housing stock changes, and "representative technology units." Such assumptions, forecasts, and other necessary simplifications, no matter how well represented, will still be imperfect approximations. It is therefore appropriate to assess the sensitivity of these results to changes in the scenario of assumptions.

(a) See the "Annual Household Energy Consumption" estimates that are presented in Table 6.1 and subtract the estimated consumption of the thermally efficient home from that of the base case home to obtain these per representative household annual energy savings estimates.

TABLE 6.7. Estimated National Annual Electrical Savings from Improved Thermal Efficiency Measures (BkWh)

<u>Year</u>	<u>Existing Home Heating</u>	<u>Existing Home Cooling</u>	<u>New Home Heating</u>	<u>New Home Cooling</u>	<u>Total Savings</u>
1985	.89	.89	.02	.02	1.82
1990	2.31	2.29	.15	.15	4.90
1995	5.86	5.82	.42	.41	12.51
2000	7.10	7.06	.79	.75	15.69

6.6 SENSITIVITY ANALYSIS

This section is an analysis of the sensitivity of the aggregate energy savings results presented in Section 6.5 to alterations in the market penetration scenario. Low and high market penetration scenarios are presented that imply a minimum/maximum range within which future energy savings are likely to occur. Also, the high penetration scenario implies what the maximum potential for national energy savings might be if programs or policies designed to increase the private utilization of the new energy saving measures were instituted.

6.6.1 Low Market Penetration Scenario

The advanced thermal efficiency measures may not penetrate the residential market as quickly or as completely, as indicated in Tables 6.5 and 6.6. Hence, it would be appropriate to investigate the implications of that possibility.

The specific low market penetration scenario investigated here assumes that the maximum potential level of penetration is only half of what it was estimated to be in both markets of the base case scenario. That is, the maximum market share was reduced from a 0.2 market share to a 0.1 market share for the retrofit market and from a 0.1 market share to a 0.05 market share for the new housing market. It is also assumed that only 75 percent of that new maximum market share potential will be achieved by the year 2000. Tables 6.8 and 6.9 combine that scenario with a housing stock forecast to obtain a low penetration estimate of the future number of thermally efficient retrofit and new housing units.

TABLE 6.8. Housing Stock Projections and Low Market Share Scenario of Thermal Efficiency Measures for Electrically Heating Residences

Year	Total Residences(a) (10 ⁶)	Retrofit Market(b) (10 ⁶)	Additional New Residences Market(a) (10 ⁶)	Residences Electrically Heated(c) (Percent)	Retrofit Market Share(d)	New Market Additions Share(d)	Cumulative Thermal Efficient Retrofitted Existing Housing Units(e) 10 ⁶	Additional Thermally Efficient New Housing Units(f) 10 ⁶	Cumulative Thermally Efficient New Housing Units(g) 10 ⁶	Annual Energy Savings From Cumulative Efficient Housing Units(h) (BkWh)
1984	90.6	90.6	1.9	14	0.02	0.01	0.25	0.003	0.003	0.72
1985	92.5	90.6	1.7	14	0.02	0.011	0.25	0.002	0.005	0.73
1986	94.2	90.6	1.7	14	0.0225	0.012	0.29	0.003	0.008	0.83
1987	95.9	90.6	1.7	14	0.025	0.013	0.32	0.003	0.011	0.93
1988	97.6	90.6	1.7	14	0.0275	0.014	0.35	0.003	0.014	1.03
1989	99.3	90.6	1.7	14	0.03	0.015	0.38	0.004	0.018	1.14
1990	101	90.6	1.6	14	0.0325	0.0165	0.41	0.004	0.021	1.24
1991	102.6	90.6	1.6	14	0.035	0.018	0.44	0.004	0.025	1.34
1992	104.2	90.6	1.6	14	0.04	0.02	0.51	0.004	0.030	1.54
1993	105.8	90.6	1.6	14	0.045	0.022	0.57	0.005	0.035	1.74
1994	107.4	90.6	1.6	14	0.05	0.025	0.63	0.006	0.040	1.94
1995	109	90.6	1.6	14	0.06	0.0275	0.76	0.007	0.047	2.32
1996	110.4	90.6	1.4	14	0.065	0.03	0.82	0.006	0.053	2.52
1997	111.8	90.6	1.4	14	0.0675	0.032	0.86	0.007	0.060	2.64
1998	113.2	90.6	1.4	14	0.07	0.034	0.89	0.007	0.067	2.76
1999	114.6	90.6	1.4	14	0.0725	0.036	0.92	0.007	0.074	2.87
2000	116	90.6	1.4	14	0.075	0.0375	0.95	0.007	0.081	2.99

(a) Source: NEPP Forecasts.

(b) Retrofit Market = Existing Stock as of 1984.

(c) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984).

(d) See Chapter 4.0.

(e) Calculated by: (Retrofit Market) x (Percent Electric) x (Retrofit Share).

(f) Calculated by: (New Market Additions) x (Percent Electric) x (New Additions Share).

(g) Calculated by: summing each years additional thermally efficient new units to the cumulative numbers of the previous year.

(h) Calculated by: [(Cumulative Retrofitted Thermally Efficient Units) x (2797 kWh) + (Cumulative New Thermally Efficient Housing Units) x (4094 kWh)].

TABLE 6.9. Housing Stock Projections and Low Market Share Scenario of Thermal Efficiency Measures for Electrically Cooled Residences

Year	Total Residences(a) (10 ⁶)	Retrofit Market(b) (10 ⁶)	Additional New Residences Market(a) (10 ⁶)	Residences Electrically Heated(c) (Percent)	Retrofit Market Share(d)	New Market Additions Share(d)	Cumulative Thermal Efficient Retrofitted Existing Housing Units(e) 10 ⁶	Additional Thermally Efficient New Housing Units(f) 10 ⁶	Cumulative Thermally Efficient New Housing Units(g) 10 ⁶	Annual Energy Savings From Cumulative Efficient Housing Units(h) (BkWh)
1984	90.6	90.6	1.9	56	0.02	0.01	1.01	0.011	0.011	0.72
1985	92.5	90.6	1.7	56	0.02	0.011	1.01	0.010	0.020	0.73
1986	94.2	90.6	1.7	56	0.0225	0.012	1.14	0.011	0.031	0.82
1987	95.9	90.6	1.7	56	0.025	0.013	1.27	0.012	0.043	0.92
1988	97.6	90.6	1.7	56	0.0275	0.014	1.40	0.013	0.056	1.02
1989	99.3	90.6	1.7	56	0.03	0.015	1.52	0.014	0.070	1.13
1990	101	90.6	1.6	56	0.0325	0.015	1.65	0.015	0.085	1.23
1991	102.6	90.6	1.6	56	0.035	0.018	1.78	0.016	0.100	1.33
1992	104.2	90.6	1.6	56	0.04	0.02	2.03	0.018	0.118	1.53
1993	105.8	90.6	1.6	56	0.045	0.022	2.28	0.020	0.138	1.72
1994	107.4	90.6	1.6	56	0.05	0.025	2.54	0.022	0.161	1.92
1995	109	90.6	1.6	56	0.06	0.0275	3.04	0.027	0.188	2.30
1996	110.4	90.6	1.4	56	0.065	0.03	3.30	0.025	0.213	2.50
1997	111.8	90.6	1.4	56	0.0675	0.032	3.42	0.026	0.240	2.62
1998	113.2	90.6	1.4	56	0.07	0.034	3.55	0.027	0.267	2.73
1999	114.6	90.6	1.4	56	0.0725	0.036	3.68	0.028	0.296	2.85
2000	116	90.6	1.4	56	0.075	0.0375	3.81	0.029	0.325	2.96

(a) Source: NEPP Forecasts.

(b) Retrofit Market = Existing Stock as of 1984.

(c) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984).

(d) See Chapter 4.0.

(e) Calculated by: (Retrofit Market) x (Percent Electric) x (Retrofit Share).

(f) Calculated by: (New Market Additions) x (Percent Electric) x (New Additions Share).

(g) Calculated by: summing each years additional thermally efficient new units to the cumulative number of the previous year.

(h) Calculated by: [(Cumulative Retrofitted Thermally Efficient Units) x (695 kWh) + (Cumulative New Thermally Efficient Housing Units) x (983 kWh)].

The national annual electrical energy savings estimates for the low market penetration scenario of the advanced thermal efficiency measures are presented in the last columns of Tables 6.8 and 6.9 and summarized in Table 6.10. The estimates were obtained by multiplying the year's estimated number of new "thermally efficient" housing units from the scenario times the estimates of the per unit annual electrical Energy savings. These results could be interpreted as being indicative of a reasonable minimum of the expected electrical energy savings from the new thermal efficiency measures.

6.6.2 High Market Penetration Scenarios

Under certain conditions, the advanced thermal efficiency measures may penetrate the market more rapidly than Tables 6.5 and 6.6 indicate. For example, if the government or certain utilities should decide that it would be a good investment to subsidize the installation of such measures, then the probable number of such installations would be increased. Hence, it is proper that the implications of that possibility be further investigated.

Specifically, the high market penetration scenario assumes that the maximum potential level of penetration is twice what it was estimated to be in both markets of the base use case scenario. To that effect, the maximum market share was increased from 0.2 for the new housing market. It is further assumed that the new maximum market share is achieved by 1995. Tables 6.11 and 6.12 combine that scenario with a housing stock forecast to arrive at high penetration estimates of the future number of thermally efficient retrofit and new housing units.

TABLE 6.10. National Annual Electrical Savings Estimates from the Low Market Penetration Scenario for Advanced Thermal Efficiency Measures (BkWh)

<u>Year</u>	<u>Existing Home Heating</u>	<u>Existing Home Cooling</u>	<u>New Home Heating</u>	<u>New Home Cooling</u>	<u>Total Savings</u>
1985	.71	.71	.02	.02	1.48
1990	1.15	1.15	.09	.08	2.48
1995	2.13	2.12	.19	.18	3.70
2000	2.56	2.55	.43	.41	5.95

The national annual electrical energy savings estimates for the high market penetration scenario of the advanced thermal efficiency measures are presented in the last columns of Tables 6.11 and 6.12, respectively, and summarized in Table 6.13. These estimates were derived at by multiplying the year's estimated number of new "thermally efficient" housing units from the high scenario by the estimates of the per unit annual electrical energy savings from the new thermal efficiency measures. They are representative of a plausible maximum for the expected future electrical energy savings from the advanced thermal efficiency measures.

6.7 COST PER KWH OF ENERGY SAVED CALCULATIONS AND COMPARISONS TO THE COST PER KWH OF CONSTRUCTING AND OPERATING NEW GENERATING CAPACITY

The advanced thermal efficiency measures may be considered as potential investments for utilities to include in their "generating portfolio". If the cost per kWh of these electricity savings produced by these investments is less than the cost per kWh of producing that power, then undertaking such investments would be cost-effective for the utility.

The calculations of the cost per kWh saved for heating, cooling, and heating and cooling combined due to the advanced thermal efficiency measures are presented in Table 6.14. These costs may be compared to the national estimated average cost of about 5.82¢/kWh for producing new generating capacity from a new coal-fired generating plant (see Table 4.3).

The specific indications are that the costs of both new and retrofit thermal efficiency installations are significantly less than the cost of new power for the purposes of heating and for heating and cooling combined. Another indication is that the thermal efficiency measures would be a relatively poor investment for locations which have large power demands for cooling relative to the demands for heating. In general, however, it appears that the advanced thermal efficiency measures are good investments and deserve further consideration on a more regional basis.

TABLE 6.11. Housing Stock Projections and High Market Share Scenario of Thermal Efficiency Measures for Electrically Heated Residences

Year	Total Residences(a) (10 ⁶)	Retrofit Market(b) (10 ⁶)	Additional New Residences Market(a) (10 ⁶)	Residences Electrically Heated(c) (Percent)	Retrofit Market Share(d)	New Market Additions Share(d)	Cumulative Thermal Efficient Retrofitted Existing Housing Units(e) 10 ⁶	Additional Thermally Efficient New Housing Units(f) 10 ⁶	Cumulative Thermally Efficient New Housing Units(g) 10 ⁶	Annual Energy Savings From Cumulative Efficient Housing Units(h) (8kWh)
1984	90.6	90.6	1.9	14	0.02	0.01	0.25	0.003	0.003	0.72
1985	92.5	90.6	1.7	14	0.04	0.02	0.51	0.005	0.007	1.45
1986	94.2	90.6	1.7	14	0.065	0.04	0.82	0.008	0.015	2.37
1987	95.9	90.6	1.7	14	0.095	0.06	1.20	0.011	0.026	3.48
1988	97.6	90.6	1.7	14	0.13	0.085	1.65	0.015	0.042	4.78
1989	99.3	90.6	1.7	14	0.17	0.115	2.16	0.020	0.062	6.29
1990	101	90.6	1.6	14	0.22	0.145	2.79	0.025	0.087	8.16
1991	102.6	90.6	1.6	14	0.28	0.165	3.55	0.031	0.118	10.42
1992	104.2	90.6	1.6	14	0.34	0.18	4.31	0.038	0.156	12.70
1993	105.8	90.6	1.6	14	0.37	0.19	4.69	0.041	0.198	13.94
1994	107.4	90.6	1.6	14	0.39	0.195	4.95	0.044	0.241	14.82
1995	109	90.6	1.6	14	0.4	0.2	5.07	0.045	0.286	15.36
1996	110.4	90.6	1.4	14	0.4	0.2	5.07	0.039	0.325	15.52
1997	111.8	90.6	1.4	14	0.4	0.2	5.07	0.039	0.365	15.68
1998	113.2	90.6	1.4	14	0.4	0.2	5.07	0.039	0.404	15.84
1999	114.6	90.6	1.4	14	0.4	0.2	5.07	0.039	0.443	16.00
2000	116	90.6	1.4	14	0.4	0.2	5.07	0.039	0.482	16.16

(a) Source: NEPP Forecasts.

(b) Retrofit Market = Existing Stock as of 1984.

(c) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984).

(d) See Chapter 4.0.

(e) Calculated by: (Retrofit Market) x (Percent Electric) x (Retrofit Share).

(f) Calculated by: (New Market Additions) x (Percent Electric) x (New Additions Share).

(g) Calculated by: summing each years additional thermally efficient new units to the cumulative numbers of the previous year.

(h) Calculated by: [(Cumulative Retrofitted Thermally Efficient Units) x (2797 kWh) + (Cumulative New Thermally Efficient Housing Units) x (4094 kWh)].

TABLE 6.12. Housing Stock Projections and High Market Share Scenario of Thermal Efficiency Measures for Electrically Cooled Residences

Year	Total Residences ^(a) (10 ⁶)	Retrofit Market ^(b) (10 ⁶)	Additional New Residences Market ^(a) (10 ⁶)	Residences Electrically Heated ^(c) (Percent)	Retrofit Market Share ^(d)	New Market Additions Share ^(d)	Cumulative Thermal Efficient Retrofitted Existing Housing Units ^(e) 10 ⁶	Additional Thermally Efficient New Housing Units ^(f) 10 ⁶	Cumulative Thermally Efficient New Housing Units ^(g) 10 ⁶	Annual Energy Savings From Cumulative Efficient Housing Units ^(h) (BkWh)
1984	90.6	90.6	1.9	56	0.02	0.01	1.01	0.011	0.011	0.72
1985	92.5	90.6	1.7	56	0.04	0.02	2.03	0.019	0.030	1.44
1986	94.2	90.6	1.7	56	0.065	0.04	3.30	0.031	0.061	2.35
1987	95.9	90.6	1.7	56	0.095	0.06	4.82	0.045	0.106	3.45
1988	97.6	90.6	1.7	56	0.13	0.085	6.60	0.062	0.168	4.75
1989	99.3	90.6	1.7	56	0.17	0.115	8.63	0.081	0.249	6.24
1990	101	90.6	1.6	56	0.22	0.145	11.16	0.099	0.347	8.10
1991	102.6	90.6	1.6	56	0.28	0.165	14.21	0.125	0.473	10.34
1992	104.2	90.6	1.6	56	0.34	0.18	17.25	0.152	0.625	12.60
1993	105.8	90.6	1.6	56	0.37	0.19	18.77	0.166	0.791	13.82
1994	107.4	90.6	1.6	56	0.39	0.195	19.79	0.175	0.965	14.70
1995	109	90.6	1.6	56	0.4	0.2	20.29	0.179	1.145	15.23
1996	110.4	90.6	1.4	56	0.4	0.2	20.29	0.157	1.301	15.38
1997	111.8	90.6	1.4	56	0.4	0.2	20.29	0.157	1.458	15.54
1998	113.2	90.6	1.4	56	0.4	0.2	20.29	0.157	1.615	15.69
1999	114.6	90.6	1.4	56	0.4	0.2	20.29	0.157	1.772	15.85
2000	116	90.6	1.4	56	0.4	0.2	20.29	0.157	1.929	16.00

(a) Source: NEPP Forecasts.

(b) Retrofit Market = Existing Stock as of 1984.

(c) Percentage based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984).

(d) See Chapter 4.0.

(e) Calculated by: (Retrofit Market) x (Percent Electric) x (Retrofit Share).

(f) Calculated by: (New Market Additions) x (Percent Electric) x (New Additions Share).

(g) Calculated by: summing each years additional thermally efficient new units to the cumulative number of the previous year.

(h) Calculated by: [(Cumulative Retrofitted Thermally Efficient Units) x (695 kWh) + (Cumulative New Thermally Efficient Housing Units) x (938 kWh)].

TABLE 6.13. National Annual Electrical Savings Estimates from the High Market Penetration Scenario for Advanced Thermal Efficiency Measures (BkWh)

<u>Year</u>	<u>Existing Home Heating</u>	<u>Existing Home Cooling</u>	<u>New Home Heating</u>	<u>New Home Cooling</u>	<u>Total Savings</u>
1985	1.42	1.41	.03	.03	2.89
1990	7.81	7.77	.35	.33	16.26
1995	14.24	14.12	1.12	1.11	30.59
2000	14.26	14.13	1.90	1.82	32.16

TABLE 6.14. Cost Per kWh Calculations for Advanced Thermal Insulation and Anti-Infiltration Techniques

Incremental Capital Cost (\$)(a)	
New Installation	= 2525
Retrofit Installation	= 1550
Levelized Capital Cost (\$/year)(b)	
New Installation	= 224.29
Retrofit Installation	= 137.68
New Installation	
Annual Energy Savings (kWh/year)(c)	
Heating	= 5,600 - 1,506 = 4,094
Cooling	= 2,275 - 1,292 = 983
Heating and Cooling	= 7,875 - 2,798 = 5,077
Retrofit Installation	
Annual Energy Savings (kWh/years)(c)	
Heating	= 5,900 - 3,103 = 2,797
Cooling	= 2,300 - 1,605 = 695
Heating and Cooling	= 8,200 - 4,708 = 3,492
New Installation Cost per kWh (¢/kWh)(d)	
Heating	= 22,429/4,094 = 5.48
Cooling	= 22,429/ 983 = 22.82
Heating and Cooling	= 22,429/5,077 = 4.42
Retrofit Installation Cost per kWh (¢/kWh)(d)	
Heating	= 13,768/2,797 = 4.92
Cooling	= 13,768/ 695 = 19.81
Heating and Cooling	= 13,769/3,492 = 3.94

- (a) See Table 6.3 f for the new and the retrofit scenario assumptions and see Table 6.4 for the incremental capital cost figure.
- (b) The level stream of annual payments the present value of which would equal the investment's incremental capital cost. Assumes a 30 year useful lifetime of the investment and an 8 percent rate of interest compounded annually. See Formula 4.11.
- (c) See Table 6.4.
- (d) Levelized Capital Cost (x 100¢/\$)/Annual Energy Savings.

6.8 REFERENCES FOR CHAPTER 6.0

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7.0 SOLAR WATER HEATERS

This chapter presents forecasts of the future electricity savings associated with adoption of solar water heaters. A technical description of this technology is provided in Section 7.1. Market availability is discussed in Section 7.2. The cost-effectiveness of a typical system is calculated in Section 7.3. Expected market penetration based on typical cost-effectiveness and the methodology of Chapter 4.0 is also provided in Section 7.3. In Section 7.4, these market penetration estimates are applied to housing stock data and forecasts in order to project numbers of solar water heaters in place in 1990, 1995 and 2000. Energy savings results and assumptions are presented in Section 7.5. Section 7.6 is an analysis of the sensitivity of the energy savings results to changes in the market penetration scenarios. Concluding Section 7.7 compares the estimated cost per kWh saved from solar water heaters with the estimated cost per kWh of new electrical generating capacity.

7.1 TECHNICAL BACKGROUND

Solar water heaters decrease the energy requirements for conventional water heaters by providing a source of preheated tap water. Solar water heaters supplement conventional water heaters and ordinarily do not replace them. All systems require collectors in a sunny location, a storage tank for the warmed water, and a back-up water heater (generally gas or electric). Solar water heaters typically preheat water to 110°F or more (McMillan 1981), and in sunny conditions can often provide all of a household's hot water. With a well-insulated hot water tank, some solar heat may be retained through night time hours and cloudy periods as well.

There are three basic types of solar water heaters: integral collector/-storage systems, passive (or thermosiphon) systems, and pumped systems. Integral collector/storage systems use the same unit for heat collection and water storage; i.e. the storage tank absorbs solar energy directly. Thermosiphon systems have separate collectors and storage tanks; fluid circulates heat between these components without use of a pump or moving parts. Heated fluids tend to rise and stratify in a given volume, with the hottest fluid on top. In

a thermosiphon water heating system, the fluid heated in the collector rises and circulates through the water storage tank. As the fluid travels, it cools down. The cooled fluid falls and returns to the bottom of the collector. Control valves may be necessary to prevent reverse siphon at night. Proper circulation in a thermosiphon system may require locating the storage tank at a higher elevation than the collector; this requirement can make use of a rooftop collector unworkable. Pumped solar water heaters have separate collectors and storage tanks. The solar water heater tank is installed next to a conventional water heater and feeds preheated water to it. Fluid is pumped from the solar system water tank to a collector, where it becomes warm. It circulates back through the solar water tank and loses its heat to this cooler reservoir. Cooled fluid is then pumped back up to the collector and the cycle is repeated.

A simple schematic of a pumped system is shown in Figure 7.1. The system shown in the diagram is known as a pumped heat exchange solar water heater and is typically used in regions where freezing occurs on a regular basis. A fluid that will not readily freeze at outside temperatures (such as a solution of ethylene glycol) is circulated through tubes connecting the solar water tank and collector components and passing through them. A flat plate collector is shown in Figure 7.1. Sunlight striking the cover of the collector plate transfers heat to the fluid-carrying tubing in the lower layer. The warmed fluid circulates to the water storage unit where it warms the stored water. The heat exchange fluid is then pumped back through the collector.

Pumped systems can circulate potable (i.e., drinkable) water instead of an anti-freeze solution. Such systems may save on capital costs and are appropriate in regions of the country where freezing is rare. However, they have greater failure potential than heat exchange systems.

The sizing of a solar water heater system depends on climate and family size. A solar system's tank should be sized to hold enough hot water for a day; on average, each person in a household uses approximately 20 gallons of hot water per day (Wright 1978). The necessary collector area may vary between regions of the country, but is unlikely that a unit providing 60 to 90 gallons a day will exceed 100 square feet. A typical range of sizes is 30 to 80 square feet.

Exploded view of flat-plate collector.

Two-tank system.

FIGURE 7.1. Pumped Heat Exchange Domestic Hot Water System
 Source: U.S. Department of Housing and Urban Development 1980a

7.2 CURRENT MARKET SITUATION

No published estimates of current national penetration of solar water heaters were located. In California, some counties require builders to consider the feasibility and benefits of solar water heating in new construction;

perhaps 30 percent of new construction has some form of solar water heater.^(a) In areas of the country where there is no local or state support, market penetration may approach zero. Climate also affects the degree of market penetration. A 1984 estimate shows overall market penetration of water heaters using neither electric resistance nor natural gas at 2 percent of households (Nesbit 1984). Oil, solar and other water heaters are included in this approximation, but the figure does not indicate how many households supplement conventional water heaters with solar.

Solar water heaters are available from numerous manufacturers and are distributed by dealers in all parts of the country. Interest in solar water heaters is increasing in some areas of the country. For example, a program designed according to U.S. Department of Housing and Urban Development (HUD) "Solarbank" requirements was implemented in Pennsylvania this year and seems to have helped sales significantly.^(b) The product mix is changing, however. Active (pumped) domestic hot water systems have dominated the market in the past, but passive (thermosiphon or integral collector/storage) systems are now gaining ground (SolarAge staff report, August 1983).

Prices of solar water heaters vary more by region than by type of system. Passive systems (thermosiphon and integral collectors/storage) typically cost less because of their relative simplicity, but in fact the more expensive passive systems are priced in the same range as many pumped systems. Heat exchange systems generally require more collector area than other systems; this feature tends to make heat exchange systems more expensive.

7.3 COST EFFECTIVENESS AND MARKET PENETRATION

The cost effectiveness and the likely market penetration of solar water heaters are discussed in this section. Both of these quantities vary by region, but time and budget constraints precluded following up on regional

(a) Personal communication with David Sizelove, Solar Industries, Inc. representative, November 1984.

(b) Personal communication with Stephen McDonnell, Pennsylvania Governor's Energy Council, 1984.

distinctions. Instead, a reference case is developed. The use of a generalized reference case may result in biases which are noted at appropriate stages of the analysis. To begin the analysis, the payback period for the representative product/region is calculated, with and without government support, according to procedures discussed in Chapter 4.0 of this document. Next, technical factors that might preclude the use of solar water heaters in some situations are considered. Forecasts of the number of solar water heaters in place in 1990 and 2000 follow. The forecasts set the stage for aggregated projections of electricity use in domestic water heating, with and without displacements of electricity demand due to the use of solar water heaters.

7.3.1 Cost Effectiveness of Representative Product

The capital cost, operating cost, and energy savings of conventional water heating versus water heating supplemented with solar energy are calculated in this subsection. The "representative" system has a payback period of 19.9 years. The assumptions and calculations are explained in the following paragraphs.

Conventional Electric Resistance Water Heating

Electric water heaters generally store water and heat it in the same unit. Incoming water (not preheated) is usually about 55°F (McMillan 1981). Water may be heated up to about 210°F depending on the model; the temperature is usually controlled with an automatic thermostat. Tank size may range from compact to about 82 gallons. A 52 gallon size is typical for a family of four.

The installed initial cost of electric water heaters may vary from about \$300 to \$600, depending on the model and whether the installation is to a newly constructed home or is a retrofit to an existing house.^(a) However, only operating costs are of concern in the present analysis because a solar water heater would always be installed with a conventional water heater, and,

(a) Sears Roebuck and Company, Pasco, Washington, November 1984, and DOE personal communication with Mr. Roehl of Roehl Plumbing, Kennewick (November 1984).

therefore, the capital costs of the conventional system can be ignored in the remainder of the analysis. Only the incremental installed cost of the solar water heater is relevant.

Energy consumption by electric water heaters varies significantly between households depending on the quantity of water used and the type of heater; samples of usage are 4515 kWh per year for single-family homes and 2730 kWh per year for multi-family dwellings (DOE/EIA 1984), and 4745 kWh per year (52 gal model, General Electric 1979). Annual energy consumption for the electric water heater reference case is assumed to be 5147 kWh per year, a weighted average based on sub-metered hot water data in the Pacific Northwest (Northwest Power Planning Council 1983). This figure is similar to that used in the Oak Ridge National Laboratory Residential Energy Use Simulation Model.^(a) Using an energy price of 7.18¢/kWh, operating costs of the reference conventional system are \$370/year.

Solar Water Heating. A pumped heat exchange water heater produced by a major manufacturer (the 80-gal capacity Solar Industries Heat Exchange System 12063) is used as the solar water heater reference, and two 4 x 8 ft collectors (appropriate for a Portland, Oregon or New Jersey location) are assumed. The necessary collector area depends on climate; one 4 x 10 ft collector might suffice in southern Florida while three 3 x 8 ft collectors would be more appropriate in Seattle.^(b)

Installed costs of standard solar water heaters actually can range from about \$1600 to \$5000. Total installed costs for a heat exchange solar system range from about \$60 to \$70 per square foot of collector space, while other pumped solar systems cost from \$50 to \$60/sq ft. For the reference case, we assume that installed costs are approximately \$60/sq ft, including materials and labor;^(c) with two 4 x 8 ft collectors (net area is 30.7 ft²/collector) the installed cost of this solar reference case is \$3684.

(a) Conversation with T.J. Secrest, Pacific Northwest Laboratory.

(b) Personal communication with David Sizelove, Solar Industries, Inc. representative, November 1984.

(c) Personal communication with David Sizelove, Solar Industries, Inc. representative, November 1984.

Government loans and some subsidies are frequently available for solar water heaters. Every state currently participates in a federal-level (HUD) program (Solar Bank) except Alaska, Wyoming, and South Dakota.^(a) To date, the solar component of this program has not been very active, but in states where the solar incentives are actively used significant loans and grants are authorized. The maximum amount of assistance for solar domestic hot water systems is \$1000 per dwelling unit or 40 percent of their cost, whichever is less, for one- to four-family residential buildings (Solar Energy and Energy Conservation Bank 1984). A variety of other incentives may exist at state and local levels, including income and property tax credits and utility rebates. As of April 10, 1984, 29 states had income tax credits for solar purchases in place (Malloy 1984). Non-market support appears to be common, but is not included in the reference system's cost since one cannot predict whether it will continue during the projection period.

Operating Cost Savings. A solar water heater reduces water heating electricity consumption from 30 to 50 percent in northern locations, and 50 to 75 percent in southern locations (HUD, 1979; conversation with Tom Shea, Heliotherm, November 1984). Assuming 50% annual savings on energy costs, 5147 kWh per year on conventionally-operated hot water heaters and 7.18¢/kWh, cost savings from a solar water heater installation amount to \$185 per year.

Hot Water System Payback Period

The payback period for a representative solar water heater is calculated in Table 7.1. In the reference case, 19.9 years are required to recover the investment. A solar water heater with the same initial cost, that supplemented the same conventional water heater with the same price for electricity should have a longer payback period in cloudier and more northern climates and a shorter payback period in sunnier and more southern climates. Where electricity prices are higher, the payback period is shorter. With a government subsidy of \$1000, an amount that is not uncommon, the payback period for the representative solar water heater would be 14.5 years.

(a) Telephone conversation with Julia Fermoile, Solar Energy and Energy Conservation Bank, November 16, 1984.

TABLE 7.1. Payback Period of Representative
Solar Water Heater

<u>Initial Installed Cost of New System:</u>	\$3684
<u>Operating Cost Savings:</u>	\$185.00/yr ^(a)
<u>Payback Period:</u>	
(Initial Cost ÷ Annual Savings)	19.9 yr

(a) Based on 50 percent displacement of hot water heating by solar system and \$370 annual electricity bill with no solar water heater supplement.

7.3.2 Technical Limits

Technical limits are defined as those limitations that preclude use of the technology at any cost. A hypothetical example would be the use of a solar water heating system without freeze protection in Minnesota. Solar water heating manufacturers appear to have developed products to meet most regional needs. Although lower savings and higher capital costs may occur in unfavorable climates, these conditions do not prohibit the use of solar water heaters for technical reasons. No quantifiable technical limits were found, and the remainder of this analysis proceeds on the assumption that any household with a conventional water heater is a potential candidate for supplemental solar water heating.

7.3.3 Market Penetration Assumptions

Market penetration is assumed to be a function of payback period, as described in the methodology chapter (refer to Table 4.1). Based upon a representative payback period of 19.9 years, the probable maximum market penetration of solar water heaters on existing units using electric resistance water heating is 5 percent. Maximum consumer acceptance in new markets may be lower; nevertheless, 5 percent is used for both energy savings calculations. As explained in Chapter 4.0, this market penetration figure implies that sales of the conservation technology, solar water heaters, in the year 2000 amount to 5

percent of the sales of the conventional technology, electric water heaters. It also implies that 5 percent of the existing 1984 stock will have been retrofitted with solar water heaters by the year 2000. Section 7.6 discusses the impacts on the analysis of higher and lower assumed market penetration.

7.4 HOUSING STOCK PROJECTIONS AND MARKET SHARE ESTIMATES

Stock data (existing number of residential electric water heaters, expected rate of growth, and expected additions of solar water heaters) are discussed in this section. Table 7.2 shows projections of housing stock, electric water heaters and solar water heaters at yearly intervals from 1984 to 2000. Housing projections are based on projections supporting the National Energy Policy Plan (DOE 1983). The percentage of houses using electricity for water heating (31.8 percent) is extracted from the 1981 Residential Energy Consumption Survey (DOE/EIA 1984).^(a) Market shares for solar water heaters are estimated as described in Chapter 4.0 and are based on a payback period exceeding 10 years.

7.5 ENERGY SAVINGS RESULTS

Energy savings of 2574 kWh per year are assumed to be typical for solar water heaters with electric resistance domestic hot water backup. In this section, expected energy savings for the nation as a whole are projected, based on per-unit savings and expected market penetration. The final column of Table 7.2 shows projections of energy savings from supplementation of electric water heating by solar water heating in the residential sector. Projected annual energy savings are 4.27 BkWh by the year 2000. These projections are summarized in Table 7.3.

The above projections of energy savings are subject to several limitations. Regional differences are not accounted for in the cost-effectiveness calculation, which was used to project market shares of solar water heaters.

(a) According to J. B. Hoyt, Manager of Forecasting and Market Analysis, Whirlpool Corporation, the 1980 Census of Housing shows a split on water heating of 57.5 percent gas, 33.5 percent electric, 8 percent fuel oil and the remainder, other sources (personal communication, November (1984)).

TABLE 7.2. Housing Stock Projections, Annual Market Share, and Electricity Savings for Solar Water Heaters With Electric Water Backup

Year	Annual New Housing Additions ^(a) (10 ⁶)	Residences With Electric Water Heating ^(b) (Percent)	Market Share for New and Retrofit Applications ^(c)	Annual Solar Water Heater Additions in New Housing ^(d) (10 ⁶)	Cumulative Solar Water Heater Additions in New Housing ^(e) (10 ⁶)	Cumulative Retrofit Solar Water Heater Additions ^(f) (10 ⁶)	Cumulative New and Retrofit Solar Water Heater Additions ^(g) (10 ⁶)	Cumulative Annual Energy Savings ^(h) BkWh
1984	1.9	0.318	0.010	0.006	0.006	0.29	0.29	0.76
1985	1.7	0.318	0.011	0.006	0.012	0.32	0.33	0.85
1986	1.7	0.318	0.012	0.006	0.018	0.35	0.36	0.94
1987	1.7	0.318	0.013	0.007	0.025	0.37	0.40	1.03
1988	1.7	0.318	0.015	0.008	0.032	0.43	0.46	1.19
1989	1.7	0.318	0.017	0.009	0.040	0.49	0.53	1.36
1990	1.6	0.318	0.020	0.010	0.049	0.58	0.63	1.61
1991	1.6	0.318	0.023	0.012	0.059	0.66	0.72	1.86
1992	1.6	0.318	0.027	0.014	0.071	0.78	0.85	2.18
1993	1.6	0.318	0.031	0.016	0.084	0.89	0.98	2.52
1994	1.6	0.318	0.035	1.018	0.100	1.01	1.11	2.85
1995	1.6	0.318	0.039	1.020	0.118	1.12	1.24	3.20
1996	1.4	0.318	0.043	1.019	0.138	1.24	1.38	3.51
1997	1.4	0.318	0.045	1.020	0.157	1.30	1.45	3.74
1998	1.4	0.318	0.047	1.021	0.177	1.35	1.53	3.94
1999	1.4	0.318	0.049	1.022	0.198	1.41	1.61	4.14
2000	1.4	0.318	0.050	1.022	0.220	1.44	1.66	4.27

(a) Source: NEPP Forecasts

(b) Percentage is based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(c) See Chapter 4.0

(d) Calculated by: (Annual housing additions) x (market share)

(e) Calculated by: Current years additions + previous years cumulative additions

(f) Calculated by: Total 1984 housing (90.6 million) x market share for retrofit applications. Assumes that there is no retirement of housing stock.

(g) Calculated by: Cumulative additions to New housing + Cumulative retrofitted additions

(h) Calculated by: (Cumulative additions of solar water heaters) x (2574 kWh/year)

TABLE 7.3. Projections of Energy Savings with Market Penetration of Solar Water Heaters

<u>Year</u>	<u>Energy Savings (BkWh)</u>
1985	.85
1990	1.61
1995	3.20
2000	4.27

In addition, projected market shares were based only on a payback criterion and did not account for other factors, such as uncertain future electricity rates, which may also be significant in consumer purchase decisions.^(a) Finally, the analysis does not extend to technologies other than solar water heating, such as heat pump water heaters, which may also displace electric water heating in future years.

7.6 SENSITIVITY OF ANALYSIS TO MARKET PENETRATION ASSUMPTIONS

This section summarizes two variations of the scenario discussed in Sections 7.3, 7.4 and 7.5. The first variation assumes the same per unit energy savings but reduces the assumed maximum market penetration by 50 percent; additionally, maximum market penetration is assumed to occur more slowly than in the base case. Thus, fewer units are installed and less energy is saved. Section 7.6.1 summarizes the low market penetration scenario. The second variation also assumes the same per unit energy savings, but the assumed maximum market penetration is doubled. In addition, maximum market penetration is assumed to occur more quickly than in the base case. Thus, more units are installed and energy savings are larger. Section 7.6.2 summarizes the high market penetration scenario.

(a) Conversation with William Dokas, Sun Solector Corporation, 11/21/84.

7.6.1 Low Market Penetration Scenario

The maximum market penetration assumed in previous sections is, at 5 percent, already very low. If it were reduced by 50 percent, and if by the year 2000 only 75 percent of the units that might eventually be installed had been installed, 640,000 solar water heaters with electric back-up are projected for residential use at the turn of the century. Assuming energy savings of 2573.5 kWh per year per unit, annual electricity savings for solar water heaters would be less than 1.64 BkWh in the year 2000. Annual market share assumptions and projected energy savings are presented in Table 7.4.

7.6.2 High Market Penetration Scenario

In the scenario of this section, maximum market penetration is assumed to reach 10 percent by the year 1995. This is double the maximum assumed in Sections 7.3, 7.4, and 7.5. Both the faster rate of adoption and the higher maximum seem reasonable given the numbers of solar water heaters already purchased despite long payback periods. For example, a 1979 report indicated that 11,000 solar domestic hot water systems were already installed in California alone, and that California installations account for about one-third of installations nationwide (HUD 1980b). The high market penetration scenario assumes 360,000 units nationwide in 1985 and more than 3 million units by 1995. Electricity savings would reach 8.67 BkWh annually by the year 1995. Table 7.5 presents annual market share assumptions and projected energy savings for the high market penetration scenario.

7.7 COMPARISON OF COSTS: NEW GENERATING CAPACITY VERSUS ENERGY CONSERVATION WITH SOLAR WATER HEATERS

The cost of conserving electricity with solar water heating does not compare favorably with the cost of generating new power using the assumptions of this analysis. The cost per kWh conserved with solar water heating is calculated in Table 7.6. The cost per kWh saved (approximately 15¢) is much higher than the cost of new power generation per kWh cited in Table 4.3.

TABLE 7.4. Low Market Scenario Housing Stock Projections, Annual Market Share, and Electricity Savings for Solar Water Heaters With Electric Water Backup

Year	Annual New Housing Additions ^(a) (10 ⁶)	Residences With Electric Water Heating ^(b) (Percent)	Market Share for New and Retrofit Applications ^(c)	Annual Solar Water Heater Additions in New Housing ^(d) (10 ⁶)	Cumulative Solar Water Heater Additions in New Housing ^(e) (10 ⁶)	Cumulative Retrofit Solar Water Heater Additions ^(f) (10 ⁶)	Cumulative New and Retrofit Solar Water Heater Additions ^(g) (10 ⁶)	Cumulative Annual Energy Savings ^(h) BkWh
1984	1.9	0.318	0.005	0.003	0.003	0.14	0.15	0.38
1985	1.7	0.318	0.006	0.003	0.006	0.16	0.16	0.42
1986	1.7	0.318	0.006	0.003	0.009	0.17	0.18	0.47
1987	1.7	0.318	0.007	0.004	0.012	0.19	0.21	0.53
1988	1.7	0.318	0.008	0.004	0.016	0.22	0.23	0.60
1989	1.7	0.318	0.009	0.005	0.020	0.24	0.26	0.68
1990	1.6	0.318	0.010	0.005	0.025	0.28	0.30	0.78
1991	1.6	0.318	0.011	0.006	0.029	0.32	0.35	0.89
1992	1.6	0.318	0.013	0.007	0.035	0.37	0.41	1.05
1993	1.6	0.318	0.015	0.007	0.042	0.42	0.46	1.18
1994	1.6	0.318	0.016	0.008	0.049	0.45	0.50	1.28
1995	1.6	0.318	0.016	0.008	0.057	0.47	0.53	1.36
1996	1.4	0.318	0.017	0.008	0.065	0.49	0.56	1.43
1997	1.4	0.318	0.018	0.008	0.073	0.50	0.58	1.49
1998	1.4	0.318	0.018	0.008	0.081	0.52	0.60	1.54
1999	1.4	0.318	0.019	0.008	0.089	0.53	0.62	1.60
2000	1.4	0.318	0.019	0.008	0.097	0.54	0.64	1.64

(a) Source: NEPP Forecasts

(b) Percentage is based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(c) See Chapter 4.0

(d) Calculated by: (Annual housing additions) x (market share)

(e) Calculated by: Current years additions + previous years cumulative additions

(f) Calculated by: Total 1984 housing (90.6 million) x market share for retrofit applications. Assumes that there is no retirement of housing stock.

(g) Calculated by: Cumulative additions to New housing + Cumulative retrofitted additions

(h) Calculated by: (Cumulative additions of solar water heaters) x (2574 kWh/year)

TABLE 7.5. High Market Scenario Housing Stock Projections, Annual Market Share, and Electricity Savings for Solar Water Heaters With Electric Water Backup

Year	Annual New Housing Additions ^(a) (10 ⁶)	Residences With Electric Water Heating ^(b) (Percent)	Market Share for New and Retrofit Applications ^(c)	Annual Solar Water Heater Additions in New Housing ^(d) (10 ⁶)	Cumulative Solar Water Heater Additions in New Housing ^(e) (10 ⁶)	Cumulative Retrofit Solar Water Heater Additions ^(f) (10 ⁶)	Cumulative New and Retrofit Solar Water Heater Additions ^(g) (10 ⁶)	Cumulative Annual Energy Savings ^(h) BkWh
1984	1.9	0.318	0.010	0.006	0.006	0.29	0.29	0.76
1985	1.7	0.318	0.012	0.006	0.012	0.35	0.36	0.92
1986	1.7	0.318	0.015	0.008	0.019	0.43	0.45	1.16
1987	1.7	0.318	0.020	0.011	0.027	0.58	0.60	1.55
1988	1.7	0.318	0.028	0.015	0.037	0.81	0.84	2.17
1989	1.7	0.318	0.038	0.021	0.053	1.09	1.15	2.95
1990	1.6	0.318	0.050	0.025	0.073	1.44	1.51	3.90
1991	1.6	0.318	0.065	0.033	0.099	1.87	1.97	5.07
1992	1.6	0.318	0.075	0.038	0.132	2.16	2.29	5.90
1993	1.6	0.318	0.084	0.043	0.170	2.42	2.59	6.67
1994	1.6	0.318	0.093	0.047	0.213	2.68	2.89	7.44
1995	1.6	0.318	0.100	0.051	0.260	2.88	3.14	8.08
1996	1.4	0.318	0.100	0.045	0.311	2.88	3.19	8.22
1997	1.4	0.318	0.100	0.045	0.355	2.88	3.24	8.33
1998	1.4	0.318	0.100	0.045	0.400	2.88	3.28	8.45
1999	1.4	0.318	0.100	0.045	0.444	2.88	3.33	8.56
2000	1.4	0.318	0.100	0.045	0.489	2.88	3.37	8.67

(a) Source: NEPP Forecasts

(b) Percentage is based on estimates from the 1982 Residential Energy Consumption Survey (DOE/EIA 1984)

(c) See Chapter 4.0

(d) Calculated by: (Annual housing additions) x (market share)

(e) Calculated by: Current years additions + previous years cumulative additions

(f) Calculated by: Total 1984 housing (90.6 million) x market share for retrofit applications. Assumes that there is no retirement of housing stock.

(g) Calculated by: Cumulative additions to New housing + Cumulative retrofitted additions

(h) Calculated by: (Cumulative additions of solar water heaters) x (2574 kWh/year)

TABLE 7.6. Cost per kWh Calculation for Representative Solar Water Heater

<u>Technology</u>	<u>Incremental Capital Cost (a) (\$1984)</u>	<u>Levelized Capital Cost (b) (\$/yr)</u>	<u>Annual Energy Savings (c) (kWh/yr)</u>	<u>Cost per kWh (d) (\$/kWh)</u>
Solar water heater	3684	375	2574	14.6

(a) Refer to Table 7.1.

(b) Refer to Equation 4.11. Assumes a 20-year lifetime of the investment and an 8 percent rate of interest compounded annually.

(c) Refer to discussion of operating cost savings in Section 7.3. Assumes 50 percent savings over a conventionally-operated water heater using 5147 kWh per year.

(d) Calculated by: $(\text{Levelized Capital Cost}) \div (\text{Annual Energy Savings}) = \text{cost per kWh}$.

The initial costs of solar water heaters and the energy savings to be expected from them vary greatly by region. Thus, there may be regions of the United States where the cost of energy conserved with solar water heating compares favorably with the cost of generating new power. Nevertheless, it appears that in most regions conserving with this technology is likely to be more expensive than generating power supplies from new power plants.

7.8. REFERENCES FOR CHAPTER 7.0

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8.0 HIGH EFFICIENCY APPLIANCES

This chapter addresses efficiency improvements to refrigerators and freezers in the residential sector. Due to the limited scope of this project, it was not feasible to estimate electricity savings for all home appliances. Refrigerators and freezers were selected for analysis because they account for the largest proportion of electricity use among residential appliances (DOE/BERD 1984; AHAM 1984a). Technical background is provided in Section 8.1. The current United States refrigerator/freezer market is profiled in Section 8.2; the popularity of various products is discussed and potential shifts in the market are identified. The cost-effectiveness of selected high efficiency products are calculated in Section 8.3. Cost and efficiency assumptions involved in this calculation are discussed in detail. Based on representative cost-effectiveness, market penetration is projected. In Section 8.4, the market penetration projections are applied to appliance stock data and forecasts in order to project new sales and retrofits by 1990, 1995 and 2000. Projected electricity savings from the adoption of more efficient refrigerators and freezers are presented in Section 8.5. Section 8.6 is an analysis of the sensitivity of the energy savings results to changes in the market penetration scenarios. Section 8.7 compares the estimated cost per kWh saved from more efficient refrigerators and freezers with the estimated cost per kWh of new electricity generation capacity.

8.1 TECHNICAL BACKGROUND

A number of products, whose energy use and other features differ markedly, are classified as refrigerators and/or freezers. Subsection 8.1.1 begins with definitions of the appliances. Typical differences in energy consumption by product type are identified. The technical bases for conservation measures are explained in Subsection 8.1.2. Measures are identified and grouped according to the subsystem of refrigeration to which they are directed. These subsystems include the heat pump, the refrigerator/freezer box, and auxiliary systems such as automatic defrost. Conservation potential from modified consumer habits is not discussed. Subsection 8.1.3 provides an overview of the extent to which

manufacturers have implemented various conservation measures. Salient differences between American refrigerators/freezers and corresponding Japanese products are addressed. This international comparison is warranted because the potential for Japan to market refrigerators and freezers in the United States introduces great uncertainty into future developments in United States appliance markets. Unfortunately, limits to test methods prevent good international comparison. Different test procedures are used in the United States and Japan to rate appliance use. These testing differences, as well as the use of test data rather than actual meter readings to rate energy use, prevent direct comparison of the relative energy use of American and Japanese refrigerators and freezers. These limitations are also discussed in Subsection 8.1.3.

8.1.1 Product Definitions

Definitions of refrigerators and freezers are standardized:

"(a) Refrigerators and refrigerator-freezers.

- (1) "Electric refrigerator" means a cabinet designed for refrigerated storage of food at temperatures above 32°F and having a source of refrigeration requiring an electrical energy input only. It may include a compartment for the freezing and storage of food at temperatures below 32°F but does not provide a separate low-temperature compartment designed for the freezing of and long-term storage of food at temperatures below 8°F. It has only one exterior door, but it may have interior doors or compartments.
- (2) "Electric refrigerator-freezer" means a cabinet which consists of two or more compartments with at least one of the compartments designed for the refrigerated storage of foods at temperatures above 32°F and with at least one of the compartments designed for the freezing of and the storage of frozen foods at temperatures of 8°F or below and which may be capable of adjustment by the user to a temperature of 0°F or below. The source of refrigeration requires an electric energy input only.

- (b) "Freezer" means a cabinet designed as a unit for the storage of food at temperatures of 0°F or below and which has the ability to freeze food. The source of refrigeration requires an electric energy input only."

(Labeling and Advertising for Consumer Appliances 1984)

In this analysis, both electric refrigerators and electric refrigerator-freezers are referred to as refrigerators. The term "freezer" describes a separate chest or upright freezer.

Each appliance category (refrigerator, refrigerator/freezer, or freezer) encompasses several product types. The product types are differentiated by size, storage temperatures, physical arrangements and amenities. Table 8.1 summarizes how these variations affect energy use. A study that weights factors influencing customer decisions was conducted by Pacific Gas & Electric in California and is cited by David Goldstein of the Natural Resources Defense Council (Goldstein 1983). The study shows that refrigerator/freezer energy efficiency is less important to customers than most other features, including brand, suitability, and color.

8.1.2 Measures to Improve Efficiency

Cold food storage has become more energy efficient in recent years and can be improved further through various design modifications. Improved heat pump systems can reduce the electricity needed to remove heat from cabinet interiors. Better refrigerator box insulation, by doing a better job at keeping warm air out, can minimize the amount of heat that needs to be removed. Automatic defrost and other auxiliary systems can be designed with better attention to energy use, so that the same convenience features are provided for less additional electric load. In this section, conservation measures directed at these refrigeration subsystems are discussed in more detail.

Obtaining Low-Temperature Interiors: Cold temperatures are produced inside refrigerators and freezers when heat from a unit's interior is rejected to the room. The flow of heat is the reverse of what would occur naturally, since heat tends to migrate from warmer to cooler objects. In refrigerators manufactured by U.S. producers, heat removal is accomplished with a compression refrigeration system. The compression refrigerator works by circulation of a fluid that absorbs heat from the refrigerator's interior and rejects heat to the refrigerator's exterior. In addition to the refrigerant fluid, a compression refrigeration system has an evaporator (i.e., a cold coil), a condenser (i.e., a hot coil), a motor-driven pump and compressor, and a capillary tube

TABLE B.1. Product Features and Their Impact on Appliance Energy Use

<u>Product Feature</u>	<u>Advantage</u>	<u>Impact on Relative Energy Use (Other Features Held Constant)</u>
Automatic Defrost	Convenience	Automatic defrost uses more energy than manual defrost. Automatic defrosting requires energy to circulate dry cold air, and to melt frost when performing a defrost cycle. In addition, defrost heat adds to the heat that must be removed from the cabinet in order to keep compartment temperatures cold.
Anti-Sweat Heater	Prevents condensation on cabinet exterior in humid climates	Cabinet heaters consume power directly, and they indirectly increase energy consumption by adding to the heat load of the refrigerator.
Physical Arrangement of Refrigerator and Freezer Compartments:		
1. Side-Mounted Freezer	Equal accessibility of fresh and frozen stored foods	Side-mounted freezers characteristically consume more energy than top mounts because of increased door seal area, and because the freezer floor is close to the hot motor compartment.
2. Bottom-Mounted Freezer	Improved access to fresh stored foods	Bottom-mounted freezers require more energy than top mounts because freezer is closer to the hot motor compartment, it takes more fan power to move cold air from the freezer evaporator to the top of the fresh-food compartment, and auxiliary heat is often needed in the crisper area to prevent freezing.
Chest Versus Upright Freezer	Suitability and customer preference	For comparable model sizes, chest freezers lose less energy through gaskets and

TABLE 8.1. (contd)

Product Feature	Advantage	Impact on Relative Energy Use (Other Features Held Constant)
Chest Versus Upright Freezer (contd)		around door openings than upright freezers. Chest freezers tend to use less energy than upright freezers.
Freezer to Fresh-Food Compartment Volume Ratio	Customer needs and preferences	Energy consumption is expected to go up at higher freezer to fresh-food compartment volume ratios. More heat must be extracted and kept out in order to maintain a larger volume at freezer, rather than refrigerator, temperatures.
Low Freezer Compartment Temperature	Allows frozen food to be stored for longer periods	Lower freezer compartment temperatures result in higher heat leakage to the freezer and greater total energy use.
Net Volume	Suitability	If the product line is held constant, larger refrigerators, refrigerator/freezers and freezers tend to use more energy than smaller units. However, the energy use per unit volume tends to decrease with larger volumes. This is because energy losses occur at surfaces, and the ratio of surface area to volume decreases as the net volume is enlarged.
Availability of Through-the-Door Service Features	Convenience	Refrigerator doors containing dispenser equipment cannot be as well-insulated as doors without dispenser equipment. In addition, electric heaters may be required to prevent condensation on the dispenser hardware. Equipment with through-the-door service tends to consume more energy than equipment without it.

Sources: Arthur D. Little, Inc. 1982; Meier, Wright and Rosenfeld 1983.

that closes the refrigerant circulation system. The evaporator, refrigerant fluid, compressor, and motor used with the compressor can all be made more efficient than common practice. The function of each of these components is described in the following paragraphs.

The evaporator, a cold coil usually installed in the freezer compartment, is where the refrigerant fluid absorbs heat from the refrigerator's interior. The fluid boils, or evaporates, because it suddenly is given room to expand (the pressure drops). A liquid will boil even at low temperatures if the pressure is low enough. When the fluid changes from its liquid to vapor state, it absorbs heat. The temperature remains constant but the heat content of the vapor is greater than the heat content of the liquid.

Two changes to the evaporator might result in lower electricity loading. First, separate evaporator coils can be installed in the refrigerator and freezer sections. Frost buildup is greatly reduced by this measure, and intervals between energy-intensive defrost cycles can be extended. One commercial model, the Amana TSC-18E, used a twin evaporator system but is no longer produced commercially (Geller 1984). A second measure to improve evaporator efficiency is to increase evaporator surface area for more rapid heat exchange (Arthur D. Little 1982).

The condenser, or hot coil, is where the refrigerant fluid parts with its heat. The refrigerant fluid condenses from vapor to liquid because of higher pressure, and it loses heat during this condensation.

The compressor is responsible for increasing the pressure so that the refrigerant fluid condenses. An electrical motor drives a pump that compresses the refrigerant while it is still a gas. The compressor, including both the motor and the pump, uses about 80 percent of the total energy of a conventional refrigerator (Goldstein 1983).

Energy use by the compressor subsystem can be reduced considerably, some analysts estimate that such measures alone could reduce a refrigerator's energy use by 29 percent (Goldstein 1983). The motor efficiency can be improved by replacement of the conventional motor core with a low-loss core and by using copper, rather than aluminum, windings in the rotating coil in the motor. The

addition of a capacitor also improves motor efficiency; the capacitor curtails unnecessary power losses that occur when current and voltage are out of phase. A side benefit of better compressor efficiency is that a more efficient unit generates less waste heat. Waste heat from the compressor and motor adds to other heat that must be rejected from the refrigerator to the room; reducing waste heat thereby indirectly reduces the refrigerator's electricity load (Goldstein 1983).

The refrigerant fluid is chosen for its boiling temperature and pressure, and for the amount of heat it absorbs in the change from its liquid to vapor state. Properties of the refrigerant fluid affect the energy consumption of the compressor. A mixture of two refrigerant fluids might perform better in this respect than the single refrigerant fluid conventionally used (Goldstein 1983). However, this technique has not been demonstrated commercially.

Keeping Cold Air In and Warm Air Out: Once the temperature differential between the refrigerator/freezer's interior and the room is established, it must be maintained. Heat can get into the refrigerator four ways: by convection, conduction, radiation or transfer. Conductive and radiant heat transfer occur through the cabinet box. Convective heat transfer occurs when warm air infiltrates through door cracks and when warm air rushes in an open door. Convection is minimized with good door seals, while conduction and radiation are minimized with good insulation. Heat is transferred into a refrigerator when room-temperature materials are placed in it to be chilled.

Improvements in insulation materials and increased insulation thickness are likely to continue to reduce refrigerator and refrigerator-freezer electricity consumption. Conventional American refrigerators and freezers may be insulated with a few inches of fiberglass or with polyurethane foam with R-values per inch of 0.5 and 1.2, respectively. The R-values indicate thermal resistance; materials with high R-values are better insulators than materials with low R-values. Researchers at Oak Ridge National Laboratory and Arthur D. Little, Inc. recently demonstrated feasible appliance insulations with R-values per inch as high as 3.5 (McElroy and Yarbrough 1984). Substantial energy savings could be realized if these high R-value materials were to replace fiberglass or polyurethane foam in refrigerator/freezer construction. Current

American practice is to use 1.5 to 2.5 inches of insulation around the refrigerator, with slightly more around freezer sections. Increasing insulation thickness reduces conductive losses but is limited commercially by consumer needs for appliances that fit into existing spaces through existing doors. Insulation materials are becoming more effective. Improved insulation materials with greater thermal resistance is a likely technological development.

Conventional American refrigerators/freezers have a single door gasket (seal) to reduce leaks. Double gaskets can reduce convective leaks and are used in some Japanese models (Arthur D. Little 1982; Goldstein 1983).

Automatic Defrost and Anti-Sweat Heaters: Automatic defrost systems are large consumers of energy. A fan blows air past the evaporator, or cold coil; the air's humidity drops as it is cooled. The dehumidified air blows into the freezer compartment where the defrost cycle is completed. In American self-defrosting refrigerator/freezers this cycle occurs automatically several times a day (Goldstein 1983, 1984).

Manual initiation of the defrost cycle could conserve substantial amounts of energy; such a system is used in Toshiba (a Japanese manufacturer) refrigerator/freezers. In the Toshiba models the user must press a button up to three times a year to initiate a self-defrost cycle (Goldstein 1984). Less energy would run a defrost system if there were two separate evaporators (cold coils), one in the freezer compartment and one in the refrigerator compartment. A twin evaporator system is discussed elsewhere in this report; a design developed by Arthur D. Little, Inc. was incorporated in the Amana refrigerator model used in one of the case studies in Section 8.3. Another way to modify the defrost system is to use a more efficient fan. Less waste heat is generated by more efficient fans. As a result, less waste heat must be removed from the freezer.

Refrigerators and refrigerator/freezers commonly have cabinet heaters so that condensation will not form on the cabinet exterior. The heaters use electricity directly and add to the heat that must be removed from cabinet interiors. In dry climates, condensation will not form on the cabinet's exterior in any case. Some units now have an energy-saving feature, the anti-sweat heater switch (Consumer Guide 1984). This switch enables users in dry climates to shut off the unnecessary heater.

The energy-saving measures discussed for each refrigeration subsystem--the refrigeration cycle, the refrigerator box, and auxiliary systems--are summarized in Table 8.2.

8.1.3 Efficiency Measures in Standard Product Design

The efficiency of American refrigerators and freezers has improved dramatically since the early 1970s. Refrigerators (including refrigerator-freezers) were 66.4 percent more efficient in 1983 than in 1972 (shipment-weighted averages; AHAM 1984a). Much of this improvement is due to better insulation, with smaller contributions from more efficient motors and heat transfer systems. The rate of efficiency improvement has slowed down since the 1970s (AHAM 1984a; Geller 1984). The energy consumption per refrigerator/freezer averaged 1726 kilowatt-hours per year (kWh/yr) for 1972 U.S. shipments and 1160 kWh/yr for 1983 shipments (AHAM 1984a). The average electricity use

TABLE 8.2. Summary of Measures to Improve Efficiency in Refrigerators, Refrigerator-Freezers and Freezers

<u>Refrigeration Sub-System</u>	<u>Measures to Improve Efficiency</u>
Refrigeration Cycle	<ul style="list-style-type: none"> • use twin-evaporator • increase evaporator surface area • use copper windings in the compressor motor • add a capacitor to the compressor motor • use mixture of two refrigerant fluids
Heat Leakage	<ul style="list-style-type: none"> • use thicker insulation • use insulation with higher thermal resistance • use double gaskets at door seals
Auxiliary Systems	<ul style="list-style-type: none"> • initiate self-defrost cycle manually • install more efficient fan • use twin-evaporator • equip unit with anti-sweat heater switch

of refrigerators in existing U.S. housing falls between these two figures; an estimated average figure of 1321 kWh/yr is used later in this report. The actual energy consumption of any unit depends on model, usage and size. It has been claimed that a refrigerator suitable for American consumers could operate at 420 kilowatt-hours a year (Goldstein 1983) but this estimate is much lower than the next lowest estimate. The most efficient American top-freezer 17-18 cubic foot automatic defrost models available now operate at about 900 kWh/yr (ACEEE 1984).

The efficiency of American freezers has also improved markedly--a 55.6 percent increase between 1983 and 1972 (shipment-weighted average; AHAM 1984a). The energy consumption per unit (shipment-weighted average) has dropped from 1460 kWh/yr in 1972 to 813 kWh/yr in 1983 (AHAM 1984a). An estimated average of 1536 kWh/yr for units in place is derived elsewhere in this report. The actual energy consumption of any unit varies enormously depending on model, usage and size.

Efficiency increases in Japanese models since 1972 appear to have been larger and less sporadic than efficiency increases for American models (Goldstein 1984). Several of the measures discussed in subsection 8.1.2 are incorporated in Japanese models. Japanese refrigerators consume less energy than American refrigerators but some of this difference is due to the popularity of much larger appliances in America than in Japan.

The actual energy consumption of refrigerators and freezers is hard to derive from available data for either nation, and even harder to compare between nations. Metered data is extremely scarce; test methods for the manufacturer's labels are of dubious value for predicting actual energy use in the home; methods of comparing efficiency between units of different capacity seem somewhat arbitrary, and different test methods are used in Japan and the United States. Because the energy consumption by these appliances is so significant, it would be particularly helpful if more metered data were available. Because the Japanese appear to lead in the manufacture of cost-effective, low energy-use models (Goldstein 1983, 1984), metered comparisons of American and Japanese models would be very timely.

8.2 CURRENT MARKET SITUATION

Although American refrigerators operate more efficiently than in the past, aggregate energy consumption by this end use has increased. Units used now are larger than in the past; the shipment-weighted average volume/unit increased from 18.16 cubic feet in 1972 to 20.31 cubic feet in 1983. Larger units tend to use more electricity. In addition, households with more than one refrigerator are increasingly common; the 1982 Residential Energy Consumption Survey indicates a saturation in residential housing of 113 percent or an average of 1.13 units per household (U.S. DOE 1984b). The high saturation is partly attributable to households where old refrigerators are left plugged into a garage or basement outlet when a new unit is purchased. In such cases, energy consumption increases sharply when a new unit is purchased, even if the new unit is relatively efficient.

Major U.S. refrigerator and refrigerator/freezer manufacturers are General Electric (GE and Hotpoint brands), Whirlpool, Frigidaire (owned by White Consolidated Industries which includes White-Westinghouse brand) and Amana. General Electric and Whirlpool each have 28-30 percent of the refrigerator market; Frigidaire and White-Westinghouse share about 23 percent of the market; Amana (owned by Raytheon Corporation) has a market share of 10-12 percent. The remainder is accounted for by Admiral and other brands (market shares from Consumers Digest 1984).

The most popular refrigerator is a top-freezer, automatic defrost model with 18 to 20 cubic feet capacity (Consumer Reports 1983). The average Japanese refrigerator, with a volume of 8.12 cubic feet, is less than half this size (Goldstein 1984).

Freezers are more efficient than in the past; they tend to be slightly smaller. The shipment-weighted capacity declined from 29.18 cubic feet in 1972, to 25.28 cubic feet in 1983 (AHAM 1984a). The 1982 Residential Energy Consumption Survey indicates 40 percent saturation of separate freezer units in residential housing (U.S. DOE 1984b).

Whirlpool has 30 percent of the freezer market (Consumers Digest 1984). White-Westinghouse also has a major market share. Other manufacturers include Admiral, G.E./Hotpoint, Amana and Revco (Geller 1983).

No single freezer type dominates either sales or stock (AHAM 1983b; Meier, Wright and Rosenfeld 1983). Only manual defrost models are available for chest freezers (Consumer Guide 1984). Upright models are more convenient for everyday use and take up less space than chest models.

Foreign competition could cause substantial shifts in American refrigerator and refrigerator-freezer markets. The American market will be quite vulnerable if Japanese manufacturers scale the size of their products up and market them in the United States.

8.3 COST EFFECTIVENESS AND MARKET PENETRATION

The cost effectiveness and likely market penetration of even higher efficiency refrigerators and freezers than typical current models are discussed in this section. Payback periods for a more efficient freezer and more efficient refrigerator-freezer are calculated in Section 8.3.1. Two scenarios, one with and one without availability of a competing Japanese product, are calculated for the refrigerator-freezer case. Technical factors that might preclude the use of high efficiency appliances are discussed in Section 8.3.2. Market penetration assumptions are discussed in Section 8.3.3.

A number of assumptions in this part of the analysis could have a large impact on the energy savings results (Section 8.5). The payback period would be much shorter if real electricity prices were assumed to increase in the 1985-2000 period, as is assumed in Geller 1983. The market penetration could be much higher if consumers accept longer payback periods for long-life appliances, such as refrigerators and freezers, than for the product analyzed in the empirical work on which our methodology is based. Furthermore, more efficient refrigerators and freezers could become readily available if international competition becomes rigorous; in such a case the price of efficient products might fall. However, the first two assumptions remain constant throughout this document, and the third involves hypotheses about products that are not commercially available in the United States. However, because alternative product

choices could have such a large impact, a scenario based on best available information regarding Japanese products is discussed in more detail in Section 8.3.1.

It is assumed that efficiency improvements that have already taken place are incorporated into NEPP projections. If this is not the case, then the NEPP projections will overestimate energy use by residential refrigerators and freezers even if the energy saving results of this chapter are applied to the projections.

8.3.1 Cost Effectiveness of More Efficient Product: Three Scenarios

The cost-effectiveness of a more efficient upright freezer and a more efficient top freezer refrigerator are calculated below. Efficiency of the case study units are compared with new units of typically available efficiency for new and retirement markets, and with the efficiency of average refrigerator/freezer stock for retrofit markets. The top-freezer refrigerator model is no longer manufactured, but may still be available in stores and incorporates many of the energy savings features discussed earlier including a twin evaporator system. The reasons that this model is no longer commercially produced is the subject of a recent Pacific Northwest Laboratory Study for the DOE/BERD (Franke et al. 1985). A hypothetical case, of a more efficient top-freezer that the Japanese could possibly offer, is also considered below. Table 8.3 lists the products selected for the payback calculation. The products listed as "conventional" are typical of what is currently available but more efficient than average installed stock.

Case 1: Freezer

Table 8.4 shows the simple payback period for a new and retrofit freezer. Prices of \$470 for the Amana ESU-136 and \$370 for the Whirlpool EV130 FXK are as quoted in Consumers Digest 1984. Annual energy consumption of 725 kWh/year for the Amana and 835 kWh/yr for the Whirlpool models are based on DOE test procedures and AHAM Consumer Selection Guide listings (AHAM 1984b). The average energy consumption of existing freezer stock is calculated as follows:

TABLE 8.3. Products Selected for Payback Analysis

Scenario	Manufacturer/Model	Product
High-Efficiency Freezer	Amana ESU-13C Defrost	13 cubic foot Upright Freezer--Manual
Conventional Freezer	Whirlpool EV130FXK Defrost	13 cubic foot Upright Freezer--Manual
High-Efficiency American Refrigerator	Amana TSC-18E	18 cubic foot Top-Freezer Refrigerator--Automatic Defrost
High-Efficiency Japanese Refrigerator	Hypothetical (a)	18 cubic foot Top-Freezer Refrigerator--Automatic Defrost
Conventional Refrigerator	White-Westinghouse RT188E Automatic Defrost	18 cubic foot Top-Freezer Refrigerator--

(a) Japanese scenario is based on published information of and phone conversations with Natural Resources Defense Council staff who have visited Japan and compared Japanese refrigerator/freezers with the refrigeration/freezers available in the U.S. These experts believe that the Japanese products are more efficiently designed than their U.S. counterparts. They also suggest that the Japanese could offer efficient units suitable for American markets at competitive prices.

TABLE 8.4. Payback Period of More Efficient 13 Cubic Foot Upright Freezer-Manual Defrost

	Capital Cost	Annual Energy Use	Years to Payback
New:			
Amana ESU-13C	\$470	725 kWh/yr	$\frac{\$470 - \$370}{110 \text{ kWh/yr} \times \$0.0718/\text{kWh}} = 12.7 \text{ yr}$
Whirlpool EV130 FXK	\$370	835 kWh/yr	
Accelerated Replacement:			
Amana ESU-13C	\$470	725 kWh/yr	$\frac{\$470}{780 \text{ kWh/yr} \times \$0.0718/\text{kWh}} = 8.4 \text{ yr}$
Average Stock	-0-	1505 kWh/yr	

7 percent electricity use of residential sector attributable to freezers (U.S. DOE 1984c)

$$\begin{aligned} & \times \text{ Total 1984 residential electricity use of 779.60 BkWh (U.S. DOE 1984a)} \\ & \div 90.6 \text{ million households (U.S. DOE 1984a)} \\ & \times 40 \text{ percent saturation (U.S. DOE 1984b)} \\ & = 1505 \text{ kWh/freezer/year.} \end{aligned}$$

As discussed in Chapter 3.0, an electricity price of 7.18¢/kWh, with no real escalation is assumed throughout this analysis.

Case 2: American Refrigerator

Table 8.5 shows the simple payback period for a new and accelerated replacement American refrigerator. Prices are as quoted in Consumer Reports 1983, as is energy use. The Amana TSC-18E is no longer produced but could theoretically be produced again for the same real costs and with the same efficiency. The average energy consumption of existing refrigerator stock is calculated as follows:

$$\begin{aligned} & 17 \text{ percent electricity use of residential sector attributable to refrigerators (U.S. DOE 1984c)} \\ & \times \text{ Total 1984 residential electricity use of 779.6 BkWh (U.S. DOE 1984a)} \\ & \div 90.6 \text{ million households (U.S. DOE 1984a)} \\ & \div 113 \text{ percent saturation (U.S. DOE 1984b)} \\ & = 1294 \text{ kWh/refrigerator/year.} \end{aligned}$$

The long payback period for the accelerated replacement case indicates that few consumers, if any, would replace a serviceable existing refrigerator for energy savings alone.

Case 3: Japanese Refrigerator

Table 8.6 shows the simple payback period for a new and accelerated replacement Japanese refrigerator. The Japanese refrigerator is assumed to be

TABLE 8.5. Payback Period of More Efficient 18 Cubic Foot Top-Freezer Refrigerator--Automatic Defrost: Actual American Model

	<u>Capital Cost</u>	<u>Annual Energy Use</u>	<u>Years to Payback</u>
New:			
Amana TSC-18E	\$851	960 kWh/yr	$\frac{\$851 - \$666}{240 \text{ kWh/yr} \times \$0.0718/\text{kWh}} = 10.7 \text{ yr}$
White-Westinghouse RT188E	\$666	1200 kWh/yr	
Accelerated Replacement:			
Amana TSC-18E	\$851	960 kWh/yr	$\frac{\$851}{334 \text{ kWh/yr} \times \$0.0718/\text{kWh}} = 35.5 \text{ yr}$
Average Refrigerator	-0-	1294 kWh/yr	

45 percent more efficient than the American refrigerator (Goldstein 1984). The Japanese refrigerator is assumed to cost an incremental \$150.00, based on a conversation with staff at the Natural Resource Defense Council. The price and energy consumption for new and stock American refrigerators are as cited in Case 2.

Because of the long payback period, the accelerated replacement case is not considered in the remaining analysis.

8.3.2 Technical Limits

The only technical limit identified is space limitations to insulator thickness. It is possible to indefinitely increase thickness for better thermal resistance. However, an appliance so insulated would not be suitable for limited kitchen spaces. No technical limits are quantified because of the mix of options available for improving appliance efficiencies. All efficiency levels used in the report could be attained by measures which do not have technical limits.

8.3.3 Market Penetration Assumptions

Market penetration rates are assumed to be based on payback period as discussed in Chapter 4.0 (refer to Table 4.1). Based on a payback period of 12.7 years for a new upright freezer, maximum market penetration is assumed to be 5 percent in the new market, which includes normal replacement. Based on lengthy payback periods, there are assumed to be no accelerated replacements of

TABLE 8.6. Payback Period of More Efficient 18 Cubic Foot Top Freezer Refrigerator--Automatic Defrost: Hypothetical Japanese Model

	<u>Capital Cost</u>	<u>Annual Energy Use</u>	<u>Years to Payback</u>
New:			
Japanese	\$816	660 kWh/yr	$\frac{\$150}{540 \text{ kWh/yr} \times \$0.0718/\text{kWh}} = 3.9 \text{ yr}$
White-Westinghouse RT188E	\$666	1200 kWh/yr	
Accelerated Replacement:			
Japanese	\$816	660 kWh/yr	$\frac{\$816}{634 \text{ kWh/yr} \times \$0.0718/\text{kWh}} = 17.9 \text{ yr}$
Average Refrigerator	-0-	1294 kWh/yr	

refrigerators in any of the three scenarios. Market penetration for new markets for American models (which includes "normal" replacement) is assumed to reach 5 percent of sales by 2000, based on a payback period of more than 10 years. Based on the shorter payback period of 3.9 years in the Japanese scenario, the maximum market penetration is assumed to be 45 percent, but because the first sales will not occur until 1990, the penetration in 2000 is assumed to be only 33 percent.

8.4 HOUSING STOCK PROJECTIONS AND MARKET SHARE ESTIMATES

Stock data (existing numbers of refrigerators and freezers, expected rate of growth, and expected number of high-efficiency units) are discussed in this section. Table 8.7 shows market shares and stock data and stock data for more efficient freezers; Table 8.8 shows market shares for more efficient refrigerators based on the American model scenario, and Table 8.9 shows market shares and stock data for more efficient refrigerators based on the Japanese competition scenario. It is assumed that the Japanese would need five years to make the efficient refrigerator/freezer available, so it is further assumed that the first sales would occur in 1990. Housing projections are based on projections supporting the National Energy Policy Plan (DOE 1983a). Market shares for more efficient appliances are estimated according to the method described in Chapter 4.0 using the assumptions discussed in Section 8.3. We have assumed

TABLE 8.7. Annual Market Share Projections--More Efficient Freezers

Year	Annual Replacements of 1984 and Earlier Vintage Freezers ^(a) (10 ⁶ units)	Annual New Freezer Additions ^(b) (10 ⁶ units)	Market Share Efficient in New and Replacement Situations ^(c)	Replacement Efficient Freezer Additions ^(d) (10 ⁶ units)	Annual New Efficient Freezer Additions ^(e) (10 ⁶ units)	Cumulative New and Replacement Efficient Freezer Additions ^(f) (10 ⁶ units)	Cumulative Savings ^(g) (BkWh)
1984	0	0.8	0.010	0.000	0.008	0.008	0.001
1985	1.8	0.7	0.011	0.020	0.007	0.035	0.004
1986	1.8	0.7	0.012	0.022	0.008	0.065	0.007
1987	1.8	0.7	0.013	0.024	0.009	0.097	0.011
1988	1.8	0.7	0.015	0.027	0.010	0.135	0.015
1989	1.8	0.7	0.017	0.031	0.012	0.177	0.019
1990	1.8	0.6	0.020	0.036	0.013	0.226	0.025
1991	1.8	0.6	0.023	0.042	0.015	0.282	0.031
1992	1.8	0.6	0.027	0.049	0.017	0.349	0.038
1993	1.8	0.6	0.031	0.056	0.020	0.425	0.047
1994	1.8	0.6	0.035	0.063	0.022	0.511	0.056
1995	1.8	0.6	0.039	0.071	0.025	0.606	0.067
1996	1.8	0.6	0.043	0.078	0.024	0.708	0.078
1997	1.8	0.6	0.045	0.082	0.025	0.815	0.090
1998	1.8	0.6	0.047	0.085	0.026	0.926	0.102
1999	1.8	0.6	0.049	0.089	0.027	1.043	0.115
2000	1.8	0.6	0.050	0.091	0.028	1.161	0.128

(a) Annual replacement of 1984 vintage appliances based on assumption that 5 percent of existing freezer stock is replaced yearly given average appliance life of 20 years. Freezer stock estimate for 1984 based on DOE, 1984 estimate of 90.6 million residences multiplied by 40 percent, the assumed portion that have freezers.

(b) Annual new freezer additions based on 1984 DOE projections of housing stock additions multiplied by 40 percent.

(c) Based on methodology presented in Chapter 4.0.

(d) Calculated by: (Annual replacements of pre 1984 freezers) x (Market share for efficient freezers).

(e) Calculated by: (Annual New Application freezer additions) x (Market share for efficient freezers).

(f) Calculated by: the sum of current years total freezer additions and the cumulative total for the previous year.

(g) Calculated by: (Cumulative New and Replacement Efficient Freezer additions) x (110 kWh/year).

TABLE 8.8. Annual Market Share Projections--More Efficient Refrigerators Based on Payback Period of American Model

Year	Annual Replacements of 1984 and Earlier Vintage Refrigerators ^(a) (10 ⁶ units)	Annual New Refrigerator Additions ^(b) (10 ⁶ units)	Market Share Efficient in New and Replacement Situations ^(c)	Replacement Efficient Refrigerator Additions ^(d) (10 ⁶ units)	Annual New Efficient Refrigerator Additions ^(e) (10 ⁶ units)	Cumulative New and Replacement Efficient Refrigerator Additions ^(f) (10 ⁶ units)	Cumulative Savings ^(g) (BkWh)
1984	5.1	2.1	0.010	0.051	0.021	0.073	0.017
1985	5.1	1.9	0.011	0.056	0.021	0.150	0.036
1986	5.1	1.9	0.012	0.063	0.024	0.237	0.057
1987	5.1	1.9	0.013	0.067	0.025	0.328	0.079
1988	5.1	1.9	0.015	0.077	0.029	0.434	0.104
1989	5.1	1.9	0.017	0.087	0.033	0.553	0.133
1990	5.1	1.8	0.020	0.102	0.036	0.692	0.166
1991	5.1	1.8	0.023	0.118	0.042	0.851	0.204
1992	5.1	1.8	0.027	0.138	0.049	1.038	0.249
1993	5.1	1.8	0.031	0.159	0.056	1.253	0.301
1994	5.1	1.8	0.035	0.179	0.063	1.496	0.359
1995	5.1	1.8	0.039	0.200	0.071	1.766	0.424
1996	5.1	1.6	0.043	0.220	0.068	2.054	0.493
1997	5.1	1.6	0.045	0.230	0.071	2.355	0.565
1998	5.1	1.6	0.047	0.241	0.074	2.670	0.641
1999	5.1	1.6	0.049	0.251	0.078	2.999	0.720
2000	5.1	1.6	0.050	0.256	0.079	3.334	0.800

(a) Annual replacement of 1984 vintage appliances based on assumption that 5 percent of existing refrigerator stock is replaced yearly given average appliance life of 20 years. Refrigerator stock estimate for 1984 based on DOE, 1984 estimate of 90.6 million residences multiplied by 40 percent, the assumed portion that have refrigerators.

(b) Annual new refrigerator additions based on 1984 DOE projections of housing stock additions multiplied by 40 percent.

(c) Based on methodology presented in Chapter 4.0.

(d) Calculated by: (Annual replacements of pre 1984 refrigerators) x (Market share for efficient refrigerators).

(e) Calculated by: (Annual new Application refrigerator additions) x (Market share for efficient refrigerators).

(f) Calculated by: the sum of current years total refrigerator additions and the cumulative total for the previous year.

(g) Calculated by: (Cumulative New and Replacement Efficient Refrigerator additions) x (240 kWh/year).

TABLE 8.9. Annual Market Share Projections--More Efficient Refrigerators Based on Payback Period of Hypothetical Japanese Model

Year	Annual Replacements of 1984 and Earlier Vintage Refrigerators ^(a) (10 ⁶ units)	Annual New Refrigerator Additions ^(b) (10 ⁶ units)	Market Share Efficient in New and Replacement Situations ^(c)	Replacement Efficient Refrigerator Additions ^(d) (10 ⁶ units)	Annual New Efficient Refrigerator Additions ^(e) (10 ⁶ units)	Cumulative New and Replacement Efficient Refrigerator Additions ^(f) (10 ⁶ units)	Cumulative Savings ^(g) (BkWh)
1984	5.1189	2.147	0.000	0.000	0.000	0.000	0.000
1985	5.1189	1.921	0.000	0.000	0.000	0.000	0.000
1986	5.1189	1.921	0.000	0.000	0.000	0.000	0.000
1987	5.1189	1.921	0.000	0.000	0.000	0.000	0.000
1988	5.1189	1.921	0.000	0.000	0.000	0.000	0.000
1989	5.1189	1.921	0.000	0.000	0.000	0.000	0.000
1990	5.1189	1.808	0.002	0.010	0.004	0.014	0.007
1991	5.1189	1.808	0.005	0.026	0.009	0.048	0.026
1992	5.1189	1.808	0.010	0.051	0.018	0.118	0.064
1993	5.1189	1.808	0.015	0.077	0.027	0.222	0.120
1994	5.1189	1.808	0.025	0.128	0.045	0.395	0.213
1995	5.1189	1.582	0.045	0.230	0.081	0.707	0.382
1996	5.1189	1.582	0.075	0.384	0.119	1.209	0.653
1997	5.1189	1.582	0.125	0.640	0.198	2.047	1.105
1998	5.1189	1.582	0.018	1.921	0.285	3.253	1.757
1999	5.1189	1.582	0.250	1.280	0.396	4.928	2.661
2000	5.1189	1.582	0.330	1.689	0.522	7.139	3.855

- (a) Annual replacement of 1984 vintage appliances based on assumption that 5 percent of existing refrigerator stock is replaced yearly given average appliance life of 20 years. Refrigerator stock estimate for 1984 based on DOE, 1984 estimate of 90.6 million residences multiplied by 40 percent, the assumed portion that have refrigerators.
- (b) Annual new refrigerator additions based on 1984 DOE projections of housing stock additions multiplied by 40 percent.
- (c) Based on methodology presented in Chapter 4.0.
- (d) Calculated by: (Annual replacements of pre 1984 refrigerators) x (Market share for efficient refrigerators).
- (e) Calculated by: (Annual New Application refrigerator additions) x (Market share for efficient refrigerators).
- (f) Calculated by: the sum of current years total refrigerator additions and the cumulative total for the previous year.
- (g) Calculated by: (Cumulative New and Replacement Efficient Refrigerator additions) x (540 kWh/year).

that total market penetration of freezers remains constant at 40 percent and of refrigerators at 113 percent through 2000. The lifetime of all appliances are assumed to be 20 years.

8.5 ENERGY SAVINGS RESULTS

In the last column of each of Tables 8.7, 8.8 and 8.9 displays the expected energy savings projected for the three scenarios. The projections are based on per-unit energy savings and expected market penetration. To use these representative saving and market penetration estimates to obtain an aggregate savings estimate, they are applied to the market share and stock data and forecasts presented in the first six columns of Tables 8.7 through 8.9 that characterize the expected changes over time of the domestic cold storage market. Table 8.10 summarizes the projected energy savings for the three cases for selected years.

Considerable uncertainty is associated with the energy savings results. The payback period might be shorter if international competition pushes product prices down and efficiency up. The extent of such an effect is unknown, in part because current test methods do not permit good international comparison of the energy consumption of refrigerators and freezers. Some apparent efficiency differences may be caused by errors in calibration. Another factor contributing to uncertainty in the results is unknown market penetration for high efficiency appliances. Market penetration might be higher, especially with long life appliances such as refrigerators and freezers. No real escalation rate for the price of electricity is projected; this may be a false assumption

TABLE 8.10. Annual Energy Savings Projections for More Efficient Freezers, More Efficient American Refrigerator Freezers, and Japanese Refrigerator/Freezers--Selected Years (BkWh)

<u>Year</u>	<u>Freezers</u>	<u>American Refrigerator/Freezers</u>	<u>Japanese Refrigerator/Freezers</u>	<u>Total</u>
1985	0	0.04	0	0.04
1990	0.03	0.17	0.01	0.21
1995	0.07	0.42	0.38	0.87
2000	0.13	0.80	3.86	4.79

that results in overestimation of payback periods, underestimation of market penetration and underestimation of energy savings.

8.6 SENSITIVITY OF ANALYSTS TO MARKET PENETRATION ASSUMPTIONS

This section summarizes variations of the scenarios discussed in Sections 8.3, 8.4 and 8.5. The first set of variations assumes the same per-unit energy savings but reduces the assumed maximum market penetration by 50 percent. Additionally, for the American models, maximum market penetration is assumed to occur more slowly than in the base case. (For the Japanese models a five-year lag preceding any market penetration is already built into the base-case estimates.) Thus, in the low market penetration scenario fewer high-efficiency units are installed, and less energy is saved. Section 8.6.1 summarizes the low market penetration scenarios. The second set of variations also assume the same per-unit energy savings. However, the assumed maximum market penetration is doubled, and, except in the Japanese scenario, this market penetration is assumed to occur more quickly than in the base case. Thus, more units are installed, and energy savings are larger. Section 8.6.2 summarizes the high market penetration scenarios.

8.6.1 Low Market Penetration Scenarios

Energy savings projected in the base estimates were not large. With lower market penetration, the savings are even smaller. The low market penetration scenario for high-efficiency freezers is summarized below and is followed by summaries of the low market penetration scenarios for refrigerator-freezers.

In the low market penetration scenario for high-efficiency freezers, the maximum market penetration of freezers bought for new and retirement markets (i.e., for installation in new homes or to replace worn-out stock), is assumed to equal 2.5 percent with only 75 percent of the maximum achieved by the year 2000. As in the base case, no early replacement of working units occurs. Per-unit energy savings for extra-high-efficiency freezers equal 110 kWh per year. Calculations are provided in Table 8.11.

In the low market penetration scenario for American high-efficiency refrigerator-freezers, units bought for new and retirement markets (i.e., for installation in new homes or to replace worn-out stock) experience maximum market penetration of 2.5 percent so slowly that only 75 percent of this maximum is realized by the year 2000. As in the base case, energy savings are insufficient to warrant early replacement of appliance in the "representative" case. The refrigerator-freezers analyzed in this scenario are assumed, on average, to use 240 kWh per year less than other new refrigerator-freezers. Details of the market share and energy savings are provided in Table 8.12.

In the low market penetration scenario for refrigerator-freezers performing at efficiencies typical of Japanese refrigerator-freezers, but scaled upward in size for American markets, maximum market penetration reaches 16 percent by the year 2000. This is half of the market penetration in the base case. The five-year lag (assumed to occur, in the base case, prior to any market penetration) is retained. No early replacement of models for energy savings alone occurs. Per-unit energy savings for models installed instead of other new stock are assumed to equal 540 kWh per year. Details of the market share and energy savings are provided in Table 8.13.

Table 8.14 summarizes energy savings results for the low market penetration scenarios. In general, energy savings results are approximately half of the values estimated in the base-case projections.

8.6.2 High Market Penetration Scenarios

High market penetration scenarios are presented in this section to test the sensitivity of the energy savings results to the market penetration assumptions. Maximum market penetration is doubled from the baseline assumptions. In the freezer and American refrigerator-freezer scenario, maximum market penetration occurs more quickly (by 1995). The Japanese product is assumed to be unavailable until 1990, with maximum market penetration by the year 2000.

In the high penetration scenario for high-efficiency freezers, maximum market penetration for freezers bought for new and retirement markets (i.e., for installation in new homes or to replace worn-out stock), is assumed to equal 10 percent by 1995. Per-unit energy savings assumptions remain 110 kWh

TABLE 8.11. Low Market Penetration Scenario and Annual Savings of Delivered Electricity--More Efficient Freezers

Year	Annual Replacements of 1984 and Earlier Vintage Freezers ^(a) (10 ⁶ units)	Annual New Freezer Additions ^(b) (10 ⁶ units)	Market Share Efficient in New and Replacement Situations ^(c)	Replacement Efficient Freezer Additions ^(d) (10 ⁶ units)	Annual New Efficient Freezer Additions ^(e) (10 ⁶ units)	Cumulative New and Replacement Efficient Freezer Additions ^(f) (10 ⁶ units)	Cumulative Savings ^(g) (BkWh)
1984	0	0.8	0.010	0.000	0.008	0.008	0.001
1985	1.8	0.7	0.010	0.018	0.007	0.033	0.004
1986	1.8	0.7	0.011	0.020	0.007	0.060	0.007
1987	1.8	0.7	0.011	0.020	0.007	0.087	0.010
1988	1.8	0.7	0.011	0.020	0.007	0.115	0.013
1989	1.8	0.7	0.012	0.022	0.008	0.145	0.016
1990	1.8	0.6	0.013	0.024	0.008	0.177	0.019
1991	1.8	0.6	0.013	0.024	0.008	0.208	0.023
1992	1.8	0.6	0.014	0.025	0.009	0.243	0.027
1993	1.8	0.6	0.015	0.027	0.010	0.280	0.031
1994	1.8	0.6	0.016	0.029	0.010	0.319	0.035
1995	1.8	0.6	0.017	0.031	0.011	0.360	0.040
1996	1.8	0.6	0.017	0.031	0.010	0.401	0.044
1997	1.8	0.6	0.018	0.033	0.010	0.443	0.049
1998	1.8	0.6	0.018	0.033	0.010	0.486	0.053
1999	1.8	0.6	0.019	0.034	0.011	0.531	0.058
2000	1.8	0.6	0.019	0.034	0.011	0.576	0.063

(a) Annual replacement of 1984 vintage appliances based on assumption that 5 percent of existing freezer stock is replaced yearly given average appliance life of 20 years. Freezer stock estimate for 1984 based on DOE, 1984 estimate of 90.6 million residences multiplied by 40 percent, the assumed portion that have freezers.

(b) Annual new freezer additions based on 1984 DOE projections of housing stock additions multiplied by 40 percent.

(c) Based on methodology presented in Chapter 4.0.

(d) Calculated by: (Annual replacements of pre 1984 freezers) x (Market share for efficient freezers).

(e) Calculated by: (Annual New Application freezer additions) x (Market share for efficient freezers).

(f) Calculated by: the sum of current years total freezer additions and the cumulative total for the previous year.

(g) Calculated by: (Cumulative New and Replacement Efficient Freezer additions) x (110 kWh/year).

TABLE 8.12. Low Market Penetration Scenario and Annual Savings of Delivered Electricity--More Efficient Refrigerators Based on Payback of American Model

Year	Annual Replacements of 1984 and Earlier Vintage Refrigerators ^(a) (10 ⁶ units)	Annual New Refrigerator Additions ^(b) (10 ⁶ units)	Market Share Efficient in New and Replacement Situations ^(c)	Replacement Efficient Refrigerator Additions ^(d) (10 ⁶ units)	Annual New Efficient Refrigerator Additions ^(e) (10 ⁶ units)	Cumulative New and Replacement Efficient Refrigerator Additions ^(f) (10 ⁶ units)	Cumulative Savings ^(g) (BkWh)
1984	5.1	2.1	0.010	0.051	0.021	0.073	0.017
1985	5.1	1.9	0.010	0.051	0.019	0.143	0.034
1986	5.1	1.9	0.010	0.051	0.019	0.213	0.051
1987	5.1	1.9	0.011	0.056	0.021	0.291	0.070
1988	5.1	1.9	0.011	0.056	0.021	0.368	0.088
1989	5.1	1.9	0.012	0.061	0.023	0.453	0.109
1990	5.1	1.8	0.013	0.067	0.024	0.543	0.130
1991	5.1	1.8	0.014	0.072	0.025	0.640	0.154
1992	5.1	1.8	0.015	0.077	0.027	0.744	0.178
1993	5.1	1.8	0.016	0.082	0.029	0.855	0.205
1994	5.1	1.8	0.016	0.082	0.029	0.965	0.232
1995	5.1	1.8	0.017	0.087	0.031	1.083	0.260
1996	5.1	1.6	0.018	0.092	0.028	1.204	0.289
1997	5.1	1.6	0.018	0.092	0.028	1.324	0.318
1998	5.1	1.6	0.018	0.092	0.028	1.445	0.347
1999	5.1	1.6	0.019	0.097	0.030	1.572	0.377
2000	5.1	1.6	0.019	0.097	0.030	1.700	0.408

(a) Annual replacement of 1984 vintage appliances based on assumption that 5 percent of existing refrigerator stock is replaced yearly given average appliance life of 20 years. Refrigerator stock estimate for 1984 based on DOE, 1984 estimate of 90.6 million residences multiplied by 40 percent, the assumed portion that have refrigerators.

(b) Annual new refrigerator additions based on 1984 DOE projections of housing stock additions multiplied by 40 percent.

(c) Based on methodology presented in Chapter 4.0.

(d) Calculated by: (Annual replacements of pre 1984 refrigerators) x (Market share for efficient refrigerators).

(e) Calculated by: (Annual New Application refrigerator additions) x (Market share for efficient refrigerators).

(f) Calculated by: the sum of current years total refrigerator additions and the cumulative total for the previous year.

(g) Calculated by: (Cumulative New and Replacement Efficient Refrigerator additions) x (240 kWh/year).

TABLE 8.13. Low Market Penetration Scenario and Annual Savings of Delivered Electricity--More Efficient Refrigerators Based on Payback Period of Hypothetical Japanese Model

Year	Annual Replacements of 1984 and Earlier Vintage Refrigerators ^(a) (10 ⁶ units)	Annual New Refrigerator Additions ^(b) (10 ⁶ units)	Market Share Efficient in New and Replacement Situations ^(c)	Replacement Efficient Refrigerator Additions ^(d) (10 ⁶ units)	Annual New Efficient Refrigerator Additions ^(e) (10 ⁶ units)	Cumulative New and Replacement Efficient Refrigerator Additions ^(f) (10 ⁶ units)	Cumulative Savings ^(g) (BkWh)
1984	5.1	2.1	0.000	0.000	0.000	0.000	0.000
1985	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1986	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1987	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1988	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1989	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1990	5.1	1.8	0.002	0.010	0.004	0.014	0.007
1991	5.1	1.8	0.005	0.026	0.009	0.048	0.026
1992	5.1	1.8	0.009	0.046	0.016	0.111	0.060
1993	5.1	1.8	0.014	0.072	0.025	0.208	0.112
1994	5.1	1.8	0.020	0.102	0.036	0.346	0.187
1995	5.1	1.8	0.030	0.154	0.054	0.554	0.299
1996	5.1	1.6	0.050	0.256	0.079	0.889	0.480
1997	5.1	1.6	0.080	0.410	0.127	1.425	0.770
1998	5.1	1.6	0.110	0.563	0.174	2.162	1.168
1999	5.1	1.6	0.140	0.717	0.221	3.100	1.674
2000	5.1	1.6	0.160	0.819	0.253	4.173	2.253

- (a) Annual replacement of 1984 vintage appliances based on assumption that 5 percent of existing refrigerator stock is replaced yearly given average appliance life of 20 years. Refrigerator stock estimate for 1984 based on DOE, 1984 estimate of 90.6 million residences multiplied by 40 percent, the assumed portion that have refrigerators.
- (b) Annual new refrigerator additions based on 1984 DOE projections of housing stock additions multiplied by 40 percent.
- (c) Based on methodology presented in Chapter 4.0.
- (d) Calculated by: (Annual replacements of pre 1984 refrigerators) x (Market share for efficient refrigerators).
- (e) Calculated by: (Annual New Application refrigerator additions) x (Market share for efficient refrigerators).
- (f) Calculated by: the sum of current years total refrigerator additions and the cumulative total for the previous year.
- (g) Calculated by: (Cumulative New and Replacement Efficient Refrigerator additions) x (540 kWh/year).

TABLE 8.14. Low Market Penetration Scenario: Energy Savings Projections for High-Efficiency Freezers and Refrigerator-Freezers

<u>Year</u>	<u>Freezer</u>	(BkWh) <u>Refrigerator-Freezer</u>		<u>Total</u>
		<u>American Model</u>	<u>Japanese Model</u>	
1985	0	0.03	0	0.03
1990	0.02	0.13	0.01	0.16
1995	0.04	0.26	0.30	0.60
2000	0.06	0.41	2.25	2.72

per year. As in the base case, no early replacement of working units is assumed to occur. Details of the market share calculations are provided in Table 8.15.

In the high market penetration scenario for American high-efficiency refrigerator-freezers, units bought for new and retirement markets experience maximum market penetration of 10 percent by 1995. No early replacement of working units occurs, as in the base case, for energy savings alone. The value for per-unit electricity savings is 240 kWh per year. Table 8.16 provides details of the market share calculations and energy savings.

In the high market penetration scenario for refrigerator-freezers performing at efficiencies typical of Japanese refrigerator-freezers, but scaled upward in size for American markets, maximum market penetration reaches 66 percent by the year 2000. No early replacement of existing stock for energy savings alone occurs. On average, per-unit energy savings for these highly efficient models are assumed to equal 540 kWh per year. Details of the market share and energy savings calculations are provided in Table 8.17.

Table 8.18 summarizes energy savings results for the high market scenarios for more efficient freezers and refrigerator-freezers. Doubling the maximum market penetration and assuming more rapid market penetration more than doubled the energy savings results.

TABLE 8.15. High Market Penetration Scenario and Annual Savings of Delivered Electricity--More Efficient Freezers

Year	Annual Replacements of 1984 and Earlier Vintage Freezers ^(a) (10 ⁶ units)	Annual New Freezer Additions ^(b) (10 ⁶ units)	Market Share Efficient in New and Replacement Situations ^(c)	Replacement Efficient Freezer Additions ^(d) (10 ⁶ units)	Annual New Efficient Freezer Additions ^(e) (10 ⁶ units)	Cumulative New and Replacement Efficient Freezer Additions ^(f) (10 ⁶ units)	Cumulative Savings ^(g) (BkWh)
1984	0	0.8	0.010	0.000	0.008	0.008	0.001
1985	1.8	0.7	0.012	0.022	0.008	0.038	0.004
1986	1.8	0.7	0.016	0.029	0.011	0.077	0.009
1987	1.8	0.7	0.025	0.045	0.017	0.140	0.015
1988	1.8	0.7	0.035	0.063	0.024	0.227	0.025
1989	1.8	0.7	0.045	0.082	0.031	0.339	0.037
1990	1.8	0.6	0.060	0.109	0.038	0.486	0.053
1991	1.8	0.6	0.075	0.136	0.048	0.670	0.074
1992	1.8	0.6	0.085	0.154	0.054	0.878	0.097
1993	1.8	0.6	0.092	0.167	0.059	1.104	0.121
1994	1.8	0.6	0.097	0.176	0.062	1.342	0.148
1995	1.8	0.6	0.100	0.181	0.064	1.587	0.175
1996	1.8	0.6	0.100	0.181	0.056	1.824	0.201
1997	1.8	0.6	0.100	0.181	0.056	2.062	0.227
1998	1.8	0.6	0.100	0.181	0.056	2.299	0.253
1999	1.8	0.6	0.100	0.181	0.056	2.536	0.279
2000	1.8	0.6	0.100	0.181	0.056	2.773	0.305

(a) Annual replacement of 1984 vintage appliances based on assumption that 5 percent of existing freezer stock is replaced yearly given average appliance life of 20 years. Freezer stock estimate for 1984 based on DOE, 1984 estimate of 90.6 million residences multiplied by 40 percent, the assumed portion that have freezers.

(b) Annual new freezer additions based on 1984 DOE projections of housing stock additions multiplied by 40 percent.

(c) Based on methodology presented in Chapter 4.0.

(d) Calculated by: (Annual replacements of pre 1984 freezers) x (Market share for efficient freezers).

(e) Calculated by: (Annual New Application freezer additions) x (Market share for efficient freezers).

(f) Calculated by: the sum of current years total freezer additions and the cumulative total for the previous year.

(g) Calculated by: (Cumulative New and Replacement Efficient Freezer additions) x (110 kWh/year).

TABLE 8.16. High Market Penetration Scenario and Annual Savings and Delivered Electricity--More Efficient Refrigerators Based on Payback Period of American Model

Year	Annual Replacements of 1984 and Earlier Vintage Refrigerators ^(a) (10 ⁶ units)	Annual New Refrigerator Additions ^(b) (10 ⁶ units)	Market Share Efficient in New and Replacement Situations ^(c)	Replacement Efficient Refrigerator Additions ^(d) (10 ⁶ units)	Annual New Efficient Refrigerator Additions ^(e) (10 ⁶ units)	Cumulative New and Replacement Efficient Refrigerator Additions ^(f) (10 ⁶ units)	Cumulative Savings ^(g) (BkWh)
1984	5.1	2.1	0.010	0.051	0.021	0.073	0.017
1985	5.1	1.9	0.015	0.077	0.029	0.178	0.043
1986	5.1	1.9	0.022	0.113	0.042	0.333	0.080
1987	5.1	1.9	0.032	0.164	0.061	0.558	0.134
1988	5.1	1.9	0.045	0.230	0.086	0.875	0.210
1989	5.1	1.9	0.058	0.297	0.111	1.284	0.308
1990	5.1	1.8	0.070	0.358	0.127	1.768	0.424
1991	5.1	1.8	0.080	0.410	0.145	2.323	0.557
1992	5.1	1.8	0.087	0.445	0.157	2.925	0.702
1993	5.1	1.8	0.092	0.471	0.166	3.562	0.855
1994	5.1	1.8	0.097	0.497	0.175	4.234	1.016
1995	5.1	1.8	0.100	0.512	0.181	4.927	1.182
1996	5.1	1.6	0.100	0.512	0.158	5.597	1.343
1997	5.1	1.6	0.100	0.512	0.158	6.267	1.504
1998	5.1	1.6	0.100	0.512	0.158	6.937	1.665
1999	5.1	1.6	0.100	0.512	0.158	7.607	1.826
2000	5.1	1.6	0.100	0.512	0.158	8.278	1.987

(a) Annual replacement of 1984 vintage appliances based on assumption that 5 percent of existing refrigerator stock is replaced yearly given average appliance life of 20 years. Refrigerator stock estimate for 1984 based on DOE, 1984 estimate of 90.6 million residences multiplied by 40 percent, the assumed portion that have refrigerators.

(b) Annual new refrigerator additions based on 1984 DOE projections of housing stock additions multiplied by 40 percent.

(c) Based on methodology presented in Chapter 4.0.

(d) Calculated by: (Annual replacements of pre 1984 refrigerators) x (Market share for efficient refrigerators).

(e) Calculated by: (Annual New Application refrigerator additions) x (Market share for efficient refrigerators).

(f) Calculated by: the sum of current years total refrigerator additions and the cumulative total for the previous year.

(g) Calculated by: (Cumulative New and Replacement Efficient Refrigerator additions) x (240 kWh/year).

TABLE 8.17. High Market Penetration Scenario and Annual Savings and Delivered Electricity--More Efficient Refrigerators Based on Payback of Hypothetical Japanese Model

Year	Annual Replacements of 1984 and Earlier Vintage Refrigerators ^(a) (10 ⁶ units)	Annual New Refrigerator Additions ^(b) (10 ⁶ units)	Market Share Efficient in New and Replacement Situations ^(c)	Replacement Efficient Refrigerator Additions ^(d) (10 ⁶ units)	Annual New Efficient Refrigerator Additions ^(e) (10 ⁶ units)	Cumulative New and Replacement Efficient Refrigerator Additions ^(f) (10 ⁶ units)	Cumulative Savings ^(g) (BkWh)
1984	5.1	2.1	0.000	0.000	0.000	0.000	0.000
1985	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1986	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1987	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1988	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1989	5.1	1.9	0.000	0.000	0.000	0.000	0.000
1990	5.1	1.8	0.002	0.010	0.004	0.014	0.007
1991	5.1	1.8	0.010	0.051	0.018	0.083	0.045
1992	5.1	1.8	0.020	0.102	0.036	0.222	0.120
1993	5.1	1.8	0.050	0.256	0.090	0.568	0.307
1994	5.1	1.8	0.090	0.461	0.163	1.191	0.643
1995	5.1	1.8	0.150	0.768	0.271	2.230	1.204
1996	5.1	1.6	0.230	1.177	0.364	3.772	2.037
1997	5.1	1.6	0.320	1.638	0.506	5.916	3.195
1998	5.1	1.6	0.440	2.252	0.696	8.864	4.787
1999	5.1	1.6	0.560	2.867	0.886	12.617	6.813
2000	5.1	1.6	0.660	3.378	1.044	17.039	9.201

(a) Annual replacement of 1984 vintage appliances based on assumption that 5 percent of existing refrigerator stock is replaced yearly given average appliance life of 20 years. Refrigerator stock estimate for 1984 based on DOE, 1984 estimate of 90.6 million residences multiplied by 40 percent, the assumed portion that have refrigerators.

(b) Annual new refrigerator additions based on 1984 DOE projections of housing stock additions multiplied by 40 percent.

(c) Based on methodology presented in Chapter 4.0.

(d) Calculated by: (Annual replacements of pre 1984 refrigerators) x (Market share for efficient refrigerators).

(e) Calculated by: (Annual New Application refrigerator additions) x (Market share for efficient refrigerators).

(f) Calculated by: the sum of current years total refrigerator additions and the cumulative total for the previous year.

(g) Calculated by: (Cumulative New and Replacement Efficient Refrigerator additions) x (540 kWh/year).

TABLE 8.18. High Market Penetration Scenario: Energy Savings Projections for High-Efficiency Freezers and Refrigerator-Freezers

<u>Year</u>	<u>Freezer</u>	(BkWh) <u>Refrigerator-Freezer</u>		<u>Total</u>
		<u>American Model</u>	<u>Japanese Model</u>	
1985	0	0.04	0	0.04
1990	0.05	0.42	0.01	0.48
1995	0.18	1.18	1.20	2.56
2000	0.31	1.99	9.20	11.50

8.7 COMPARATIVE COSTS: NEW GENERATING CAPACITY VERSUS HIGH-EFFICIENCY REFRIGERATORS AND FREEZERS

Costs per conserved kWh for the representative case studies of Section 8.3 are calculated in Table 8.19. In these case studies, costs per conserved kWh for the most efficient American models equal 8 to 9¢/kWh when compared with an average new American model. The cost is slightly higher than the average cost of new generation cited in Table 4.3 of 5.8¢/kWh. The calculated costs of conserved energy are extremely sensitive to the values assumed for the costs and potential magnitude of further efficiency improvements. The scenario constructed from hypotheses about possible development of refrigerator-freezers as efficient as typical Japanese models, but scaled upward in the size for the American consumer, demonstrates this sensitivity. In the scenario that uses such assumptions, the cost of conserved energy is only 2.8¢/kWh.

TABLE 8.19. Cost per kWh Calculation for More Efficient Freezers and Refrigerator-Freezers

Technology	Incremental Capital Cost (\$ 1984)	Levelized ^(d) Capital Cost (\$/yr)	Annual Energy Savings (kWh/yr)	Cost ^(e) per kWh (cents kWh)
Freezer-- Most Efficient Versus Average New Model	100 ^(a)	10	110 ^(a)	9.1
Refrigerator-Freezer-- American Scenario Most Efficient Versus Average New Model	185 ^(b)	19	240 ^(b)	7.9
New Refrigerator- Freezer--Japanese Scenario	150 ^(c)	15	540 ^(c)	2.8

(a) Refer to Table 8.4.

(b) Refer to Table 8.5.

(c) Refer to Table 8.6.

(d) Refer to Equation 4.11. Assumes 20-year lifetime and 8 percent rate of interest compounded annually.

(e) Calculated on delivered energy basis by: $(\text{Levelized Capital Cost}) \div (\text{annual Energy Savings}) = \text{cost per kWh}$.

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9.0. GLAZING AND OTHER WINDOW TECHNOLOGIES

This chapter analyzes the electricity savings potential of selected window energy conservation technologies in commercial buildings. Section 9.1 provides technical background for conventional windows and new designs. Section 9.2 describes the market situation, in terms of product availability, vendors, popularity and increasing acceptance. In Section 9.3.1, costs and energy savings experienced in several building redesigns are presented. Assumptions for cost and energy savings to be used in the nationally aggregated analysis are chosen. Technical limits are discussed in Section 9.3.2; market penetration assumptions are identified in Section 9.3.3. Population estimates, i.e., commercial building space and projected market shares for the energy-conserving window applications, are shown in Section 9.4. Aggregate energy savings results, conclusions, and a summary of assumptions are presented in Section 9.5. Section 9.6 presents an analysis of the sensitivity of the energy savings results to changes in the market/penetration scenarios. Section 9.7 compares the estimated cost per kWh saved with the estimated cost per kWh of new electrical generating capacity.

9.1 TECHNICAL BACKGROUND

Windows are integral to building design and affect building energy consumption in a number of ways. When placed without consideration for the amount of sunlight they admit, windows usually drain energy from a building. On the other hand, carefully designed windows can diminish cooling loads, supplement or replace other heating, lighting and ventilation equipment, and increase occupant comfort by providing a thermally comfortable and aesthetically pleasing environment.

Sun shining through an average clear window can warm a room. This heat gain may significantly add to summer cooling loads or, in winter, may supplement other heating. On a clear day in June, hourly solar heat gain through standard vertical double glazing can range from 440 British thermal units per square foot (36 degree North latitude, windows oriented toward the north) to 1200 British thermal units per square foot (56 degree North latitude, windows

oriented toward the east or west) (Mazria 1979). In general, summer heat gain is largest through east- and west-facing glass, but heat gain through unshaded south-facing glass may also be significant.

New window products can reduce cooling loads by controlling solar gain. Some glass products and special coatings selectively reflect thermal radiation back to its source: to the outdoors in summer and to the indoors in winter. The effectiveness of these products is measured by their shading coefficient: the shading coefficient measures the ratio of solar gain through a glazing system to solar gain through a pane of double strength float glass in the same set of conditions. A window that has good ability to reject solar heat has a low shading coefficient. Cooling loads can also be diminished if exterior blinds reflect solar energy before it penetrates the room to be cooled. In addition, the extent of summer solar gain can be controlled if only moderate glass areas face east and west.

Lighting in commercial buildings uses significant amounts of electricity during daytime hours. Conventionally, light is admitted indiscriminately through windows and may be of uneven quality or accompanied by glare. Lighting hardware at the building's perimeter is often linked to lighting hardware in the building's interior, so it is not technically feasible to turn out lights only on the building's perimeter in order to save electricity. This may lead to lights being on in areas where they are not needed.

Daylighting, i.e., the use of solar illumination to reduce electrical lighting requirements, has been used with good results in several commercial buildings (Elliott 1984; Selkowitz et al. 1983; Pansky et al. 1984). This relatively new concept is most likely to succeed when coordinated with architectural plans, other illumination systems, and interior design. Daylighting may supplement or replace other light at perimeter areas if the daylighting system is integrated with other lighting hardware.

As the weakest component of a building's thermal envelope windows significantly affect heat loss in cool weather and at night. Relative to other building materials, windows have low resistance to heat loss (R) and high

coefficients of heat transfer ($U = 1/R$). If installation is similar, in terms of size, caulking, fit and other factors, a window material with a high U value loses more heat than a window material with a lower U value.

Heating requirements are reduced when windows are made more resistant to heat loss. Improved thermal resistance may also decrease cooling loads, but the effect is usually insignificant in comparison to cooling savings from reduced solar gain. Wooden-framed windows generally have lower U values than aluminum-framed windows. It appears to be less expensive, in general, to choose aluminum over wooden windows, but for comparable thermal performance it is necessary to equip them with some type of enclosed "thermal break" that prevents rapid heat conduction to the outdoors. Double or triple glazings, various plastic products, and insulation products are other measures available to reduce heat loss through windows. Heating energy requirements can also be reduced by reductions in window surface area.

The product selected for payback analysis for new commercial buildings saves energy primarily by reducing cooling loads. However, it also has better insulating ability than ordinary glass. Marketed by Southwall Technologies under the trade name Heat Mirror™, it transmits solar radiation at desirable wavelengths (i.e., visible light) but reflects it at unwanted wavelengths (i.e., near infrared that would otherwise contribute to heat gain). Three climate-specific variations of the basic product are available.

It should be emphasized that several competing window energy conservation technologies are available. Plastic films, other glazings and exterior shading devices are available that also decrease heating requirements, cooling loads, or both. Films and glazings are generally product substitutes; exterior blinds and shading devices may complement other window technologies. The product selected for payback analysis for retrofit applications is a double-pane thermal window with solar film.

Technical performance characteristics of Heat Mirror™ are compared with those of other windows in Table 9.1. The table shows that solar heat gain may be reduced by as much as 73 percent if a Heat Mirror™ product is used instead of clear double glazing. Winter heat loss by conduction through windows may be reduced by 62 percent.

TABLE 9.1. Technical Performance of Conventional and Energy-Conserving Windows

<u>Glass Type/Thickness/Makeup</u>	<u>Shading Coefficient</u>	<u>Relative Heat Gain^(a) (Btu/hr/ft²)</u>	<u>Summer U Value (Btu/hr/ft²/ F)</u>	<u>Winter U Value (Btu/hr/ft²/ F)</u>
Clear Glass: 1/8 in. thick				
Single-glazed, no air space	1.00	215	1.04	1.16
Double-glazed, 1/4 in. air space	0.89	187	0.61	0.58
Triple-glazed, two 1/4 in. air spaces	0.85	176	0.46	0.39
Pella Windows				
Double Glazing/Solarcool	0.59	N/A	N/A	N/A
Insulating Glass/Casement, 4860 fixed (5/8 in.), total unit	N/A	N/A	N/A	0.52
Air-Flow Window by Ekono	N/A	N/A	N/A	0.06
Heat Mirror[™] Products				
Clear	0.39-0.70	82-144	0.23-0.36	0.22-0.32
Bronze Exterior	0.27-0.42	66-88	0.23-0.36	0.22-0.32
Gray Exterior	0.23-0.36	50-76	0.23-0.36	0.22-0.32
Blue-Green Exterior	0.28-0.46	60-95	0.23-0.36	0.22-0.32

(a) Assumes indoor/outdoor temperature difference of 14 F, and ASHRAE solar heat (radiant) gain factor of 200 Btu per hour per square foot (Btu/hr/ft²).

[™]Registered trademark of the Southwall Corporation.

N/A Data not available.

Source: Literature from SIGMA and window manufacturers.

Unfortunately, it is impossible to generalize what fraction of building energy requirements is attributable to windows. Each building must be analyzed separately, with architectural information as well as detailed knowledge of weather, geographic location and HVAC systems. In theory, a window load study could be conducted on a prototypical commercial building, but such a simulation model is outside the scope of this study. In practice, it is found in most cases that careful window design and the use of window energy-conservation technologies saves electricity during heating season and especially during cooling season.

9.2 CURRENT MARKET SITUATION

Telephone interviews with dealers and manufacturers and a literature review confirm marked progress in both the technical sophistication and market acceptance of energy-efficient windows. Numerous vendors supply a variety of

energy efficient window products. Most of these products are suitable for retrofit applications but are even more effective if incorporated into original building design. The market is characterized by rapid change as research leads to practical high-efficiency products.

The popularity of energy-efficient window products is increasing. According to several manufacturers and dealers, high-performance windows are a high growth market.^(a) Heat Mirror™ windows will probably experience increasing market penetration (Aitken 1984; manufacturer literature).

The market situation in a location with high heating bills may be completely dissimilar to the market situation in a milder climate. This is because building design requirements and appropriate window technologies are extremely region-specific. State building codes, whose comprehensiveness and initial date of adoption vary greatly by state, also affect market acceptance. Despite the rapid innovation in window markets and increasing market acceptance perceived in the present study, therefore, more extensive, region-specific research would be required to characterize these markets with greater certainty.

9.3 COST EFFECTIVENESS, TECHNICAL LIMITS AND MARKET PENETRATION

This section appraises the cost effectiveness of the use of more efficient window technologies in the commercial sector, as typified by Heat Mirror™ for new buildings and solar film combined with thermal windows for existing buildings. Values for representative payback and energy savings are chosen in Section 9.3.1. In Section 9.3.2, technical limits are discussed. Section 9.3.3 presents projections for potential market penetration of these energy-efficient windows in commercial buildings.

(a) Conversations with Leonard Brunette, Architectural Products Manager, Belknap Industries; Wayne Shallenberer, owner, Bliss Windows; Bill Proesch, Marketing Department, Anderson Window Corporation, et al.

9.3.1 Payback Periods and Representative Energy Saving

This section describes the values used in the analysis for representative payback periods and energy savings. Costs and energy savings for new commercial buildings with Heat Mirror™ windows are presented. The cost-effectiveness of retrofitting a commercial building with thermal windows and solar film is also described.

Heat Mirror™ on a New Commercial Building. Table 9.2 summarizes the cost impacts of using Heat Mirror™ on a new commercial building in place of tinted double glass. The costs are the results of a case study published by the manufacturer in which a computer simulates building energy performance given square feet of floor space, square feet of glass, building location, window U-values and shading coefficients, costs of windows, costs of energy and other physical and economic data. The results are case-specific, but in general Heat Mirror™ windows pay for themselves rapidly.^(a)

In the case study, the Heat Mirror™ windows increased overall building energy performance by so much that the building's design load was substantially reduced. As a result, the HVAC system for the Heat Mirror™-equipped building is smaller than the HVAC system for the building with tinted double glass. The down-sizing saves more on first building costs than the incremental cost of equipping the building with Heat Mirror™ instead of tinted double glass. Thus, in the case study, the use of Heat Mirror™ actually reduces first costs and the payback is immediate.

First costs of the HVAC system are further reduced, in the case study, by the elimination of perimeter heaters and cooling vents. This equipment is conventionally installed near windows to eliminate drafts in winter and overheated spots in summer. These problems are eliminated with the Heat Mirror™ system so that the expensive perimeter heaters and cooling vents may be omitted.

Thermal Windows and Solar Film for a Commercial Building Retrofit. The retrofit case study is of a clothing store in Evanston, Illinois that is being converted to office space. The building will simultaneously be retrofit with

(a) Leonard Brunette, Architectural Products Manager, Belknap Industries, personal communication.

TABLE 9.2. Cost Effectiveness of Heat Mirror™55 Equipped Double Glass Versus Tinted Double Glass on a New Two-Floor Commercial Building of 21,000 square feet in Dallas, Texas.
CALPAS computer simulation; 1,760 square feet of windows.

9.7	Type of Glass	U Value	Shading Coefficient	First Costs			First Cost Increase (Decrease)	Annual Costs for Heating and A/C ^(a)	Annual Cost Savings (percent)	Payback Period
				Draft Heater	A/C System	Total				
	Double Glass, Tinted	0.58	0.54	\$6,160	\$47,498	\$53,658	(\$13,622)	\$6,539	15.7	immediate
	Double Glass, Equipped with Heat Mirror™ 55	0.22	0.39	-0-	\$40,036	\$40,036		\$5,511		

(a) Price of energy not cited in original.
Source: Southwall Technologies 1984.

energy-efficient windows. Table 9.3 compares relevant energy parameters between the original and retrofit building and shows expected initial costs, annual savings and payback. According to a representative of Scandinavian Insulating Glass of North America (SIGNA), which is supplying the basic thermal window system for the retrofit, similar projects have paid for themselves in as little time as 14 months (Galvin 1984). Solar film, made by Deposition Technology, Inc., is also part of the retrofit package. Expected payback for this case study is 3.5 years (Galvin 1984).

Representative Energy Savings. Window conservation technologies impact energy requirements for space heating, air conditioning, ventilation, and lighting. Insufficient data are available from the case studies to evaluate energy-savings potential by these end uses. Unfortunately, such subdivision is necessary for consistency with other parts of the analysis.

The approach taken in order to address this problem of insufficient data is to base the energy-savings assumptions on a larger data set available from other commercial buildings research. Table 9.4 presents energy savings, by end use, for several cases of commercial buildings redesign. Each element of this table represents the percentage energy savings for the end-use listed in the

TABLE 9.3. Cost Effectiveness for Retrofitting a 6-Story Commercial Building of 40,000 sq ft in Evanston, Illinois with Solar Film and Thermal Windows for 1,233 sq ft of Windows

<u>Building</u>	<u>Type of Glass</u>	<u>U Value</u>	<u>First Cost, Inclusive</u>	<u>Expected Annual Heating and Cooling Cost Savings^(a)</u>	<u>Payback</u>
Original	Single-Pane	1.13	--	--	
Retrofit	Double-Pane Thermal with Solar Film	0.36	\$13,000	\$2,900-\$3,700	3.5 yr

(a) Assumed energy costs not cited in original.
Source: Galvin 1984

TABLE 9.4. Potential Commercial Building Energy Savings Due to Assorted Building Conservation and Redesign Measures

End Use	Electricity Savings from Building Energy Conservation Measures, Retrofit ^(a) (percent)	Electricity Savings from Building Energy Conservation Measures No Daylighting, New Building ^(b) (percent)	Electricity Savings from Building Energy Conservation Measures, Including Daylighting, New Building ^(b) (percent)
Total	Unknown	15.4	22.0
Space Heat	25.0	15.6	19.4
Cooling Energy	19.8	13.7	21.5
Ventilation	13.0	5.6	5.6
Lighting	28.9	25.5	36.5

(a) Schultz, California Energy Commission 1984.

(b) Pacific Northwest Laboratory 1983, average improvements over all climate areas for base case.

first column associated with a particular set of building conservation measures (listed in the column headings). The retrofit case is based on data collected by the California Energy Commission in extensive audits (Schultz 1984).

Depending on end use and not including ventilation, average estimated potential for reductions in electricity use, through the application of various building conservation measures, ranges from 20 to 29 percent. The new building case is based on computer simulations of the response of a medium office building to various redesign measures (Pacific Northwest Laboratory 1983). The measures considered include both window and non-window technologies. Depending on end use, and not including ventilation, the estimates range from 14 to 26 percent energy savings (without daylighting) to 19 to 37 percent energy savings (with daylighting).

The larger data set summarized in Table 9.4 is not ideal because contributions to overall energy savings by individual energy conservation measures are not provided. The redesigns included such conservation measures as increases

in HVAC efficiencies as well as improvements in window performance. Thus, the energy savings estimates in Table 9.4 overstate the potential energy savings from window conservation measures alone.

Window conservation measures, such as selective glass orientation, thermal envelope improvements and solar control, are usually significant contributors to energy savings in commercial building redesigns (Deringer, Misuriello, et al. 1983). Referring to Table 9.4, it will be assumed that in this analysis window conservation measures accounted for three-fourths (75 percent) of the building redesign cooling and heating savings, for none of the ventilation savings, and for all of the lighting savings (in the new building case where daylighting was explicitly modeled).

The combined estimate of energy savings potential from improvements to windows are summarized in Table 9.5. Using the estimates of potential percent reductions in energy use through adoptions of window improvements, it is possible to derive the reductions in annual kWh consumption per square foot of commercial floorspace based on DOE and EIA end use estimates. For retrofit commercial buildings, annual electricity savings are 2.63 kWh per square foot for buildings using electricity for both heating and cooling, and are 1.63 kWh per square foot for buildings using electricity for cooling only. For new commercial buildings, annual electricity savings are 3.19 kWh per square foot for buildings using electricity for both heating and cooling, and are 2.42 kWh per square foot for buildings using electricity for cooling only.

This is clearly a construct chosen for purposes of developing a scenario that might indicate the order of magnitude of potential energy savings from window energy conservation technologies. It might be noted, however, that the energy savings in the case study of Heat Mirror™ on a new commercial building is roughly consistent with this construction. Heat Mirror™ reduced annual energy costs by 15.7 percent in the case study of a commercial building in Dallas, Texas. This percentage energy savings is higher than the value of 14.4 percent chosen to represent the energy-savings potential for an electrically heated and cooled commercial building, but is approximately equal to

TABLE 9.5. Potential Reductions in Annual Energy Use per Square Foot
for Commercial Buildings Due to Window Redesign

(kWh per square foot)

End Use	Base Case Electricity Use per Square Foot ^(a) kWh	Buildings Electrically Heated and Cooled				Buildings Electrically Cooled Only			
		Percent Decrease In Energy Use In Retrofit Applications	Decrease In Energy Use In Retrofit Applications (kWh/sq ft)	Percent Decrease In Energy Use In New Applications	Decrease In Energy Use In New Applications (kWh/sq ft)	Percent Decrease In Energy Use In Retrofit Applications	Decrease In Energy Use In Retrofit Applications (kWh/sq ft)	Percent Decrease In Energy Use In New Applications	Decrease In Energy Use In New Applications (kWh/sq ft)
Space Heat	5.29	19.0	1.00	14.6	.77	--	--	--	--
Cooling	10.97	14.9	1.63	16.1	1.77	14.9	1.63	16.1	1.77
Lighting	5.94	0	0	11.0	0.65	0	0	11.0	0.65
Total ^(b)	22.22		2.63		3.19		1.63		2.42

(a) Derived from EIA 1984 and DOE 1984.

(b) Electricity end uses potentially affected by window technologies.

the estimated cooling savings of 16.1 percent. This is probably the more appropriate comparison since a commercial building in Dallas would be dominated by cooling loads.

9.3.2 Technical Limits

Not all structures are suitable for window redesign. For new buildings, some construction occurs in congested areas where existing structures block the sun. In addition, architects may be limited to specific building orientations or window locations and size by the land parcel, zoning laws or interior design specifications.

In addition, some redesign attempts may fail, with energy consumption increasing over the base case instead of declining. There was a 6 percent failure rate in a recent study involving the redesign of more than one hundred commercial new buildings (Deringer, Misuriello, et al. 1983). A technical limit value of 25 percent is chosen to represent these technical limits to energy savings through window redesign on new commercial buildings. This means that 25 percent of newly constructed commercial buildings are assumed to be unable to use window energy conservation measures to improve building energy performance.

For retrofits, limitations similar to those on new buildings may be encountered. The failure rate may be even higher; a DOE survey of retrofits of over 200 existing commercial buildings discovered a failure rate of about 10 percent (Deringer, Misuriello et al. 1983). In addition, existing windows may be of nonstandard sizes so that their replacement could require prohibitively expensive customization. Finally, it may not be feasible to shut down a utilized commercial building for long enough duration to perform a retrofit. A technical limit value of 40 percent is chosen to represent these technical limits to energy savings through window retrofits on existing commercial buildings. This means that 40 percent of existing commercial buildings are assumed to be unable to use window energy-conservation measures to improve building energy performance.

9.3.3 Market Penetration Assumptions

Table 9.6 summarizes the first costs and payback periods calculated in Section 9.3.1. Based on these economic data and on Table 4.2, estimated maximum potential market penetration of the Heat Mirror™ conservation technology on new commercial buildings is 75 percent. The purpose of this exercise is to construct an energy conservation scenario; it is not intended to suggest any most likely case regarding the market share of Heat Mirror™ products versus market shares of competing window products. The first row of Table 4.2 is assumed to apply to the retrofit case, resulting in an assumed maximum potential market penetration for the retrofit technology of 50 percent.

Table 9.7 summarizes the values for maximum potential market share, energy savings and technical limits to be used in the remainder of the analysis for the most likely case estimates.

9.4 COMMERCIAL BUILDING STOCK AND MARKET SHARE PROJECTIONS

In this section, projections of future additions to total national commercial floorspace (DOE 1984a) are employed to estimate the amount of commercial building space likely to use energy-conserving window technologies by the years 1990, 1995, and 2000. Table 9.8 shows details of the population projections for more energy efficient windows on buildings that are electrically cooled and electrically heated. Table 9.9 shows details of the population projections for energy-efficient windows on buildings that are electrically cooled only. The

TABLE 9.6 First Costs and Paybacks for Heat Mirror™ on New Commercial Buildings, and for Thermal Windows and Solar Film on an Existing Commercial Building^(a)

<u>Measure</u>	<u>First Cost Increase</u>	<u>Payback Period</u>
Heat Mirror™, New Building	0	Immediate
Thermal Windows or Solar Film, Retrofit	N/A ^(b)	3.5 yr

(a) Assumptions stated in Section 9.3.1.

(b) First cost increase for retrofit case is not applicable to estimation of market share with Table 4.2.

TABLE 9.7. Summary of Values Assumed for Market Share, Energy Savings and Technical Limits (Percent)

<u>Value</u>	<u>New Building, Heat Mirror</u>	<u>Retrofit Thermal Windows and Solar Film</u>
Technical Limit	25	40
Market Share:	75	50
1985	11	5
1990	25	12
1995	48	26
2000	56	30
Energy Savings:		
Space Heat	14.6	19
Cooling Energy	16.1	14.9
Lighting	11	0

split of 70-30 between buildings using electricity for air-conditioning only and buildings using electricity for both air-conditioning and space heating was taken from EIA (1984). All commercial buildings are assumed to use electricity for lighting.

9.5 ELECTRICITY SAVINGS RESULTS

Window conservation technologies that are available now are likely to find increasing use in commercial architecture. This section assesses the degree to which window conservation technologies for commercial buildings could likely reduce national electricity consumption in 1985, 1990, 1995, and 2000.

National annual electrical energy savings projections from window conservation technologies for each of the years 1984-2000 are provided in the last columns, respectively of Tables 9.8 and 9.9. These estimates are summarized in Table 9.10 which contains projections for the years 1985, 1990, 1995, and 2000.

The estimates in Table 9.10 represent per-unit energy savings multiplied by the number of units projected to be employing energy-conserving window technologies, with units given in square feet of commercial floorspace. Results of the analyses indicate that significant electricity savings are possible at the national level.

TABLE 9.8. Commercial Floorspace Projections and Market Share Estimates for Window Conservation Technologies on Electrically Heated and Cooled Buildings

Year	Total Commercial Floorspace (a) (10 ⁶ ft ²)	Additional New Commercial Floorspace (a) (10 ⁶ ft ²)	Percent Commercial Floorspace Electrically Heated and Cooled (a)	Retrofit Market Share (b)	Cumulative Commercial Floorspace Retrofit with Energy-Conserving Windows (c) (10 ⁶ ft ²)	Percent New Market Share (b) (/100)	Cumulative Commercial Floorspace Built with Energy Conserving Windows (d) (10 ⁶ ft ²)	Annual Energy Savings from Cumulative Energy Saving Windows (e) (BkWh)
1984	50,700	2,000	30	0.040	584	0.100	60	1.73
1985	52,300	1,600	30	0.045	657	0.110	113	2.09
1986	53,900	1,600	30	0.055	804	0.130	175	2.67
1987	55,400	1,500	30	0.065	950	0.150	243	3.37
1988	56,700	1,300	30	0.080	1,169	0.180	313	5.04
1989	58,000	1,300	30	0.100	1,461	0.210	395	5.1
1990	59,300	1,300	30	0.120	1,753	0.250	492	6.18
1991	60,500	1,200	30	0.140	2,045	0.300	600	7.29
1992	61,700	1,200	30	0.170	2,484	0.350	726	8.85
1993	62,900	1,200	30	0.210	3,068	0.410	874	10.85
1994	64,200	1,300	30	0.240	3,506	0.450	1,049	12.56
1995	65,700	1,500	30	0.255	3,726	0.480	1,265	13.83
1996	67,000	1,300	30	0.270	3,945	0.500	1,460	15.03
1997	68,400	1,400	30	0.280	4,091	0.520	1,679	16.12
1998	69,700	1,300	30	0.290	4,237	0.540	1,889	17.17
1999	71,100	1,400	30	0.295	4,310	0.550	2,120	18.10
2000	72,500	1,400	30	0.300	4,383	0.560	2,356	19.04

(a) DOE 1984a.

(b) See Table 13.9 and Chapter 4.0; includes technical limits.

(c) Calculated by [(Existing Commercial Floorspace in 1984) x (% Electric) x (Market Share for the year)].

(d) Calculated by adding [(Additional New Commercial Floorspace) x (Market Share)] for the year to the cumulative number of the previous year.

(e) Calculated by: [(Cumulative Floorspace Retrofitted) x (2.63 kWh/ft²) + (Cumulative New Floorspace) x (3.19 kWh/ft²)].

TABLE 9.9. Commercial Floorspace Projections and Market Share Estimates for Window Conservation Technologies on Electrically Cooled Buildings

Year	Total Commercial Floorspace (a) (10 ⁶ ft ²)	Additional New Commercial Floorspace (a) (10 ⁶ ft ²)	Percent Commercial Floorspace Electrically Heated and Cooled (a)	Percent Retrofit Market Share (b) (/100)	Cumulative Commercial Floorspace Retrofit with Energy-Conserving Windows (c) (10 ⁶ ft ²)	Percent New Market Share (b) (/100)	Cumulative Commercial Floorspace Built with Energy Conserving Windows (d) (10 ⁶ ft ²)	Annual Energy Savings from Cumulative Energy Saving Windows (e) (BkWh)
1984	50,700	2,000	70	0.040	1,364	0.100	140	2.56
1985	52,300	1,600	70	0.045	1,534	0.110	263	3.14
1986	53,900	1,600	70	0.055	1,875	0.130	409	4.05
1987	55,400	1,500	70	0.065	2,216	0.150	566	4.98
1988	56,700	1,300	70	0.080	2,727	0.180	730	6.22
1989	58,000	1,300	70	0.100	3,409	0.210	921	7.79
1990	59,300	1,300	70	0.120	4,091	0.250	1,149	9.45
1991	60,500	1,200	70	0.140	4,773	0.300	1,401	11.17
1992	61,700	1,200	70	0.170	5,795	0.350	1,695	13.55
1993	62,900	1,200	70	0.210	7,159	0.410	2,039	16.60
1994	64,200	1,300	70	0.240	8,182	0.450	2,449	19.27
1995	65,700	1,500	70	0.255	8,693	0.480	2,953	21.32
1996	67,000	1,300	70	0.270	9,204	0.500	3,408	23.25
1997	68,400	1,400	70	0.280	9,545	0.520	3,917	25.04
1998	69,700	1,300	70	0.290	9,886	0.540	4,409	26.78
1999	71,100	1,400	70	0.295	10,057	0.550	4,948	28.36
2000	72,500	1,400	70	0.300	10,227	0.560	5,496	29.97

(a) DOE 1984a and Chapter 8.

(b) See text and Chapter 4.0; includes technical limits.

(c) Calculated by $[(\text{Existing Commercial Floorspace in 1984}) \times (\% \text{ Electric}) \times (\text{Market Share for the year})]$.

(d) Calculated by adding $[(\text{Additional New Commercial Floorspace}) \times (\% \text{ Electric}) \times (\text{Market Share})]$ for the year to the cumulative number of the previous year.

(e) Calculated by: $[(\text{Cumulative Floorspace Retrofitted}) \times (1.63 \text{ kWh/ft}^2)] + [(\text{Cumulative New Floorspace}) \times (2.42 \text{ kWh/ft}^2)]$.

TABLE 9.10. Estimated National Annual Electricity Savings from Window Conservation Technologies on Commercial Buildings

(BkWh)

Year	Savings for Retrofit Commercial Floorspace Electrically Heated and Cooled	Savings for New Commercial Floorspace Electrically Heated and Cooled	Savings for Retrofit Commercial Floorspace Electrically Cooled Only	Savings for New Commercial Floorspace Electrically Cooled Only	Total Electricity Savings of Window Conservation Technologies
1985	1.74	.35	2.50	.64	5.23
1990	4.62	1.56	6.67	2.78	15.65
1995	9.81	4.02	14.22	7.10	35.15
2000	11.53	7.51	16.66	13.31	49.01

This analysis could not have taken place without the use of several simplifying and limiting assumptions. The scenario is highly simplistic and the numerical energy savings results should be treated accordingly; the results demonstrate possibility rather than actuality. However, the analysis does indicate large energy conservation possibilities from energy-conscious commercial building design. Designing with the climate appears to lead to cost-effective energy savings.

9.6 SENSITIVITY ANALYSIS

This section is an analysis of the sensitivity of the aggregate energy savings results presented in Section 9.5 to alterations in the market penetration scenario. Market share estimates and energy savings results that are lower than the Section 9.5 base case are presented in Section 9.6.1 and Section 9.6.2. Market share estimates and energy savings results that exceed the Section 9.5 base case are presented in Section 9.6.3 and Section 9.6.4.

9.6.1 Low Market Penetration Scenario

A low market penetration scenario investigates the possibility that energy-efficient windows will not penetrate the commercial building market as

quickly or as completely as indicated in Table 9.8 and Table 9.9. This would reduce the maximum projected energy savings potential of energy-efficient windows.

In the low market penetration scenario, maximum market penetration of energy-efficient windows is estimated as half of the maximum of the base cases. For commercial building retrofits, this implies maximum market penetration of 15 percent. For new commercial buildings, it implies maximum market penetration of 28 percent. The rate of market penetration is assumed to slow for the low market penetration scenario. Thus, in the estimates, only 75 percent of maximum estimated penetration is achieved by the year 2000.

Table 9.11 and Table 9.12 present market share estimates for the low market penetration scenario for window energy conservation technologies. Market shares for window energy conservation technologies are unlikely to fall below these estimates.

9.6.2 National Annual Electrical Energy Savings Estimates--Low Scenario

The national annual electricity savings estimates for the low market penetration scenario of energy-conserving window technologies are presented in the final columns of Tables 9.11 and 9.12, and summarized in Table 9.13. It is estimated that total annual electrical energy savings would not be less than 7.69 BkWh by 1990 nor less than 18.96 BkWh in 2000.

9.6.3 High Market Penetration Scenario

Window energy conservation technologies may penetrate the commercial building market more rapidly and to a greater extent than Table 9.8 and Table 9.9 indicate. This would occur, for example, if technical limits were smaller than the assumptions used in that analysis indicate. It would also occur if market acceptance were unusually rapid or complete.

In the high market penetration scenario, maximum market penetration of energy-efficient windows is estimated to equal 60 percent of existing commercial buildings and 90 percent of new commercial structures. These maxima are estimated to be approached at a more rapid rate than in the base case and to be achieved by 1995.

TABLE 9.11. Commercial Floorspace Projections and Low Scenario Market Share Estimates for Window Conservation Technologies on Electrically Heated and Cooled Buildings

Year	Total Commercial Floorspace ^(a) (10 ⁶ ft ²)	Additional New Commercial Floorspace ^(a) (10 ⁶ ft ²)	Percent Commercial Floorspace Electrically Heated and Cooled ^(a)	Percent Retrofit Market Share ^(b) (/100)	Cumulative Commercial Floorspace Retrofit with Energy-Conserving Windows ^(c) (10 ⁶ ft ²)	Percent New Market Share ^(b) (/100)	Cumulative Commercial Floorspace Built with Energy Conserving Windows ^(d) (10 ⁶ ft ²)	Annual Energy Savings from Cumulative Energy Saving Windows ^(e) (BkWh)
1984	50,700	2,000	30	0.030	438	0.070	42	1.29
1985	52,300	1,600	30	0.032	468	0.073	77	1.48
1986	53,900	1,600	30	0.035	511	0.077	114	1.71
1987	55,400	1,500	30	0.040	584	0.082	151	2.02
1988	56,700	1,300	30	0.045	657	0.088	185	2.32
1989	58,000	1,300	30	0.050	731	0.095	222	2.73
1990	59,300	1,300	30	0.056	818	0.105	263	2.99
1991	60,500	1,200	30	0.062	906	0.115	305	3.36
1992	61,700	1,200	30	0.069	1008	0.130	351	3.77
1993	62,900	1,200	30	0.076	1110	0.145	404	4.21
1994	64,200	1,300	30	0.084	1227	0.160	466	4.71
1995	65,700	1,500	30	0.091	1330	0.170	543	5.23
1996	67,000	1,300	30	0.096	1403	0.180	613	5.65
1997	68,400	1,400	30	0.101	1476	0.190	693	6.09
1998	69,700	1,300	30	0.105	1534	0.198	770	6.49
1999	71,100	1,400	30	0.109	1592	0.205	856	2.89
2000	72,500	1,400	30	0.113	1651	0.210	944	7.35

(a) DOE 1984a.

(b) See text and Chapter 1.0; includes technical limits.

(c) Calculated by [(Existing Commercial Floorspace in 1984) x (% Electric) x (Market Share for the year)].

(d) Calculated by adding [(Additional New Commercial Floorspace) x (Market Share)] for the year to the cumulative number of the previous year.

(e) Calculated by: [(Cumulative Floorspace Retrofitted) x (2.63 kWh/ft²) + (Cumulative New Floorspace) x (3.19 kWh/ft²)].

TABLE 9.12. Commercial Floorspace Projections and Low Scenario Market Share Estimates for Window Conservation Technologies on Electrically Heated and Cooled Buildings

Year	Total Commercial Floorspace ^(a) (10 ⁶ ft ²)	Additional New Commercial Floorspace ^(a) (10 ⁶ ft ²)	Percent Commercial Floorspace Electrically Heated and Cooled ^(a)	Percent Retrofit Market Share ^(b) (/100)	Cumulative Commercial Floorspace Retrofit with Energy-Conserving Windows ^(c) (10 ⁶ ft ²)	Percent New Market Share ^(b) (/100)	Cumulative Commercial Floorspace Built with Energy Conserving Windows ^(d) (10 ⁶ ft ²)	Annual Energy Savings from Cumulative Energy Saving Windows ^(e) (BkWh)
1984	50,700	2,000	70	0.030	1,023	0.070	98	1.90
1985	52,300	1,600	70	0.032	1,091	0.073	180	2.21
1986	53,900	1,600	70	0.035	1,193	0.077	266	2.59
1987	55,400	1,500	70	0.040	1,364	0.082	352	3.08
1988	56,700	1,300	70	0.045	1,534	0.088	432	3.55
1989	58,000	1,300	70	0.050	1,705	0.095	519	4.03
1990	59,300	1,300	70	0.056	1,909	0.105	614	4.60
1991	60,500	1,200	70	0.062	2,114	0.115	711	5.17
1992	61,700	1,200	70	0.069	2,352	0.130	820	5.81
1993	62,900	1,200	70	0.076	2,591	0.145	942	6.50
1994	64,200	1,300	70	0.084	2,864	0.160	1,087	7.30
1995	65,700	1,500	70	0.091	3,102	0.170	1,266	8.12
1996	67,000	1,300	70	0.096	3,273	0.180	1,430	8.80
1997	68,400	1,400	70	0.101	3,443	0.190	1,616	9.52
1998	69,700	1,300	70	0.105	3,579	0.198	1,796	10.18
1999	71,100	1,400	70	0.109	3,716	0.205	1,997	10.89
2000	72,500	1,400	70	0.113	3,852	0.210	2,203	11.61

(a) DOE 1984a.

(b) See text and Chapter 4.0; includes technical limits.

(c) Calculated by [(Existing Commercial Floorspace in 1984) x (% Electric) x (Market Share for the year)].

(d) Calculated by adding [(Additional New Commercial Floorspace) x (Market Share)] for the year to the cumulative number of the previous year.

(e) Calculated by: [(Cumulative Floorspace Retrofitted) x (1.63 kWh/ft²) + (Cumulative New Floorspace) x (2.42 kWh/ft²)].

TABLE 9.13. Estimated National Annual Electricity Savings from Window Conservation Technologies on Commercial Buildings, Low Market Penetration Scenario

(BkWh)

Year	Savings for Retrofit Commercial Floorspace Electrically Heated and Cooled	Savings for New Commercial Floorspace Electrically Heated and Cooled	Savings for Retrofit Commercial Floorspace Electrically Cooled Only	Savings for New Commercial Floorspace Electrically Cooled Only	Total Electricity Savings of Window Conservation Technologies
1985	1.23	.25	1.79	.43	3.69
1990	2.16	.83	3.11	1.49	7.59
1995	3.51	1.72	5.03	3.07	13.33
2000	4.34	3.01	6.30	5.31	18.96

Table 9.14 and Table 9.15 present market share estimates for the high market penetration scenario for window energy conservation technologies. Market shares for window energy conservation technologies are unlikely to exceed these estimates.

9.6.4 National Annual Electrical Energy Savings Estimates--High Scenario

The national annual electricity savings estimates for the high market penetration scenario of energy-conserving window technologies are presented in the final columns of Tables 9.14 and 9.15, and are summarized in Table 9.16.

9.7 COST PER KWH OF ENERGY SAVED CALCULATIONS AND COMPARISONS TO THE COST PER KWH OF PRODUCING NEW GENERATION CAPACITY

In this section, the cost of electricity conserved by the use of energy-efficient windows in commercial buildings is compared with the cost of new electrical energy generating capacity. If this conserved energy is cheaper than newly generated resources, then it may make economic sense to increase the use of this conserved energy in order to supply electricity at least cost.

For new commercial construction, the case study clearly indicates that energy conservation through the use of energy-conserving window technologies is cheaper than any alternative source of energy. This is because first costs of

TABLE 9.14. Commercial Floorspace Projections and High Scenario Market Share Estimates for Window Conservation Technologies on Electrically Heated and Cooled Buildings

Year	Total Commercial Floorspace (a) (10 ⁶ ft ²)	Additional New Commercial Floorspace (a) (10 ⁶ ft ²)	Percent Commercial Floorspace Electrically Heated and Cooled (a)	Percent Retrofit Market Share (b) (/100)	Cumulative Commercial Floorspace Retrofit with Energy-Conserving Windows (c) (10 ⁶ ft ²)	Percent New Market Share (b) (/100)	Cumulative Commercial Floorspace Built with Energy Conserving Windows (d) (10 ⁶ ft ²)	Annual Energy Savings from Cumulative Energy Saving Windows (e) (BkWh)
1984	50,700	2,000	30	0.04	584	0.10	60	1.73
1985	52,300	1,600	30	0.05	731	0.13	122	2.31
1986	53,900	1,600	30	0.07	1,023	0.17	204	3.34
1987	55,400	1,500	30	0.11	1,607	0.22	303	5.19
1988	56,700	1,300	30	0.16	2,338	0.28	412	7.49
1989	58,000	1,300	30	0.24	3,506	0.35	549	10.97
1990	59,300	1,300	30	0.34	4,967	0.45	724	15.29
1991	60,500	1,200	30	0.50	7,305	0.56	926	22.17
1992	61,700	1,200	30	0.65	9,497	0.70	1,179	28.74
1993	62,900	1,200	30	0.75	10,958	0.78	1,459	33.47
1994	64,200	1,300	30	0.80	11,688	0.85	1,790	36.45
1995	65,700	1,500	30	0.85	12,419	0.90	2,195	39.66
1996	67,000	1,300	30	0.85	12,419	0.90	2,546	40.78
1997	68,400	1,400	30	0.85	12,419	0.90	2,924	41.89
1998	69,700	1,300	30	0.85	12,419	0.90	3,275	43.11
1999	71,100	1,400	30	0.85	12,419	0.90	3,653	44.32
2000	72,500	1,400	30	0.85	12,419	0.90	4,031	45.52

(a) DOE 1984a.

(b) See text and Chapter 4.0; includes technical limits.

(c) Calculated by [(Existing Commercial Floorspace in 1984) x (% Electric) x (Market Share for the year)].

(d) Calculated by adding [(Additional New Commercial Floorspace) x (Market Share)] for the year to the cumulative number of the previous year.

(e) Calculated by: [(Cumulative Floorspace Retrofitted) x (2.63 kWh/ft²) + (Cumulative New Floorspace) x (3.19 kWh/ft²)].

TABLE 9.15. Commercial Floorspace Projections and High Scenario Market Share Estimates for Window Conservation Technologies on Electrically Heated and Cooled Buildings

Year	Total Commercial Floorspace ^(a) (10 ⁶ ft ²)	Additional New Commercial Floorspace ^(a) (10 ⁶ ft ²)	Percent Commercial Floorspace Electrically Heated and Cooled ^(a)	Percent Retrofit Market Share ^(b) (/100)	Cumulative Commercial Floorspace Retrofit with Energy-Conserving Windows ^(c) (10 ⁶ ft ²)	Percent New Market Share ^(b) (/100)	Cumulative Commercial Floorspace Built with Energy Conserving Windows ^(d) (10 ⁶ ft ²)	Annual Energy Savings from Cumulative Energy Saving Windows ^(e) (BkWh)
1984	50,700	2,000	70	0.04	1,364	0.10	140	2.56
1985	52,300	1,600	70	0.05	1,705	0.13	286	3.47
1986	53,900	1,600	70	0.07	2,386	0.17	476	5.04
1987	55,400	1,500	70	0.11	3,750	0.22	707	7.82
1988	56,700	1,300	70	0.16	5,454	0.28	962	11.22
1989	58,000	1,300	70	0.24	8,182	0.35	1,280	16.43
1990	59,300	1,300	70	0.34	11,591	0.45	1,690	22.98
1991	60,500	1,200	70	0.50	17,045	0.56	2,160	33.01
1992	61,700	1,200	70	0.65	22,159	0.70	2,748	42.77
1993	62,900	1,200	70	0.75	25,568	0.78	3,403	49.91
1994	64,200	1,300	70	0.80	27,272	0.85	4,177	54.56
1995	65,700	1,500	70	0.85	28,977	0.90	5,122	59.63
1996	67,000	1,300	70	0.85	28,977	0.90	5,941	61.61
1997	68,400	1,400	70	0.85	28,977	0.90	6,823	63.74
1998	69,700	1,300	70	0.85	28,977	0.90	7,642	65.73
1999	71,100	1,400	70	0.85	28,977	0.90	8,524	67.86
2000	72,500	1,400	70	0.85	28,977	0.90	9,406	70.00

(a) DOE 1984a.

(b) See text and Chapter 4.0; includes technical limits.

(c) Calculated by [(Existing Commercial Floorspace in 1984) x (% Electric) x (Market Share for the year)].

(d) Calculated by adding [(Additional New Commercial Floorspace) x (Market Share)] for the year to the cumulative number of the previous year.

(e) Calculated by: [(Cumulative Floorspace Retrofitted) x (1.63 kWh/ft²) + (Cumulative New Floorspace) x (2.42 kWh/ft²)].

TABLE 9.16 Estimated National Annual Electricity Savings from Window Conservation Technologies on Commercial Buildings, High Market Penetration Scenario

(BkWh)

Year	Savings for Retrofit Commercial Floorspace Electrically Heated and Cooled	Savings for New Commercial Floorspace Electrically Heated and Cooled	Savings for Retrofit Commercial Floorspace Electrically Cooled Only	Savings for New Commercial Floorspace Electrically Cooled Only	Total Electricity Savings of Window Conservation Technologies
1985	1.92	.39	2.78	.69	5.78
1990	12.98	2.31	18.89	4.09	38.27
1995	32.65	7.01	47.22	12.41	99.29
2000	32.65	12.87	47.22	22.78	115.52

new buildings may actually be reduced, and are reduced in the case study, by the use of energy-efficient windows. The incremental cost of the windows is smaller than the savings that result from reduced design loads and consequent down-sizing of HVAC equipment.

Table 9.17 presents the calculations of the cost per kWh saved due to retrofitting commercial buildings with energy-efficient windows. The analysis indicates a large cost advantage for this energy-conservation measure. However, this result may not be representative. The effectiveness of window conservation technologies, and their cost, vary so much that it is difficult to generalize the results of the case study without introducing a potentially large error.

TABLE 9.17. Cost per kWh Calculations for Energy-Efficient Windows,
as a Retrofit Measure for Existing Commercial Buildings

Incremental Capital Cost ^(a)	33¢ per square foot
Levelized Capital Cost ^(b)	2.9¢ per square foot per year
Annual Electricity Savings	
Heating and Cooling	2.638 kWh per square foot
Cooling Only	1.634 kWh per square foot
Cost per kWh ^(c)	
Heating and Cooling	1.1¢ per kWh
Cooling only	1.8¢ per kWh

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- (a) See Table 9.3. $\$13,000 \div 40,000$ square feet = 33¢ per square foot.
- (b) The level stream of annual payments the present value of which would equal the investment's incremental capital cost. Assumes a 30-year useful lifetime of the investment and an 8 percent rate of interest compounded annually.
- (c) Levelized capital cost divided by annual energy savings.

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10.0 ADVANCED LIGHTING TECHNOLOGIES

One of the most widespread uses for electricity in the U.S. is for lighting. In all end use sectors, lighting energy is almost totally from electric sources and the potential for energy savings exists. The most significant savings are likely to be in the commercial sector, where 237 BkW or more than 35 percent of total electricity use was consumed in 1984 for lighting commercial buildings (DOE 1985). Several advanced technologies recently developed and marketed can reduce future electricity use in commercial sector lighting. These new technologies include electronic (solid state) ballasts, energy-saving fluorescent lamps, fluorescent dimming controls, energy-efficient fluorescent fixtures, and fluorescent lamps that operate in incandescent fixtures.

This chapter focuses on the future electricity savings that may be achieved from the use of electronic ballasts and energy-saving fluorescent lamps. Since both the new ballasts and the new lamps are perfect substitutes for their respective conventional technologies, and since approximately 70 percent of commercial sector lighting is fluorescent, these two technologies appear to have savings potential.^(a) Because of resource constraints we were unable to evaluate all of the lighting technologies mentioned above. Instead we limited our analysis to those technologies that demonstrate the greatest potential in terms of maximum market penetration and aggregate energy savings.

The remainder of this chapter discusses the development, current availability, and estimated market penetration for both electronic ballasts and energy-saving fluorescent lamps. Section 10.1 contains information about the development of these two technologies, including descriptions of how each saves electricity. Section 10.2 discusses the current state of the markets for the technologies and Section 10.3 discusses their cost effectiveness and potential market penetration. Finally, Section 10.4 gives the quantitative estimates of energy savings for both electronic ballasts and energy-saving fluorescent lamps. Section 10.5 analyzes the sensitivity of the energy savings results to

(a) Based on estimates by PNL commercial buildings experts and the PG&E survey (1981).

changes in market penetration. Section 10.6 concludes with an estimate of the cost per kWh saved through the installation of electronic ballasts and energy efficient fluorescent bulbs.

10.1 TECHNICAL BACKGROUND

Electricity savings in commercial lighting really began with the introduction of the fluorescent lamp in 1939. The ability of this lamp to operate four to five times as efficiently as the incandescent lamp, plus its longer service life, resulted in its widespread use.^(a) A fluorescent lamp assembly has three basic parts, each of which can contribute to electricity consumption: the ballast, the tube or lamp, and the fixture. The development of efficient ballasts and lamps is given below.

10.1.1 The Electronic Ballast

Any electric-discharge lamp needs a ballast to provide the necessary circuit conditions (voltage, current, wave form) for starting and operating. The heart of a conventional ballast is the transformer, where the principle of mutual induction is used to convert the current from the electric source into the voltage and current needed by the fluorescent lamp. These ballasts are essentially "stepdown" transformers that reduce the standard 60 Hertz electric current to the 40 watts used by the lamp systems studied in this chapter. In addition to the electricity consumed in the process of magnetic induction, conventional ballasts have standard resistance and hysteresis losses. These ballasts have a rated life of 10 to 12 years at proper operating temperatures; higher temperatures (usually the result of electric losses) can significantly shorten ballast life (Kaufman 1981).

As early as 1950 it was discovered that fluorescent lamps operated more efficiently at high frequencies (20,000 to 30,000 Hz). Shortly after this discovery a small effort was made to develop centralized lighting systems that could take advantage of high frequencies, but cost considerations soon shut down work in this direction. With the introduction of electronic circuitry about 20 years ago, renewed efforts to develop a more efficient ballast again

(a) Unpublished article on lighting standards by Stanley H. Pansky, Architect.

encountered high component costs that precluded unit feasibility. Two major events in the early 1970s finally provided a basis for reconsidering the commercialization of electronic ballasts: the sharp increases in the price of energy and the adoption of electronic systems by the auto industry. This latter development resulted in price reductions for the switching power transistors essential for the manufacture of solid state ballasts.

Despite these important break-throughs, the large ballast manufacturers did little to develop the new ballasts even though small companies believed a cost-effective electronic ballast could be developed and sold. In 1976, the U.S. Department of Energy (DOE) initiated a lighting program to assist in the commercialization of energy-efficient lighting products, including electronic ballasts. After three years of testing, demonstrations showed that cost-effective, energy-efficient ballasts were ready for widespread application. Tests in both laboratories and buildings confirmed estimates of 20 to 25 percent improvements in energy efficiency (Stevens 1978).

The electronic ballasts on the market today have solid state circuitry which transforms the input electrical power to the lamp more efficiently, consuming about 10 percent less power than conventional ballasts. In addition, solid state ballasts also dissipate less power in the form of heat than the magnetic ballasts with their hysteresis losses and larger resistance losses. Equally or even more important than savings in the ballast itself are electricity savings gained by the high frequency operation of the fluorescent lamps used with these new ballasts. Fluorescent lamps operated at high frequency convert the input electricity from the ballast to visible light with better efficacy. This happens because at higher frequencies the rate of change of the applied lamp voltage is more rapid than the recombination of the ionized gas inside the bulb; therefore, there is virtually no ion or light decay during each cycle.

Electronic ballasts have more components than conventional ballasts in order to raise the frequency of the current before it is adjusted by the transformer. A rectifier converts the input power from alternating current (AC) to direct current (DC) and then a capacitor evens out the curve frequency. Next, an oscillator changes the flat DC current to 20,000 or more Hertz and converts

it back to AC. The current then goes to a solid state transformer and to the lamp. The switching power supply used by the electronic ballasts is fundamentally more efficient than the magnetic power supply of conventional ballasts, contributing to the electricity savings. Electronic ballasts have several other advantages over magnetic ballasts: 1) extended lamp life; 2) continuous dimming capability; 3) lighter weight; 4) reduced audible hum; 5) longer useful life; and 6) reduced heat generation which leads to lighter air condition loads. The major disadvantage of electronic ballasts with respect to conventional ballasts is potential radio frequency interference, although no documented instances of this could be found (Johnson 1981).

10.1.2 Energy-Saving Fluorescent Lamps

The standard 40-watt, 48-inch long fluorescent lamp is one type of gas discharge lamp. The lamp bulb, usually in the shape of a long tube, is filled with mercury vapor at low pressure (and a small amount of argon gas for starting), is coated with fluorescent powders on the inner wall, and is hermetically sealed at each end with a cathode plug. The operation of the fluorescent lamp depends upon the development of a discharge between the two electrodes (cathodes) at the extremities of the bulb. This discharge is developed by the ionization of the mercury gas that occurs when electric current enters the lamp through the electrodes. The discharge or "mercury arc" produces ultraviolet light that excites the fluorescent powders, or phosphors, to emit visible light. Typically, a higher initial voltage is needed to establish the arc than is needed to maintain it (Kaufman 1981).

The bulk of the energy-saving lamps designed to replace the standard, 40-watt lamp are 34-watt lamps, although a few 32-watt and 28-watt lamps are currently being marketed. The new lamps save electricity in a variety of ways. Some of these lamps have increased pressure within the bulb while others have an enriched phosphor coating. The newest lamps use the full rated wattage to start the lamp, but have heat activated switches that disconnect the cathodes inside the light after starting, reducing the power consumed to the lesser amount needed for lamp operation. As with electronic ballasts, a reduction in radiant heat losses from the efficient bulbs also contributes to electricity savings by reducing air conditioning loads.

10.2 CURRENT MARKET SITUATION

Both electronic ballasts and energy-saving fluorescent lamps are currently available for new construction and retrofit applications. Although no published information is available on the market shares presently commanded by these technologies, sources in both industries claim that sales are growing.^(a) Specific information about the two markets is discussed below.

10.2.1 The Fluorescent Ballast Market

The existing ballast business can be classified as a low technology mature industry. The market is dominated by Universal Manufacturing Company and Advanced Transformer Company, each of which is estimated to control about 40 percent of the magnetic ballast market (Warrock, November 12, 1984). Small profit margins, products that are near-perfect substitutes from brand to brand, and virtually identical prices for like goods characterize the ballast market. The resulting focus of marketing strategy in this industry has been on distribution, product warranties, and service to promote brand loyalty. Manufacturers of conventional ballasts are firmly entrenched in the business with relatively large investments in capital equipment and tooling, most of which has probably been fully depreciated.

The major vendors of electronic ballasts currently available are listed in Table 10.1. It is estimated that electronic ballasts currently account for 3 percent of the total ballast market.^(b) General Electric Company recently announced that an electronic ballast will be added to its ballast line, but price and rated life information on it was not available for inclusion in Table 10.1. Since the commercial introduction of electronic ballasts in 1980, two manufacturers have gone out of the business: Thomas Industries, Inc. and Jefferson Electric. Although Universal Manufacturing purchased Luminoptics (one of the leaders in the development of electronic ballasts) in 1981, neither of the two dominant ballast manufacturers has developed an electronic ballast.

(a) Personal communication with Ben Miller, GTE Sylvania (December 5, 1984); Lowell Blankenship, North America Philips (December 4, 1984); and Dr. Rudolph Verderber, LBL (November 30, 1984).

(b) Personal communication with Dr. Rudolph Verderber, LBL (November 30, 1984).

TABLE 10.1. Electronic Ballast Manufacturers

	<u>Manufacturer</u>	<u>Year Introduced</u>	<u>Price</u>	<u>Rated Life</u>	<u>Warranty</u>
1.	Electronic Ballast Technology, Inc.	1980	\$25-31	6-10 years +	3 years
2.	General Electric	1984	NA	NA	1 year
3.	Hunt Electronics Co.	1983	\$30-40	10-20 years	3 years
4.	Luminoptics, Div. (University Mfg)	1980	\$40-90	10 years	2 years
5.	Triad-Utrad	1980	\$33-45	17-20 years	3 years

Source: Energy User News, April 9, 1984.

LMP Corporation, formerly Luminoptics, brought suit against Universal Manufacturing in federal court in November 1984, alleging that both Universal and Advance Transformer have conspired in a monopolistic way to prevent the effective development of the electronic ballast market (Warrock, November 12, 1984). LMP claims that this conspiracy has kept the prices of the new ballasts higher than the prices for conventional ballasts.

Despite any market limitations imposed by Universal and Advance Transformer, other events suggest that the electronic ballast market will continue to grow. Probably the most significant indicator of continued sales is the recent development by General Electric and GTE Sylvania of fluorescent lamps designed specifically for use with the high-frequency, solid-state ballasts. This recognition of the electronic ballast by the major lamp manufacturers is an important market signal. In addition, General Electric announced on November 15, 1984 that an electronic ballast will be added to its ballast line. The State of Oregon, AT&T, and several other companies have begun retrofitting with electronic ballasts (Barber, April 30, 1984; Gardner, May 7, 1984; Weaver May 23, 1983). Based on this and other information, Dr. Rudolph

Verderber, Program Manager of the DOE Lighting program, predicts that the electronic ballast will dominate the ballast market by the turn of the century.^(a)

10.2.2 The Fluorescent Lamp Market

The market for fluorescent lamps is similar, in many respects, to the ballast market. Several large firms dominate the market, products are substitutable and similarly priced, and marketing strategy aims at developing brand name loyalty. Unlike the ballast market, however, it is the larger manufacturers who are actively participating in the development of energy-efficient bulbs. The major energy-saving alternatives to the standard 40-watt, 48-inch fluorescent lamp along with standard lamps are listed by manufacturer in Table 10.2.

Representatives from all three manufacturers listed in Table 10.2 indicated that sales of the energy-saving lamps are growing rapidly. One representative estimated that sales of the new lamps are currently approaching 50 percent of all fluorescent sales.^(b) The energy-efficient lamps are perfect substitutes for standard lamps on standard ballasts. A few of the new lamps are not recommended for use with electronic ballasts. Since the majority of lamps are compatible with either type of ballast and since the market share is growing rapidly, it is likely that the energy-saving fluorescent lamp will dominate the lamp industry in the future.

10.2.3 Competition from Other Technologies

Both electronic ballasts and energy-efficient lamps may face significant competition from technologies outside their narrowly defined industries. For example, the strong emergence of dimming controls, which allow continuous variation in level of lighting, could affect sales of both these technologies by reducing the payback on the incremental energy savings the ballasts and lamps can add to the relatively large energy saving potential of dimmer-controlled

(a) Personal communication with Dr. Rudolph Verderber, LBL (November 30, 1984).

(b) Personal communication with Ben Miller, GTE Sylvania (December 5, 1984).

TABLE 10.2 Standard and Energy Efficient 48 inch Fluorescent Bulbs

Manufacturer/Model	Watts	Rated Life (hr)	Price	Incremental Price Over Standard Bulb ^(a)
General Electric				
Cool White Watt-Miser	34	20,000	\$2.64	.89
Lite White Watt-Miser II	34	20,000	2.91	1.16
Lite White Deluxe Watt-Miser II	34	20,000	3.20	1.45
Optimizer	28	18,000	NA	NA
Watt Miser Plus	34	20,000	3.30	1.55
GTE Sylvania				
Cool White Super Saver I	34	20,000	2.64	.89
Lite White Super Saver II	34	20,000	2.91	1.16
Lite White Deluxe Super Saver III	34	20,000	3.20	1.45
Cool White Super Saver Plus	32	20,000	3.29	1.54
Octron (not for retrofit)	32	20,000	3.08	1.33
North America Philips				
Cool White Econowatt	34	20,000	2.63	.88

(a) Incremental prices is based on the comparison of the price of energy efficient bulbs to standard bulbs produced by the three major manufacturers at \$1.75. These bulbs have the same rated life but use 40 watts.

lighting. This is particularly true for fluorescent lamps, as continuous dimming (the most efficient kind) is facilitated by the use of electronic ballasts. The limited information available on the trade offs between lighting technologies, many of which are not compatible, does not allow for in-depth analysis here.

10.3 COST-EFFECTIVENESS AND MARKET PENETRATION

The cost-effectiveness and likely market penetration of electronic ballasts and energy-saving fluorescent lamps are discussed in this section. Cost-effectiveness will be measured by the estimated payback period, which is then used to estimate likely market penetration according to the methodology outlined in Chapter 4.0. Incremental capital costs will not be used directly to estimate penetration (although they are used to calculate the payback period).

Using the incremental costs in this case would imply little market penetration by the year 2000 for either technology. As stated previously, information available suggests that both energy saving fluorescent lamps and electronic ballasts have already achieved some market penetration which is expected to grow. It is possible that the level of market penetration for these items may be much greater than the methodology based on factors including incremental cost would suggest. While the incremental cost on "big-ticket" items may be an important factor for building owners and managers, incremental cost may be ignored by these decision makers when it is quite small in absolute terms (such as \$14 for electronic ballasts or \$1.25 for energy saving fluorescent bulbs). Building owners and managers may also be so keen to save money that they may invest in these comparatively inexpensive measures without relying on the same methods for determining cost effectiveness that they would apply to other measures.

10.3.1 Cost Effectiveness of Electronic Ballasts

To calculate the payback for an electronic ballast, representative conventional and electronic ballast and lamp units are specified as two lamp (40 watts each), 48-inch standard fluorescent fixtures. To compute the payback period, the value of the annual electricity savings for a typical electronic ballast light fixture is compared to the difference in cost between a conventional ballast and an electronic ballast (see Chapter 4.0). In this analysis, only the ballast is assumed to change; no allowance is made for electronic ballasts installed with energy-saving lamps, since electronic ballast manufacturers claim ballasts are cost-efficient when retrofitted with standard lamps (Energy User News, July 16, 1984). For purposes of this analysis all fluorescent lighting in the commercial sector is assumed to be from reference case fixtures. It is difficult to assess the affect of this assumption on the estimates of total electricity savings generated for the new ballasts since ballasts are used with all fluorescent lights no matter how many lamps or what shape the lamps are in a fixture. The limited data available suggest that the longer the lamp tube the greater the total savings for the ballast/lamp unit (Kaufman 1981), so the results in this chapter are probably fairly conservative.

Based on manufacturers estimates, guidelines for the IES (Illuminating Engineering Society) Handbook, and discussion with Dr. Verderber, electronic ballasts are estimated to save 19 to 32 percent of the 96 watts needed to operate a conventional ballast and lamp unit according to reference case specifications. Assuming that electricity savings with the electronic ballast are 25 percent (a reduction of approximately 8 watts in ballast consumption and losses and 16 watts in power needed to operate the lamps), use of the new ballast will result in 24 watts of electricity saved. Electronic ballast testing generally assumes 4000 hours of operation per year (Verderber 1980), which would mean electricity savings of 96 kWh per year per reference case fixture. With commercial sector electricity prices at 7.01¢ per kWh, the value of these electricity savings is \$6.73 per year for each two-lamp fixture with an electronic ballast. Throughout our analysis we have assumed 4000 hours of operation a year. In Section 10.6, in order to test the sensitivity of our estimate of total energy savings to this assumption, we present a scenario which assumes usage of 2600 hours a year.

Representative costs for electronic ballasts are given in Table 10.1. A fairly wide range of prices is shown, with the Luminoptics ballasts priced slightly higher than the rest. Since both replacement and new construction sales of ballasts are likely to occur in large lots with discounts, these prices may be slightly high. Mention of the price paid for ballasts by the media indicated that this was so (Duffy, September 26, 1983). Assuming some discounts are available, the price of a reference case electronic ballast is assumed to be \$28.00. Conventional ballasts generally range in price from \$11.00 for a basic unit to \$25.00 for an energy-efficient magnetic unit. Making the same assumption of large lot discounts, a representative price of \$14.00 is chosen for use in this analysis.

Since electronic ballasts are perfect substitutes for conventional ballasts, no incremental installation costs need to be added to the incremental capital cost calculation. Therefore, the incremental capital cost for an electronic ballast is simply the difference in cost between the new ballast (\$28.00) and the conventional ballast (\$14.00), or \$14.00. Dividing this increment by the value of electricity savings for one year (\$6.73) yields a

payback period of 2.05 years (at 4000 hours of operation a year). This figure is consistent with manufacturers estimated paybacks, which range from one to five years (Energy User News, April 9, 1984).

Accelerated replacement of conventional ballasts by electronic ballasts does not appear to be economically possible. In addition to the incremental capital costs of \$28.00 (\$28.00 minus zero), significant installation costs would be incurred that would likely cause the payback period associated with such accelerated replacement to be more than five years. Since the estimated penetration of investments with payback periods exceeding five years is zero (Chapter 4.0), such replacement is not considered in the remainder of this chapter.

10.3.2 Electronic Ballast Market Penetration

Market penetration of electric ballasts is assumed to be a function of the payback period (as described in Chapter 4.0), as tempered by any technical limitations. There are only two potential technical limitations that would appear to have any possible effect on market penetration. First, there are some compatibility problems between electronic ballasts and a few of the energy-saving fluorescent lamps (e.g., GTE Sylvania's Super Saver Plus and GE's Watt-Miser Plus). In fixtures where these lamps have been retrofitted, use of electronic ballasts may be precluded or at least delayed until the lamps are ready to be replaced. At that time, other lamps compatible with the new ballasts could be introduced. There are so many lamps that can be used with electronic ballasts that this problem is assumed to have no effect on market penetration. The second potential problem is radio frequency interference caused by the new ballasts' high frequency. Since quality engineering and manufacture appear to be able to handle this problem (no instances of occurrence could be identified), this will also be assumed to have no effect on market penetration.

The payback period of 2.05 years (at 4000 hours of operation a year) leads to an estimated maximum market penetration for electronic ballasts of 65 percent in the year 2000 as shown in Table 10.3. This penetration rate is assumed to apply to both the new construction market and the normal replacement market. This relatively high penetration rate despite high incremental capital costs,

TABLE 10.3. Market Share Estimates for Electronic Ballasts

<u>Year</u>	<u>Percent of Total Annual Ballast Sales</u>
1984	10
1985	12
1990	29
1995	55
2000	65

is consistent with the positive market signals discussed above: the entrance of a major manufacturer (General Electric) into the market, the optimistic state of the current market, and the need for electronic ballasts in order to take advantage of the potentially large electricity savings attainable with the use of continuous dimming.

10.3.3 Cost Effectiveness of Energy-Saving Fluorescent Lamps

The payback calculation used to assess the cost effectiveness of energy efficient fluorescent lamps is based on the selection of the 40-watt, 48-inch lamp as the Representative example of a standard lamp. Standard 40-watt lamps generally consume 40 watts, while most of the energy-saving lamps consume 34 watts or less electricity for approximately the same light output (Burt Hill Kosar Rittelman Associates 1984). Using a 34-watt lamp as the representative energy-saving lamp, each energy-saving lamp saves 6 watts over the reference case standard lamp. Assuming lamp operation of 4000 hours per year, the electricity savings per year for one lamp are estimated as 24 kWh. Using the 1983 commercial sector electricity price of 7.01¢ per kWh, the value of these energy savings are \$1.68 per year for one lamp.

The incremental capital cost of energy-saving lamps versus standard lamps is calculated as the difference in the cost of the lamps, since installation costs are identical for both. The range of prices for the energy-saving lamps is given in Table 10.2. A simple average of these prices gives a price of \$2.98 for the representative energy-saving lamp. The price for a standard 40-watt fluorescent lamp is \$1.75 for all three of the manufacturers listed in

Table 10.2 (Energy User News, May 16, 1983), so that price will be assigned to the representative conventional lamp. The resulting incremental capital cost for energy-saving fluorescent lamps then becomes \$1.23 and with the \$1.70 worth of electricity savings implies a payback period of 0.72 years, or approximately 8.5 months. This estimate is consistent with manufacturer payback estimates which range from 8 months to 1.3 years (Energy User News, May 16, 1983).

As with electronic ballasts, accelerated replacements of conventional bulbs is not considered in the remainder of this analysis because we believe the associated payback period would lead to an estimate of zero penetration. This belief is consistent with our observation that building owners do not replace working bulbs early to obtain energy savings.

10.3.4 Energy-Saving Fluorescent Lamp Market Penetration

Like the case for electronic ballasts, the market penetration for energy-saving fluorescent lamps is assumed to be a function of the payback period and any technical limitations. No technical limitations appear to be relevant to the potential market penetration of the new lamps; even though some lamps cannot be used with an electronic ballast, there are plenty of energy-saving lamps that can be used effectively with these ballasts. Using the payback period of 8.5 months and the methodology described in Chapter 4.0, market penetration for the energy saving fluorescent lamps is estimated to reach a maximum of 75 percent by the year 2000, as shown in Table 10.4. This relatively high penetration rate actually appears conservative if industry estimates of 50 percent penetration in today's market are accurate. This 75 percent market penetration rate is assumed to apply to both the new construction and the normal replacement markets.

10.4 COMMERCIAL BUILDING AND MARKET SHARE PROPERTIES

Under the resource constraints of this study no estimate of the total stock of either ballasts or lamps could be identified. The only measure of commercial activity found was commercial floorspace; unfortunately, no estimate of fluorescent fixtures per square foot of floorspace could be found to make

TABLE 10.4. Market Share Estimates for Energy Saving Fluorescent Lamps

<u>Year</u>	<u>Percent of Total Annual Fluorescent Lamp Sales</u>
1984	10
1985	13
1990	36
1995	65
2000	75

the transition from energy savings per lamp or ballast/lamp unit to energy savings per square foot simpler. However, a commercial building survey performed by Pacific Gas and Electric Company (PG&E 1981) provided an estimate of the commercial floorspace lighted with fluorescent fixtures as equaling approximately 70 percent of commercial floorspace. This estimate of the portion of commercial floorspace fluorescently lit was applied to estimates for commercial floorspace for 1983-1990 and 1985 obtained from DOE (DOE 1984). Yearly floorspace estimates for 1991-1994 were interpolated at 2 percent based on the 1990-1995 estimated growth. Estimates for 1996-2000 were derived assuming a continuation of this 2 percent annual growth in commercial floorspace. It was assumed that 70 percent of total new floorspace is lighted with fluorescent fixtures. The resulting estimates for fluorescently-lighted commercial floorspace for each of the years 1984-2000 are shown in Table 10.5 and 10.6.

Use of the new ballast and lamp technologies, particularly in the retrofit market, is also dependent on the rate at which the conventional equipment needs replacement. This retirement rate, in most cases, is directly related to the useful life of the equipment. To calculate energy savings, ballasts are assumed to be retired every eight years (a rate of 12.5 percent per year) while fluorescent lamps are assumed to be retired every five years (a rate of 20 percent per year). These retirement rates are applied directly to the commercial floorspace lighted by fluorescent fixtures.

10.5. ENERGY SAVINGS RESULTS

Electricity savings from electronic ballasts and energy-saving lamps for the nation as a whole are estimated below as described in Chapter 4.0. Electricity savings are presented for both the new construction and normal replacement markets.

Electronic Ballasts

Energy savings per foot of fluorescently-lighted commercial floorspace for electronic ballasts are based on three assumptions: 1) that fluorescent floorspace is approximately 70 percent of all commercial floorspace; 2) that the remainder of commercial floorspace is lighted primarily by incandescent sources; and 3) that incandescent sources use four times as much energy as standard fluorescent sources. The first step in the calculation is to find how much of the 237 BkWh of electricity used for commercial lighting is used in fluorescent fixtures. Using the assumptions above, the following equation was generated:

$$\begin{aligned} 237 \text{ BkWh} &= (.30)4F + (.70)F \\ 124.7 \text{ BkWh} &= F \end{aligned}$$

where:

F = electricity consumed for fluorescent lighting

Electricity consumption by fluorescent lighting currently utilizing electronic ballasts is not accounted for in this calculation. This was done for the sake of simplicity given that electronic ballasts account for less than 1 percent of current ballast population and given that our estimates are approximations of the portion of commercial floorspace that is fluorescently lighted.

According to this calculation, 123.1 BkWh (53 percent) of all commercial lighting energy is consumed by fluorescent lighting. Since 70 percent of the 50.7 billion square feet of commercial floorspace is assumed to be fluorescently-lighted (35.5 billion square feet), fluorescent lighting energy amounts to 3.51 kWh per square foot of fluorescently-lighted floorspace not presently

using electronic ballasts. The estimated 25 percent savings used to calculate the payback period implies energy savings per fluorescently-lighted square foot equal to .88 kWh annually.

Using the methodology described in Chapter 4.0, the energy savings results shown in the final column of Table 10.5 and summarized in Table 10.7 were estimated. This suggests that in 2000 a total of 37.93 kWh can be saved by the electronic ballast. This is probably a conservative estimate, since some of the incandescently-lighted floorspace is expected to change to fluorescent lighting as well.

Energy-Saving Fluorescent Lamps

Fluorescent lamp energy savings per square foot of fluorescently-lighted floorspace are computed using the three main assumptions and the procedure described above for electronic ballasts. Instead of a savings rate of 25 percent, however, the savings rate of 15 percent used in the payback calculation is used. This yields estimated energy savings of .53 kWh per square foot of fluorescently-lighted floorspace annually for energy-saving lamps.

The last column of Table 10.6 gives the energy savings results for fluorescent lamps in both the new construction and retrofit markets. These savings are further summarized in Table 10.7. In the year 2000 energy savings in new fluorescently lighted floorspace are estimated at 41.30 BkWh. These estimates are conservative if industry estimates of 50 percent penetration rates in today's market are accurate, since the beginning penetration rate for 1984 is 10 percent in this analysis. Since no empirical data on actual penetration rates were available to confirm the industry estimates, the procedure from Chapter 4.0 was used even though the beginning market penetration rates seem to be low for energy-efficient lamps.

10.6 SENSITIVITY ANALYSIS

This section provides an assessment of the sensitivity of the aggregate energy savings results presented in Section 10.4 to changes in the thermal storage market penetration scenarios. Low and high market penetration

TABLE 10.5. Annual Market Share and Energy Savings Projections for Electronic Ballasts

Year	Total Estimated Commercial Fluorescent Floorspace ^(a) (10 ⁶ ft ²)	Total New Fluorescent Floorspace ^(b) (10 ⁶ ft ²)	Fluorescent Floorspace Replacing Conventional Technology ^(c) (10 ⁶ ft ²)	Market Share for For Energy Efficient Technology ^(d) Units ^(d)	Annual Floorspace Additions Employing New Technology ^(e)	Cumulative Floorspace Additions Employing New Technology ^(f)	Cumulative Annual Energy Savings ^(g) (Bkwh)
1984	35490	1,400	4,262	0.10	566	566	0.57
1985	36610	1,120	4,436	0.12	667	1,233	1.16
1986	37730	1,120	4,576	0.14	797	2,030	1.86
1987	38780	1,050	4,716	0.17	980	3,010	2.72
1988	39690	910	4,848	0.20	1,152	4,162	3.73
1989	40600	910	4,961	0.24	1,409	5,571	4.97
1990	41510	910	5,075	0.29	1,736	7,307	6.50
1991	42350	840	5,189	0.34	2,050	9,357	8.31
1992	43190	840	5,294	0.40	2,454	11,810	10.46
1993	44030	840	5,399	0.46	2,870	14,680	12.99
1994	44240	910	5,504	0.51	3,271	17,951	15.87
1995	45990	1,050	5,530	0.55	3,619	21,570	19.05
1996	46900	910	5,749	0.58	3,862	25,432	22.45
1997	47880	980	5,863	0.60	4,106	29,537	26.06
1998	48790	910	5,985	0.62	4,275	33,812	29.83
1999	49770	980	6,099	0.64	4,530	38,343	33.81
2000	50750	980	6,221	0.65	4,681	43,024	37.93

- (a) Fluorescent floorspace estimate based on EIA estimates for commercial floorspace (DOE 1984) multiplied by estimate of portion that is fluorescently lit of .70 (Pacific Gas and Electric 1982). It is assumed that there will be no commercial floorspace retirements.
- (b) Calculated by fluorescent floorspace estimate for current year minus estimate for previous year. 1983 floorspace estimate is 48,700 x 10⁶ ft² (DOE 1984).
- (c) Based on assumption that ballasts are to be replaced every eight years. Calculated by: (Estimated Floorspace for previous year) x (.125).
- (d) Based on Methodology presented in Chapter 4.0 and assumptions presented in this chapter.
- (e) Calculated by: (Floorspace replacing conventional technology + Floorspace additions employing new technology) x (Market Share)
- (f) Calculated by: (Current years additions + previous years cumulative additions).
- (g) Calculated by: Cumulative additions of New Technology x (.88 kwh).

TABLE 10.6. Annual Market Share and Energy Savings Projections for Energy-Efficient Fluorescent Lamps

Year	Total Estimated Commercial Fluorescent Floorspace ^(a) (10 ⁶ ft ²)	Total New Fluorescent Floorspace ^(b) (10 ⁶ ft ²)	Fluorescent Floorspace Replacing Conventional Technology ^(c) (10 ⁶ ft ²)	Market Share for For Energy Efficient Technology ^(d) Units ^(d)	Annual Floorspace Additions Employing New Technology ^(e)	Cumulative Floorspace Additions Employing New Technology ^(f)	Cumulative Annual Energy Savings ^(g) (BkWh)
1984	35,845	1,400	6,818	0.10	822	822	0.44
1985	36,976	1,120	7,169	0.13	1,078	1,900	1.01
1986	38,107	1,120	7,395	0.16	1,362	3,262	1.73
1987	39,168	1,050	7,621	0.20	1,734	4,996	2.65
1988	40,087	910	7,834	0.24	2,098	7,095	3.76
1989	41,006	910	8,017	0.30	2,678	9,773	5.18
1990	41,925	910	8,201	0.36	3,280	13,053	6.92
1991	42,774	840	8,385	0.43	3,967	17,020	9.02
1992	43,622	840	8,555	0.50	4,697	21,717	11.51
1993	44,470	840	8,724	0.56	5,356	27,073	14.35
1994	44,682	910	8,894	0.61	5,980	33,054	17.52
1995	46,450	1,050	8,936	0.65	6,491	39,545	20.96
1996	47,369	910	9,290	0.68	6,936	46,481	24.64
1997	48,359	980	9,474	0.71	7,422	53,903	28.57
1998	49,278	910	9,672	0.73	7,725	61,628	32.67
1999	50,268	980	9,856	0.74	8,018	69,646	36.92
2000	51,258	980	10,054	0.75	8,275	77,921	41.30

- (a) Fluorescent floorspace estimate based on EIA estimates for commercial floorspace (DOE 1984) multiplied by estimate of portion that is fluorescently lit of .70 (Pacific Gas and Electric 1982). It is assumed that there will be no commercial floorspace retirements.
- (b) Calculated by fluorescent floorspace estimate for current year minus estimate for previous year. 1983 floorspace estimate is 48,700 x 10⁶ ft² (DOE 1984).
- (c) Based on assumption that lamps are to be replaced every five years. Calculated by: (Estimated Floorspace for previous year) x (.2).
- (d) Based on Methodology presented in Chapter 4.0 and assumptions presented in this chapter.
- (e) Calculated by: (Floorspace replacing conventional technology + Floorspace additions employing new technology) x (Market Share)
- (f) Calculated by: (Current years additions + previous years cumulative additions).
- (g) Calculated by: Cumulative additions of New Technology) x (.53 kWh).

TABLE 10.7. Energy Savings Results: Electronic Ballasts and High Efficiency Fluorescent Lamps

<u>Year</u>	<u>Estimated Annual Energy Savings From Electronic Ballasts (BkWh)</u>	<u>Estimated Annual Energy Savings From High Efficiency Fluorescent Lamps (BkWh)</u>	<u>Total For Both Technologies</u>
1985	1.16	1.01	2.17
1990	6.50	6.92	13.42
1995	19.05	20.96	14.01
2000	37.93	41.30	79.23

scenarios are examined to determine an implied minimum/maximum range of potential future energy savings. Section 10.6.1 presents low market penetration scenario assumptions. Section 10.6.2 presents the electrical savings estimates associated with this scenario. Sections 10.6.3 and 10.6.4 discuss high market penetration scenario assumptions and energy savings estimates respectively. Section 10.6.5 and 10.6.6 present the assumptions and energy savings estimates for a low usage scenario in which both the high efficiency fluorescent bulbs and the electronic ballasts are assumed to have 2600 hours of usage a year.

10.6.1 Low Market Scenario

Electronic ballasts and/or energy saving fluorescent lamps may not penetrate the commercial building lighting market as quickly or completely as suggested by the base-case estimates. High cost differentials and long payback periods may inhibit the market penetration of these technologies to levels below those indicated previously.

The specific assumption for the low market penetration scenario is that the maximum potential level of penetration is only half of what it was estimated to be in the base case scenario. Thus the maximum potential market share was reduced from 65 percent to 32.5 percent for electronic ballasts and from 75 percent to 37.5 percent for energy saving fluorescent lamps. The assumed rate of market penetration was reduced such that only 75 percent of that new

maximum potential will be reached by the year 2000. Market penetration for both electronic ballasts and energy saving fluorescent lamps are given in Table 10.8.

10.6.2 National Annual Electrical Energy Savings Estimates - Low Scenario

The national annual electrical energy savings estimates for the low market penetration scenario for electronic ballasts and energy saving fluorescent bulbs are presented in Tables 10.9 and 10.10 and further summarized in Table 10.11. These estimates were obtained by multiplying the estimated new floor-space and floorspace utilizing these technologies in retrofit capacity by the expected energy savings for each year. These results can be interpreted as being indicative of reasonable minimum expected energy savings due to these technologies.

10.6.3 High Market Penetration Scenarios

It is possible that under certain circumstances, efficient lighting technologies might penetrate the market more rapidly than outlined in the base case scenario. Possible circumstances would include government or utility subsidization of the technologies, increases in electric rates or drops in the incremental costs of the efficient technologies over their standard counterparts.

TABLE 10.8. Low Scenario Market Share Penetration Estimates for Energy Saving Fluorescent Lamps and Electronic Ballasts (percent of total annual sales)

<u>Year</u>	<u>Electronic Ballasts</u>	<u>Energy Saving Fluorescent Lamps</u>
1984	7	7
1985	7.5	7.5
1990	12	13
1995	21	23.5
2000	24.4	28

**TABLE 10.9. Low Scenario Annual Market Share and Energy Savings
Projections for Electronic Ballasts**

Year	Total Estimated Commercial Fluorescent Floorspace ^(a) (10 ⁶ ft ²)	Total New Fluorescent Floorspace ^(b) (10 ⁶ ft ²)	Fluorescent Floorspace Replacing Conventional Technology ^(c) (10 ⁶ ft ²)	Market Share for For Energy Efficient Technology Units ^(d)	Annual Floorspace Additions Employing New Technology ^(e)	Cumulative Floorspace Additions Employing New Technology ^(f)	Cumulative Annual Energy Savings ^(g) (BkWh)
1984	35,490	1,400	4,262	0.07	396	396	0.35
1985	36,610	1,120	4,436	0.08	417	813	0.72
1986	37,730	1,120	4,576	0.08	456	1,268	1.12
1987	38,780	1,050	4,716	0.09	490	1,759	1.55
1988	39,690	910	4,848	0.10	547	2,306	2.03
1989	40,600	910	4,961	0.11	616	2,922	2.57
1990	41,510	910	5,075	0.12	718	3,640	3.20
1991	42,350	840	5,189	0.14	814	4,454	3.92
1992	43,190	840	5,294	0.16	951	5,405	4.76
1993	44,030	840	5,399	0.18	1,092	6,497	5.72
1994	44,240	910	5,504	0.20	1,283	7,779	6.85
1995	45,990	1,050	5,530	0.21	1,382	9,161	8.06
1996	46,900	910	5,749	0.22	1,465	10,626	9.35
1997	47,880	980	5,863	0.23	1,574	12,200	10.74
1998	48,790	910	5,985	0.24	1,620	13,820	12.16
1999	49,770	980	6,099	0.24	1,699	15,519	13.66
2000	50,750	980	6,221	0.24	1,757	17,276	15.20

- (a) Fluorescent floorspace estimate based on EIA estimates for commercial floorspace (DOE 1984) multiplied by estimate of portion that is fluorescently lit of .70 (Pacific Gas and Electric 1982). It is assumed that there will be no commercial floorspace retirements.
- (b) Calculated by fluorescent floorspace estimate for current year minus estimate for previous year. 1983 floorspace estimate is 48,700 x 10⁶ ft² (DOE 1984).
- (c) Based on assumption that ballasts are to be replaced every eight years. Calculated by: (Estimated Floorspace for previous year) x (.125).
- (d) Based on Methodology presented in Chapter 4.0 and assumptions presented in this chapter.
- (e) Calculated by: (Floorspace replacing conventional technology + Floorspace additions employing new technology) x (Market Share)
- (f) Calculated by: (Current years additions + previous years cumulative additions).
- (g) Calculated by: Cumulative additions of New Technology) x (.88 kWh).

TABLE 10.10. Low Scenario Annual Market Share and Energy Savings Projections for Energy-Efficient Fluorescent Bulbs

Year	Total Estimated Commercial Fluorescent Floorspace ^(a) (10 ⁶ ft ²)	Total New Fluorescent Floorspace ^(b) (10 ⁶ ft ²)	Fluorescent Floorspace Replacing Conventional Technology ^(c) (10 ⁶ ft ²)	Market Share for Energy Efficient Technology Units ^(d)	Annual Floorspace Additions Employing New Technology ^(e)	Cumulative Floorspace Additions Employing New Technology ^(f)	Cumulative Annual Energy Savings ^(g) (BkWh)
1984	35,757	1,400	6,818	0.07	575	575	0.30
1985	52,300	1,120	7,149	0.08	620	1,195	0.63
1986	53,900	1,120	10,460	0.08	926	2,122	1.12
1987	55,400	1,050	10,780	0.09	1,065	3,186	1.68
1988	56,700	910	11,080	0.10	1,199	4,385	2.32
1989	58,000	910	11,340	0.12	1,409	5,794	3.07
1990	59,300	910	11,600	0.13	1,626	7,420	3.93
1991	60,500	840	11,860	0.15	1,905	9,325	4.94
1992	61,700	840	12,100	0.17	2,200	11,525	6.10
1993	62,900	840	12,340	0.20	2,636	14,161	7.50
1994	63,200	910	12,580	0.22	2,968	17,129	9.07
1995	65,700	1,050	12,640	0.24	3,217	20,346	10.78
1996	67,000	910	13,140	0.25	3,442	23,788	12.60
1997	68,400	980	13,400	0.26	3,667	27,455	14.55
1998	69,700	910	13,680	0.27	3,866	31,322	16.60
1999	71,100	980	13,940	0.28	4,103	35,425	18.77
2000	72,500	980	14,220	0.28	4,256	39,681	21.03

- (a) Fluorescent floorspace estimate based on EIA estimates for commercial floorspace (DOE 1984) multiplied by estimate of portion that is fluorescently lit of .70 (Pacific Gas and Electric 1982). It is assumed that there will be no commercial floorspace retirements.
- (b) Calculated by fluorescent floorspace estimate for current year minus estimate for previous year. 1983 floorspace estimate is 48,700 x 10⁶ ft² (DOE 1984).
- (c) Based on assumption that lamps are to be replaced every five years. Calculated by: (Estimated Floorspace for previous year) x (.2).
- (d) Based on Methodology presented in Chapter 4.0 and assumptions presented in this chapter.
- (e) Calculated by: (Floorspace replacing conventional technology + Floorspace additions employing new technology) x (Market Share).
- (f) Calculated by: (Current years additions + previous years cumulative additions).
- (g) Calculated by: Cumulative additions of New Technology x (.53 kWh).

TABLE 10.11. Low Market Penetration Scenario Energy Savings
Results: Electronic Ballasts and High
Efficiency Fluorescent Lamps

<u>Year</u>	<u>Estimated Annual Energy Savings From Electronic Ballasts (BkWh)</u>	<u>Estimated Annual Energy Savings from High Efficiency Fluorescent Lamps (BkWh)</u>	<u>Total For Both Technologies</u>
1985	.72	.63	1.35
1990	3.20	3.93	7.13
1995	8.06	10.78	18.84
2000	15.20	21.03	36.23

Specifically the high market penetration scenario assumes that the maximum market share is attained by 1995 instead of 2000. Table 10.12 displays the expected market penetration for both energy saving fluorescent lamps and electronic ballasts under this scenario.

10.6.4 National Annual Electrical Energy Savings Estimates - High Scenario

The national annual electrical energy savings estimates for the high market penetration scenario for electronic ballasts and high efficiency fluorescent bulbs are displayed in Tables 10.13 and 10.14 and further summarized in Table 10.15. These estimates were derived in the same manner as the low scenario estimates. These results can be interpreted as being indicative of reasonable maximum expected energy savings due to the adoption of these technologies.

10.6.5 Lower Usage Scenario

Throughout our analysis we have assumed annual usage of both energy-saving fluorescent lamps and electronic ballasts at 4000 hours a year. The amount of usage either product gets would directly affect the resulting payback period of the investment in energy saving technologies. This would in turn influence the rate of market penetration. In this scenario we will assume usage of 2600 hours a year. This may more closely represent average commercial sector use that the 4000 hours a year used previously.

TABLE 10.12. High Scenario Market Share Estimates for Energy Saving Fluorescent Lamps and Electronic Ballasts (percent of total annual sales)

<u>Year</u>	<u>Electronic Ballasts</u>	<u>Energy Saving Fluorescent Lamps</u>
1984	10	10
1985	12	13
1990	42	48
1995	95	95
2000	95	95

For electronic ballasts, this level of usage would imply annual electricity savings of 62.9 kWh based on the assumptions made in Section 10.3.1. With a commercial sector electricity price of 7.01¢/kWh the savings would equal \$4.37 a year. This implies a payback period of 3.2 years based on an incremental cost of \$14 for electronics ballasts. For energy-saving fluorescent bulbs, 2600 hours annual usage would imply annual energy saving of 15.6 kWh equal to \$1.10 at commercial sector electricity prices of 7.01¢/kWh. Assuming the incremental capital cost of \$1.23 stated in Section 10.32, the payback period would equal 1.12 years, or approximately 13 months.

Market penetration is assumed to be more a function of payback period than of the percentage increase in incremental cost as with the base case and low and high market penetration scenarios.

Specifically, the lower usage scenario assumes that electronic ballasts will achieve market penetration of 50 percent by the year 2000 and energy-saving fluorescent bulbs will achieve 70 percent market penetration. Table 10.16 displays the expected market penetration for both energy saving fluorescent lamps and electronic ballasts under this scenario.

10.6.6 National Annual Electrical Energy Savings Estimates-Lower Usage Scenario

The national annual electrical energy savings for the lower usage scenario for electric ballasts and high efficiency fluorescent bulbs are displayed in Tables 10.17 and 10.18 and further summarized in Table 10.19.

TABLE 10.13. High Scenario Annual Market Share and Energy Savings Projections for Electronic Ballasts

Year	Total Estimated Commercial Fluorescent Floorspace ^(a) (10 ⁶ ft ²)	Total New Fluorescent Floorspace ^(b) (10 ⁶ ft ²)	Fluorescent Floorspace Replacing Conventional Technology ^(c) (10 ⁶ ft ²)	Market Share for Energy Efficient Technology Units ^(d)	Annual Floorspace Additions Employing New Technology ^(e)	Cumulative Floorspace Additions Employing New Technology ^(f)	Cumulative Annual Energy Savings ^(g) (BkWh)
1984	35,747	1,400	4,262	0.10	566	566	0.50
1985	36,875	1,120	4,468	0.12	469	1,035	0.91
1986	38,003	1,120	4,609	0.15	602	1,637	1.44
1987	39,061	1,050	4,750	0.20	812	2,449	2.16
1988	39,977	910	4,883	0.26	1,054	3,503	3.08
1989	40,894	910	4,997	0.33	1,365	4,868	4.29
1990	41,811	910	5,112	0.42	1,770	6,638	5.84
1991	42,657	840	5,226	0.52	2,208	8,846	7.79
1992	43,503	840	5,332	0.64	2,765	11,612	10.22
1993	44,349	840	5,438	0.75	3,296	14,907	13.12
1994	44,560	910	5,544	0.85	3,840	18,747	16.50
1995	46,323	1,050	5,570	0.95	4,402	23,150	20.37
1996	47,240	910	5,790	0.95	4,456	27,605	24.29
1997	48,227	980	5,905	0.95	4,578	32,184	28.32
1998	49,143	910	6,028	0.95	4,614	36,798	32.38
1999	50,130	980	6,143	0.95	4,737	41,535	36.55
2000	51,118	980	6,266	0.95	4,819	46,353	40.79

- (a) Fluorescent floorspace estimate based on EIA estimates for commercial floorspace (DOE 1984) multiplied by estimate of portion that is fluorescently lit of .70 (Pacific Gas and Electric 1982). It is assumed that there will be no commercial floorspace retirements.
- (b) Calculated by fluorescent floorspace estimate for current year minus estimate for previous year. 1983 floorspace estimate is 48,700 x 10⁶ ft² (DOE 1984).
- (c) Based on assumption that ballasts are to be replaced every eight years. Calculated by: (Estimated Floorspace for previous year) x (.125).
- (d) Based on Methodology presented in Chapter 4.0 and assumptions presented in this chapter.
- (e) Calculated by: (Floorspace replacing conventional technology + Floorspace additions employing new technology) x (Market Share)
- (f) Calculated by: (Current years additions + previous years cumulative additions).
- (g) Calculated by: Cumulative additions of New Technology) x (.88 kWh).

TABLE 10.14. High Scenario Annual Market Share and Energy Savings Projections for Energy-Efficient Fluorescent Lamps

Year	Total Estimated Commercial Fluorescent Floorspace ^(a) (10 ⁶ ft ²)	Total New Fluorescent Floorspace ^(b) (10 ⁶ ft ²)	Fluorescent Floorspace Replacing Conventional Technology ^(c) (10 ⁶ ft ²)	Market Share for Energy Efficient Technology Units ^(d)	Annual Floorspace Additions Employing New Technology ^(e)	Cumulative Floorspace Additions Employing New Technology ^(f)	Cumulative Annual Energy Savings ^(g) (BkWh)
1984	35,490	1,400	6,818	0.10	822	822	0.44
1985	36,610	1,120	7,098	0.13	1,068	1,890	1.01
1986	37,730	1,120	7,322	0.17	1,435	3,325	1.77
1987	38,780	1,050	7,546	0.22	1,891	5,217	2.77
1988	39,690	910	7,756	0.29	2,513	7,730	4.10
1989	40,600	910	7,938	0.38	3,362	11,092	5.88
1990	41,510	910	8,120	0.48	4,334	15,426	8.18
1991	42,350	840	8,302	0.60	5,485	20,912	11.09
1992	43,190	840	8,470	0.71	6,610	27,522	14.59
1993	44,030	840	8,638	0.81	7,677	35,199	18.66
1994	44,240	910	8,806	0.90	8,744	43,943	23.29
1995	45,990	1,050	8,848	0.95	9,403	53,346	28.28
1996	46,900	910	9,198	0.95	9,603	62,949	33.37
1997	47,880	980	9,380	0.95	9,842	72,791	38.58
1998	48,790	910	9,576	0.95	9,962	82,753	43.86
1999	49,770	980	9,758	0.95	10,201	92,954	49.27
2000	50,750	980	9,954	0.95	10,387	103,341	54.78

- (a) Fluorescent floorspace estimate based on EIA estimates for commercial floorspace (DOE 1984) multiplied by estimate of portion that is fluorescently lit of .70 (Pacific Gas and Electric 1982). It is assumed that there will be no commercial floorspace retirements.
- (b) Calculated by fluorescent floorspace estimate for current year minus estimate for previous year. 1983 floorspace estimate is $48,700 \times 10^6 \text{ ft}^2$ (DOE 1984).
- (c) Based on assumption that lamps are to be replaced every five years. Calculated by: (Estimated Floorspace for previous year) $\times$ (.2).
- (d) Based on Methodology presented in Chapter 4.0 and assumptions presented in this chapter.
- (e) Calculated by: (Floorspace replacing conventional technology + Floorspace additions employing new technology) $\times$ (Market Share)
- (f) Calculated by: (Current years additions + previous years cumulative additions).
- (g) Calculated by: Cumulative additions of New Technology) $\times$ (.53 kWh).

TABLE 10.15. High Market Penetration Scenario Energy Savings Results

<u>Year</u>	<u>Estimated Annual Energy Savings from Electronic Ballasts (BkWh)</u>	<u>Estimated Annual Savings from High Efficiency Electronic Ballasts (BkWh)</u>	<u>Total For Both Technologies</u>
1985	.91	1.01	1.92
1990	5.84	8.18	14.02
1995	20.37	28.28	48.65
2000	40.79	54.78	95.57

TABLE 10.16. Lower Scenario Market Penetration Estimates for Energy Saving Fluorescent Lamps and Electronic Ballasts (percent market share)

<u>Year</u>	<u>Electronic Ballasts</u>	<u>Energy Saving Fluorescent Lamps</u>
1984	10	10
1985	11	12
1990	25	35
1995	40	60
2000	50	70

10.7 COST PER KWH OF ENERGY SAVED CALCULATIONS AND COMPARISONS TO THE COST PER KWH OF PRODUCTION NEW GENERATING CAPACITY

Comparisons of the levelized costs per kWh for energy efficient fluorescent lamps and electronic ballasts are presented in this section. Representative estimates of the levelized costs per kWh saved by these technologies are presented in Table 10.20. These estimates are based upon new and replacement installations. Retrofit installations would yield slightly higher levelized costs per kWh saved as the undepreciated portion of the equipment being replaced would be added to the incremental capital costs.

The resulting costs per kWh saved with electronic ballasts and energy efficient fluorescent lamps is equivalent to 2.18¢ and 1.29¢, respectively. This is significantly less than the estimated average generation cost for new coal-fired generating plants of 5.82¢/kWh (presented in Table 4.3).

TABLE 10.17. Low Usage (2600/hours/year) Scenario Annual Market Share and Energy Savings Projections for Electronic Ballasts

Year	Total Estimated Commercial Fluorescent Floorspace ^(a) (10 ⁶ ft ²)	Total New Fluorescent Floorspace ^(b) (10 ⁶ ft ²)	Fluorescent Floorspace Replacing Conventional Technology ^(c) (10 ⁶ ft ²)	Market Share for Energy Efficient Technology Units ^(d)	Annual Floorspace Additions Employing New Technology ^(e)	Cumulative Floorspace Additions Employing New Technology ^(f)	Cumulative Annual Energy Savings ^(g) (BkWh)
1984	35,490	1,400	2,727	0.10	413	413	0.36
1985	36,610	1,120	2,839	0.11	436	849	0.74
1986	37,730	1,120	2,929	0.13	526	1,375	1.21
1987	38,780	1,050	3,018	0.16	651	2,026	1.78
1988	39,690	910	3,102	0.18	722	2,748	2.41
1989	40,600	910	3,175	0.21	858	3,606	3.17
1990	41,510	910	3,248	0.25	1,040	4,645	4.08
1991	42,350	840	3,321	0.29	1,207	5,852	5.15
1992	43,190	840	3,388	0.33	1,395	7,247	6.37
1993	44,030	840	3,455	0.36	1,546	8,794	7.73
1994	44,240	910	3,522	0.38	1,684	10,478	9.22
1995	45,990	1,050	3,539	0.40	1,836	12,314	10.83
1996	46,900	910	3,679	0.43	1,973	14,287	12.57
1997	47,880	980	3,752	0.45	2,129	16,416	14.44
1998	48,790	910	3,830	0.47	2,228	18,644	16.40
1999	49,770	980	3,903	0.49	2,393	21,037	18.51
2000	50,750	980	3,982	0.50	2,481	23,518	20.69

- (a) Fluorescent floorspace estimate based on EIA estimates for commercial floorspace (DOE 1984) multiplied by estimate of portion that is fluorescently lit of .70 (Pacific Gas and Electric 1982). It is assumed that there will be no commercial floorspace retirements.
- (b) Calculated by fluorescent floorspace estimate for current year minus estimate for previous year. 1983 floorspace estimate is 48,700 x 10⁶ ft² (DOE 1984).
- (c) Based on assumption that ballasts are to be replaced every eight years. Calculated by: (Estimated Floorspace for previous year) x (.125).
- (d) Based on Methodology presented in Chapter 4.0 and assumptions presented in this chapter.
- (e) Calculated by: (Floorspace replacing conventional technology + Floorspace additions employing new technology) x (Market Share)
- (f) Calculated by: (Current years additions + previous years cumulative additions).
- (g) Calculated by: Cumulative additions of New Technology) x (.88 kWh).

TABLE 10.18. Low Usage (2600 hours/year) Scenario Annual Market Share and Energy Savings Projections for Fluorescent Lamps

Year	Total Estimated Commercial Fluorescent Floorspace ^(a) (10 ⁶ ft ²)	Total New Fluorescent Floorspace ^(b) (10 ⁶ ft ²)	Fluorescent Floorspace Replacing Conventional Technology ^(c) (10 ⁶ ft ²)	Market Share for Energy Efficient Technology Units ^(d)	Annual Floorspace Additions Employing New Technology ^(e)	Cumulative Floorspace Additions Employing New Technology ^(f)	Cumulative Annual Energy Savings ^(g) (BkWh)
1984	35,490	1,400	4,432	0.10	583	583	0.31
1985	36,610	1,120	4,614	0.12	688	1,271	0.67
1986	37,730	1,120	4,759	0.15	882	2,153	1.14
1987	38,780	1,050	4,905	0.19	1,131	3,284	1.74
1988	39,690	910	5,041	0.24	1,428	4,713	2.50
1989	40,600	910	5,160	0.29	1,760	6,473	3.43
1990	41,510	910	5,278	0.35	2,166	8,639	4.58
1991	42,350	840	5,396	0.42	2,619	11,258	5.97
1992	43,190	840	5,506	0.48	3,046	14,304	7.58
1993	44,030	840	5,615	0.52	3,356	17,660	9.36
1994	44,240	910	5,724	0.56	3,715	21,375	11.33
1995	45,990	1,050	5,751	0.60	4,081	25,456	13.49
1996	46,900	910	5,979	0.63	4,340	29,796	15.79
1997	47,880	980	6,097	0.65	4,600	34,396	18.23
1998	48,790	910	6,224	0.67	4,780	39,176	20.76
1999	49,770	980	6,343	0.69	5,053	44,229	23.44
2000	50,750	980	6,470	0.70	5,215	49,444	26.21

- (a) Fluorescent floorspace estimate based on EIA estimates for commercial floorspace (DOE 1984) multiplied by estimate of portion that is fluorescently lit of .70 (Pacific Gas and Electric 1982). It is assumed that there will be no commercial floorspace retirements.
- (b) Calculated by fluorescent floorspace estimate for current year minus estimate for previous year. 1983 floorspace estimate is 48,700 x 10⁶ ft² (DOE 1984).
- (c) Based on assumption that lamps are to be replaced every five years. Calculated by: (Estimated Floorspace for previous year) x (.2).
- (d) Based on Methodology presented in Chapter 4.0 and assumptions presented in this chapter.
- (e) Calculated by: (Floorspace replacing conventional technology + Floorspace additions employing new technology) x (Market Share)
- (f) Calculated by: (Current years additions + previous years cumulative additions).
- (g) Calculated by: Cumulative additions of New Technology) x (.53 kWh).

TABLE 10.19. Lower Usage Scenario Energy Savings Results

Year	Electronic Ballasts (BkWh)	Energy Saving Fluorescent Lamps (BkWh)	Total for Both Technologies
1985	.74	.67	1.41
1990	4.08	4.58	8.64
1995	10.83	13.49	24.32
2000	20.69	26.21	46.90

TABLE 10.20. Cost per kWh for Electronic Ballasts and Energy Efficient Fluorescent Lamps in New and Retirement Situations

Technology	Incremental Capital Costs in New and Retirement Applications ^(a)	Levelized Capital Cost (\$/year) ^(b)	Annual Energy Savings (kWh/year) ^(c)	Cost Per kWh Saved (\$/kWh) ^(d)
Electronic Ballasts	\$14.00	\$2.09	96	2.18
Energy Efficient Fluorescent Lamps	1.23	.31	24	1.29

- (a) The incremental capital cost is equivalent to the difference between the average cost for the advanced technologies and the base case technologies as cited in this chapter.
- (b) The level stream of annual payments, the present value of which would equal the investment's incremental capital costs. This cost was calculated using an 8 percent discount rate and operating lifetimes of 10 years for electronic ballasts and 5 years for energy efficient fluorescent lamps.
- (c) Calculated as savings in watts times the assumed 4000 hours of operation a year.
- (d) Calculated as the levelized capital cost (\$/year) divided by annual energy savings in kWh/year and multiplied by 100.

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11.0 HEAT AND COOL STORAGE IN COMMERCIAL BUILDINGS

In this chapter, the potential national electrical energy savings in the years 1990, 1995, and 2000 from heat and cool storage techniques for commercial space conditioning is estimated. The principal objective of any space conditioning system is to maintain the living space temperature within some predetermined "comfort zone." When used in combination with conventional heating and cooling systems, modern thermal storage systems can provide a means of meeting that objective while significantly reducing its cost by using cheaper off-peak rather than peak power.

Section 11.1 is a technical review of how commercial storage systems work. The current level of utilization of thermal storage systems is discussed in Section 11.2 while Section 11.3 is an analysis of their cost effectiveness and potential for penetrating the commercial space conditioning market. Section 11.4 applies commercial building stock forecasts to the market penetration estimates to approximate future yearly installations of heat and cool storage systems. The potential national electrical energy savings results are presented in Section 11.5. Section 11.6 is an analysis of the sensitivity of the energy savings results to alterations in the market penetration scenarios. Finally, Section 11.7 presents the estimated cost per kWh saved by thermal storage systems and discusses how those costs compare with the cost per kWh of new electrical generating capacity.

11.1 TECHNICAL BACKGROUND

Cool storage is not a common technology but neither is it a new technology. In the earlier decades of this century, ice was cut from frozen lakes and ponds and then stored in the basements of banks, hotels, department stores, and other commercial buildings. As the ice melted during the hot summer months, the cool water was collected in tanks and pumped to devices called "air washers." These devices forced air over a chilled water spray and circulated the cooled air throughout the building.

By the mid-1930's small air conditioning (AC) units had arrived on the space conditioning market. However, those AC units were not practical for all

uses. For example, some large buildings such as auditoriums and churches required the capacity to produce a lot of cooling for only a few hours a week. In such a case, it would have been difficult to justify the purchase of an AC unit of sufficient size and capacity because it would have been used so infrequently. One solution was to employ a cool storage technique called "ice banking."

The technique of ice banking used modestly sized refrigeration units to produce ice all week long. The ice was collected and stored until it came time for the building to be cooled. Air or water was then chilled over the ice and subsequently blown or pumped throughout the building to effectively provide the necessary cooling. Such systems were common until the 1950s when large AC units became less costly to purchase and to operate.

Modern cool storage systems are used primarily to support the cooling capacity of conventional AC systems. They operate in much the same way as the ice-banking system described above. In addition to a modern version of the ice-storage system (see Figure 11.1), there are also the very similar chilled-water storage systems (see Figure 11.2), and the somewhat different chilled-air storage systems.

Chilled-air storage systems utilize the infrastructure of the building (i.e., the space between the walls, beneath the floors, above the ceiling panels, and in the hollow cores of concrete pillars and floor slabs) to store a reserve of pre-cooled air. When the time comes to use it, the reserve of cool air is vented into the central duct system and subsequently distributed throughout the building.

One reason why these systems may use less energy than strictly conventional AC systems is because the cooling capacity is produced overnight. Energy is saved because night air is cooler to begin with than mid-day air so it requires less energy input for further cooling to a desired temperature.

Another reason why cool storage systems conserve energy is because they allow the installation of smaller or "downsized" conventional AC systems. That is, because a cool storage system can be held in reserve until the work day's

Ice Storage

During off-peak periods, compressors compress a refrigerant that is circulated through evaporator coils submerged in a tank of water. As the refrigerant expands, it absorbs heat, and a sheath of ice builds up around the coils (some ice systems spray water on the evaporator coils and harvest thin layers of ice instead). When cooling is required, the cold water in the tank is circulated through the building's cooling coils.

FIGURE 11.1. Ice Storage (EPRI 1983)

Chilled-Water Storage

During off-peak periods, water is chilled by the chiller's compressors and pumped to the storage tank. When peak period cooling is required, the chilled water is pumped through the building's cooling coils or through a heat exchanger that cools the water in those coils.

FIGURE 11.2. Chilled-Water Storage (EPRI 1983)

period of peak cooling demand, it can be used as a support system of a conventional AC unit. Consequently, the conventional AC unit does not need to be sized to worst-case conditions. Power is conserved because for a given level of cooling, a downsized AC unit operated mostly at full capacity requires less energy input than a larger AC unit operated mostly at less than full capacity.

The primary benefit of a thermal storage system is, however, economy rather than conservation because it uses considerably cheaper off-peak power to operate. This is significant since statistics indicate that space cooling of commercial buildings uses 25 to 40 percent of the summer season's peak load electrical production (EPRI 1983).

It is important to recognize that many types of thermal storage systems can serve the dual purpose of storing heat as well as cool. Under certain conditions, this dual purpose can significantly contribute to the overall economy of such systems (Tamblyn 1982). That is, modern commercial buildings typically require year-round cooling on almost a daily basis so cooling is usually a matter of more serious concern than heating. But even large commercial buildings require some heating on holidays, weekends, Monday mornings, and during the evenings of the winter. A thermal storage space heating system can usually be employed to meet some of these heating requirements by capturing and storing the excess "waste heat" generated within the building during the active part of the work week.

There are various means of storing the waste heat until it is needed. One such method is to use the heat to warm large tanks of water which, when needed, can be pumped to the peripheral areas of the building. Another method is to use the waste heat to warm a large mass of brick or even the hollow-core concrete of the building structure itself. During the peak heating period a fan can push air through the core of the brick or concrete mass to be warmed and subsequently delivered to the living/working space.

Probably the most common method of heat storage is the heating of a concrete floor slab of a one-story commercial building. Often this is accomplished with electrical resistance cable or heating mats placed directly into the concrete. Alternatively, a reservoir of heat can be stored somewhat beneath the concrete floor slab as well as within it. With a layer of sand or

rock between the heating element and the bottom of the floor slab, the heat storage capacity of the system is effectively increased.

Yet another alternative method is by circulating heated water through pipes that have been embedded in the floor slab. When the water for such a system is heated either with what otherwise would have been waste heat or with heat collected by solar panels, there is more of a potential for energy savings.

Heating with heat that otherwise would have been wasted reduces costs and saves energy directly. In addition, a building with a thermal storage system need not have conventional heating equipment that is sized to worst-case conditions because of the load-leveling capabilities of the thermal storage system. Hence, these systems use somewhat less energy than conventional electric heating, ventilating, and air conditioning (HVAC) systems. They are, however, also primarily designed to shift the heating energy load to the off-peak hours.

11.2 CURRENT MARKET SITUATION

Despite the combined incentives of energy savings and off-peak cost of energy savings, thermal storage has not yet become a popular commercial space conditioning option.

According to one report, cool storage technology is presently being used in approximately 100 commercial buildings in the United States, with more under construction (EPRI 1983). However, even with this many cool storage systems presently in operation, there is still surprisingly little information available on their design, performance, economics, operation, and maintenance. Apparently, only a few of the new installations have been monitored for performance in these respects.

It seems that due to the paucity of good information on these systems, the consulting engineers and architects for new commercial buildings still prefer to recommend the installation of conventional HVAC units (EPRI 1983). That is, even though thermal storage systems are not excessively complicated, consulting engineers and building architects are generally unfamiliar with them and regard conventional HVAC units as tried-and-true systems for achieving their design

objectives. Furthermore, it is likely that this attitude will prevail unless the engineer, architect, or building owner becomes aware of thermal storage space conditioning options (Tamblyn 1982).

The facilities at the Equitec Properties Company's Los Angeles World Trade Center and at the Union Oil Company of California's Fred L. Hartley Research Center in Brea, California are two notable examples of thermal storage installations. Also, the engineering firms of Engineering Interface, Ltd., Ontario, Canada, and of Thomas Gilbertson and Associates, Moraga, California are two principals in design and installation of thermal storage systems.

An informed estimate of the total number of floor-slab type thermal storage installations presently in operation could not be found. However, the Mayfran, Inc., building of Cleveland, Ohio is an example of one such installation. Other common trade names for similar systems are Deepheat, Spiroll, Flexicore, Spandeck, Sponcrete, Thermodeck, and Airfloor of California.

11.3 COST EFFECTIVENESS AND MARKET PENETRATION

In this section, an example of an assumed prototypical commercial building will be described and analyzed for the potential energy savings and consequent cost savings that could be realized from the installation of a particular thermal storage heating and cooling system. These estimates are then used to calculate of the degree to which such systems may penetrate the commercial building space conditioning market by the year 2000.

11.3.1 Cost Effectiveness

Commercial buildings vary a great deal in terms of their physical characteristics (i.e., size, building configuration, and location, etc.) and, consequently, in terms of their heating and cooling load requirements as well. Therefore, for a generalized analysis of this sort, it becomes necessary to establish a benchmark set of characteristics which could conceivably be representative of a typical commercial building in the United States.

Veronika Rabl, manager of cool storage research projects in EPRI's Energy Management and Utilization Division, suggested a hypothetical 100,000-ft² building might be considered appropriate (EPRI 1983). By her estimate, such a

conventionally cooled office building would have a load profile that would peak at about 200 kW during a peak demand period. Alternatively, she suggests, the installation of 1,000 ton-hours of cool storage (100,000 gallons of chilled water or about 90,000 lb of ice storage) would reduce the peak of the load profile to less than 100 kW. The cool storage system would likely cost between 20 and 40 thousand dollars more than a conventional full-sized HVAC system. However, such a system would result in about \$7,000 to \$9,000 saved annually due to the lower rates for off-peak power. These savings would be in addition to the cost savings due to reduced energy consumption. For this analysis, the higher incremental capital cost figure (i.e., \$40,000) is considered to be a more appropriate figure. This is because the higher figure appears to be more representative of cost estimates for similar systems from other sources (see Ayres 1982 and Cassedy 1982).

With regard to cost savings due to an actual reduction of energy consumption, Rabl reports that those are likely to be minimal.^(a) Because in the present analysis we are interested in the maximum potential for energy savings, we will use Thomas Gilbertson's estimate that actual electrical power consumption for cooling will be reduced by 5 percent due to nighttime operation and downsized conventional AC units.^(b)

The same thermal storage system described above for cooling may be operated in reverse when the heating of the facility is called for. That is, rather than discarding whatever surplus heat a commercial building might generate during an active winter work week, the heat can be collected in the thermal storage system for later redistribution back into the building when the heating of the facility is called for. Using such a system could potentially reduce the electrical heating requirements of the building by up to 20 percent.^(c)

To determine the actual cost and energy savings contribution such a system might result in, some other pieces of relevant information must be employed.

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- (a) Personal communication with Veronika Rabl of EPRI on January 17, 1985.
 - (b) Personal communication with Thomas Gilbertson of Thomas Gilbertson and Associates, Manager, California on January 17, 1985.
 - (c) Personal communication with Robert Paterson of Cleveland Electrical Illuminating Systems on January 17, 1985.

It has been reported that the estimated average annual electrical energy use per square foot of commercial space for 1984 was 36.185 kWh (EIA 1984). Also, it has been estimated that 30.3 percent of that electricity is used for cooling and 19.6 percent is used for heating (DOE 1984). Hence, the prototypical 100,000 square foot commercial building would use an annual average of 1,096,405 kWh for cooling and 528,301 kWh for heating (i.e., total kWh/sq ft x percent used for cooling or heating x 100,000 sq ft/building). Upon the installation and optimal operation of the above described thermal storage system, electrical consumption for cooling could be reduced by 54,820 kWh (5 percent of 1,096,405 kWh) and for heating by 105,660 kWh (20 percent of 528,301 kWh). At an average 1983 price of electricity of 7.01¢ per kWh these energy savings represent reductions in energy expenditures of \$3,892 per year for cooling and \$7,502 per year for heating. The reader will recall that these cost savings are in addition to the \$8,000 reported by Rabl (EPRI 1983) due to the use of cheaper off-peak power. Hence, the total maximum annual energy cost savings would be in the range of \$19,250. For a system with an incremental capital cost of \$40,000, these savings represent an approximate two-year payback period.

11.3.2 Market Penetration

At present, it appears that the market penetration potential of thermal storage systems will be moderated by the inherent uncertainties that accompany a new technology. One of the more important questions relates to the appropriate selection of system size and design. This being because commercial buildings vary greatly in their size and function and, consequently, their space conditioning requirements. Other important questions pertain to the operation and the maintenance of such systems which, although not necessarily more complex than conventional HVAC systems, are still far from being widely understood. Basically, the new thermal storage systems are still not well enough understood by building designers to allow proper system fitting and operation for a specific application.

Another serious constraint to the more widespread use of such systems is that in most cases they could not be retrofitted into an existing structure. The tanks of a water or ice storage system are likely to be of such a size as

to require more space than what could be made available for them and a floor slab system almost certainly would require installation at the time of building construction. Therefore, the market penetration of such systems is restricted to applications in newly constructed buildings.

Keeping these limitations in mind, the reader is referred to Table 4.2 which, for a two year payback, provides an estimate of 65 percent for the maximum percent rate of market penetration. The results of the entire foregoing analysis are presented in Table 11.1.

11.4 COMMERCIAL BUILDING STOCK AND MARKET SHARE PROJECTIONS

In this section, a forecast of future additions to total national commercial floor space (DOE/EIA 1984) is employed to estimate the number of square feet of commercial building space likely to be serviced by thermal storage systems in each of the years 1984-2000. Since virtually all commercial space cooling is done with electric power while only about 30 percent of commercial space heating is done with electric power (DOE 1984), it was necessary to perform two separate market penetration estimations. Table 11.2 presents estimates for the commercial floorspace that is both electrically heated and cooled and Table 11.3 presents estimates for the remainder of the commercial floorspace, which is electrically cooled but not electrically heated. The market share estimates are derived as described in Chapter 4.0 and are based on the payback period and maximum market penetration estimates presented in Table 11.1.

While noting these estimates, the reader is encouraged to keep in mind that they represent a potential market penetration scenario that should be regarded as being subject to the technical limitations described above. The reader will also note that a market for the retrofitting of thermal storage units into existing structures is assumed to be nonexistent.

11.5 NATIONAL ENERGY SAVINGS

Thermal storage systems can contribute to the reduction of electricity consumption for the purpose of commercial space conditioning. The intent of this section is to use the above per-unit savings estimates and national market

TABLE 11.1. Payback Calculations of a Thermal Storage System for a 100,000 Square Foot Commercial Building

	Base Case Conventional HVAC System	New Building With Built-in Thermal Storage System
Incremental Capital Cost (\$) ^(a)	--	40,000
Energy Savings (Percent)		
Heating ^(b)	--	20
Cooling ^(c)	--	5
Annual Energy Consumption for 100,000 Square Feet ^(d)		
Heating (kWh)	528,301	422,641
Cooling (kWh)	<u>1,096,405</u>	<u>1,041,585</u>
Total Heating and Cooling (kWh)	1,624,706	1,464,226
Energy Cost (cents per kWh) ^(e)	7.01	7.01
Annual Fuel Bill ^(f)		
Heating (\$/yr)	37,034	29,627
Cooling (\$/yr)	<u>76,858</u>	<u>73,015</u>
Total Heating and Cooling (\$/yr)	113,892	102,642
Off-Peak Cost Savings (\$/yr) ^(g)	<u>--</u>	<u>-8,000</u>
Total Annual Fuel Bill (\$/yr)	113,892	94,642
Annual Savings on Fuel Bill (\$/yr)	--	19,250
Simple Payback Period (yr) ^(h)	--	2
Maximum Market Penetration (Percent) ⁽ⁱ⁾	--	65

(a) EPRI 1983 (in 1983 dollars).

(b) Personal communication with Robert Paterson, Cleveland Electrical Illuminating system, January 17, 1985.

(c) Personal communication with Thomas Gilbertson of Thomas Gilbertson and Associates, Moraga, California on January 17, 1985.

(d) Derived from EIA 1984 and DOE 1984.

(e) EIA 1984.

(f) Kilowatt hours times cents per kWh.

(g) EPRI 1983.

(h) Rounded to nearest complete year.

(i) See Table 4.2. Also, the reader is reminded to consider the market limitations discussed in the above text. Hence, this is a MAXIMUM potential figure.

TABLE 11.2. Commercial Floorspace Projections and Thermal Storage Market Share Estimates for Electrically Heated and Cooled Buildings

Year	Total Commercial Floorspace (10 ⁶ ft ²) (a)	Additional New Commercial Floorspace (10 ⁶ ft ²) (a)	Percent Commercial Floorspace Electrically Heated and Cooled (a)	Market Share Estimates (b)	Additional Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (c)	Cumulative Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (d)	Annual Energy Savings from Cumulative Thermal Stor- age Heated and Cooled Floorspace (BkWh)
1984	50,700	2,000	30	0.1	60	60	0.10
1985	52,300	1,600	30	0.12	57.6	117.6	0.19
1986	53,900	1,600	30	0.14	67.2	184.8	0.30
1987	55,400	1,500	30	0.17	76.5	261.3	0.42
1988	56,700	1,300	30	0.2	70	339.3	0.54
1989	58,000	1,300	30	0.24	93.6	432.9	0.69
1990	59,300	1,300	30	0.29	113.1	546	0.87
1991	60,500	1,200	30	0.34	122.4	668.4	1.07
1992	61,700	1,200	30	0.4	144	812.4	1.30
1993	62,900	1,200	30	0.46	165.6	978	1.56
1994	64,200	1,300	30	0.51	198.9	1,176.9	1.88
1995	65,700	1,500	30	0.55	247.5	1,424.4	2.28
1996	67,000	1,300	30	0.58	226.2	1,650.6	2.64
1997	68,400	1,400	30	0.6	252	1,902.6	3.04
1998	69,700	1,300	30	0.62	241.8	2,144.4	3.43
1999	71,100	1,400	30	0.64	268.8	2,413.2	3.86
2000	72,500	1,400	30	0.65	273	2,686.2	4.30

(a) DOE 1984.

(b) See Table 11.1 and Chapter 4.0 (assume retrofit market share equals 0).

(c) Calculated by: (Additional New Floorspace) x (Percent Electric) x (Market Share).

(d) Calculated by summing each year's additional thermal storage heated and cooled floorspace to the cumulative number of the previous year.

(e) Calculated by: (Cumulative Floorspace) x (1.60 kWh/ft²).

TABLE 11.3. Commercial Floorspace Projections and Thermal Storage Market Share Estimates for Electrically Cooled Buildings

Year	Total Commercial Floorspace, (10 ⁶ ft ²) (a)	Additional New Commercial Floorspace, (10 ⁶ ft ²) (a)	Percent Commercial Floorspace Electrically Heated and Cooled (a)	Market Share Estimates (b)	Additional Thermal Storage Heated and Cooled Floorspace, (10 ⁶ ft ²) (c)	Cumulative Thermal Storage Heated and Cooled Floorspace, (10 ⁶ ft ²) (d)	Annual Energy Savings from Cumulative Thermal Stor- age Heated and Cooled Floorspace (BkWh)
1984	50,700	2,000	70	0.1	140	140	0.08
1985	52,300	1,600	70	0.12	134.4	274.4	0.15
1986	53,900	1,600	70	0.14	156.8	431.2	0.24
1987	55,400	1,500	70	0.17	170.5	609.7	0.34
1988	56,700	1,300	70	0.2	182	791.7	0.44
1989	58,000	1,300	70	0.24	218.4	1,010.1	0.55
1990	59,300	1,300	70	0.29	260.9	1,274	0.70
1991	60,500	1,200	70	0.34	285.6	1,559.6	0.85
1992	61,700	1,200	70	0.4	336	1,895.6	1.04
1993	62,900	1,200	70	0.46	386.4	2,282	1.25
1994	64,200	1,300	70	0.51	464.1	2,746.1	1.51
1995	65,700	1,500	70	0.55	577.5	3,323.6	1.83
1996	67,000	1,300	70	0.58	527.8	3,851.4	2.11
1997	68,400	1,400	70	0.6	588	4,439.4	2.44
1998	69,700	1,300	70	0.62	364.2	5,003.6	2.75
1999	71,100	1,400	70	0.64	627.2	5,630.8	3.09
2000	72,500	1,400	70	0.65	637	6,267.8	3.45

(a) DOE 1984.

(b) See Table 11.1 and Chapter 4.0 (assume retrofit market share equals 0).

(c) Calculated by: (Additional New Floorspace) x (Percent Electric) x (Market Share).

(d) Calculated by summing each year's additional thermal storage heated and cooled floorspace to the cumulative number of the previous year.

(e) Calculated by: (Cumulative Floorspace) x (0.55 kWh/ft²).

penetration projections to assess the degree to which thermal storage could potentially reduce national electrical consumption in each of the years 1984-2000.

The above described representative 100,000 ft² commercial building that employs a thermal storage system would obtain estimated annual savings of 0.5482 kWh/ft² for cooling services alone and 1.6048 kWh/ft² for both heating and cooling services combined. Therefore, the national annual electrical savings can be computed by multiplying these savings estimates by the projected number of square feet of commercial space conditioned by a thermal storage system (see the final columns of Tables 11.2 and 11.3).

The dichotomy between the cooled-only and the heated-and-cooled combined categories is because commercial space heating is just 30 percent electric, while space cooling is close to 100 percent electric. Hence, the total annual electrical savings is determined by simply combining the projected savings of the two categories for a given year. These national annual electrical energy savings results are presented in Table 11.4.

The estimated electrical power savings in the year 2000 due to thermal storage is 7.75 BkWh. By comparison, the estimated 1984 national total for commercial electrical consumption is 680.22 BkWh (EIA 1984). Hence, the total estimated savings represent approximately 1 percent of the 1984 figure for total consumption. Furthermore, because the above described technical limitations are likely to inhibit the degree of market penetration to less than the estimated maximum of 65 percent, the energy savings are probably over-estimated. It is, however, also important not to let these estimates obscure the more meaningful "load-leveling" contribution of thermal storage systems. The potential for such systems to shift power consumption from peak-use periods to off-peak-use periods helps to alleviate the necessity for building new generating capacity by improving load factors.

It is clear that portions of the above analysis were treated in a somewhat simplistic fashion so that the task could be completed within the available resource limitations. Some of the more consequential simplifications include the employment of a specific scenario of assumed future electrical and product

TABLE 11.4. Estimated National Annual Electrical Savings from New Commercial Thermal Storage Installations (BkWh)

<u>Year</u>	<u>Savings for Commercial Floorspace Electrically Heated and Cooled</u>	<u>Savings for Commercial Floorspace Electrically Cooled Only</u>	<u>Total Electrical Savings of Thermal Storage Systems</u>
1985	0.19	0.15	0.34
1990	0.87	0.70	1.57
1995	2.28	1.83	4.11
2000	4.30	3.45	7.75

prices, assumed market penetration rates, the abstraction from climatic differences, and assumed "representative" technology-related energy savings. Such simplifications, although appropriate within the scope of this analysis, should be kept in mind when one is determining the level of confidence that these estimates deserve. In that regard, it is appropriate to assess the sensitivity of the above results to alterations in the scenario of assumptions.

11.6 SENSITIVITY ANALYSIS

This section is an assessment of the sensitivity of the aggregate energy savings results presented in Section 11.5 to changes in the thermal storage market penetration scenarios. Low and high market penetration scenarios are examined to determine an implied minimum/maximum range of potential future energy savings.

11.6.1 Low Market Penetration Scenario

Thermal storage systems may not penetrate the commercial HVAC market as quickly or as completely as suggested by the above base-case estimates. For example, the previously mentioned technical limitations may inhibit the market penetration of such systems to levels significantly below those that simple cost studies might otherwise imply.

The specific assumption for the low market penetration scenario is that the maximum potential level of penetration is only half of what it was estimated to be in the base case scenario. That is, the maximum potential market

share was reduced from a 0.65 market share to a 0.325 market share. Furthermore, the assumed rate of penetration was reduced such that only 75 percent of that new maximum potential market share will be reached by the year 2000. Tables 11.5 and 11.6 employ that scenario with a forecast of national additions to commercial floorspace to obtain a low penetration estimate of the number of square feet of floorspace that would be space conditioned by a thermal storage system.

11.6.2 National Annual Electrical Energy Savings Estimates - Low Scenario

The national annual electrical energy savings estimates for the low market penetration scenario of thermal storage systems are presented in the final columns of Tables 11.5 and 11.6 and summarized in Table 11.7. The estimates were obtained by multiplying the year's estimated number of square feet of thermal storage space conditioned buildings from the scenario times the estimates of the per unit annual electrical energy savings. These result could be interpreted as being indicative of a reasonable minimum of the expected electrical energy savings from the new thermal storage systems.

11.6.3 High Market Penetration Scenarios

Under certain conditions, thermal storage systems may penetrate the market more rapidly than Tables 11.2 and 11.3 indicate. For example, if the government or certain utilities should decide that it would be a good investment to subsidize the installation of such measures, then the probable number of such installations would be enhanced. Hence, it is proper that the implications of that possibility be further investigated.

Specifically, the high market penetration scenario assumes that the maximum market share is achieved by 1995 instead of by the year 2000. Tables 11.8 and 11.9 combine that scenario with a forecast of future commercial building space to arrive at high penetration estimates of the future number of square feet of thermal storage space conditioned buildings.

11.6.4 National Annual Electrical Energy Savings Estimates - High Scenario

The national annual electrical energy savings estimates for the high market penetration scenario of the thermal storage systems are displayed in Tables 11.8 and 11.9 and summarized in Table 11.10. These estimates were arrived at

TABLE 11.5. Commercial Floorspace Projections and Low Market Share Scenario of Thermal Storage Systems for Electrically Heated and Cooled Buildings

Year	Total Commercial Floorspace (10 ⁶ ft ²) (a)	Additional New Commercial Floorspace (10 ⁶ ft ²) (a)	Percent Commercial Floorspace Electrically Heated and Cooled (a)	Market Share Estimates (b)	Additional Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (c)	Cumulative Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (d)	Annual Energy Savings from Cumulative Thermal Stor- age Heated and Cooled Floorspace (BkWh)
1984	50,700	2,000	30	0.1	60	60	0.1
1985	52,300	1,600	30	0.104	49.92	109.92	0.18
1986	53,900	1,600	30	0.11	52.8	162.72	0.26
1987	55,400	1,500	30	0.12	54	216.72	0.35
1988	56,700	1,300	30	0.13	50.7	267.42	0.43
1989	58,000	1,300	30	0.145	56.55	323.97	0.52
1990	59,300	1,300	30	0.16	62.4	386.37	0.62
1991	60,500	1,200	30	0.18	64.8	451.17	0.72
1992	61,700	1,200	30	0.195	70.2	521.37	0.83
1993	62,900	1,200	30	0.205	73.8	595.17	0.95
1994	64,200	1,300	30	0.212	82.68	677.85	1.08
1995	65,700	1,500	30	0.219	98.55	776.4	1.24
1996	67,000	1,300	30	0.225	87.75	864.15	1.38
1997	68,400	1,400	30	0.23	96.6	960.75	1.54
1998	69,700	1,300	30	0.235	91.65	1,052.4	1.68
1999	71,100	1,400	30	0.24	100.8	1,153.2	1.84
2000	72,500	1,400	30	0.244	102.48	1,255.68	2.01

(a) DOE 1984.

(b) See Table 11.1 and Chapter 4.0 (assume retrofit market share equals 0).

(c) Calculated by: (Additional New Floorspace) x (Percent Electric) x (Market Share).

(d) Calculated by summing each year's additional thermal storage heated and cooled floorspace to the cumulative number of the previous year.

(e) Calculated by: (Cumulative Floorspace) x (1.60 kWh/ft²).

TABLE 11.6. Commercial Floorspace Projections and Low Market Share Scenario of Thermal Storage Systems for Electrically Cooled Buildings

Year	Total Commercial Floorspace (10 ⁶ ft ²) (a)	Additional New Commercial Floorspace (10 ⁶ ft ²) (a)	Percent Commercial Floorspace Electrically Heated and Cooled (a)	Market Share Estimates (b)	Additional Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (c)	Cumulative Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (d)	Annual Energy Savings from Cumulative Thermal Stor- age Heated and Cooled Floorspace (BkWh)
1984	50,700	2,000	70	0.1	140	140	0.08
1985	52,300	1,600	70	0.104	116.48	256.48	0.14
1986	53,900	1,600	70	0.11	123.2	379.68	0.21
1987	55,400	1,500	70	0.12	126	505.68	0.27
1988	56,700	1,300	70	0.13	118.3	623.98	0.34
1989	58,000	1,300	70	0.145	131.95	755.93	0.42
1990	59,300	1,300	70	0.16	145.6	901.53	0.50
1991	60,500	1,200	70	0.18	151.2	1,052.73	0.58
1992	61,700	1,200	70	0.195	163.8	1,216.53	0.67
1993	62,900	1,200	70	0.205	172.2	1,388.73	0.76
1994	64,200	1,300	70	0.212	192.92	1,581.65	0.87
1995	65,700	1,500	70	0.219	229.95	1,811.6	0.99
1996	67,000	1,300	70	0.225	204.75	2,016.35	1.11
1997	68,400	1,400	70	0.23	225.4	2,241.75	1.23
1998	69,700	1,300	70	0.235	213.85	2,455.6	1.35
1999	71,100	1,400	70	0.24	235.2	2,690.8	1.48
2000	72,500	1,400	70	0.244	239.12	2,929.92	1.61

(a) DOE 1984.

(b) See Table 11.1 and Chapter 4.0 (assume retrofit market share equals 0).

(c) Calculated by: (Additional New Floorspace) x (Percent Electric) x (Market Share).

(d) Calculated by summing each year's additional thermal storage heated and cooled floorspace to the cumulative number of the previous year.

(e) Calculated by: (Cumulative Floorspace) x (0.55 kWh/ft²).

TABLE 11.7. Estimated National Annual Electrical Savings from New Commercial Thermal Storage Installations - Low Market Penetration Scenario (BkWh)

<u>Year</u>	<u>Savings for Commercial Floorspace Electrically Heated and Cooled</u>	<u>Savings for Commercial Floorspace Electrically Cooled Only</u>	<u>Total Electrical Savings of Thermal Storage Systems</u>
1985	0.18	0.14	0.32
1990	0.62	0.50	1.13
1995	1.24	0.99	2.23
2000	2.01	1.61	3.62

by multiplying the year's estimated number of square feet of thermal storage space conditioned buildings from the high scenario times the estimates of the per unit annual electrical energy savings from the thermal storage systems. They are representative of a plausible maximum for the expected future electrical energy savings from those systems.

11.7 COST PER KWH OF ENERGY SAVED CALCULATIONS AND COMPARISONS TO THE COST PER KWH OF PRODUCING NEW GENERATION CAPACITY

The thermal storage systems may be considered as investments the return for which is a reduction in the future amount of energy that must be purchased for a given level of space conditioning. If the cost per kWh of those energy savings is less than the cost per kWh of producing that power, then the undertaking of such investments would contribute to both private and social welfare.

The calculations of the cost per kWh saved for heating, cooling, and heating and cooling combined due to thermal storage systems are presented in Table 11.11. These costs may be compared to the national average cost of about 5.82 ¢/kWh for producing new generating capacity from a new coal-fired generating plant (see Table 4.3).

The specific indications are that the costs of new thermal storage installations are significantly less than the cost of new power for the purposes of heating and for heating and cooling combined. In general, it appears that the advanced thermal efficiency measures are likely to be good investments and deserve more detailed consideration on a more regional basis.

TABLE 11.8. Commercial Floorspace Projections and High Market Share Scenario of Thermal Storage Systems for Electrically Heated and Cooled Buildings

Year	Total Commercial Floorspace (10 ⁶ ft ²) (a)	Additional New Commercial Floorspace (10 ⁶ ft ²) (a)	Percent Commercial Floorspace Electrically Heated and Cooled (a)	Market Share Estimates (b)	Additional Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (c)	Cumulative Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (d)	Annual Energy Savings from Cumulative Thermal Stor- age Heated and Cooled Floorspace (BkWh) (e)
1984	50,700	2,000	30	0.1	60	60	0.10
1985	52,300	1,600	30	0.13	62.4	122.4	0.20
1986	53,900	1,600	30	0.17	81.6	204	0.33
1987	55,400	1,500	30	0.22	99	303	0.48
1988	56,700	1,300	30	0.28	109.2	412.2	0.66
1989	58,000	1,300	30	0.35	136.5	548.7	0.88
1990	59,300	1,300	30	0.43	167.7	716.4	1.15
1991	60,500	1,200	30	0.5	180	896.4	1.43
1992	61,700	1,200	30	0.55	198	1,094.4	1.75
1993	62,900	1,200	30	0.59	212.4	1,306.8	2.09
1994	64,200	1,300	30	0.63	245.7	1,552.5	2.48
1995	65,700	1,500	30	0.65	292.5	1,845	2.95
1996	67,000	1,300	30	0.65	253.5	2,098.5	3.36
1997	68,400	1,400	30	0.65	273	2,371.5	3.79
1998	69,700	1,300	30	0.65	253.5	2,625	4.20
1999	71,100	1,400	30	0.65	273	2,898	4.64
2000	72,500	1,400	30	0.65	273	3,171	5.07

(a) DOE 1984.

(b) See Table 11.1 and Chapter 4.0 (assume retrofit market share equals 0).

(c) Calculated by: (Additional New Floorspace) x (Percent Electric) x (Market Share).

(d) Calculated by summing each year's additional thermal storage heated and cooled floorspace to the cumulative number of the previous year.

(e) Calculated by: (Cumulative Floorspace) x (1.50 kWh/ft²).

TABLE 11.9. Commercial Floorspace Projections and High Market Share Scenarios of Thermal Storage Systems for Electrically Cooled Buildings

Year	Total Commercial Floorspace (10 ⁶ ft ²) (a)	Additional New Commercial Floorspace (10 ⁶ ft ²) (a)	Percent Commercial Floorspace Electrically Heated and Cooled (a)	Market Share Estimates (b)	Additional Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (c)	Cumulative Thermal Storage Heated and Cooled Floorspace (10 ⁶ ft ²) (d)	Annual Energy Savings from Cumulative Thermal Storage Heated and Cooled Floorspace (BkWh)
1984	50,700	2,000	70	0.1	140	140	0.08
1985	52,300	1,600	70	0.13	134.4	274.4	0.15
1986	53,900	1,600	70	0.17	168	442.4	0.24
1987	55,400	1,500	70	0.22	199.5	641.9	0.35
1988	56,700	1,300	70	0.28	218.4	860.3	0.47
1989	58,000	1,300	70	0.35	273	1,133.3	0.62
1990	59,300	1,300	70	0.43	336.7	1,470	0.81
1991	60,500	1,200	70	0.5	378	1,848	1.02
1992	61,700	1,200	70	0.55	436.8	2,284.8	1.26
1993	62,900	1,200	70	0.59	487.2	2,772	1.52
1994	64,200	1,300	70	0.63	564.2	3,336.2	1.83
1995	65,700	1,500	70	0.65	682.5	4,018.7	2.21
1996	67,000	1,300	70	0.65	591.5	4,610.2	2.53
1997	68,400	1,400	70	0.65	637	5,247.2	2.89
1998	69,700	1,300	70	0.65	591.5	5,838.7	3.21
1999	71,100	1,400	70	0.65	637	6,475.7	3.56
2000	72,500	1,400	70	0.65	637	7,112.7	3.91

(a) DOE 1984.

(b) See Table 11.1 and Chapter 4.0 (assume retrofit market share equals 0).

(c) Calculated by: (Additional New Floorspace) x (Percent Electric) x (Market Share).

(d) Calculated by summing each year's additional thermal storage heated and cooled floorspace to the cumulative number of the previous year.

(e) Calculated by: (Cumulative Floorspace) x (0.55 kWh/ft²).

TABLE 11.10. Estimated National Annual Electrical Savings from New Commercial Thermal Storage Installations - High Market Penetration Scenario (BkWh)

<u>Year</u>	<u>Savings for Commercial Floorspace Electrically Heated and Cooled</u>	<u>Savings for Commercial Floorspace Electrically Cooled Only</u>	<u>Total Electrical Savings of Thermal Storage Systems</u>
1985	0.20	0.15	0.35
1990	1.15	0.81	1.96
1995	2.95	2.21	5.16
2000	5.07	3.91	8.98

TABLE 11.11. Cost per kWh Calculations of a Thermal Storage System

Incremental Capital Cost^(a) \$40,000

Levelized Capital Cost^(b) \$3,553.10/yr

Annual Energy Savings (kWh/yr)^(a)

Heating = 528,301 - 422,641 = 105,660

Cooling = 1,096,405 - 1,041,585 = 54,820

Heating and Cooling = 1,624,706 - 1,464,226 = 160,480

Cost per kWh (¢/kWh)^(c)

Heating = 355,310/105,660 = 3.36

Cooling = 355,310/54,820 = 6.48

Heating and Cooling = 355,310/160,480 = 2.21

(a) See Table 11.1.

(b) The level stream of annual payments the present value of which would equal the investment's incremental capital cost. Assumes a 30 year useful lifetime of the investment and an 8 percent rate of interest compounded annually.

(c) Levelized Capital Cost (x 100¢/\$)/Annual Energy Savings.

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12.0 HIGH-EFFICIENCY ELECTRIC MOTORS

High-efficiency electric motors have the potential to produce significant electrical energy savings by reducing the internal electrical losses of electric motors. Because most of the electricity used in electric motor drive applications is consumed in the industrial sector, this analysis of the market penetration and energy savings potential of high-efficiency motors will concentrate on this sector.

Electric motors are by far the largest end-user of electricity in the industrial sector. In 1980, electric motor drives consumed approximately 63 percent of all electricity used in the industrial sector (EPRI 1984).

Current industrial electric motors are relatively efficient, in terms of their mechanical power output for a given electrical energy input, compared to most energy-consuming processes. However, because of the large amount of electricity used by electric motors, even a small increase in electric motor efficiency can potentially result in significant electricity savings.

12.1 TECHNOLOGY DESCRIPTION

High-efficiency electric motors improve motor efficiency and reduce electricity usage by reducing energy losses that occur in various internal parts of the motors. To facilitate an understanding of the nature of electric motor energy losses, an illustration of a typical type of electric motor is presented in Figure 12.1.

In an electric motor, an electromagnetic field is created to produce force that turns a drive shaft. The two components of a motor that produce voltage for the creation of the electromagnetic field are known as the stator and the rotor. Because they are not perfect conductors of electricity, some of the energy supplied to the stator and rotor is lost in the form of resistance losses.

The mechanical parts of an electric motor include a frame to hold the stator, a drive shaft, a cooling fan, and end shields with bearings. Friction produced by the actions of these mechanical parts also increases motor electricity consumption.

FIGURE 12.1. Large Polyphase AC Industrial Motor

Various material and design changes are employed in high-efficiency motors to reduce stator, rotor, friction and other energy losses. It should be emphasized that these changes are not standardized across all motors. However, some common design changes employed in high-efficiency motors are the following (Hunt et al. 1976):

- longer rotor and stator cores that reduce the density of the electromagnetic field of the motor and increase the conductivity of the rotor and stator to electrical input

- thinner rotor and stator cores that reduce the amount of current lost through the outside of the rotor and stator
- use of silicon steel rather than carbon steel in rotor and stator cores to reduce the amount of energy lost in the creation of the electromagnetic field.

High-efficiency motors can be operated in the same manner as standard electric motors and their expected operating lifetimes should also be equal to that of standard motors. However, a larger amount of higher quality materials are required for manufacturing high-efficiency motors and this increases their initial purchase cost (Hane et al. 1983). Thus, a potential purchaser of a high-efficiency motor is faced with determining whether the electricity cost savings of the motor will be sufficient to justify a higher initial purchase price.

A number of studies of high-efficiency motors (Hane et al. 1983, Hunt et al. 1976, and Argonne National Laboratory 1980) indicate that industrial users of electric motors will generally not replace standard electric motors with high-efficiency motors unless the standard electric motors are no longer operating properly. The costs of motor installation and disrupting industrial operations are perceived to exceed any potential energy cost savings that could result from improving electric motor efficiencies. Thus, this analysis of high-efficiency motors will be limited to new and retirement applications of such motors and will exclude retrofit applications.

It should be emphasized that the market penetration and energy savings potential of high-efficiency motors will vary substantially depending upon such factors as the type of motor, how the motor is used, electricity prices, and many other factors. One factor that is crucial in determining the desirability of high-efficiency motors is motor size. Thus, this analysis is segmented into five motor-size categories: 1-5 horsepower (HP) motors, 5-20 HP motors, 20-50 HP motors, 50-125 HP motors and motors larger than 125 HP. Motors of less than 1 HP in size were excluded from analysis because of their small potential for energy savings (Argonne National Laboratory 1980).

Because of the large number of factors that impact upon the desirability of using high-efficiency motors, the information presented in this chapter can only provide a representative picture of these motors in terms of their cost-effectiveness, market penetration potential and energy savings potential. The chapter begins with a presentation of information on the current market situation of high-efficiency electric motors.

12.2 CURRENT MARKET SITUATION

High-efficiency electric motors have been available in the marketplace for several years (Hunt et al. 1976). However, according to one manufacturer of electric motors, interest in purchases of high-efficiency electric motors has increased dramatically in the last two years.^(a)

The rate of market penetration for high-efficiency electric motors has been slow because of the small percentage of total manufacturing costs comprised by electricity purchased for motor drive applications, the high perceived costs of retrofitting electric motors and the slow rate of retirement of electric motors.^(b) However, virtually all electric motor vendors contacted stated that high-efficiency motors are being purchased in increasing numbers in situations where 1) a motor needs replacing because it no longer operates properly, or 2) a completely new motor drive process is being installed.

Many of the major electric motor manufacturers, including General Electric, Century Electric, Emerson Electric, and Siemens-Allis manufacture high-efficiency electric motors.^(c) Thus, the commercial availability of this conservation technology is high. Normally, manufacturers offer both standard-efficiency and high-efficiency motors for a given application and, in some cases, three efficiency levels are offered.

(a) Personal communication with Silby Carroll, Electric Apparatus Company, Howell, Michigan, November 15, 1984.

(b) Personal communication with Frank Seabury, Arthur D. Little, Cambridge, Massachusetts, November 15, 1984.

(c) Personal communication with John Matthews, a sales representative for K&N Electric, Spokane, Washington, November 15, 1984.

The electricity savings that will result from the use of high-efficiency electric motors are dependent upon the usage rate of the motors, the size of the motors, and other factors. It is reported that sales of high-efficiency motors of less than 1 HP are significantly lower as a proportion of total motor sales of this size than is the case for sales of high-efficiency motors in the larger horsepower classes.^(a)

Vendors of electric motors that were contacted indicated that the development and marketing of electric motors has been driven by the demand for such motors on the part of motor purchasers. One representative of a custom motor manufacturer stated that it is becoming increasingly common for purchasers of electric motors to require in their bid specifications that an electric motor attain a minimum level of efficiency.^(b) Motor manufacturers have responded to such demands by developing entire lines of high-efficiency electric motors.^(c)

12.3 COST EFFECTIVENESS AND MARKET PENETRATION

Evaluations of the cost effectiveness and likely market penetration of high-efficiency electric motors are presented in this section. These evaluations begin with the presentation of information on representative incremental capital costs and payback periods for the various size categories of high-efficiency electric motors. These estimates are then integrated with information on technical factors that could inhibit the use of high-efficiency electric motors to derive estimates of the maximum potential market penetration of high-efficiency motors.

12.3.1 Cost Effectiveness of High-Efficiency Motors

The cost effectiveness of high-efficiency electric motors, as measured by their incremental capital costs and payback periods, are dependent upon the capital costs of high-efficiency motors compared to standard electric motors,

(a) Personal communication with John Allen, Emerson Electric Co., St. Louis, Missouri, November 16, 1984.

(b) Personal communication with Silby Carroll, Electric Apparatus Co., Howell, Michigan, November 15, 1984.

(c) Unpublished product line catalogue from Century Electric Co., St. Louis, Missouri, November 1984.

the level of the energy savings produced by high-efficiency motors, and the value of these energy savings measured in dollars. All of these factors are addressed in this section.

Representative Capital Costs for High-Efficiency and Standard Electric Motors

Product catalogues from two major electric motor manufacturers were used as the basis for developing representative estimates of the capital costs of high-efficiency and standard electric motors (Siemens-Allis 1984 and Century Electric 1984). Both of these manufacturers produce high-efficiency and standard electric motors that are similar in almost all respects except for the level of energy-use efficiency that they achieve.

Several models are produced in various sizes. The list prices for the various models were averaged across models to derive representative estimates of the capital costs for motors within the size classifications selected for use in this study. For example, Siemens-Allis produces four models of electric motors in both one and five HP sizes (i.e., eight motors in the 1-5 HP class used in this study). The capital costs of these models were averaged to derive a representative estimate of capital costs for motors in the one-to-five HP size classification.

Estimates of the initial costs for high-efficiency and standard electric motors, obtained by averaging the list prices presented in the manufacturers' product catalogues, are shown in Table 12.1. It is important to note that the estimates presented in Table 12.1 represent only motor purchase costs and do not include installation costs. In new and retirement applications, the installation costs for high-efficiency motors should not differ significantly from those for standard motors (Hunt et al. 1976). Thus, except for retrofit applications (which are excluded from this analysis), installation costs should have no significant impact on the cost-effectiveness of high-efficiency motors. Representative estimates of first cost percentage increases for high-efficiency electric motors are shown in the last column of Table 12.1.

TABLE 12.1. Representative Costs for High-Efficiency Electric Motors^(a)

Motor Size (HP)	Initial Cost for High -Efficiency Motors (\$1984)	Initial Cost for Standard- Efficiency Motors (\$1984)	Incremental Cost (\$)	First Cost Percentage Increase (percent)
1 to 5	324	245	79	32
5 to 20	720	545	175	32
20 to 50	1616	1273	343	27
50 to 125	4712	3849	863	22
>125	8950	7370	1580	21

(a) Source: Calculated from data presented in Siemens-Allis Selection and Pricing Guide--Integral Horsepower AC Motors, 1984 and Century Electric Product Catalogue, 1984.

Representative Energy-use Efficiency Improvements
for High-Efficiency Motors

The energy-use efficiency of an electric motor represents the ratio of electric power output from an electric motor to the electricity input to the motor. Estimates of representative efficiencies were obtained by averaging the efficiencies of various models produced by a major electric motor manufacturer (Siemens-Allis 1984) that were within the size classifications selected for use in this study. The representative estimates are shown in Table 12.2.

The last column of Table 12.2 presents representative estimates of the percentage reductions in electricity use that are likely to result from using high-efficiency motors rather than standard motors. These estimates were calculated by dividing the representative efficiencies for high-efficiency motors into the representative efficiencies for standard motors, subtracting one, and multiplying by 100. Note that the percentage reductions in electricity use for high-efficiency motors decline as motor size is increased. This result was also obtained in other studies of energy-efficient motors (Hane 1983 and Hunt et al. 1976).

TABLE 12.2. Representative Efficiency Improvements for High-Efficiency Electric Motors^(a)

Motor Size (HP)	Representative Efficiency for High-Efficiency Motors (percent)	Representative Efficiency for Standard Motors (percent)	Estimated Electricity Savings (percent) ^(b)
1 to 5	84.67	74.25	14.0
5 to 20	91.12	83.99	8.5
20 to 50	93.85	88.03	6.6
50 to 125	94.59	91.42	3.5
>125	94.79	93.98	0.9

(a) Source: Siemens-Allis Selection and Pricing Guide--Integral Horsepower AC Motors, 1984.

(b) Calculated by dividing the efficiency of high-efficiency motors into the efficiency of standard motors, subtracting one, and multiplying by 100.

Representative Electricity Savings for High-Efficiency Motors

In order to estimate representative kWh electricity savings for high-efficiency electric motors using the percentage electricity savings estimates shown in Table 12.2, it is necessary to develop representative estimates of the electricity consumed per unit by standard electric motors in the various size classifications. This task was performed in a series of steps. First, data on electricity use for electric motors in industry was collected from the ISTUM model (Carhart et al. 1979). ISTUM results were selected for use in deriving representative estimates of the electric use per electric motor because the results of this model are also used for forecast future growth in electric motor populations. The model indicated that 632.7 BkWh of electricity was consumed in such applications in 1978. Second, data on electricity consumption by motors in the five size classes selected for use in this study and the number of motors in each class was obtained from an Argonne National Laboratory (1980) study. The Argonne consumption data was used to calculate the share of total industrial motor electricity use associated with each size classification.

Third, the calculated size shares were multiplied by the ISTUM total use estimate to obtain estimates of the electricity consumption by electric motors in each size classification. These estimates are provided in the second column of Table 12.3. Fourth, the estimated number of motors in each size class (column three of Table 12.3) was divided into the estimated total annual electricity use for each class to obtain an estimate of the annual electricity use per motor in each size class. These estimates are presented in column four of Table 12.3.

Once representative estimates of electricity use per unit for standard electric motors were derived, estimates of the annual kWh savings per motor for high-efficiency electric motors were calculated. These estimates were developed by multiplying annual electricity use per motor estimates (shown in the last column of Table 12.3) by estimates of the percentage electricity savings that will result from the use of high-efficiency motors (shown in Table 12.2).

TABLE 12.3. Representative Electricity Use per Motor for Conventional Electric Motors Calculated from a Baseline Electricity Use for Industrial Motor Drives of 632.7 billion kWh^(a)

Motor Size (HP)	Percent of Total Electricity Use in This HP Classification (percent) ^(b)	Annual Electricity Use in This HP Classification (Billion kWh)	Estimated Number of Motors in This HP Class (000s) ^(b)	Annual Estimated Electricity Use Per Motor (kWh)
1 to 5	0.9	5.69	8082	704
5 to 20	7.7	48.72	5191	9,385
20 to 50	12.3	77.82	1973	39,442
50 to 125	24.0	151.85	928	163,629
>125	55.0	347.99	782	444,994

(a) Source: Documentation on the ISTUM forecasting model presented in The Least-Cost Energy Strategy--Technical Appendix, (Carhart et al. 1979).

(b) Source: Calculated from data presented in Classification and Evaluation of Electric Motors and Pumps, (Argonne National Laboratory 1980).

Representative Operating Cost Savings for High-Efficiency Motors

The reduction in operating costs that will result from the use of high-efficiency motors is a direct function of the kWh electricity savings that will be obtained from using these motors and the price per kWh charged for electricity. For purposes of this study, an average electricity price of 4.97¢ per kWh was used in all cost savings calculations. This figure represents the average price paid by industrial electricity users in 1983 (EIA 1983).

Representative Payback Periods for High-Efficiency Electric Motors

Estimates of representative payback periods for high-efficiency electric motors are presented in Table 12.4. These estimates were derived using manufacturers' data on motor costs and efficiencies and a U.S. average industrial electricity price of 4.97¢ per kWh as inputs to the calculation process. Note that the estimated payback periods for motors in the middle size categories are much shorter than for motors in the smallest and largest size categories. These results are in agreement with results obtained in other studies that found that the greatest opportunities for cost-effective electricity savings from the use of high-efficiency motors are in the middle motor size ranges (Hane et al. 1983 and Hunt 1976).

TABLE 12.4. Representative Payback Periods for High-Efficiency Electric Motors

Motor Size (HP)	Estimated Electricity Savings for High-Efficiency Motors (percent)	Estimated Electricity Use for Conventional Motors (kWh)	Estimated Annual Electricity Cost Savings(\$)	Incremental Capital Costs for High-Efficiency Motors (\$)	Estimated Payback Period (Years)
1 to 5	14.0	704	4.90	79	16.1
5 to 20	8.5	9,385	39.65	175	4.4
20 to 50	6.6	39,442	129.38	343	2.7
50 to 125	3.5	163,629	284.64	863	3.0
>125	0.9	444,994	199.05	1580	8.0

12.3.2 Technical Limits on the Use of High-Efficiency Motors

No justification was found for applying any technical limits to the use of high-efficiency electric motors. All available information indicated that high-efficiency motors can be used in any situation where standard motors are used.

12.3.3 Maximum Potential Market of High-Efficiency Motors

Estimates of the maximum market penetration for high-efficiency electric motors in the industrial sector were obtained by applying representative estimates of the first cost percentage increases for these motors (from Table 12.1) and payback period estimates (from Table 12.4) to data presented previously in Table 4.2. The results of this process are shown in Table 12.5.

12.4 POPULATION DATA

In this section, data on current electric motor populations, growth rates in electric motor populations, and retirement rates for electric motors are presented.

The most current data that could be located on electric motor populations in the various size categories were for 1978 (Argonne National Laboratory

TABLE 12.5. Estimates of the Maximum Market Penetration Potential^(a) of High-Efficiency Electric Motors in New and Retirement Applications

Motor Size (HP)	Estimated First Cost Percentage Increase (percent)	Estimated Payback Period (Years)	Estimated Maximum Market Penetration Potential (percent)
1 to 5	32	16.1	5
5 to 20	32	4.4	20
20 to 50	27	2.7	30
50 to 125	22	3.0	40
>125	21	8.0	10

(a) Obtained from information from DOE/BERD presented previously in Table 4.2.

1980). These data were presented previously in the fourth column of Table 12.3 and will be used to represent the current level of electric motor populations. Data on growth rates in sales of electrical equipment between 1978 and 1982 indicated that this growth was relatively small (DRI 1982). Thus, the results of our analysis will likely not be affected significantly by the use of 1978 data to represent current motor populations.

The growth in electric motor populations incorporated in this study are intended to be consistent with those assumed in the ISTUM industrial energy use forecasting model. This model assumes that electric equipment sales will increase at an average rate of approximately 7.2 percent in constant dollar terms between 1984 and 2000 (EEA 1982). Fluctuations in forecast annual growth rates around the forecast average growth rate of 7.2 percent were generally less than .5 percent (EEA 1982). Thus, use of an average growth rate should not significantly affect the results of this study. This growth rate is used to derive the number of potential new applications of high-efficiency motors in all size categories.

Retirement rates for electric motors will vary depending upon the size of the motors, with smaller motors having shorter expected lifetimes and faster retirement rates than larger motors. Motor retirement rates were derived from information on the expected lifetimes of various sizes of motors developed in a comprehensive study of electric motors (Argonne National Laboratory 1980). These retirement rates represent the percent of the current motor stock that will be retired in each year from 1984 to 2000. They were calculated by dividing one by the expected lifetimes of motors in the various size classifications.

The current populations, growth rates, and retirement rates assumed for use in this study for the various size classifications of electric motors are summarized in Table 12.6. These numbers were integrated with estimates of the maximum potential market penetration of high-efficiency motors in the various size categories and an S-shaped market adoption rate (see Chapter 4) to develop estimates of the number of high-efficiency motors that will likely be installed between 1984 and 2000. These annual estimates are presented Tables 12.7 to 12.11.

TABLE 12.6. Current Electric Motor Populations, Growth Rates and Retirement Rates Employed in This Study

Motor Size (HP)	Current Motor Population ^(a) (000s)	Future Annual Growth Rate ^(b) (percent)	Additional Units Added Annually (000s)	Annual Retirement Rate (percent) ^(a)	Units Retired Annually (000s)
1 to 5	8082	7.2	582	5.8	473
5 to 20	5191	7.2	374	5.2	268
20 to 50	1973	7.2	142	4.6	91
50 to 125	928	7.2	67	3.5	32
>125	782	7.2	56	3.4	27

(a) Source: Calculated from data presented in Classification and Evaluation of Electric Motors and Pumps, (Argonne National Laboratory 1980).

(b) Source: Documentation on the ISTUM forecasting model presented in Proposed ISTUM Runs and Inputs, Outputs and Schedule, (EEA 1982).

12.5 ENERGY SAVINGS RESULTS

Estimates of the energy savings that are forecast to result from the use of high-efficiency electric motors in selected years are shown in the last columns of Tables 12.7 to 12.11. Also shown in Table 12.7 to 12.11 are the number of units of high-efficiency motors projected to be installed. Note that projected energy savings (in BkWh) were obtained by multiplying representative energy savings per unit in each motor size category (in kWh) by the projected number of high-efficiency motors that will be installed in each year.

The last column of Table 12.12 presents the likely level of electricity savings for high-efficiency motors in the industrial sector summed across all motor sizes. These estimates are projected to reach approximately 6.19 BkWh by the year 2000.

12.6 SENSITIVITY ANALYSIS

This section presents the results of an analysis of the sensitivity of the energy savings estimates for high-efficiency electric motors to changes in the maximum potential market penetration the technology achieves and the rate at

TABLE 12.7. Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 1 to 5 Horsepower Motors

Year	Retired Units Market (a)	New Market Additions (b)	Retired Units Market Share (c)	New Market Additions Share (c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors (d) (BkWh)
1984	473,000	582,000	0.020	0.020	11,600	9,500	21,100	0.002
1985	473,000	582,000	0.021	0.021	12,200	9,900	43,200	0.004
1986	473,000	582,000	0.022	0.022	12,800	10,400	66,400	0.007
1987	473,000	582,000	0.024	0.024	14,000	11,400	91,800	0.009
1988	473,000	582,000	0.026	0.026	15,100	12,300	119,200	0.012
1989	473,000	582,000	0.029	0.029	16,900	13,700	149,800	0.015
1990	473,000	582,000	0.032	0.032	18,600	15,100	183,500	0.018
1991	473,000	582,000	0.035	0.035	20,400	16,600	220,500	0.022
1992	473,000	582,000	0.039	0.039	22,700	18,400	261,600	0.026
1993	473,000	582,000	0.042	0.042	24,400	19,900	305,900	0.030
1994	473,000	582,000	0.044	0.044	25,600	20,800	352,300	0.035
1995	473,000	582,000	0.045	0.045	26,200	21,300	399,800	0.040
1996	473,000	582,000	0.046	0.046	26,800	21,800	448,400	0.044
1997	473,000	582,000	0.047	0.047	27,400	22,200	498,000	0.049
1998	473,000	582,000	0.048	0.048	27,900	22,700	548,600	0.054
1999	473,000	582,000	0.049	0.049	28,500	23,200	600,300	0.059
2000	473,000	582,000	0.050	0.050	29,100	23,600	653,000	0.065

(a) Current original stock in this size category of motors is estimated to be 8.082×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 5.8 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 5 percent and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (99 kWh/year).

TABLE 12.8. Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 5 to 20 Horsepower Motors

Year	Retired Units Market (a)	New Market Additions (b)	Retired Units Market Share (c)	New Market Additions Share (c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High- Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors (d) (BkWh)
1984	268,000	374,000	0.075	0.075	28,000	20,100	48,100	0.04
1985	268,000	374,000	0.080	0.080	29,900	21,400	99,400	0.08
1986	268,000	374,000	0.085	0.085	31,800	22,800	154,000	0.12
1987	268,000	374,000	0.091	0.091	34,000	24,400	212,400	0.17
1988	268,000	374,000	0.097	0.097	36,300	26,000	274,700	0.22
1989	268,000	374,000	0.105	0.105	39,300	28,100	342,100	0.27
1990	268,000	374,000	0.113	0.113	42,300	30,300	414,700	0.33
1991	268,000	374,000	0.123	0.123	46,000	33,000	493,700	0.39
1992	268,000	374,000	0.133	0.133	49,700	35,600	579,000	0.46
1993	268,000	374,000	0.144	0.144	53,800	38,600	671,400	0.54
1994	268,000	374,000	0.155	0.155	58,000	41,500	770,900	0.62
1995	268,000	374,000	0.165	0.165	61,700	44,200	876,800	0.70
1996	268,000	374,000	0.174	0.174	65,100	46,600	988,500	0.79
1997	268,000	374,000	0.182	0.182	68,100	48,800	1,105,400	0.88
1998	268,000	374,000	0.190	0.190	71,100	50,900	1,227,400	0.98
1999	268,000	374,000	0.196	0.196	73,300	52,500	1,353,200	1.08
2000	268,000	374,000	0.200	0.200	74,800	53,600	1,481,600	1.18

(a) Current original stock in this size category of motors is estimated to be $5,191 \times 10^6$ (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 5.2 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 20 percent and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (798 kWh/year).

TABLE 12.9. Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 20 to 50 Horsepower Motors

Year	Retired Units Market (a)	New Market Additions (b)	Retired Units Market Share (c)	New Market Additions Share (c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High- Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors (d) (BkWh)
1984	91,000	142,000	0.100	0.100	14,200	9,100	23,300	0.06
1985	91,000	142,000	0.103	0.103	14,600	9,400	47,300	0.12
1986	91,000	142,000	0.106	0.106	15,000	9,600	71,900	0.19
1987	91,000	142,000	0.116	0.116	16,500	10,600	99,000	0.26
1988	91,000	142,000	0.126	0.126	17,900	11,500	128,400	0.33
1989	91,000	142,000	0.138	0.138	19,600	12,600	160,600	0.42
1990	91,000	142,000	0.152	0.152	21,600	13,800	196,000	0.51
1991	91,000	142,000	0.166	0.166	23,600	15,100	234,700	0.61
1992	91,000	142,000	0.182	0.182	25,800	16,600	277,100	0.72
1993	91,000	142,000	0.200	0.200	28,400	18,200	323,700	0.84
1994	91,000	142,000	0.218	0.218	31,000	19,800	374,500	0.97
1995	91,000	142,000	0.238	0.238	33,800	21,700	430,000	1.12
1996	91,000	142,000	0.256	0.256	36,400	23,300	489,700	1.27
1997	91,000	142,000	0.272	0.272	38,600	24,800	553,100	1.44
1998	91,000	142,000	0.284	0.284	40,300	25,800	619,200	1.61
1999	91,000	142,000	0.294	0.294	41,700	26,800	687,700	1.79
2000	91,000	142,000	0.300	0.300	42,600	27,300	757,600	1.97

(a) Current original stock in this size category of motors is estimated to be 1.973×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 4.6 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 30 percent and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) x (2603 kWh/year).

TABLE 12.10. Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 50 to 125 Horsepower Motors

Year	Retired Units Market ^(a)	New Market Additions ^(b)	Retired Units Market Share ^(c)	New Market Additions Share ^(c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors ^(d) (BkWh)
1984	32,000	67,000	0.135	0.135	9,000	4,300	13,300	0.08
1985	32,000	67,000	0.140	0.140	9,400	4,500	27,200	0.16
1986	32,000	67,000	0.145	0.145	9,700	4,600	41,500	0.24
1987	32,000	67,000	0.155	0.155	10,400	5,000	56,900	0.33
1988	32,000	67,000	0.165	0.165	11,100	5,300	73,300	0.42
1989	32,000	67,000	0.185	0.185	12,400	5,900	91,600	0.52
1990	32,000	67,000	0.205	0.205	13,700	6,600	111,900	0.64
1991	32,000	67,000	0.230	0.230	15,400	7,400	134,700	0.77
1992	32,000	67,000	0.260	0.260	17,400	8,300	160,400	0.92
1993	32,000	67,000	0.300	0.300	20,100	9,600	190,100	1.09
1994	32,000	67,000	0.330	0.330	22,100	10,600	222,800	1.28
1995	32,000	67,000	0.350	0.350	23,500	11,200	257,500	1.47
1996	32,000	67,000	0.370	0.370	24,800	11,800	294,100	1.68
1997	32,000	67,000	0.385	0.385	25,800	12,300	332,200	1.90
1998	32,000	67,000	0.390	0.390	26,100	12,500	370,800	2.12
1999	32,000	67,000	0.395	0.395	26,500	12,600	409,900	2.35
2000	32,000	67,000	0.400	0.400	26,800	12,800	449,500	2.57

(a) Current original stock in this size category of motors is estimated to be 0.0928×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 3.5 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 40 percent and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (5727 kWh/year).

TABLE 12.11. Motor Stock Projections and High-Efficiency Motor Market Share Estimates for >125 Horsepower Motors

Year	Retired Units Market ^(a)	New Market Additions ^(b)	Retired Units Market Share ^(c)	New Market Additions Share ^(c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors ^(d) (BkWh)
1984	27,000	56,000	0.040	0.040	2,200	1,100	3,300	0.01
1985	27,000	56,000	0.041	0.041	2,300	1,100	6,700	0.03
1986	27,000	56,000	0.043	0.043	2,400	1,200	10,300	0.04
1987	27,000	56,000	0.045	0.045	2,500	1,200	14,000	0.06
1988	27,000	56,000	0.049	0.049	2,700	1,300	18,000	0.07
1989	27,000	56,000	0.053	0.053	3,000	1,400	22,400	0.09
1990	27,000	56,000	0.058	0.058	3,200	1,600	27,200	0.11
1991	27,000	56,000	0.063	0.063	3,500	1,700	32,400	0.13
1992	27,000	56,000	0.069	0.069	3,900	1,900	38,200	0.15
1993	27,000	56,000	0.076	0.076	4,300	2,100	44,600	0.18
1994	27,000	56,000	0.083	0.083	4,600	2,200	51,400	0.21
1995	27,000	56,000	0.088	0.088	4,900	2,400	58,700	0.24
1996	27,000	56,000	0.092	0.092	5,200	2,500	66,400	0.27
1997	27,000	56,000	0.095	0.095	5,300	2,600	74,300	0.30
1998	27,000	56,000	0.097	0.097	5,400	2,600	82,300	0.33
1999	27,000	56,000	0.099	0.099	5,500	2,700	90,500	0.36
2000	27,000	56,000	0.100	0.100	5,600	2,700	98,800	0.40

(a) Current original stock in this size category of motors is estimated to be 0.782×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 3.4 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 10 percent and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (4005 kWh/year).

TABLE 12.12. Projections of Energy Savings from the Use of High-Efficiency Electricity Motors (BkWh)

<u>Year</u>	<u>1 to 5 HP</u>	<u>5 to 20 HP</u>	<u>20 to 50 HP</u>	<u>50 to 125 HP</u>	<u>>125 HP</u>	<u>All Motors</u>
1985	0.004	0.08	0.12	0.16	0.03	0.39
1990	0.018	0.33	0.51	0.64	0.11	1.61
1995	0.040	0.70	1.12	1.47	0.24	3.57
2000	0.065	1.18	1.97	2.57	0.40	6.19

which this maximum is achieved. The sensitivity of the energy savings estimates is evaluated for both a low scenario and a high scenario.

12.6.1 Low Market Penetration Scenario

The maximum potential market penetration estimates used in the low scenario of the sensitivity analysis are shown in the second column of Table 12.13. These maximum penetration estimates are half as large as those assumed in the baseline analysis. In addition, it was assumed in the low scenario that the rate of market adoption for high-efficiency motors would be slower so that only approximately 75 percent of the assumed maximum potential market penetration would be achieved by the year 2000. Thus, the market penetration levels reached by the year 2000 for high-efficiency motors in the low scenario are those shown in the third column of Table 12.13.

TABLE 12.13. Low Scenario Maximum Market Penetration Potentials and Market Penetrations Assumed to be Reached in 2000

<u>Motor Size (HP)</u>	<u>Estimated Maximum Market Penetration Potential (percent)</u>	<u>Market Penetration Assumed to be Reached in 2000 (percent)</u>
1 to 5	2.5	1.9
5 to 20	10.0	7.5
20 to 50	15.0	11.3
50 to 125	20.0	15.0
>125	5.0	3.8

The results of the low-scenario sensitivity analysis as well as input data and assumptions are summarized in used to obtain the estimates are shown in Tables 12.14 to 12.18 and summarized in Table 12.19. These results indicate that under the conservative market penetration assumptions of the low scenario, a total of 2.84 BkWh of electricity could be saved in 2000 through the use of high-efficiency electric motors. This level of savings is approximately 45 percent of the savings obtained in the baseline estimation. A summary of total energy savings for all size motors for selected years is included in Table 12.19.

12.6.2 High Market Penetration Scenario

The maximum potential market penetration estimates used in the high scenario of the sensitivity analysis are shown in Table 12.20. These penetration estimates are twice as large as those used in the original baseline estimation. There appeared to be no basis for assuming that the maximum potential market penetration of high-efficiency motors would be limited by technical factors. An additional assumption employed in the high scenario is that a rapid rate of market adoption would cause the maximum potential market penetration for high-efficiency motors to be reached by 1995. The results of the high scenario sensitivity analysis as well as input data and assumption used are shown in Tables 12.21 to 12.25.

The total electricity savings of 12.11 BkWh by 2000 estimated in the high scenario are almost twice as large as those obtained in the baseline estimation. A summary of the results of the high scenario is presented in Table 12.26.

12.7 COST PER kWh OF ENERGY SAVED CALCULATIONS AND COMPARISONS TO THE COST PER kWh OF PRODUCING NEW GENERATING CAPACITY

High-efficiency electric motors can potentially be considered as investments which can produce power at costs that are less than the costs of power produced by new generating facilities. If high-efficiency motors can produce power for less than new generating facilities, then benefits can potentially be obtained by utilities and others undertaking investments to promote the use of high-efficiency motors as a means of meeting future power demands.

TABLE 12.14. Low-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 1 to 5 Horsepower Motors

Year	Retired Units Market ^(a)	New Market Additions ^(b)	Retired Units Market Share ^(c)	New Market Additions Share ^(c)	Additions of High-Efficiency Motors In New Applications	Additions of High-Efficiency Motors In Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors ^(d) (BkWh)
1984	473,000	582,000	0.0050	0.0050	2,900	2,400	5,300	0.001
1985	473,000	582,000	0.0055	0.0055	3,200	2,600	11,100	0.001
1986	473,000	582,000	0.0060	0.0060	3,500	2,800	17,400	0.002
1987	473,000	582,000	0.0065	0.0065	3,800	3,100	24,300	0.002
1988	473,000	582,000	0.0075	0.0075	4,400	3,500	32,200	0.003
1989	473,000	582,000	0.0085	0.0085	4,900	4,000	41,100	0.004
1990	473,000	582,000	0.0095	0.0095	5,500	4,500	51,100	0.005
1991	473,000	582,000	0.0110	0.0110	6,400	5,200	62,700	0.006
1992	473,000	582,000	0.0125	0.0125	7,300	5,900	75,900	0.008
1993	473,000	582,000	0.0135	0.0135	7,900	6,400	90,200	0.009
1994	473,000	582,000	0.0145	0.0145	8,400	6,900	105,500	0.010
1995	473,000	582,000	0.0155	0.0155	9,000	7,300	121,800	0.012
1996	473,000	582,000	0.0165	0.0165	9,600	7,800	139,200	0.014
1997	473,000	582,000	0.0175	0.0175	10,200	8,300	157,700	0.016
1998	473,000	582,000	0.0180	0.0180	10,500	8,500	176,700	0.017
1999	473,000	582,000	0.0185	0.0185	10,800	8,800	196,300	0.019
2000	473,000	582,000	0.0190	0.0190	11,100	9,000	216,400	0.021

(a) Current original stock in this size category of motors is estimated to be 0.782×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 3.4 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 1.9 percent assumed to be reached in 2000 and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (99 kWh/year).

TABLE 12.15. Low-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 5 to 20 Horsepower Motors

Year	Retired Units Market ^(a)	New Market Additions ^(b)	Retired Units Market Share ^(c)	New Market Additions Share ^(c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors ^(d) (BkWh)
1984	268,000	374,000	0.0400	0.0400	15,000	10,700	25,700	0.02
1985	268,000	374,000	0.0410	0.0410	15,300	11,000	52,000	0.04
1986	268,000	374,000	0.0420	0.0420	15,700	11,300	79,000	0.06
1987	268,000	374,000	0.0430	0.0430	16,500	11,500	106,600	0.09
1988	268,000	374,000	0.0440	0.0440	17,200	11,800	134,900	0.11
1989	268,000	374,000	0.0460	0.0460	18,300	12,300	164,400	0.13
1990	268,000	374,000	0.0490	0.0490	19,400	13,100	195,800	0.16
1991	268,000	374,000	0.0520	0.0520	19,400	13,900	229,100	0.18
1992	268,000	374,000	0.0560	0.0560	20,900	15,000	265,000	0.21
1993	268,000	374,000	0.0600	0.0600	22,400	16,100	303,500	0.24
1994	268,000	374,000	0.0630	0.0630	23,600	16,900	344,000	0.27
1995	268,000	374,000	0.0660	0.0660	24,700	17,700	386,400	0.31
1996	268,000	374,000	0.0680	0.0680	25,400	18,200	430,000	0.34
1997	268,000	374,000	0.0700	0.0700	26,200	18,800	475,000	0.38
1998	268,000	374,000	0.0720	0.0720	26,900	19,300	521,200	0.42
1999	268,000	374,000	0.0740	0.0740	27,700	19,800	568,700	0.45
2000	268,000	374,000	0.0750	0.0750	28,000	20,100	616,800	0.49

(a) Current original stock in this size category of motors is estimated to be 0.782×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 3.4 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 7.5 percent assumed to be reached in 2000, and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (798 kWh/year).

TABLE 12.16. Low-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 20 to 50 Horsepower Motors

Year	Retired Units Market ^(a)	New Market Additions ^(b)	Retired Units Market Share ^(c)	New Market Additions Share ^(c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors ^(d) (BkWh)
1984	91,000	142,000	0.070	0.070	9,900	6,400	16,300	0.04
1985	91,000	142,000	0.071	0.071	10,100	6,500	32,900	0.09
1986	91,000	142,000	0.073	0.073	10,400	6,600	49,900	0.13
1987	91,000	142,000	0.075	0.075	10,700	6,800	67,400	0.18
1988	91,000	142,000	0.078	0.078	11,100	7,100	85,600	0.22
1989	91,000	142,000	0.082	0.082	11,600	7,500	104,700	0.27
1990	91,000	142,000	0.086	0.086	12,200	7,800	124,700	0.32
1991	91,000	142,000	0.091	0.091	12,900	8,300	145,900	0.38
1992	91,000	142,000	0.097	0.097	13,800	8,800	168,500	0.44
1993	91,000	142,000	0.103	0.103	14,600	9,400	192,500	0.50
1994	91,000	142,000	0.106	0.106	15,100	9,500	217,100	0.57
1995	91,000	142,000	0.108	0.108	15,300	9,800	242,200	0.63
1996	91,000	142,000	0.109	0.109	15,500	9,900	267,600	0.70
1997	91,000	142,000	0.110	0.110	15,600	10,000	293,200	0.76
1998	91,000	142,000	0.111	0.111	15,800	10,100	319,100	0.83
1999	91,000	142,000	0.112	0.112	15,900	10,200	345,200	0.90
2000	91,000	142,000	0.113	0.113	16,000	10,300	371,500	0.97

(a) Current original stock in this size category of motors is estimated to be 0.782×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 3.4 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 11.3 percent assumed to be reached in 2000, and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (2603 kWh/year).

TABLE 12.17. Low-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 50 to 125 Horsepower Motors

Year	Retired Units Market (a)	New Market Additions (b)	Retired Units Market Share (c)	New Market Additions Share (c)	Additions of High-Efficiency Motors In New Applications	Additions of High-Efficiency Motors In Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors (d) (BkWh)
1984	32,000	67,000	0.100	0.100	6,700	3,200	9,900	0.06
1985	32,000	67,000	0.101	0.101	6,800	3,200	19,900	0.11
1986	32,000	67,000	0.103	0.103	6,900	3,300	30,100	0.17
1987	32,000	67,000	0.105	0.105	7,000	33,400	40,500	0.23
1988	32,000	67,000	0.108	0.108	7,200	3,500	51,200	0.29
1989	32,000	67,000	0.112	0.112	7,500	3,600	62,300	0.36
1990	32,000	67,000	0.117	0.117	7,800	3,700	73,800	0.42
1991	32,000	67,000	0.122	0.122	8,200	3,900	85,900	0.49
1992	32,000	67,000	0.128	0.128	8,600	4,100	98,600	0.56
1993	32,000	67,000	0.134	0.134	9,000	4,300	111,900	0.64
1994	32,000	67,000	0.139	0.139	9,300	4,400	125,600	0.72
1995	32,000	67,000	0.143	0.143	9,600	4,600	139,800	0.80
1996	32,000	67,000	0.145	0.145	9,700	4,600	154,100	0.88
1997	32,000	67,000	0.147	0.147	9,800	4,700	58,600	0.97
1998	32,000	67,000	0.148	0.148	9,900	4,700	183,200	1.05
1999	32,000	67,000	0.149	0.149	10,000	4,800	198,000	1.13
2000	32,000	67,000	0.150	0.150	10,100	4,800	212,900	1.22

(a) Current original stock in this size category of motors is estimated to be $8,082 \times 10^6$ (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 5.8 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 15 percent assumed to be reached in 2000, and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (5727 kWh/year).

TABLE 12.18. Low-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for >125 Horsepower Motors

Year	Retired Units Market ^(a)	New Market Additions ^(b)	Retired Units Market Share ^(c)	New Market Additions Share ^(c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors ^(d) (BkWh)
1984	27,000	56,000	0.010	0.010	600	300	900	0.004
1985	27,000	56,000	0.011	0.011	600	300	1,800	0.007
1986	27,000	56,000	0.012	0.012	700	300	2,800	0.011
1987	27,000	56,000	0.013	0.013	700	400	3,900	0.016
1988	27,000	56,000	0.015	0.015	800	400	5,100	0.020
1989	27,000	56,000	0.017	0.017	1,000	500	6,600	0.026
1990	27,000	56,000	0.020	0.020	1,100	500	8,200	0.033
1991	27,000	56,000	0.023	0.023	1,300	600	10,100	0.040
1992	27,000	56,000	0.027	0.027	1,500	700	12,300	0.049
1993	27,000	56,000	0.030	0.030	1,700	800	14,800	0.059
1994	27,000	56,000	0.032	0.032	1,800	900	17,500	0.070
1995	27,000	56,000	0.033	0.033	1,800	900	20,200	0.081
1996	27,000	56,000	0.034	0.034	1,900	900	23,000	0.092
1997	27,000	56,000	0.035	0.035	2,000	900	25,900	0.104
1998	27,000	56,000	0.036	0.036	2,000	1,000	28,900	0.116
1999	27,000	56,000	0.037	0.037	2,100	1,000	32,000	0.128
2000	27,000	56,000	0.038	0.038	2,100	1,000	35,100	0.141

- (a) Current original stock in this size category of motors is estimated to be 8.082×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 5.8 percent annually (Argonne National Laboratory 1980).
 (b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).
 (c) Function of an estimated maximum market penetration of 3.8 percent assumed to be reached in 2000, and an S-shaped adoption curve.
 (d) Calculated by: (Cumulative Units) $\times$ (4005 kWh/year).

TABLE 12.19. Low-Scenario Estimates of Electricity Savings from the Use of Electric Motors (RkWh)

<u>Year</u>	<u>1 to 5 HP</u>	<u>5 to 20 HP</u>	<u>20 to 50 HP</u>	<u>50 to 125 HP</u>	<u>>125 HP</u>	<u>All Motors</u>
1985	0.00	0.04	0.90	0.11	0.07	0.25
1990	0.01	0.16	0.32	0.42	0.33	0.93
1995	0.01	0.31	0.63	0.80	0.81	1.83
2000	0.02	0.44	0.97	1.22	0.141	2.52

TABLE 12.20. High Scenario Maximum Market Potential's Assumed to be Reached in 1995

<u>Motor Size (HP)</u>	<u>Maximum Market Penetration (Assumed to be Reached in 1995), (percent)</u>
1 to 5	10
5 to 20	40
20 to 50	60
50 to 125	80
>125	10

Representative estimates of the levelized costs per kWh saved for high-efficiency electric motors are presented in Table 12.27. Comparing these estimates to a representative average generation cost for new coal-fired generation plants of 5.82¢/kWh (presented in Table 4.3) implies that high-efficiency motors would generally be lower cost sources of new electricity than new coal generating units. The only exception to this finding is for high-efficiency motors of less than 5 HP in size. The estimated costs per kWh saved for high-efficiency motors larger than 5 HP are significantly less than the regional cost of new power estimates (presented in Table 4.3) in all regions of the country.

TABLE 12.21. High-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 1 to 5 Horsepower Motors

Year	Retired Units Market (a)	New Market Additions (b)	Retired Units Market Share (c)	New Market Additions Share (c)	Additions of High-Efficiency Motors In New Applications	Additions of High-Efficiency Motors In Retirement Applications	Cumulative Units of High- Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors (d) (BkWh)
1984	473,000	582,000	0.020	0.020	11,600	9,500	21,100	0.002
1985	473,000	582,000	0.022	0.022	12,800	10,400	44,300	0.004
1986	473,000	582,000	0.025	0.025	14,600	11,800	70,700	0.007
1987	473,000	582,000	0.030	0.030	17,500	14,200	102,400	0.010
1988	473,000	582,000	0.038	0.038	22,100	18,000	142,500	0.014
1989	473,000	582,000	0.048	0.048	27,900	22,700	193,100	0.019
1990	473,000	582,000	0.060	0.060	34,900	28,400	256,400	0.025
1991	473,000	582,000	0.075	0.075	43,700	35,500	335,600	0.033
1992	473,000	582,000	0.085	0.085	49,500	40,200	425,300	0.042
1993	473,000	582,000	0.092	0.092	53,500	43,500	522,300	0.052
1994	473,000	582,000	0.097	0.097	56,500	45,900	624,700	0.062
1995	473,000	582,000	0.100	0.100	58,200	47,300	730,200	0.072
1996	473,000	582,000	0.100	0.100	58,200	47,300	835,700	0.083
1997	473,000	582,000	0.100	0.100	58,200	47,300	941,200	0.093
1998	473,000	582,000	0.100	0.100	58,200	47,300	1,046,700	0.104
1999	473,000	582,000	0.100	0.100	58,200	47,300	1,152,200	0.114
2000	473,000	582,000	0.100	0.100	58,200	47,300	1,257,700	0.125

(a) Current original stock in this size category of motors is estimated to be $8,082 \times 10^6$ (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 5.8 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 10 percent assumed to be reached in 1995, and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (99 kWh/year).

TABLE 12.22. High-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 5 to 20 Horsepower Motors

Year	Retired Units Market ^(a)	New Market Additions ^(b)	Retired Units Market Share ^(c)	New Market Additions Share ^(c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High- Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors ^(d) (BkWh)
1984	268,000	374,000	0.075	0.075	28,100	20,100	48,200	0.04
1985	268,000	374,000	0.085	0.085	31,800	22,800	102,800	0.08
1986	268,000	374,000	0.100	0.100	37,400	26,800	167,000	0.13
1987	268,000	374,000	0.120	0.120	44,900	32,200	244,100	0.19
1988	268,000	374,000	0.140	0.140	52,400	37,500	334,000	0.27
1989	268,000	374,000	0.170	0.170	63,600	45,600	443,200	0.35
1990	268,000	374,000	0.210	0.210	78,500	56,300	578,000	0.46
1991	268,000	374,000	0.260	0.260	97,200	69,700	744,900	0.59
1992	268,000	374,000	0.320	0.320	119,700	85,800	950,400	0.76
1993	268,000	374,000	0.360	0.360	134,600	96,500	1,181,500	0.94
1994	268,000	374,000	0.380	0.380	142,100	101,800	1,425,400	1.14
1995	268,000	374,000	0.400	0.400	149,600	107,200	1,682,200	1.34
1996	268,000	374,000	0.400	0.400	149,600	107,200	1,939,000	1.55
1997	268,000	374,000	0.400	0.400	149,600	107,200	2,195,800	1.75
1998	268,000	374,000	0.400	0.400	149,600	107,200	2,452,600	1.96
1999	268,000	374,000	0.400	0.400	149,600	107,200	2,709,400	2.16
2000	268,000	374,000	0.400	0.400	149,600	107,200	2,966,200	2.37

(a) Current original stock in this size category of motors is estimated to be 8.082×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 5.8 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 40 percent assumed to be reached in 1995, and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (798 kWh/year).

TABLE 12.23. High-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 20 to 50 Horsepower Motors

Year	Retired Units Market (a)	New Market Additions (b)	Retired Units Market Share (c)	New Market Additions Share (c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors (d) (BkWh)
1984	91,000	142,000	0.100	0.100	14,200	9,100	23,300	0.06
1985	91,000	142,000	0.105	0.105	14,900	9,600	47,800	0.12
1986	91,000	142,000	0.115	0.115	16,300	14,100	78,200	0.20
1987	91,000	142,000	0.130	0.130	18,500	11,800	108,500	0.28
1988	91,000	142,000	0.150	0.150	21,300	13,700	143,500	0.37
1989	91,000	142,000	0.190	0.190	27,000	17,300	187,800	0.49
1990	91,000	142,000	0.250	0.250	35,500	22,700	246,000	0.64
1991	91,000	142,000	0.320	0.320	45,400	29,100	320,500	0.83
1992	91,000	142,000	0.400	0.400	56,800	36,400	413,700	1.08
1993	91,000	142,000	0.470	0.470	66,700	42,800	523,200	1.36
1994	91,000	142,000	0.540	0.540	76,700	49,100	649,000	1.69
1995	91,000	142,000	0.600	0.600	85,200	54,600	788,800	2.05
1996	91,000	142,000	0.600	0.600	85,200	54,600	928,600	2.42
1997	91,000	142,000	0.600	0.600	85,200	54,600	1,068,400	2.78
1998	91,000	142,000	0.600	0.600	85,200	54,600	1,208,200	3.14
1999	91,000	142,000	0.600	0.600	85,200	54,600	1,348,000	3.51
2000	91,000	142,000	0.600	0.600	85,200	54,600	1,487,800	3.87

(a) Current original stock in this size category of motors is estimated to be 8.082×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 5.8 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 60 percent assumed to be reached in 1995, and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) x (2603 kWh/year).

TABLE 12.24. High-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for 50 to 125 Horsepower Motors

Year	Retired Units Market (a)	New Market Additions (b)	Retired Units Market Share (c)	New Market Additions Share (c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors (d) (BkWh)
1984	32,000	67,000	0.135	0.135	9,000	4,300	13,300	0.08
1985	32,000	67,000	0.145	0.145	9,700	4,600	27,600	0.16
1986	32,000	67,000	0.160	0.160	10,700	5,100	43,400	0.25
1987	32,000	67,000	0.190	0.190	12,700	6,100	62,200	0.36
1988	32,000	67,000	0.240	0.240	16,100	7,700	86,000	0.49
1989	32,000	67,000	0.300	0.300	20,100	9,600	115,700	0.66
1990	32,000	67,000	0.370	0.370	24,800	11,800	152,300	0.87
1991	32,000	67,000	0.450	0.450	30,200	14,400	196,900	1.13
1992	32,000	67,000	0.550	0.550	36,900	17,600	251,400	1.44
1993	32,000	67,000	0.650	0.540	43,600	20,800	315,800	1.81
1994	32,000	67,000	0.740	0.740	49,600	23,680	389,080	2.23
1995	32,000	67,000	0.800	0.800	53,600	25,600	468,280	2.68
1996	32,000	67,000	0.800	0.800	53,600	25,600	547,480	3.14
1997	32,000	67,000	0.800	0.800	53,600	25,600	626,680	3.59
1998	32,000	67,000	0.800	0.800	53,600	25,600	705,880	4.04
1999	32,000	67,000	0.800	0.800	53,600	25,600	785,080	4.50
2000	32,000	67,000	0.800	0.800	53,600	25,600	864,280	4.95

- (a) Current original stock in this size category of motors is estimated to be $8,082 \times 10^6$ (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 5.8 percent annually (Argonne National Laboratory 1980).
 (b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).
 (c) Function of an estimated maximum market penetration of 80 percent assumed to be reached in 1995, and an S-shaped adoption curve.
 (d) Calculated by: (Cumulative Units) x (5727 kWh/year).

TABLE 12.25. High-Scenario Motor Stock Projections and High-Efficiency Motor Market Share Estimates for >125 Horsepower Motors

Year	Retired Units Market ^(a)	New Market Additions ^(b)	Retired Units Market Share ^(c)	New Market Additions Share ^(c)	Additions of High-Efficiency Motors in New Applications	Additions of High-Efficiency Motors in Retirement Applications	Cumulative Units of High-Efficiency Electric Motors	Annual Energy Savings from Cumulative Additions of High-Efficiency Motors ^(d) (BkWh)
1984	27,000	56,000	0.040	0.040	2,200	1,100	3,300	0.01
1985	27,000	56,000	0.045	0.045	2,500	1,200	7,000	0.03
1986	27,000	56,000	0.052	0.052	2,900	1,400	11,300	0.05
1987	27,000	56,000	0.062	0.062	3,500	1,700	16,500	0.07
1988	27,000	56,000	0.080	0.080	4,500	2,200	23,200	0.09
1989	27,000	56,000	0.095	0.095	5,300	2,600	31,100	0.12
1990	27,000	56,000	0.115	0.115	6,400	3,100	40,600	0.16
1991	27,000	56,000	0.140	0.140	7,800	3,800	52,200	0.21
1992	27,000	56,000	0.165	0.165	9,200	4,500	65,900	0.26
1993	27,000	56,000	0.180	0.180	10,100	4,900	80,900	0.32
1994	27,000	56,000	0.190	0.190	10,600	5,100	96,600	0.39
1995	27,000	56,000	0.200	0.200	11,200	5,400	113,200	0.45
1996	27,000	56,000	0.200	0.200	11,200	5,400	129,800	0.52
1997	27,000	56,000	0.200	0.200	11,200	5,400	146,400	0.59
1998	27,000	56,000	0.200	0.200	11,200	5,400	163,000	0.65
1999	27,000	56,000	0.200	0.200	11,200	5,400	179,600	0.72
2000	27,000	56,000	0.200	0.200	11,200	5,400	196,200	0.79

(a) Current original stock in this size category of motors is estimated to be 8.082×10^6 (Argonne National Laboratory 1980) retirement assumed to occur at a rate of 5.8 percent annually (Argonne National Laboratory 1980).

(b) Growth in stock assumed to occur at a rate of 7.2 percent annually (EEA 1982).

(c) Function of an estimated maximum market penetration of 10 percent assumed to be reached in 1995, and an S-shaped adoption curve.

(d) Calculated by: (Cumulative Units) $\times$ (4005 kWh/year).

TABLE 12.26. High-Scenario Estimates of Electricity Savings from the Use of High-Efficiency Electric Motors

Year	1 to 5 HP	5 to 20 HP	20 to 50 HP	50 to 125 HP	>125 HP	All Motors
1985	0.00	0.08	0.12	0.16	0.03	0.39
1990	0.02	0.46	0.64	0.87	0.16	2.15
1995	0.07	1.34	2.05	2.68	0.45	7.24
2000	0.12	2.37	3.87	4.95	0.79	12.11

TABLE 12.27. Cost Per kWh Saved Calculations for High-Efficiency Electric Motors

Motor Size (HP)	Incremental Capital Cost (1984 \$) in New and Retirement Applications (a)	Levelized Capital Cost (\$/year) (b)	Annual Energy Savings (kWh/year) (c)	Cost per kWh Saved in New and Retirement Applications (\$/kWh) (d)
1 to 5	79	8.66	99	8.75
5 to 20	175	18.22	798	2.28
20 to 50	343	33.62	2603	1.29
50 to 125	863	77.34	5727	1.35
>125	1580	141.60	4005	3.54

(a) See Table 12.1.

(b) The level stream of annual payments the present value of which would equal the investment's incremental capital cost. The levelized cost was calculated using an 8 percent discount rate and operating lifetimes of 17 years for 1 to 5 HP motors, 19 years for 5 to 20 HP, 22 years for 20 to 50 HP, and 29 years for all other motors.

(c) Calculated as the percent electricity savings for high-efficiency motors (from Table 12.4) multiplied by the estimated electricity use in kWh for conventional motors (also from Table 12.4).

(d) Calculated as levelized capital costs (\$/year) divided by annual energy savings (kWh/year) and multiplied by 100.

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13.0 ADJUSTABLE SPEED MOTOR DRIVES

Adjustable speed electric motor drives (ASDs) can potentially produce electrical energy savings by properly matching electric motor speeds with motor power output requirements. As reported in Chapter 12.0, electric motors are the largest end user of electricity in the industrial sector, consuming approximately 63 percent of all electricity used in the sector (EPRI 1984a). ASDs can reduce the amount of electricity used by electric motors in any situation where motor power output requirements are not the same at all times. Though ASDs generally cost several times as much as their corresponding motors, they can be quite cost effective due to the magnitude of potential energy savings.

13.1 TECHNOLOGY DESCRIPTION

In many applications, the power output required from an electric motor varies significantly over time. An example of such an application is process chemical mixing operations where small chemical flows are required at certain times, while at other times much larger flows are required.

When constant speed motor drives are used in motor drive applications that have variable output requirements, control valves are necessary to limit outputs when full output levels are not required. Significant amounts of energy are wasted as a result of constant speed drives providing full output levels that in turn must be limited by control valves. ASDs reduce this waste by changing motor speeds to match motor output requirements.

An example of a potential application of ASDs is illustrated in Figure 13.1. A constant-speed motor drive is being used in the top and middle segments of Figure 13.1. In the top segment of Figure 13.1, full air flow is required from the motor drive and no energy savings would result from the use of an ASD in this situation. However, in the middle segment of Figure 13.1, the air flow requirements from the fan are reduced and a control valve at the inlet is required to limit air flow. Energy is wasted as air that is not required is deflected from the inlet valve.

FIGURE 13.1. Illustration of a Potential Application of an Adjustable Speed Motor Drive (EPRI 1984b)

A motor equipped with an ASD is illustrated in the bottom segment of Figure 13.1. The ASD allows for motor speed to be reduced in response to changing flow requirements and energy is no longer wasted against the inlet valve.

There are two primary types of ASDs--mechanical and electronic. Mechanical ASDs, such as those that utilize hydraulic clutches to change electric motor speeds, have been available for some time. However, several problems, including the difficulty and costs of installing mechanical ASDs, energy losses from friction, and high maintenance costs, have limited the widespread use of mechanical ASDs (EPRI 1984b).

Electronic ASDs appear to offer the most potential for future gains in ASD usage. These ASDs utilize solid-state electronic hardware and software to control motor speed. The most common type of electronic ASD controls motor speed by changing the frequency of the electric power input pulses provided to the motor (Hane et al. 1983). Electronic ASDs are more compact than mechanical

ESDs, which facilitates their ease of installation. In addition, because electronic ESDs have no moving parts, they have no friction, and both their energy losses and maintenance costs are reduced compared to mechanical ESDs.

The benefits of using ASDs will depend to a large degree upon the specific situation in which they are applied. These benefits can often include lower motor wear and tear, as well as energy cost savings. The back pressures produced by the use of control valves with constant speed motors are often considerable, and may quickly wear out component parts. ASDs can eliminate the need for control valves and the back pressures they produce.

A crucial factor in determining the relative benefits of ASDs is the variability in the required outputs of the electric motor drives on which ESDs can potentially be applied. If the required outputs from electric motor drives never vary, then ASDs provide no advantage compared to constant speed motors. The greater the variation in required outputs, the greater the likely benefits of using ASDs. The variation in required motor drive outputs can often differ from one motor drive to another within a single industrial plant. In this study, representative estimates of the variability of required outputs for electric motors will be used in deriving estimates of energy savings benefits of ASDs. It should be recognized, however, that these estimates are only representative and will not apply in all situations.

The market analysis of ASDs will be segmented into the same motor size categories as were used for high-efficiency motors (i.e., 1 to 5 horsepower (HP) motors, 5 to 20 HP motors, 20 to 50 HP motors, 50 to 125 HP motors, and motors larger than 125 HP). The analysis begins with a presentation of information on the current market situation of ASDs for electric motors.

13.2 CURRENT MARKET SITUATION

Both mechanical and electronic ASDs have been available for use in industrial applications for a number of years. However, the bulkiness of mechanical ASDs and reliability concerns about electronic ASDs have limited their historical market acceptance. In addition, electronic ASDs for alternating current (AC) motors have only been available for five years. Thus, a significant number of electric motors were excluded from using ASDs until recently.

ASDs are currently produced and marketed by most of the major electric motor manufacturers, including General Electric, Westinghouse Corporation, and Century Electric. Representatives of these companies report that interest in and sales of ASDs have been expanding in recent years.^(a,b) This reported growth in ASD sales supports forecasts made by the Electric Power Research Institute (EPRI 1984b) which predict that ASD usage will expand rapidly in the next 10 to 20 years. EPRI also reports that the current market penetration of ASDs is significantly below their potential market penetration.

13.3 COST EFFECTIVENESS AND MARKET PENETRATION

Evaluations of the cost effectiveness and likely market penetration of ASDs are presented in this section. The evaluations begin with the presentation of estimates on representative capital costs and payback periods for using ASDs on various sizes of motors. These estimates are then integrated with information on any technical factors that could limit the use of ASDs to derive estimates of the maximum potential market penetration of ASDs.

13.3.1 Cost Effectiveness of Adjustable Speed Drives

The cost effectiveness of ASDs for electric motors, as measured by their incremental capital costs and payback periods, are dependent upon the capital costs of purchasing and installing adjustable speed drives, the level of energy savings produced by using these drives, the value of these energy savings measured in dollars, and the reduction in operating costs that may result from using ASDs. These factors are addressed in this section.

Representative Capital Costs for ASDs

Price data from electric motor manufacturers were used in developing representative estimates of the capital costs of ASDs (Century Electric 1984 and Westinghouse Corporation 1984). These estimates are shown in Table 13.1

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- (a) Personal communication with Pete Graven, sales representative with General Electric Motor Division, Seattle, Washington, January 11, 1985.
 - (b) Personal communication with J. L. Sharpe, representative of Westinghouse Electric Corporation Control Division, Asheville, North Carolina, January 11, 1985.

TABLE 13.1. Representative Estimates of Adjustable Speed Drive Costs, 1984 Dollars^(a)

Motor Size (HP)	ASD Purchase Cost in New Applications (1984\$/Motor)	ASD Purchase and Installation Cost ^(b) in Retrofit Applications (1984\$/Motor)	Initial Cost for Standard Efficiency Motors ^(c) (\$1984)
1 - 5	1,490	1,860	245
5 - 20	6,425	8,030	545
21 - 50	13,060	16,325	1273
51 - 125	24,205	30,255	3849
>125	49,000	61,250	7370

- (a) Representative estimates derived by averaging estimates provided in Century Electrical Motor Product Catalogue, 1984 and Westinghouse Electric Corp. Price List 8710, 1984.
- (b) Purchase and installation cost calculated as purchase cost multiplied by 1.25. 25 percent cost premium estimate for installation cost obtained from information presented in a previous study (Hane et al. 1983).
- (c) Source: Calculated from data presented in Siemens-Allis Selection and Pricing Guide--Integral Horsepower AC Motors, 1984 and Century Electric Product Catalogue, 1984.

for the five motor size categories specified for use in this study. The estimates presented in Table 13.1 were derived by averaging list prices for ASDs offered by the manufacturers within the various size categories.

Estimates shown in the third column of Table 13.1 include the costs of installing ASDs in retrofit and retirement applications. Significant installation costs will often be incurred in implementing ASDs in existing motor installations because of space limitations around the motors and other factors. Although these costs will vary widely from one ASD application to another, an appropriate representative average cost for installing ASDs in retrofit and retirement applications is 25 percent of the ASD purchase cost (Hane et al. 1983). In new applications, the additional installation costs for incorporating ASDs in a motor drive system should not be significant.

The estimates presented in Table 13.1 imply that the incremental capital costs of ASDs for electric motors are significant. In comparing these

estimates to representative costs for electric motors (presented in the fourth column of Table 13.1), it can be seen that the costs for ASDs will generally be five to ten times larger than the costs of the electric motors upon which they are used.

Representative Percentage Energy Savings for ASDs

As stated previously, the energy savings resulting from using ASDs will vary significantly depending upon the amount of variability in the required output of the motor. However, no information on the relative degree of variability in required output from the various sizes of motors could be obtained within the time frame of this study. Thus, it was necessary to use average estimates of the percentage energy savings that should be expected from the use of ASDs to derive estimates of the kWh savings for ASDs.

EPRI has contracted for extensive field testing of ASDs and analyses of the energy savings that can be obtained from ASD usage. Information published by EPRI (EPRI 1984b) indicates that the percentage energy savings from using ASDs should generally range from 30 to 50 percent. The results of field tests of the use of ASDs in industrial applications ranging from waste water treatment to iron casting indicate that the percentage energy savings from ASDs will generally range from 20 percent to 65 percent (CRS Sirrine 1984). Estimates published in a previous study of ASDs (Hane et al. 1983) place the savings that should be expected from ASDs at a more conservative level of 25 percent to 30 percent.

An estimate of 35 percent will be used in this analysis to represent the average percentage energy savings for implementing ASDs on electric motors. This estimate is well within the range of the results of field tests of ASD effectiveness.

Representative kWh Savings for ASDs

In this study, representative kWh savings for ASDs are derived simply by multiplying the average estimate of the percentage energy savings for ASDs of 35 percent by representative estimates of the electricity consumed per unit by standard electric motors in the various size classifications. It is recognized that using one estimate of the percentage energy savings from ASDs for all

types of motors ignores the considerable variation in savings that is likely to occur from one ASD motor application to another. However, available information did not permit the development of disaggregate estimates of the percentage energy savings likely to result from the use of ASDs.

Representative estimates of the electricity consumption of standard electric motors were presented previously in Table 12.3 and are reproduced in Table 13.2. These estimates are used directly in deriving estimates of the kWh savings for ASDs. The methods used to develop the motor electricity consumption estimates were described in Chapter 12.0, and this description is not repeated here.

Representative Operating Cost Savings for ASDs

The reduction in operating cost savings from using ASDs will be a function of the energy cost savings that will result from ASD usage, and the reduction in motor-drive equipment repair and replacement costs produced by ASDs. Available evidence indicates that using ASDs will likely reduce motor-drive equipment repair and replacement costs. For example, a number of electric utility

TABLE 13.2. Representative Electricity Use per Motor for Conventional Electric Motors Calculated from a Baseline Electricity Use for Industrial Motor Drives of 632.7 billion kWh^(a)

Motor Size (HP)	Percent of Total Electricity Use in This HP Classification (%) ^(b)	Annual Electricity Use in This HP Classification (Billion kWh)	Estimated Number of Motors in This HP Class (000s) ^(b)	Annual Estimated Electricity Use Per Motor (kWh)
1 to 5	0.9	5.69	8082	704
5 to 20	7.7	48.72	5191	9,385
20 to 50	12.3	77.82	1973	39,442
50 to 125	24.0	151.85	928	163,629
>125	55.0	347.99	782	444,994

(a) Source: Documentation on the ISTUM forecasting model presented in The Least-Cost Energy Strategy--Technical Appendix, (Carhart et al. 1979).

(b) Source: Calculated from data presented in Classification and Evaluation of Electric Motors and Pumps, (Argonne National Laboratory 1980).

users of ASDs state that a major reason for installing ASDs on their generating plant motors drives was to reduce costly wear and tear on motor drive parts (EPRI 1984b).

No quantitative estimates of the savings in motor-drive equipment repair and replacement costs that will result from using ASDs could be obtained. Field tests of ASDs have generally not attempted to quantify these savings, although the results of such analyses demonstrate that equipment repair and replacement cost savings from using ASDs are likely.^(a)

It is believed that ignoring the equipment repair and replacement cost savings that will result from using ASDs, because of a lack of available data on the level of these savings, will tend to make the payback periods for ASDs longer than would generally be the case in real applications. Thus, in this study, the reduction in equipment repair and replacement costs from using ASDs is assumed to equal 10 percent of the energy cost savings for ASDs. These energy cost savings are calculated simply by multiplying representative kWh savings for ASDs by a representative average cost for electricity in the industrial sector of 4.97¢ per kWh (EIA 1984).

Representative Payback Periods for ASDs

Estimates of representative payback periods for ASDs on electric motors in both new and retirement/retrofit applications are presented in Tables 13.3 and 13.4. These results indicate that the payback periods for ASDs on motors of 50 HP or less in size will generally equal or exceed the expected lives of these motors.

It appears that ASD usage on motors of 50 HP or less in size is done for reasons other than reduced energy and equipment maintenance costs. In general, ASDs are used on small motors in situations where precise industrial process flow rates are required, and ASDs have already achieved a relatively high market share in such situations (EPRI 1984b). Prospects for increases in the usage of ASDs on motors of 50 HP or less in size appear limited.

(a) Personal communication with Tom Johnson, principle investigator on a study of industrial applications for ASDs, CRS Serrine Co., Research Triangle Park, North Carolina, January 23, 1985.

TABLE 13.3. Representative Payback Periods for Adjustable Speed Drives on Electric Motors in New Applications

Motor Size (HP)	Estimated Electricity Use for Conventional Motors (kWh)	Estimated Annual Electricity Cost Sav- ings ^(a) (\$)	Estimated Annual Equipment Cost Savings (\$)	Capital Costs for ASDs (\$)	Estimated Payback Period (Years)
1 to 5	704	12.25	1.37	1,490	109.4
6 to 20	9,385	163.25	18.27	6,425	35.4
21 to 50	39,442	686.09	76.76	13,060	17.1
51 to 125	163,629	2,846.33	318.42	24,205	7.7
>125	444,994	7,740.67	865.96	49,000	5.7

(a) Calculated by multiplying representative percentage electricity savings for ASDs of 35 percent by estimates of electricity use for conventional motors and an average cost for electricity of 4.97¢ per kWh.

TABLE 13.4. Representative Payback Periods for Adjustable Speed Drives on Electric Motors in Retirement/Retrofit Applications

Motor Size (HP)	Estimated Electricity Use for Conventional Motors (kWh)	Estimated Annual Electricity Cost Sav- ings ^(a) (\$)	Estimated Annual Equipment Cost Savings (\$)	Capital Costs for ASDs (\$)	Estimated Payback Period (Years)
1 to 5	704	12.25	1.37	1,860	136.6
6 to 20	9,385	163.25	18.27	8,030	44.2
21 to 50	39,442	689.09	76.76	16,325	21.4
51 to 125	163,629	2,946.33	318.42	30,255	9.3
>125	444,994	7,740.67	865.96	61,250	7.1

(a) Calculated by multiplying representative percentage electricity savings for ASDs of 35 percent by estimates of electricity use for conventional motors and an average cost for electricity of 4.97¢ per kWh.

Because of the long payback periods and poor prospects for increased market share for ASDs on motors of 50 HP or less in size, all further analysis of the energy savings potential for ASDs will be limited to applications on motors greater than 50 HP. This limitation is in agreement with the strategy employed in EPRI sponsored research on ASDs, which is limited to applications on electric motors that are generally greater than 100 HP in size.^(a)

13.3.2 Technical Limits on the Use of ASDs

No justification was found for applying technical limits to the use of ASDs in any applications where such use is cost effective.

13.3.3 Maximum Potential Market Penetration of ASDs

Estimates of the maximum market penetration for adjustable speed drives in the industrial are shown in Table 13.5 for motors exceeding 50 HP in size. These estimates were developed by applying the payback period estimates presented in Tables 13.3 and 13.4 to data presented previously in the first row of Table 4.2.

In selecting the appropriate maximum market penetration estimates for ASDs, the incremental capital costs for ASDs were ignored because incorporating these costs would have led to the conclusion that the maximum potential market

TABLE 13.5. Estimates of the Maximum Market Penetration Potential^(a) of Adjustable Speed Drives in New and Retirement/Retrofit Applications

Motor Size (HP)	Estimated Payback (Years) for ASDs in New Applications	Estimated Payback Period (Years) for ASDs in Retrofit/Retirement Applications	Estimated Maximum Market Penetration Potential (%) in New Applications	Estimated Maximum Market Penetration Potential (%) in Retirement/Retrofit Applications
50 to 125	6.9	9.3	20	20
>125	5.1	7.1	20	20

(a) Obtained from information from DOE/BERO presented previously in Table 4.2.

(a) Personal communication with Ralph Ferraro, manager of adjustable-speed drive industrial program, Electric Power Research Institute, Palo Alto, California, January, 1985.

penetration of ASDs is zero for all types of motors. Such a conclusion would be inconsistent with current market evidence that ASDs are already being used in some industrial situations and that interest in ASD usage is increasing rapidly. A maximum potential market penetration of 20 percent for ASDs is consistent with the current market situation for this equipment.

13.4 POPULATION DATA

Estimates of current electric motor populations, growth rates in these populations, and retirement rates for electric motors were developed previously in Chapter 12.0 of this paper and are reproduced in Table 13.6. The estimates for motors greater than 50 HP in size are used as a basis for deriving estimates of the number of potential applications of ASDs and the energy savings that will result from such applications. The method used to derive the estimates presented in Table 13.6 were explained previously in Section 12.4, and this explanation is not repeated here.

The estimates presented in Table 13.6 for motors greater than 50 HP in size were integrated with estimates of the maximum potential market penetration

TABLE 13.6. Current Electric Motor Populations, Growth Rates and Retirement Rates Employed in This Study

Motor Size (HP)	Current Motor Population ^(a) (000s)	Future Annual Growth Rate ^(b) (%)	Additional Units Added Annually (000s)	Annual Retirement Rate (%) ^(a)	Units Retired Annually (000s)
1 to 5	8082	7.2	582	5.8	473
5 to 20	5191	7.2	374	5.2	268
20 to 50	1973	7.2	142	4.6	91
50 to 125	928	7.2	67	3.5	32
>125	782	7.2	56	3.4	27

- (a) Source: Calculated from data presented in Classification and Evaluation of Electric Motors and Pumps, (Argonne National Laboratory 1980).
 (b) Source: Documentation on the ISTUM forecasting model presented in Proposed ISTUM Runs and Inputs, Outputs and Schedule, (EEA 1982).

of ASDs and an S-shaped market adoption rate (see Chapter 4.0) to develop estimates of the number of ASDs that will likely be installed between 1984 and 2000. A faster rate of market adoption was assumed for ASDs on motors greater than 125 HP in size compared to motors from 50 to 125 HP in size because of the shorter representative payback periods estimated for the larger motors. These annual estimates are presented in Tables 13.7 and 13.8.

13.5 ENERGY SAVINGS RESULTS

Estimates of the potential energy savings that are forecast to result from the implementation of adjustable speed drives on electric motors in selected years are shown in the last columns of Tables 13.7 and 13.8. Table 13.9 shows the energy savings as well as the number of adjustable speed drives projected to be installed on motors in the selected forecast years. The projected energy savings for ASDs (in BkWh) were obtained by multiplying representative estimates of the energy savings per unit (in kWh) for ASDs on motors greater than 50 HP by the projected number of ASDs that will be installed in each year. Representative estimates of the energy savings per unit for ASDs were 57,000 kWh for 50 to 125 HP motors and 156,000 kWh on motors greater than 125 HP in size.

The final column of Table 13.9 presents estimates of the potential electricity savings for ASDs in the industrial sector summed across all motors greater than 5 HP in size. These savings are expected to be approximately 51.2 BkWh in the year 2000.

13.6 SENSITIVITY ANALYSIS

An analysis was performed of the sensitivity of the energy savings estimates for ASDs to changes in the maximum potential market penetration the technology achieves and the rate at which this maximum is achieved. The results of this sensitivity analysis for both a low and a high scenario are presented in this section.

TABLE 13.7. Annual Market Share Projections - Adjustable Speed Drives on Industrial Electric Motors of 50 to 125 HP

Year	Number of 1984 and Pre- 1984 Motors Not Retired ^(a)	Number of New Motors ^(b)	Number of Retired Motors ^(c)	Retrofit Units Market Share ^(d)	Retired Units Market Share ^(d)	New Units Market Share ^(d)	Cumulative Retrofitted Units ^(e)	Annual Additions and Retirement In New Applications ^(f)	Cumulative Additions of ASD's ^(g)	Cumulative Energy Savings from ASD Installations ^(h) (BkWh)
1984	928,000	67,000	32,000	0.040	0.050	0.050	37,120	4,950	42,070	2.40
1985	896,000	67,000	32,000	0.041	0.051	0.051	36,736	5,049	46,735	2.66
1986	864,000	67,000	32,000	0.043	0.053	0.053	37,152	5,247	52,398	2.99
1987	832,000	67,000	32,000	0.046	0.056	0.056	38,292	5,544	59,062	3.37
1988	800,000	67,000	32,000	0.050	0.060	0.060	40,000	5,940	66,730	3.80
1989	768,000	67,000	32,000	0.055	0.065	0.065	42,240	6,435	75,405	4.30
1990	736,000	67,000	32,000	0.062	0.072	0.072	45,632	7,129	85,925	4.90
1991	704,000	67,000	32,000	0.070	0.080	0.080	49,280	7,820	97,493	5.56
1992	672,000	67,000	32,000	0.070	0.090	0.090	47,040	8,910	104,163	5.94
1993	640,000	67,000	32,000	0.090	0.100	0.100	57,600	9,900	124,623	7.10
1994	608,000	67,000	32,000	0.105	0.115	0.115	63,840	11,385	142,248	8.11
1995	576,000	67,000	32,000	0.120	0.130	0.130	69,120	12,870	160,398	9.14
1996	544,000	67,000	32,000	0.135	0.145	0.145	73,440	14,355	179,073	10.21
1997	512,000	67,000	32,000	0.150	0.160	0.160	76,800	15,840	198,273	11.30
1998	484,000	67,000	32,000	0.170	0.175	0.175	82,280	17,325	221,078	12.60
1999	452,000	67,000	32,000	0.190	0.190	0.190	85,880	18,810	243,488	13.88
2000	420,000	67,000	32,000	0.200	0.200	0.200	84,000	19,800	261,408	14.90

(a) Current original stock of motors estimated to be (Argonne National Laboratory 1980) minus number of retired motors.

(b) Growth in stock assumed to occur at a rate of 67,000 annually (EIA, 1982).

(c) Retirement assumed to occur at a rate of 32,000 annually (Argonne National Laboratory 1980).

(d) Based on methodology outlined in Chapter 4.0.

(e) Calculated by: (number of pre 1985 motors not retired) x (Retrofit Market Share).

(f) Calculated by: (annual new motors) x (new units market share) + (Annual Retired motors) x (Retired motors market share).

(g) Calculated by the sum of Cumulative Retrofitted Units plus each years annual additions in new and retirement situations.

(h) Calculated by: Cumulative units multiplied by 57,000 kWh/year.

TABLE 13.8. Annual Market Share Projections - Adjustable Speed Drives on Industrial Electric Motors Greater than 125 HP

Year	Number of 1984 and Pre- 1984 Motors Not Retired(a)	Number of New Motors(b)	Number of Retired Motors(c)	Retrofit Units Market Share(d)	Retired Units Market Share(d)	New Units Market Share(d)	Cumulative Retrofitted Units(e)	Annual Additions and Retirement In New Applications(f)	Cumulative Additions of ASD's(g)	Cumulative Energy Savings from ASD Installations(h) (BkWh)
1984	782,000	56,000	27,000	0.040	0.050	0.050	31,280	4,150	34,870	5.44
1985	755,000	56,000	27,000	0.043	0.053	0.053	32,465	4,399	39,894	6.22
1986	728,000	56,000	27,000	0.046	0.056	0.056	33,485	4,648	45,005	7.02
1987	701,000	56,000	27,000	0.050	0.060	0.060	35,050	4,980	50,987	7.95
1988	674,000	56,000	27,000	0.055	0.065	0.065	37,070	5,395	57,842	9.02
1989	647,000	56,000	27,000	0.0673	0.070	0.070	40,761	5,810	66,951	10.44
1990	620,000	56,000	27,000	0.073	0.080	0.080	45,260	6,640	77,698	12.12
1991	593,000	56,000	27,000	0.084	0.090	0.090	49,812	7,470	89,384	13.94
1992	566,000	56,000	27,000	0.100	0.105	0.105	56,600	8,715	104,607	16.32
1993	541,000	56,000	27,000	0.120	0.120	0.120	64,920	9,960	122,887	19.17
1994	512,000	56,000	27,000	0.140	0.140	0.140	71,690	11,620	141,267	22.04
1995	485,000	56,000	27,000	0.160	0.160	0.160	77,600	13,280	160,467	25.03
1996	458,000	56,000	27,000	0.180	0.180	0.180	82,440	14,940	180,247	28.12
1997	430,000	56,000	27,000	0.190	0.190	0.190	81,700	15,770	195,277	30.46
1998	404,000	56,000	27,000	0.195	0.195	0.195	78,780	16,185	208,542	32.53
1999	377,000	56,000	27,000	0.198	0.198	0.198	74,646	16,434	220,842	34.45
2000	350,000	56,000	27,000	0.200	0.200	0.200	70,000	16,600	232,796	36.32

(a) Current original stock of motors estimated to be (Argonne National Laboratory 1980) minus number of retired motors.

(b) Growth in stock assumed to occur at a rate of 56,000 annually (EIA, 1982).

(c) Retirement assumed to occur at a rate of 27,000 annually (Argonne National Laboratory 1980).

(d) Based on methodology outlined in Chapter 4.0.

(e) Calculated by: (number of pre 1985 motors not retired) x (Retrofit Market Share).

(f) Calculated by: (annual new motors) x (new units market share) + (Annual Retired motors) x (Retired motors market share).

(g) Calculated by the sum of Cumulative Retrofitted Units plus each years annual additions in new and retirement situations.

(h) Calculated by: Cumulative units multiplied by 156,000 kWh/year.

TABLE 13.9. Estimated Energy Savings (BkWh) and Number of Units Projected to Be Installed for Adjustable Speed Drives on Industrial Electric Motors

Year	50 to 125 HP Motors		>125 HP Motors		All Motors >50 HP	
	No. of Motors Projected to Be Installed	Estimated Energy Savings	No. of Motors Projected to Be Installed	Estimated Energy Savings	No. of Motor Projected to Be Installed	Estimated Energy Savings
1985	46,735	2.66	39,894	6.22	86,629	8.88
1990	85,925	4.40	77,698	12.12	163,623	17.02
1995	160,398	9.14	164,674	29.03	324,072	34.17
2000	261,408	14.90	232,796	36.32	494,204	51.22

13.6.1 Low Market Penetration Scenario

The maximum potential market penetration assumed in the low scenario of the sensitivity analysis for ASDs was 10 percent for both 50 to 125 HP motors and motors greater than 125 HP. This number was half as large as that assumed in the baseline analysis. It was also assumed that only 75 percent of the maximum potential market penetration would be achieved by the year 2000. These assumptions resulted in the use of an estimate of 7.5 percent market penetration for ASDs by the year 2000 on all motors greater than 50 HP in size.

The results of using an estimate of 7.5 percent market penetration by 2000 and other low scenario market penetration assumptions are shown in Tables 13.10 and 13.11. The total estimated energy savings for ASDs by 2000 is 34.92. The results are summarized for selected years in Table 13.12.

13.6.2 High Market Penetration Scenario

The maximum potential market penetration assumed for ASDs in the high scenario was 40 percent for all motors greater than 50 HP in size. It was also assumed that a rapid rate of market adoption would cause this maximum penetration to be reached by 1995.

The results obtained using the high scenario market penetration assumptions are shown in Table 13.13 and 13.14. The total estimated energy savings in the year 2000 are 107.46 BkWh. The results are summarized for selected years in Table 13.15.

TABLE 13.10. Low Scenario Annual Market Share Projections - Adjustable Speed Drives on Industrial Electric Motors of 50 to 125 HP

Year	Number of 1984 and Pre- 1984 Motors Not Retired(a)	Number of New Motors(b)	Number of Retired Motors(c)	Retrofit Units Market Share(d)	Retired Units Market Share(d)	New Units Market Share(d)	Cumulative Retrofitted Units(e)	Annual Additions and Retirement In New Applications(f)	Cumulative Additions of ASD's(g)	Cumulative Energy Savings from ASD Installations(h)
1984	928,000	67,000	32,000	0.030	0.040	0.040	27,840	3,960	31,800	1.81
1985	896,000	67,000	32,000	0.041	0.041	0.041	36,736	4,059	44,755	2.55
1986	864,000	67,000	32,000	0.043	0.043	0.043	37,152	4,257	49,428	2.82
1987	832,000	67,000	32,000	0.045	0.045	0.045	37,440	4,455	54,171	3.09
1988	800,000	67,000	32,000	0.049	0.049	0.049	39,200	4,851	60,782	3.46
1989	768,000	67,000	32,000	0.053	0.053	0.053	40,704	5,247	67,533	3.85
1990	736,000	67,000	32,000	0.056	0.056	0.056	41,216	5,544	73,589	4.19
1991	704,000	67,000	32,000	0.061	0.061	0.061	42,944	6,039	81,356	4.64
1992	672,000	67,000	32,000	0.065	0.065	0.065	43,680	6,435	88,527	5.05
1993	640,000	67,000	32,000	0.067	0.067	0.067	42,880	6,633	94,360	5.38
1994	608,000	67,000	32,000	0.069	0.069	0.069	41,952	6,831	100,263	5.71
1995	576,000	67,000	32,000	0.070	0.070	0.070	40,320	6,930	105,561	6.02
1996	544,000	67,000	32,000	0.071	0.071	0.071	38,624	7,029	110,894	6.32
1997	512,000	67,000	32,000	0.072	0.072	0.072	36,864	7,128	116,262	6.63
1998	484,000	67,000	32,000	0.073	0.073	0.073	35,332	7,227	121,957	6.95
1999	452,000	67,000	32,000	0.074	0.074	0.074	33,448	7,326	127,399	7.26
2000	420,000	67,000	32,000	0.075	0.075	0.075	31,500	7,425	132,876	7.57

(a) Current original stock of motors estimated to be (Argonne National Laboratory 1980) minus number of retired motors.

(b) Growth in stock assumed to occur at a rate of 67,000 annually (EIA, 1982).

(c) Retirement assumed to occur at a rate of 32,000 annually (Argonne National Laboratory 1980).

(d) Based on methodology outlined in Chapter 4.0.

(e) Calculated by: (number of pre 1985 motors not retired) x (Retrofit Market Share).

(f) Calculated by: (annual new motors) x (new units market share) + (Annual Retired motors) x (Retired motors market share).

(g) Calculated by the sum of Cumulative Retrofitted Units plus each years annual additions in new and retirement situations.

(h) Calculated by: Cumulative units multiplied by 57,000 kWh/year.

TABLE 13.11. Low Scenario Annual Market Share Projections - Adjustable Speed Drives on Industrial Electric Motors Greater than 125 HP

Year	Number of 1984 and Pre- 1984 Motors Not Retired ^(a)	Number of New Motors ^(b)	Number of Retired Motors ^(c)	Retrofit Units Market Share ^(d)	Retired Units Market Share ^(d)	New Units Market Share ^(d)	Cumulative Retrofitted Units ^(e)	Annual Additions and Retirement In New Applications ^(f)	Cumulative Additions of ASD's ^(g)	Cumulative Energy Savings from ASD Installations ^(h) (BkWh)
1984	782,000	56,000	27,000	0.030	0.040	0.040	23,460	24,540	26,780	4.18
1985	755,000	56,000	27,000	0.031	0.041	0.041	23,405	24,512	30,128	4.70
1986	728,000	56,000	27,000	0.033	0.043	0.043	24,024	25,185	34,316	5.35
1987	701,000	56,000	27,000	0.035	0.045	0.045	24,535	25,750	38,562	6.02
1988	674,000	56,000	27,000	0.039	0.049	0.049	26,286	27,609	44,380	6.92
1989	647,000	56,000	27,000	0.043	0.053	0.053	27,871	29,252	50,314	7.85
1990	620,000	56,000	27,000	0.047	0.056	0.056	29,140	30,652	56,281	8.78
1991	593,000	56,000	27,000	0.052	0.061	0.061	30,836	32,483	63,040	9.83
1992	566,000	56,000	27,000	0.059	0.065	0.065	33,394	35,149	70,993	11.07
1993	541,000	56,000	27,000	0.063	0.067	0.067	34,083	35,892	77,243	12.05
1994	512,000	56,000	27,000	0.066	0.069	0.069	33,792	35,655	82,679	12.90
1995	485,000	56,000	27,000	0.069	0.070	0.070	33,465	35,355	88,162	13.75
1996	458,000	56,000	27,000	0.071	0.071	0.071	32,518	34,435	93,108	14.52
1997	430,000	56,000	27,000	0.072	0.072	0.072	30,960	32,904	97,526	15.21
1998	404,000	56,000	27,000	0.073	0.073	0.073	29,492	31,463	102,117	15.93
1999	377,000	56,000	27,000	0.074	0.074	0.074	27,898	29,896	106,665	16.64
2000	350,000	56,000	27,000	0.075	0.075	0.075	26,250	28,275	111,242	17.35

(a) Current original stock of motors estimated to be (Argonne National Laboratory 1980) minus number of retired motors.

(b) Growth in stock assumed to occur at a rate of 56,000 annually (EIA, 1982).

(c) Retirement assumed to occur at a rate of 27,000 annually (Argonne National Laboratory 1980).

(d) Based on methodology outlined in Chapter 4.0.

(e) Calculated by: (number of pre 1985 motors not retired) x (Retrofit Market Share).

(f) Calculated by: (annual new motors) x (new units market share) + (Annual Retired motors) x (Retired motors market share).

(g) Calculated by the sum of Cumulative Retrofitted Units plus each years annual additions in new and retirement situations.

(h) Calculated by: Cumulative units multiplied by 156,000 kWh/year.

TABLE 13.12. Low Scenario Estimated Energy Savings (BkWh) and Number of Units Projected to Be Installed for Adjustable Speed Drives on Industrial Electric Motors

Year	50 to 125 HP Motors		>125 HP Motors		All Motors >50 HP	
	No. of Motors Projected to Be Installed	Estimated Energy Savings	No. of Motors Projected to Be Installed	Estimated Energy Savings	No. of Motor Projected to Be Installed	Estimated Energy Savings
1985	44,755	2.55	30,128	4.70	74,883	7.25
1990	67,533	3.85	56,281	8.78	123,814	12.65
1995	105,561	6.02	88,162	13.75	193,725	19.77
2000	132,876	7.57	111,242	17.35	244,118	34.92

13.7 COST PER KWH OF ENERGY SAVED CALCULATIONS AND COMPARISONS TO THE COST PER KWH OF PRODUCING NEW GENERATING CAPACITY

Comparisons of the estimated levelized costs per kWh for ASDs versus the estimated costs per kWh for new generating plants are presented in this section. Representative estimates of the levelized costs per kWh saved for ASDs on electric motors are presented in Tables 13.16 and 13.17.

The estimated costs per kWh saved for ASDs in new retirement and retrofit applications on motors less than 50 HP in size are significantly higher than an estimated average generation cost for new coal-fired generating plants of 5.82¢/kWh (presented in Table 4.3). However, the estimated costs per kWh saved for ASDs on motors greater than 50 HP in size are below the estimated average new coal-plant generating cost. The ASD costs per kWh saved on motors greater than 50 HP in size are also less than the regional cost of new power estimates (presented in Table 4.3) in most regions of the country.

TABLE 13.13. High Scenario Annual Market Share Projections - Adjustable Speed Drives on Industrial Electric Motors of 50 to 125 HP

Year	Number of 1984 and Pre- 1984 Motors Not Retired(a)	Number of New Motors(b)	Number of Retired Motors(c)	Retrofit Units Market Share(d)	Retired Units Market Share(d)	New Units Market Share(d)	Cumulative Retrofitted Units(e)	Annual Additions and Retirement In New Applications(f)	Cumulative Additions of ASD's(g)	Cumulative Energy Savings from ASD Installations(h)
1984	928,000	67,000	32,000	0.040	0.050	0.050	37,120	4,950	42,070	2.40
1985	896,000	67,000	32,000	0.042	0.052	0.052	37,632	5,148	47,730	2.72
1986	864,000	67,000	32,000	0.045	0.055	0.055	38,880	5,445	54,423	3.10
1987	832,000	67,000	32,000	0.055	0.065	0.065	45,760	6,435	67,738	3.86
1988	800,000	67,000	32,000	0.070	0.080	0.080	56,000	7,920	85,898	4.90
1989	768,000	67,000	32,000	0.100	0.110	0.110	76,800	10,890	117,588	6.70
1990	736,000	67,000	32,000	0.140	0.150	0.150	103,040	14,850	158,678	9.04
1991	704,000	67,000	32,000	0.190	0.200	0.200	133,760	19,800	209,198	11.92
1992	672,000	67,000	32,000	0.250	0.260	0.260	168,000	25,740	269,178	15.34
1993	640,000	67,000	32,000	0.320	0.320	0.320	204,800	31,680	337,658	19.25
1994	608,000	67,000	32,000	0.370	0.370	0.370	224,960	36,630	394,448	22.48
1995	576,000	67,000	32,000	0.400	0.400	0.400	230,400	39,600	439,488	25.05
1996	544,000	67,000	32,000	0.400	0.400	0.400	217,600	39,600	466,288	26.58
1997	512,000	67,000	32,000	0.400	0.400	0.400	204,800	39,600	493,088	28.11
1998	484,000	67,000	32,000	0.400	0.400	0.400	193,600	39,600	521,488	29.72
1999	452,000	67,000	32,000	0.400	0.400	0.400	180,800	39,600	548,288	31.25
2000	420,000	67,000	32,000	0.400	0.400	0.400	168,000	39,600	575,088	32.78

(a) Current original stock of motors estimated to be (Argonne National Laboratory 1980) minus number of retired motors.

(b) Growth in stock assumed to occur at a rate of 67,000 annually (EIA, 1982).

(c) Retirement assumed to occur at a rate of 32,000 annually (Argonne National Laboratory 1980).

(d) Based on methodology outlined in Chapter 4.0.

(e) Calculated by: (number of pre 1985 motors not retired) x (Retrofit Market Share).

(f) Calculated by: (annual new motors) x (new units market share) + (Annual Retired motors) x (Retired motors market share).

(g) Calculated by the sum of Cumulative Retrofitted Units plus each years annual additions in new and retirement situations.

(h) Calculated by: Cumulative units multiplied by 57,000 kWh/year.

TABLE 13.14. High Scenario Annual Market Share Projections - Adjustable Speed Drives on Industrial Electric Motors Greater than 125 HP

Year	Number of 1984 and Pre- 1984 Motors Not Retired ^(a)	Number of New Motors ^(b)	Number of Retired Motors ^(c)	Retrofit Units Market Share ^(d)	Retired Units Market Share ^(d)	New Units Market Share ^(d)	Cumulative Retrofitted Units ^(e)	Annual Additions and Retirement In New Applications ^(f)	Cumulative Additions of ASD's ^(g)	Cumulative Energy Savings from ASD Installations ^(h) (BkWh)
1984	782,000	56,000	27,000	0.040	0.050	0.050	31,280	4,150	35,430	5.53
1985	755,000	56,000	27,000	0.042	0.052	0.052	31,710	4,316	40,176	6.27
1986	728,000	56,000	27,000	0.045	0.055	0.055	32,760	4,565	45,791	7.14
1987	701,000	56,000	27,000	0.055	0.065	0.065	38,555	5,395	56,981	8.89
1988	674,000	56,000	27,000	0.070	0.080	0.080	47,180	6,640	72,246	11.27
1989	647,000	56,000	27,000	0.100	0.110	0.110	64,700	9,130	98,896	15.43
1990	620,000	56,000	27,000	0.140	0.150	0.150	86,800	12,450	133,446	20.82
1991	593,000	56,000	27,000	0.190	0.200	0.200	112,670	16,600	175,916	27.44
1992	566,000	56,000	27,000	0.250	0.260	0.260	141,500	21,580	226,326	35.31
1993	541,000	56,000	27,000	0.320	0.320	0.320	173,120	26,560	284,506	44.38
1994	512,000	56,000	27,000	0.370	0.370	0.370	189,440	30,710	331,536	51.72
1995	485,000	56,000	27,000	0.400	0.400	0.400	194,000	33,200	369,296	57.61
1996	458,000	56,000	27,000	0.400	0.400	0.400	183,200	33,200	391,696	61.10
1997	430,000	56,000	27,000	0.400	0.400	0.400	172,000	33,200	413,696	64.54
1998	404,000	56,000	27,000	0.400	0.400	0.400	161,600	33,200	436,496	68.09
1999	377,000	56,000	27,000	0.400	0.400	0.400	150,800	33,200	458,896	71.59
2000	350,000	56,000	27,000	0.400	0.400	0.400	140,000	33,200	481,296	75.08

(a) Current original stock of motors estimated to be (Argonne National Laboratory 1980) minus number of retired motors.

(b) Growth in stock assumed to occur at a rate of 56,000 annually (EIA, 1982).

(c) Retirement assumed to occur at a rate of 27,000 annually (Argonne National Laboratory 1980).

(d) Based on methodology outlined in Chapter 4.0.

(e) Calculated by: (number of pre 1985 motors not retired) x (Retrofit Market Share).

(f) Calculated by: (annual new motors) x (new units market share) + (Annual Retired motors) x (Retired motors market share).

(g) Calculated by the sum of Cumulative Retrofitted Units plus each years annual additions in new and retirement situations.

(h) Calculated by: Cumulative units multiplied by 156,000 kWh/year.

TABLE 13.15. High Scenario Estimated Energy Savings and Number of Units Projected to Be Installed for Adjustable Speed Drives on Industrial Electric Motors

Year	50 to 125 HP Motors		>125 HP Motors		All Motors >50 HP	
	No. of Motors Projected to Be Installed	Estimated Energy Savings	No. of Motors Projected to Be Installed	Estimated Energy Savings	No. of Motor Projected to Be Installed	Estimated Energy Savings
1985	47,730	2.72	40,176	6.27	87,906	8.99
1990	158,678	9.04	133,446	20.82	292,124	29.86
1995	439,388	25.05	369,296	57.61	808,684	82.66
2000	575,088	32.78	481,296	75.08	1,056,284	107.86

TABLE 13.16. Cost per kWh Saved Calculations for Adjustable Speed Drives on Electric Motors in New and Retirement Applications

Motor Size (HP)	Incremental Capital Cost (1984 \$) in New and Retirement Applications (a)	Levelized Capital Cost (\$/year) (b)	Annual Energy Savings (kWh/year) (c)	Cost per kWh Saved in New and Retirement Applications (¢/kWh) (d)
1 to 5	1,490	153.95	246	62.58
6 to 20	6,425	654.40	3,285	190.92
21 to 50	13,060	1,330.19	13,805	9.64
51 to 125	24,205	2,465.33	57,270	4.30
>125	49,000	4,990.76	155,748	3.20

(a) See Table 13.1.

(b) The level stream of annual payments the present value of which would equal the investment's incremental capital cost. The levelized cost was calculated using an 8 percent discount rate and operating lifetimes of 20 years for adjustable speed drives.

(c) Calculated as the percent electricity savings for adjustable speed drives (35 percent) multiplied by the estimated electricity use in kWh for conventional motors (from Table 13.2).

(d) Calculated as levelized capital costs (\$/year) divided by annual energy savings (kWh/year) and multiplied by 100.

TABLE 13.17. Cost per kWh Saved Calculations for Adjustable Speed Drives on Electric Motors in Retrofit Applications

Motor Size (HP)	Incremental Capital Cost (1984 \$) in Retrofit Applications (a)	Levelized Capital Cost (\$/year) (b)	Annual Energy Savings (kWh/year) (c)	Cost per kWh Saved in New and Retirement Applications (\$/kWh) (d)
1 to 5	1,860	189.45	246	77.01
6 to 20	8,030	817.87	3,285	24.90
21 to 50	16,325	1,662.74	13,805	12.04
51 to 125	30,255	3,081.54	57,270	5.38
>125	61,250	6,238.45	155,748	4.01

(a) See Table 13.1.

(b) The level stream of annual payments the present value of which would equal the investment's incremental capital cost. The levelized cost was calculated using an 8 percent discount rate and operating lifetimes of 20 years for adjustable speed drives.

(c) Calculated as the percent electricity savings for adjustable speed drives (35 percent) multiplied by the estimated electricity use in kWh for conventional motors (from Table 13.2).

(d) Calculated as levelized capital costs (\$/year) divided by annual energy savings (kWh/year) and multiplied by 100.

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14.0 ELECTROLYTIC PROCESSES: THE CASE OF ALUMINUM

This chapter analyzes the impacts on energy use of new conservation technologies for industrial electrolytic processes. Electrolytic processes are processes that use electrical energy to produce chemical changes. In industry, electrolytic processes are used to convert raw or only partially refined materials to materials having more useful and valuable properties. Electrolysis is used for the chlor-alkali process, electroplating, electrolytic production of magnesium, manganese, zinc and copper, aluminum production and specialty applications (Beck 1977; Van Nostrands 1983; Jansson 1984). The primary metals industry uses the most energy for electrolytic processes, and aluminum production accounts for almost all of this energy use (Whitaker 1984). Aluminum production is analyzed in detail because only one case study could be performed due to resource constraints, and the electrolytic smelting of aluminum uses more electricity than any other United States industrial electrolytic process.

Section 14.1 provides technical background for the existing smelting process and for potential efficiency improvements. The current and likely future market situation for U.S. aluminum producers is described in Section 14.2. Section 14.3 discusses technologies, estimated costs and energy conservation possibilities of a potential retrofit measures and a potential new process. Technical limits and market penetration assumptions are also discussed in Section 14.3. Section 14.4 develops values for baseline projections of U.S. aluminum production; the market penetration estimates developed in Section 14.3 for new technologies are applied to these production estimates. Section 14.5 presents energy savings results and assumptions. Section 14.6 analyzes the sensitivity of the energy savings results to changes in the market penetration scenario. Section 14.7 concludes the analysis with an estimate of the estimated cost per kWh saved from electrolytic process improvements in aluminum smelting.

14.1 TECHNICAL BACKGROUND

Aluminum production is a three stage process. First bauxite, a mined mineral ore containing aluminum oxide (Al_2O_3), is refined to obtain the

aluminum oxide. Next, the aluminum oxide (also referred to as alumina) is smelted and chemically changed to pure aluminum metal (Al). This chapter focuses on the conversion from alumina to aluminum, which is an electrolytic process. In the third stage of aluminum production, the aluminum metal is fabricated into foil, sheets and other saleable shapes.

There are two kinds of electrolytic processes: reduction and oxidation. Whenever one substance is oxidized, another is reduced and vice versa. The conversion of alumina to aluminum is a chemical reduction in which the alumina is reduced. Carbon is simultaneously oxidized. In the United States, all but experimental alumina reduction is performed using the Hall-Heroult process, which is explained in the following paragraphs (Pierce et al. 1984).

Alumina reduction occurs in an area called a cell or a pot. The Hall cell is made of steel and has a baked carbon lining. The reduction cell is 10 to 15 feet wide, 20 to 40 feet long, and 3 to 4 feet deep (Berk et al. 1982). It is filled with a medium that conducts electricity (an electrolyte). In Hall-Heroult cells, molten cryolite (Na_3AlF_6) serves as a large electrolyte bath.

Electricity is conducted into the cell at a carbon anode; the anode is the cell's negative pole. The electricity is passed through the electrolyte to the cathode, the cell's positive pole. The anode and cathode are referred to collectively as electrodes. The electric current is conducted out of the cell through steel bars (Beck 1977).

The carbon anode is partly consumed in the smelting process and needs regular replacement. The method of anode replacement distinguishes two variants of the Hall process: the Soderberg process and the prebake process. Prebaked anodes are more common in the United States, are replaced less frequently than Soderberg anodes, and are more energy-efficient than Soderberg anodes (Pierce et al. 1984).

The theoretical minimum energy use per pound of aluminum reduced is 2.89 kWh, assuming 100 percent efficiency of the overall cell reaction (Beck

1977)).^(a) As of October 1983, the industry average Hall-cell energy consumption was 7.5 kWh per pound of aluminum produced (Aluminum Association 1983). Thus, the industry average efficiency was approximately 39 percent, despite widespread use of prebaked anodes. This is an improvement: the average was 12 kWh per pound during World War II, and was 8 kWh per pound as recently as 1980 (Cochran 1981).

Almost 40 percent of Hall-Heroult cell power losses are due to electrolyte resistance between the anode and the cathode. These losses cannot be eliminated using molten cryolite as the electrolyte. However, in a technology for new smelters, molten cryolite is replaced with a chloride bath, and several other changes are made in the smelting process to make the use of a chloride electrolyte feasible. This technology, called the Alcoa process, saves electricity because the chloride bath conducts electricity better than the cryolite medium and has lower resistance losses over equivalent distances. Resistance losses are also dependent on the distance between the electrodes, and decrease as the interelectrode separation decreases. The interelectrode separation in a chloride bath electrolyte can be smaller than in a cryolite electrolyte, again contributing to smaller power losses. The Alcoa process has as much as 30 percent energy savings over the Hall-Heroult cell (Peacey and Davenport 1974; Jarrett 1984; Beck 1977).

A retrofit measure to decrease the interelectrode separation in the Hall-Heroult cell, and thereby decrease power losses due to resistance, involves the use of a titanium diboride cathode coating. In conventional cells, the cathode is essentially a mass of molten aluminum that is very unstable. A titanium diboride coating would permit the reduction of interelectrode separation by stabilizing the cathode. Aluminum metal would deposit on the titanium diboride plates and drip down into collecting wells. Although early estimates indicated energy savings of 6 to 15 percent over the standard Hall cell, more recent estimates are for about 2 percent energy savings (Beck 1977; Whitaker 1984).

(a) The overall cell reaction is:

It takes place at 975°C (Beck 1977).

Some power inefficiency occurs because of an electrolytic reaction between the anode, which is made of carbon, and cathodically deposited aluminum. An inert anode, that is not destroyed by electrolytic action, is another retrofit possibility that might someday decrease electric power consumption of smelters. Some patents for inert anodes using a tin oxide material exist, but to date no commercial development efforts have succeeded (Jarrett 1984). If development efforts are successful, one estimate indicates that such inert anodes have energy savings potential of up to 35 percent (Whitaker 1984).

Potential energy-conserving technologies that are described elsewhere in the literature include carbothermic reduction (Landi, DaRoit and Piras 1984), the Alcan process (Rogers, MacMillan and Wright 1984), and some standard pot modifications to reduce power losses in old plants (Chaudhry 1984). The technologies selected for further analysis in this chapter are the Alcoa process, for new smelters, and the titanium diboride cathode coating, for retrofits of existing smelters. These technologies are not fully developed, and only preliminary cost estimates are available. However, measures that are both technically mature and economically sensible are already adopted by the industry. The industry pays considerable attention to reducing electric power costs for smelting and appears to apply the mix of measures available to it to achieve energy conservation goals.

14.2 CURRENT MARKET SITUATION

All commercial alumina reduction in the United States is performed using the Hall-Heroult process (Pierce et al. 1984). The industry has experimented with several alternatives to conventional Hall-Heroult smelting, but commercial potential for all these measures appears limited. Unfortunately, power costs for this country are so much higher than at other locations in Canada and overseas (Brazil and Australia, for example), that potential energy conservation measures for U.S. plants are becoming increasingly irrelevant. The very high power rates encourage efficiency, but it may (and often does) cost less to relocate than to undertake the retrofitting that would be needed to obtain an efficient plant (Kennedy 1985).

Most U.S. aluminum smelters were built when electric power was relatively inexpensive. The plants are relatively old; in 1980 their average age was 20.5 years (Aluminum Association 1980). Most likely, these old plants will not be replaced, and new capacity will be built outside the United States where power rates are much more attractive. The average cost to aluminum smelters for electric power is 23 mills in the United States (1983); the free world average, excluding the United States and some high energy-cost Asian countries, is 12 mills; and in Canada, power can be obtained for approximately 3 mills per kWh.^(a) In an industry where electricity costs constitute 19 to 30 percent of all variable cost of production (from bauxite to fabricated products), these power cost differentials are extremely significant (Aluminum Association 1980; Whitaker 1984).

Worldwide demand for aluminum products will likely grow, despite competition from substitute materials (Berk et al. 1982). Aluminum continues to be a versatile material that is reliable and cost effective in numerous applications. However, primary aluminum production is shifting out of the United States. The share of world production capacity accounted for by the United States was 45 percent in 1970; this share has been declining and is forecast to decrease to 26 percent by 1990 (Kennedy 1985). The U.S. share of world production declined from about a third in 1980-1981 to 24 percent by 1984 (Berk et al. 1982; Jarrett 1984). Capacity is higher than production because plants are operated below capacity.

The commercial development of the Alcoa process has been severely hampered by the current U.S. market situation for producers of primary aluminum. This is because further development is necessary to make the system economical for commercial aluminum production, even though a pilot plant has already demonstrated the potential for large power savings. Joint technology development between Arco and Alcoa seemed likely to produce a more economical system until recently. Now, however, Arco is exiting the primary metals business and the effort that had been planned is unlikely to occur.^(b)

(a) Conversations with Noel Jarrett, Alcoa, and James S. Kennedy, U.S. Department of Commerce.

(b) Noel Jarrett, Alcoa Laboratories, personal communication.

The titanium diboride cathode coating is used on an experimental basis. Kaiser Aluminum is working with the U.S. Department of Energy on this technology (final report forthcoming). Martin Marietta has developed and tested an effective low cost TiB_2 coating, but the material is proprietary (Boxall and Cooke 1984). Thus, the titanium diboride cathode coating is in late stages of development, but no commercial product is generally available.

14.3 COST EFFECTIVENESS AND MARKET PENETRATION

In this section, the adoption of the technologies described in Section 14.1 is estimated according to the methodology described in Chapter 4.0. First-cost increases and payback periods for the Alcoa process on new plants and titanium diboride (TiB_2) cathode coatings on retrofits are presented in Section 14.3.1. The base case is a U.S. Hall-Heroult plant with capacity of 160,000 tons of aluminum annually. Although, given the current market situation, the base case would be more realistic if it represented capital and operating costs of a new plant overseas, resources did not permit such cost comparisons. Technical limits are discussed in Section 14.3.2. Since neither technology is yet used commercially, it is difficult to verify technical limits that may be encountered in commercial operation. Market penetration assumptions are presented in Section 14.3.3.

14.3.1 Simple Payback of Alcoa Process, for New Plants and Titanium Diboride (TiB_2) Coating for Retrofit Applications

In the Alcoa plant, overall production costs appear to have been greater than anticipated at earlier research stages despite large power savings. This may be attributable to the need for a different, more expensive feedstock for the Alcoa process as opposed to the Hall-Heroult process. The costs of constructing and operating the pilot plant are not publicly available, and a payback period cannot be calculated without these data. However, payback periods for the Alcoa process are largely irrelevant to the analysis of probable electricity use by electrolytic processes in U.S. aluminum production, since it is unlikely that new aluminum production facilities will be added to existing United States capacity. The process is for new plants, so its commercial prospects in the United States are extremely poor.

The costs of retrofitting an existing Hall plant with titanium diboride coated cathodes are difficult to confirm, since this technology is not yet available on a general unproprietary basis. A representative payback period of 3 to 4 years is calculated in Table 14.1 from the data that are available. Energy savings are estimated to be about 2 percent (Whitaker 1984).

TABLE 14.1. Simple Payback of Titanium Diboride Cathode Coating for Retrofits of Hall-Heroult Cells

	First Cost ^(a) (\$ per ton of capacity)	Annual Savings ^(b) (\$ per year per ton of capacity)	Simple ^(c) Payback (years)
Hall with TiB ₂	22.95	6.90	3.3 yr

(a) First Cost = 0.9 percent of fixed capital investment (Skovronek et al. 1976)
 x \$2,550 capital investment per annual ton capacity (Castera 1984)
 = \$22.95 per ton capacity.

(b) Cost Savings Per Ton
 Per Year = 2 percent energy savings (Whitaker 1984)
 x 7.5 kWh per pound (U.S. industry average; Aluminum Association 1983).
 x 2000 pounds per ton.
 x 23 mills per kWh (U.S. industry average; Kennedy 1985).
 x \$1/1000 mills
 = \$6.90 per year per ton.

(c) Obtained by dividing first cost by annual savings.

14.3.2 Technical Limits

Several problems are often experienced with TiB₂ in aluminum smelting cells. These problems include chemical instability, poor resistance to thermal shock and impact, and/or intergranular penetration (Jarrett 1984; Boxall and Cooke 1984). A proprietary material that Martin Marietta developed may circumvent these problems (Boxall and Cooke 1984). This material would give the retrofit cathodes a 3 to 5 year life. To account for technical problems whose

solutions are not publicly available, retrofitting with TiB_2 cathodes is assumed to occur no earlier than the eighth year of the forecast period (i.e., 1991). In addition, a 4-year lifetime is assumed.

14.3.3 Market Penetration Assumptions

The process for new plants, i.e. the Alcoa process, is assumed to have no market penetration. The retrofit measure of coating cathodes with TiB_2 is estimated to have a maximum market penetration of 50 percent, with no adoption of the technology until 1991. This estimate is based on a payback of 3.3 years, calculated in Section 14.3.1, a first cost increase of less than 10 percent, and technical limits discussed in Section 14.3.2. The maximum market penetration depends on the methodology in Chapter 4.0 (refer to Table 4.2).

14.4 POPULATION DATA

This section develops assumptions for primary aluminum production in the United States for the years 1985-2000. Market share estimates for TiB_2 -retrofitted production capacity are also summarized. These estimates are based on the market penetration assumptions discussed in Section 14.3.3.

Industry experts expect that aluminum production will continue to shift away from the developed economies to the bauxite producers (Fitzgerald and Pollio 1982; Berk et al. 1982). No U.S. capacity additions are expected in the projection period, and several plant retirements are likely to occur. Estimates of U.S. aluminum primary capacity and utilization, in 1983 and in 2000, are shown in Table 14.2.

The assumed primary capacity in 2000 was chosen by eliminating all U.S. capacity with less than 50 percent capacity utilization in 1983 from the capacity base, except in the Pacific Northwest where the only smelter assumed to continue operating is Intalco. Data on capacity utilization are summarized in Adams et al. (1983). This process of elimination is intended to select out the least efficient plants, i.e., those that are first to be idled. This scenario eliminates all but 2,749,000 tons per year primary capacity by the year 2000. Assumed capacity utilization is 80 percent for all projection years. The

TABLE 14.2. Estimates of 1983 Capacity Utilization and Primary Aluminum Production, with Assumptions Regarding Capacity and Utilization in 2000

	U.S. Total Estimated Primary Capacity (10^3 TPY)	U.S. Aluminum Production (10^3 T)	% Capacity Utilization (/100)
1983	5,526 ^(a)	3,640 ^(b)	0.66
2000	2,749	2,199	0.80

(a) Adams et al. 1983.

(b) Jarrett 1984.

decline in production is assumed to occur at a constant rate of 4.2 percent beginning in 1983 and ending in 2000. Approximately half of the projected decline is estimated to occur in the first 5 years.

Table 14.3 shows results of the market share calculations. The first retrofits occur in 1991; market penetration increases to 50 percent by 2000. Details of the market share calculation may be found in Table 14.4

The scenario in Table 14.3 shows U.S. primary aluminum capacity diminishing by approximately 4.2 percent per year. Observations of industry experts lead one to believe that this scenario is optimistic. In contrast, scenarios

TABLE 14.3. Estimates for Cathode Retrofits of Hall Reduction Cells Using a TiB_2 Coating^(a)

	U.S. Total Projected Primary Capacity (10^6 TPY)	U.S. Aluminum Production (10^6 T)	Production with TiB_2 Retrofit Measure (10^6 T)
1985	5.29	4.23	-0-
1990	4.27	3.42	-0-
1995	3.45	2.76	0.57
2000	2.75	2.20	1.11

(a) Assumptions stated in text.

TABLE 14.4. Primary Aluminum Industry in the United States: Projected Capacity, TiB₂ Retrofits, and Energy Savings by Year, 1985-2000

Year	Remaining Production Capacity (10 ⁶ Tons) ^(a)	Capacity Retired (10 ⁶ Tons) ^(a)	Energy Use Reductions Due to Capacity Retirement ^(b) (BkWh)	Market Share of TiB ₂ Coating ^(c)	Energy Savings Due to TiB ₂ Coating (BkWh) ^(d)	Total Reduc- tions in Annual Elec- tricity Use (BkWh) ^(e)
1985	5.29	0.22	5.45	-0-	-0-	5.45
1986	5.07	0.21	8.01	-0-	-0-	8.01
1987	4.86	0.20	10.46	-0-	-0-	10.46
1988	4.66	0.20	12.80	-0-	-0-	12.80
1989	4.46	0.19	15.19	-0-	-0-	15.19
1990	4.27	0.18	17.19	-0-	-0-	17.19
1991	4.09	0.17	19.25	0.03	0.03	19.28
1992	3.92	0.17	21.24	0.07	0.06	21.30
1993	3.76	0.16	23.13	0.12	0.11	23.24
1994	3.60	0.15	24.95	0.18	0.16	25.11
1995	3.45	0.15	26.69	0.26	0.21	26.90
1996	3.30	0.14	28.32	0.34	0.27	28.59
1997	3.16	0.13	29.95	0.41	0.31	30.26
1998	3.03	0.13	31.48	0.44	0.32	31.80
1999	2.90	0.12	32.94	0.47	0.33	33.26
2000	2.78	0.12	34.35	0.50	0.33	34.68

(a) Capacity in 1983 of 5,526,000 tons per year is assumed to decline at a constant rate of approximately 4.2 percent per year. This rate of decline implies that all U.S. capacity with less than 50 percent capacity utilization in 1983 is eliminated by the year 2000.

(b) Calculated by: (Capacity Retirement) x (15,000 kWh/ton).

(c) See Chapter 4.0.

(d) Energy savings are assumed to be 2 percent (300 kWh/ton).

(e) Calculated by: (Energy Reductions due to Capacity Retirement) + (Energy Savings Due to TiB₂ Coating).

of a recent Brookhaven study (Pierce et al. 1984) assume that growth in demand for fabricated aluminum products drives growth in United States primary production. The rate of demand growth assumed in the Brookhaven model appears to be reasonable, but the assumptions in that and the present study differ markedly with respect to the amount of U.S. primary capacity that will be employed to meet demand growth.

14.5 ENERGY SAVINGS RESULTS

The impacts on electricity use due to the special cathode coating retrofit measure are estimated in this section. Reductions in electricity use due to projected retirements of capacity, without replacement, are also summarized since these are very significant in the scenario that is analyzed.

Energy savings in primary aluminum production that are attributable to plant retirements and the TiB_2 cathode coating are shown in Table 14.4 and summarized in Table 14.5. It is assumed that the TiB_2 cathode coating is not installed commercially until 1991, but then penetrates 50 percent of remaining capacity by 2000 (refer to Section 14.4). The delay in the measure's adoption is assumed to occur because a tested coating is not yet generally available.

TABLE 14.5. Estimates and Projections of Annual Energy Savings in Primary Aluminum Due to Declining Production and Adoption of a Special Cathode Coating^(a)

	Energy Use Reductions Due to Capacity Retirement (BkWh)	Energy Savings Due to TiB_2 Coating (BkWh)	Remaining Electricity Use (BkWh)
1995	5.45	-0-	63.6
1990	17.19	-0-	51.3
1995	26.69	0.21	41.3
2000	34.35	0.33	33.4

(a) Assumes 80 percent capacity utilization and 7.5 kWh/lb.

The energy savings estimates in Table 14.4 show a scenario in which electricity use for primary aluminum smelting falls at approximately the same rate as production for selected years. Electricity use reductions due to decreasing production are much larger (100 times as large) than electricity use reductions from the retrofit measure analyzed.

14.6 SENSITIVITY OF ENERGY SAVINGS RESULTS TO MARKET PENETRATION ASSUMPTIONS

Estimated energy savings from retrofitting aluminum smelters with special titanium diboride (TiB_2) cathode coatings are small in the base case (Table 14.4). Would these energy savings results be larger if the special coatings were assumed to be introduced earlier and have more rapid market penetration? Alternatively, how much smaller would the results be if market penetration were assumed to occur more slowly? The sensitivity of the energy savings results to variations in the market penetration assumptions is tested in this section.

14.6.1 Low Market Penetration Scenario

The possibility that market penetration of titanium diboride cathode coatings on existing aluminum smelters will occur less quickly than was assumed in the base case is explored in this section. Maximum market penetration is reduced to 25 percent (from 50 percent in the base case) of remaining capacity by the year 2000. The assumption that the coating is not generally available commercially until 1991 is retained.

Table 14.6 presents the low market penetration scenario estimates of market shares and energy savings for the titanium diboride coating retrofit measure. Table 14.7 summarizes these projection. It is apparent that the savings are an insignificant fraction of total electricity demand for aluminum production.

14.6.2 High Market Penetration Scenario

This section explores the possibility that market penetration of titanium diboride cathode coatings may be higher than assumed in the base case

TABLE 14.6. Low Market Penetration Scenario Estimates of Annual Market Share and Energy Savings for TiB_2 Cathode Coating Retrofit Measure

Year	Remaining Production Capacity (10^6 Tons) (a)	Capacity Retired (10^6 Tons) (a)	Electricity Use Reductions Due to Capacity Retirement (BkWh) (b)	Market Share of TiB_2 Coating (c)	Electricity Savings Due to TiB_2 Coating (BkWh) (d)	Total Reduc- tions in Annual Elec- tricity Use (BkWh) (e)
1985	5.29	0.22	5.45	-0-	-0-	5.45
1986	5.07	0.21	8.01	-0-	-0-	8.01
1987	4.86	0.20	10.40	-0-	-0-	10.46
1988	4.66	0.20	12.80	-0-	-0-	12.80
1989	4.46	0.19	15.19	-0-	-0-	15.19
1990	4.27	0.18	17.19	-0-	-0-	17.19
1991	4.09	0.17	19.25	0.02	0.02	19.25
1992	3.92	0.17	21.24	0.04	0.04	21.28
1993	3.76	0.16	23.13	0.06	0.05	23.18
1994	3.60	0.15	24.95	0.08	0.06	25.01
1995	3.45	0.15	26.69	0.10	0.08	26.77
1996	3.30	0.14	28.32	0.12	0.10	29.42
1997	3.16	0.13	29.95	0.16	0.15	30.10
1998	3.03	0.13	31.48	0.20	0.15	31.63
1999	2.90	0.12	32.94	0.23	0.16	33.10
2000	2.78	0.12	34.35	0.25	0.17	39.52

(a) Capacity in 1983 of 5,526,000 tons per year is assumed to decline at a constant rate of approximately 4.2 percent per year. This rate of decline implies that all U.S. capacity with less than 50 percent capacity utilization in 1983 is eliminated by the year 2000.

(b) Calculated by: (Capacity Retirement) $\times$ (15,000 kWh/ton).

(c) See Chapter 4.0.

(d) Energy savings are assumed to be 2 percent (300 kWh/ton).

(e) Calculated by: (Energy Reductions due to Capacity Retirement) + (Energy Savings Due to TiB_2 Coating).

TABLE 14.7. Estimated National Annual Electricity Savings in Primary Aluminum Production Due to Capacity Retirement and TiB_2 Retrofit--Low Market Penetration Scenario

<u>Year</u>	<u>Energy Use Reductions Due to Capacity Retirement (BkWh)</u>	<u>Electricity Savings Due to TiB_2 Coating (BkWh)</u>
1985	5.45	0
1990	17.19	0
1995	26.69	0.08
2000	34.35	0.17

(Table 14.4). The measure is assumed to become generally commercially available in 1988, three years sooner than in the base case. Maximum market penetration is increased to include practically all (95 percent) of remaining U.S. aluminum smelting capacity.

Table 14.8 presents the year-by-year estimates of annual market share and electricity savings for titanium diboride cathode coatings in the primary aluminum production industry for the high market penetration scenario. These projections are summarized in Table 14.9. Even with 95 percent market penetration and commercial adoption beginning in 1988, the expected electricity savings are relatively small.

14.7 ESTIMATED COST PER kWh FOR ENERGY CONSERVED WITH SPECIAL TITANIUM DIBORIDE CATHODE COATING IN PRIMARY ALUMINUM PRODUCTION

This section provides an estimate of the cost per kWh for energy conserved by the use of a titanium diboride coating for cathodes in existing U.S. aluminum smelters. The cost of conserved energy may be compared with the cost of new generating capacity to determine which source of energy is cheaper.

Table 14.10 shows the calculation of cost per kWh energy conserved by the primary aluminum production retrofit measure. The calculated cost is 2.3 cents per kWh, and is cheaper than the costs of new generating capacity cited in Chapter 4.0.

TABLE 14.8. High Market Penetration Scenario Estimates of Annual Market Share and Energy Savings for TiB_2 Cathode Coating Retrofit Measure

Year	Remaining Production Capacity (10^6 Tons) (a)	Capacity Retired (10^6 Tons) (a)	Electricity Use Reductions Due to Capacity Retirement (BkWh) (b)	Market Share of TiB_2 Coating (c)	Electricity Savings Due to TiB_2 Coating (BkWh) (d)	Total Reduc- tions in Annual Elec- tricity Use (BkWh) (e)
1985	5.29	0.22	5.45	-0-	-0-	5.45
1986	5.07	0.21	8.01	-0-	-0-	8.01
1987	4.86	0.20	10.46	-0-	-0-	10.46
1988	4.66	0.20	12.80	0.02	0.02	12.82
1989	4.46	0.19	15.19	0.05	0.05	15.24
1990	4.27	0.18	17.19	0.09	0.09	17.28
1991	4.09	0.17	19.25	0.15	0.15	19.40
1992	3.92	0.17	21.24	0.22	0.21	21.45
1993	3.76	0.16	23.13	0.30	0.27	23.40
1994	3.60	0.15	24.95	0.39	0.34	25.29
1995	3.45	0.15	26.69	0.49	0.40	27.09
1996	3.30	0.14	28.32	0.60	0.47	28.79
1997	3.16	0.13	29.95	0.70	0.53	30.48
1998	3.03	0.13	31.48	0.80	0.58	32.06
1999	2.90	0.12	32.94	0.89	0.62	33.06
2000	2.78	0.12	34.35	0.95	0.64	34.99

(a) Capacity in 1983 of 5,526,000 tons per year is assumed to decline at a constant rate of approximately 4.2 percent per year. This rate of decline implies that all U.S. capacity with less than 50 percent capacity utilization in 1983 is eliminated by the year 2000.

(b) Calculated by: (Capacity Retirement) $\times$ (15,000 kWh/ton).

(c) See Chapter 4.0.

(d) Energy savings are assumed to be 2 percent (300 kWh/ton).

(e) Calculated by: (Energy Reductions due to Capacity Retirement) + (Energy Savings Due to TiB_2 Coating).

TABLE 14.9. Estimated National Annual Electricity Savings in Primary Aluminum Production Due to Capacity Retirement and TiB₂ Retrofit--High Market Penetration Scenario

Year	Energy Use Reductions Due to Capacity Retirement (BkWh)	Electricity Savings Due to TiB ₂ Coating (BkWh)
1985	5.45	0
1990	17.19	0.09
1995	26.69	0.40
2000	34.35	0.64

TABLE 14.10. Cost per kWh Calculations for Titanium Diboride Cathode Coatings, as a Retrofit Measure for Existing U.S. Aluminum Smelters

Incremental Capital Cost ^(a)	\$22.95 per ton
Levelized Capital Cost ^(b)	\$6.93 per ton per year
Annual Electricity Savings ^(c)	300 kWh per ton
Cost per kWh ^(d)	2.3¢ per kWh

- (a) Estimated by; 0.9 percent of fixed capital investment (Skovronek et al. 1976)
x \$2250 capital investment per annual ton capacity (Castera 1984)
= \$22.95 per ton capacity.
- (b) The level stream of annual payments the present value of which would equal the investment's incremental capital cost. Assumes a 4-year useful lifetime of the investment and an 8 percent rate of interest compounded annually.
- (c) Calculated by:
2 percent energy savings (Whitaker 1984)
x 7.5 kWh per pound (U.S. industry average; Aluminum Association 1983)
x 2000 pounds per ton
= 300 kWh per ton.
- (d) Calculated by: \$6.93 per ton per year ÷ 300 kWh per year = 2.3¢ per kWh.

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