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National Uranium Resource Evaluation

AERIAL GAMMA RAY AND MAGNETIC SURVEY
VINCENNES QUADRANGLE
INDIANA, ILLINOIS, AND KENTUCKY

FINAL REPORT

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 **EG&G GEOMETRICS**
Sunnyvale, California 94086

March 1981



GEOLOGICAL SURVEY OF WYOMING
GEOLOGY

SED
PREPARED FOR U.S. DEPARTMENT OF ENERGY
Assistant Secretary for Resource Applications
Grand Junction Office, Colorado

metadc1202356

This report is a result of work performed by EG&G geoMetrics through a Bendix Field Engineering Corporation Subcontract, as part of the National Uranium Resource Evaluation. NURE is a program of the U.S. Department of Energy's Grand Junction, Colorado, Office to acquire and compile geologic and other information with which to assess the magnitude and distribution of uranium resources and to determine areas favorable for the occurrence of uranium in the United States.

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Prepared by
EG&G geoMetrics
Sunnyvale, California

MARCH 1981

Prepared for the U.S. Department of Energy
Assistant Secretary for Resource Applications
Grand Junction Office, Colorado
Under Contract No. DE-AC13-76GJ01664
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ABSTRACT

The Vincennes quadrangle covers 7,000 square miles of Indiana, Illinois, and Kentucky within the southeastern Midwestern Physiographic Province. The region contains a moderate to thick section of Paleozoic sediments, which are covered by surficial Quaternary glacial deposits in the western half of the area.

A search of available literature revealed no known uranium deposits.

A total of eighty-eight (88) uranium anomalies were detected and are discussed briefly in this report. The average concentrations of potassium, uranium, and thorium are moderate at best. All anomalies appear culturally induced, and none appear to represent significant concentrations of uranium.

The magnetic data appears to principally reflect the depth and complexities of the Precambrian basement.

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INTRODUCTION

General

The Vincennes quadrangle covers 7,000 square miles in southwestern Indiana, southeastern Illinois, and northern Kentucky (see Figure 1).

Several geologic references were used in the interpretation. The base map was compiled by ESKA-TECH Incorporated in 1980, using the 1:250,000 scale Indiana State Geologic map of the region as their primary reference (also used in the interpretation). Outlined units on the two maps do not register together properly, which casts some doubt on the accuracy of the digitized units used in the interpretation. Map unit descriptions, found in Appendix C, were taken from both these maps as appropriate. Some glacial geologic information was taken from Flint (1959 and 1971). Physiographic descriptions were taken in part from Fairbridge (1972). Structural information came largely from Cohee (1972) and the Indiana State Geologic Map series (Gray and others, 1970). Cultural and physiographic information were taken from the 1:250,000 scale Vincennes topographic sheet (1969 version).

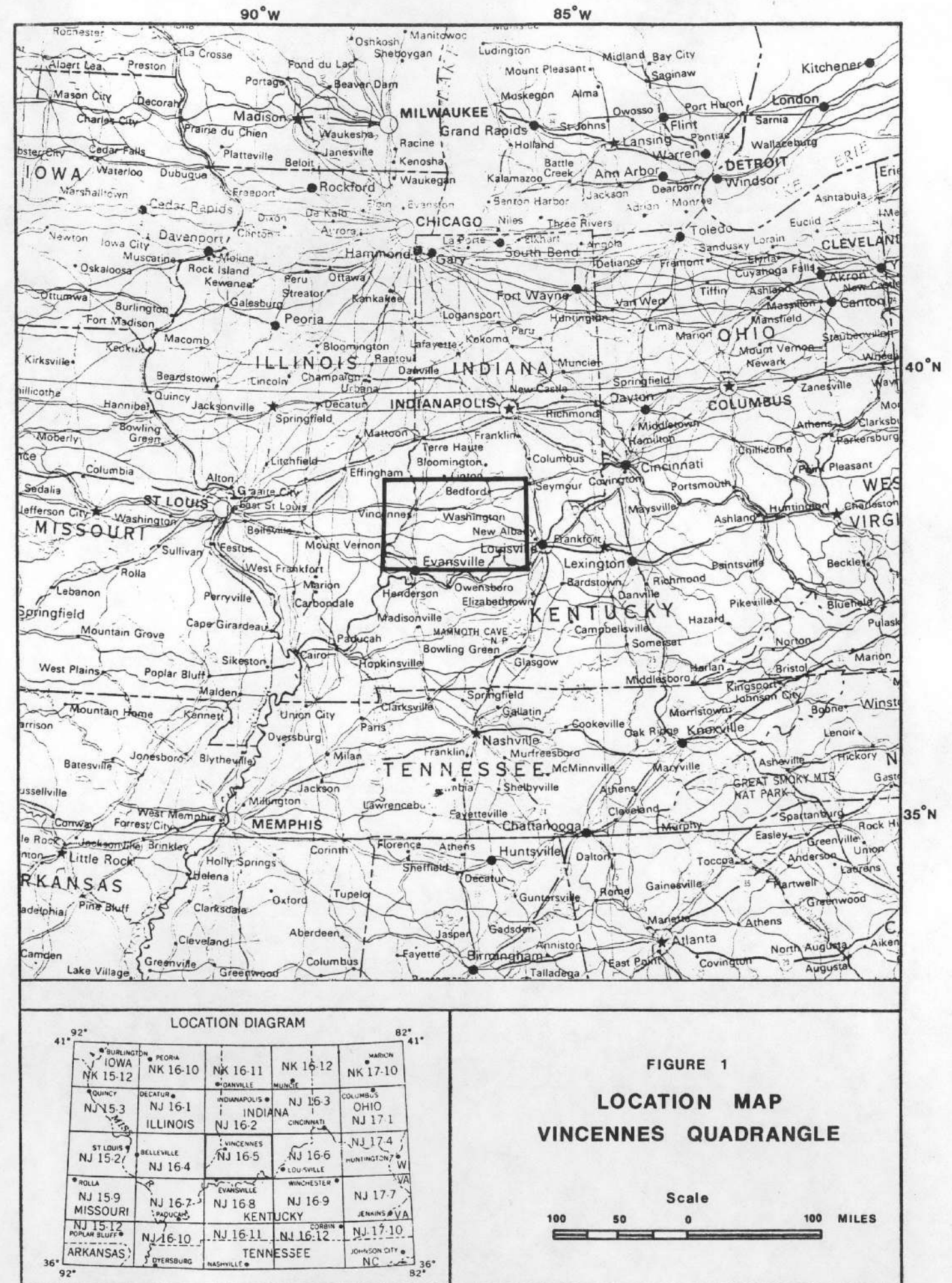
Data for the Vincennes quadrangle was acquired in November and December of 1980, and processed in January of 1981. A detailed summary of the data acquisition, processing, interpretation, and presentation methods appears in Appendix A. Appendix B contains a detailed flight summary for the Vincennes quadrangle.

Physiography

The Vincennes quadrangle comprises an irregular to mountainous region intermediate between the Midwestern and the Gulf Coastal Physiographic Provinces. The western half of the quadrangle is dominated by agricultural activity, as are portions of the more mountainous eastern half.

The region is drained by the Ohio River and several of its main tributaries. The Ohio River itself meanders through the extreme southeastern region. The White River watershed covers the largest percentage of the total quadrangle, including the entire northeastern quadrant. This river flows southwesterly into the Wabash, which flows SSW along the western border. The Wabash River drains the western border region directly. South and east of these two watersheds, small tributaries flow southward directly into the Ohio. All major river systems appear to be antecedent to present topography, with entrenched meanders throughout most of their length.

Elevations range from approximately 350 feet at the lowest base level of the Wabash River (at the extreme southwestern corner), to over 800 feet atop several mountains throughout the eastern half of the quadrangle. The quadrangle contains moderate amounts of cultural influence. The largest city in the area is Evansville (pop. 132,000) at the



western south edge of the quadrangle. The quadrangle contains a moderate to dense rectangular grid of roads and highways, and several railroad lines. Strip mining occurs throughout the region but is concentrated north of Evansville. Numerous oil fields are present in the west.

GEOLOGY

Structure

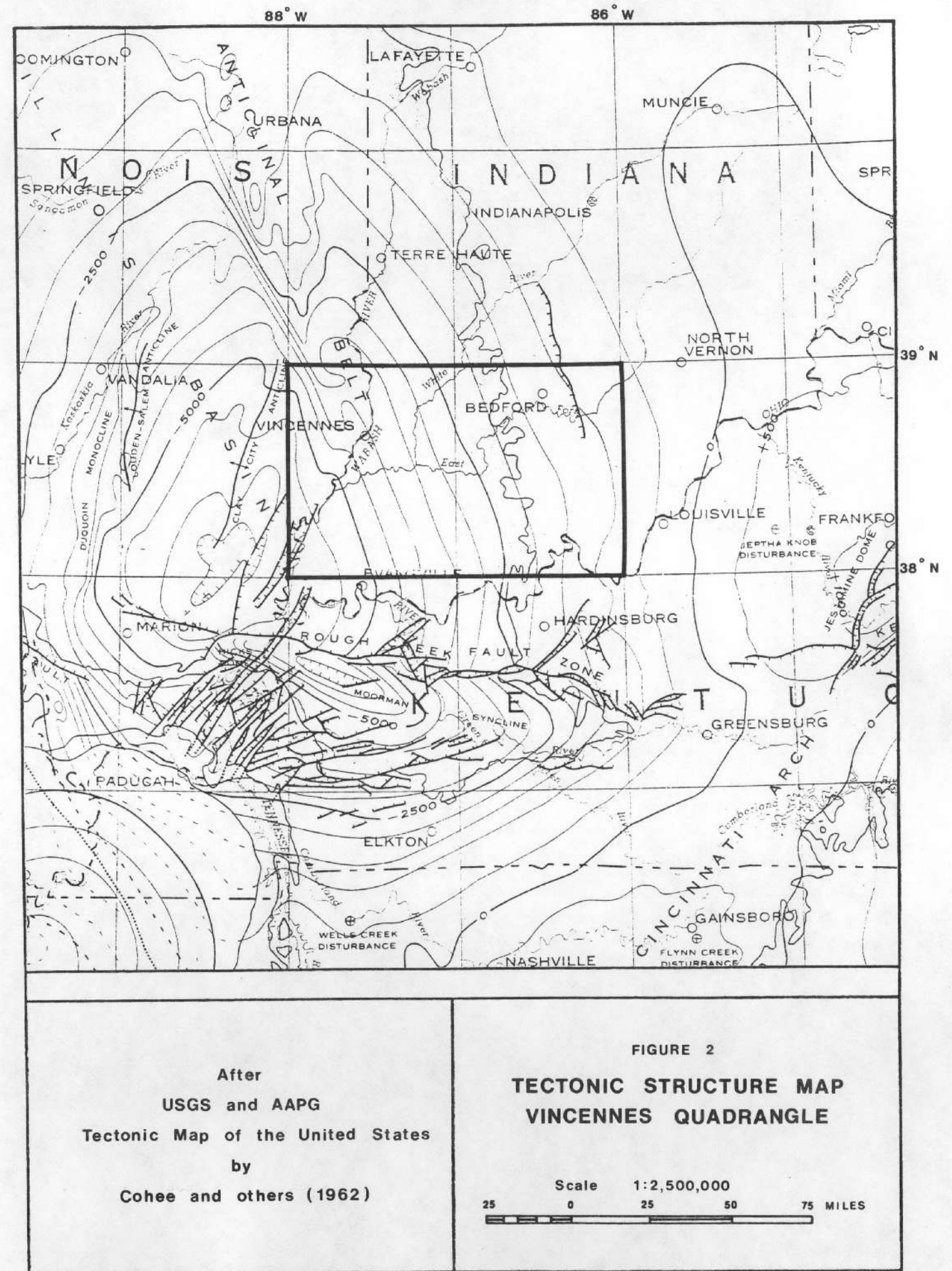
The region defined by the Vincennes quadrangle lies on the eastern edge of the Illinois Sedimentary Basin. Sediments of Paleozoic age shoal from 12,000 feet at the southwestern corner, to less than 4,500 feet in the extreme northeast (on the southwestern limb of the Kankakee Arch). The Illinois Basin is a roughly circular structure that is complicated by several secondary structural features. The LaSalle Anticlinal belt strikes SSE through the central portion of the basin (in the western half of the Vincennes quadrangle). Several dip slip faults have been mapped in this area by Cohee and others (1962), some of which appear associated with the anticlinal belt. Though these faults are largely subsurface, they have been mapped in detail by Gray and others (1970), and also appear on the ESKA-TECH map.

Surface Geology

Though Paleozoic sediments dominate the subsurface structure, they are, to a large extent, masked by overlying glacial, periglacial, and post-glacial sediments of Illinoian through Post-Wisconsinan (Quaternary). The quadrangle is essentially divided in half by a north-south trending line, with exposed Paleozoics in the east, and extensive Quaternary cover in the west. Some exposures of Paleozoics exist west of this line, primarily in the south. The eastern half has some localized regions containing thick Quaternary sections, particularly the extreme northeastern corner. In all, mapped Quaternary units cover 55 percent of the surface.

The Quaternary section is composed of a combination of glacially related deposits of Pleistocene age, and Recent deposits along the flood plains of the major rivers (alluvial, colluvial, fluvial, paludal, and related sedimentary processes). Of the mapped Quaternary section, Recent deposits cover 25 percent.

Till of Illinoian age is mapped in the northeastern corner and throughout the northwestern quadrant away from the flood plain areas. These sediments account for approximately 20 percent of the Pleistocene section. Large areas of drainage systems that were blocked by the glaciers contain lacustrine sediments. These sediments are quite extensive, covering 25 percent of the represented Pleistocene. The most extensive glacially-related deposits are eolian sands and silts (loess) of interglacial and post-glacial age. These amount for 45



percent of the Pleistocene surface deposits and are exposed throughout the western half of the quadrangle. The remaining 10 percent of the Pleistocene is covered with a combination of glacial outwash and miscellaneous alluvial, colluvial, and paludal deposits of glacial or interglacial age that largely occur adjacent to major rivers.

The Paleozoic section is completely dominated by Pennsylvanian age (in the western exposures) and Mississippian age (to the east) sediments. Mississippian limestones, shales and sandstones cover 60 percent of the Paleozoic surface. The remainder of the exposures compose thick sandstone and shales of Pennsylvanian age primarily of the Pottsville and Alleghanian epochs, that contain some limestones and numerous coal beds. The Pennsylvanian - Mississippian boundary is marked by a significant unconformity that represents a major erosional period between the Kaskaskia and the Absaroka transgressive phases.

Uranium

According to available resources, there are no known uranium deposits in the Vincennes quadrangle.

INTERPRETATION OF GEOPHYSICAL DATA

Radiometric Data

A total of 88 groups of uranium (Bi214) samples meet the minimum statistical requirements for anomaly definitions as set forth in the data interpretation section of Appendix A. These are displayed, along with all other anomalous samples and pertinent data, on Figure 3. The anomalies are summarized in a table in Appendix G. The potassium, uranium, thorium, and ratio pseudo-contour maps, which reflect radiometric responses for the entire quadrangle, are found in Appendix H. Discussion of the abundances of potassium, uranium, and thorium are in terms of apparent equivalent percent and apparent equivalent ppm. These equivalent units are derived from scaling of counts per second data by the sensitivities calculated for the detection system and as such cannot be taken as directly determined geochemical values.

The Vincennes quadrangle contains moderately low concentrations of potassium, uranium, and thorium. All three elements appear to be distributed somewhat uniformly throughout the quadrangle. Potassium has a quadrangle mean of 1.0 percent. Uranium averages 2.0 ppmeU, and thorium has a mean of 5.9 ppmeT.

Uranium concentrations vary considerably over short distances, but through a narrow range centered around the quadrangle mean. The highest peak uranium concentration is 6.8 ppmeU in map unit QC (Holocene colluvium), whereas map unit QM (modified land; coal and strip mines, quarries) contains the highest average uranium concentration at 2.6 ppmeU. In general, the northern third of the quadrangle shows slightly

lower concentrations, this is mainly attributed to the Wabash and White River floodplains, along with the slightly lower concentration values in the Illinoian glacial till.

Potassium exhibits relatively narrow concentration ranges, and tends to vary only over long distances. In general, concentrations appear to define two populations (see Appendix H). The eastern half contains values that range around 0.875 percent, while the western half averages about 1.25 percent. The lower concentrations may represent the pre-Quaternary bedrock exposures. The highest peak and average potassium concentrations both occur in map unit Q1 (Quaternary loess) at 2.0 and 1.15 percent, respectively.

Thorium also exhibits relatively narrow concentration ranges, with significant variations occurring only over long distances. Only the floodplains of the Wabash and White Rivers in the northwest, and the White River (East Fork) floodplain in the northeast corner (see Appendix H) exhibit significantly lower thorium concentrations. The peak thorium concentration occurs in map unit QL, at 10.74 ppmeT, while the highest average concentration of 6.9 ppmeT occurs in map unit PMC (Pennsylvanian McLeansboro Group).

Generally speaking, the concentrations of the three radioactive elements within those areas of mapped exposed bedrock are very similar to those in the overlying Quaternary materials. This suggests that glacial material may in part be of local origin.

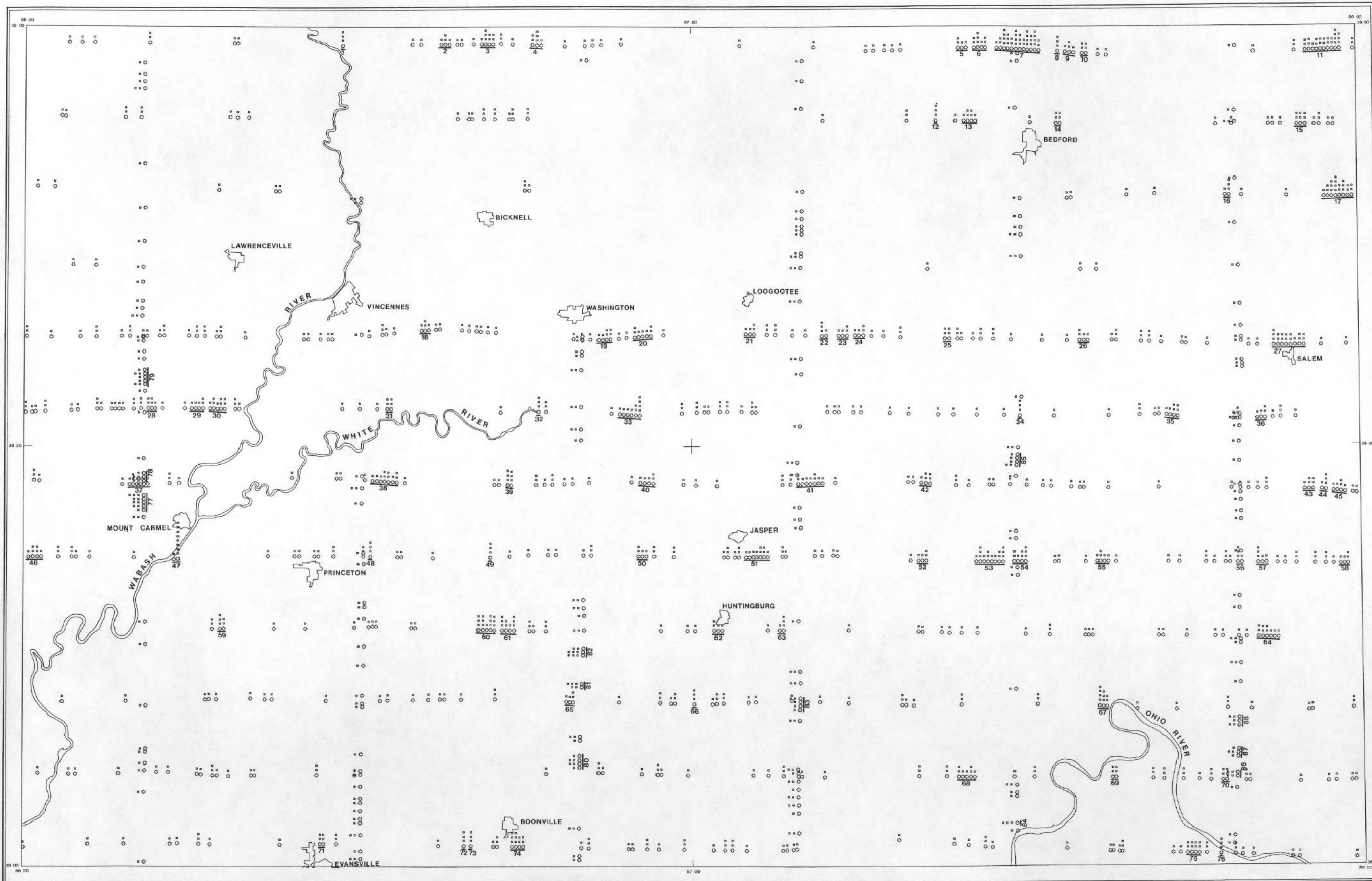
Anomalies occur mainly in the southeast quadrant, and an area just east of the Wabash River. All these anomalies appear to have cultural origins (such as roads, railroads, quarries, oil fields, etc.). These anomalies range in peak concentrations from 2.5 to 6.1 ppmeU. Anomaly 47 has the highest peak uranium concentration, and occurs within a partially flooded oxbow over cultural activity of an unknown sort. Otherwise, the cultural associations, coupled with the low concentration levels, indicates that none of the anomalies have any significance.

Magnetic Data

The pseudo-contour map of the magnetic data appears in the Appendix H.

The quadrangle is mainly dominated by moderate to long wavelengths of very low amplitude, with the exception of the eastern border area which shows strikingly higher gradients that define isolated structures. The resulting picture suggests a large complex structural pattern at depth. Though gradients slightly decrease away from the axis of the LaSalle Anticline, the resulting picture appears to depict complexities in lithology and/or structure in the underlying Precambrian basement rather than in the Paleozoic sediments.

VINCENNES



URANIUM ANOMALY/
INTERPRETATION MAP

VINCENNES QUADRANGLE
U.S. DEPARTMENT OF ENERGY

APPROXIMATE SCALE 1:500,000

EXPLANATION

- - CITY OR TOWN
- - URANIUM SAMPLE MEETING FOLLOWING CRITERIA:
 - (1) $1.0 \leq U \leq \infty$
 - (2) $-1.0 \leq T \leq \infty$
 - (3) $1.0 \leq U/T \leq \infty$
- IN STANDARD DEVIATION UNITS.
EACH SQUARE REPRESENTS 1 STANDARD DEVIATION.
- ⊞ - URANIUM ANOMALY:
A SINGLE SAMPLE OF 3 OR MORE STANDARD DEVIATIONS OR GROUP OF ADJOINING SAMPLES WHICH TOGETHER TOTAL 4 OR MORE STANDARD DEVIATIONS, $4.0 \leq \sum U \leq \infty$, WITH AT LEAST ONE SAMPLE OF 2 OR MORE STANDARD DEVIATIONS.



SURVEY AND
COMPILED BY:

EG&G GEOMETRICS

Figure 3 - Uranium Anomaly/Interpretation Map - Vincennes Quadrangle

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**APPENDIX A - Data Acquisition, Processing, and
Interpretation Methods**

INTRODUCTION

General

Under the U.S. Department of Energy's (DoE), National Uranium Resource Evaluation (NURE) Program, geoMetrics, Inc., conducted a high sensitivity airborne radiometric and magnetic survey. The data collection and processing were conducted under requirements set forth in Bendix Field Engineering Corporation specification 1200-C, dated February, 1979. The objectives of the (DoE)/NURE program, of which this project is a small part, may be summarized as follows:

"To develop and compile geologic and other information with which to assess the magnitude and distribution of uranium resources and to determine areas favorable for the occurrence of uranium in the United States." (DoE)

As an integral part of the DoE/NURE Program, the National Airborne Radiometric Program is designed to provide cost effective, semiquantitative reconnaissance radio element distribution information to aid in the assessment of regional distribution of uraniferous materials within the United States.

All Airborne data collected by geoMetrics during the course of this project were done so utilizing a Beechcraft B65 Queen Air Airplane (U.S. Registry No. N9AG) and a Rockwell Aero Commander (Registry No. N1213B). Both aircraft used 3584 cubic inches of NaI crystal and a high sensitivity proton magnetometer (0.25 gamma).

Each report contains a detailed geologic summary, interpretation report, reduced scale copies of all maps and profiles, histograms, and statistical tables for each quadrangle contained within the project. In addition, each report contains an appendix detailing the survey description, specifications, data collection and processing methods, and interpretation methods.

All data processing, statistical analyses, and interpretation were performed at the geoMetrics computer facility, Sunnyvale, California. After processing, the corrected data were statistically evaluated to define those areas which were radiometrically anomalous relative to other areas within each computer map unit. Standard deviation maps and radiometric and magnetic profile data were first evaluated individually and then integrated into a final interpretation map for each NTMS quadrangle.

Corrected profiles of all radiometric variables (total count, potassium, uranium, thorium, uranium/thorium, uranium/potassium, and thorium

/potassium, ratios), magnetic data, radar altimeter data, barometric altimeter data, air temperature, and airborne bismuth contributions are presented as profiles in this report. Single record and averaged data are presented on microfiche in report. These data are given at 1.0 second sample intervals, corrected for Compton Scatter, referenced to 400 foot mean terrain clearance as Standard Temperature and Pressure and corrected for atmospheric bismuth. Digital magnetic tapes are available containing raw spectral data, single record data, magnetic data, and statistical analysis results.

OPERATIONS

PRODUCTION SUMMARY

The production summary presented below describes the general procedures involved in gathering data for the entire project. The detailed daily production summary in Appendix B describes a portion of the total project.

Prior to the start of the survey operations, the airplanes were calibrated at the DoE test pads and Dynamic Test Range (the Queen Air in April 1980, and the Aero Commander in October 1980). Requirements for system calibrations are listed in the 1250-A specifications from BFEC.

Throughout the course of the overall project, the average ground speed maintained by the Queen Air was 140 mph. The Aero Commander averaged 150 mph.

Nearly 100% of the data collected were within the specification limits of 200-700 feet. Several deviations over short distances were required to meet military regulations, FAA safety requirements, and to ensure that livestock were not endangered due to low flying aircraft. A sample altitude statistical distribution is shown in Figure I.

DATA COLLECTION PROCEDURES

Operating Parameters/Sampling Procedures

This survey was conducted using data collection parameters summarized below:

1. Data sampling was performed by a time-base system using 1.0 second sample intervals. All sensor data with analog output were digitally sampled at each scan based upon the clock timing rate of 1.0 seconds. The data so collected are the instantaneous values of the altimeter, temperature, pressure, and magnetometer parameters determined at the time of the data scan, but represent a count time of 1.0 seconds for the gamma ray spectrometer data.
2. The airplanes' objective ground speeds, mentioned previously, were not exceeded unless dictated by safety.
3. The airplane's downward looking crystal volume was 3,072 cubic inches providing an objective V/V (crystal volume in cubic inches divided by ground speed in miles per hour) of 22.0 at 140 m.p.h.
4. The upward looking crystal volume was 512 cubic inches.

NUMBER OF OCCURRENCES

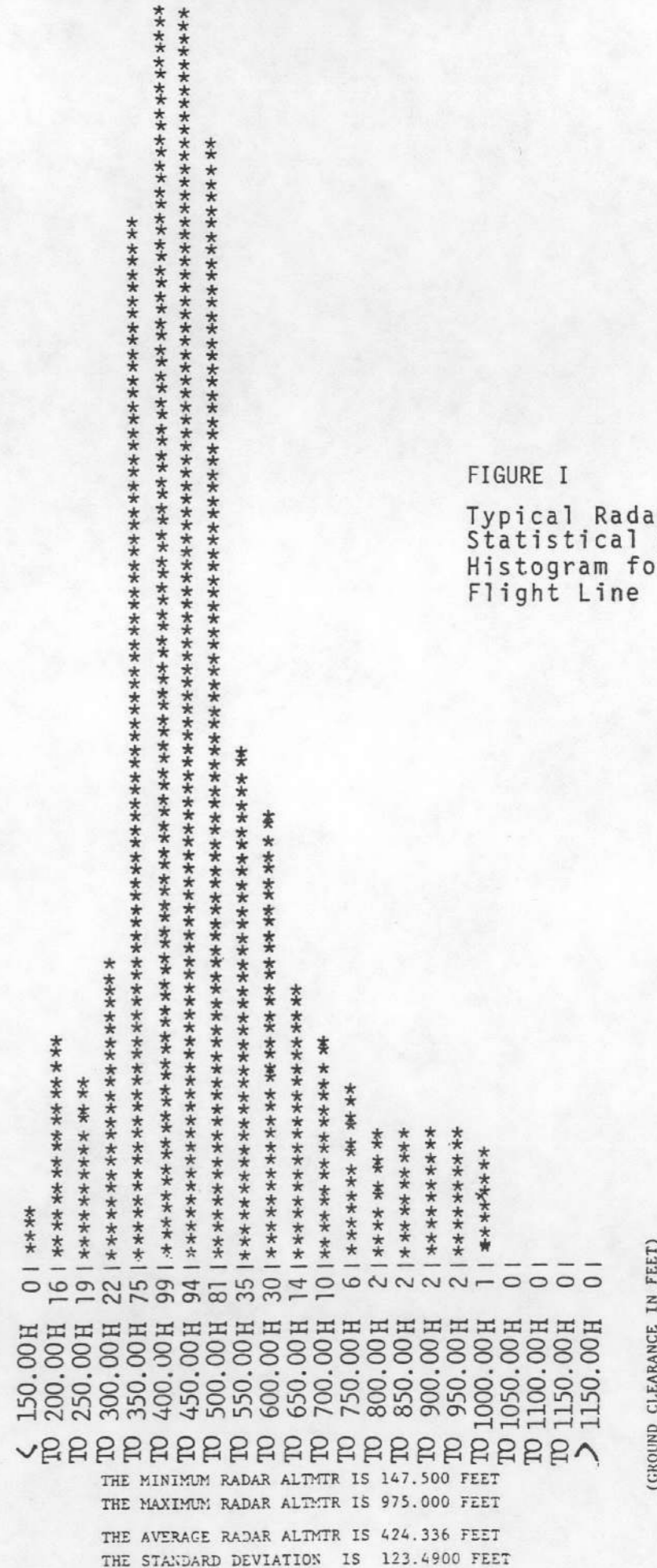


FIGURE I
Typical Radar Altimeter
Statistical Summary
Histogram for Single
Flight Line

Navigation/Flight Path Recovery

For all of the quadrangles, profiles were flown east-west at 6 mile (9.6 km) spacing. North-south tie lines were flown at 18 mile (28.8 km) spacing.

Navigation was accomplished using visual navigation techniques. Flight lines were drawn on 1:250,000 quadrangles and the pilot/navigator utilized these maps to provide visual navigation features.

Simultaneously, a 35 mm tracking camera was used to record actual flight position. This camera's fiducial numbering system was directly synchronized to the digital recording system such that a one-to-one correlation between position and data could be made. Upon completion of a data collection flight, the 35 mm film was processed and actual flight path positions located on the appropriate scale map sheets.

Infield System Calibration

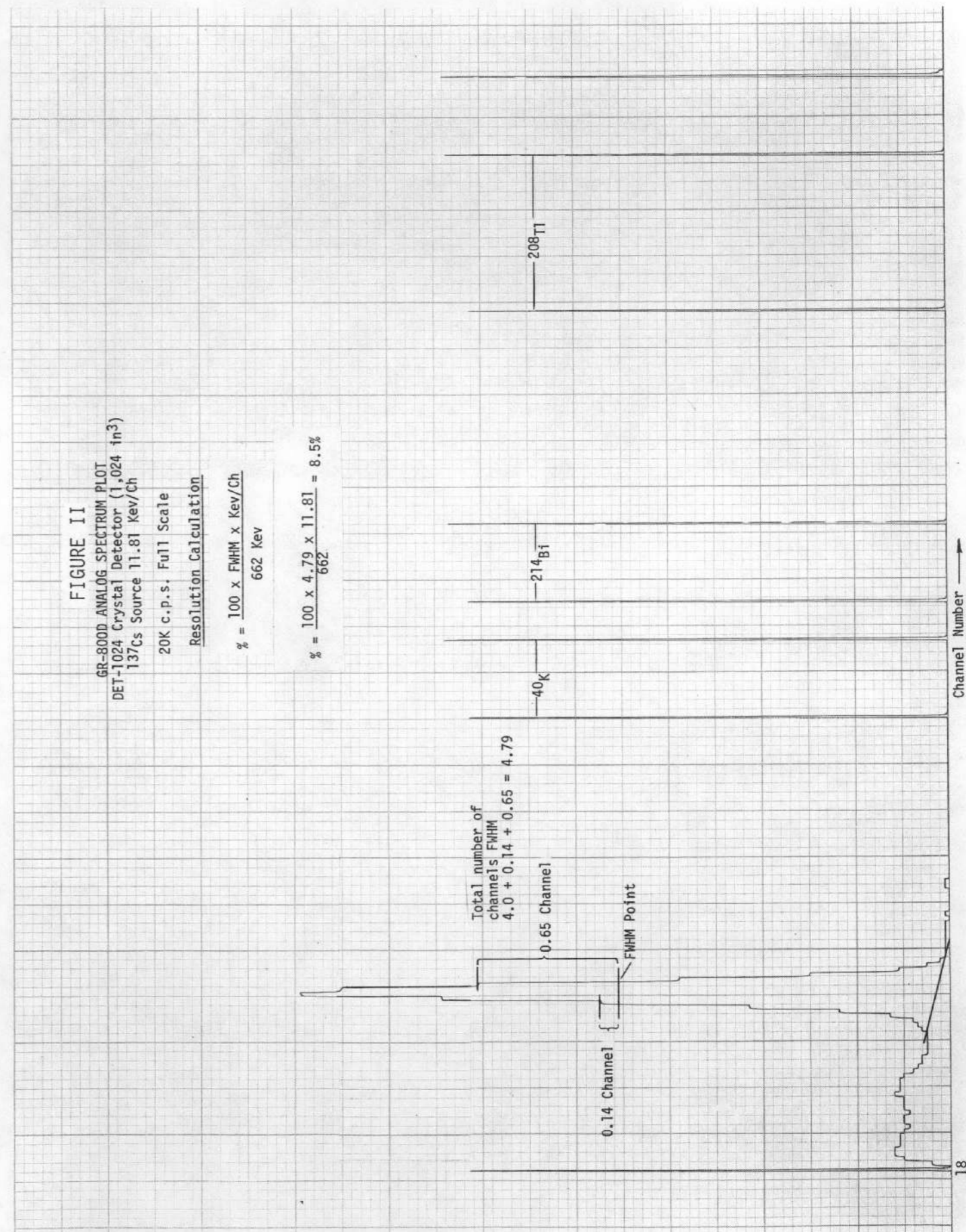
Due to the complex nature of both the system and the required data interpretation, much emphasis was placed on infield calibration of the data collection system. The objective of this calibration was to ensure continuous high quality of the data collected. The daily calibration procedures used are summarized below:

A. Pre Flight

1. Use cesium sources (same positioning on crystals every day), peak each Photomultiplier tube/crystal using the digital split-window detector of the GR-800. Then using thallium sources, repeat the tuning of the individual crystals.
2. Run full cesium spectrum on analog recorder for both down and up looking crystals. Calculate the cesium resolution (see sample in Figure II). Run spectrum out past the K40 peak on down crystals for evaluation of system tuning.
3. Finally run a full thorium analog spectrum of the down crystals and check for centering of K40 and Tl208 peaks in spectrum.
4. Repeat 1-3 until system is within contract specifications.

B. During Flight

1. Fly test line at survey altitude (400 ft), for approximately five miles, prior to production data collection (record both analog and digital).
2. Prior to production data collection, the above data are evaluated to ensure +20% limits on total count compared to average of all test flights from that base of operations.



DATA COLLECTION SYSTEM

3. During production data collection, monitor radon analog data for unusual increases. Visually correlate these with temperature and barometric pressure.
4. Upon completion of production data collection, re-fly test line at survey altitude (400 ft). Record both analog and digital.

C. Post Flight

1. Verify test line total count within 20% of average for all test lines at that base of operations.
2. Using cesium sources (same position as pre-flight), run full cesium spectrum for both down and up crystals (allow it to record through the K40 peak in the down crystals). Repeat the procedure using thallium sources and examine the T1208 window.
3. Calculate the resolution of down and up crystal pack.
4. Determine shift, if any, in T1208 peak position.

Field Digital Data Verification

At the completion of each flight, the raw digital data tapes were checked for data quality and completeness on geoMetrics' G-725. The G-725 system is a totally portable mini computer (and peripherals) consisting of; an Interdata 516, two 9 track tape drives, a CRT, a line printer, and two floppy discs. Any digital problems encountered were immediately evaluated by the electronics operator and data man, thus assuring optimum data quality. In addition, histogram information for each measured variable was generated. Thus a summary display of altitude, etc., is available for immediate evaluation.

AIRCRAFT

Two aircraft were used for this survey: (1) a Beechcraft Queen Air - Model 65 (U.S. Reg. No. N9AG), and (2) a Rockwell Aero Commander 680F (U.S. Reg. No. N1213B). Both these aircraft, being medium size with twin engines, possess overall performance and safety features which make them ideal for low level, fixed-wing airborne geophysical surveys in areas of up to moderately high topographic relief. They can carry adequate payloads at low constant airspeeds, while maintaining economy and a wide envelope of safety. Performance data for the two craft in their present survey configuration are given below.

	<u>QUEEN AIR</u>	<u>AERO COMMANDER</u>
Maximum Aircraft Gross Weight	7,700 lbs.	8,500 lbs.
Aircraft Empty (dry)	4,640 lbs.	5,200 lbs.
Max. useful load including fuel	3,060 lbs.	3,300 lbs.
Geophysical Package	1,110 lbs.	1,110 lbs.
Navigation Equipment	125 lbs.	125 lbs.
Fuel Tanks Full	528 lbs.	1,338 lbs.
Pilot & Electronics Operator	350 lbs.	350 lbs.
Total	2,113 lbs.	2,923 lbs.
Min. Control Speed at G.W. (IAS)	95 mph	NG
Safe Single Eng. Speed @ G.W. (IAS)	105 mph	NG
Rate of Climb 2 engines @ gross (FPM)	1,300	1,500
Rate of climb 1 engine @ gross (FPM)	210	250
Avgas consumption (ga/hr) at 75% power	36	38
Endurance (75% power)	6 hrs/6 mins.	5 hrs/30 mins.
Range (75% power - 45 min. reserve)	1,200 miles	1,100 miles
Cruise Configuration stalling speed at gross weight (IAS)		
0° bank	80 mph	80 mph
45° bank	95 mph	NG

Electronics

The major components of the airborne data collection system are summarized below (shown schematically in Figure III):

1. Gamma Ray Spectrometer, geoMetrics GR-800, utilizing a dual 256 channel capability to provide spectral data in the 0.4 to 3.0 MeV range for both the downward looking and the upward looking crystal packages and coverage in the 3.0 to 6.0 MeV range for cosmic background.
2. Crystal Detector, geoMetrics Model DET-3072/512R consisting of 3072 cubic inches in the downward looking configuration and 512 cubic inches appropriately shielded in an upward looking configuration.
3. A geoMetrics Digital Data Acquisition System, Model G-714 with "read-after-write" data verification, recording the following on magnetic tape:
 - a. 512 channels of gamma ray spectrometer data
 - b. Total magnetic intensity
 - c. Fiducial number from data system/camera
 - d. Manually inserted information, i.e. date, survey area, and flight line number
 - e. Altitude from radar altimeter and barometric altimeter (by analog-to-digital conversion)
 - f. Time in days, hours, minutes and seconds
 - g. Outside air temperature
4. Magnetometer, geoMetrics Airborne Model G-803, capable of 0.125 gamma sensitivity, but operated at 0.25 gamma sensitivity.
5. Radar Altimeter, Bonzer Model Mark 10 with recording output and display operating over an altitude range of 0 to 2,500 feet.
6. Rosemont Barometric Altimeter with recording output and display.
7. Recording Thermometer for monitoring outside air temperature.
8. Tracking Camera. Automax 35 mm framing camera with wide angle lens and 10 character fiducial/line number display to provide flight path recovery data.

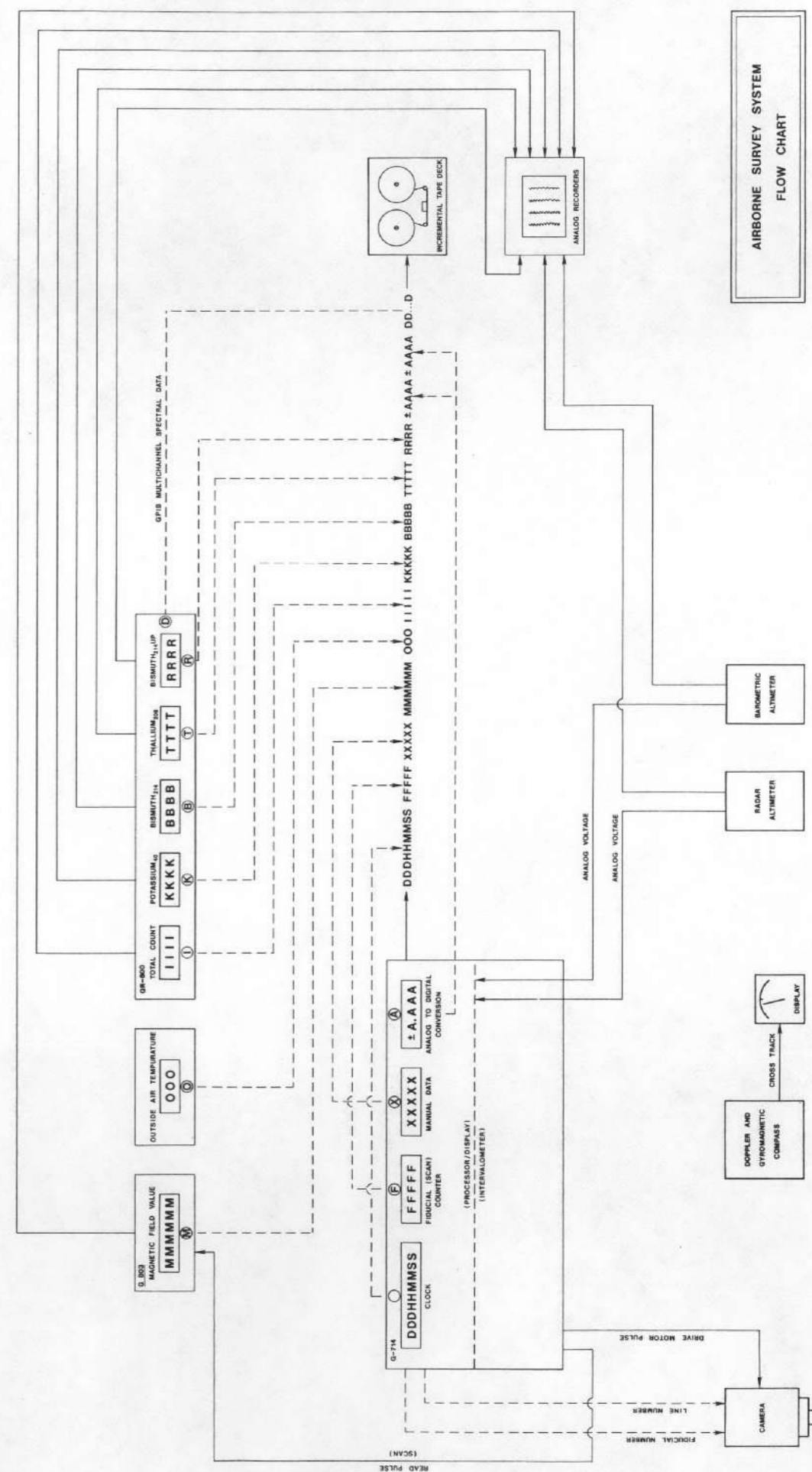


FIGURE III

SYSTEM CALIBRATION

9. Analog Recorder geoMetrics (MARS 6) to record the following data:
- Bi214 using a window about the 1.76 MeV peak from the downward looking system.
 - Bi air background from the upward looking system.
 - Magnetometer
 - Radar Altitude
 - Total count for downward looking system (0.4 to 3.0 MeV)
 - Barometric Altitude
 - Time markers
10. HP 7155 single channel analog recorder during pre and post flight calibrations, this recorder is used to plot a full analog spectra for both the down and up crystal systems via the GR-800. Thus, a hard copy record of the data used for resolution, drift, etc., checks are available at all times. This approach provides instant verification of system parameters (refer to Figure II).

AIRCRAFT AND COSMIC BACKGROUND

Full spectral data are collected at five (5) altitudes over water (14,000 feet, 12,000 feet; 10,000 feet; 8,000 feet and 6,000 feet) in an area where the existence of no airborne Bi214 can be assured (off shore over the Pacific Ocean). This results in separate spectra as shown schematically in Figure 10. We define $S(12,000)$ to be the spectra at 12,000 feet from 0.4 MeV to 3.0 MeV with $S(8,000)$ the same spectra at a lower altitude (8,000) and $C_i(h)$ the total count between 3.0 and 6.0 MeV at respective altitudes. Since the aircraft background is constant, the difference between any two altitudes separated sufficiently - typically, 2,000 feet - yields the cosmic spectral curve shape as shown schematically in Figure VI. Thus

$$S(12,000) - S(8,000) = \Delta S$$

and

$$\Sigma C_{12}(h_i) - \Sigma C_8(h_i) = \Delta C$$

This cosmic spectral curve is scaled back to 12,000 feet as follows:

$$\frac{C_{12}(h_i)}{\Delta C} \times \Delta S = \Delta C(12,000) \text{ the Cosmic Spectrum (shape and magnitude at 12,000 feet)}$$

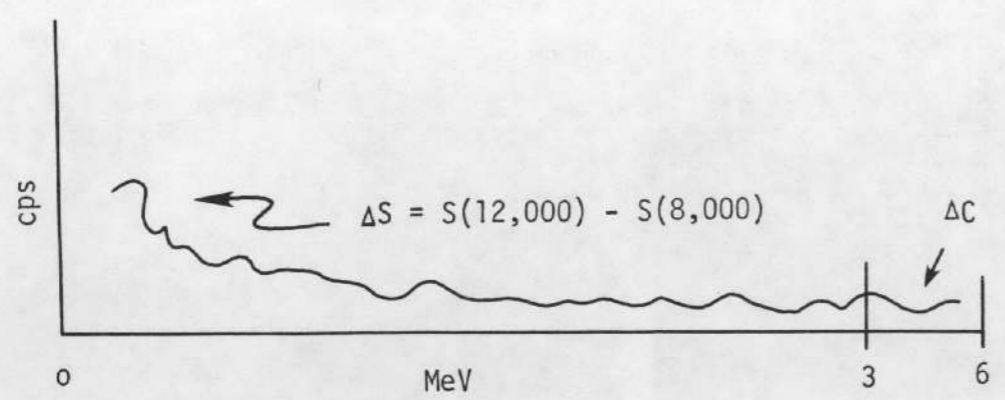
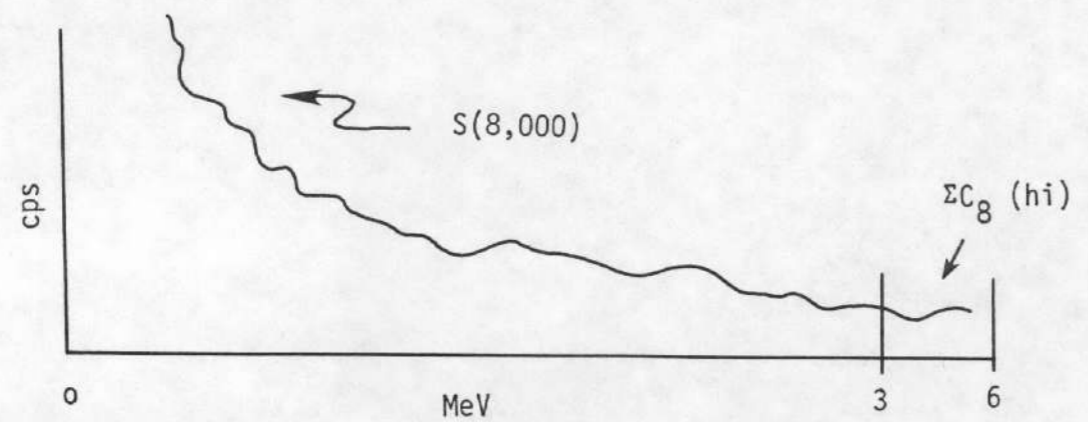
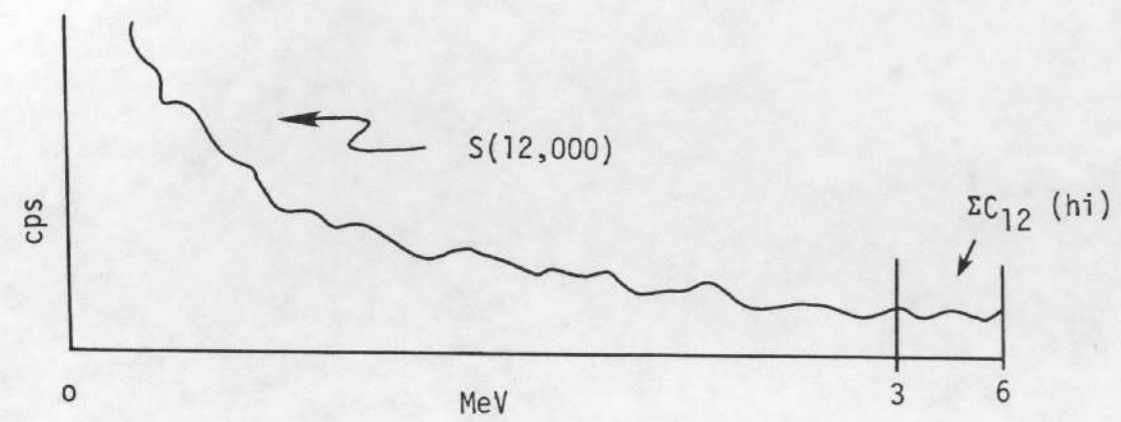
The aircraft background is derived as follows:

$$S(12,000) - C(12,000) = \text{A/C Background}$$

Since data were collected at five altitudes, this procedure was repeated for each combination of altitudes and results averaged. Typical aircraft and cosmic spectra are shown in Figures V, AND VI respectively.

SYSTEM CONSTANTS

System constants were determined by occupation of the DoE Walker Field Test Pads. (See Ward, 1978, and Stromswold, 1978, for complete descriptions of the building and monitoring of the pads). The five test pads contained varying concentrations of K, U, and T as presented by BFEC:



<u>PAD</u>	<u>K</u>	<u>U</u>	<u>I</u>
Matrix	1.45%	2.19 ppm	6.26 ppm
K	5.14%	5.09 ppm	8.48 ppm
U	2.03%	30.29 ppm	9.19 ppm
T	2.01%	5.14 ppm	45.33 ppm
Mixed	4.11%	20.39 ppm	17.52 ppm

Since the measurements were taken over a relatively short time period (a few hours), it was assumed that the matrix pad measurements contain not only the effects of the matrix pad itself, but also aircraft background (which is a constant), cosmic background (constant over the time period of interest), and all other local background (e.g. BiAir, etc.) effects. (The matrix pad is constructed with only the basic concrete mix without the additional elemental minerals). Thus, by subtracting the matrix pad count rates from the count rates in the four pads, we have eliminated aircraft and cosmic background and BiAir effects for the four pads. The pad concentrations are then modified in a similar fashion by the subtraction of the matrix pad concentrations. The differential concentrations in the pads are given in the table below.

<u>PAD</u>	<u>K</u>	<u>U</u>	<u>I</u>
K-Matrix	3.7%	2.9 ppm	2.2 ppm
U-Matrix	0.6%	28.5 ppm	2.9 ppm
T-Matrix	0.6%	3.0 ppm	39.0 ppm
Mixed-Matrix	2.7%	18.8 ppm	11.3 ppm

Considering the above, we can define a functional relationship between the differential concentrations and the residual count rates which will provide a method of determining the calibration constants for the spectrometer system. These calibration constants are the six (6) stripping coefficients which account for the interactions occurring between the elemental channels in the system (Compton scatter coefficients, etc.).

On the basis of an ideal situation, one would anticipate that some of these interactions should be negligible. This is not totally the case, since we are dealing with a system which has less than infinite resolving power (i.e. the energies are smeared to some extent).

FIGURE IV - Multiple altitude spectra schematic

Thus, energy peaks within a spectrum of a given element are Gaussian shaped rather than pure line spectra. Additionally, we are dealing with finite spectral windows, multiple peaked spectra, and pulse pileup; all tend to couple each window's response to the other.

Keeping in mind that we are dealing with the count rates corresponding to the concentrations presented in the last table, we define the following:

KC_i = uncorrected system count rate for the K channel

UC_i = uncorrected system count rate for the U channel

TC_i = uncorrected system count rate for the T channel

K_i = the percent differential concentration of potassium

U_i = ppm differential concentration of uranium

T_i = ppm differential concentration of thorium

where "i" refers to the ith pad.

We also define the following:

ζ_{kk} = sensitivity of KC_i to concentrations of K_i

ζ_{ku} = sensitivity of KC_i to concentrations of U_i

ζ_{kt} = sensitivity of KC_i to concentrations of T_i

ζ_{uk} = sensitivity of UC_i to concentrations of K_i

ζ_{uu} = sensitivity of UC_i to concentrations of U_i

ζ_{ut} = sensitivity of UC_i to concentrations of T_i

ζ_{tk} = sensitivity of TC_i to concentrations of K_i

ζ_{tu} = sensitivity of TC_i to concentrations of U_i

ζ_{tt} = sensitivity of TC_i to concentrations of T_i

Using the above definitions, we now construct the functional relationship by means of the following nine (9) equations in sets of three (3) per pad.

$$\text{K pad} \quad KC_k = \zeta_{kk}K + \zeta_{ku}U + \zeta_{kt}T$$

$$UC_k = \zeta_{uk}K + \zeta_{uu}U + \zeta_{ut}T$$

$$TC_k = \zeta_{tk}K + \zeta_{tu}U + \zeta_{tt}T$$

$$\text{U pad} \quad KC_u = \zeta_{kk}K + \zeta_{ku}U + \zeta_{kt}T$$

$$UC_u = \zeta_{uk}K + \zeta_{uu}U + \zeta_{ut}T$$

$$TC_u = \zeta_{tk}K + \zeta_{tu}U + \zeta_{tt}T$$

$$\text{T pad} \quad KC_t = \zeta_{kk}K + \zeta_{ku}U + \zeta_{kt}T$$

$$UC_t = \zeta_{uk}K + \zeta_{uu}U + \zeta_{ut}T$$

$$TC_t = \zeta_{tk}K + \zeta_{tu}U + \zeta_{tt}T$$

Separating these equation into consistent groups, we get for the uncorrected count rates in the K channel

$$(K \text{ pad}) \quad KC_k = \zeta_{kk}K_k + \zeta_{ku}U_k + \zeta_{kt}T_k$$

$$(U \text{ pad}) \quad KC_u = \zeta_{kk}K_u + \zeta_{ku}U_u + \zeta_{kt}T_u$$

$$(T \text{ pad}) \quad KC_t = \zeta_{kk}K_t + \zeta_{ku}U_t + \zeta_{kt}T_t$$

The equations can be expressed in matrix notation

$$\begin{bmatrix} KC_k \\ KC_u \\ KC_t \end{bmatrix} = \begin{bmatrix} K_k & U_k & T_k \\ K_u & U_u & T_u \\ K_t & U_t & T_t \end{bmatrix} \cdot \begin{bmatrix} \zeta_{kk} \\ \zeta_{ku} \\ \zeta_{kt} \end{bmatrix}$$

Where the k, u and t subscripts represent the K, U and T pads.

In a similar manner we can write two other matrix equations for UC_i and TC_i respectively.

$$\begin{bmatrix} UC_k \\ UC_u \\ UC_t \end{bmatrix} = \begin{bmatrix} K_k & U_k & T_k \\ K_u & U_u & T_u \\ K_t & U_t & T_t \end{bmatrix} \cdot \begin{bmatrix} \zeta_{uk} \\ \zeta_{uu} \\ \zeta_{ut} \end{bmatrix}$$

$$\begin{bmatrix} TC_k \\ TC_u \\ TC_t \end{bmatrix} = \begin{bmatrix} K_k & U_k & T_k \\ K_u & U_u & T_u \\ K_t & U_t & T_t \end{bmatrix} \cdot \begin{bmatrix} \zeta_{tk} \\ \zeta_{tu} \\ \zeta_{tt} \end{bmatrix}$$

Collecting the above, these equations can be expressed in matrix form as

$$\begin{bmatrix} KC_k & UC_k & TC_k \\ KC_u & UC_u & TC_u \\ KC_t & UC_t & TC_t \end{bmatrix} = \begin{bmatrix} K_t & U_k & T_k \\ K_u & U_u & T_u \\ K_t & U_t & T_t \end{bmatrix} \cdot \begin{bmatrix} \zeta_{kk} & \zeta_{uk} & \zeta_{tk} \\ \zeta_{ku} & \zeta_{uu} & \zeta_{tu} \\ \zeta_{kt} & \zeta_{ut} & \zeta_{tt} \end{bmatrix}$$

or

$$\bar{A} = \bar{B} \cdot \bar{\zeta}$$

where \bar{A} is the residual count rate matrix, \bar{B} is the matrix of the known differential concentrations and $\bar{\zeta}$ the sensitivity matrix.

Rearranging the above equations we have

$$\bar{B} = \bar{A} \cdot \bar{\zeta}^{-1}$$

We now define

$$\bar{\zeta}^{-1} = \bar{\Delta}$$

Eliminating $\bar{\zeta}$, we get

$$\bar{B} = \bar{A} \cdot \bar{\Delta}$$

We can now solve for $\bar{\Delta}$ by matrix inversion.

Therefore, the differential concentrations in the mixed pad can be derived from the k,u,t pads to check the computed $\bar{\Delta}$.

$$\begin{bmatrix} K_m \\ U_m \\ T_m \end{bmatrix} = \begin{bmatrix} \Delta_{kk} & \Delta_{ku} & \Delta_{kt} \\ \Delta_{uk} & \Delta_{uu} & \Delta_{ut} \\ \Delta_{tk} & \Delta_{tu} & \Delta_{tt} \end{bmatrix} \cdot \begin{bmatrix} KC_m \\ UC_m \\ TC_m \end{bmatrix}$$

where the subscript m refers to the mixed pad. Expanding this in algebraic form we obtain the following set of equations:

$$K_m = \Delta_{kk}(KC_m) + \frac{\Delta_{ku}UC_m}{\Delta_{kk}} + \frac{\Delta_{kt}TC_m}{\Delta_{kk}}$$

$$U_m = \Delta_{uu}(UC_m) + \frac{\Delta_{ut}TC_m}{\Delta_{kk}} + \frac{\Delta_{uk}KC_m}{\Delta_{uu}}$$

$$T_m = \Delta_{tt}(TC_m) + \frac{\Delta_{tu}UC_m}{\Delta_{tt}} + \frac{\Delta_{tk}KC_m}{\Delta_{tt}}$$

The terms in parentheses in the above 3 equations are the "corrected stripped count rates" for the system, and the stripping coefficients are as follows:

$$S_{ku} = \frac{\Delta_{ku}}{\Delta_{kk}} \quad (\text{effect of uranium on potassium})$$

$$S_{kt} = \frac{\Delta_{kt}}{\Delta_{kk}} \quad (\text{effect of thorium on potassium})$$

$$S_{ut} = \frac{\Delta_{ut}}{\Delta_{uu}} \quad (\text{effect of thorium on uranium})$$

$$S_{uk} = \frac{\Delta_{uk}}{\Delta_{uu}} \quad (\text{effect of potassium on uranium})$$

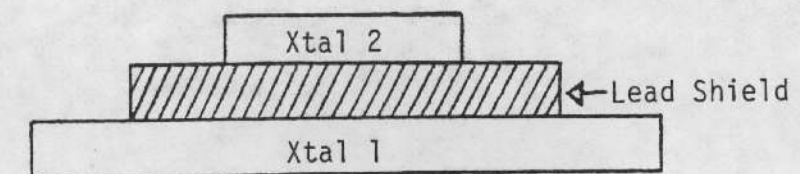
$$S_{tu} = \frac{\Delta_{tu}}{\Delta_{tt}} \quad (\text{effect of uranium on thorium})$$

$$S_{tk} = \frac{\Delta_{tk}}{\Delta_{tt}} \quad (\text{effect of potassium on thorium})$$

These stripping coefficients are defined in terms of S_{ij} in order to eliminate confusion with α , β , and γ , which are sometimes defined slightly differently.

ATMOSPHERIC RADON CORRECTION

Consider the crystal configuration shown below:



Let 1 and 2 designate the down and up crystal respectively. The down crystal sees radiation rates of I_1 composed of the air signal I_a and the ground signal I_g plus aircraft and cosmic background.

$$\text{Therefore } I_1 = I_g + I_a + A_1 + C_1$$

Similarly, the up crystal sees the air signal and ground signal (both somewhat attenuated) plus an aircraft and cosmic background.

$$\text{Therefore } I_2 = \ell I_g + m I_a + A_2 + C_2$$

Where m is the response to the air signal and ℓ is the % of the ground signal getting through to the up detector.

Using the test pad data, the factor ℓ can be determined. Consider the two previous equations. When we subtract the matrix pad data from the K, U, and T pad data, we have essentially set A_1 , A_2 , C_1 , and C_2 and I_a equal to zero.

$$\begin{aligned} \text{Therefore } I_1 &= I_g \\ I_2 &= \ell I_g \\ &= \left(\frac{I_2}{I_1} \right) \end{aligned}$$

Instead of using the count rates we can use the resultant sensitivities $1/\Delta_{uu}$ to determine ℓ for the elemental channel U.

$$= \frac{1/\Delta_{uu} \text{ (up)}}{1/\Delta_{uu} \text{ (down)}}$$

It should be noted that due to "shine around" (since the shielding is not an infinite plane, the upward looking crystal responds to the surrounding terrain) on the test pads, as altitude increases, should decrease, thus $\ell = f(h)$.

Only the factor m remains to be determined. This unfortunately cannot be determined from test pad data. It can however be determined by flying over water (e.g. use of the Lake Mead over-water data).

Consider the equations for I_1 and I_2 again

$$I_1 = I_g + I_a + A_1 + C_1$$

$$I_2 = \ell I_g + m I_a + A_2 + C_2$$

Over water $I_g = 0$

We have A_1 , A_2 , C_1 , and C_2 defined.

Removing the aircraft and cosmic background from the over water data and we are left with

$$I_1 = I_a$$

$$I_2 = m I_a$$

Since m is the shielding factor response to the air signal, we should have an air signal to "shield". Thus m is best determined if there is radon present.

Both up and down counting rates are corrected for aircraft and cosmic background and so we can solve the following two equations for I_a .

$$I_1 = I_g + I_a$$

$$I_2 = \ell I_g + m I_a$$

$$m I_a = I_2 - \ell I_g$$

$$\text{but } I_g = I_1 - I_a$$

$$\text{then } I_a (m - \ell) = I_2 - \ell I_1$$

$$\text{or } I_a = \frac{I_2 - \ell I_1}{m - \ell} = \text{Bi Air}$$

and I_a is then the Bi Air contribution from the surrounding air. This is then subtracted from the down looking U count resulting in corrected data.

DATA PROCESSING

DATA PREPARATION

The following sections summarize the techniques used for reduction and processing of the airborne data collected by geoMetrics.

Field Tape Verification and Edit

The field data tapes containing the airborne data are read on a computer to verify the recording and data quality. Data recovery is essentially 100% from the field tapes. During this phase, statistics are generated summarizing all the variables recorded for each flight line. Simultaneously, the spectral peaks are evaluated for shifts using a centroid calculation and the particular window's peak channel. The data are also checked for correct scan lengths and proper justification of data fields within each scan and live time calculations are made. During this process, the desired window data fields are extracted from each spectrum and rewritten as a reformatted copy tape. (Portions of this operation were performed in the field using the G-725 field computer system.)

The reformatted raw data for each flight line (with aborted or unnecessary flight line data edited out) are then checked for consistency, data spikes, gradients, etc. Every correction suggested by the computer is evaluated by the data processing personnel prior to implementation. Upon completion of the phase, the data on the output tape are "clean" and ready for subsequent correction of the radiometrics and tying of the magnetics.

Flight Line Location

A single frame 35 mm camera is used for obtaining position recovery information. The photo locations are spotted or transferred to a suitable base map and are digitized. The fiducial numbers of the spotted points along each line are entered during the digitizing process. A computer program is used to check the consistency of these data using calculated intersections from tie line to tie line and from traverse to traverse. This program allows easy detection of entry errors as well as potential flight path recovery errors.

A computer program then calculates the map location for each intersection and the beginning and end of each line based on the fiducial numbers and the control line/tie grid. A computer plot is made of these locations to check against the field plot and correct editing

information. These flight lines are then overlain on the geologic base map and each map unit is digitized such that each sample falls within a single unit. This resulting location information is then merged with the geophysical data using the fiducial numbers as common reference.

RADIOMETRIC DATA REDUCTION

Reduction of the raw window data was carried out utilizing system calibration constants as derived from high altitude over water flights, Lake Mead Dynamic Test Range, and the Walker Field Test Pads. The data reduction sequence used is summarized in Figure VII. Processing of the data was performed using the window energies given below:

Total count - 0.4 to 3.0 MeV

K - 1.37 to 1.57 MeV

U - 1.66 to 1.87 MeV (downward looking system)

U_{up} - 1.04 to 1.21 MeV and 1.65 to 2.42 MeV (upward looking system)

T - 2.41 to 2.81 MeV

Cosmic - 3 to 6 MeV (downward and upward looking system)

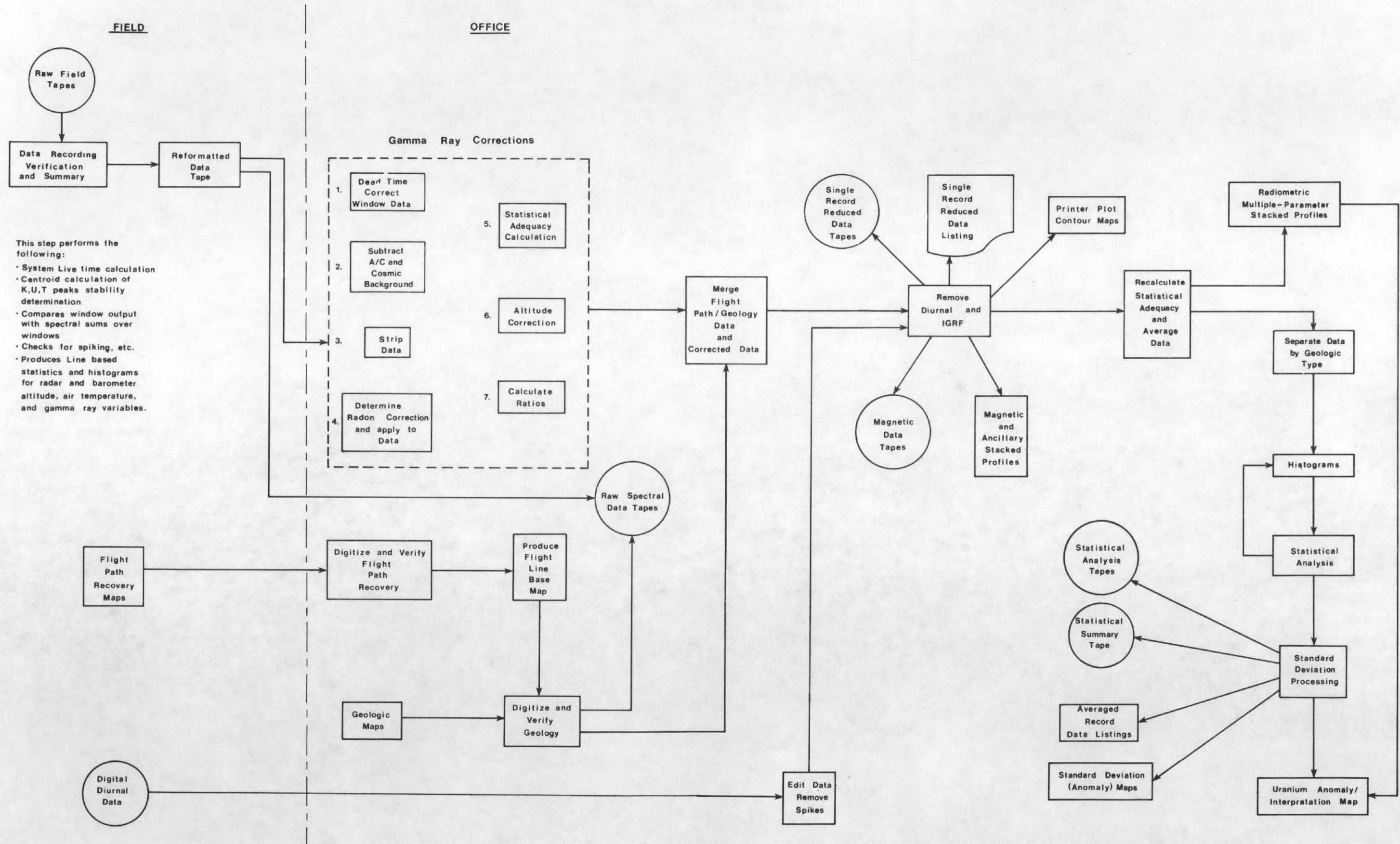
Aircraft and Cosmic background for the Queen Air/Aero Commander over these windows are as follows:

	<u>QUEEN AIR</u>		<u>AERO COMMANDER</u>	
	Aircraft	Cosmic*	Aircraft	Cosmic*
TC (cps)	152.04	2.3833	220.37	2.3915
K (cps)	16.06	0.1322	18.82	0.1334
U _{dn} (cps)	6.50	0.1098	10.85	0.1082
U _{up} (cps)	3.17	0.5540	5.35	0.5915
T (cps)	3.42	0.1503	4.35	0.1513

*Cosmic background values are in cps per 1.0 cps in the 3-6 MeV window.

DATA PROCESSING FLOW DIAGRAM

FIGURE VII



Compton corrections to the down data were made using the following constants:

S_{ij}	QUEEN AIR	AERO COMMANDER
S_{ku}	0.8437	0.8717
S_{kt}	0.1584	0.1408
S_{ut}	0.2703	0.2877
S_{uk}	0.0	0.0
S_{tu}	0.05614	0.09453
S_{tk}	0.0	0.0

The ij subscripts represent the influence of the j^{th} window on the i^{th} window.

All parameters except for S_{ut} are considered constants. S_{ut} was considered an altitude dependent parameter utilizing the following expression (after Grasty, 1975).

$$S_{ut} = S_{ut_0} + 0.0076h, \text{ where } h \text{ is the altitude in hundreds of feet.}$$

Altitude attenuation coefficients used are defined as follows:

	ALTITUDE ATTENUATION COEFFICIENTS	
	QUEEN AIR	AERO COMMANDER
TC (per foot)	0.002011	0.001688
K (per foot)	0.002740	0.002800
U (per foot)	0.002479	0.002536
T (per foot)	0.002048	0.002102

All radiometric data presented in the strip charts have been normalized to 400 feet mean terrain clearance at STP using the expression:

$$\exp - u_i \frac{273.15}{760} \times \frac{P}{T} (h - 400)$$

where h is the height in feet, i is the appropriate altitude attenuation coefficient, P is in mm of Hg, and T is in degrees Kelvin. In cases where the altitude exceeds 1,000 feet, the correction coefficients were limited to the 1,000 foot value.

Bi Air calculations are made using the following expressions:

$$U_{up} - (R_{us} + \frac{C'_{uk}}{C'_{uu}} R_{ks} + \frac{C'_{ut}}{C'_{uu}} R_{ts}) \ell$$

$$Bi_{Air} = \frac{\text{---}}{m - \ell}$$

Where U_{up} = count rate from upward detectors

ℓ = crystal coupling constant

m = crystal geometric factor

$C'_{uk}, C'_{ut}, C'_{uu}$ = stripping coefficients relating down data to up data

R_{us} = stripped uranium count rate - down system

R_{ks} = stripped potassium count rate - down system

R_{ts} = stripped thorium count rate - down system

The numerical values for the constants ℓ, m, C'_{uk} , and C'_{uu} are given below:

	QUEEN AIR	AERO COMMANDER
ℓ	0.1101	0.0890
m	0.596	0.445
C'_{uk}	0.00947	0.00964
C'_{uu}	0.07136	0.08562
C'_{ut}	0.04636	0.05644
$\mu \ell$	-0.000032	-0.00019
μm	-0.000192	-0.000112

μ_l & μ_m are altitude dependent as follows:

$$l = l - \mu_l \times h, \text{ where } h \text{ is in feet}$$

$$m = m - \mu_m \times h, \text{ where } h \text{ is in feet}$$

These Bi Air data are filtered and the filtered results are then removed on a point by point basis from the corrected uranium window data.

The window data are then evaluated for statistical adequacy prior to altitude correction to ensure they are significant within the context of the anticipated errors in count statistics.

Statistical Adequacy Test

The statistical adequacy test is made to determine whether the corrected data sample is sufficiently greater than the "noise" to represent the "signal" of interest.

We can define three separate criteria for detection thresholds (ref. Currie, Analytical Chemistry, Volume 40, No. 3, March 1968) of which only one is directly applicable to our case; this is the "critical level". This is the level at which the decision is made that a signal is "detected". We thus define this critical level as that level at which the data are statistically adequate.

Setting the actual levels in counts per second, "a priori" for each elemental window is difficult at best since the full effect of all parameters affecting the counts is not known to a sufficient degree of certainty. If the corrections to the data are a significant portion of the count rate, most of the error (exclusive of systematic errors due to electronics, etc.) in the corrected data can be ascribed to random errors within the applied corrections. The corrections are basically the results of counting radioactive decay products (gamma rays) and are therefore assumed to follow the classical Poisson distribution. The following assumptions concerning these corrections are:

1. In the best case, the error in each correction is additive.
2. The sum of these corrections also follows a Poisson distribution.
3. The uncertainty in the correction itself is equal to the square root of the correction applied.
4. This uncertainty is directly reflected in the corrected single record count rate.

With these assumptions in mind, the criterion for determining the statistical adequacy of a given data sample is defined as follows:

"If a corrected single record data sample exceeds 1.5 times the square root of the summed correction applied to that data sample, then that data sample is statistically adequate."

Since any calculation using statistically inadequate data (such as ratios) is also inadequate, the adequacy of each element of the single sample record data is tested prior to the calculation. This is done during the course of the processing by retaining all corrections applied to each data sample and determining its adequacy as explained above.

Not only are the results of this statistical adequacy test used to insure that calculated ratios will be meaningful but they are also utilized to determine the optimum interval over which the data should be averaged (e.g. 5 seconds or 7 seconds, etc.) to improve the overall data statistical adequacy. In the case of this project, the resulting averaging sample interval was 7 seconds.

Conversion to Equivalent ppm and Percent

At this point the data are single record corrected samples in units of counts per second. These data are then converted to equivalent ppm (parts per million) uranium, thorium and percent potassium. The conversion factors are the sensitivities derived from the Lake Mead Dynamic Test Range data at 400 feet mean terrain clearance.

<u>Radioelement</u>	<u>Equivalent Percent/ppm</u>	<u>Queen Air Counts/Second</u>	<u>Aero Commander Counts/Second</u>
K	1%K	91.5	96.3
U	1 ppmeU	10.4	9.2
T	1 ppmeT	6.4	6.7

DATA PRESENTATION

MAGNETIC DATA REDUCTION

The magnetic data reduction processes are: correction for diurnal variation, tying to a common magnetic datum, and subtraction of the regional magnetic field as defined by the International Geomagnetic Reference Field (IGRF). During data acquisition, the magnetic field is monitored by a ground-based diurnal magnetometer that samples every four seconds at a sensitivity of one-quarter gamma. These data are recorded on magnetic tape along with the time for synchronization with the airborne data.

The diurnal data are edited to keep only samples taken during flight time and remove spikes and man-made magnetic events. After editing, these data are displayed in profile form to ensure that all corrections necessary have been made. Next, the data are synchronized in time with the airborne data, interpolated, and subtracted from the airborne magnetic data.

The diurnally corrected magnetic data are then processed by a tying program that compares the magnetic differences at intersections of flight lines and tie lines. This program calculates individual magnetic field biases for each flight tie line based on tie line intersections. This allows miss-ties to be minimized throughout the survey. These biases usually represent, after diurnal correction, systematic magnetic changes caused by such things as heading error, changes in location of the ground-based magnetometer, or changes in the airborne equipment. The biases are manually evaluated and selectively applied.

General

The majority of the data products are presented in this report. These include the uranium anomaly/interpretation maps and pseudo-contour maps of potassium, uranium, thorium, and magnetic data which are integrated as part of the text in the interpretation section. In addition to these data, this report contains data presented in the form of radiometric profiles, flight path recovery maps, standard deviation maps, and histograms. Microfiche data are contained in the back cover of each report. Data tapes are available separately.

Radiometric Profiles

Stacked profiles were prepared from the averaged data for each traverse and tie line. These stacked profiles, plotted at a linear scale of 1:250,000, contain the following parameters: corrected Total Count, percent potassium, equivalent ppm uranium, equivalent ppm thorium, eU/eT, eU/%K, and eT/%K ratios, equivalent ppm Bi Air, radar altimeter, and magnetometer data. Each of the stacked profile sheets contains a plot of the flight path superimposed on a geologic strip map. Included along these profiles are the fiducial numbers which correspond to flight path position as displayed on the flight path recovery maps. Each of the stacked profiles represents the data contained on the specific flight line within the boundaries of the specified NTMS Quadrangle sheet.

Radiometric traces on the stacked profiles contain an indicator showing those data which are statistically inadequate. These statistically inadequate data are marked by a small vertical tick at the sample location. The altitude profile has been limited in display to 1,000 feet. A dashed line at the 700 foot level is presented to show those data which do not meet the altitude specifications. The vertical scale of each variable remains constant on all stacked profiles. When overranging occurs, the trace is stepped and the step labeled showing the actual value. A pictorial representation of such a stepping profile is shown in Figure VIII. At the end of each stacked profile, a statistical summary of the minimum value, maximum value, mean, and standard deviation for that variable is presented.

This report contains an equivalent set of stacked profiles for each quadrangle, photographically reduced to an approximate scale of 1:500,000.

MAGNETIC PROFILES

A set of profiles containing the magnetic data (corrected, with IGRF removed), barometric altimeter data, radar altimeter data, diurnal monitor data, and temperature data are available at a linear scale of 1:250,000. Each of the stacked profiles contains a plot of the flight path superimposed on the geology over which the aircraft flew. Reduced scale (1:500,000) copies of these are presented in of this report.

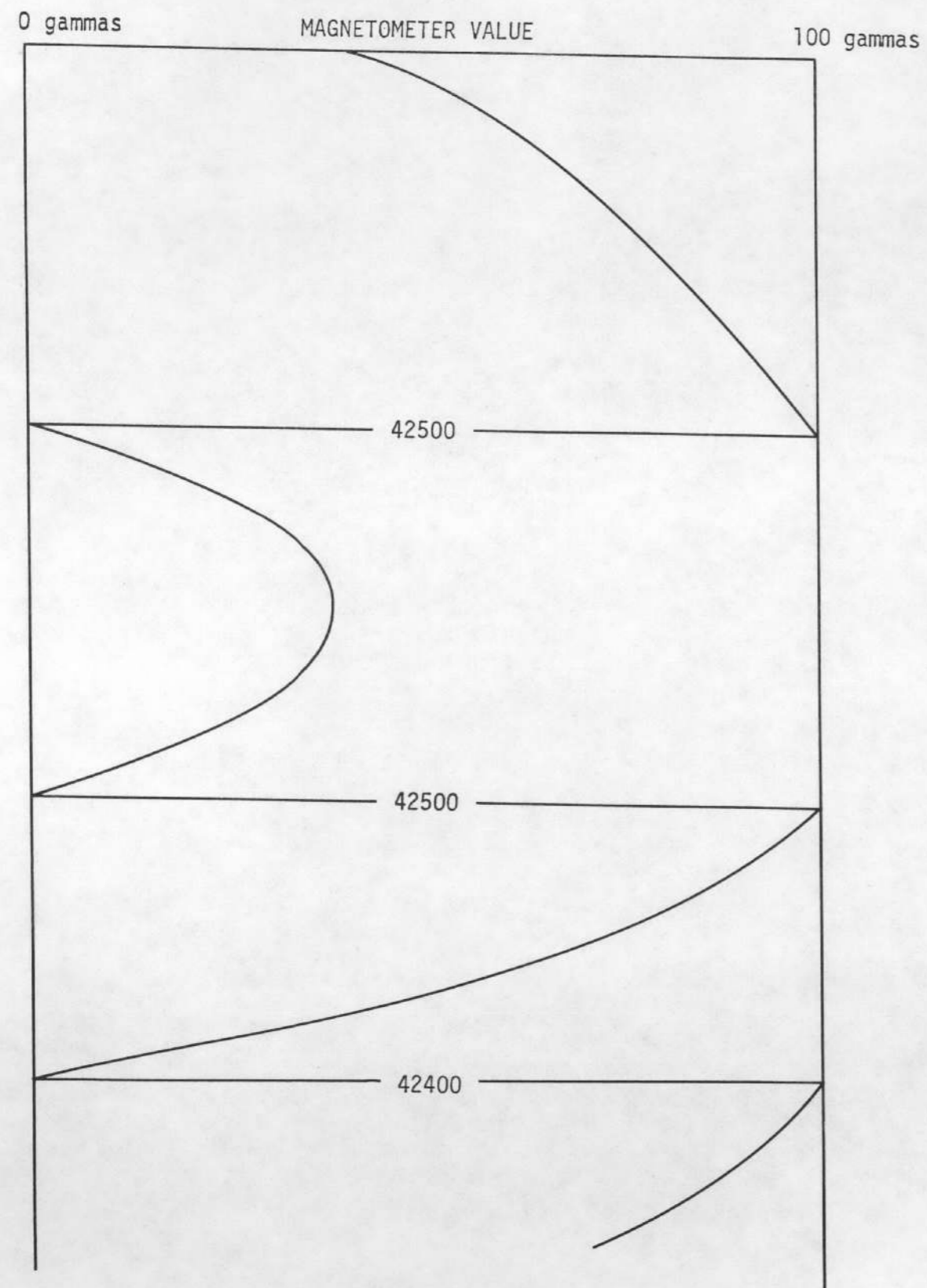


FIGURE VIII Plotter Step Value Labeling

FLIGHT PATH MAPS

For each of the NTMS quadrangle sheets covered by this survey, a flight path position map is available at a scale of 1:250,000. The actual flight path has been superimposed on the geologic quadrangle maps. Flight lines and tie lines are annotated along with fiducial numbers of located positions. Reduced scale (1:500,000) copies of these can be found in this report.

STANDARD DEVIATION MAPS

Gamma ray standard deviation maps have been prepared for each NTMS quadrangle included in this survey. The six maps generated represent the following parameters: percent potassium, equivalent ppm uranium, equivalent ppm thorium, and eU/eT, eU/%K and eT/%K ratios. The data contained in each map represent only those data which are considered statistically adequate. This automatically excludes all data collected over water or data which falls outside of altitude specifications (i.e. altitude greater than 700 and less than 200 feet). The symbolism of each of the six maps is identical. The center of each circle represents the central averaged sample since the data had been averaged over a 7 second interval. The small boxes adjacent to each of the circles represents one standard deviation from the mean for that specific data sample. In order to determine whether the data shown are represented by positive or negative standard deviations, consider each map with north pointing away from the viewer. For east/west lines (traverse lines) positive standard deviations lie above or to the north of the traverse line with negative standard deviation below or to the south. On the north/south lines (tie lines) positive standard deviations are to the left of the viewer (west) with negative standard deviations to the right (east).

These maps were generated at a scale of 1:250,000 for each NTMS sheet and in addition, are presented in each report at a reduced scale of approximately 1:500,000.

HISTOGRAMS

Computer generated histograms, showing the equivalent ppm and percent distributions for the three gamma ray emitters and their ratios measured and calculated as a function of computer map unit are presented in this report (See Figure IX). Information contained on these histograms includes the standard deviation as calculated about the arithmetic mean (or median), and the total number of samples from which the statistics were derived.

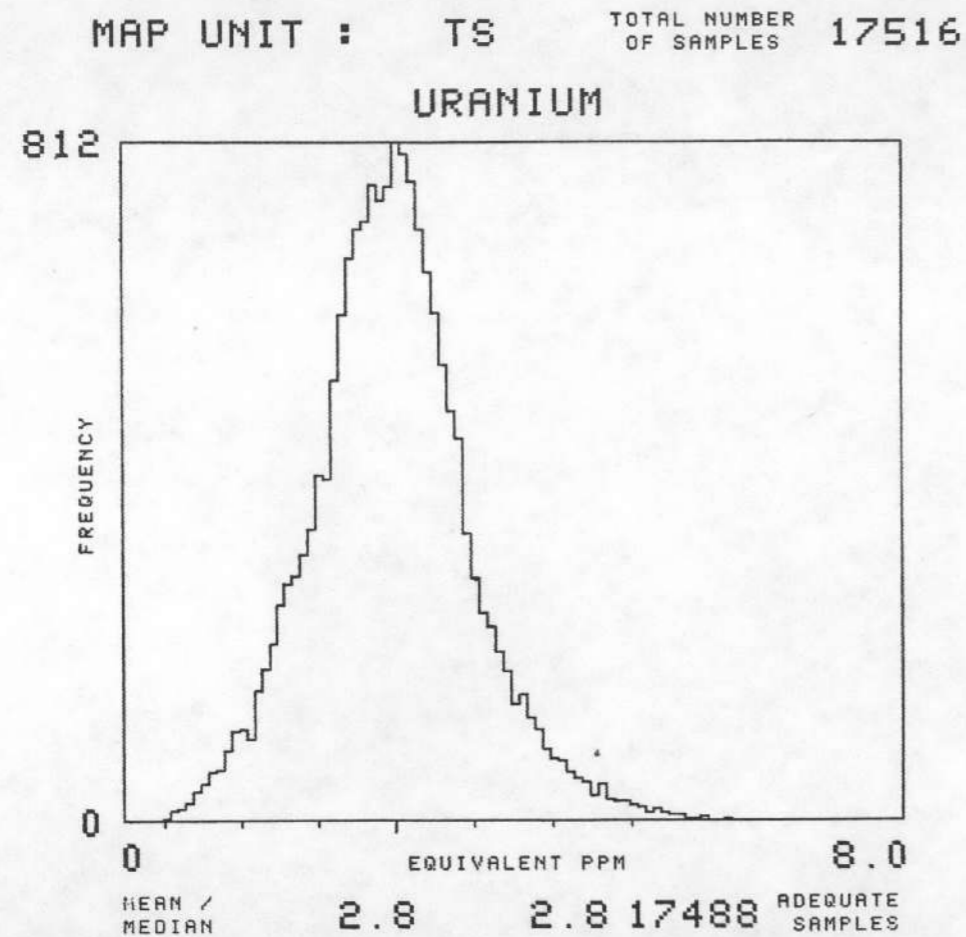


FIGURE IX Sample Computer Map Unit Histogram

DATA LISTINGS

Single record reduced and averaged record (statistical analysis) data listings have been prepared on microfiche. The microfiche are contained in each report. Each of the single record and averaged record data listings are presented for the data contained in a single quadrangle. The data contained in the single record data listings are summarized below:

1. Fiducial number
2. System/Quality (SAKUT) - The first digit identifies the system used to collect the sample. The remaining digits define the results of statistical adequacy testing for altitude, potassium, uranium, and thorium. A value of 0 indicated that the data are statistically adequate. A value of 1 indicates that the data are statistically inadequate. All data collected in excess of 700 feet and less than 200 feet are considered statistically inadequate.
3. Time - time presented in hours, minutes, and seconds
4. Altitude - altitude presented in feet above terrain
5. LAT/LONG - Latitude and Longitude presented in terms of decimal degrees
6. Magnetic field expressed in residual gammas
7. Geology - code representing geologic units
8. %K, eU, eT - percent potassium, equivalent ppm of uranium and thorium
9. eU/eTH, eU/%K, eTH/%K - calculated ratios of the three parameters
10. Total count - corrected total count data (0.4 to 3.0 MeV)
11. COS - downward looking cosmic count rate in the 3-6 MeV channel
12. Uair - atmospheric Bi-214 equivalent ppm
13. Temperature - outside air temperature in degrees centigrade
14. Press - barometric pressure in mm of mercury

The averaged record (statistical analysis) data listings are summarized below:

1. Fiducial number
2. System/Quality (SAKUT) - The first digit identifies the system used to collect the sample. The remaining digits define the results of statistical adequacy testing for altitude, potassium, uranium, and thorium. A value of 0 indicates that the data are statistically adequate. A value of 1 indicates that the data are statistically inadequate. All data collected in excess of 700 feet and less than 200 feet are considered statistically inadequate.
3. LAT/LONG - Latitude and longitude presented in terms of decimal degrees
4. Magnetic field expressed in residual gammas
5. Geology - code representing geologic formations
6. %K, eU, eT - percent potassium, equivalent ppm of uranium and thorium data and the number of (+) standard deviations from the mean
7. eU/eTH, eU/%K, eTh/%K - calculated ratios of the three parameters, and the number of (+) standard deviations from the mean
8. Total count - corrected total count data (0.4 to 3.0 MeV)
9. COS - downward looking cosmic count rate in the 3-6 MeV channel
10. Uair - atmospheric Bi-214 in equivalent ppm

DATA TAPES

Data tape files have been generated for each of the 1:250,000 NTMS quadrangle sheets. The tapes are IBM compatible and recorded on 9 track EBCDIC at 800 bpi. Five separate types of data tapes are presented: raw spectral data tapes, single record reduced data tapes, statistical analysis tapes, magnetic data tapes and a statistical analysis summary tape. Detailed descriptions of the data tape formats follow this discussion.

DATA INTERPRETATION METHODS

General

The stated objective of the NURE Program is the evaluation of the uranium potential of the United States. In support of this goal, high sensitivity airborne radiometric and magnetic surveys have been implemented to obtain reconnaissance information pertaining to regional distribution of uranium materials. Within this context, data interpretation has been oriented toward regional detection and description of anomalously high concentrations of uranium.

By far the most significant natural sources of gamma radiation in the geologic environment are the radioactive decay series of potassium 40 (K40), thorium 232 (Th232) and uranium 238 (U238) of which 0.7% is uranium 235. Potassium 40 is the largest contributor to natural radioactivity, accounting for nearly 98%, as it is the most abundant gamma ray emitter-.012% of all potassium in nature. (Refer to GSA Memoir 97 for abundances of uranium, thorium, and potassium).

Potassium 40 is directly identified by the airborne spectrometer from a single clear peak at 1.46 mev (million electron volts) in its gamma ray spectrum. However, thorium 232 and uranium 238 do not have any clear, distinct peaks at sufficiently high energies to allow direct detection from airborne systems. Instead, daughter products which do have distinct peaks are measured as representing the abundance of the parent element. For thorium 232, the daughter nuclide thallium 208 (Tl208) has a distinct peak at 2.62 mev while uranium 238 has a daughter, bismuth 214 (Bi214) possessing a clear peak at 1.76 mev (see Figure 7 for a composite decay series spectrum). Consequently the fundamental assumption implicit to airborne uranium and thorium measurements is that the measured daughter products are in radioactive equilibrium - the number of atoms of disintegrating daughter nuclides are equal to the number being formed (see Adams and Gasparini, 1970).

An airborne gamma ray measurement is the sum of photons counted during a specified time interval from a multitude of gamma ray sources which include the three geologic emitters that are being sought plus other interfering sources. These others include, but are not limited to higher energy cosmic rays, aircraft and instruments, contributions from overlapping decay series and airborne radon 222. (See Burson, 1974 and McSharry, 1973 for a more complete discussion of airborne radiometric measurements, and Radiometric Data Reduction in this volume for a complete description of data correction procedures).

When correlating ground data (geochemical, geological, etc.) with the corrected data derived from raw airborne measurements, the interpreter must remember what an individual airborne gamma ray sample physically measures. First, the terrestrial component of the gamma radiation measured by the airborne detector emanated primarily from the upper 18 inches of material on the earth's surface (Gregory and

Horwood, 1963). The airborne measurement cannot "see" any deeper into the underlying rock material and is essentially a measurement of the soil's or exposed (weathered) rock's radioactivity. Secondly, since each airborne sample is an accumulation of gamma rays measured on a moving platform over a fixed period of time, the individual sample represents a large areal extent of surficial material. For this survey, with specifications of 400 feet mean terrain clearance and an average ground speed of 140 miles per hour, a one second sample corresponds to an oval approximately 750 feet long by 600 feet wide (assuming an infinite, uniformly distributed source). Accordingly, averaged samples represent tremendous volumes of surficial materials.

Methodology

As described previously, the gamma ray data were located by computer map units, histograms were produced and statistical analyses performed. The basic unit for interpretation then is the averaged sample and its attendant deviations about a particular map unit's mean.

The uranium anomaly/interpretation map displays each individual averaged sample that meets the following criteria:

1. The averaged uranium sample must be greater than or equal to 1 standard deviation above its map unit mean.
2. The sample must have a U/T ratio greater than or equal to 1 standard deviation above its unit mean.
3. Each U/T ratio defined in (2) must have a corresponding thorium value lying at least greater than minus one (-1) standard deviation below the mean. If the thorium sample is less than one standard deviation below the mean, the U/T ratio is considered questionable.

All the possible anomalies displayed on the map are then examined for clusters, trends, and comparisons with all other available data.

Minimum requirements in the subsequent interpretation discussions of each quadrangle for anomalies listed in the uranium anomaly summary are defined as follows:

Two (2) consecutive averaged U samples lying two or more standard deviations above the mean or three (3) consecutive averaged U samples, two of which are one (1) or more standard deviations and the third of which is two (2) or more standard deviations above the mean.

Statistical anomalies which meet the above criteria can result from several factors or circumstances including: (1) true concentration of uraniferous minerals, (2) differential surface cover (soils and/or

vegetation) within a lithologic unit, (3) local weather conditions such as rain and snow, (4) extreme facies variation within a mapped unit, and (5) differential weathering of rocks within mapped units. Obviously an averaged sample which lies on the boundary between two map units is not truly reflecting either one, but is rather an average of both. Thus, for two markedly different units, such a sample would be anomalous relative to one of the units and not be a true indication of radioactive differences within the unit.

The percent potassium, equivalent ppm thorium and uranium, the three ratios and residual magnetic data were plotted as separate pseudo-contour maps and overlain on the geologic base map and standard deviation maps. Regional trends of each variable and average values could thus be easily and quickly determined and compared with the associated geological, magnetic, and statistical trends. Only the long wavelengths within each variable would show any line-to-line continuity on the pseudo-contour maps and thus, only regional trends will appear.

Each quadrangle's stacked profiles were also overlain on the corresponding geologic and standard deviation maps and anomaly map to further delineate trends and to allow a more detailed analysis of individual anomalies. Since the interpretation was concentrated on detection of anomalous uranium, subtle trends present in the potassium and thorium channels and ratios were only examined in a cursory manner. Even during such a brief examination of the profiles, it was evident that the spectrometer system was highly sensitive to changes in surface materials even in areas of low counting rates such as glacial drift. Thus radiometrics have a real potential for performing general surficial mapping "geochemical analysis" on a geologic unit (or soils) basis in addition to merely radioactive mineral "anomaly hunting".

TAPE FORMATS

SINGLE RECORD REDUCED DATA TAPE

REFERENCE: Paragraphs 4.7.6 and 6.1.6, BFEC 1200-C

The Single Record Tape is an unlabeled, nine track, 800 BPI, NRZI. All data are recorded as EBCDIC characters. Each tape contains but one file of format, header, data, and trailer records for no more than one quadrangle. The tape is divided into 6900-character blocks containing the following information.

Block 1 - Format Data

This block contains 6768 characters in 94 consecutive lines of 72 characters containing the following literal description.

02 0978 (DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)

SINGLE RECORD REDUCED DATA TAPE

FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)

<u>ITEM</u>	<u>FORMAT</u>	<u>DESCRIPTION</u>
1.	A40	QUADRANGLE NAME AS PROJECT IDENTIFICATION
2.	A20	NAME OF SUBCONTRACTOR
3.	I4	APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
4.	I1	NUMBER OF AERIAL SYSTEMS USED TO COLLECT DATA FOR THIS QUADRANGLE
5.	I1	AERIAL SYSTEM IDENTIFICATION CODE FOR FIRST SYSTEM
6.	A20	AIRCRAFT IDENTIFICATION BY TYPE AND FAA NUMBER FOR FIRST SYSTEM
7.	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN CPS PER PERCENT K
8.	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT U
9.	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT TH

<u>ITEM</u>	<u>FORMAT</u>	<u>DESCRIPTION</u>
13	I3	NUMBER OF CHANNELS (0-3 MEV) IN 4PI SYSTEM FOR FIRST AERIAL SYSTEM
14	I3	NUMBER OF CHANNELS (0-3 MEV) IN 2PI SYSTEM FOR FIRST AERIAL SYSTEM
15-24	(SAME)	REPEAT OF ITEMS 5-14 FOR SECOND AERIAL SYSTEM
*	*	*
*	*	*
*	*	*
85-94	(SAME)	REPEAT OF ITEMS 5-14 FOR NINTH AERIAL SYSTEM
95	I3	NUMBER OF FLIGHT LINES ON THIS TAPE
96	I4	FIRST FLIGHT LINE NUMBER ON THIS TAPE
97	I6	FIRST RECORD NUMBER OF FIRST FLIGHT LINE
98	I3	JULIAN DATE (DAY OF YEAR) FIRST FLIGHT-LINE DATA WAS COLLECTED
99-101	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR SECOND FLIGHT LINE ON THIS TAPE
*	*	*
*	*	*
*	*	*
390-392	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR 99th FLIGHT LINE ON THIS TAPE

FORMAT FOR SINGLE RECORD REDUCED DATA RECORD (THIRD THRU LAST BLOCK)

<u>ITEM</u>	<u>FORMAT</u>	<u>DESCRIPTION</u>
1	I1	AERIAL SYSTEM IDENTIFICATION CODE
2	I4	FLIGHT LINE NUMBER
3	I6	RECORD IDENTIFICATION NUMBER
4	I6	GMT TIME OF DAY (HHMMSS)
5	F8.4	LATITUDE TO FOUR DECIMAL PLACES IN DEGREES
6	F8.4	LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
7	F6.1	TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
8	F7.1	RESIDUAL (IGRF REMOVED) MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
9	A8	SURFACE GEOLOGIC MAP UNIT CODE
10	I4	QUALITY FLAG CODES
11	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
12	F4.1	UNCERTAINTY IN TERRESTRIAL POTASSIUM TO ONE DECIMAL PLACE IN PERCENT K
13	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
14	F4.1	UNCERTAINTY IN TERRESTRIAL URANIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
15	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
16	F4.1	UNCERTAINTY IN TERRESTRIAL THORIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH

ITEM	FORMAT	DESCRIPTION
17	F6.1	URANIUM-TO-THORIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
18	F6.1	URANIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
19	F5.1	THORIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
20	F8.1	GROSS GAMMA (0.4-3.0 MEV) COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
21	F6.1	UNCERTAINTY IN GROSS GAMMA COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
22	F5.1	ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
23	F4.1	UNCERTAINTY IN ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
24	F4.1	OUTSIDE AIR TEMPERATURE TO ONE DECIMAL PLACE IN DEGREES CELSIUS
25	F5.1	OUTSIDE AIR PRESSURE TO ONE DECIMAL PLACE IN MMHG

This description serves to identify the format of data on subsequent blocks on the tape. The remaining 132 characters on this block are blanks.

Block 2 - Single Record Reduced Identification Data

The second block contains the identifier information for the data contained in subsequent blocks. The identification information is written according to the format description in the first half of the first block. The remaining 4978 characters on this block are blanks.

Block 3 - Single Record Reduced Data

These blocks contain data written according to the format description in the second half of the first block. There will be 50 logical records per physical block. As of August 1979, the method for determining uncertainties specified in the data blocks remains undefined, and those values are filled with 9's under format control.

STATISTICAL ANALYSIS TAPE

REFERENCE: Paragraphs 4.7.7 and 6.1.6, BFEC 1200-C

The statistical analysis data tape is an unlabeled, nine track, 800 BPI, NRZI. All data is recorded as EBCDIC characters. The block length is 8000 characters long. Each tape contains one file of data for no more than one quadrangle.

Block 1 - Format Description Data

The first physical block on this tape contains a format description for data on subsequent blocks. The first 7560 characters on this block contains 105 lines of 72 characters exactly as written below:

03 0978 (DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)

STATISTICAL ANALYSIS DATA TAPE

FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)

ITEM	FORMAT	DESCRIPTION
1	A40	QUADRANGLE NAME AS PROJECT IDENTIFICATION
2	A20	NAME OF SUBCONTRACTOR
3	I4	APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
4	I1	NUMBER OF AERIAL SYSTEMS USED TO COLLECT DATA FOR THIS QUADRANGLE
5	I1	AERIAL SYSTEM IDENTIFICATION CODE FOR FIRST SYSTEM
6	A20	AIRCRAFT IDENTIFICATION BY TYPE AND FAA NUMBER FOR FIRST SYSTEM
7	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN CPS PER PERCENT K
8	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT U
9	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT TH
10	I6	BLANK FIELD (99999)
11	F6.3	4PI-SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS FOR FIRST SYSTEM
12	F6.3	2PI-SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS FOR FIRST SYSTEM
13	I3	NUMBER OF CHANNELS (0-3 MEV) IN 4PI SYSTEM FOR FIRST AERIAL SYSTEM
14	I3	NUMBER OF CHANNELS (0-3 MEV) IN 2PI SYSTEM FOR FIRST AERIAL SYSTEM

ITEM	FORMAT	DESCRIPTION
15-24	(SAME)	REPEAT OF ITEMS 5-14 FOR SECOND AERIAL SYSTEM
*	*	*
*	*	*
*	*	*
85-94	(SAME)	REPEAT OF ITEMS 5-14 FOR NINTH AERIAL SYSTEM
95	I3	NUMBER OF FLIGHT LINES ON THIS TAPE
96	I4	FIRST FLIGHT LINE NUMBER ON THIS TAPE
97	I6	FIRST RECORD NUMBER OF FIRST FLIGHT LINE
98	I3	JULIAN DATE (DAY OF YEAR) FIRST FLIGHT-LINE DATA WAS COLLECTED
99-101	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR SECOND FLIGHT LINE ON THIS TAPE
*	*	*
*	*	*
*	*	*
390-392	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR 99th FLIGHT LINE ON THIS TAPE

FORMAT FOR STATISTICAL ANALYSIS DATA RECORD (THIRD THRU LAST BLOCK)

ITEM	FORMAT	DESCRIPTION
1	I1	AERIAL SYSTEM IDENTIFICATION CODE
2	I4	FLIGHT LINE NUMBER
3	I6	RECORD IDENTIFICATION NUMBER
4	I6	GMT TIME OF DAY (HHMMSS)
5	F8.4	LATITUDE TO FOUR DECIMAL PLACES IN DEGREES
6	F8.4	LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
7	F6.1	TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
8	F7.1	RESIDUAL (IGRF Removed) MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
9	A8	SURFACE GEOLOGIC MAP UNIT CODE
10	I4	QUALITY FLAG CODES
11	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN PERCENT K
12	F4.1	UNCERTAINTY IN TERRESTRIAL POTASSIUM TO ONE DECIMAL PLACE IN PERCENT K
13	F5.1	POTASSIUM STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
14	F6.1	AVERAGED CONCENTRATION OF TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
15	F4.1	UNCERTAINTY IN TERRESTRIAL URANIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
16	F5.1	URANIUM STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
17	F6.1	AVERAGED CONCENTRATION OF TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
18	F4.1	UNCERTAINTY IN TERRESTRIAL THORIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
19	F5.1	THORIUM STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRIACALLY SIGNED.

ITEM	FORMAT	DESCRIPTION
20	F8.1	GROSS GAMMA (0.4-3.0 MEV) COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
21	F6.1	UNCERTAINTY IN GROSS GAMMA COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
22	F5.1	ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
23	F4.1	UNCERTAINTY IN ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DEICMAL PLACE IN PPM EQUIVALENT U
24	F4.1	AVERAGED URANIUM-TO-THORIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
25	F5.1	URANIUM-TO-THORIUM RATIO STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
26	F6.1	AVERAGED URANIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
27	F5.1	THORIUM-TO-POTASSIUM RATIO STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
D8	F6.1	AVERAGED THORIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
29	F5.1	THORIUM-TO-POTASSIUM RATIO STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED

The remaining 440 characters in this block are blanks.

Block 2 - Statistical Analysis Identification Data

The second block contains the identifier information for the data contained in subsequent blocks according to the format specification in the first part of Block 1. The final 6078 characters on this block are blanks.

Block 3 - Statistical Analysis Data

The third and subsequent blocks contain statistical analysis data in the format specified by the second part of the Block 1. Fifty logical records are allowed per block. The method for determining uncertainty values shown, as of August 1979, remains undefined. These values are filled with 9's under format control.

MAGNETIC DATA TAPE

REFERENCE: Paragraphs 4.7.8 and 6.1.6, BFEC 1200-C

The Magnetic Data Tape is an unlabeled, nine track, 800 BPI, NRZI. All data are recorded as EBCDIC characters. Each tape contains data for no more than one quadrangle and are divided into 8000-character blocks as described below.

Block 1 - Tape Format Description

The first block contains 3384 characters of format information in exactly the following format:

04 0978 (DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)

MAGNETIC DATA TAPE

FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)

ITEM	FORMAT	DESCRIPTION
1	A40	QUADRANGLE NAME AS PROJECT IDENTIFICATION
2	A20	NAME OF SUBCONTRACTOR
3	I4	APPROXIMATE DATE OF SURVEY (MONTH., YEAR)
4	I3	NUMBER OF FLIGHT LINES ON THIS TAPE
5	I4	FIRST FLIGHT LINE ON THIS TAPE
6	I6	FIRST RECORD NUMBER OF FIRST FLIGHT LINE
7	I3	JULIAN DATE (DAY OF YEAR) FIRST FLIGHT-LINE DATA WAS COLLECTED
8	F8.4	LATITUDE OF GROUND BASE STATION TO FOUR DECIMAL PLACES IN DEGREES FOR FIRST FLIGHT LINE
9	F8.4	LONGITUDE OF GROUND BASE STATION TO FOUR DECIMAL PLACES IN DEGREES FOR FIRST FLIGHT LINE
10-14	(SAME)	REPEAT OF ITEMS 5-9 FOR SECOND FLIGHT LINE ON THIS TAPE
*	*	*
*	*	*
*	*	*
495-499	(SAME)	REPEAT OF ITEMS 5-9 FOR 99th FLIGHT LINE ON THIS TAPE

FORMAT FOR MAGNETIC DATA RECORD (THIRD THRU LAST BLOCK)

ITEM	FORMAT	DESCRIPTION
1	I1	AERIAL SYSTEM IDENTIFICATION CODE
2	I4	FLIGHT LINE NUMBER
3	I6	RECORD IDENTIFICATION NUMBER
4	I6	GMT TIME OF DAY (HHMMSS)
5	F8.4	LATITUDE TO FOUR DECIMAL PLACES IN DEGREES

ITEM	FORMAT	DESCRIPTION
6	F8.4	LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
7	F6.1	TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
8	F5.1	OUTSIDE AIR PRESSURE TO ONE DECIMAL PLACE IN MMHG
9	A8	SURFACE GEOLOGIC MAP UNIT CODE
10	F7.1	TOTAL MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
11	F7.1	RESIDUAL (IGRF REMOVED) MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
12	F7.1	DIURNAL MAGNETIC INTENSITY VARIATION TO ONE DECIMAL PLACE IN GAMMAS
13	F7.1	MAGNETIC DEPTH-TO-BASEMENT TO ONE DECIMAL PLACE IN METERS (IF REQUIRED)

The remaining 4616 characters in this block are blanks.

Block 2 - Magnetic Tape Identification Data

This block contains information about the data in subsequent blocks organized according to the format specification in the first half of Block 1.

Block 3 - Magnetic Data

This block and subsequent block contains magnetic data for the quadrangle organized according to the format specifications in the second half of Block 1. There will be 100 logical records per physical block.

STATISTIC ANALYSIS SUMMARY TAPE

REFERENCE: Paragraphs 4.7.9, BFEC 1200-C

The statistical analysis summary tape is an unlabeled, nine track, 800 BPI, NRZI. All data is recorded as EBCDIC characters. The block length is 700 characters long. Each tape contains one file of data for no more than one quadrangle.

Block 1 - Format Description Data

The first physical block on this tape contains a format description for data on subsequent blocks. The first 4320 characters on this block contains 60 lines of 72 characters exactly as written below:

05 0978 (DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODE)

STATISTICAL ANALYSIS SUMMARY TAPE (OR FILE)

FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)

ITEM	FORMAT	DESCRIPTION
1	A40	QUADRANGLE NAME AS PROJECT IDENTIFICATION
2	A20	NAME OF SUBCONTRACTOR
3	I4	APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
4	I6	NUMBER OF GEOLOGIC MAP UNITS USED FOR THIS QUADRANGLE

FORMAT FOR STATISTICAL ANALYSIS SUMMARY DATA RECORD (THIRD THRU LAST BLOCK)

ITEM	FORMAT	DESCRIPTION
1	A8	SURFACE GEOLOGIC MAP UNIT IDENTIFYING CODE
2	I6	TOTAL RECORDS FOR GEOLOGIC MAP UNIT
3	I6	NUMBER OF POTASSIUM RECORDS COMPUTED FOR GEOLOGIC UNIT
4	F6.1	POTASSIUM CONCENTRATION MEAN TO ONE DECIMAL PLACE IN PERCENT K
5	F6.1	POTASSIUM CONCENTRATION STANDARD DEVIATION TO ONE DECIMAL PLACE IN PERCENT K
6	A3	POTASSIUM CONCENTRATION DISTRIBUTION CODE
7	I6	NUMBER OF URANIUM RECORDS COMPUTED FOR GEOLOGIC UNIT
8	F6.1	URANIUM CONCENTRATION MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
9	F6.1	URANIUM CONCENTRATION STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
10	A3	URANIUM CONCENTRATION DISTRIBUTION CODE
11	I6	NUMBER OF THORIUM RECORDS COMPUTED FOR GEOLOGIC UNIT
12	F6.1	THORIUM CONCENTRATION MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
13	F6.1	THORIUM CONCENTRATION STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
14	A3	THORIUM CONCENTRATION DISTRIBUTION CODE
15	I6	NUMBER OF URANIUM-TO-THORIUM RATIO RECORDS COMPUTED FOR GEOLOGIC UNIT

16	F6.1	URANIUM-TO-THORIUM RATIO MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT U PER PPM EQUIVALENT TH
17	F6.1	URANIUM-TO-THORIUM RATIO STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
18	A3	URANIUM-TO-THORIUM RATIO DISTRIBUTION CODE
19	I6	NUMBER OF URANIUM-TO-POTASSIUM RATIO RECORDS COMPUTED FOR GEOLOGIC UNIT
20	F6.1	URANIUM -TO-POTASSIUM RATIO MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
21	F6.1	URANIUM-TO-POTASSIUM RATIO STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT
22	A3	URANIUM-TO-POTASSIUM RATIO DISTRIBUTION
23	I6	NUMBER OF THORIUM-TO-POTASSIUM RATIO RECORDS COMPUTED FOR GEOLOGIC UNIT
24	F6.1	THORIUM-TO-POTASSIUM RATIO MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
25	F6.1	THORIUM-TO-POTASSIUM RATIO STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
26	A3	THORIUM-TO-POTASSIUM RATIO DISTRIBUTION CODE

The remaining 2680 characters on this block shall be blanks.

Block 2 - Statistical Analysis Identification Data

The second block contains the identifier information for the data contained in subsequent blocks according to the format specification in the first part of Block 1. The final 6930 characters on this block are blanks.

Block 3 - Statistical Analysis Summary Data

The third and subsequent blocks contain statistical analysis data in the format specified by the second part of the Block 1. Fifty logical records are allowed per block.

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APPENDIX B - Flight Summary

APPENDIX B
DAILY PRODUCTION SUMMARY
NOVEMBER, DECEMBER, 1980
QUEEN AIR N9AG

Nov. 27-30	Aircraft Maintenance
Dec. 1-3	Base Mobilization
4	434 line miles Louisville, Huntington
5	434 " " " "
6	868 " " " "
7	Weather - nil production
8	848 line miles Louisville, Huntington
9	Weather - nil production
10	848 line miles Louisville, Huntington
11	Weather - nil production
12	630 line miles Marion
13	630 " " Marion
14	671 " " Marion, Toledo
15	Weather - nil production
16	" " " "
17	1055 line miles Cincinnati

AERO COMMANDER

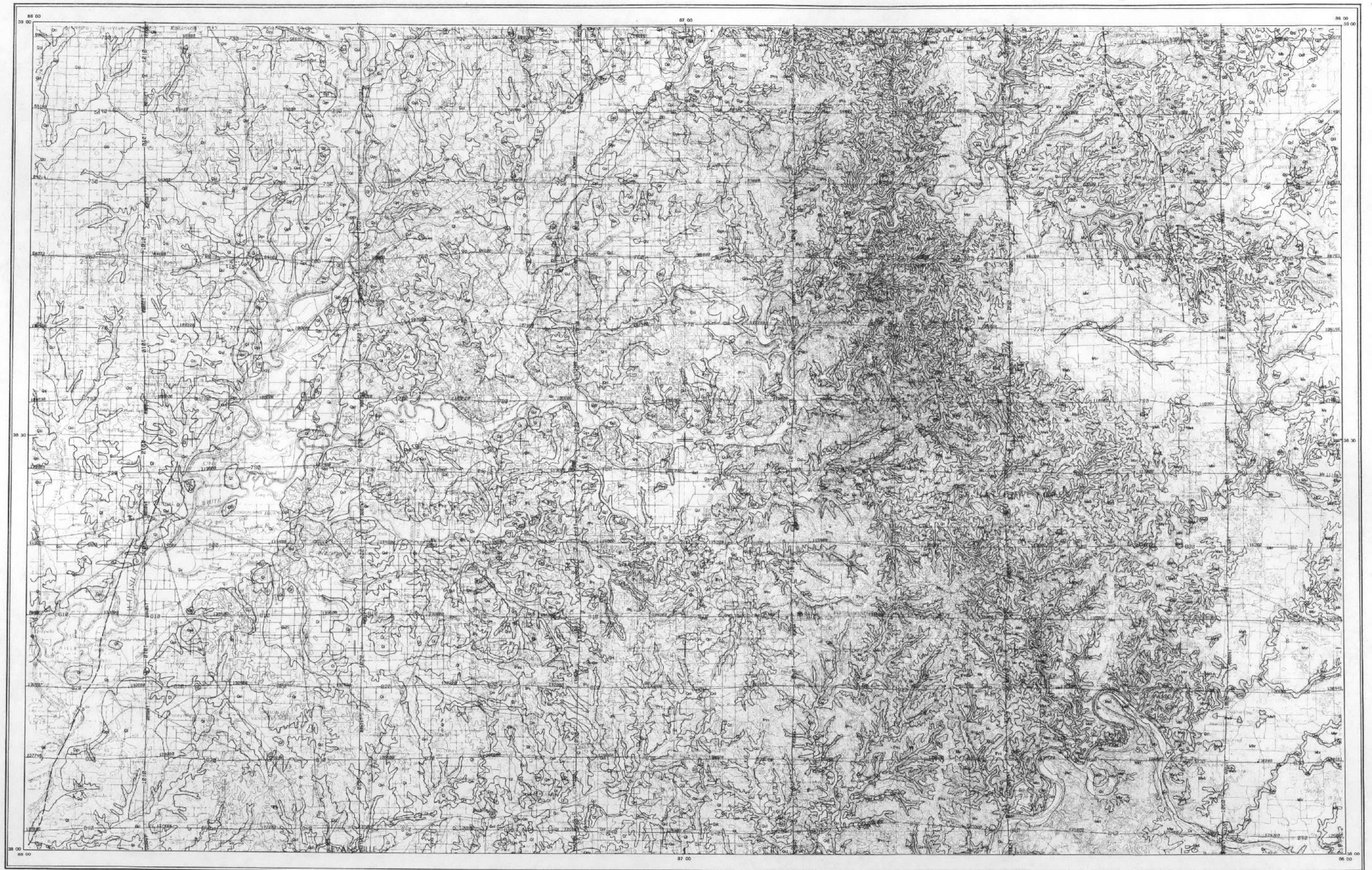
Nov. 21	200 line miles Cincinnati
22	480 " " Vincennes
23-25	Weather - nil production
26	480 line miles Vincennes
27-30	Weather - nil production
Dec. 1	448 line miles Cincinnati, Vincennes
2	Weather - nil production
3	528 line miles Vincennes, Indianapolis
4	368 " " Indianapolis
5	206 " " "
6	206 " " "
7	Weather - nil production
8	Equipment problem
9	Weather - nil production
10	" " " "
11	" " " "
12	300 line miles Indianapolis
13	Weather - nil production
14	434 line miles Indianapolis
15	Weather - nil production
16	" " " "
17	399 line miles Cincinnati

Total miles for the above period = 10,467 line miles.
Total miles for the included quadrangles:

Louisville	1716.0
Huntington	1716.0
Indianapolis	1693.8
Cincinnati	1693.8
Vincennes	1716.0
Toledo	Unfinished
Marion	Unfinished

APPENDIX C - Flight Path and Geologic Map

VINCENNES



SCALE 1:500,000



FLIGHT LINE SPACING 6.0 MILES
 FLIGHT ALTITUDE 400 FEET A.M.T.
 FLOWN AND COMPILED 1980

LOCATION DIAGRAM

38° 45'	38° 40'	38° 35'	38° 30'	38° 25'	38° 20'	38° 15'	38° 10'	38° 05'	38° 00'
86° 00'	86° 10'	86° 20'	86° 30'	86° 40'	86° 50'	87° 00'	87° 10'	87° 20'	87° 30'

SURVEY AND
 COMPILED BY:
EG&G GEOMETRICS

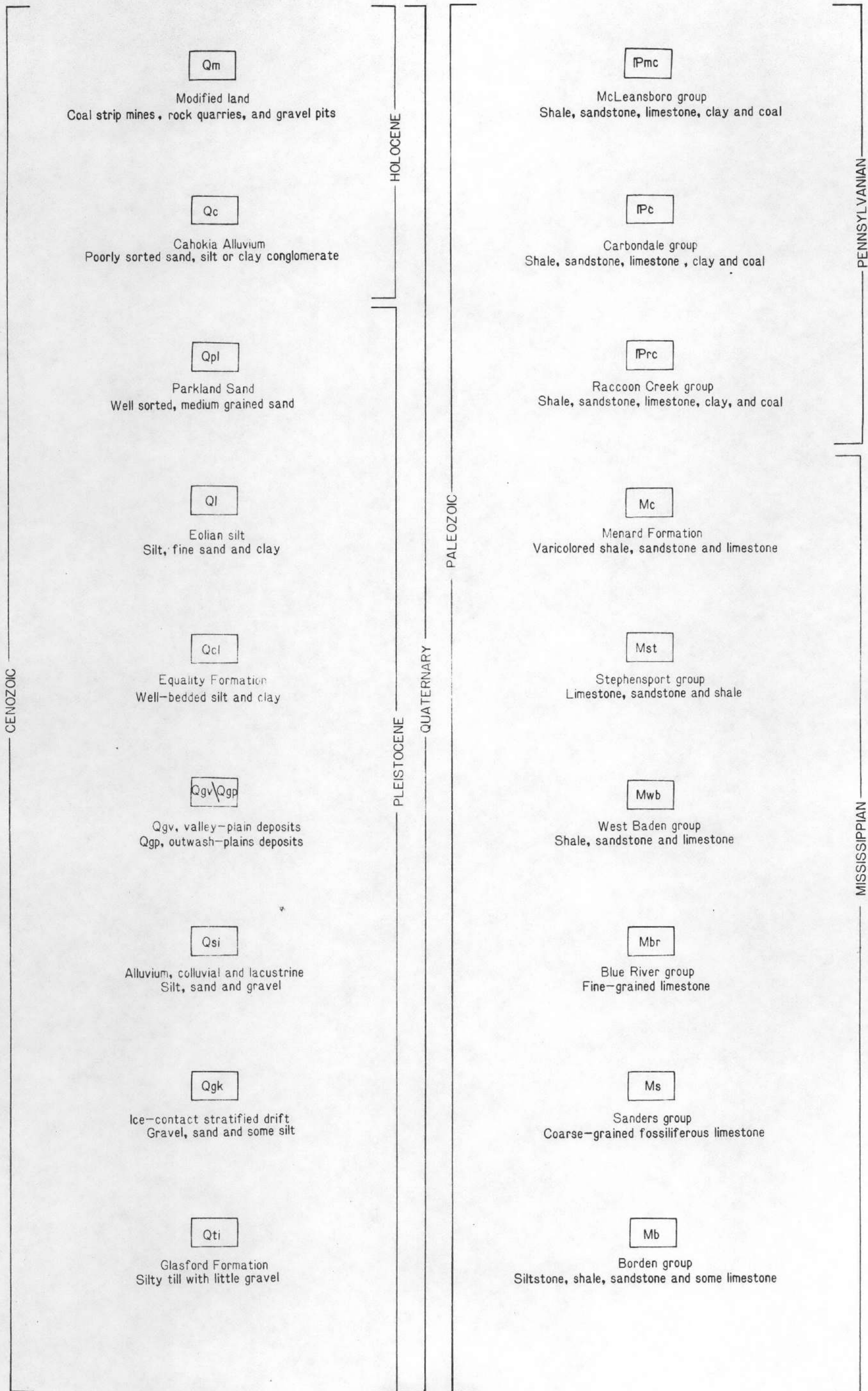
FLIGHT PATH RECOVERY

GREAT LAKES PROJECT

U. S. DEPARTMENT OF ENERGY




UNCONSOLIDATED DEPOSITS

BEDROCK UNITS



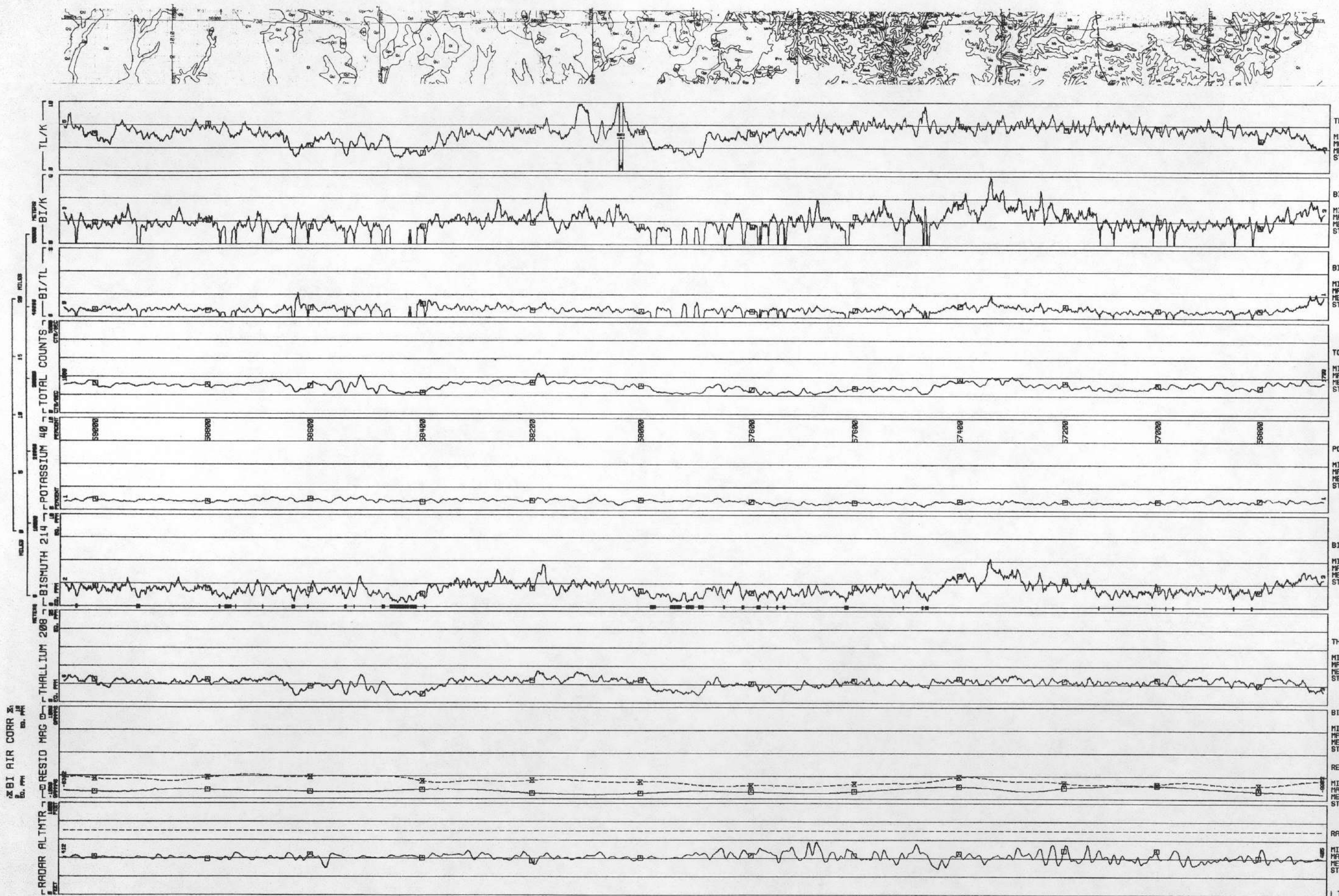
VINCENNES QUADRANGLE
GEOLOGIC MAP EXPLANATION
(Martel Laboratories, 1981)

GEOLOGIC SYMBOLS

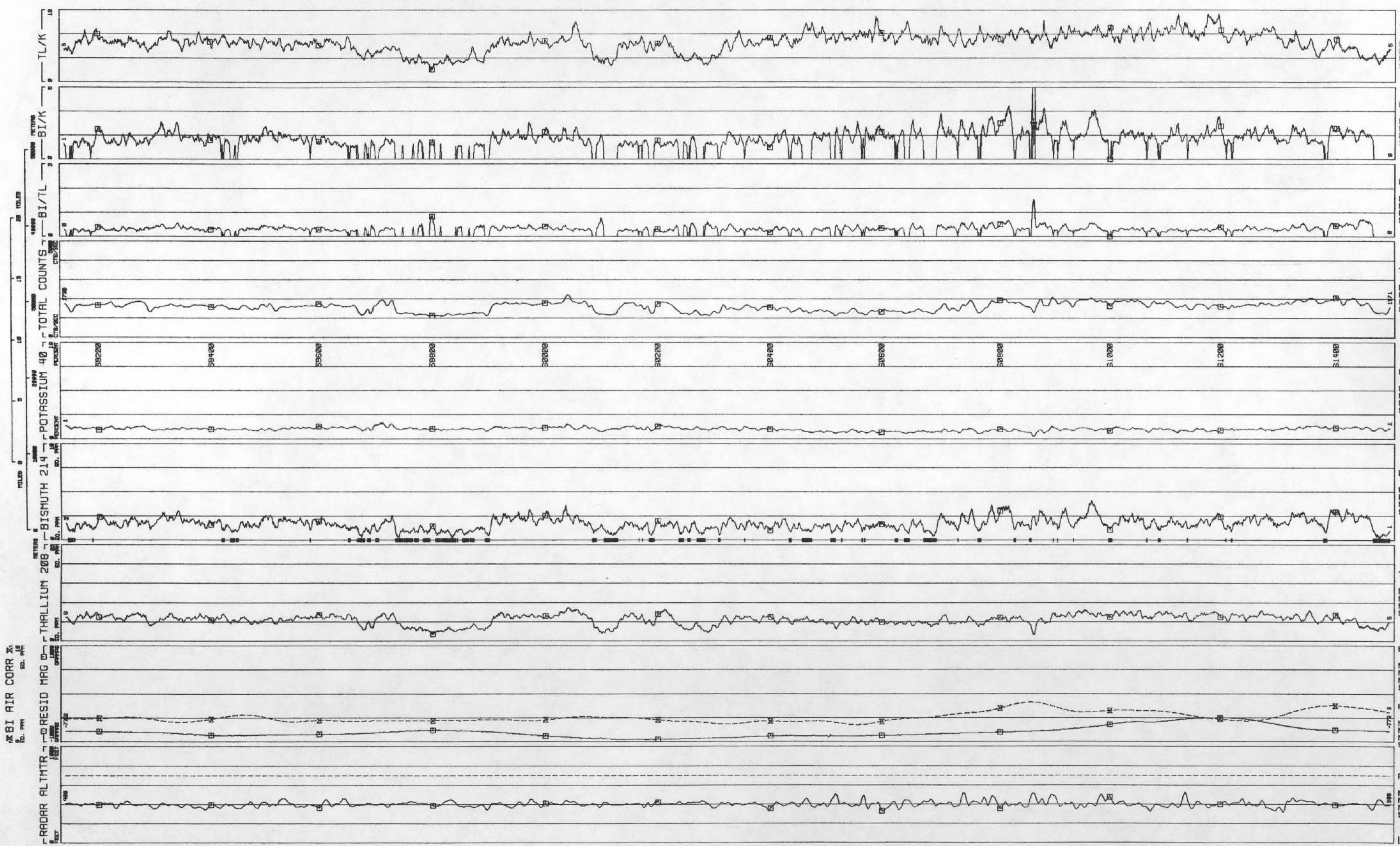
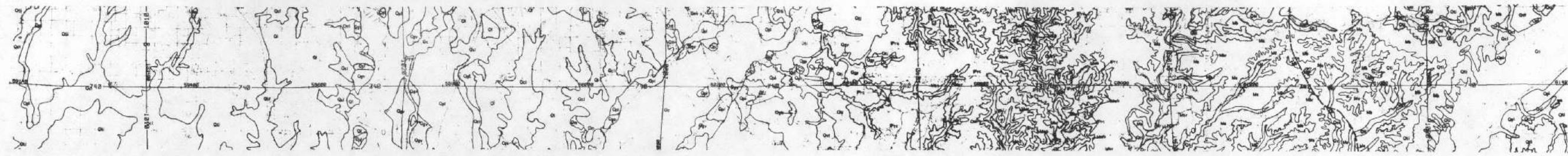
-  CONTACT
-  FAULTS, dashed where approximate
-  WATER BODIES

APPENDIX D - Profiles

LINE 730
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80327

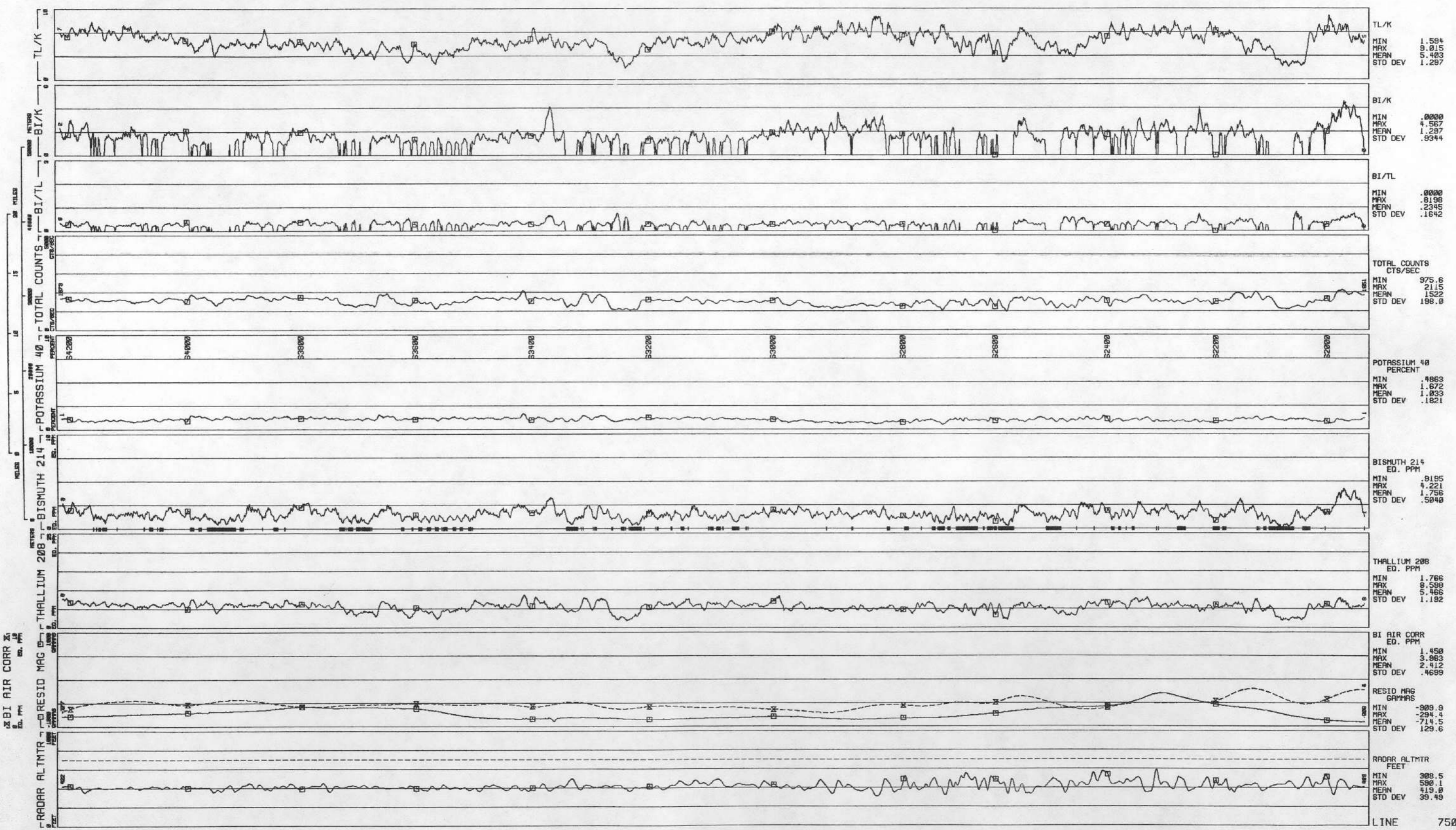
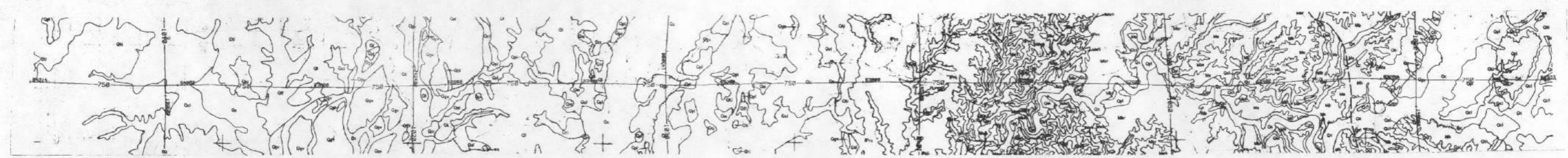


LINE 740
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80327

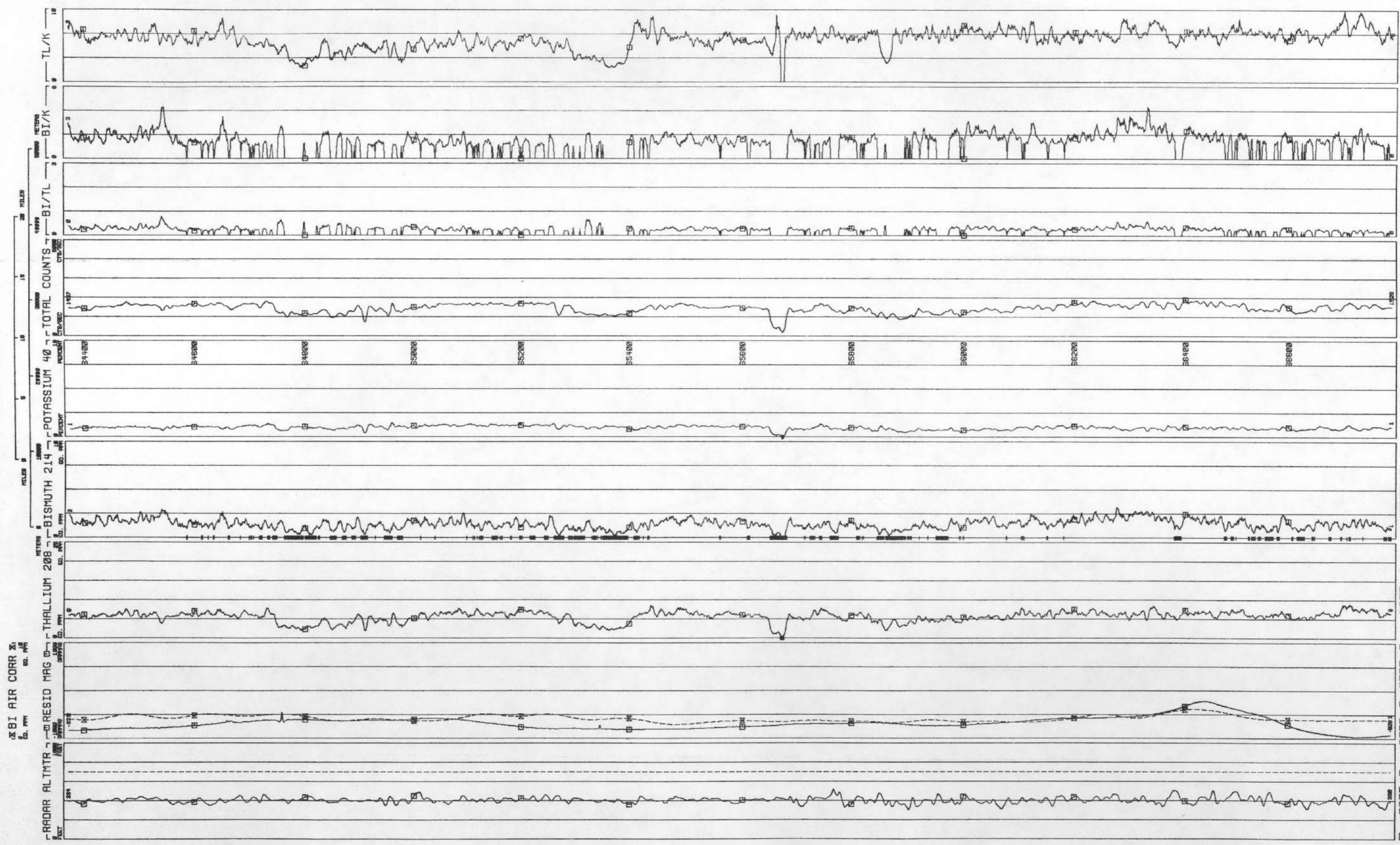
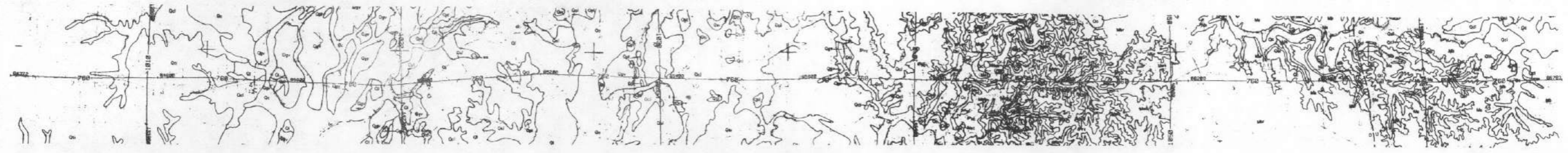


TL/K	MIN 1.675 MAX 9.382 MEAN 5.530 STD DEV 1.332
BI/K	MIN .0000 MAX 9.489 MEAN 1.559 STD DEV .9064
BI/TL	MIN .0000 MAX 1.532 MEAN .2787 STD DEV .1586
TOTAL COUNTS CTS/SEC	MIN 1186 MAX 2293 MEAN 1588 STD DEV 231.3
POTASSIUM 40 PERCENT	MIN .2668 MAX 1.657 MEAN 1.881 STD DEV .1777
BISMUTH 214 EQ. PPM	MIN 1.000 MAX 4.840 MEAN 1.881 STD DEV .5148
THALLIUM 208 EQ. PPM	MIN 1.638 MAX 8.686 MEAN 5.574 STD DEV 1.392
BI AIR CORR EQ. PPM	MIN 1.768 MAX 4.195 MEAN 2.571 STD DEV .5421
RESID MAG GAMMAS	MIN -855.8 MAX -499.8 MEAN -796.4 STD DEV 112.7
RADAR ALTMTR FEET	MIN 319.2 MAX 522.7 MEAN 483.8 STD DEV 28.17

LINE 750
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80327

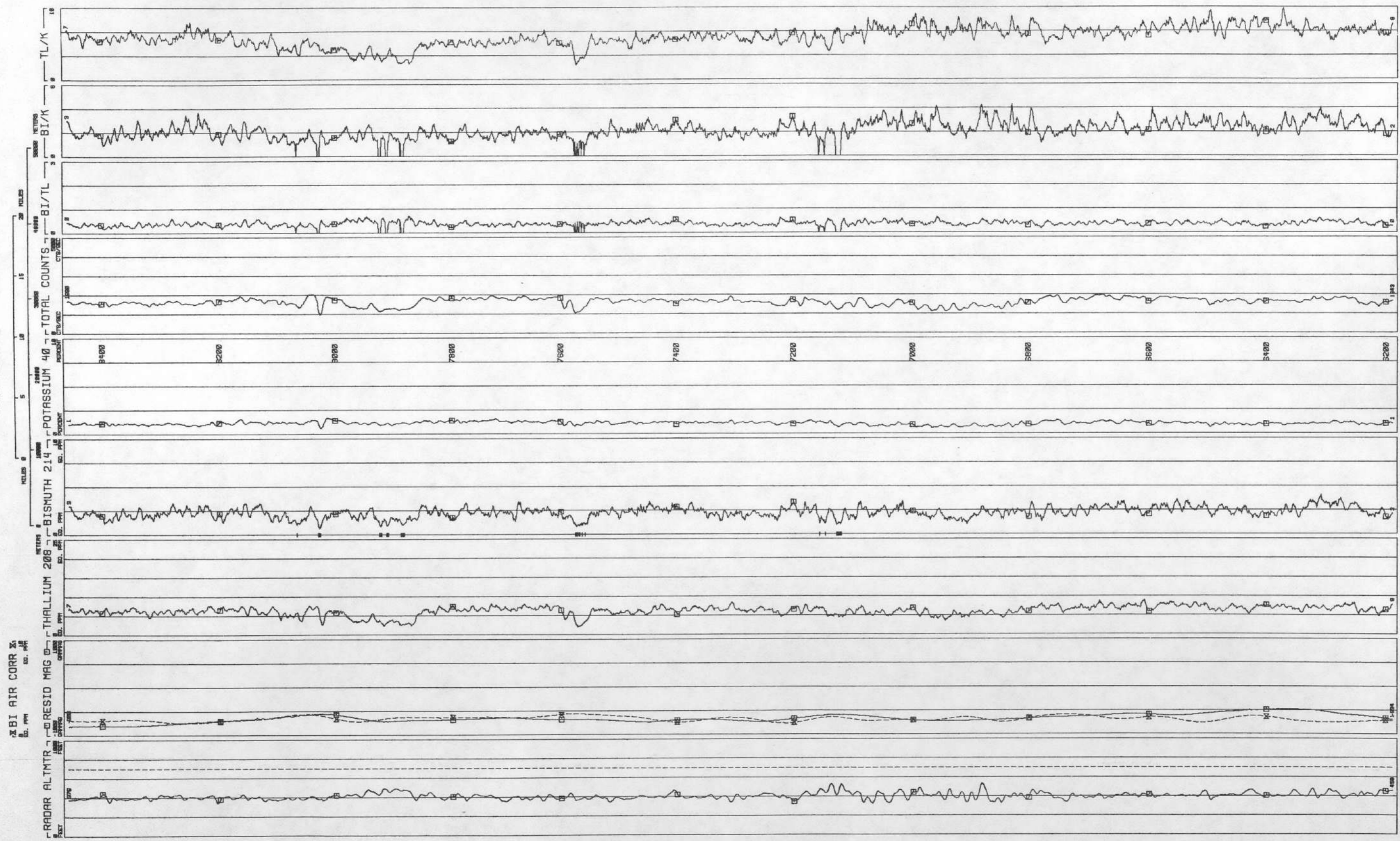


LINE 760
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 8032Z



TL/K	MIN .0000 MAX 9.951 MEAN 5.818 STD DEV 1.379
BI/K	MIN .0000 MAX 4.328 MEAN 1.276 STD DEV .8689
BI/TL	MIN .0000 MAX .7828 MEAN .2083 STD DEV .1402
TOTAL COUNTS CTS/SEC	MIN 202.3 MAX 1911 MEAN 1448 STD DEV 233.4
POTASSIUM 40 PERCENT	MIN .0863 MAX 1.440 MEAN .9580 STD DEV .1888
BISMUTH 214 EQ. PPM	MIN .7865 MAX 3.175 MEAN 1.622 STD DEV .3918
THALLIUM 208 EQ. PPM	MIN .9201 MAX 8.897 MEAN 5.613 STD DEV 1.362
BI AIR CORR EQ. PPM	MIN 1.459 MAX 3.864 MEAN 2.887 STD DEV .3348
RESID MAG GAMMAS	MIN -970.8 MAX -221.9 MEAN -680.8 STD DEV 138.5
RADAR ALTMTR FEET	MIN 304.2 MAX 513.7 MEAN 404.0 STD DEV 38.72

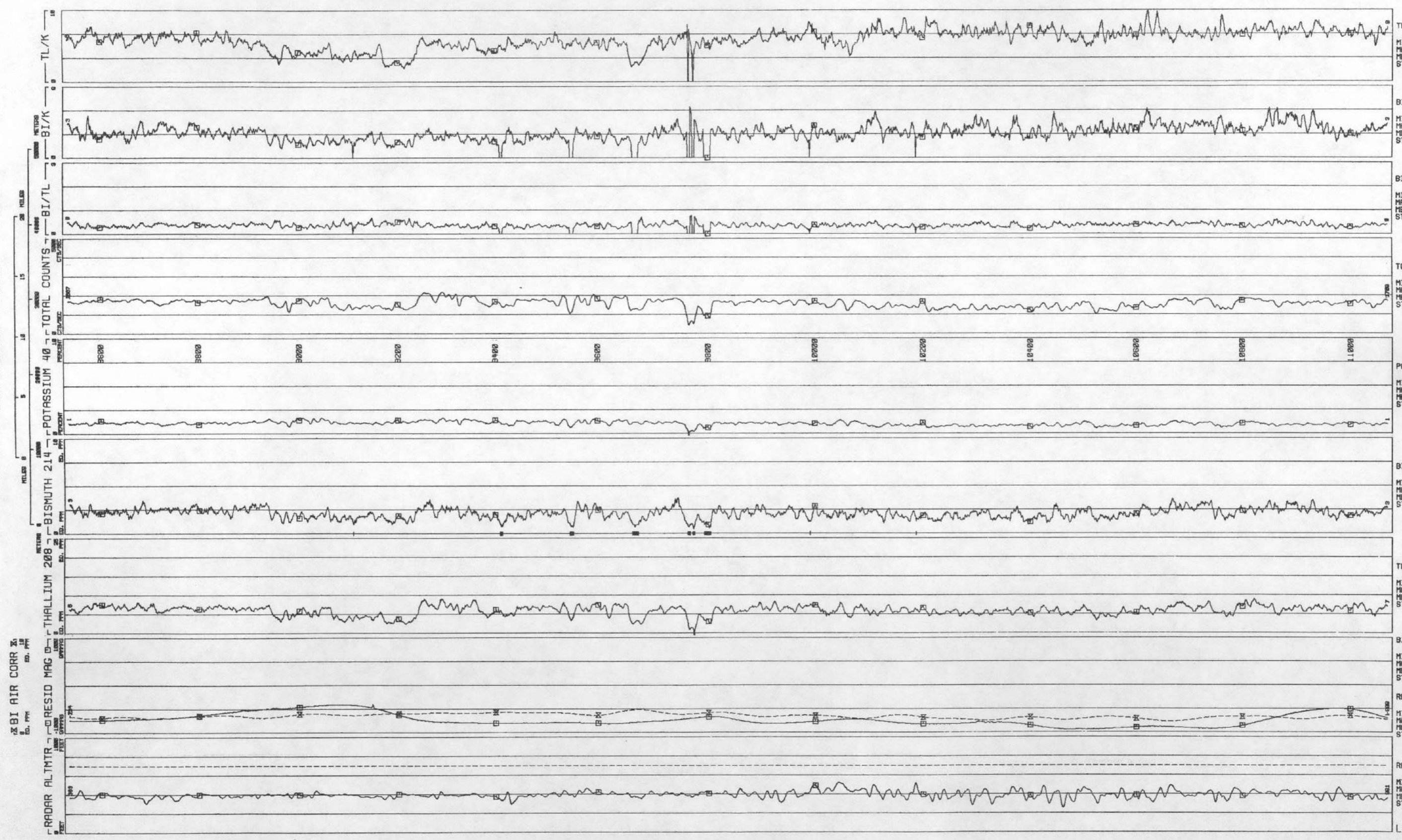
LINE 770
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80331



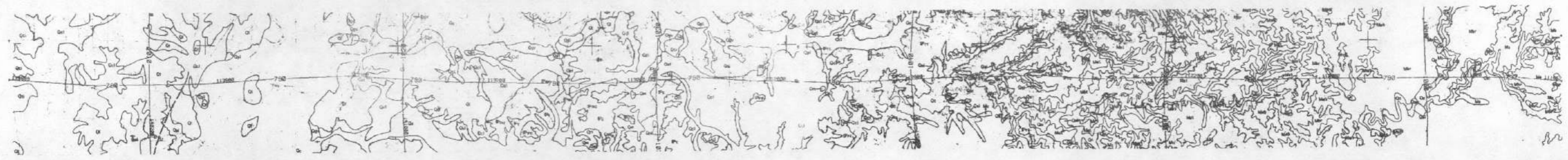
TL/K	MIN 1.993 MAX 9.779 MEAN 5.808 STD DEV 1.238
BI/K	MIN .0000 MAX 4.265 MEAN 2.144 STD DEV .6541
BI/TL	MIN .0000 MAX .7001 MEAN .3656 STD DEV .0971
TOTAL COUNTS CTS/SEC	MIN 964.3 MAX 2034 MEAN 1615 STD DEV 186.1
POTASSIUM 40 PERCENT	MIN .5269 MAX 1.720 MEAN 1.078 STD DEV .1673
BISMUTH 214 ED. PPM	MIN .9781 MAX 4.054 MEAN 2.276 STD DEV .5020
THALLIUM 208 ED. PPM	MIN 1.974 MAX 8.901 MEAN 6.185 STD DEV 1.136
BI AIR CORR ED. PPM	MIN 1.171 MAX 2.201 MEAN 1.643 STD DEV .2507
RESID MAG GAMMAS	MIN -806.9 MAX -477.1 MEAN -637.7 STD DEV 73.73
RADAR ALTMTR FEET	MIN 323.6 MAX 530.0 MEAN 405.7 STD DEV 30.60



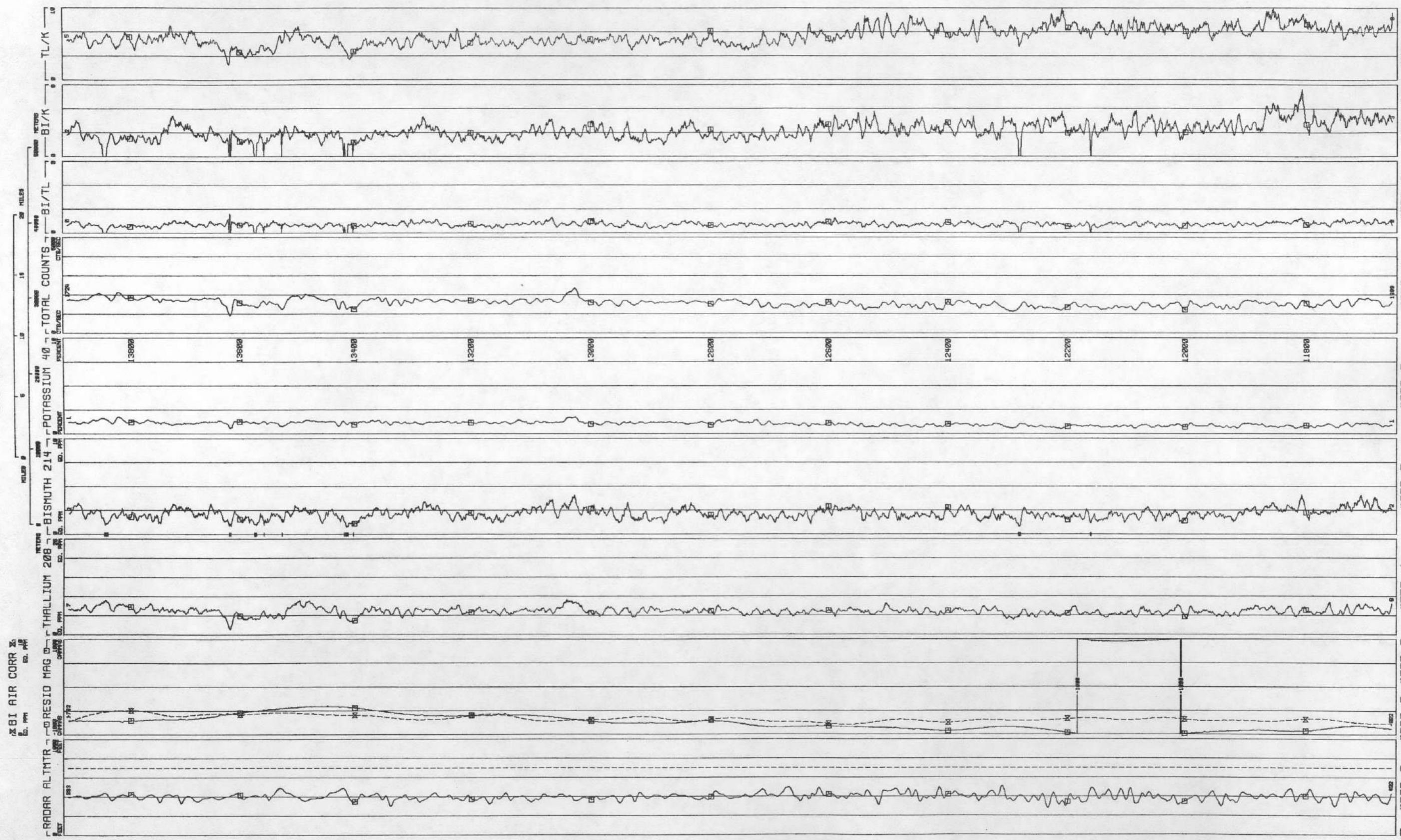
LINE 780
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80331



TL/K	MIN .0000
	MAX 9.864
	MEAN 5.866
	STD DEV 1.319
BI/K	MIN .0000
	MAX 4.270
	MEAN 2.060
	STD DEV .6384
BI/TL	MIN .0000
	MAX .7532
	MEAN .3544
	STD DEV .0945
TOTAL COUNTS CTS/SEC	MIN 429.7
	MAX 2179
	MEAN 1568
	STD DEV 226.0
POTASSIUM 40 PERCENT	MIN .1531
	MAX 1.661
	MEAN 1.036
	STD DEV .2261
BISMUTH 214 ED. PPM	MIN .0358
	MAX 3.716
	MEAN 2.120
	STD DEV .5055
THALLIUM 208 ED. PPM	MIN .0183
	MAX 9.058
	MEAN 5.921
	STD DEV 1.265
BI AIR CORR ED. PPM	MIN 1.146
	MAX 2.428
	MEAN 1.736
	STD DEV .2651
RESID MAG GAMMAS	MIN -954.3
	MAX -403.0
	MEAN -728.7
	STD DEV 138.8
RADAR ALTMTR FEET	MIN 256.0
	MAX 520.4
	MEAN 393.5
	STD DEV 34.19

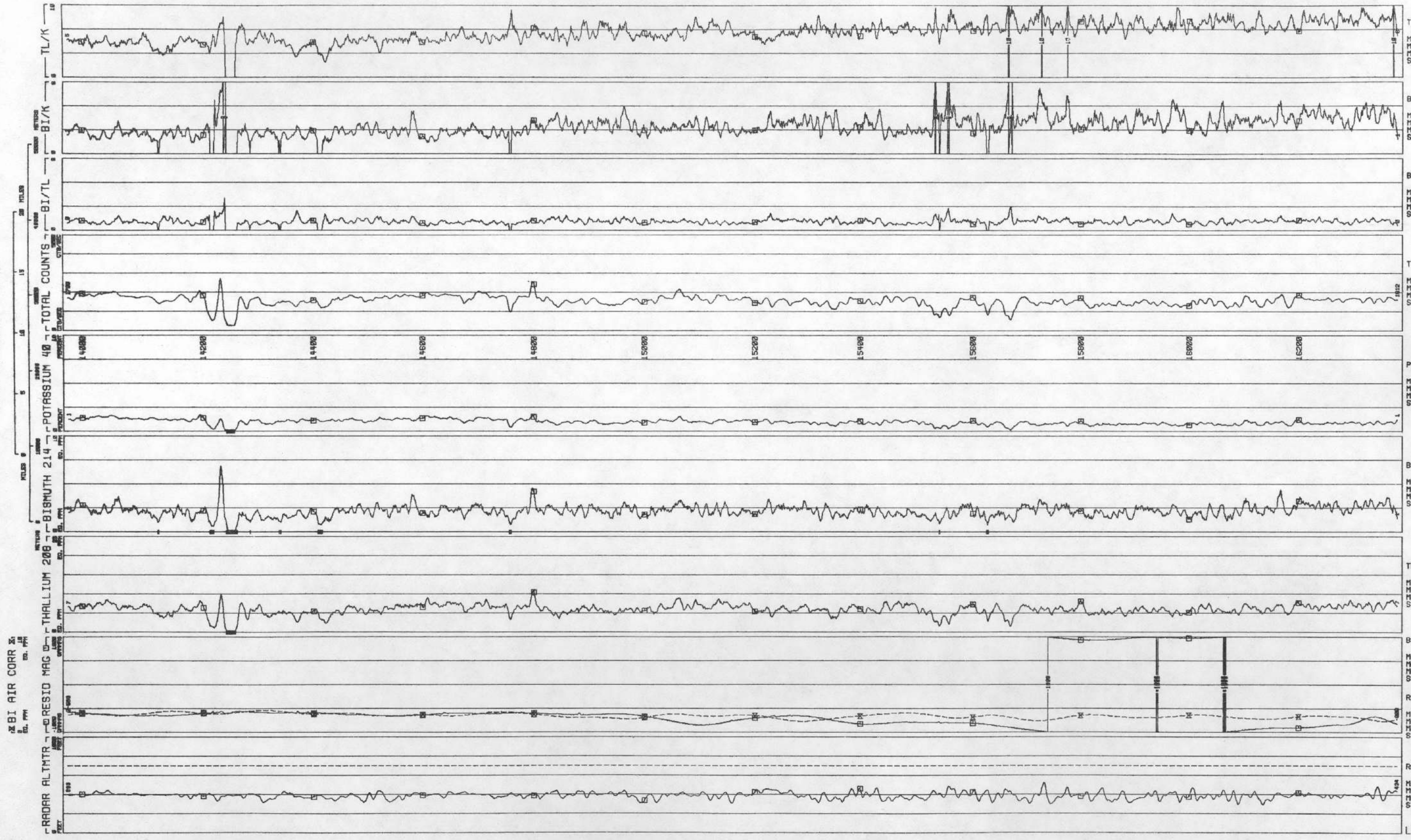
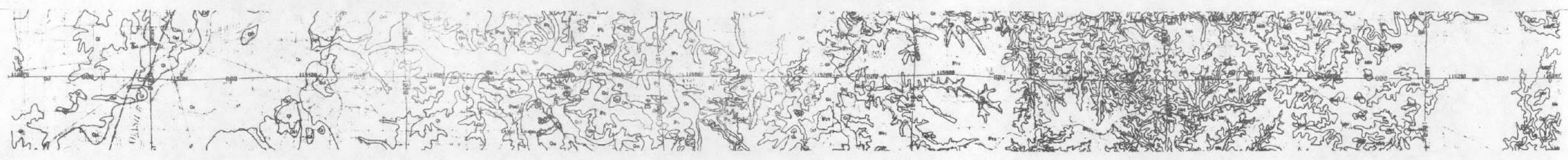


LINE 790
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80331



TL/K	MIN 2.148 MAX 9.997 MEAN 6.097 STD DEV 1.203
BI/K	MIN .0000 MAX 5.620 MEAN 2.159 STD DEV .7094
BI/TL	MIN .0000 MAX .7860 MEAN .3528 STD DEV .0896
TOTAL COUNTS CTS/SEC	MIN 888.7 MAX 2358 MEAN 1577 STD DEV 191.6
POTASSIUM 40 PERCENT	MIN .5073 MAX 1.767 MEAN 1.023 STD DEV .2175
BISMUTH 214 EQ. PPM	MIN .9514 MAX 4.084 MEAN 2.146 STD DEV .5179
THALLIUM 208 EQ. PPM	MIN 1.374 MAX 8.187 MEAN 6.052 STD DEV .9463
BI AIR CORR EQ. PPM	MIN 1.047 MAX 2.575 MEAN 1.678 STD DEV .3413
RESID MAG GAMMAS	MIN -1053 MAX -484.8 MEAN -750.6 STD DEV 171.4
RADAR ALTMTR FEET	MIN 279.8 MAX 510.8 MEAN 398.5 STD DEV 34.91

LINE 800
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80331



TL/K
MIN .0000
MAX 10.39
MEAN 6.290
STD DEV 1.434

BI/K
MIN .0000
MAX 9.225
MEAN 2.329
STD DEV .9086

BI/TL
MIN .0000
MAX 1.342
MEAN .3658
STD DEV .1130

TOTAL COUNTS
CTS/SEC
MIN 251.2
MAX 2784
MEAN 1551
STD DEV 267.3

POTASSIUM 40
PERCENT
MIN .1047
MAX 1.723
MEAN .9728
STD DEV .2559

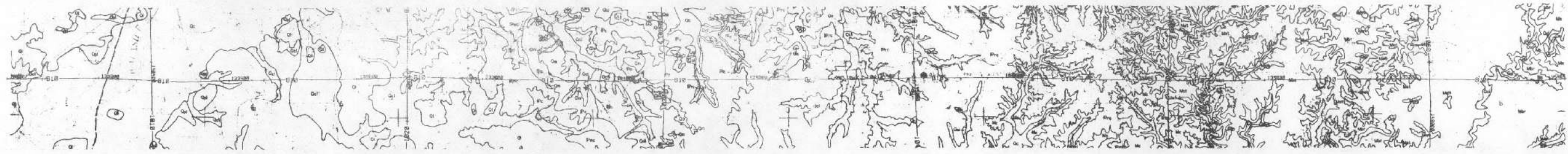
BISMUTH 214
EQ. PPH
MIN 1.029
MAX 6.871
MEAN 2.197
STD DEV .5661

THALLIUM 208
EQ. PPH
MIN 1.004
MAX 10.58
MEAN 5.965
STD DEV 1.241

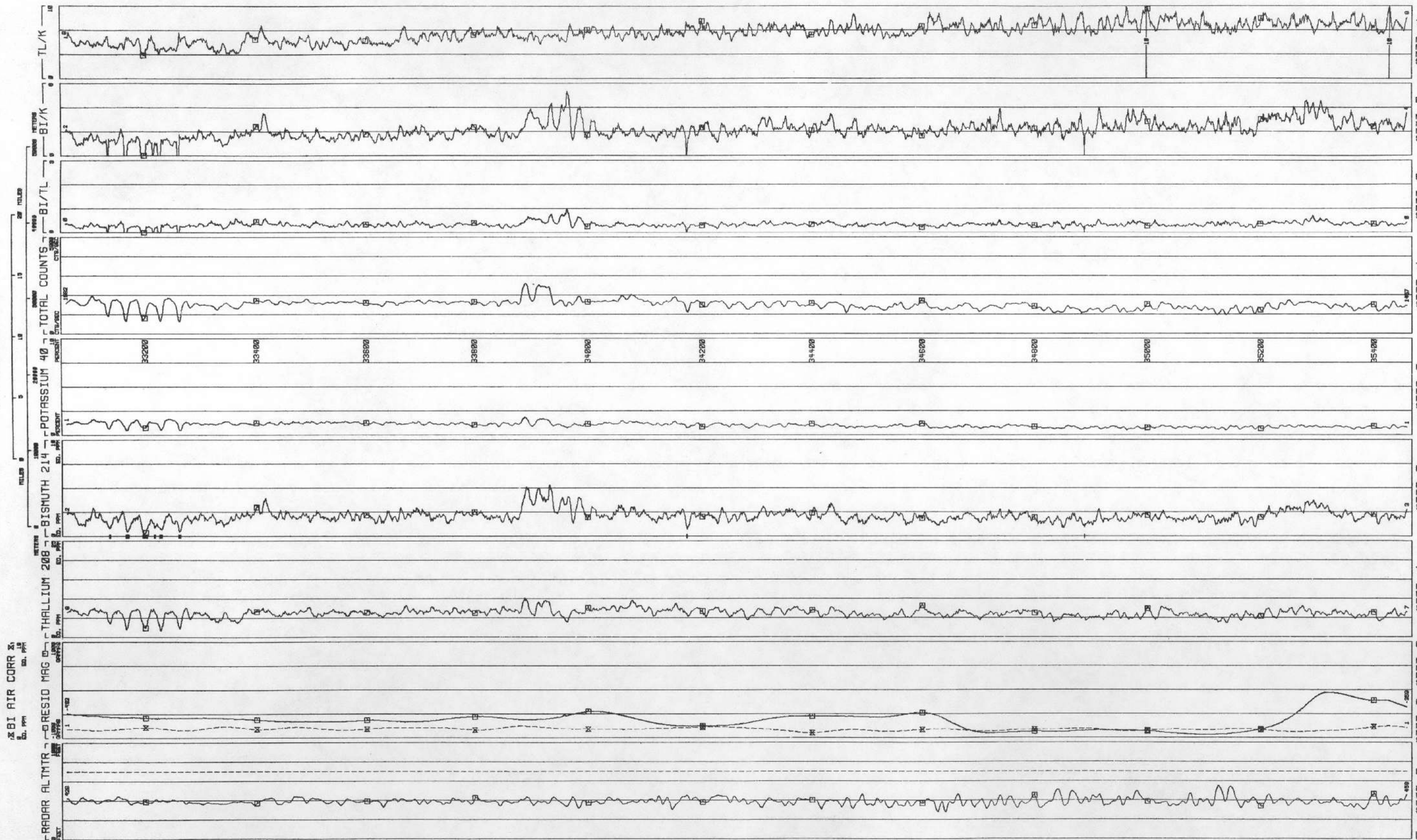
BI AIR CORR
EQ. PPH
MIN 1.152
MAX 2.300
MEAN 1.731
STD DEV .2516

RESID MAG
GAMMAS
MIN -1075
MAX -552.1
MEAN -756.7
STD DEV 155.3

RADAR ALTMTR
FEET
MIN 293.4
MAX 520.3
MEAN 388.1
STD DEV 32.15



LINE 810
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80336



TL/K
 MIN 3.140
 MAX 10.29
 MEAN 6.353
 STD DEV 1.225

BI/K
 MIN .0000
 MAX 5.329
 MEAN 2.129
 STD DEV .7063

BI/TL
 MIN .0000
 MAX .9956
 MEAN .3345
 STD DEV .0960

TOTAL COUNTS
 CTS/SEC
 MIN 634.7
 MAX 2609
 MEAN 1488
 STD DEV 231.1

POTASSIUM 40
 PERCENT
 MIN .4853
 MAX 1.848
 MEAN 1.006
 STD DEV .2418

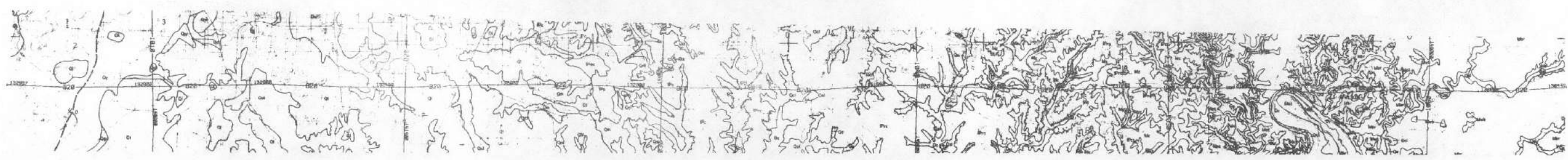
BISMUTH 214
 EQ. PPM
 MIN .0601
 MAX 5.300
 MEAN 2.098
 STD DEV .5926

THALLIUM 208
 EQ. PPM
 MIN 1.775
 MAX 10.07
 MEAN 6.181
 STD DEV 1.025

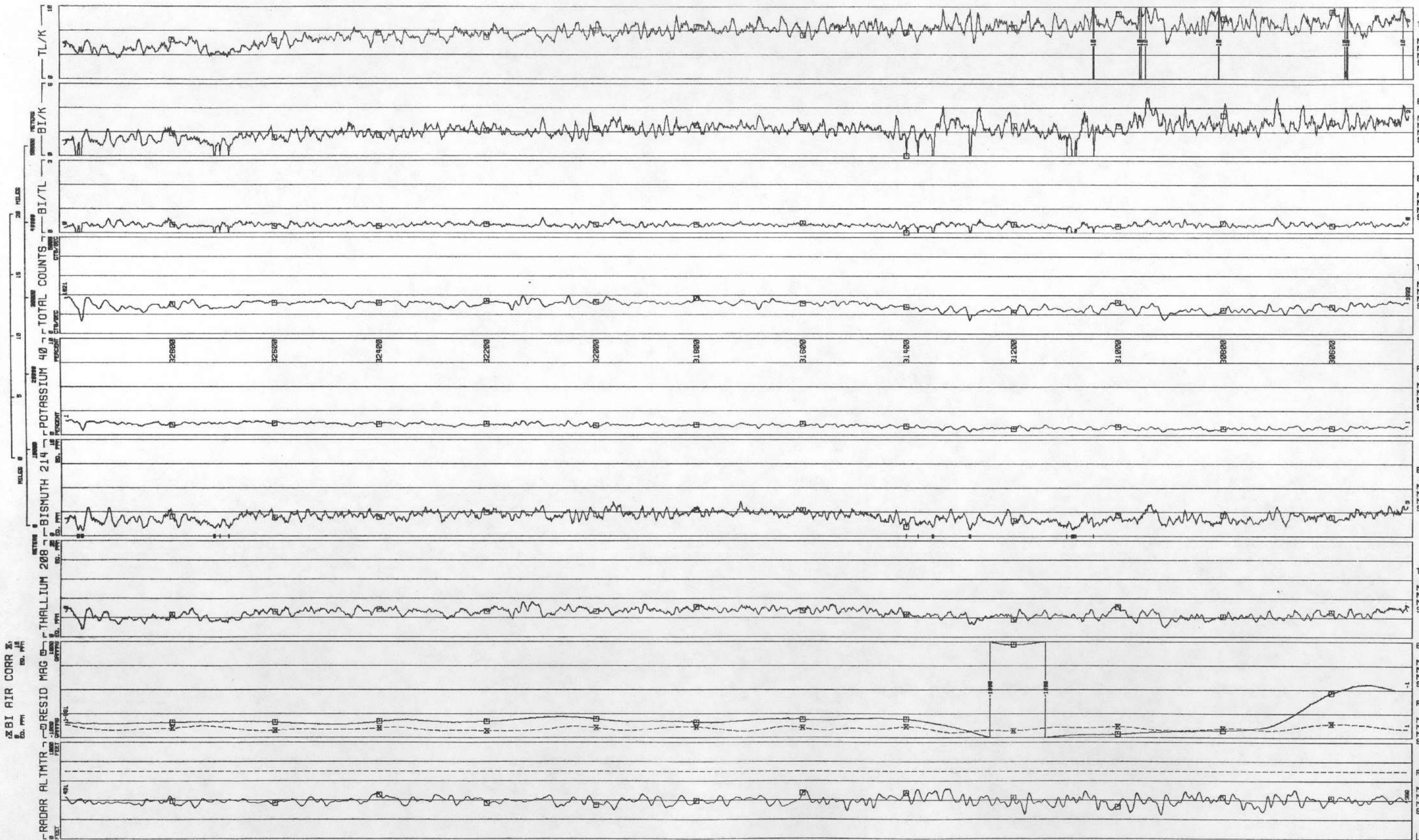
BI AIR CORR
 EQ. PPM
 MIN .4889
 MAX 1.240
 MEAN .8950
 STD DEV .1586

RESID MAG
 GAMMAS
 MIN -942.4
 MAX -56.94
 MEAN -632.9
 STD DEV 186.5

RADAR ALTMTR
 FEET
 MIN 281.4
 MAX 548.0
 MEAN 359.3
 STD DEV 33.84



LINE 820
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80336



TL/K
 MIN 2.884
 MAX 11.15
 MEAN 6.585
 STD DEV 1.423

BI/K
 MIN .0000
 MAX 4.936
 MEAN 2.157
 STD DEV .6795

BI/TL
 MIN .0000
 MAX .6867
 MEAN .3281
 STD DEV .0806

TOTAL COUNTS
 CTS/SEC
 MIN 644.1
 MAX 1966
 MEAN 1468
 STD DEV 208.4

POTASSIUM 40
 PERCENT
 MIN .3591
 MAX 1.571
 MEAN .8664
 STD DEV .2299

BISMUTH 214
 EQ. PPM
 MIN .8187
 MAX 3.618
 MEAN 2.027
 STD DEV .4871

THALLIUM 208
 EQ. PPM
 MIN 1.876
 MAX 9.165
 MEAN 6.123
 STD DEV 1.119

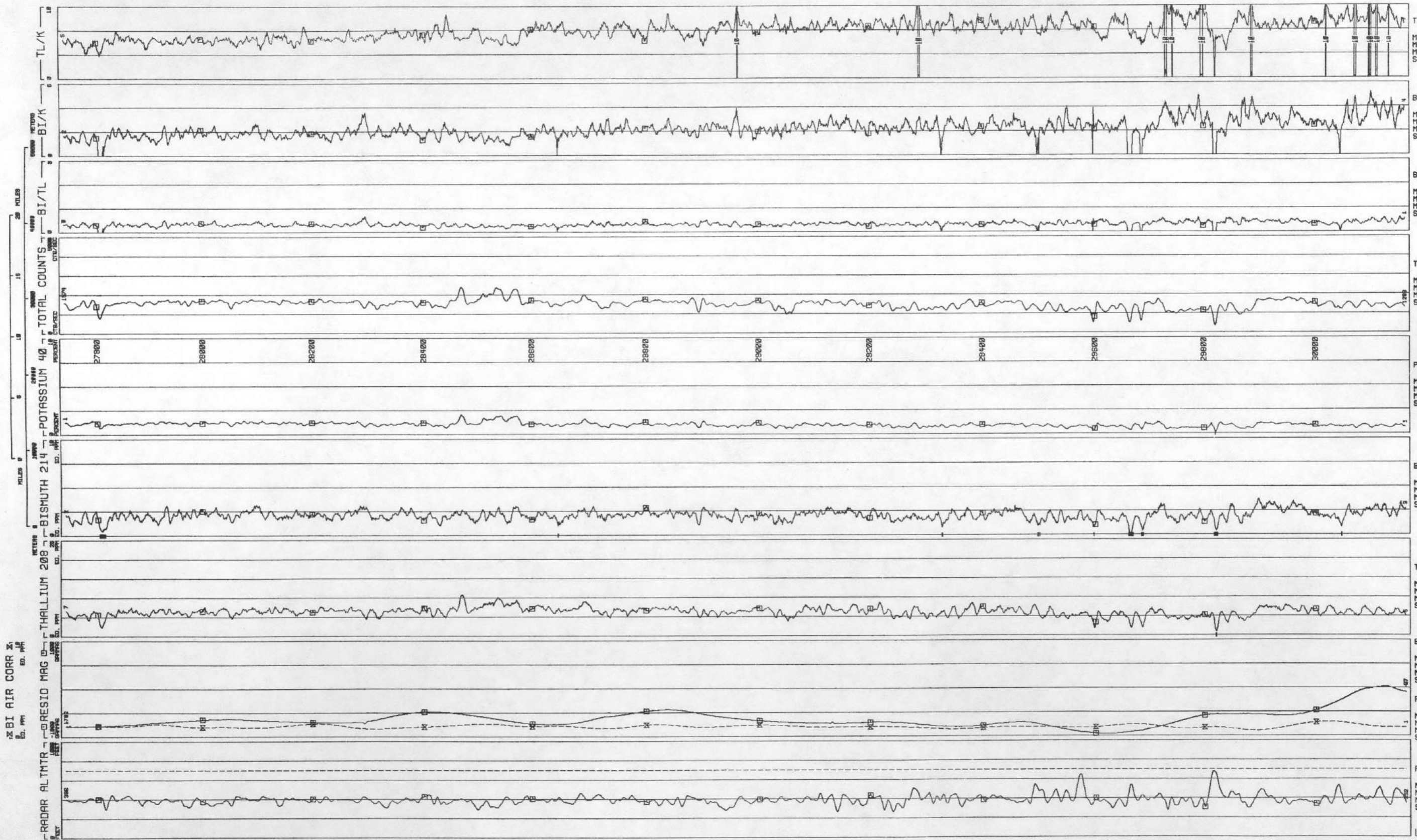
BI AIR CORR
 EQ. PPM
 MIN .5089
 MAX 1.452
 MEAN .9316
 STD DEV .1900

RESID MAG
 GAMMAS
 MIN -1065
 MAX 109.5
 MEAN 655.1
 STD DEV 228.8

RADAR ALTMTR
 FEET
 MIN 248.5
 MAX 516.2
 MEAN 393.9
 STD DEV 38.81



LINE 830
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80336



TL/K
 MIN .0000
 MAX 11.01
 MEAN 6.655
 STD DEV 1.249

BI/K
 MIN .0000
 MAX 5.208
 MEAN 2.185
 STD DEV .7180

BI/TL
 MIN .0000
 MAX .6501
 MEAN .3283
 STD DEV .0845

TOTAL COUNTS
 CTS/SEC
 MIN 340.4
 MAX 2410
 MEAN 1487
 STD DEV 244.2

POTASSIUM 40
 PERCENT
 MIN .1559
 MAX 2.032
 MEAN .8693
 STD DEV .2585

BISMUTH 214
 EQ. PPM
 MIN .7594
 MAX 3.636
 MEAN 2.070
 STD DEV .4558

THALLIUM 208
 EQ. PPM
 MIN 1.234
 MAX 10.75
 MEAN 6.236
 STD DEV 1.144

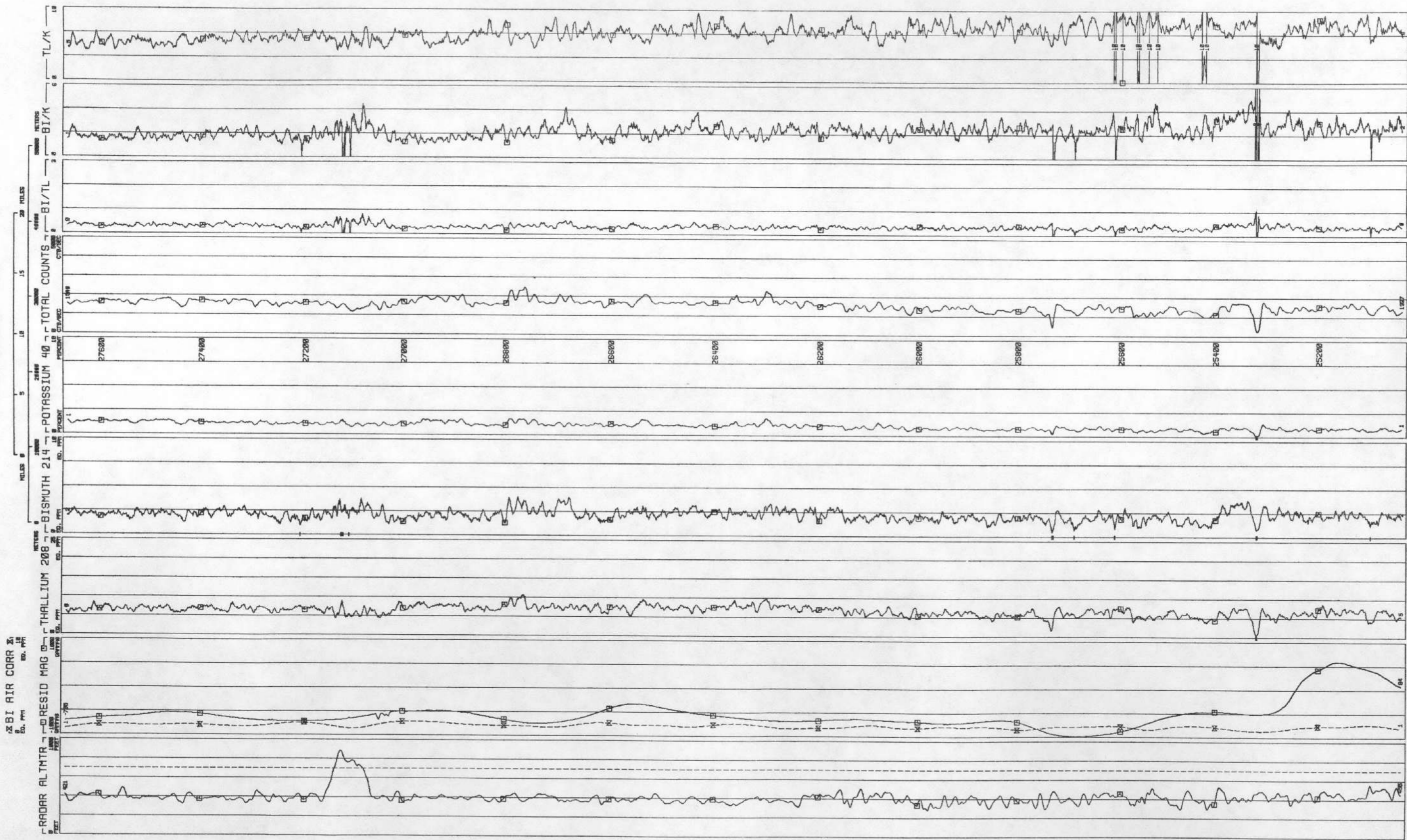
BI AIR CORR
 EQ. PPM
 MIN .5186
 MAX 1.465
 MEAN 1.015
 STD DEV .1742

RESID MAG
 GAMMAS
 MIN -964.8
 MAX 22.63
 MEAN -841.5
 STD DEV 177.8

RADAR ALTMTR
 FEET
 MIN 266.0
 MAX 675.7
 MEAN 390.7
 STD DEV 47.59



LINE 840
 VINCENTES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80336



TL/K
 MIN .0000
 MAX 13.87
 MEAN 6.847
 STD DEV 1.266

BI/K
 MIN .0000
 MAX 9.733
 MEAN 2.245
 STD DEV .6853

BI/TL
 MIN .0000
 MAX 1.068
 MEAN .3298
 STD DEV .0888

TOTAL COUNTS
 CTS/SEC
 MIN 241.9
 MAX 2461
 MEAN 1558
 STD DEV 238.7

POTASSIUM 40
 PERCENT
 MIN .1203
 MAX 1.805
 MEAN .8957
 STD DEV .2454

BISMUTH 214
 EQ. PPM
 MIN .0748
 MAX 3.986
 MEAN 2.158
 STD DEV .5102

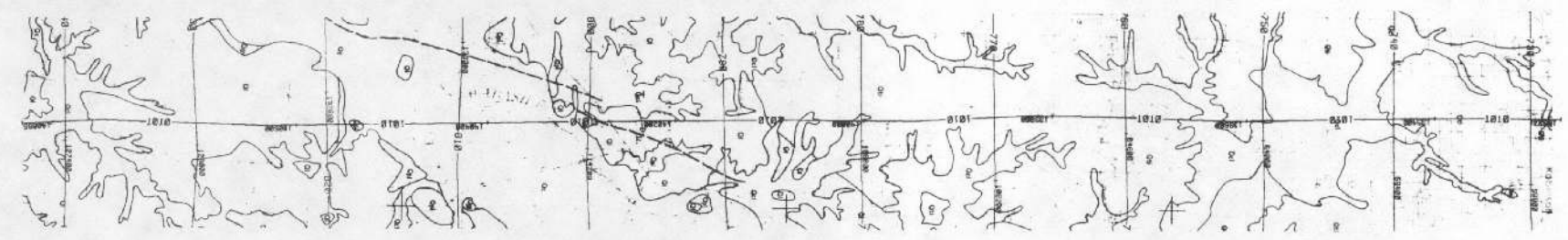
THALLIUM 208
 EQ. PPM
 MIN .0702
 MAX 10.65
 MEAN 6.604
 STD DEV 1.115

BI AIR CORR
 EQ. PPM
 MIN .0712
 MAX 1.463
 MEAN 1.057
 STD DEV .1698

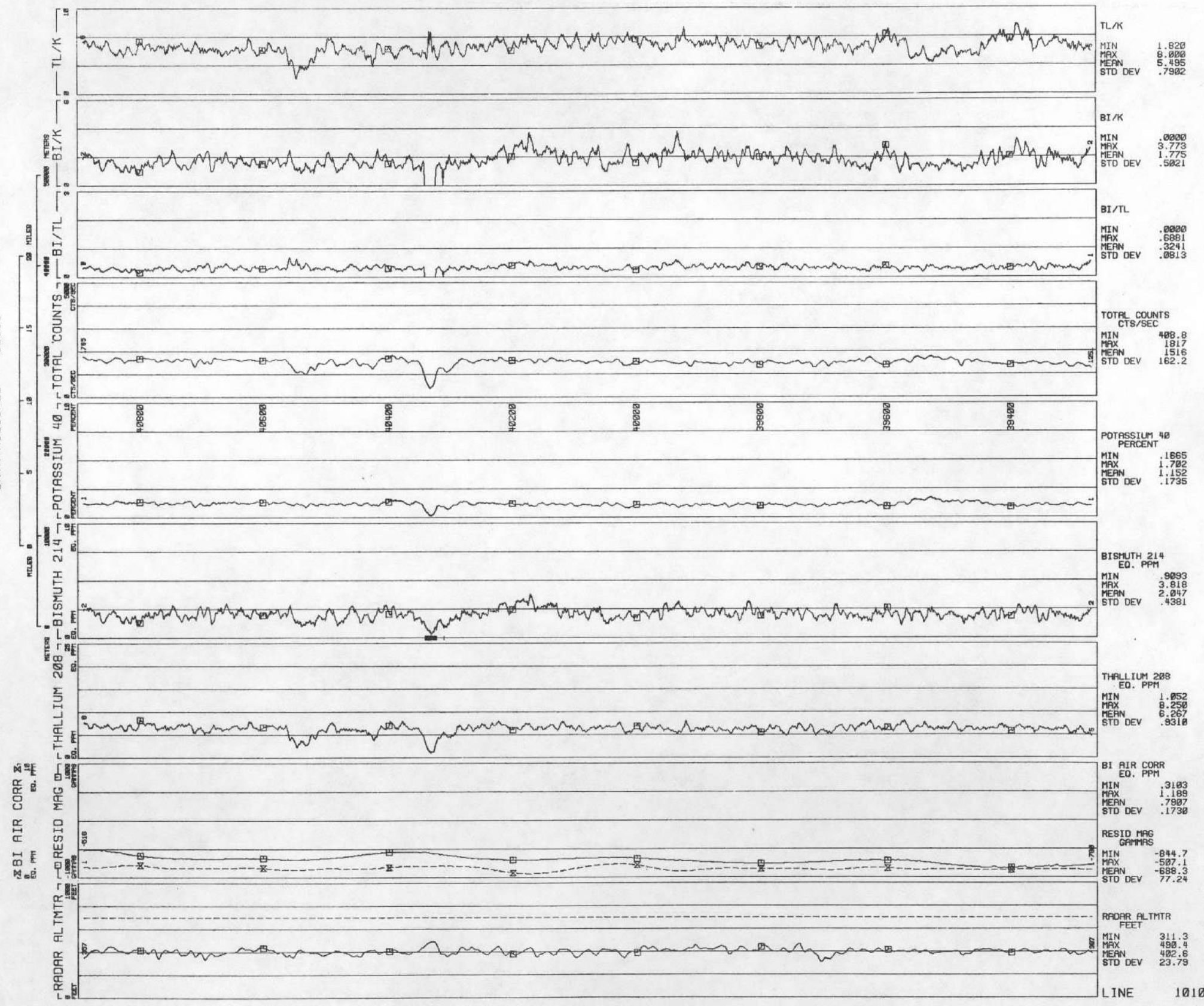
RESID MAG
 GAMMAS
 MIN -990.8
 MAX 594.5
 MEAN -543.8
 STD DEV 307.2

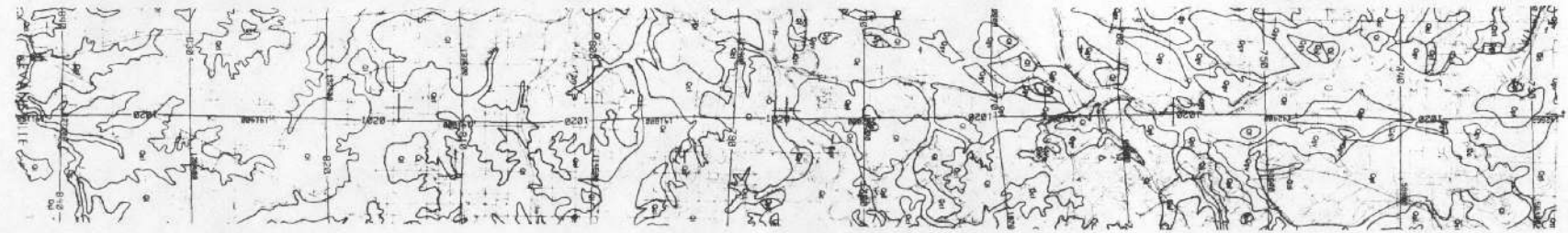
RADAR ALTMTR
 FEET
 MIN 284.1
 MAX 884.3
 MEAN 409.9
 STD DEV 73.58

LINE 840

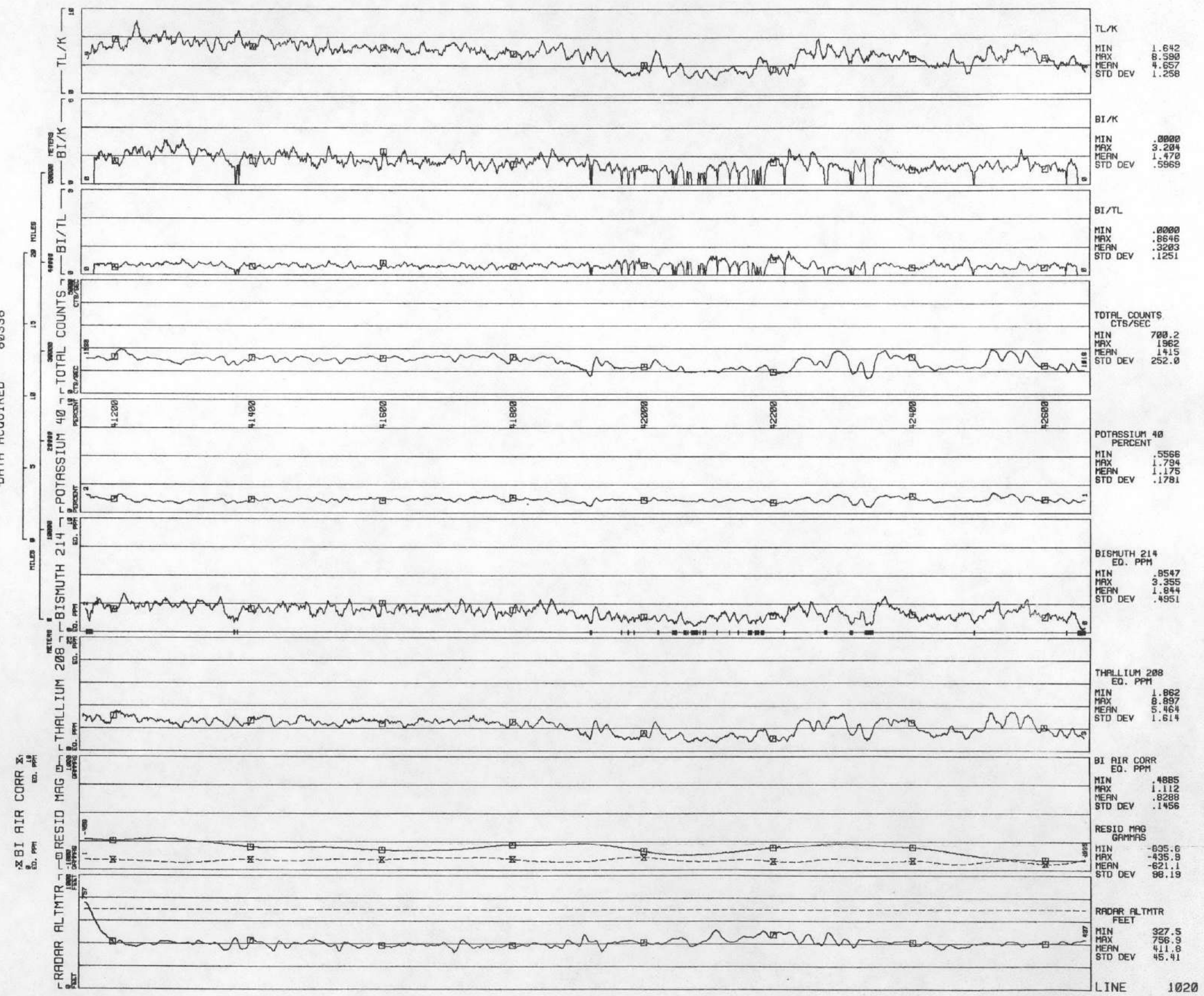


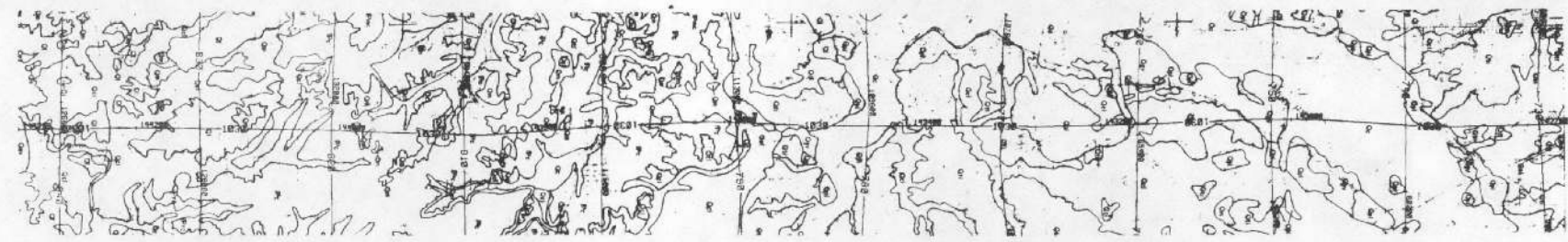
LINE 1010
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80338



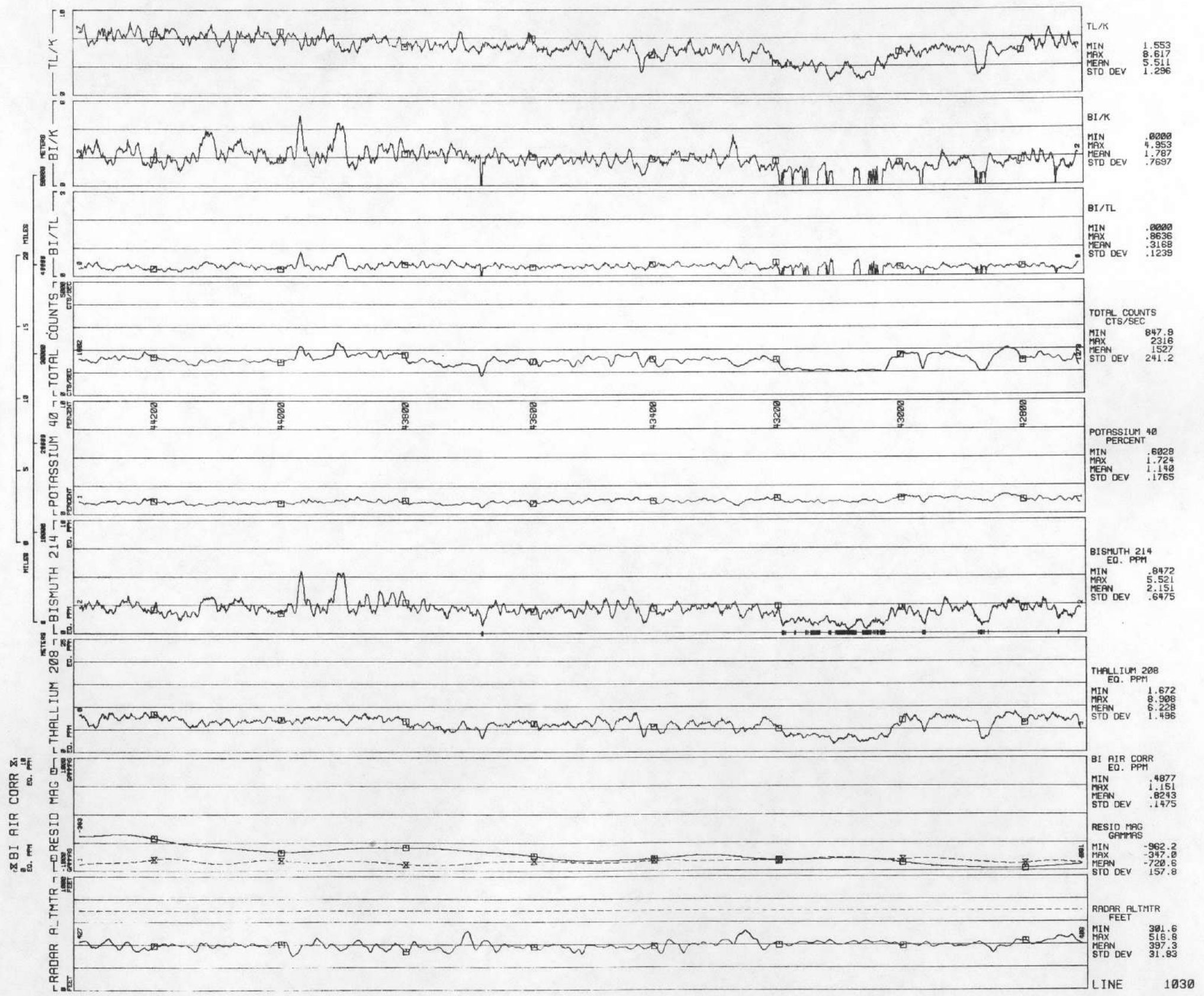


LINE 1020
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80338



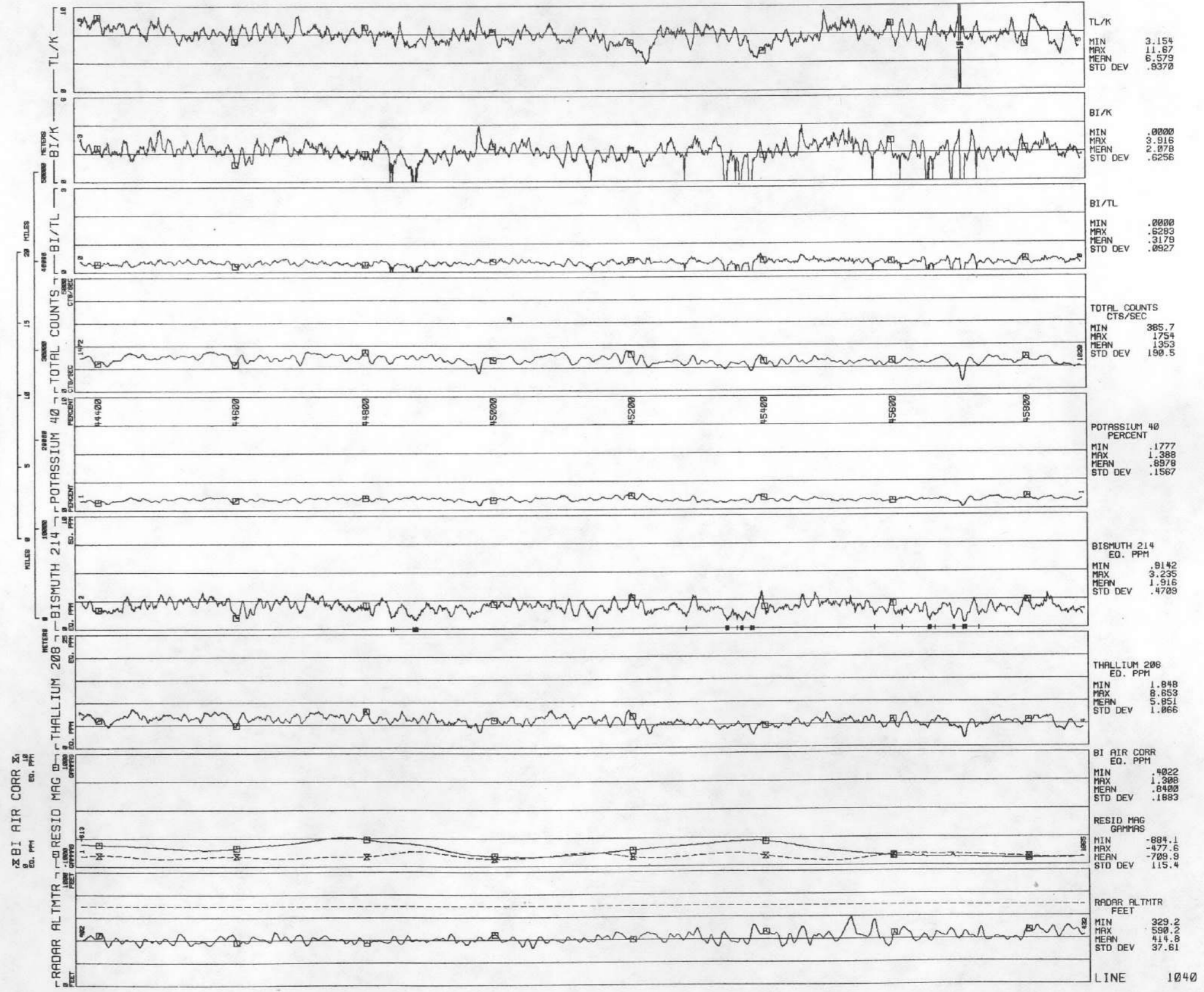


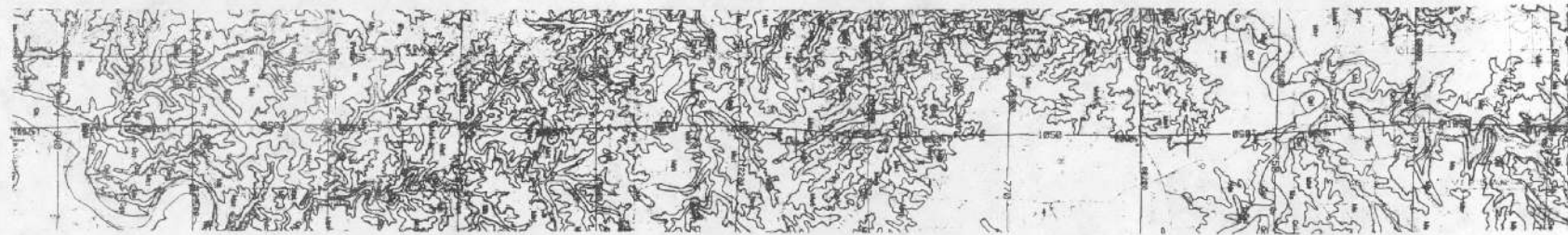
LINE 1030
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80338



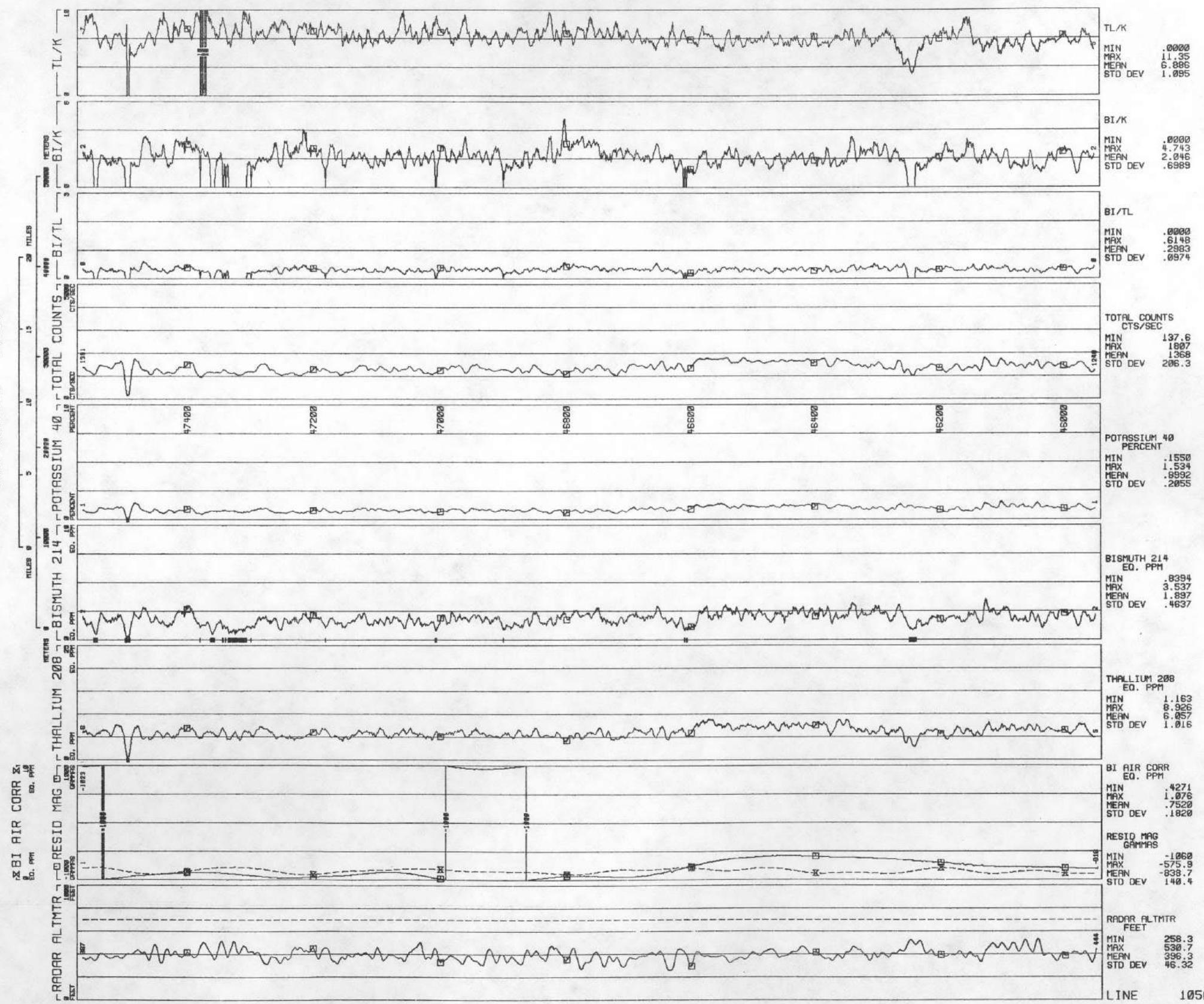


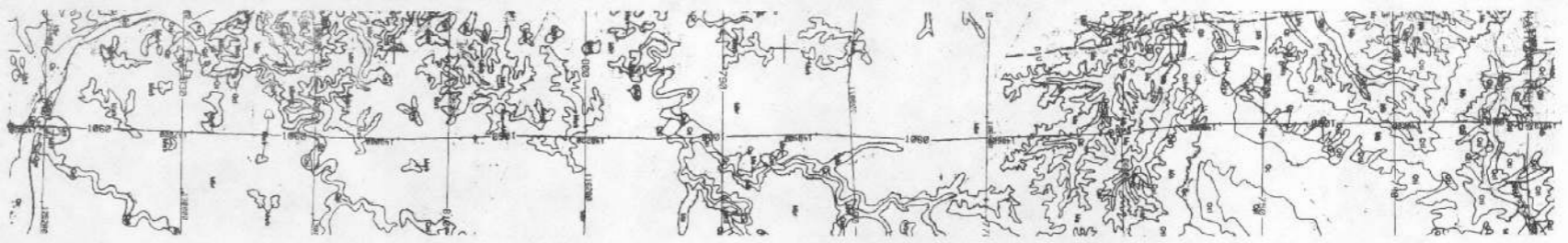
LINE 1040
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80338



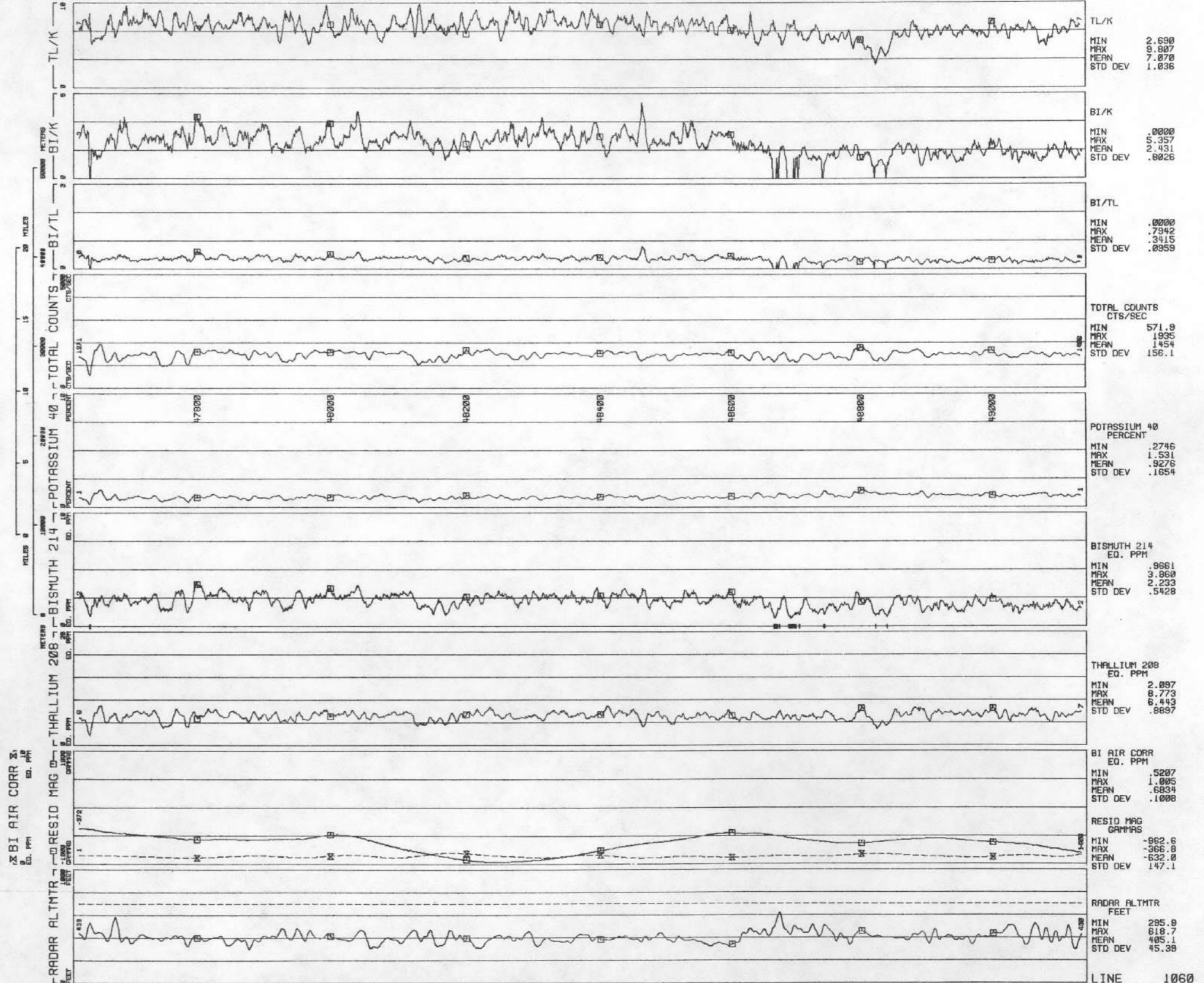


LINE 1050
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80338

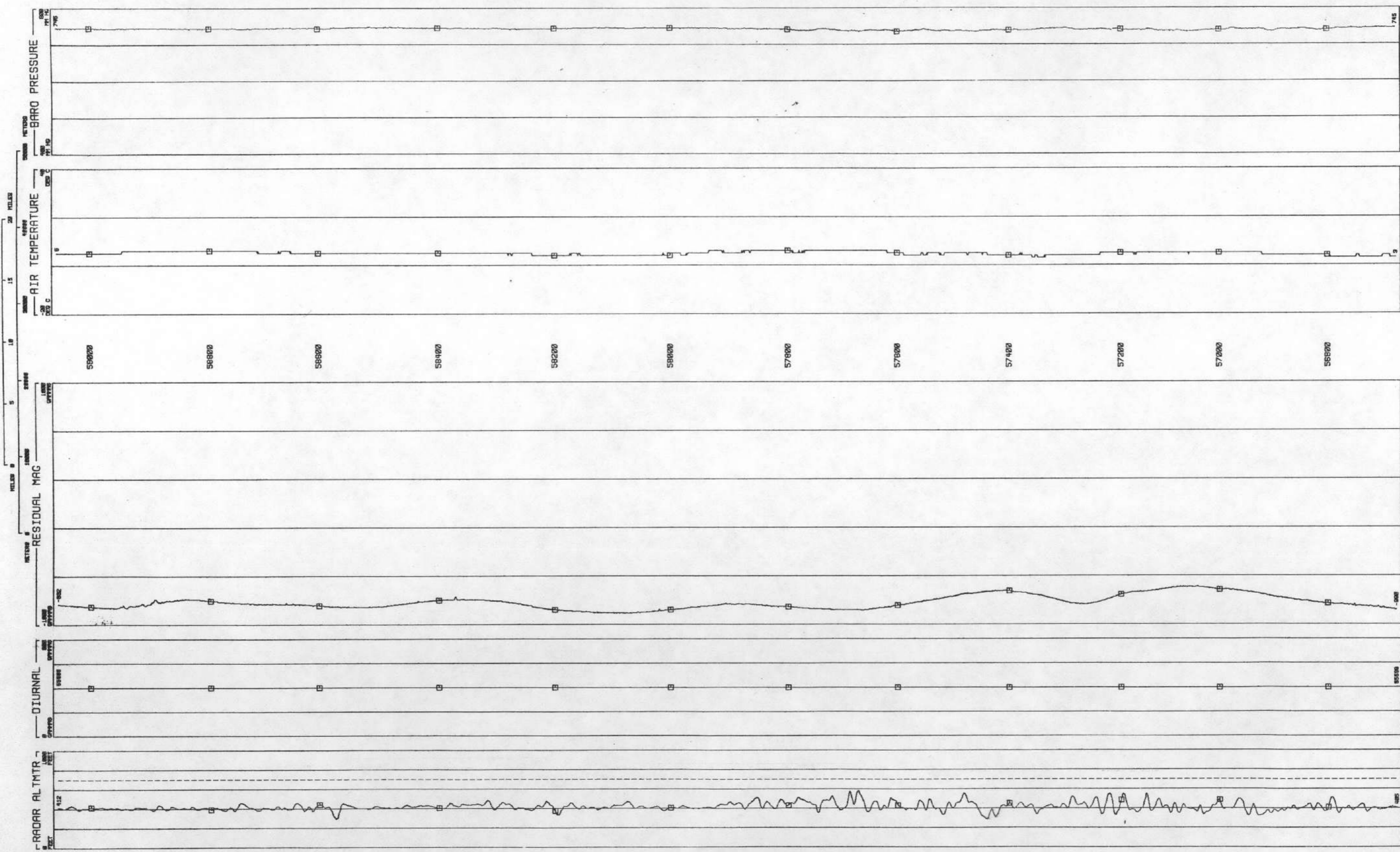




LINE 1060
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80338



LINE 730
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80327



BARO PRESSURE
MM HG
MIN 733.7
MAX 748.1
MEAN 742.1
STD DEV 3.238

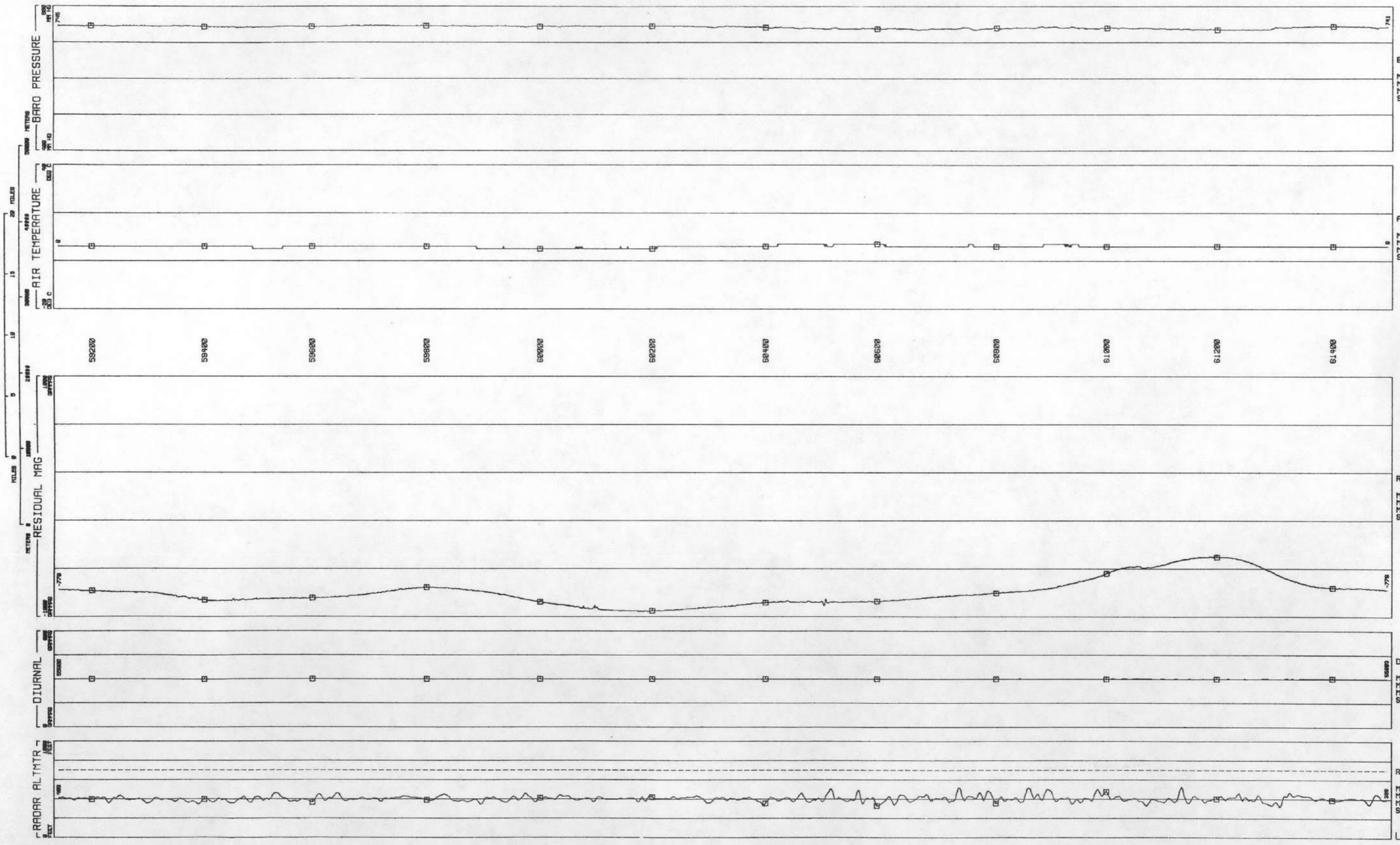
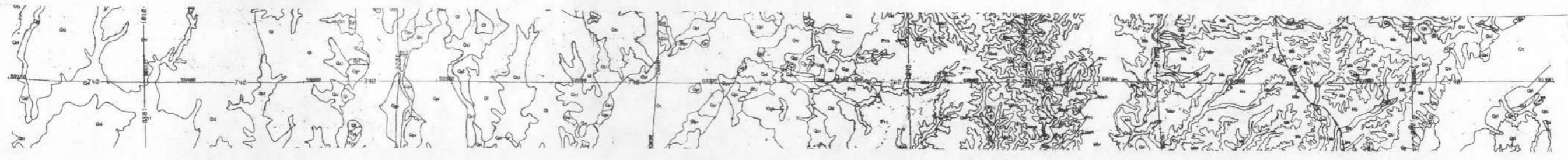
AIR TEMPERATURE
DEG C
MIN 3.000
MAX 6.000
MEAN 4.553
STD DEV .8078

RESIDUAL MAG
GAMMAS
MIN -907.4
MAX -689.2
MEAN -817.8
STD DEV 54.02

DIURNAL
GAMMAS
MIN 55598
MAX 55600
MEAN 55589
STD DEV 9.758

RADAR ALTMTR
FEET
MIN 287.1
MAX 578.2
MEAN 416.6
STD DEV 38.94

740
LINE
VINCENNES QUADRANGLE - NTMS NJ 16-5
80327



BARO PRESSURE
MM HG
MIN 733.7
MAX 747.6
MEAN 742.1
STD DEV 3.398

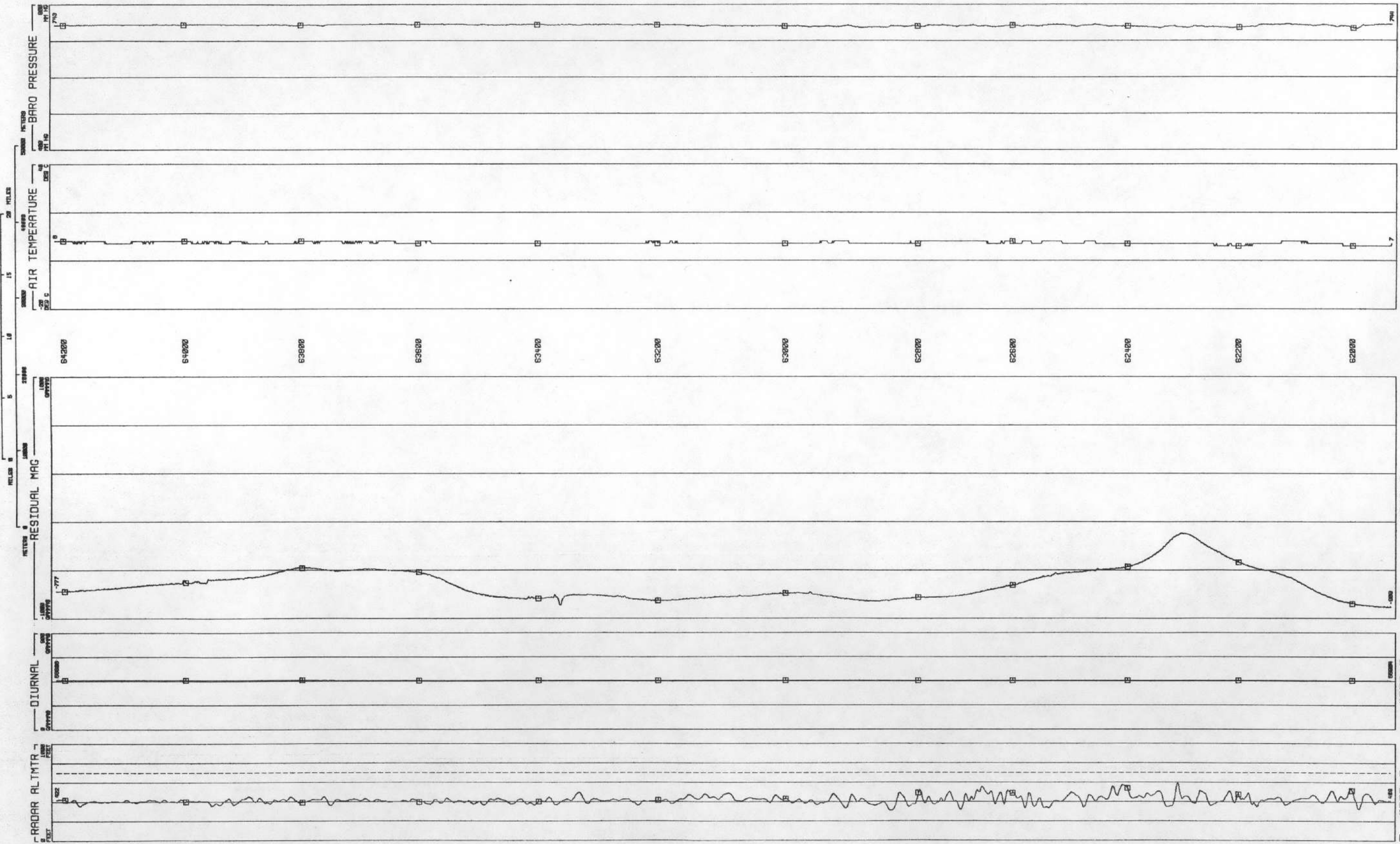
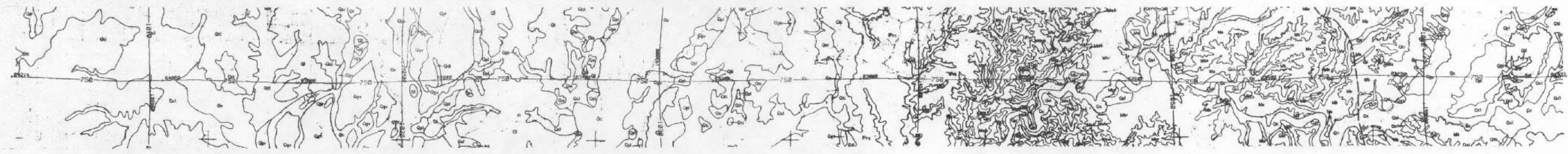
AIR TEMPERATURE
DEG C
MIN 5.000
MAX 7.000
MEAN 5.944
STD DEV .5126

RESIDUAL MAG
GAMMAS
MIN -955.8
MAX -499.8
MEAN -796.4
STD DEV 112.7

DIURNAL
GAMMAS
MIN 55599
MAX 55603
MEAN 55598
STD DEV 1.806

RADAR ALTHTR
FEET
MIN 319.2
MAX 522.7
MEAN 403.0
STD DEV 28.17

LINE 750
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80327



BARO PRESSURE
MM HG
MIN 732.4
MAX 747.1
MEAN 742.0
STD DEV 2.756

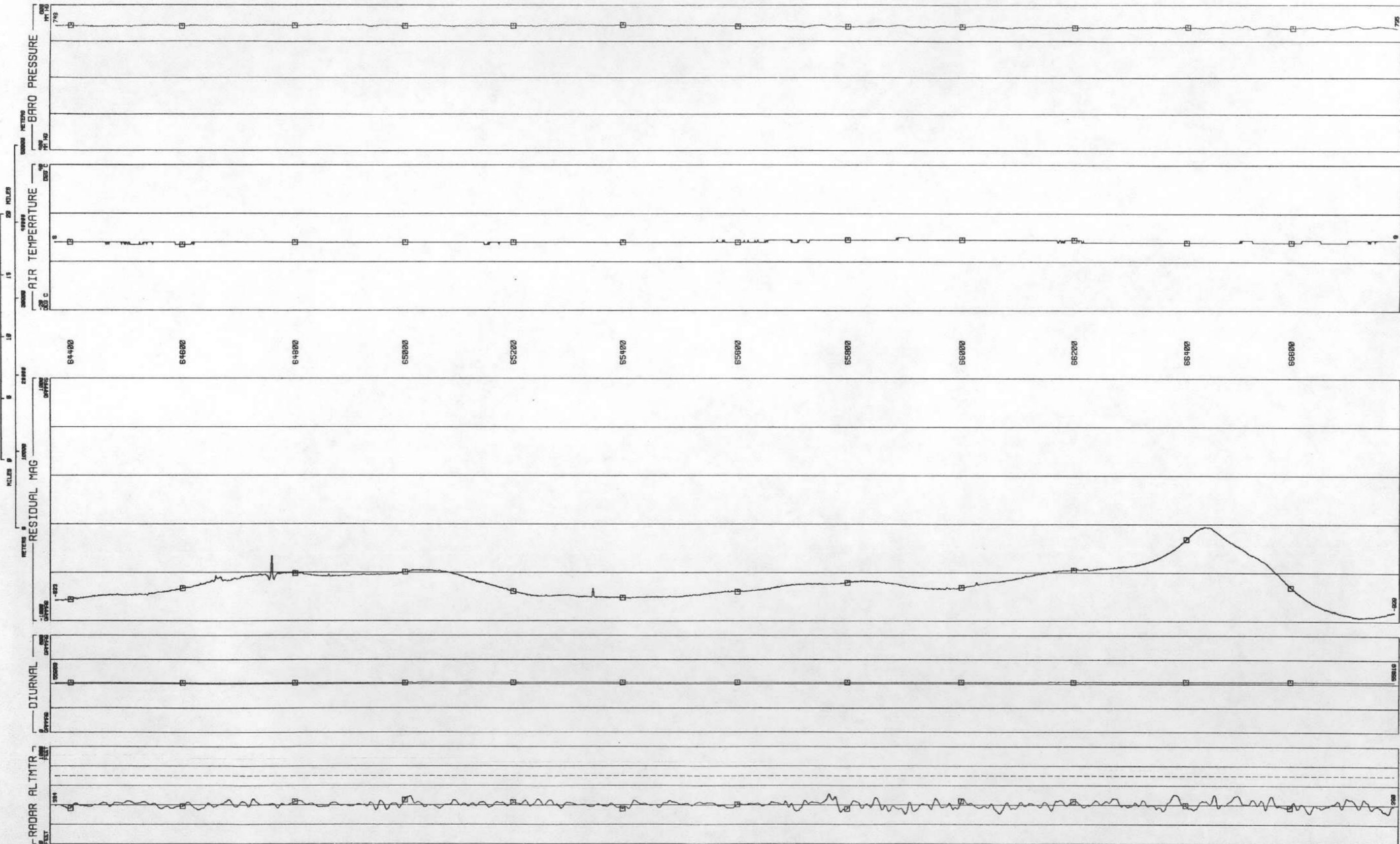
AIR TEMPERATURE
DEG C
MIN 6.000
MAX 8.000
MEAN 7.243
STD DEV .5583

RESIDUAL MAG
GAMMAS
MIN -909.9
MAX -294.4
MEAN -714.5
STD DEV 129.6

DIURNAL
GAMMAS
MIN 55603
MAX 55688
MEAN 55681
STD DEV 3.761

RADAR ALTMTR
FEET
MIN 388.5
MAX 598.1
MEAN 419.0
STD DEV 35.48

LINE 760
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80327



BARO PRESSURE
MM HG
MIN 733.7
MAX 746.5
MEAN 741.2
STD DEV 2.842

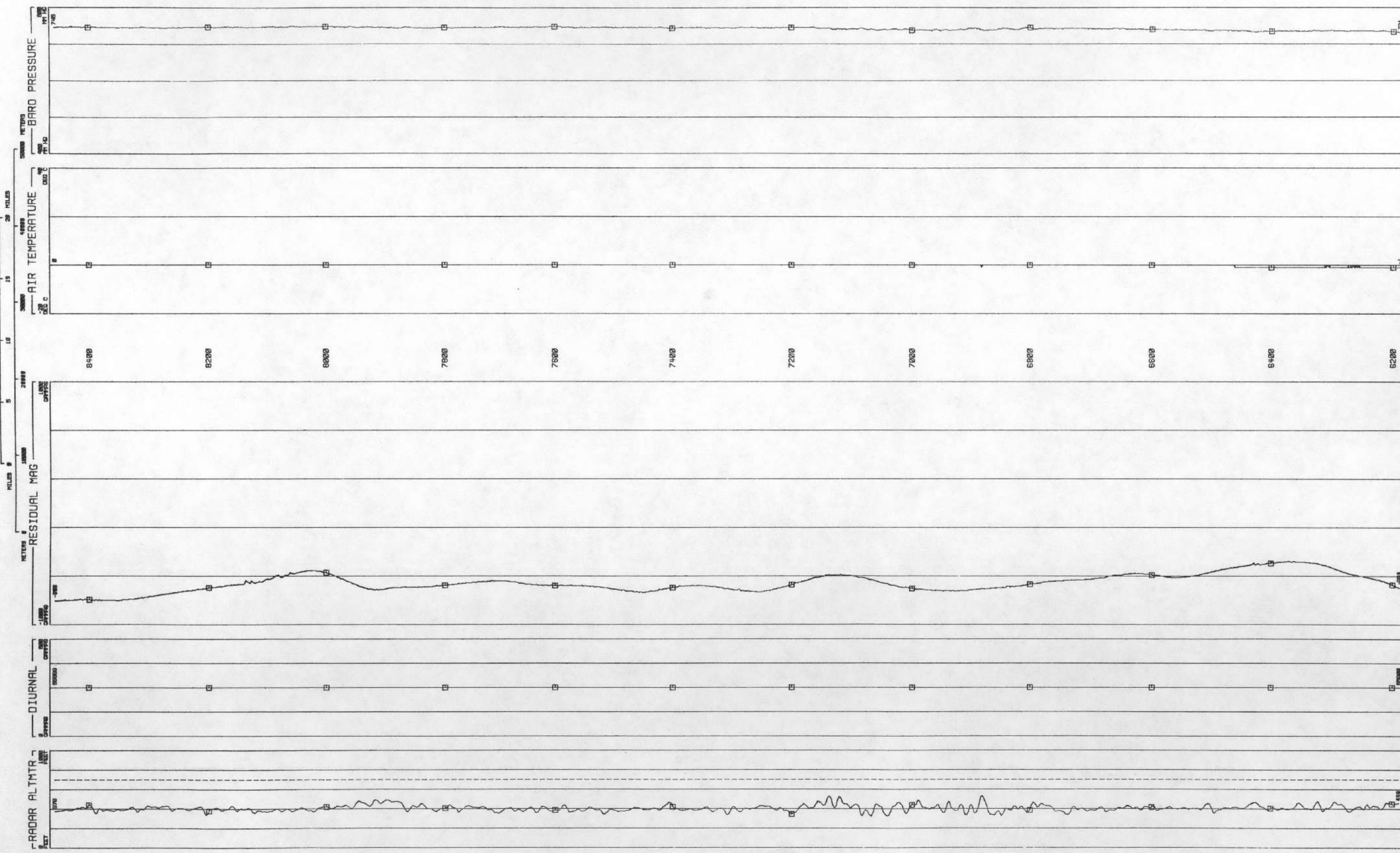
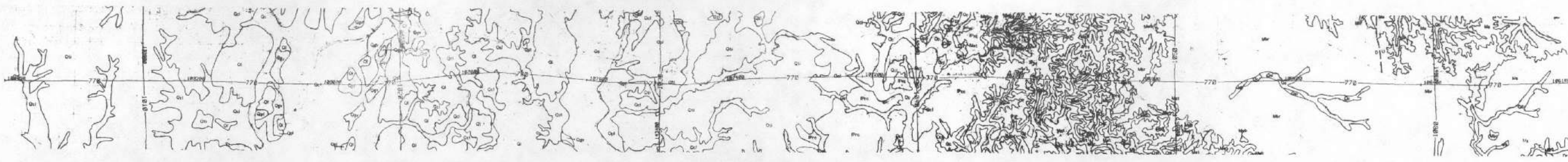
AIR TEMPERATURE
DEG C
MIN 7.000
MAX 10.00
MEAN 8.262
STD DEV .5194

RESIDUAL MAG
GAMMAS
MIN -970.8
MAX -221.9
MEAN -680.8
STD DEV 138.5

DIURNAL
GAMMAS
MIN 55608
MAX 55616
MEAN 55604
STD DEV 7.688

RADAR ALTMTR
FEET
MIN 304.2
MAX 513.7
MEAN 404.0
STD DEV 38.72

LINE 770
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80331



BARO PRESSURE
MM HG
MIN 731.0
MAX 749.7
MEAN 742.9
STD DEV 4.154

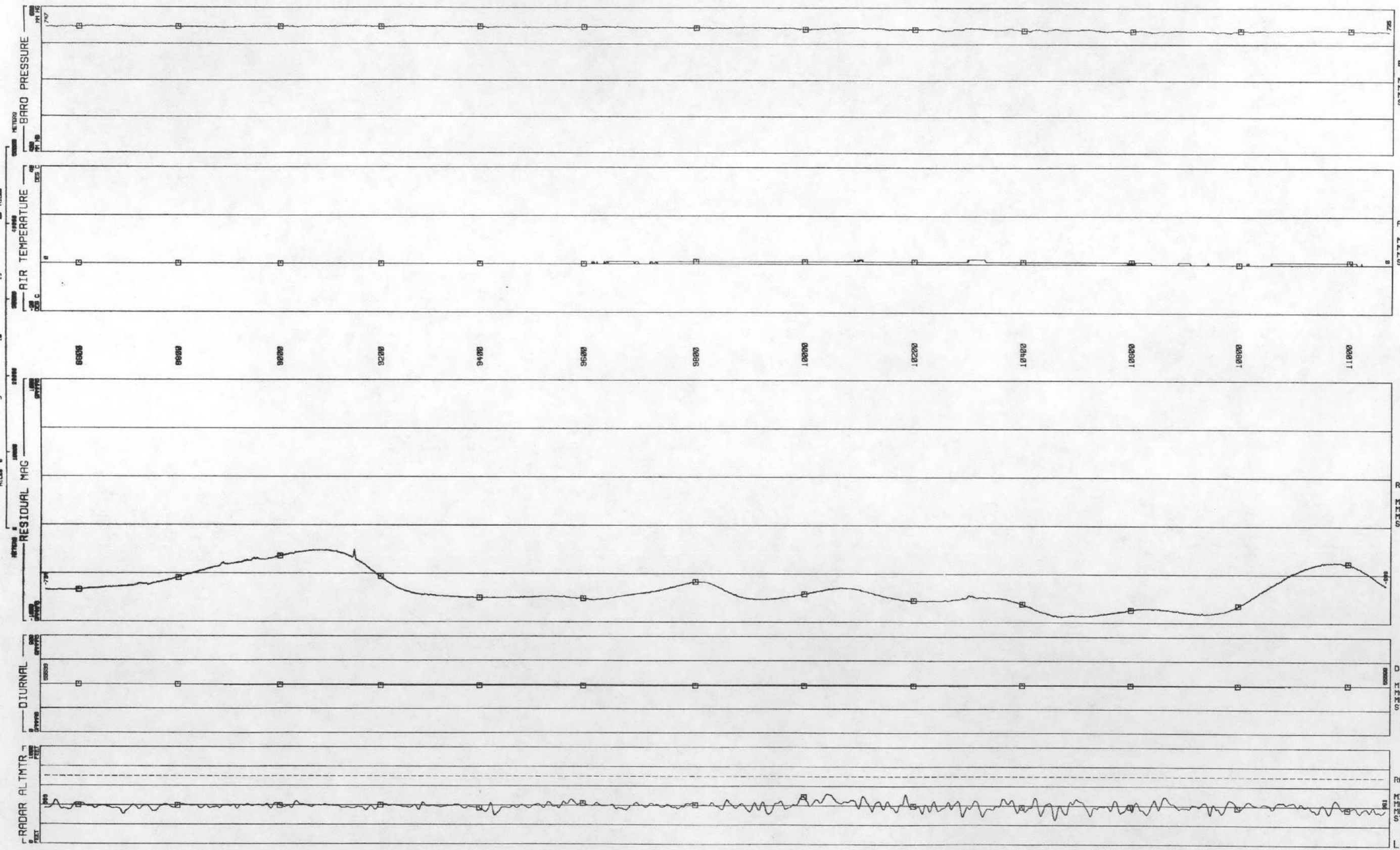
AIR TEMPERATURE
DEG C
MIN -1.000
MAX .0000
MEAN -.1154
STD DEV .3195

RESIDUAL MAG
GAMMAS
MIN -806.9
MAX -477.1
MEAN -657.7
STD DEV 73.73

DIURNAL
GAMMAS
MIN 55598
MAX 55601
MEAN 55591
STD DEV 8.493

RADAR ALTMTR
FEET
MIN 323.6
MAX 530.0
MEAN 405.7
STD DEV 30.60

LINE 780
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80331



BARO PRESSURE
MM HG
MIN 732.1
MAX 748.7
MEAN 743.1
STD DEV 4.396

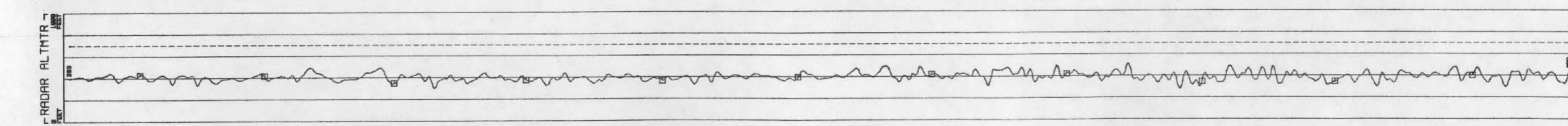
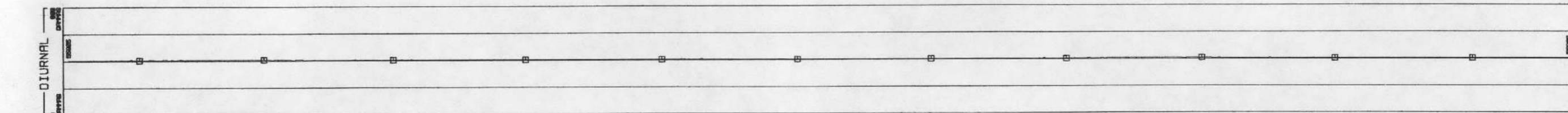
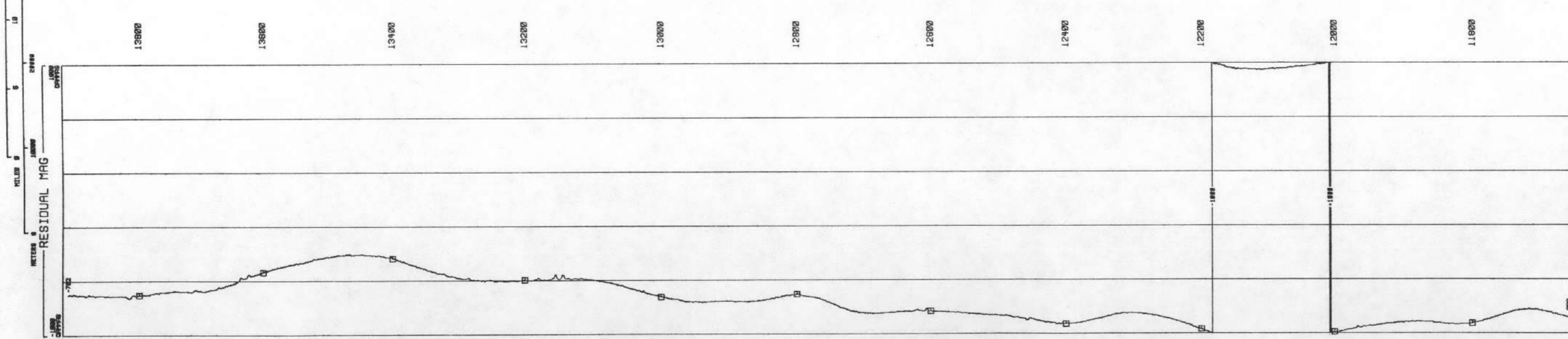
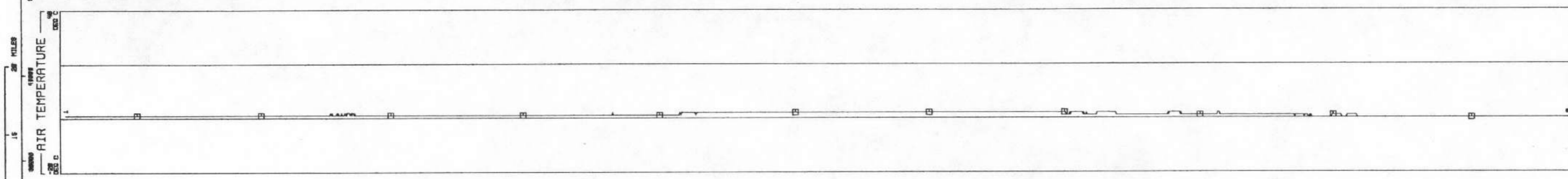
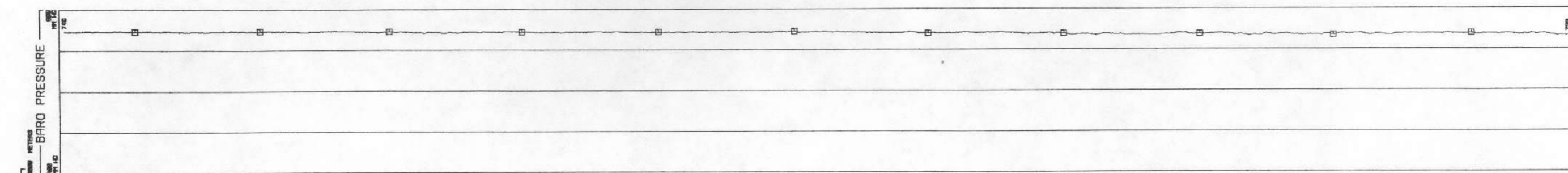
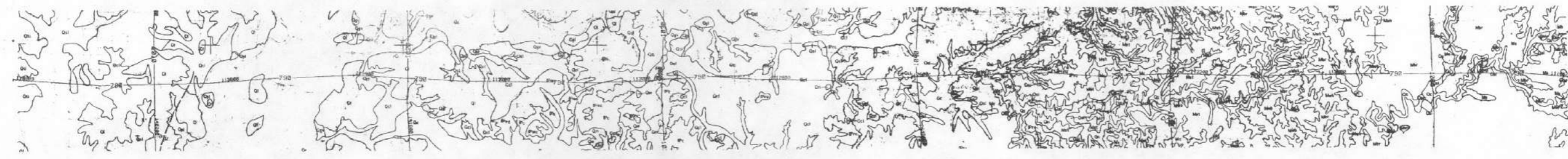
AIR TEMPERATURE
DEG C
MIN .0000
MAX 2.0000
MEAN .4654
STD DEV .5294

RESIDUAL MAG
GAMMAS
MIN -954.3
MAX -403.0
MEAN -728.7
STD DEV 138.8

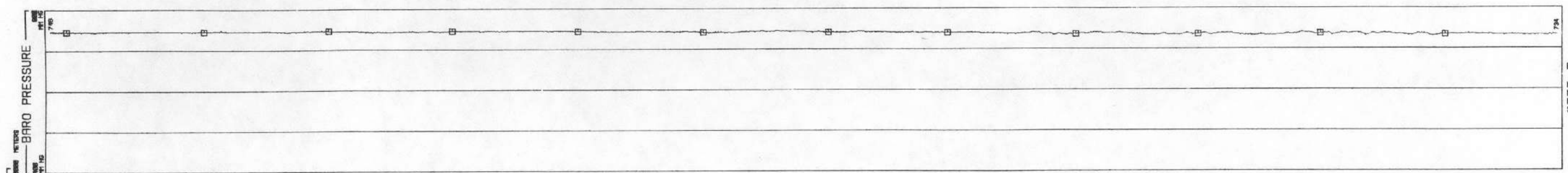
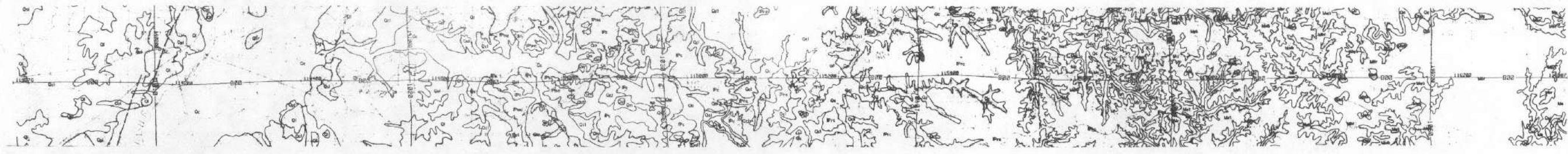
DIURNAL
GAMMAS
MIN 55592
MAX 55601
MEAN 55589
STD DEV 6.867

RADAR ALTMTR
FEET
MIN 256.0
MAX 520.4
MEAN 393.5
STD DEV 34.19

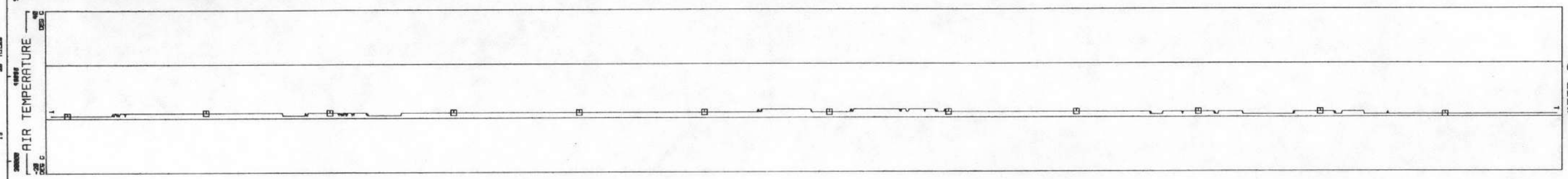
790
LINE
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80331



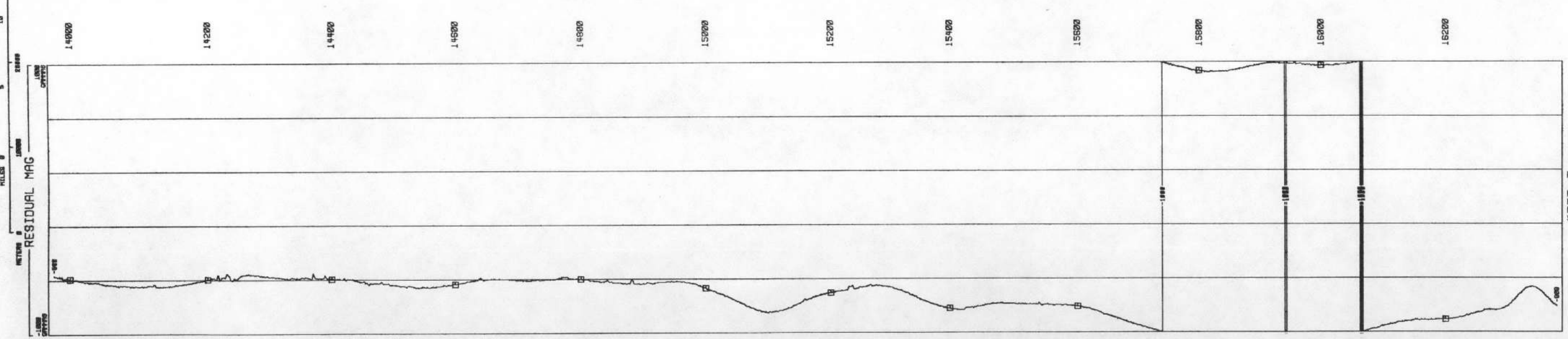
LINE 800
VINCENNES QUADRANGLE - NTMS NJ 16-5
80331 DATA ACQUIRED



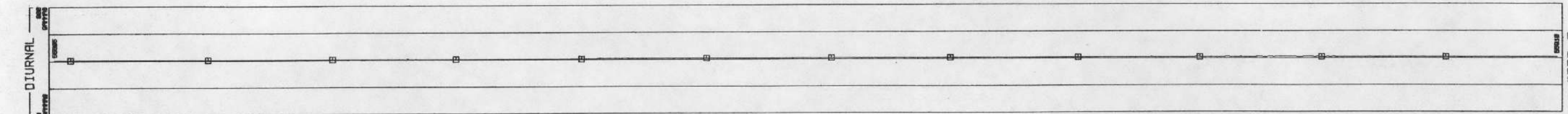
BARO PRESSURE
MIN HG 731.0
MAX 747.6
MEAN 740.8
STD DEV 4.182



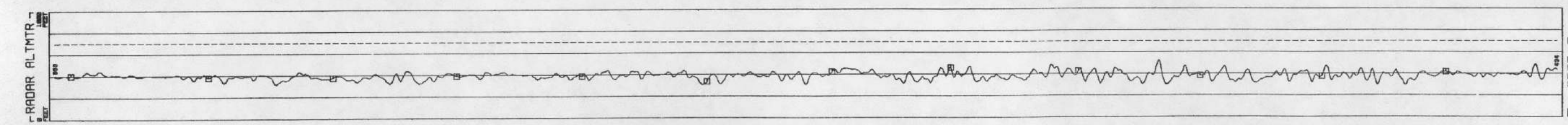
AIR TEMPERATURE
DEG C
MIN 1.000
MAX 3.000
MEAN 1.829
STD DEV .5693



RESIDUAL MAG
GAMMAS
MIN -1075
MAX -552.1
MEAN -756.7
STD DEV 155.3



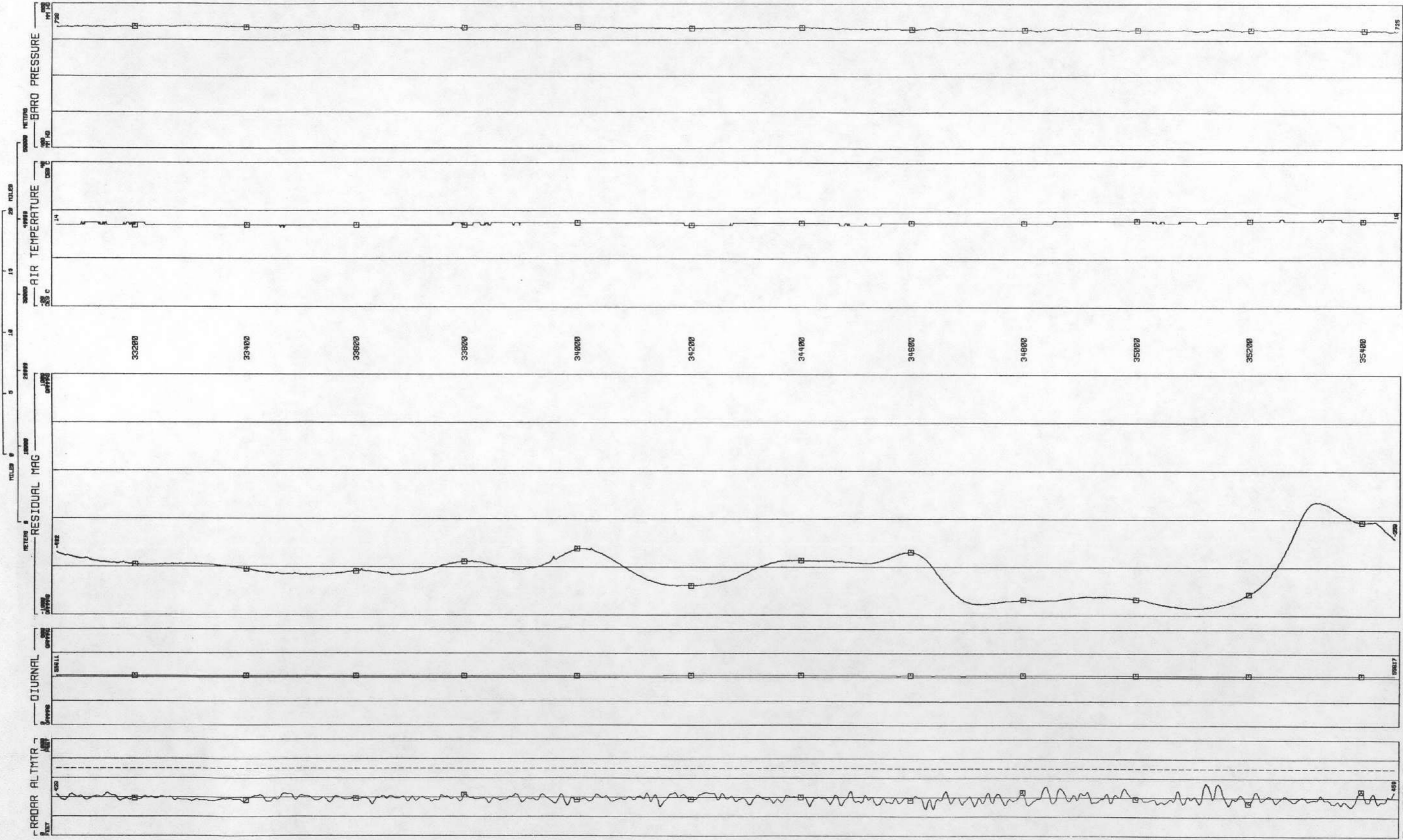
DIURNAL
GAMMAS
MIN 5560.4
MAX 5561.0
MEAN 5560.1
STD DEV 6.323

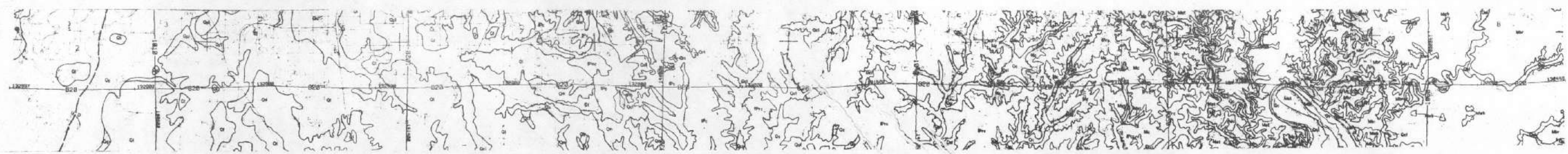


RADAR ALTMTR
FEET
MIN 293.4
MAX 520.3
MEAN 388.1
STD DEV 32.15

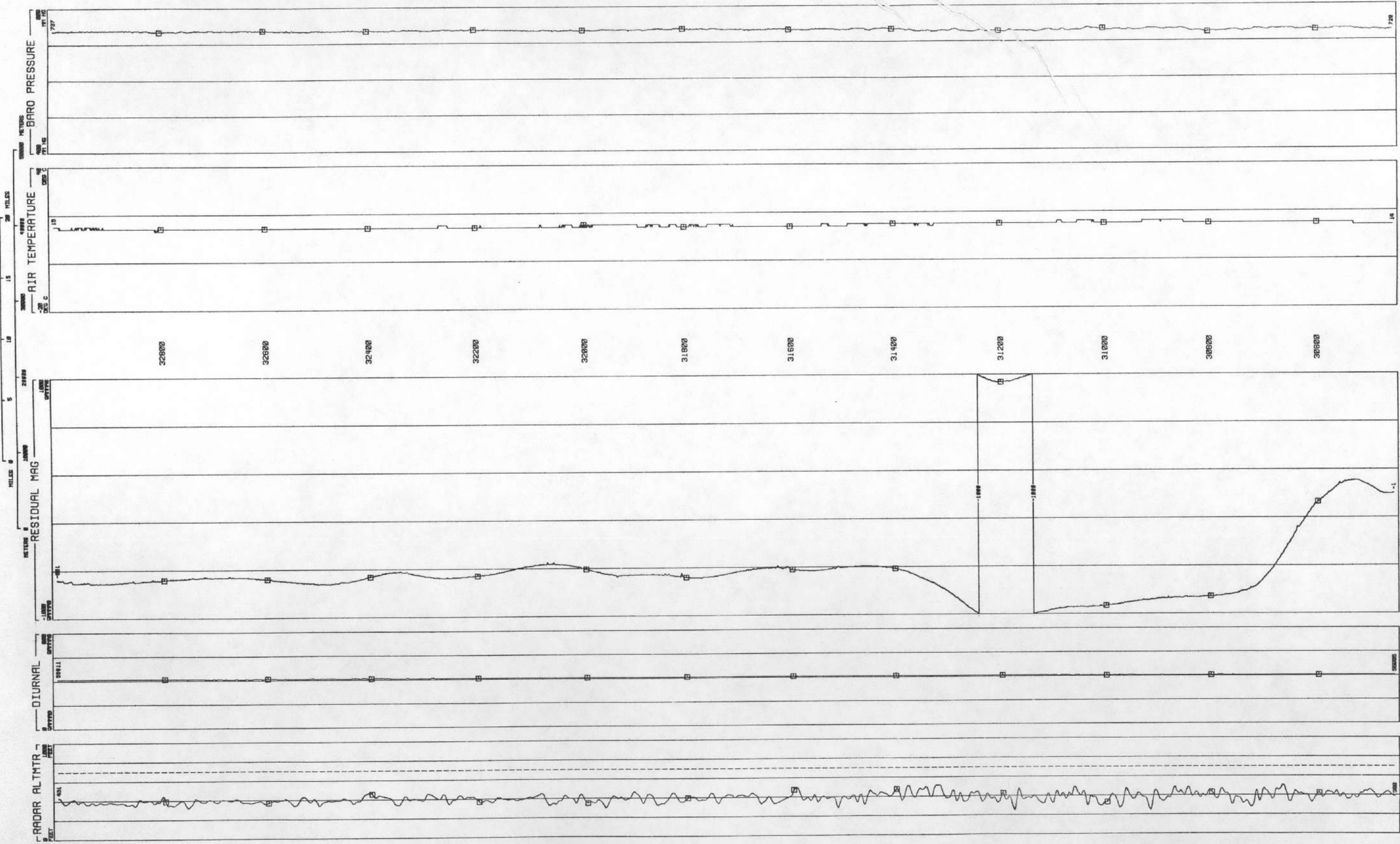


LINE 810
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80336





LINE 820
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80336



BARO PRESSURE
 MM HG
 MIN 723.3
 MAX 738.9
 MEAN 733.5
 STD DEV 3.854

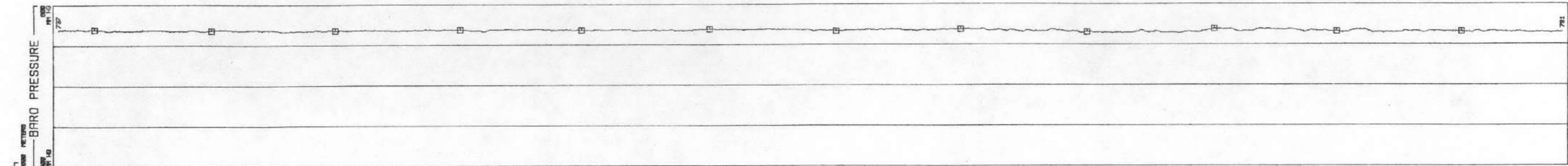
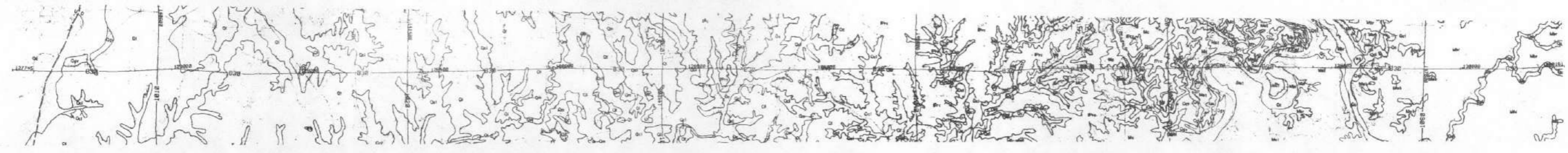
AIR TEMPERATURE
 DEG C
 MIN 13.00
 MAX 16.00
 MEAN 14.53
 STD DEV .5878

RESIDUAL MAG
 GAMMAS
 MIN -1065
 MAX 109.5
 MEAN -666.1
 STD DEV 228.8

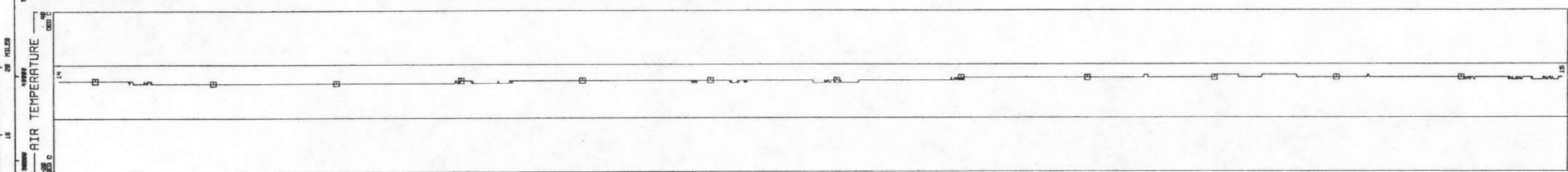
DIURNAL
 GAMMAS
 MIN 55605
 MAX 55611
 MEAN 55603
 STD DEV 5.238

RADAR ALTMTR
 FEET
 MIN 249.5
 MAX 518.2
 MEAN 393.9
 STD DEV 38.81

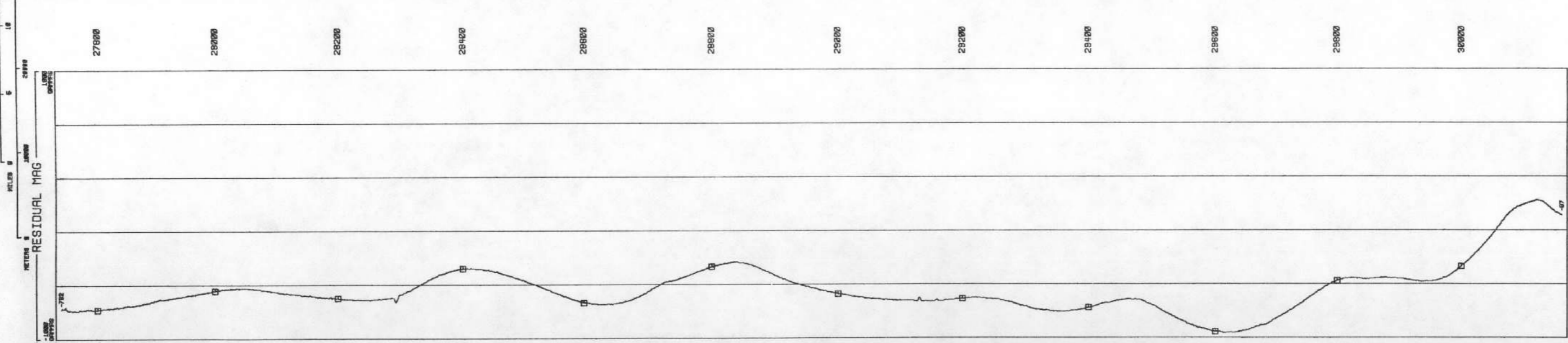
LINE 830
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80336



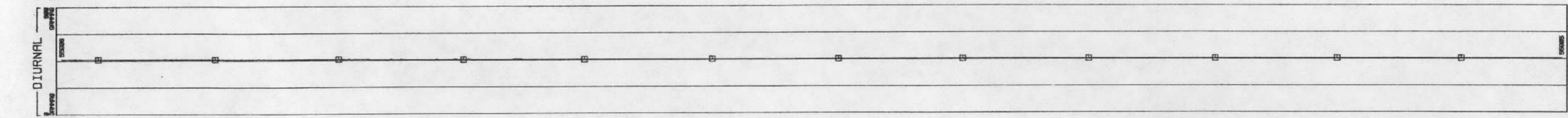
BARO PRESSURE
MM HG
MIN 727.9
MAX 739.7
MEAN 734.5
STD DEV 2.688



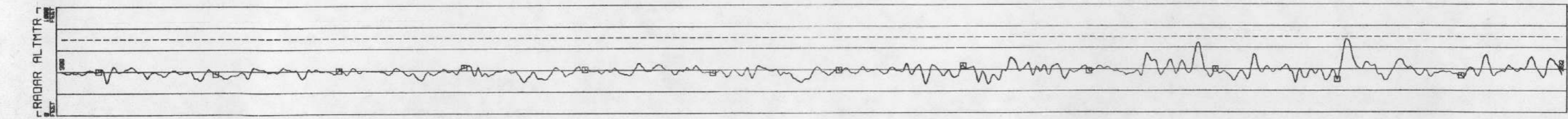
AIR TEMPERATURE
DEG C
MIN 13.00
MAX 16.00
MEAN 14.15
STD DEV .8677



RESIDUAL MAG
GAMMAS
MIN -964.8
MAX 22.63
MEAN -64.5
STD DEV 177.8



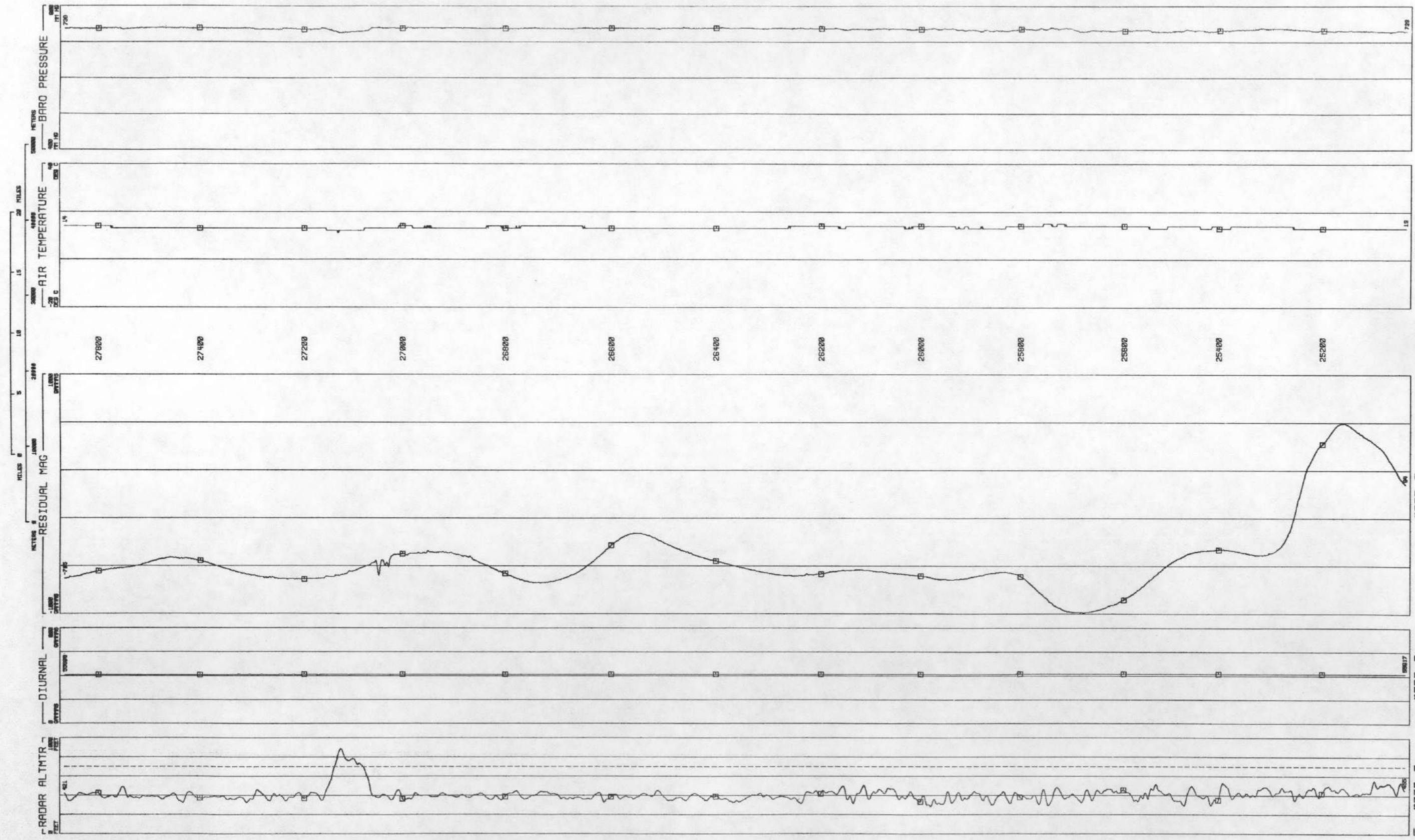
DIURNAL
GAMMAS
MIN 55603
MAX 55608
MEAN 55601
STD DEV 3.974



RADAR ALTMTR
FEET
MIN 266.0
MAX 675.7
MEAN 398.7
STD DEV 47.59



LINE 840
 VINCENTES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80336



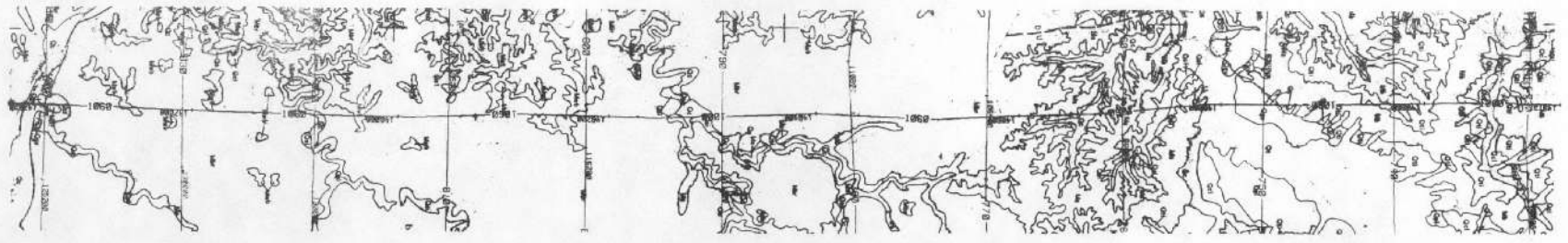
BARO PRESSURE
 MM HG
 MIN 725.3
 MAX 740.7
 MEAN 735.4
 STD DEV 3.296

AIR TEMPERATURE
 DEG C
 MIN 11.00
 MAX 15.00
 MEAN 13.28
 STD DEV .5710

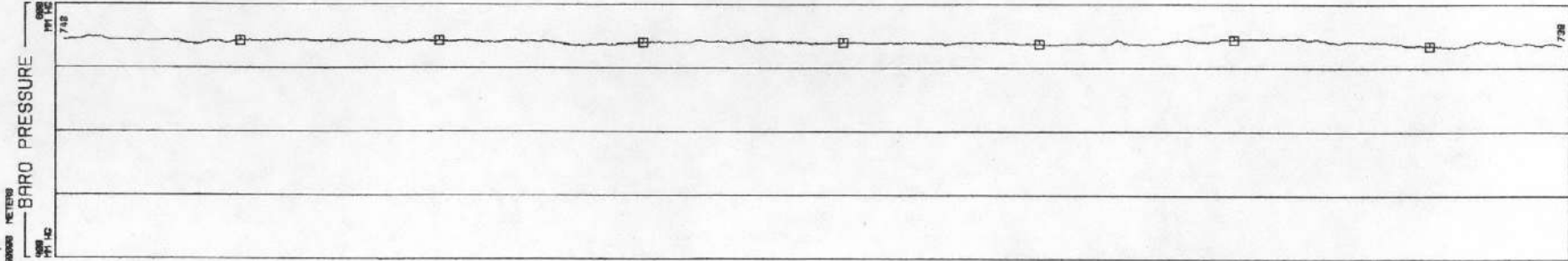
RESIDUAL MAG
 GAMMAS
 MIN -990.8
 MAX 594.5
 MEAN -543.8
 STD DEV 307.2

DIURNAL
 GAMMAS
 MIN 55608
 MAX 55617
 MEAN 55604
 STD DEV 8.658

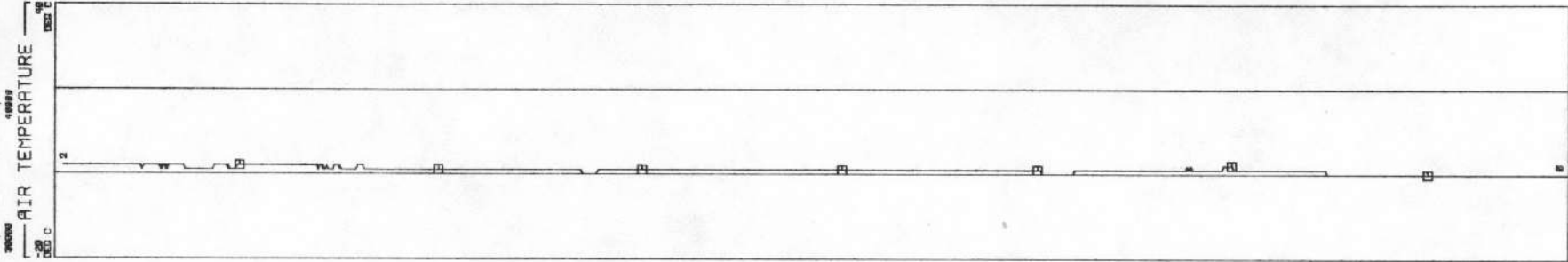
RADAR ALTMTR
 FEET
 MIN 284.1
 MAX 884.3
 MEAN 499.9
 STD DEV 73.58



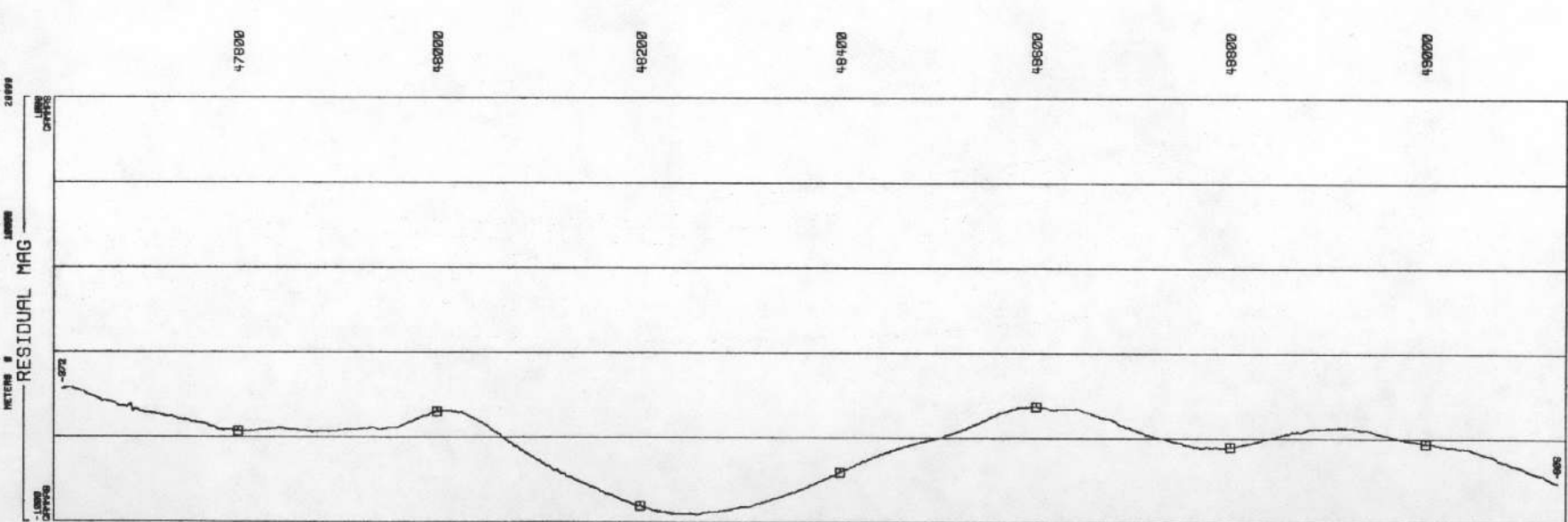
LINE 1060
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80338



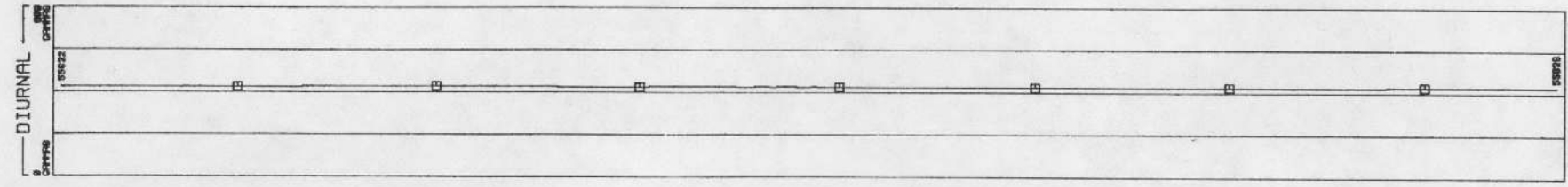
BARO PRESSURE
 MM HG
 MIN 731.5
 MAX 749.2
 MEAN 740.4
 STD DEV 2.955



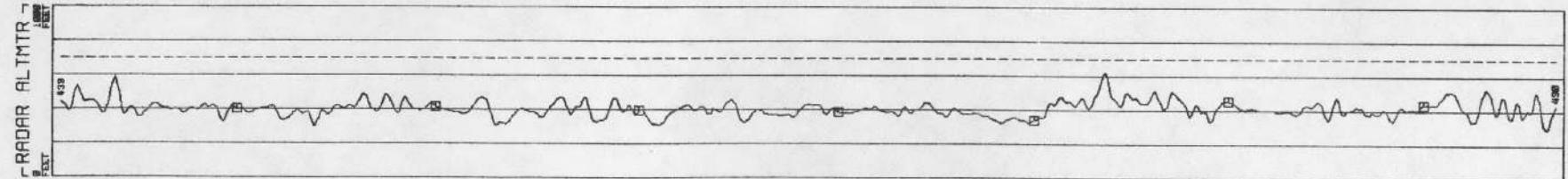
AIR TEMPERATURE
 DEG C
 MIN .0000
 MAX 2.0000
 MEAN .9669
 STD DEV .5935



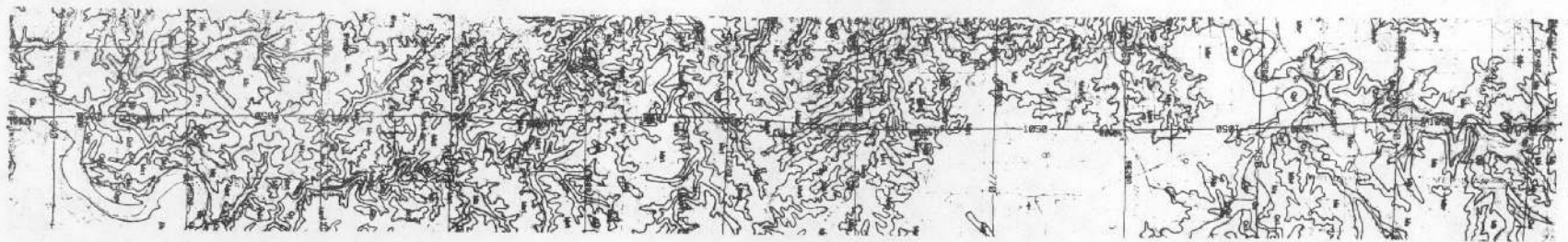
RESIDUAL MAG
 GAMMAS
 MIN -962.6
 MAX -366.8
 MEAN -632.0
 STD DEV 147.1



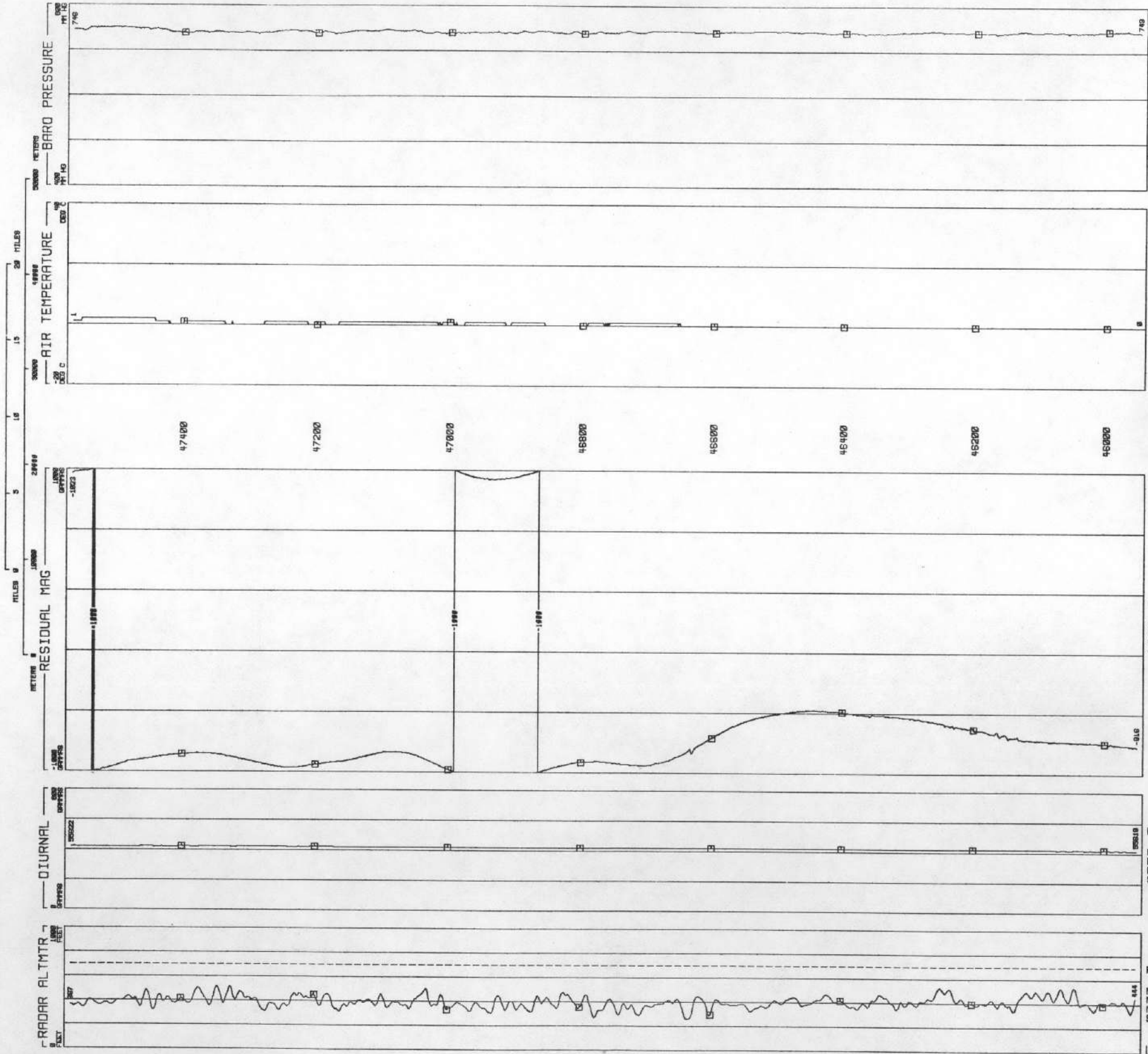
DIURNAL
 GAMMAS
 MIN 55622
 MAX 55629
 MEAN 55622
 STD DEV 3.943



RADAR ALTMTR
 FEET
 MIN 295.9
 MAX 618.7
 MEAN 405.1
 STD DEV 45.39

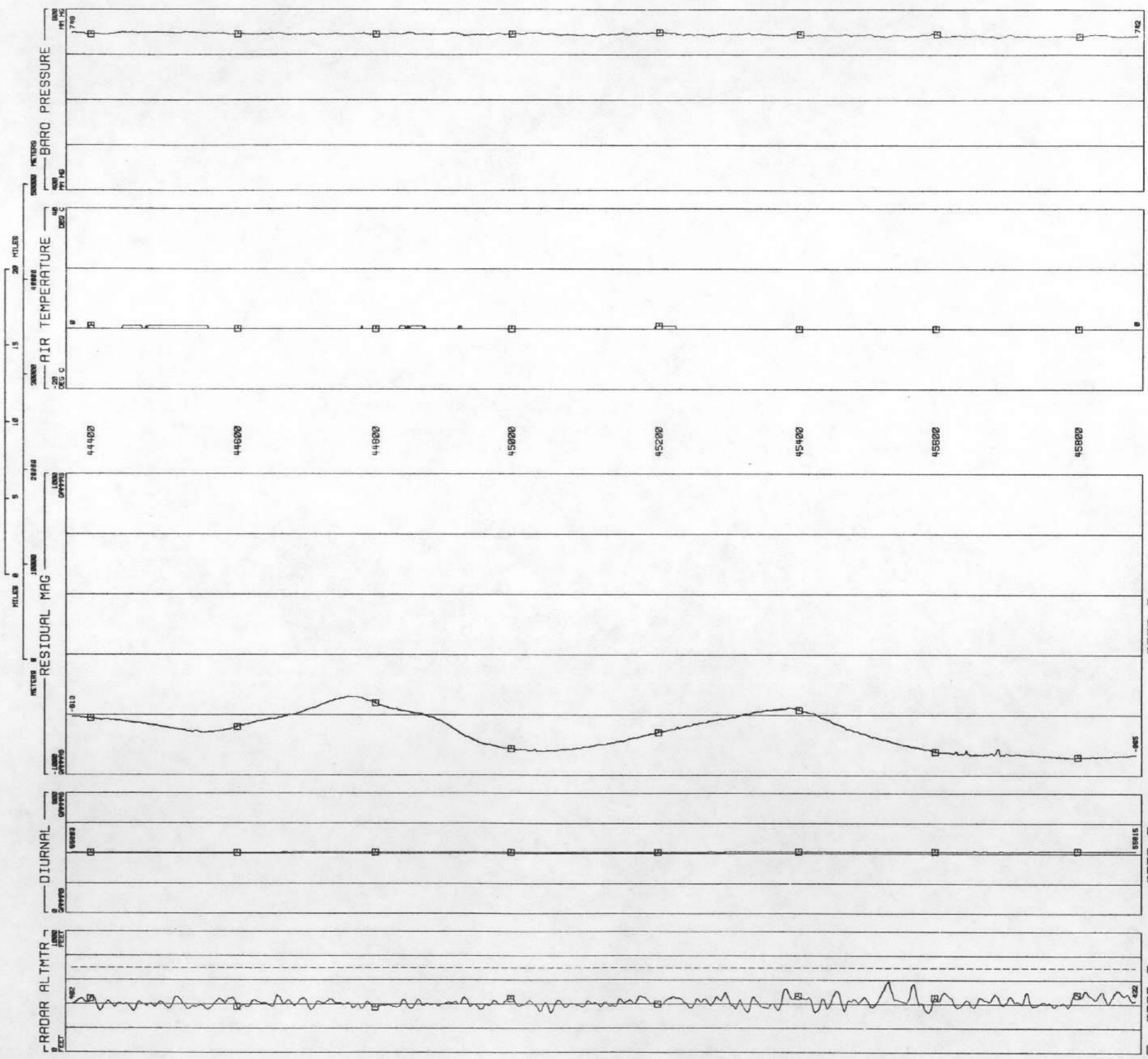


LINE 1050
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80338





LINE 1040
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80338



BARO PRESSURE
 MM HG
 MIN 737.4
 MAX 750.7
 MEAN 744.6
 STD DEV 2.761

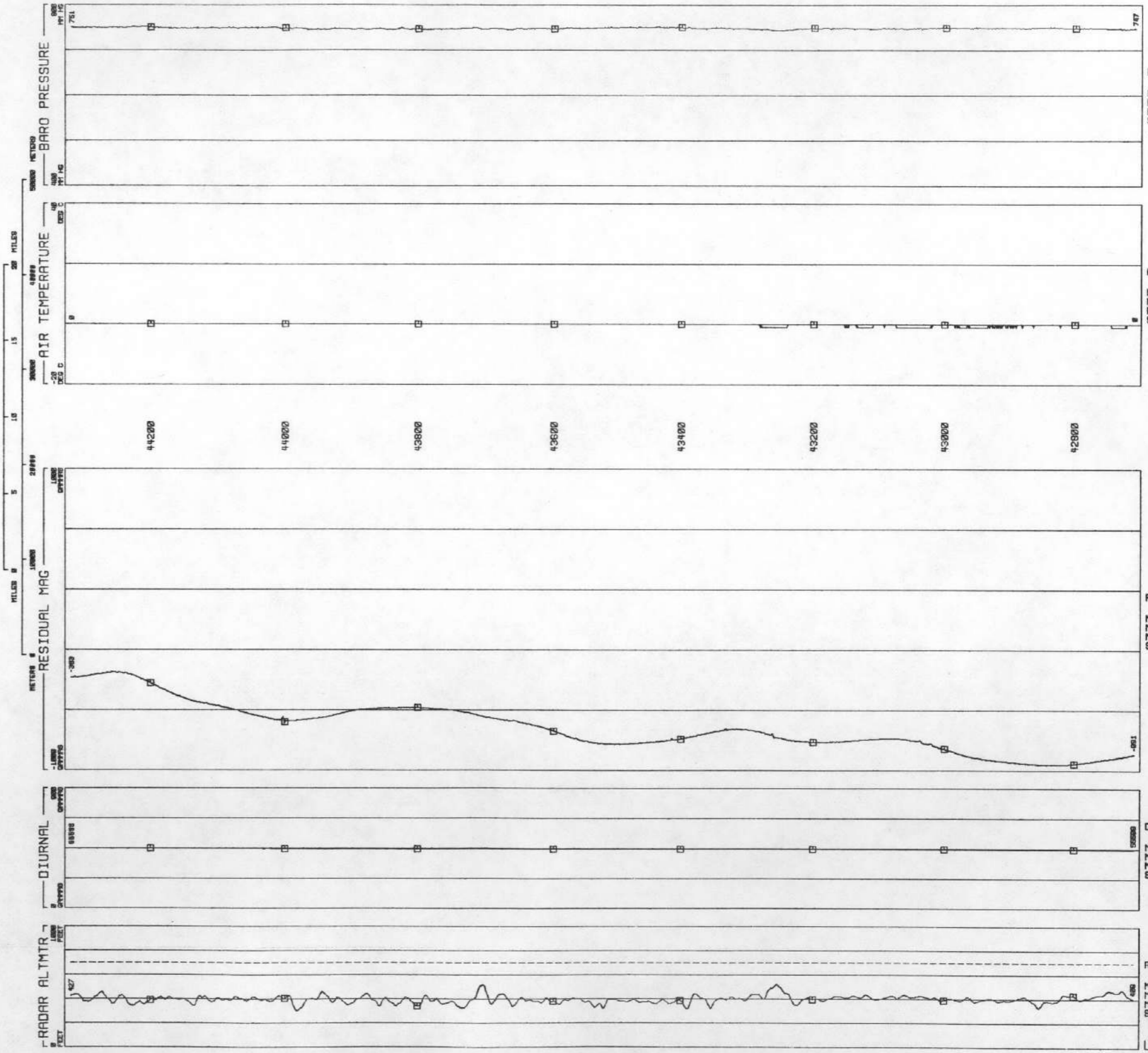
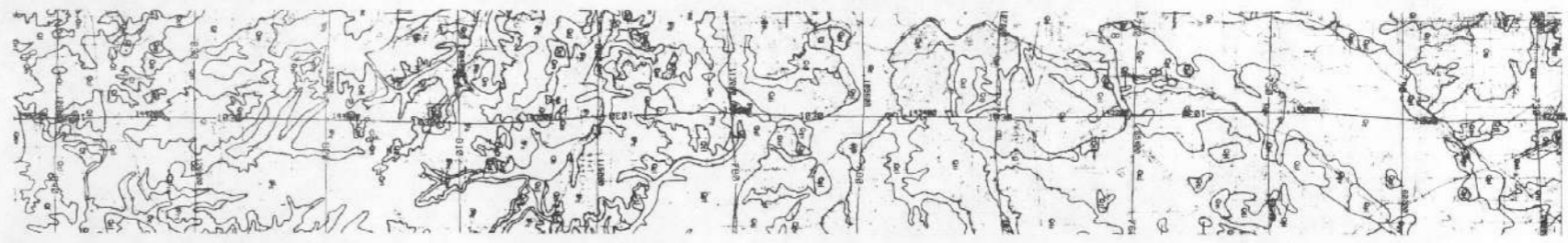
AIR TEMPERATURE
 DEG C
 MIN .0020
 MAX 1.000
 MEAN .1213
 STD DEV .3265

RESIDUAL MAG
 GAMMAS
 MIN -884.1
 MAX -477.6
 MEAN -709.9
 STD DEV 115.4

DIURNAL
 GAMMAS
 MIN 55603
 MAX 55615
 MEAN 55605
 STD DEV 5.590

RADAR ALTMTR
 FEET
 MIN 329.2
 MAX 590.2
 MEAN 414.8
 STD DEV 37.61

LINE 1030
VINCENNES QUADRANGLE - NTMS NJ 16-5
DATA ACQUIRED 80338



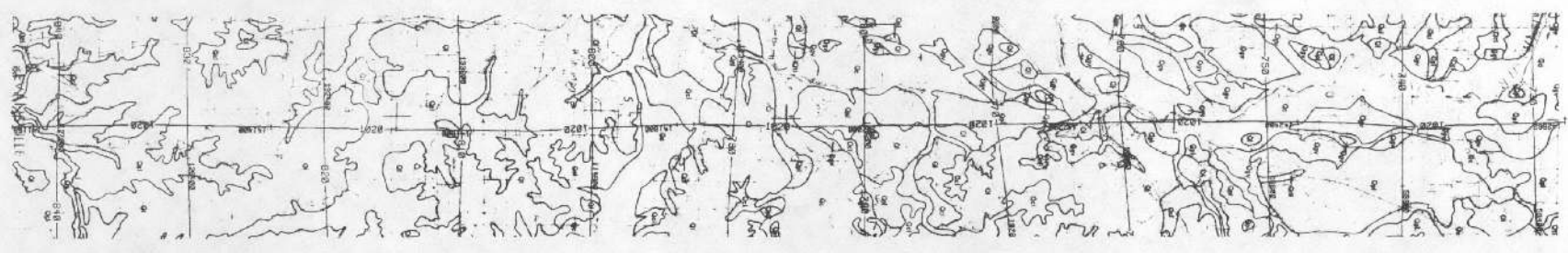
BARO PRESSURE
MM HG
MIN 743.6
MAX 752.3
MEAN 746.3
STD DEV 1.576

AIR TEMPERATURE
DEG C
MIN -1.000
MAX .0000
MEAN -.1323
STD DEV .3366

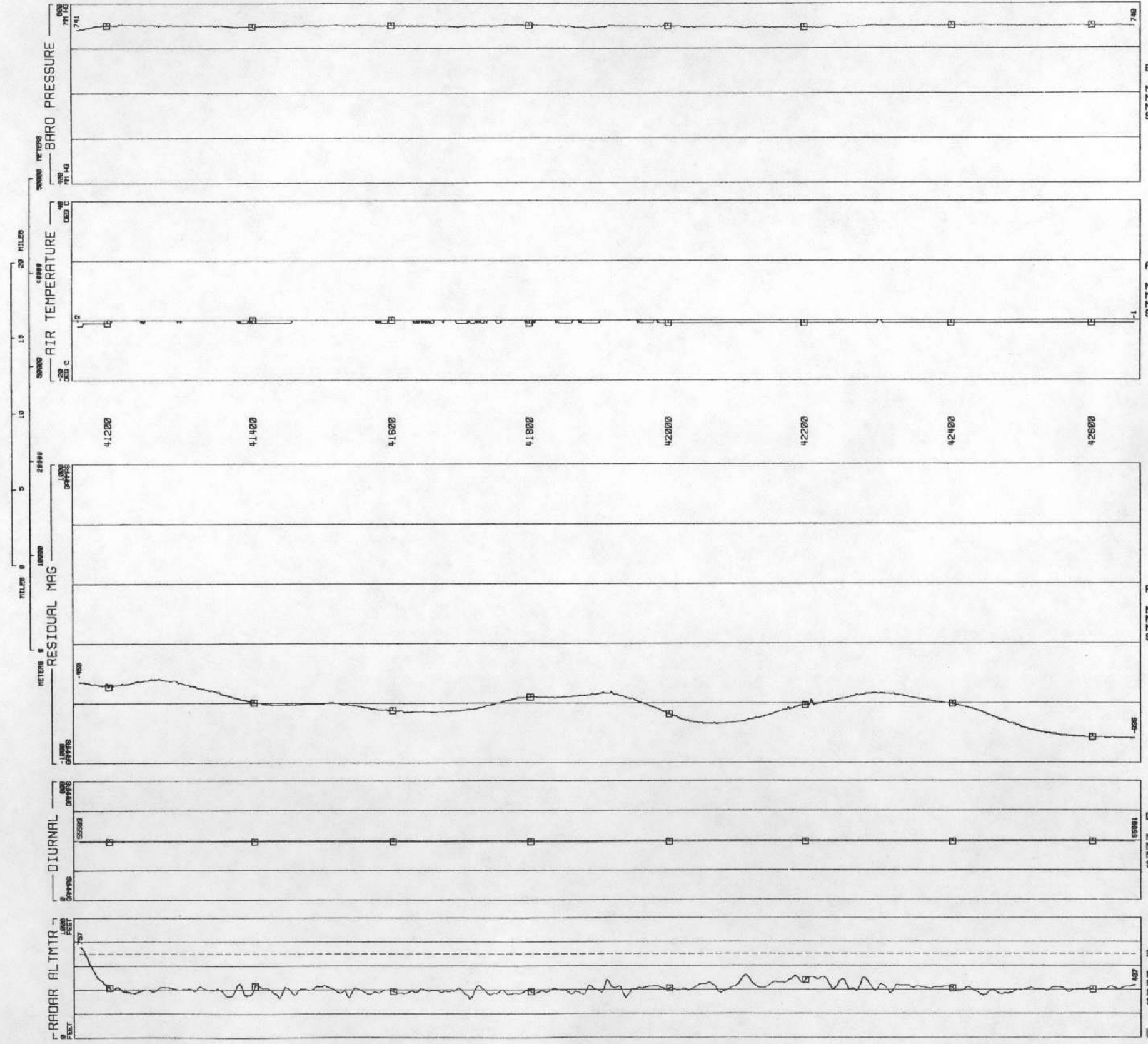
RESIDUAL MAG
GAMMAS
MIN -962.2
MAX -347.0
MEAN -720.6
STD DEV 157.8

DIURNAL
GAMMAS
MIN 55594
MAX 55800
MEAN 55592
STD DEV 4.688

RADAR ALTMTR
FEET
MIN 301.6
MAX 518.8
MEAN 397.3
STD DEV 31.63



LINE 1020
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80338



BARO PRESSURE
 MM HG
 MIN 740.7
 MAX 753.4
 MEAN 749.3
 STD DEV 1.688

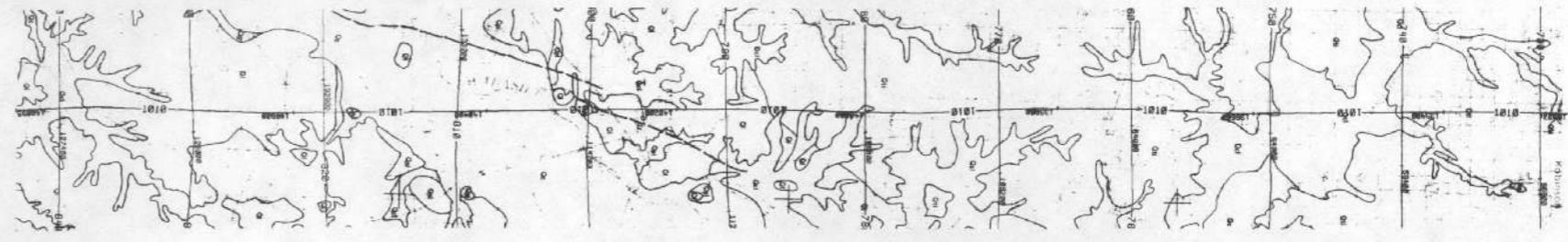
AIR TEMPERATURE
 DEG C
 MIN -2.000
 MAX .0000
 MEAN -.6354
 STD DEV .4822

RESIDUAL MAG
 GAMMAS
 MIN -835.6
 MAX -435.9
 MEAN -621.1
 STD DEV 98.19

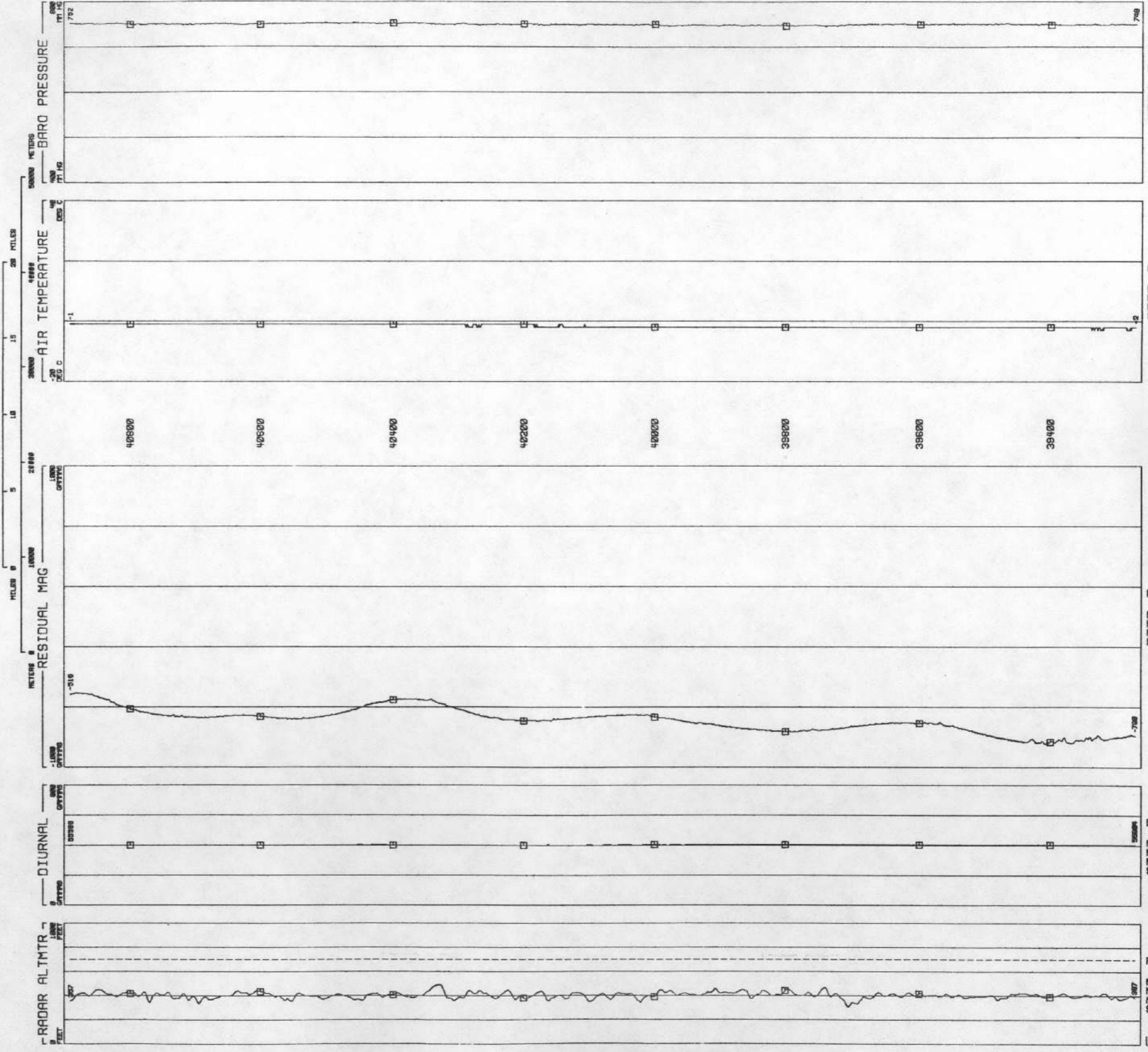
DIURNAL
 GAMMAS
 MIN 55591
 MAX 55594
 MEAN 55589
 STD DEV 3.210

RADAR ALTMTR
 FEET
 MIN 327.5
 MAX 756.9
 MEAN 411.8
 STD DEV 45.41

LINE 1020



LINE 1010
 VINCENNES QUADRANGLE - NTMS NJ 16-5
 DATA ACQUIRED 80338



BARO PRESSURE
 MM HG
 MIN 745.8
 MAX 753.4
 MEAN 749.7
 STD DEV 1.349

AIR TEMPERATURE
 DEG C
 MIN -3.000
 MAX -1.000
 MEAN -1.574
 STD DEV .5104

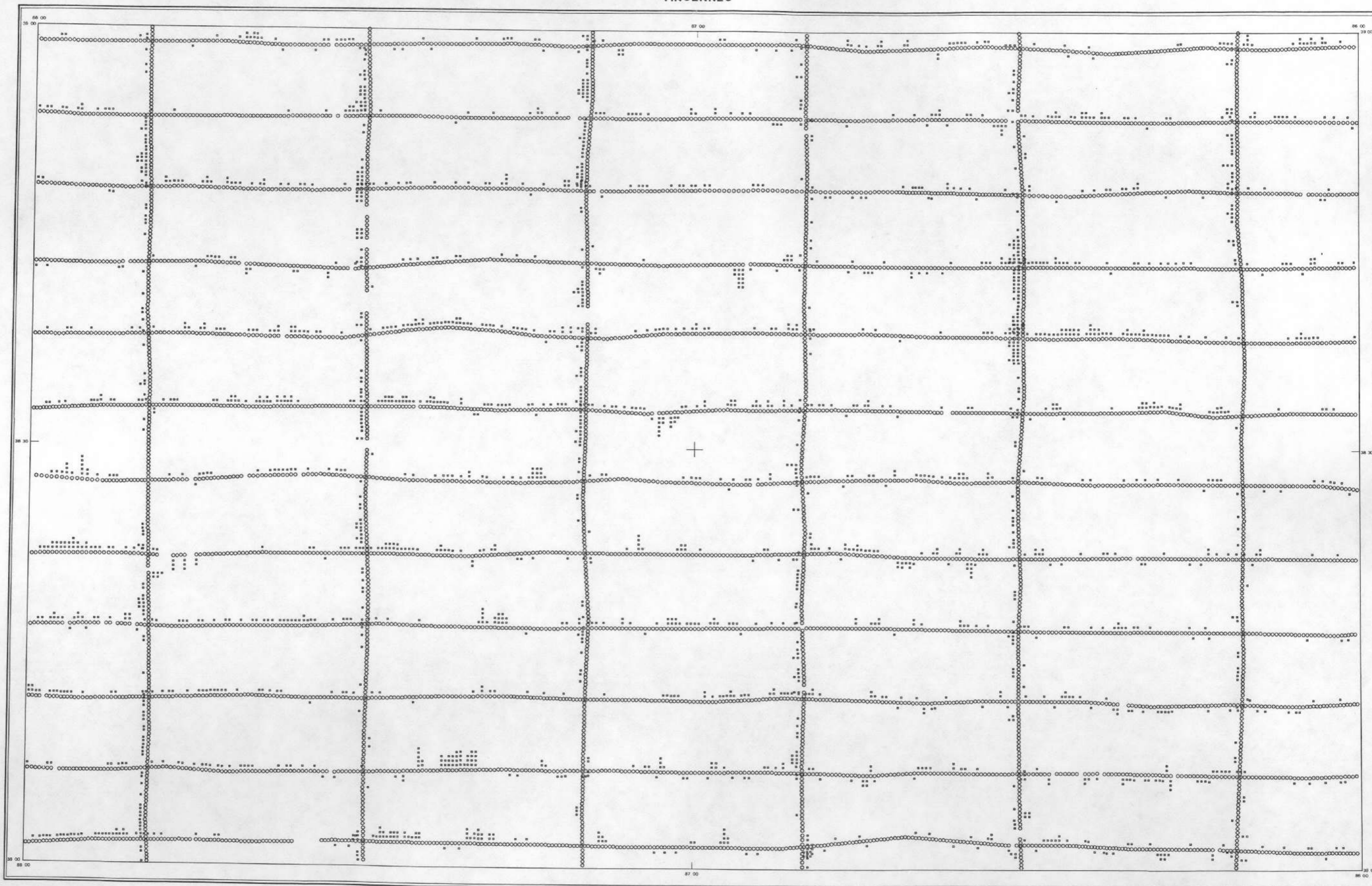
RESIDUAL MAG
 GAMMAS
 MIN -844.7
 MAX -507.1
 MEAN -688.3
 STD DEV 77.24

DIURNAL
 GAMMAS
 MIN 55599
 MAX 55604
 MEAN 55600
 STD DEV 2.322

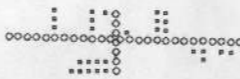
RADAR ALTMTR
 FEET
 MIN 311.3
 MAX 400.4
 MEAN 402.6
 STD DEV 23.78

APPENDIX E - Standard Deviation Maps

VINCENNES



SCALE 1:500,000



○ - DATA STATISTICALLY ADEQUATE
 BLANK - DATA STATISTICALLY INADEQUATE
 ✕ - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY
 NOTE: ON E-W LINES, +σ TO NORTH, -σ TO SOUTH,
 ON N-S LINES, +σ TO WEST, -σ TO EAST.

LOCATION DIAGRAM

IA 151	IA 152	IA 153	IA 154	IA 155	IA 156	IA 157	IA 158	IA 159	IA 160
IA 161	IA 162	IA 163	IA 164	IA 165	IA 166	IA 167	IA 168	IA 169	IA 170
IA 171	IA 172	IA 173	IA 174	IA 175	IA 176	IA 177	IA 178	IA 179	IA 180
IA 181	IA 182	IA 183	IA 184	IA 185	IA 186	IA 187	IA 188	IA 189	IA 190
IA 191	IA 192	IA 193	IA 194	IA 195	IA 196	IA 197	IA 198	IA 199	IA 200

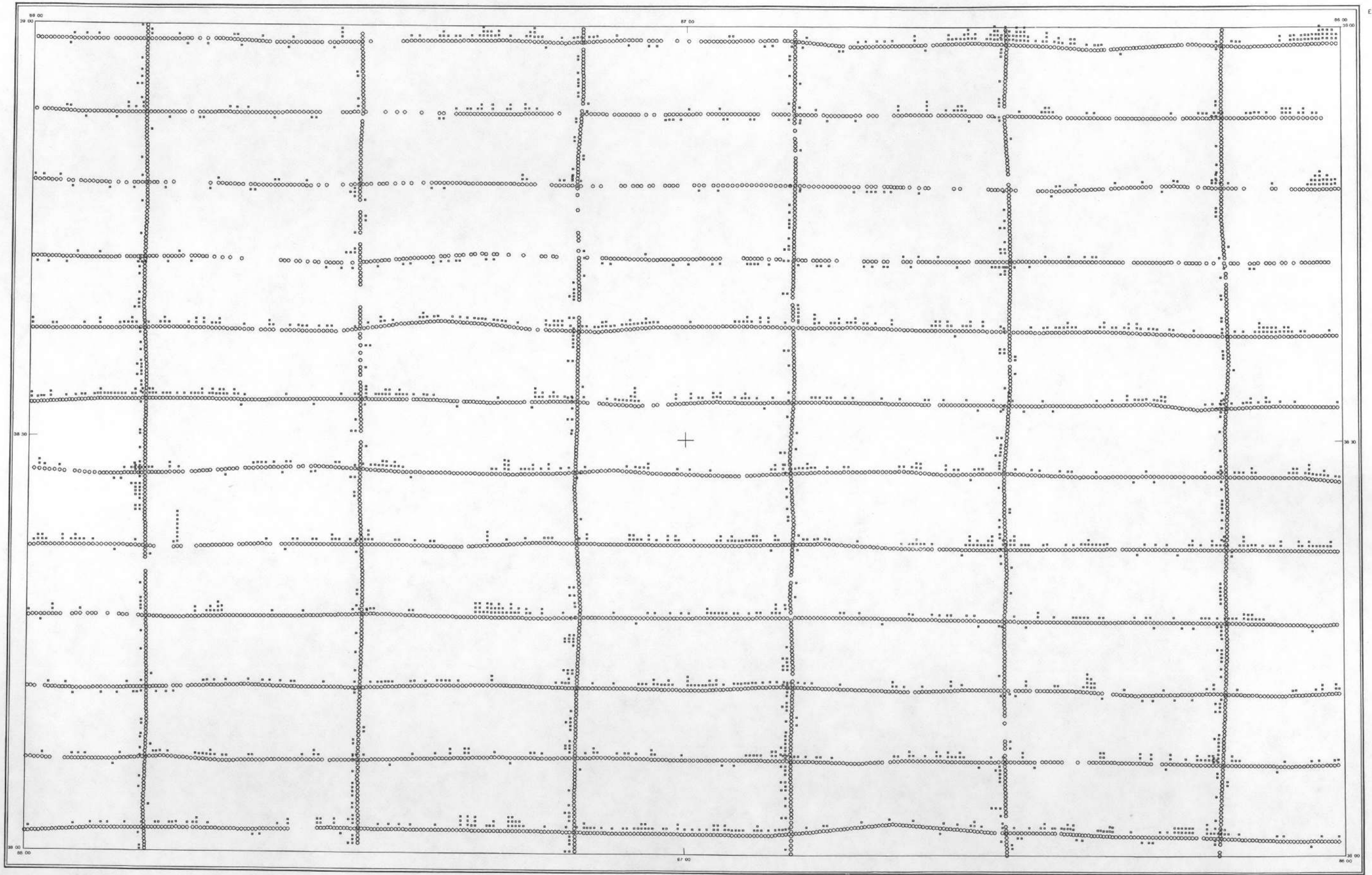
POTASSIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

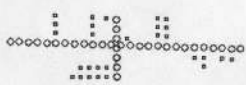
U. S. DEPARTMENT OF ENERGY

SURVEY AND
 COMPILATION BY
EG&G GEOMETRICS

VINCENNES



SCALE 1:500,000



○ - DATA STATISTICALLY ADEQUATE
 ■ - DATA STATISTICALLY INADEQUATE
 + - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY
 NOTE: ON E-W LINES, +σ TO NORTH, -σ TO SOUTH.
 ON N-S LINES, +σ TO WEST, -σ TO EAST.

LOCATION DIAGRAM

INDEPA	NK 1510	NK 1511	NK 1512	NK 1710
NK 1512	NK 1513	NK 1514	NK 1515	NK 1711
NK 1516	NK 1517	NK 1518	NK 1519	NK 1712
NK 1520	NK 1521	NK 1522	NK 1523	NK 1713
NK 1524	NK 1525	NK 1526	NK 1527	NK 1714
NK 1528	NK 1529	NK 1530	NK 1531	NK 1715
NK 1532	NK 1533	NK 1534	NK 1535	NK 1716
NK 1536	NK 1537	NK 1538	NK 1539	NK 1717
NK 1540	NK 1541	NK 1542	NK 1543	NK 1718
NK 1544	NK 1545	NK 1546	NK 1547	NK 1719
NK 1548	NK 1549	NK 1550	NK 1551	NK 1720

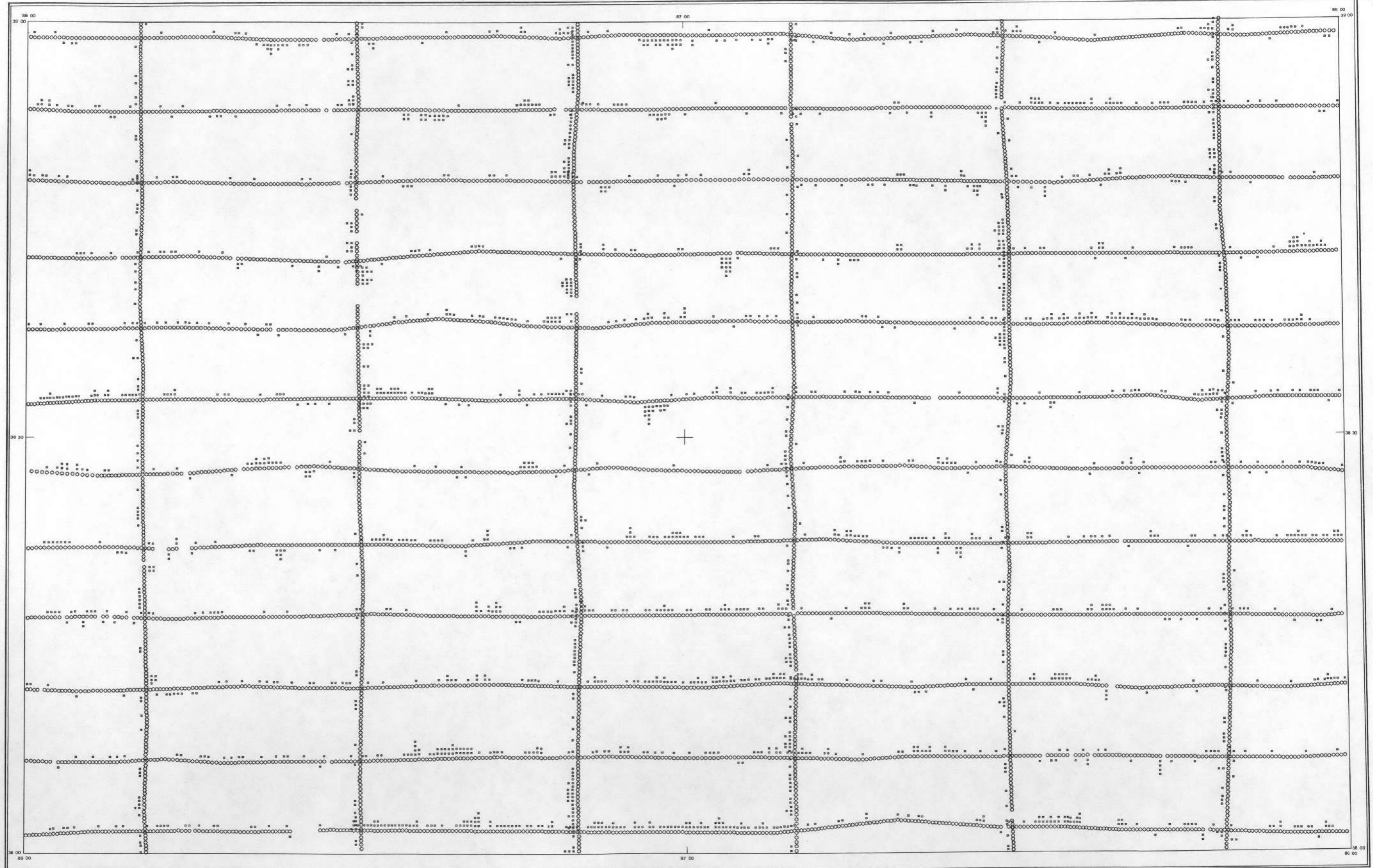
URANIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

U. S. DEPARTMENT OF ENERGY

SURVEY AND
 COMPIATION BY:
 EG&G GEOMETRICS

VINCENNES



SCALE 1:500,000



○ - DATA STATISTICALLY ADEQUATE
 ○ - DATA STATISTICALLY INADEQUATE
 * - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY
 NOTE: ON E-W LINES, +σ TO NORTH, -σ TO SOUTH.
 ON N-S LINES, +σ TO WEST, -σ TO EAST.

LOCATION DIAGRAM

OHIO	MI	IN	IL	MO	AR	MS	AL	GA	NC	VA	MD	DE	PA	NY	CT	RI	MA	NH	VT	ME
15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	17.0	17.1	17.2

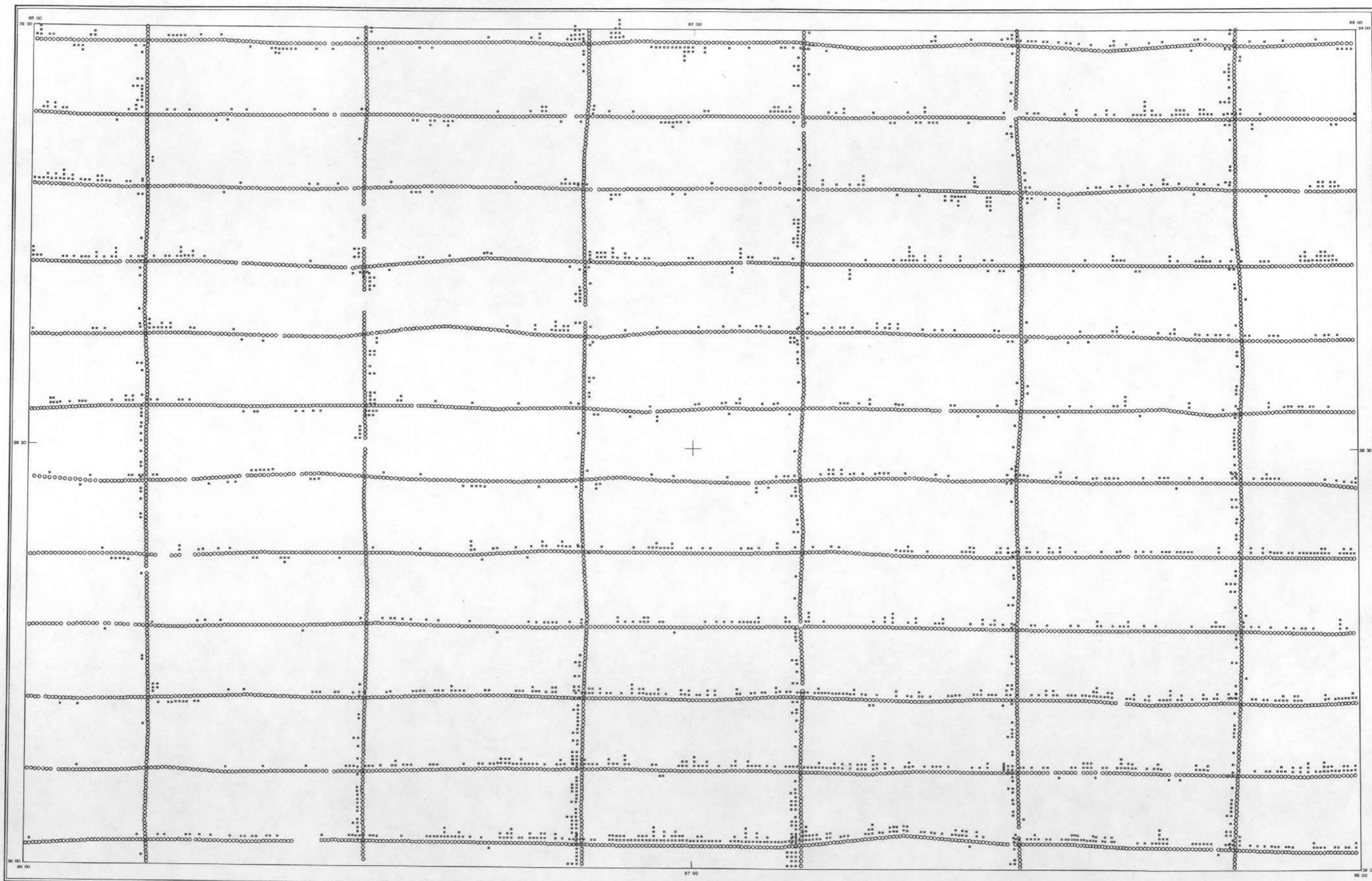
THORIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

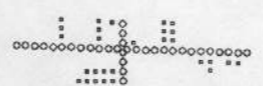
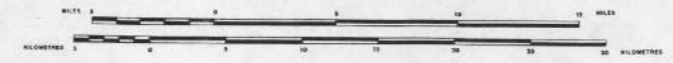
U. S. DEPARTMENT OF ENERGY

SURVEY AND
 COMPILED BY:

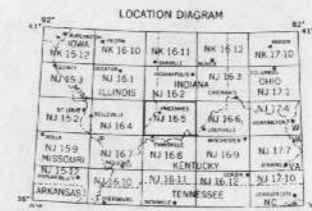
VINCENNES



SCALE 1:500,000



○ - DATA STATISTICALLY ADEQUATE
 ✕ - DATA STATISTICALLY INADEQUATE
 + - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY
 NOTE: ON E-W LINES, ++ TO NORTH, -- TO SOUTH
 ON N-S LINES, ++ TO WEST, -- TO EAST.



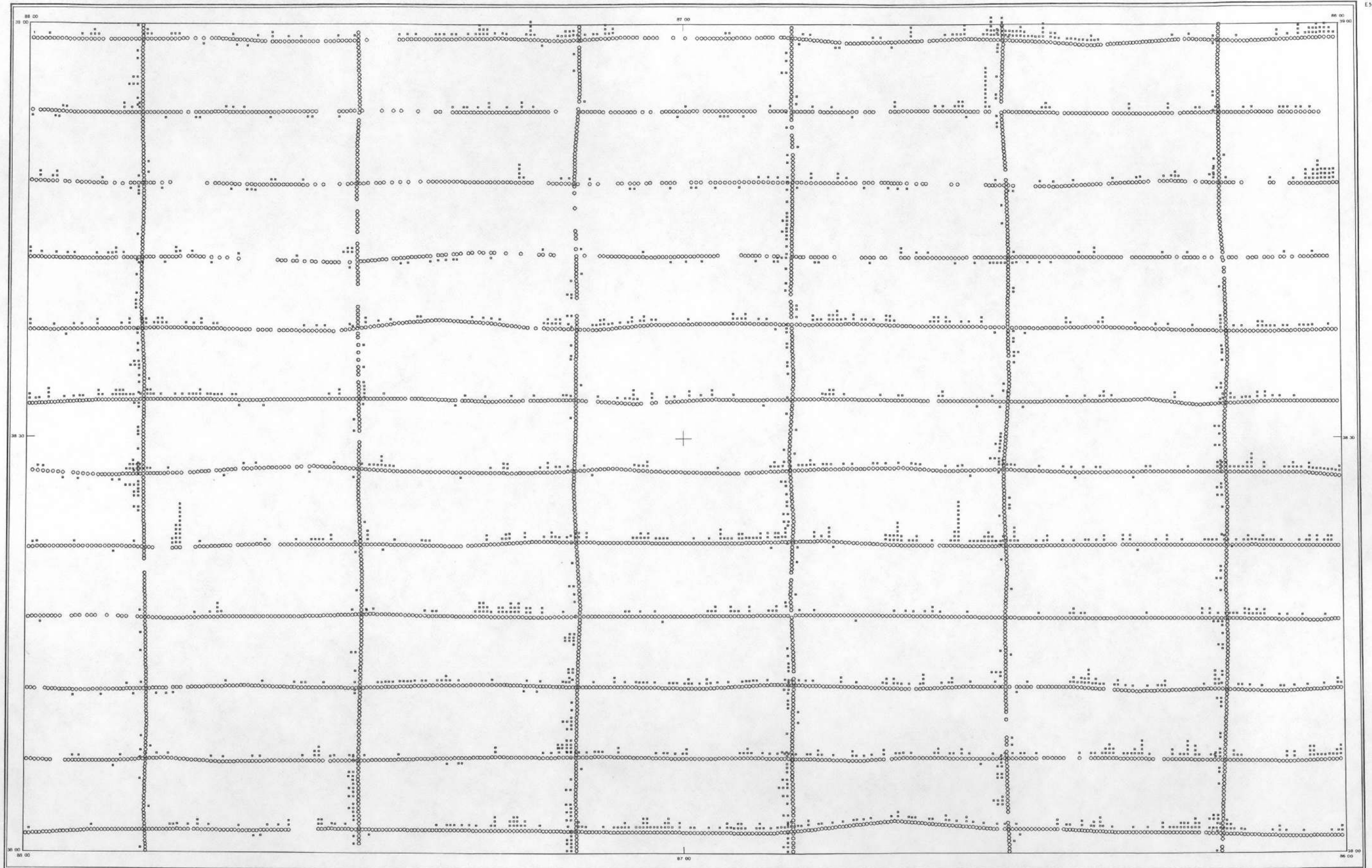
THORIUM/POTASSIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

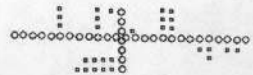
U. S. DEPARTMENT OF ENERGY

SURVEY AND
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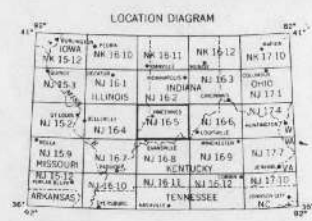
VINCENNES



SCALE 1:500,000



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 BLANK - DATA STATISTICALLY INADEQUATE
 + - 1 σ ABOUT MEASURE OF CENTRAL TENDENCY
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 ON N-S LINES, +σ TO WEST, -σ TO EAST.



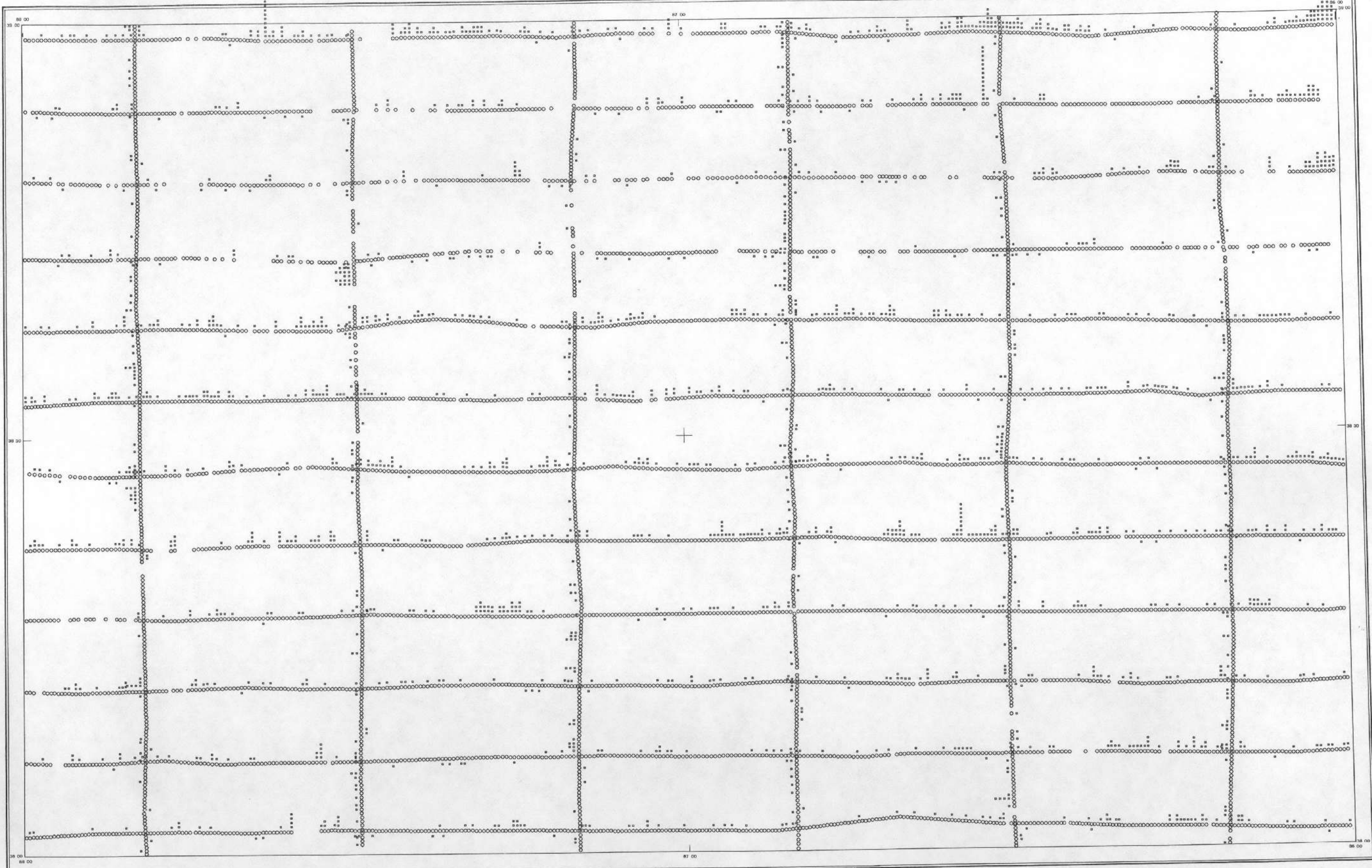
URANIUM/POTASSIUM STANDARD DEVIATION MAP

GREAT LAKES PROJECT

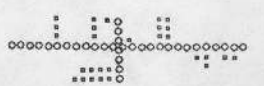
U. S. DEPARTMENT OF ENERGY

SURVEY AND
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 EG&G GEOMETRICS

VINCENNES



SCALE 1:500,000



○ - DATA STATISTICALLY ADEQUATE
BLANK - DATA STATISTICALLY INADEQUATE
+ - MEASURE OF CENTRAL TENDENCY
NOTE: ON E-W LINES, ++ TO NORTH, -- TO SOUTH.
ON N-S LINES, ++ TO WEST, -- TO EAST.

LOCATION DIAGRAM

IL	IN	IND	IA	MI	OH	PA
NY 15.1	NY 15.2	NY 15.3	NY 15.4	NY 15.5	NY 15.6	NY 15.7
NY 15.8	NY 15.9	NY 16.0	NY 16.1	NY 16.2	NY 16.3	NY 16.4
NY 16.5	NY 16.6	NY 16.7	NY 16.8	NY 16.9	NY 17.0	NY 17.1
NY 17.2	NY 17.3	NY 17.4	NY 17.5	NY 17.6	NY 17.7	NY 17.8
NY 17.9	NY 18.0	NY 18.1	NY 18.2	NY 18.3	NY 18.4	NY 18.5
NY 18.6	NY 18.7	NY 18.8	NY 18.9	NY 19.0	NY 19.1	NY 19.2
NY 19.3	NY 19.4	NY 19.5	NY 19.6	NY 19.7	NY 19.8	NY 19.9
NY 20.0	NY 20.1	NY 20.2	NY 20.3	NY 20.4	NY 20.5	NY 20.6
NY 20.7	NY 20.8	NY 20.9	NY 21.0	NY 21.1	NY 21.2	NY 21.3
NY 21.4	NY 21.5	NY 21.6	NY 21.7	NY 21.8	NY 21.9	NY 22.0

URANIUM/THORIUM STANDARD DEVIATION MAP

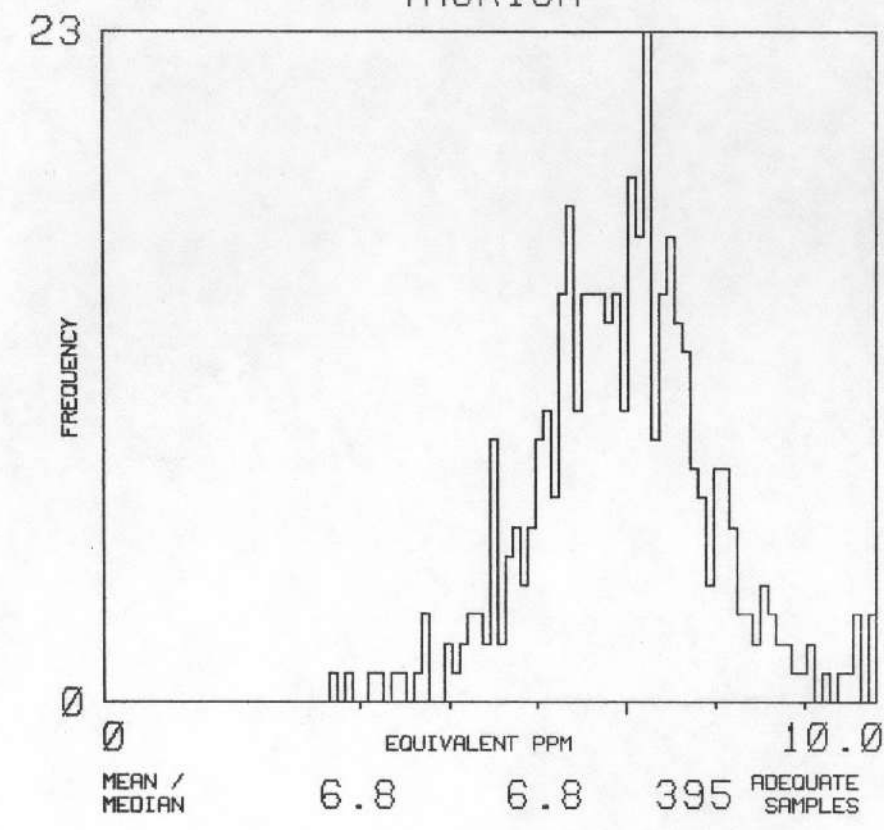
GREAT LAKES PROJECT

U. S. DEPARTMENT OF ENERGY

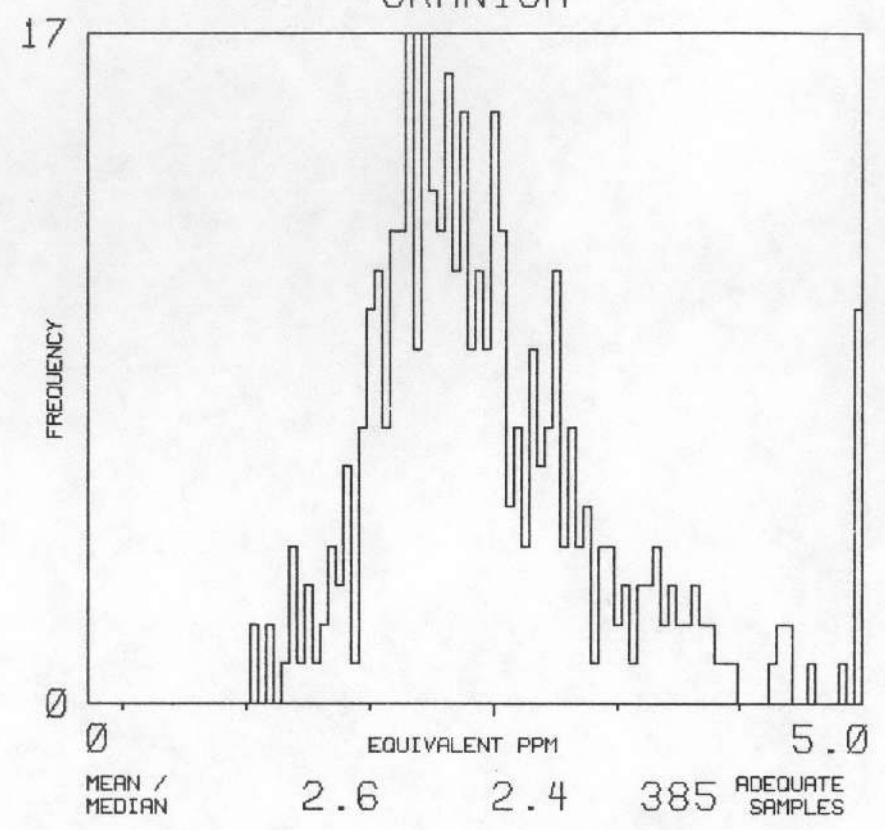
SURVEY AND COMPIATION BY:
EG&G GEOMETRICS

**APPENDIX F - Histograms and Map Unit Conversion
Table**

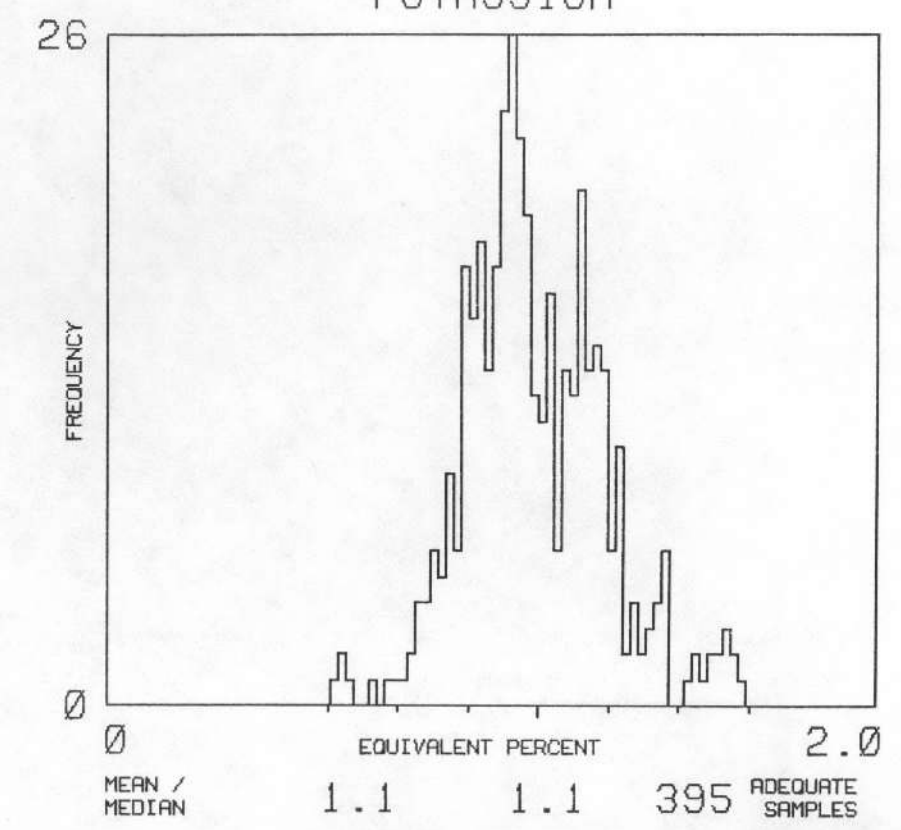
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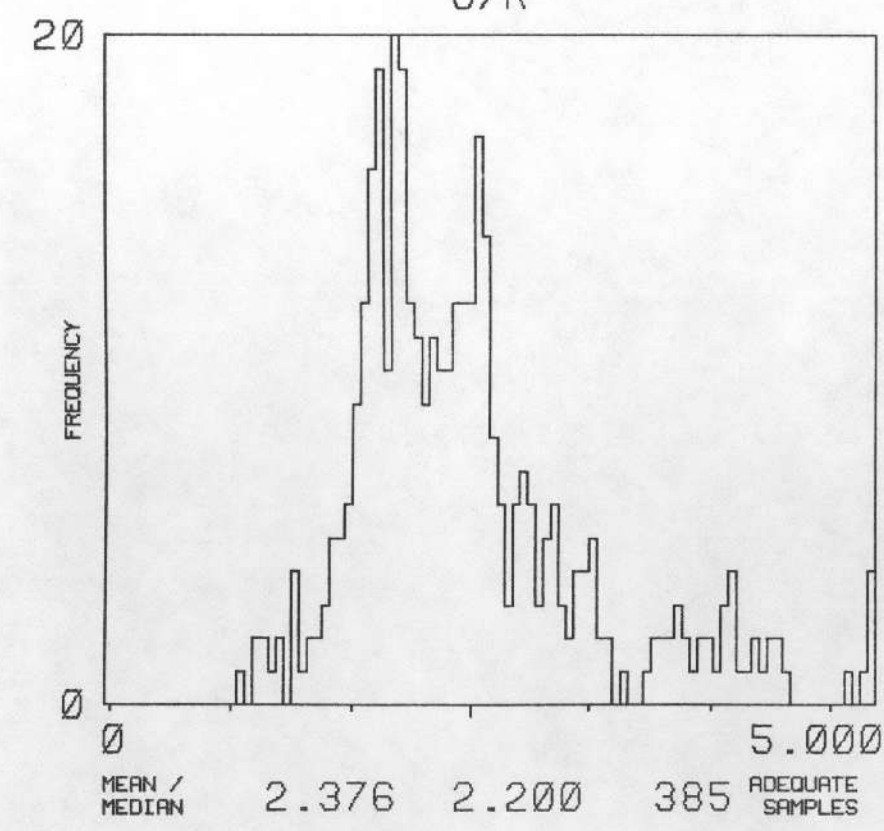
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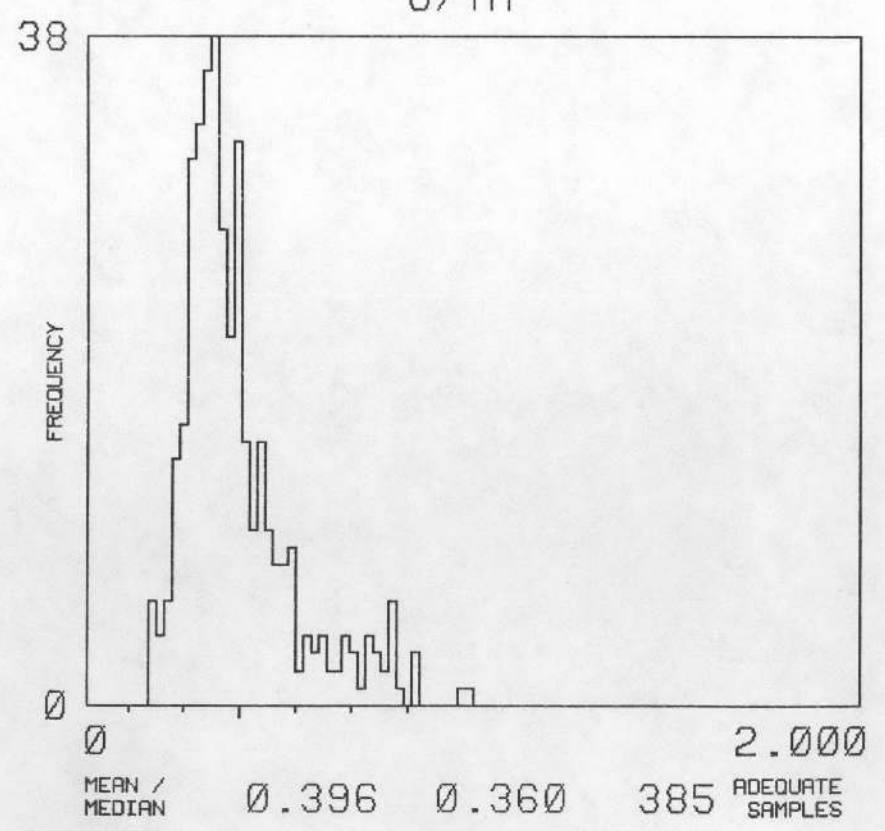
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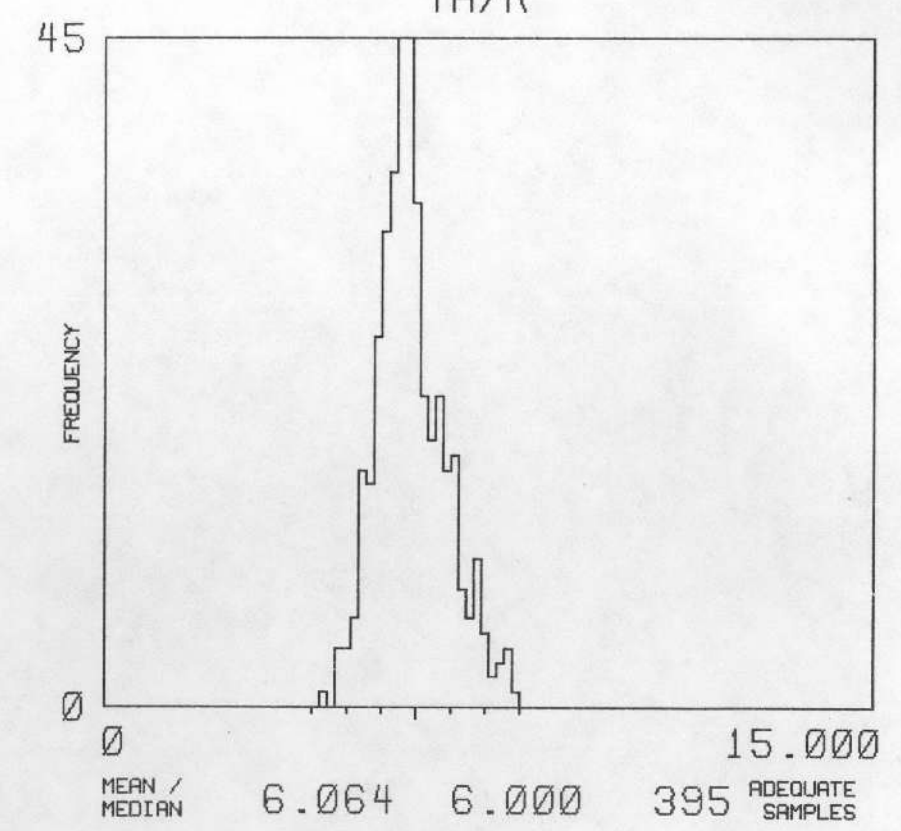
U/K



U/TH



TH/K

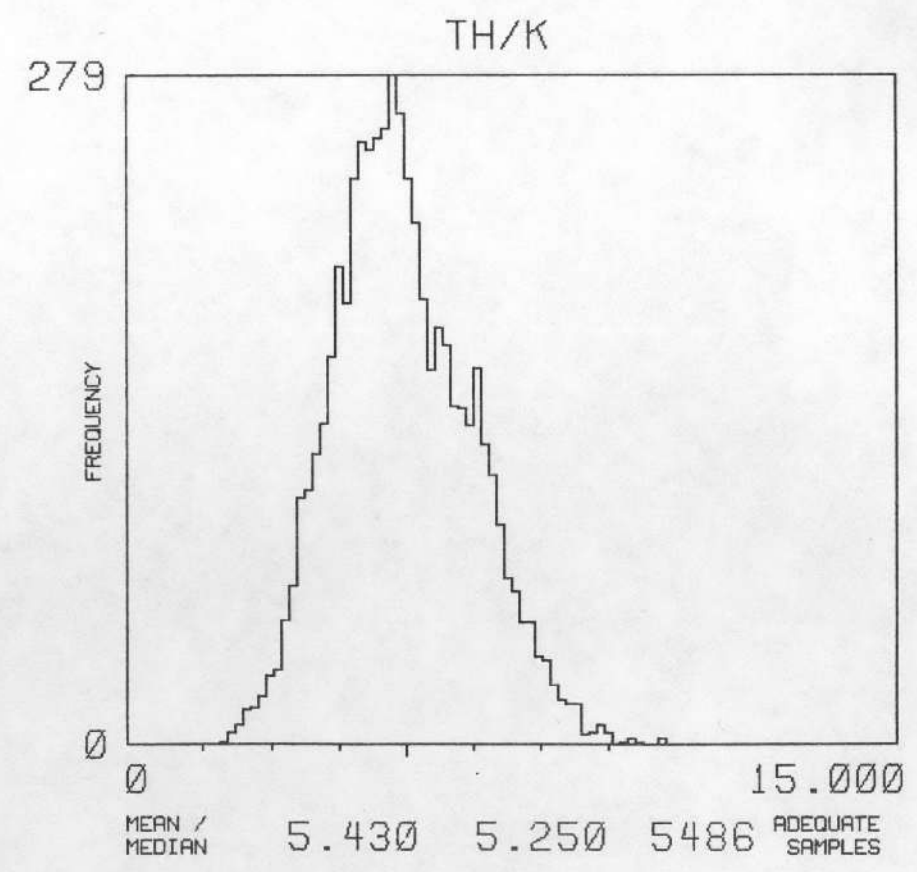
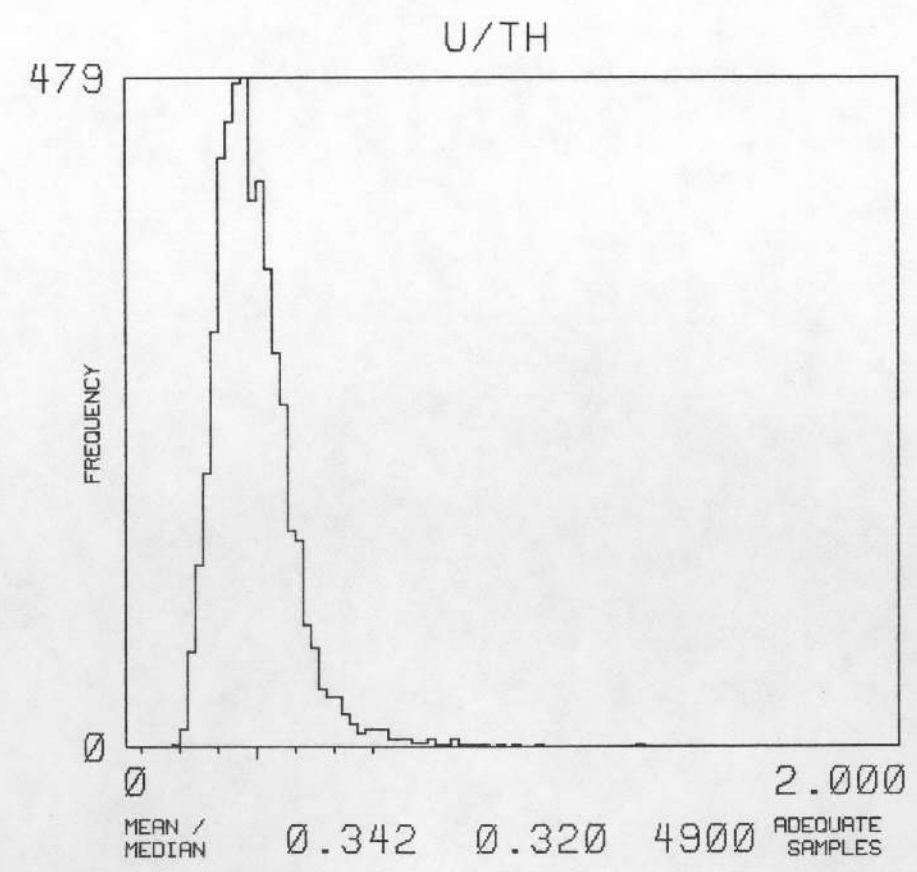
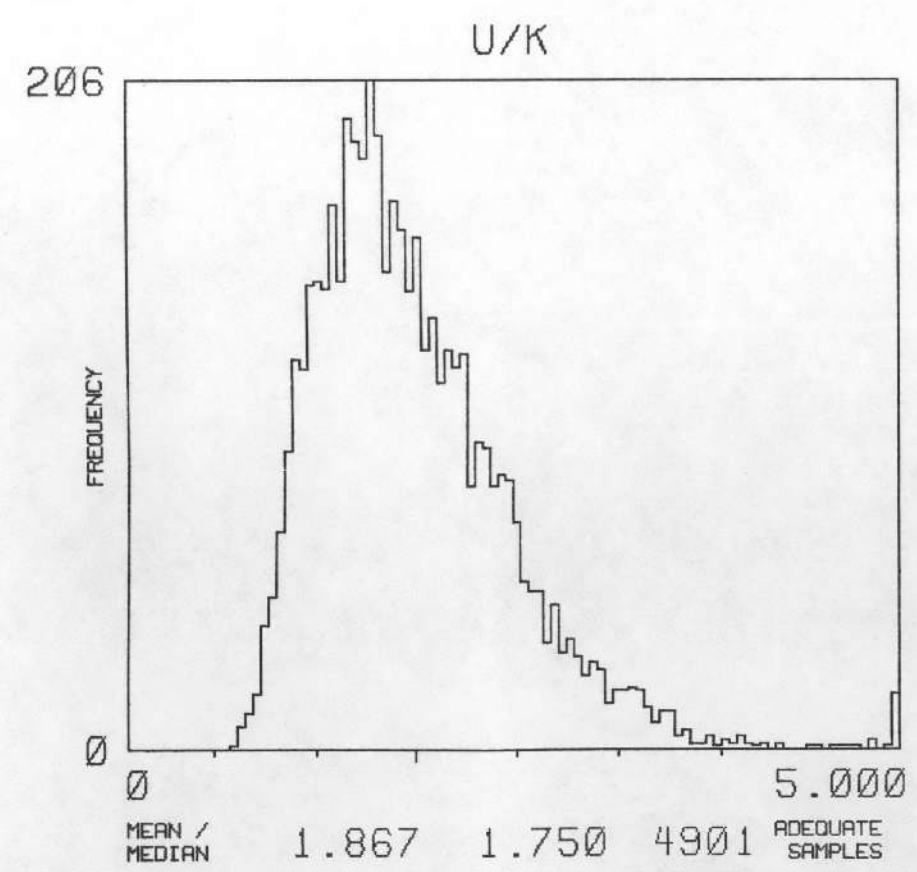
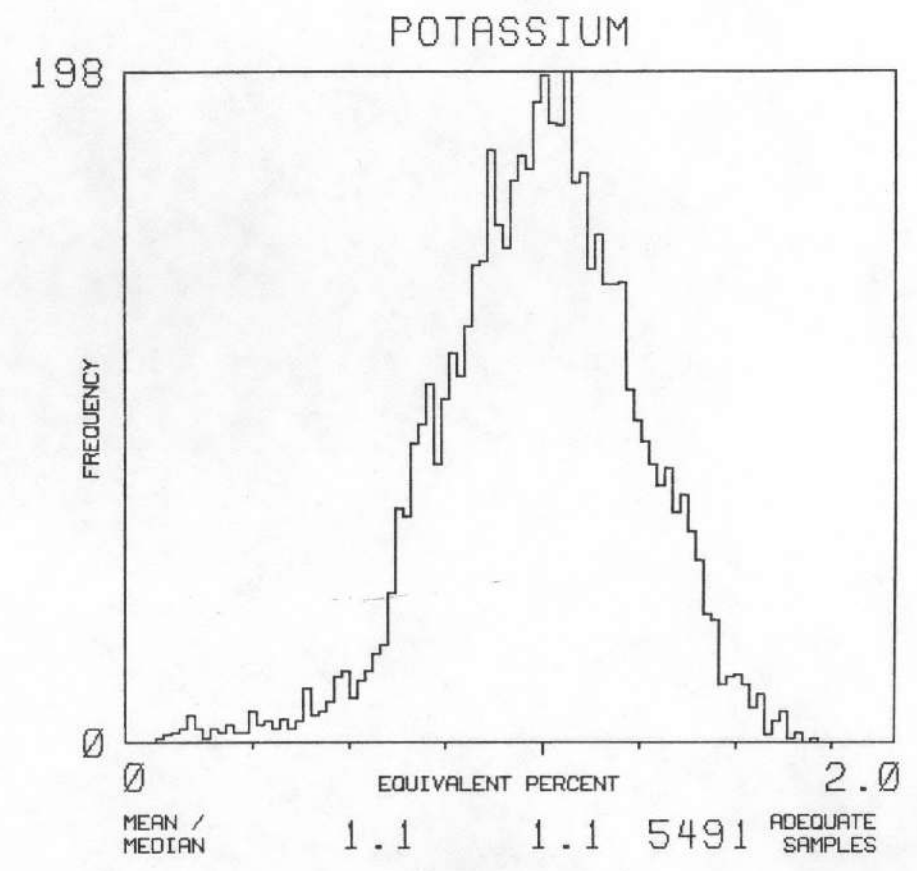
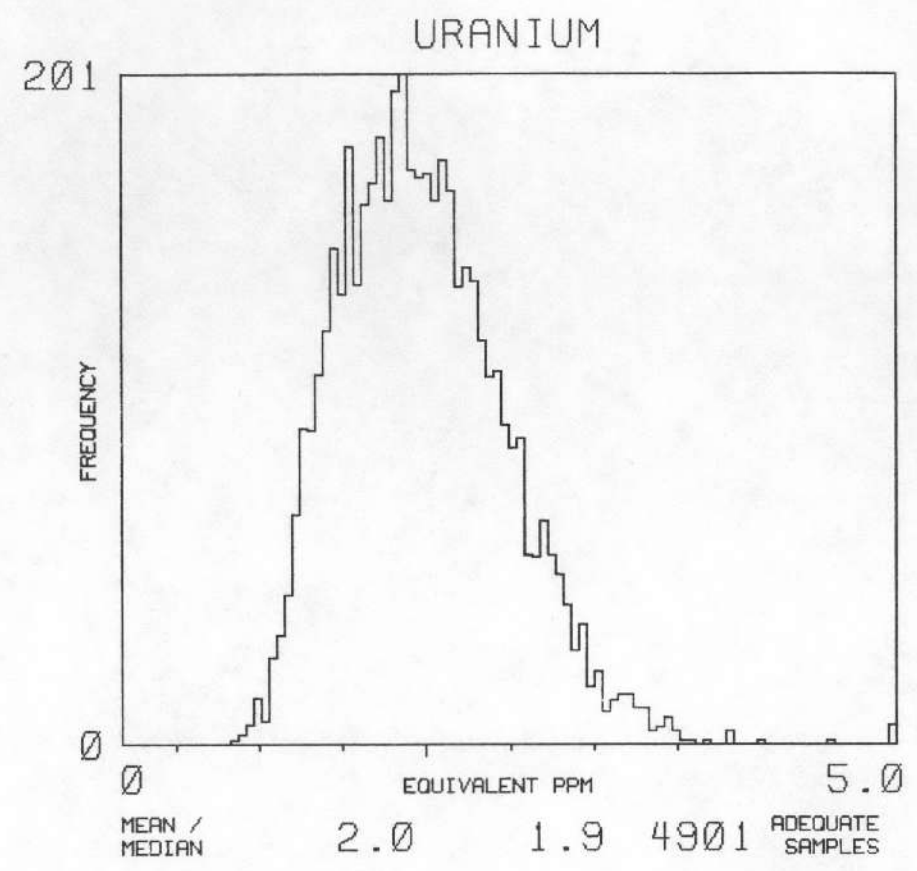
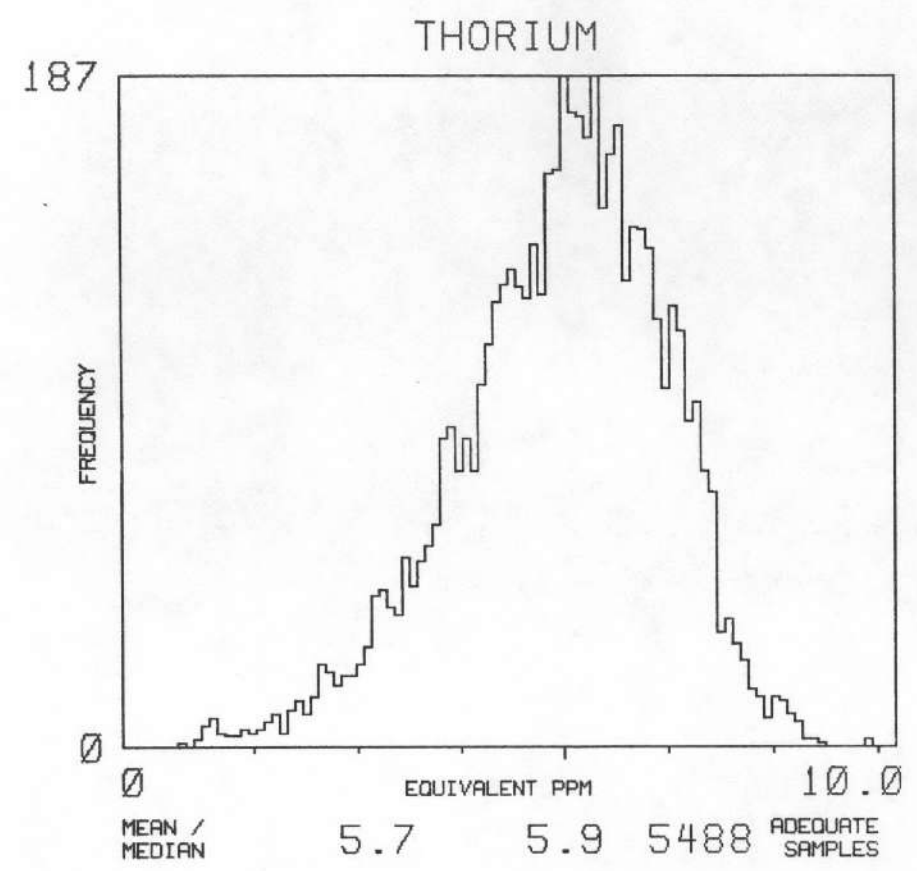


NJ 16-5

VINCENNES

MAP UNIT : QC

TOTAL NUMBER OF SAMPLES 5509



NJ 16-5

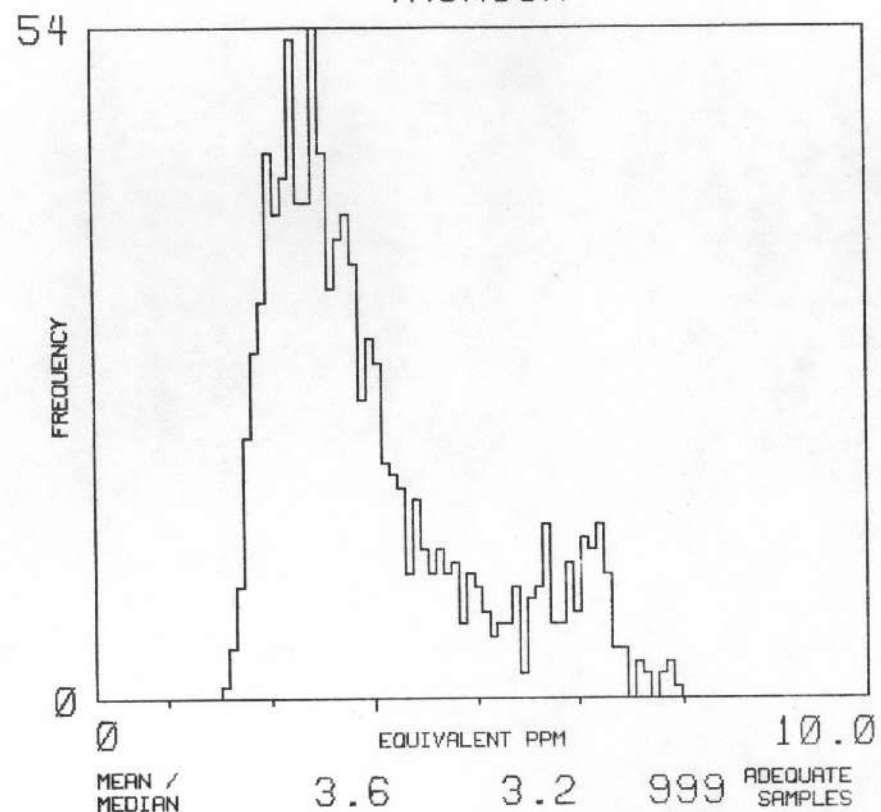
VINCENNES

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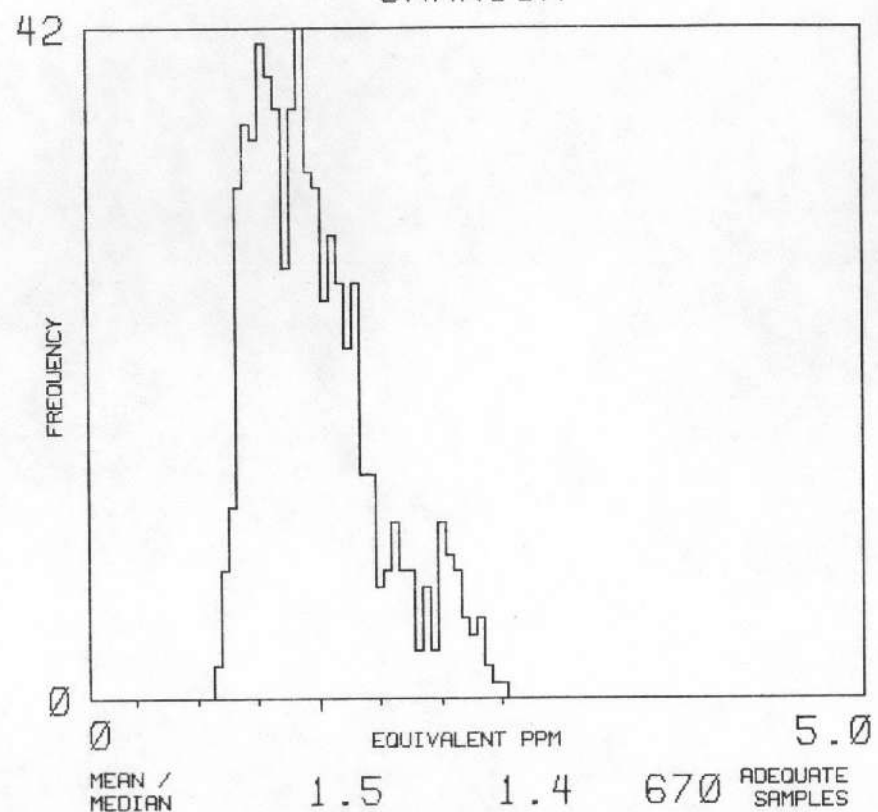
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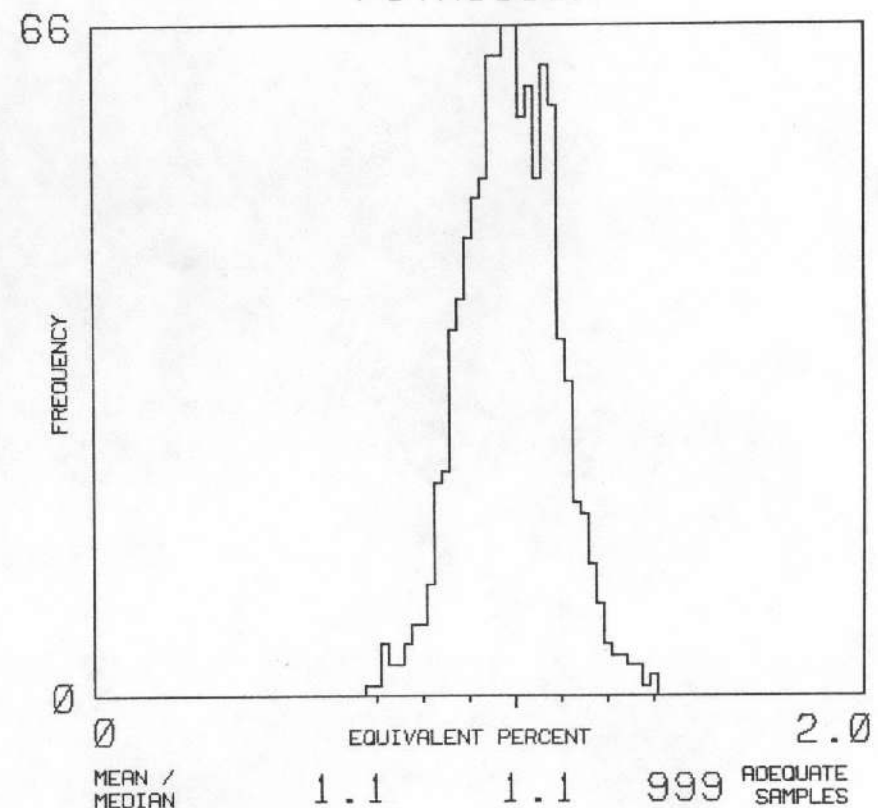
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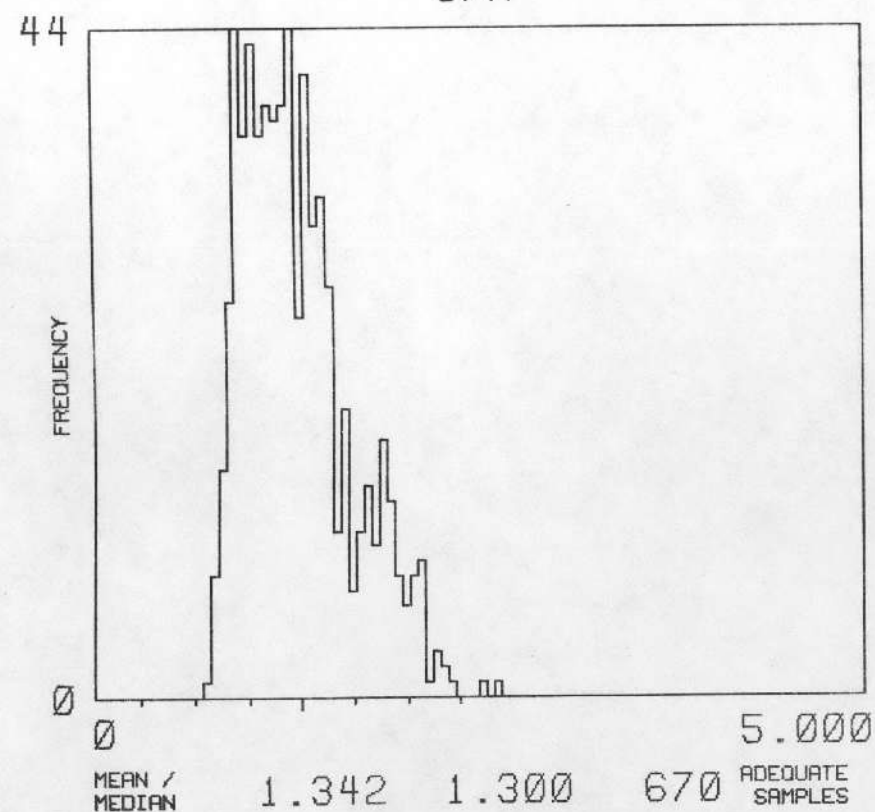
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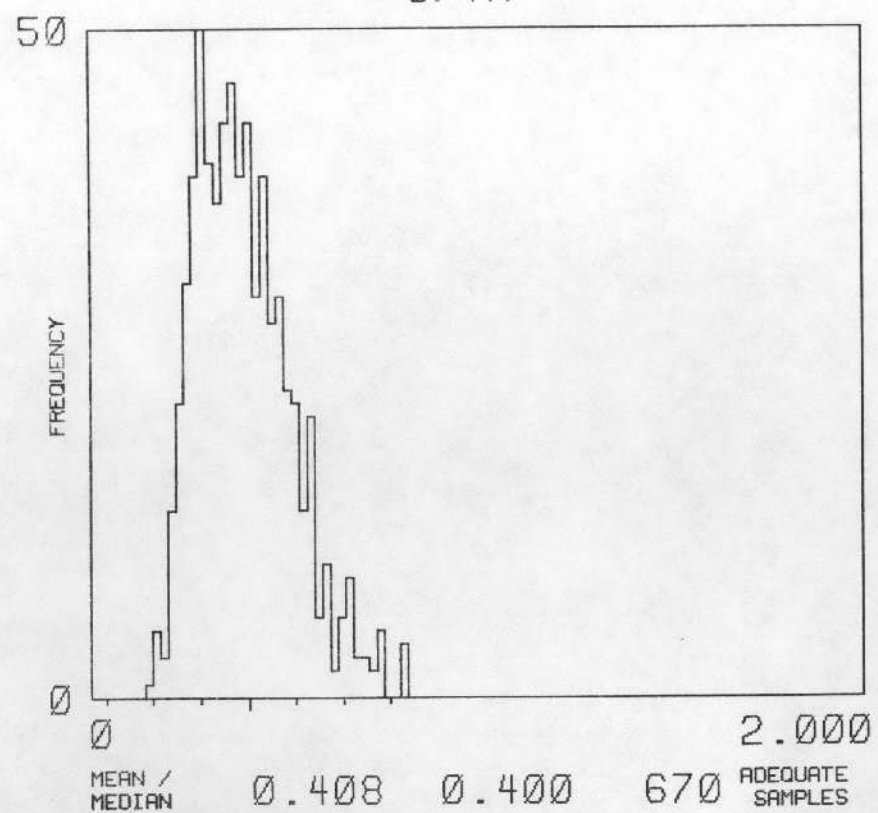
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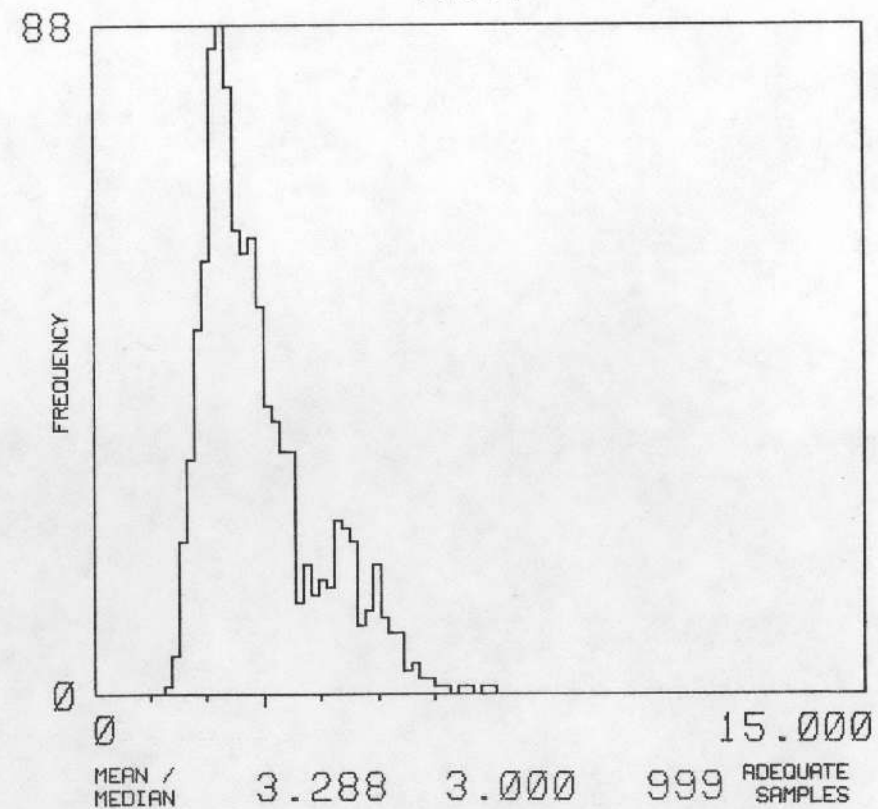
U/K



U/TH



TH/K

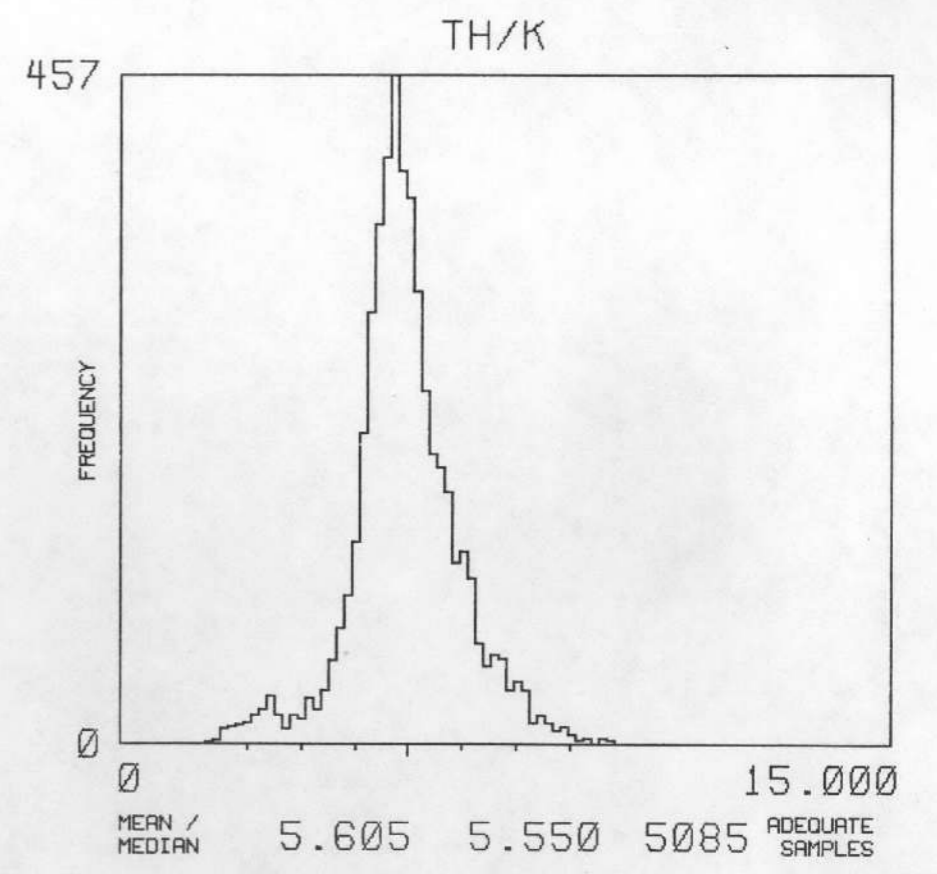
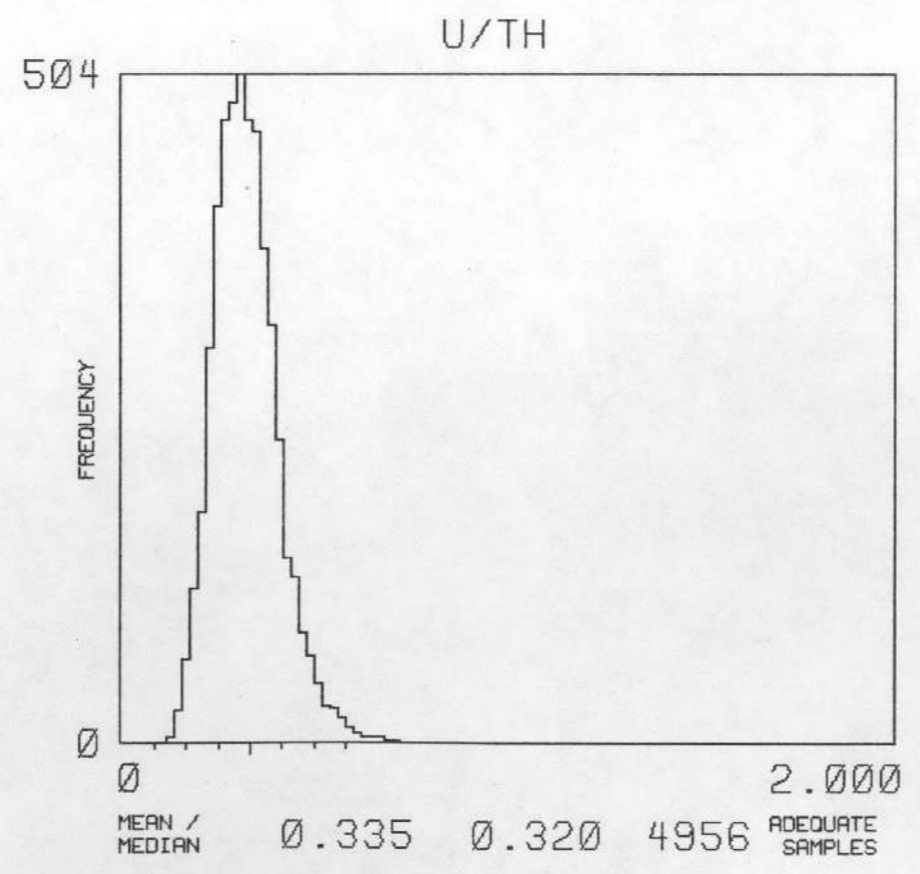
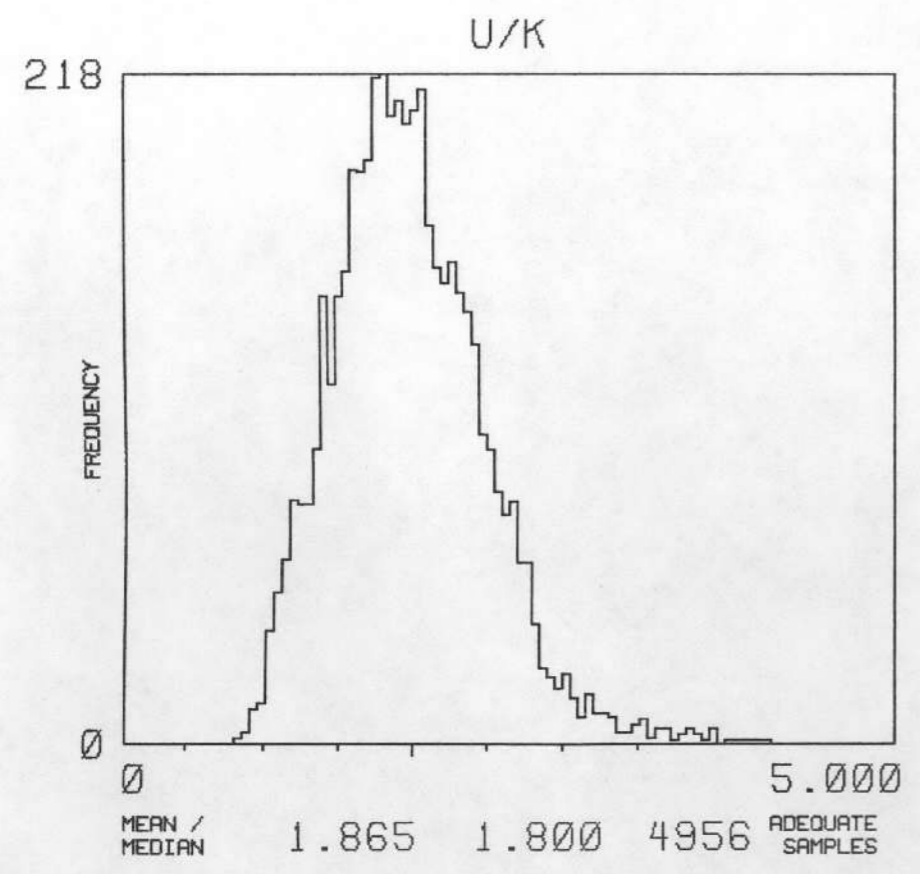
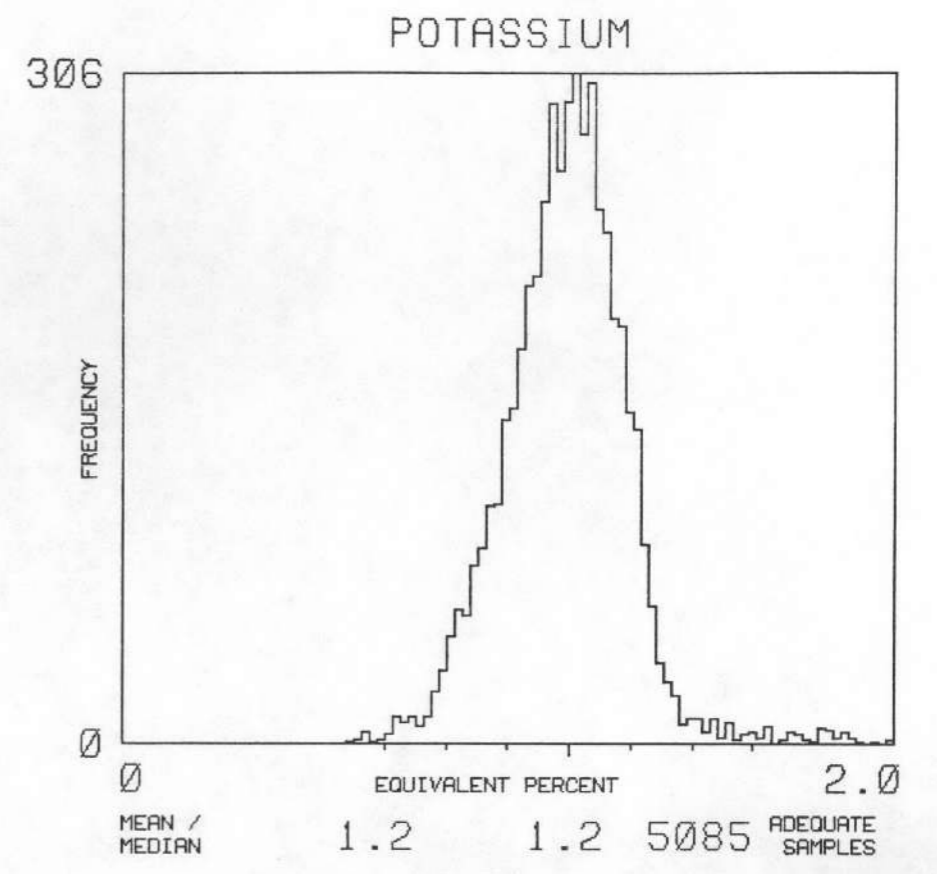
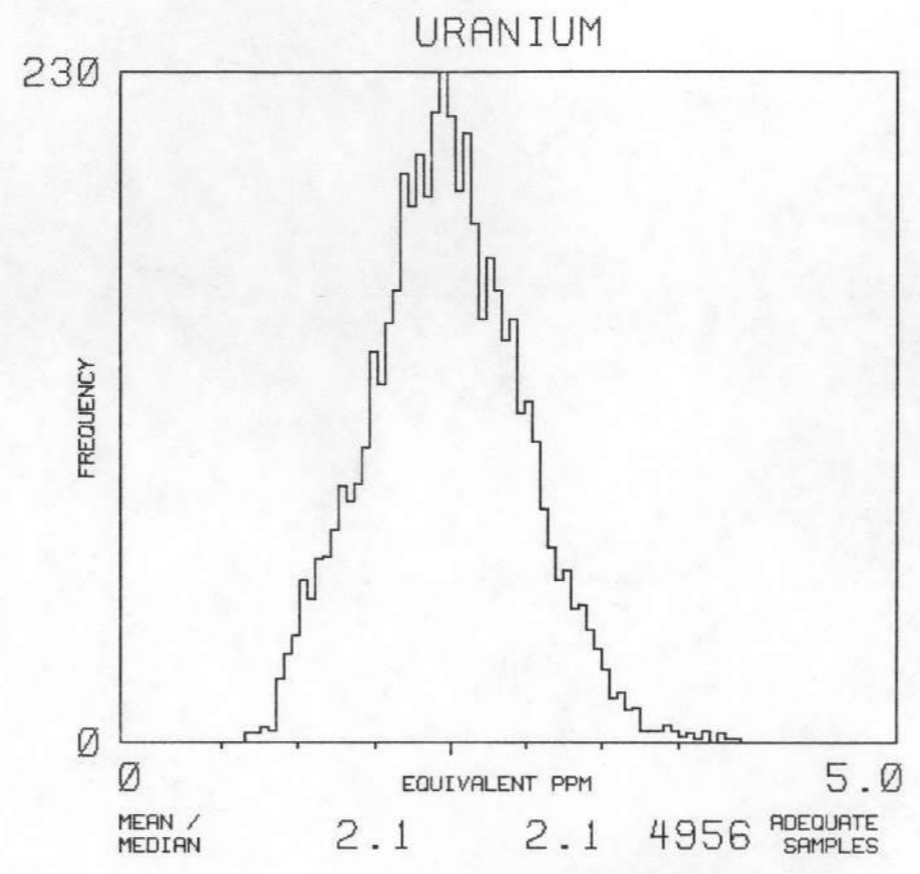
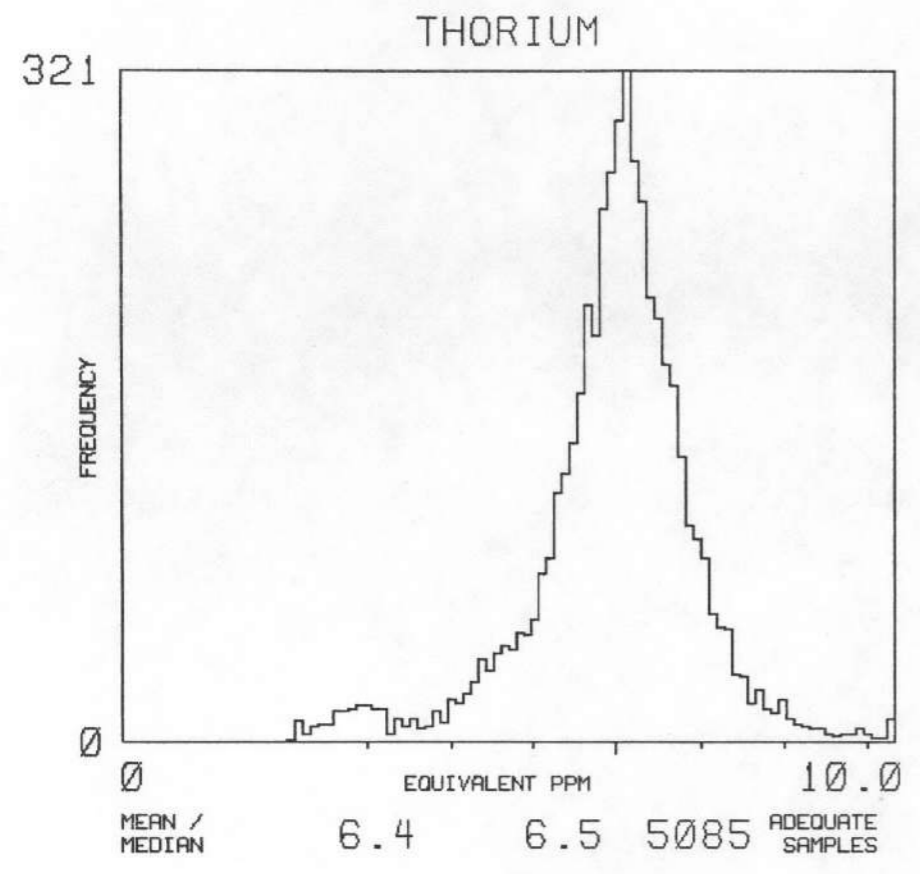


NJ 16-5

VINCENNES

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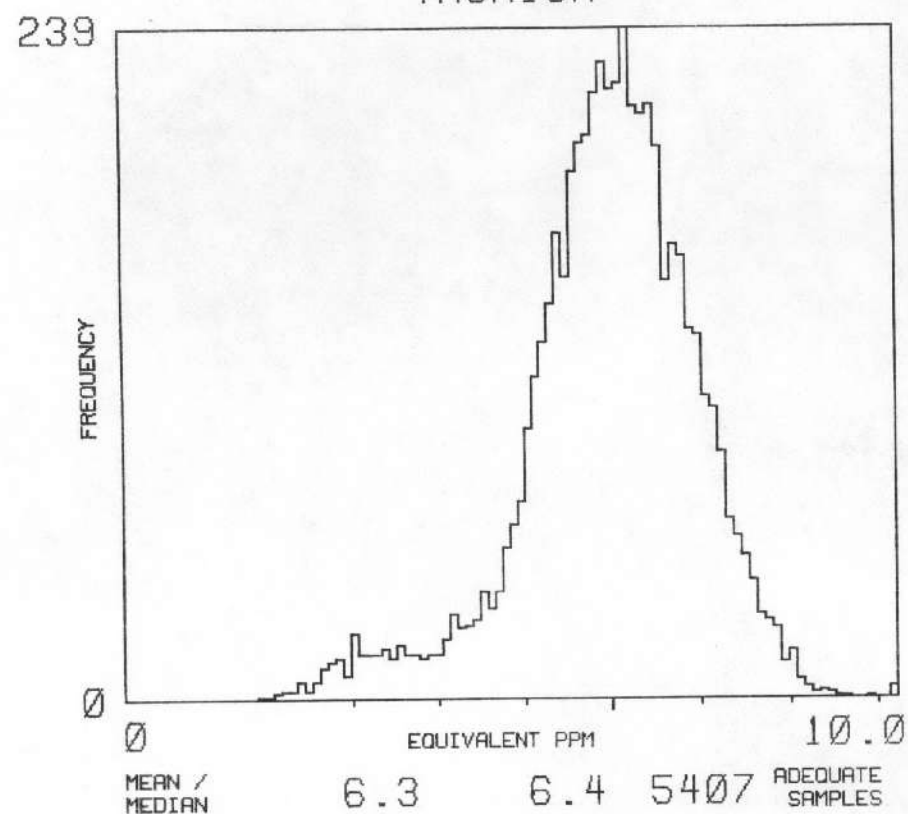
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VINCENNES

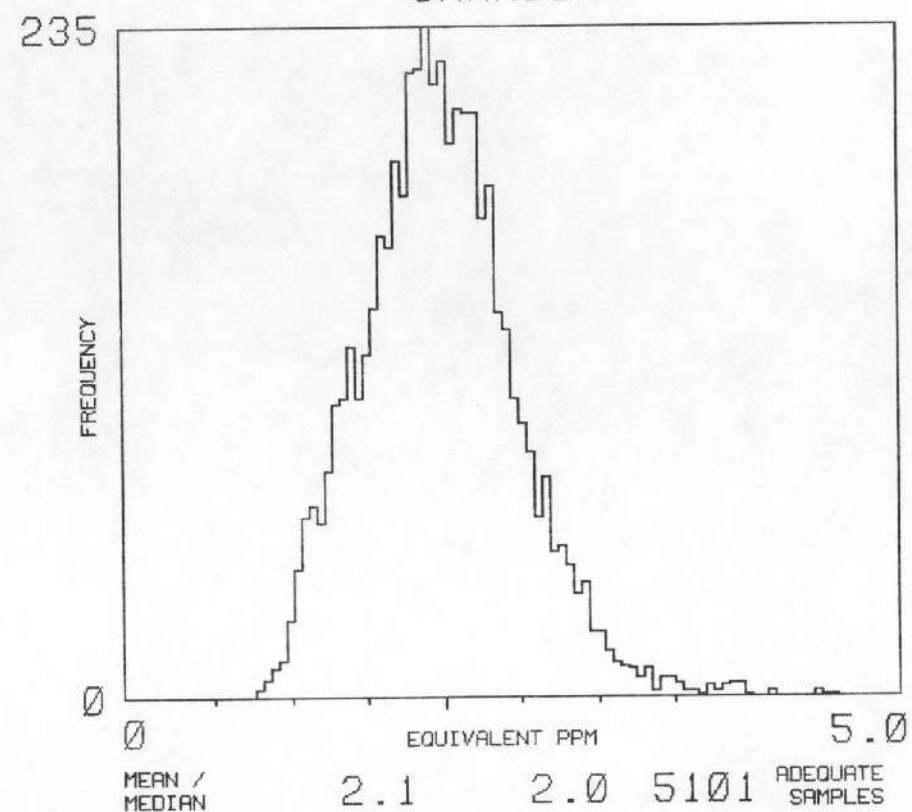
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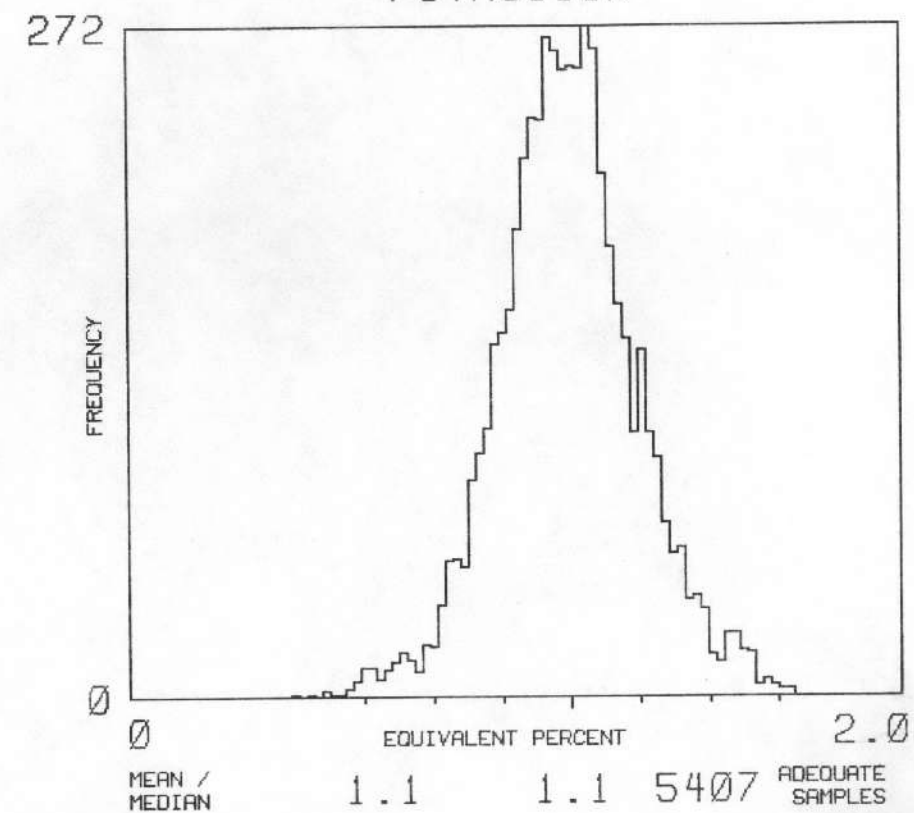
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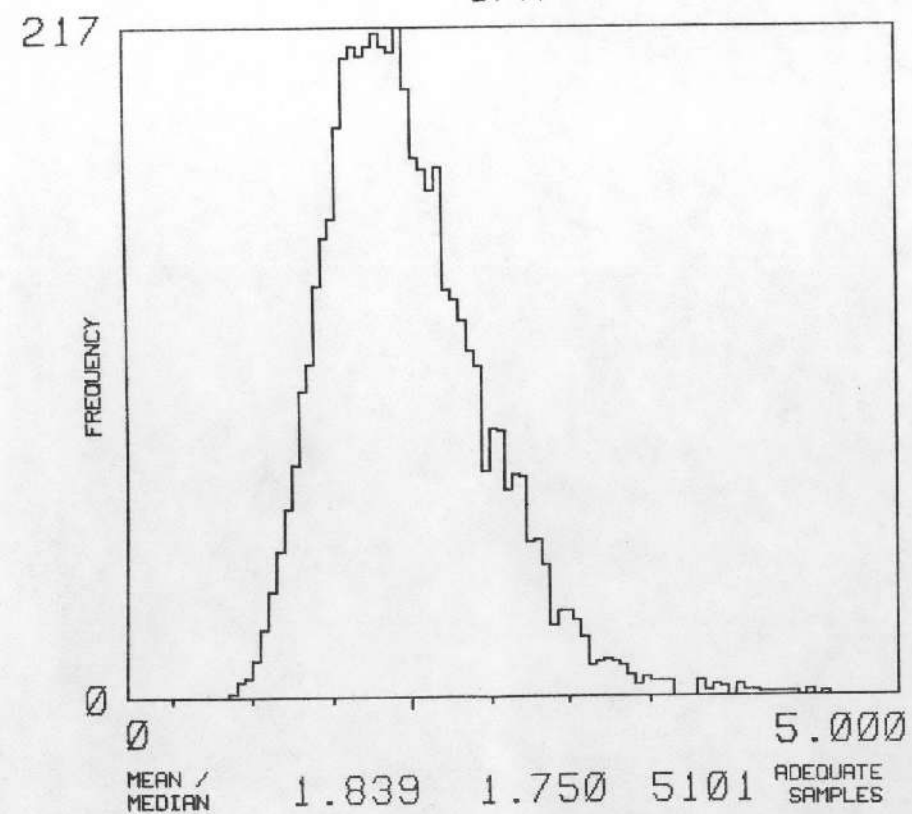
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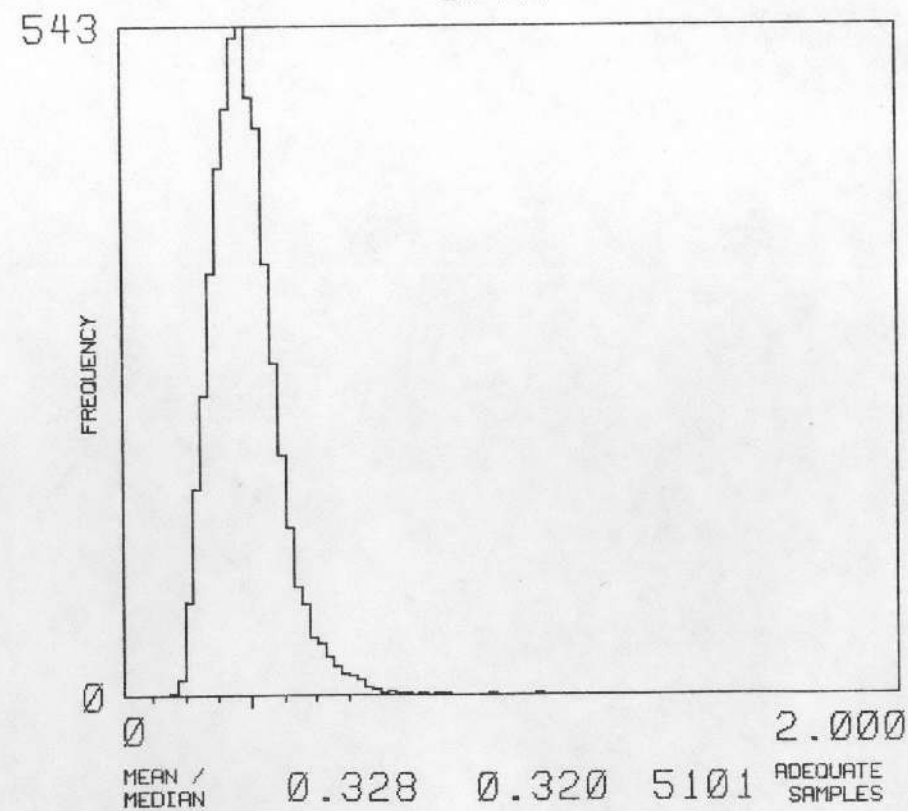
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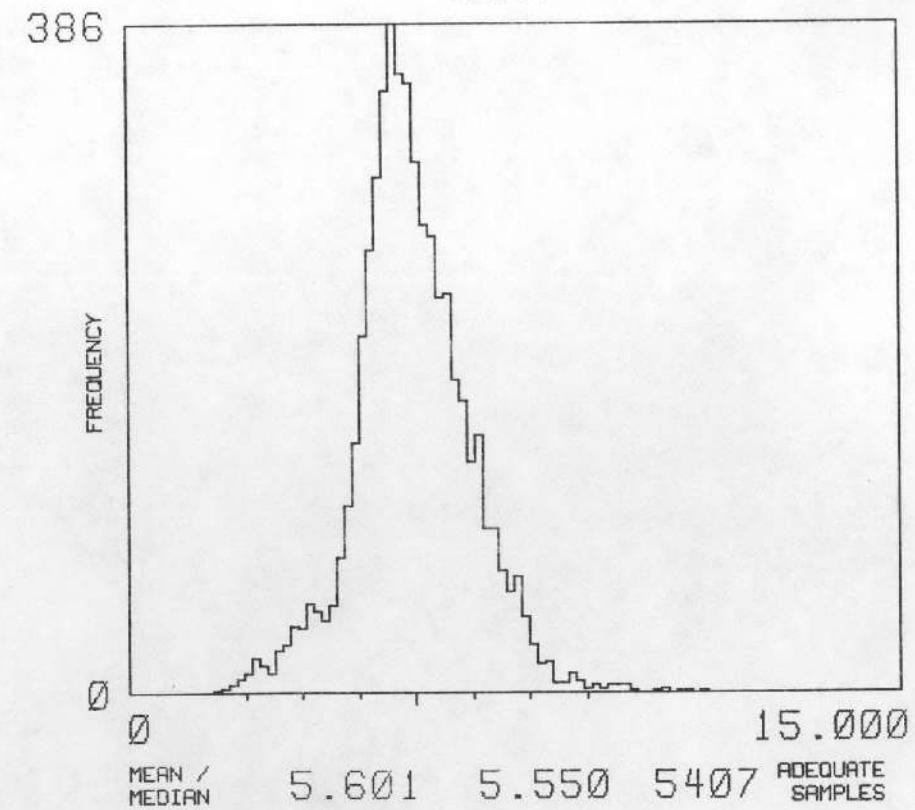
U/K



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TH/K



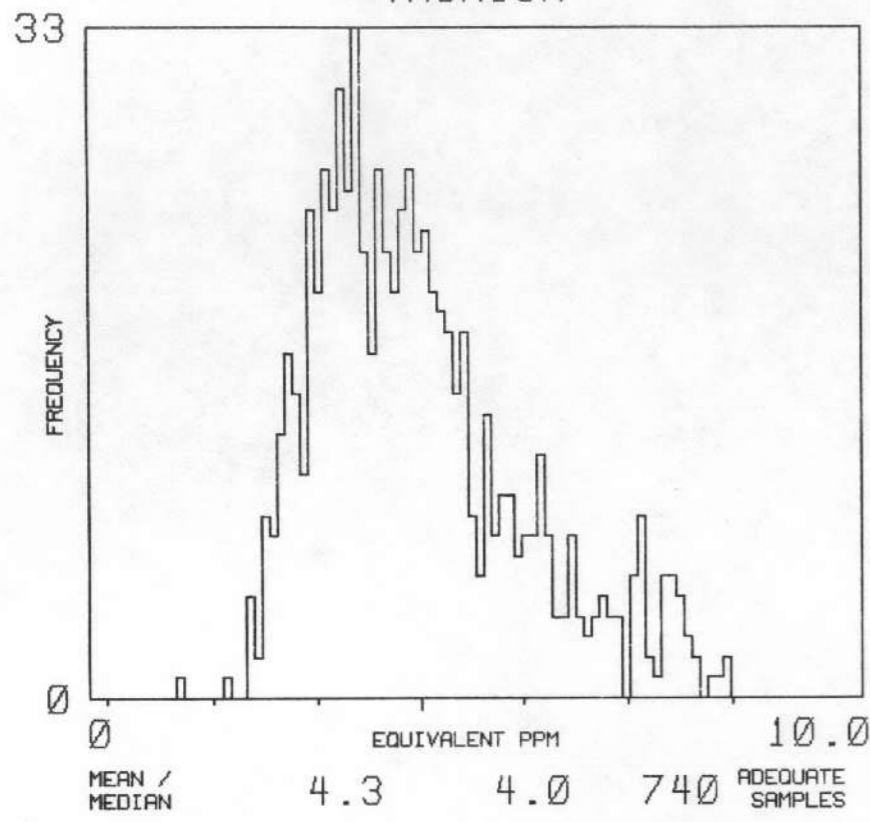
NJ 16-5

VINCENNES

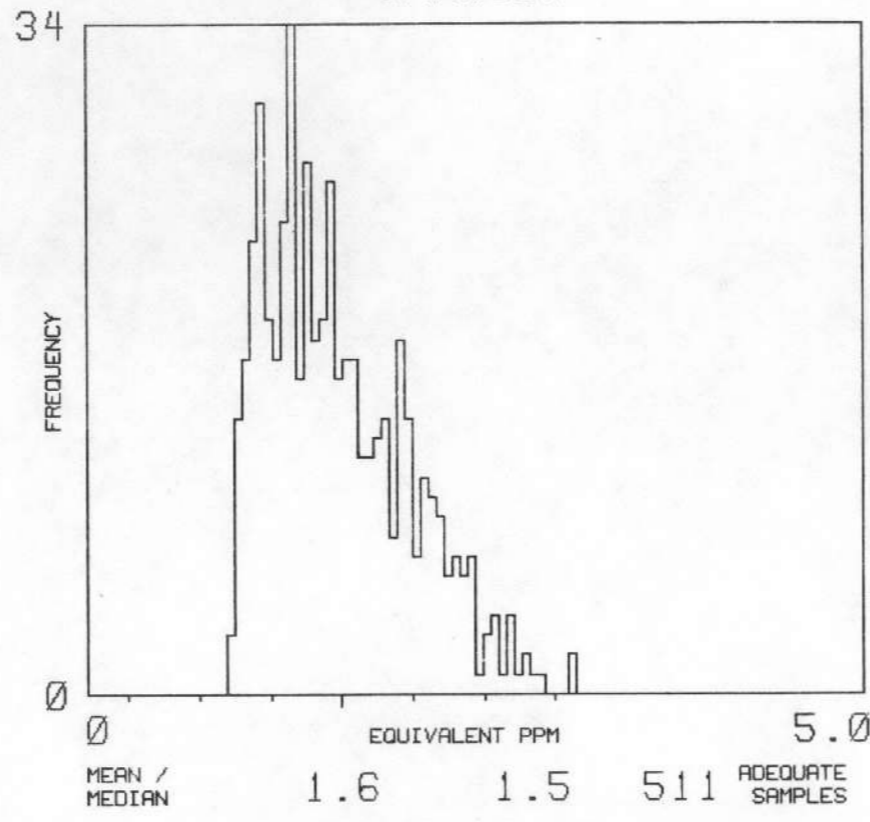
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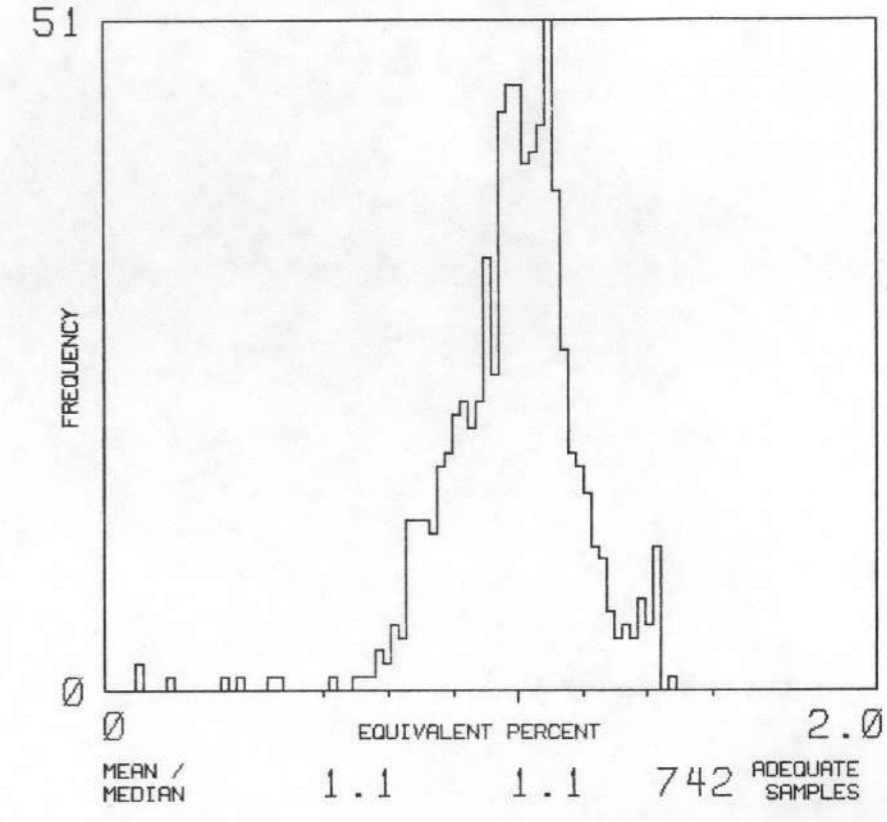
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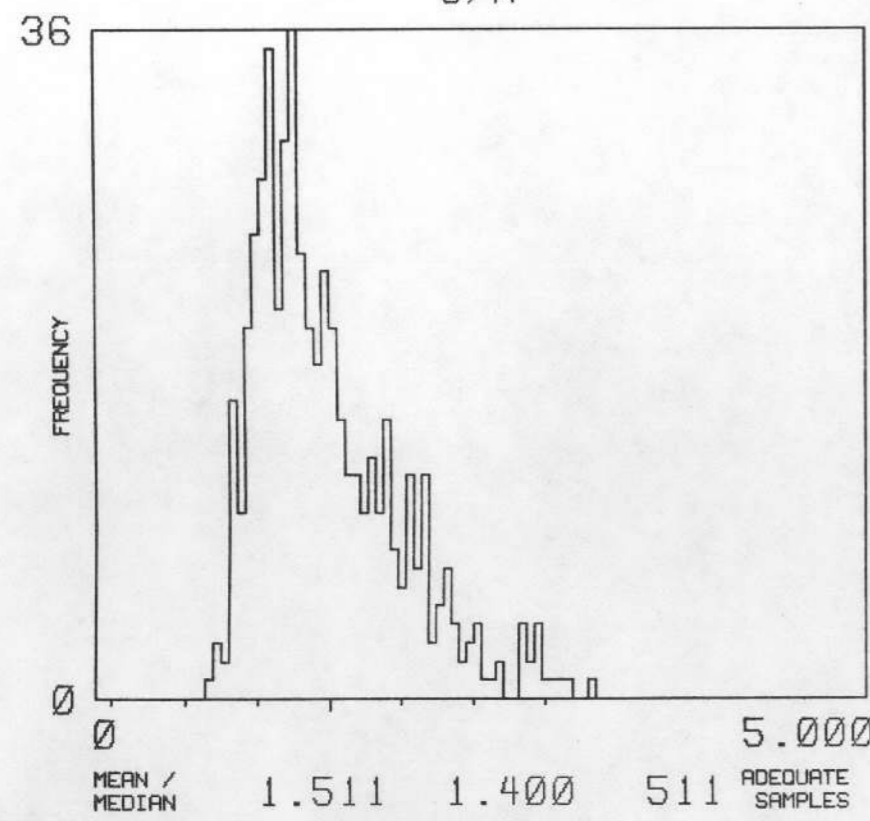
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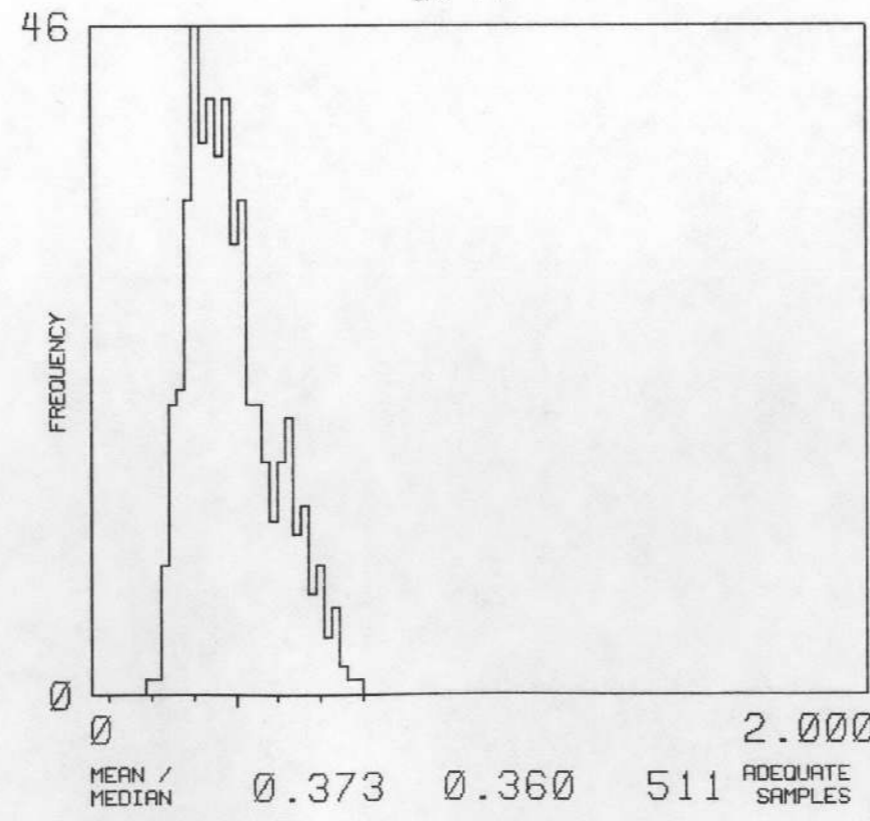
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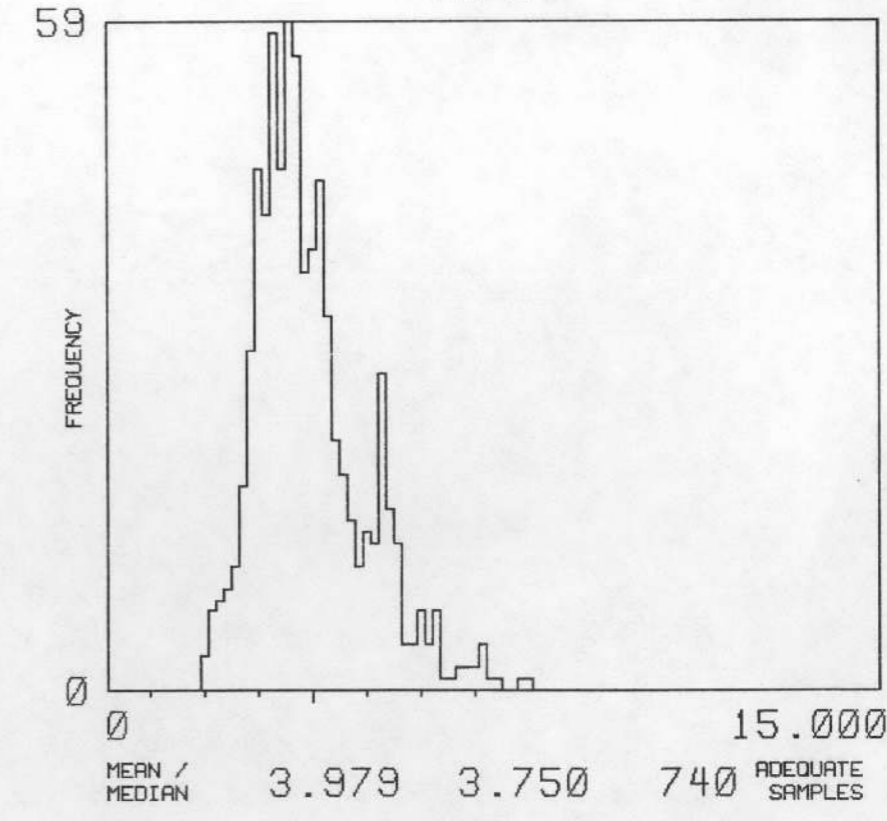
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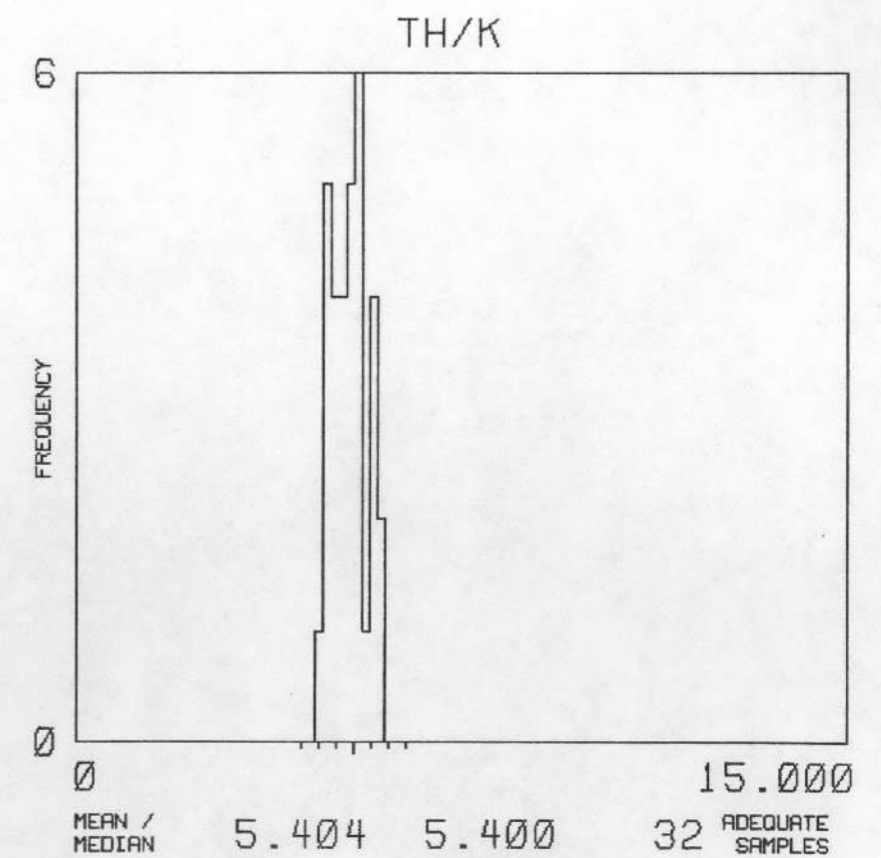
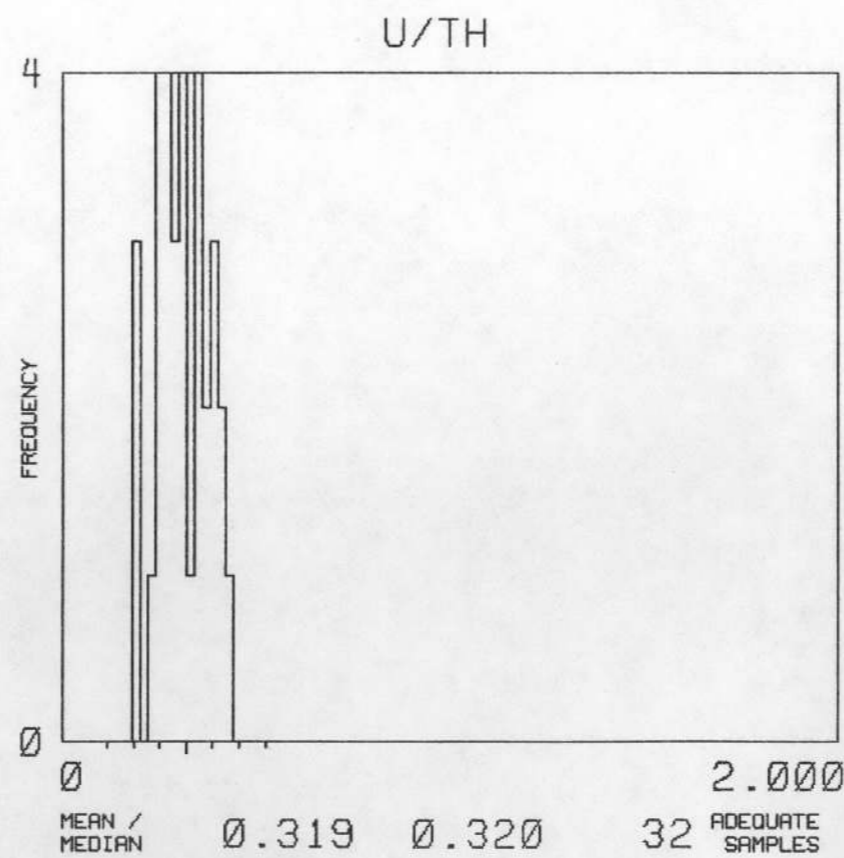
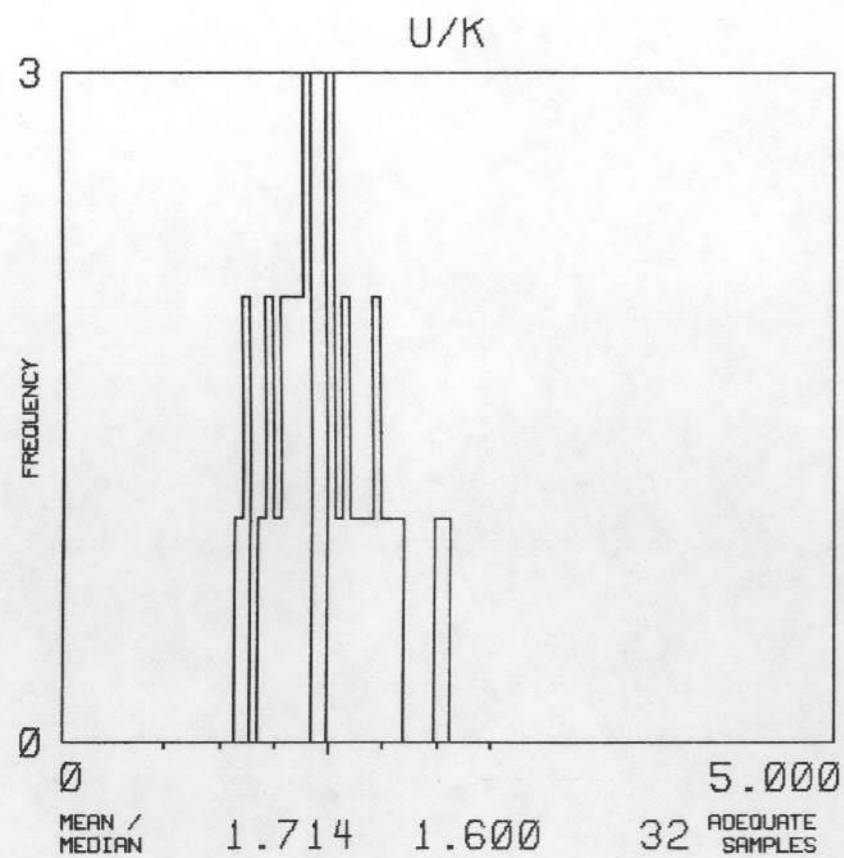
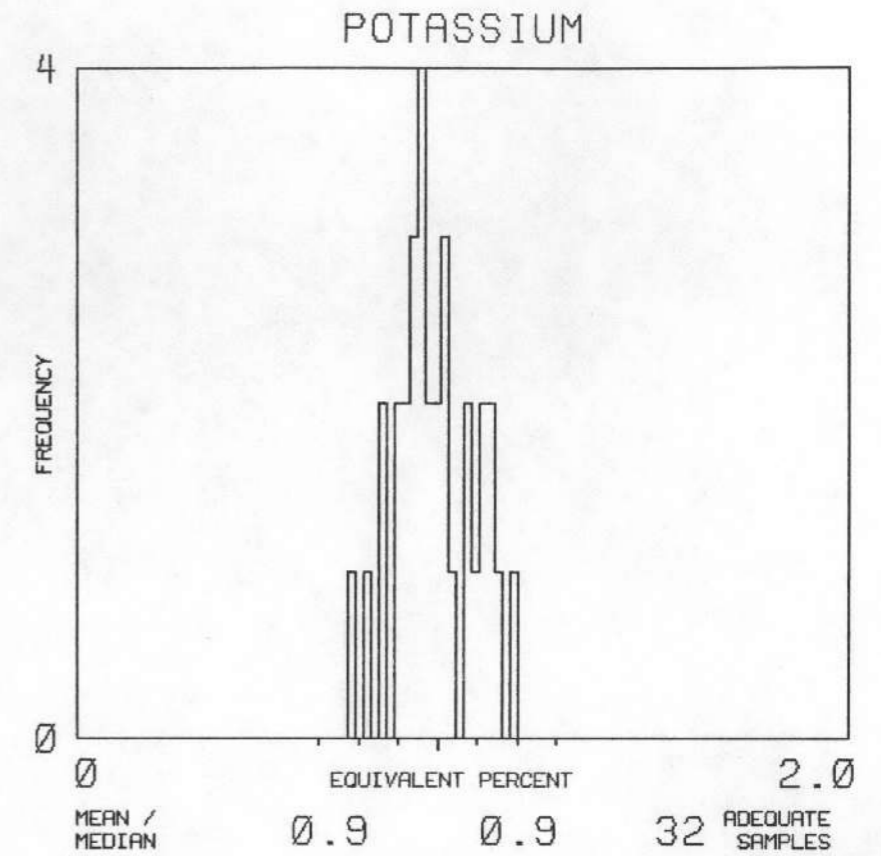
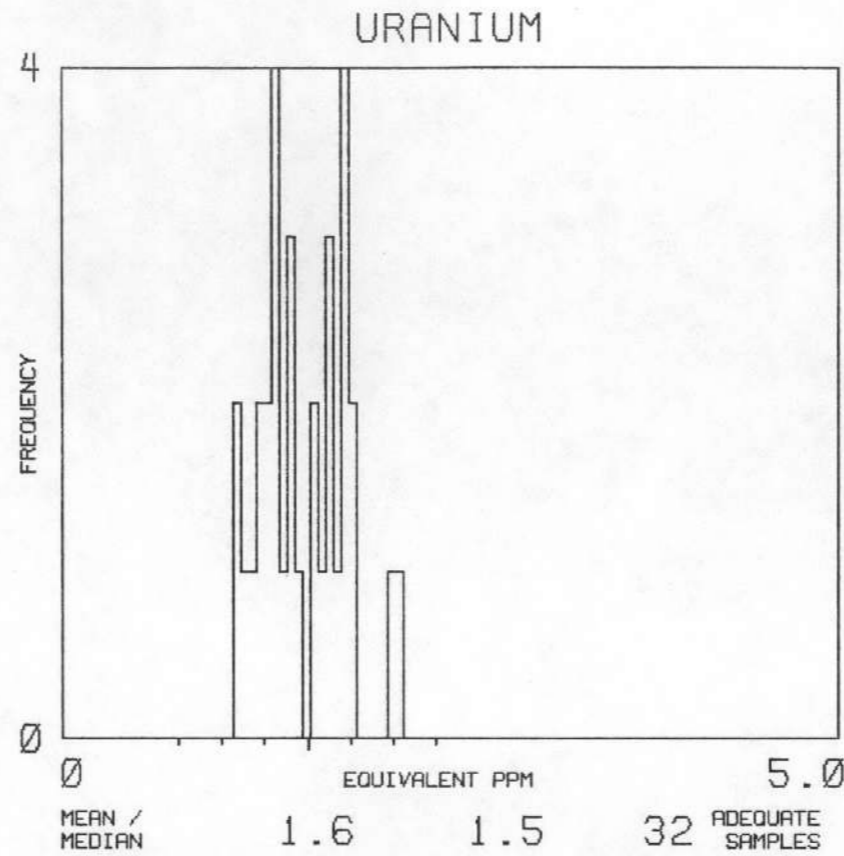
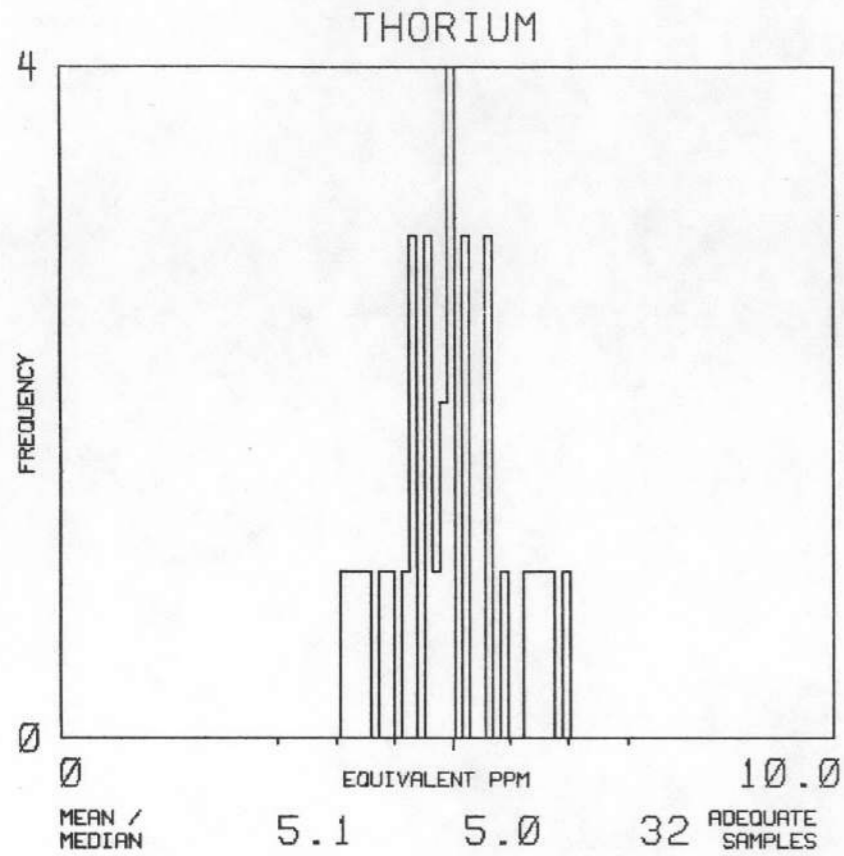


U/TH



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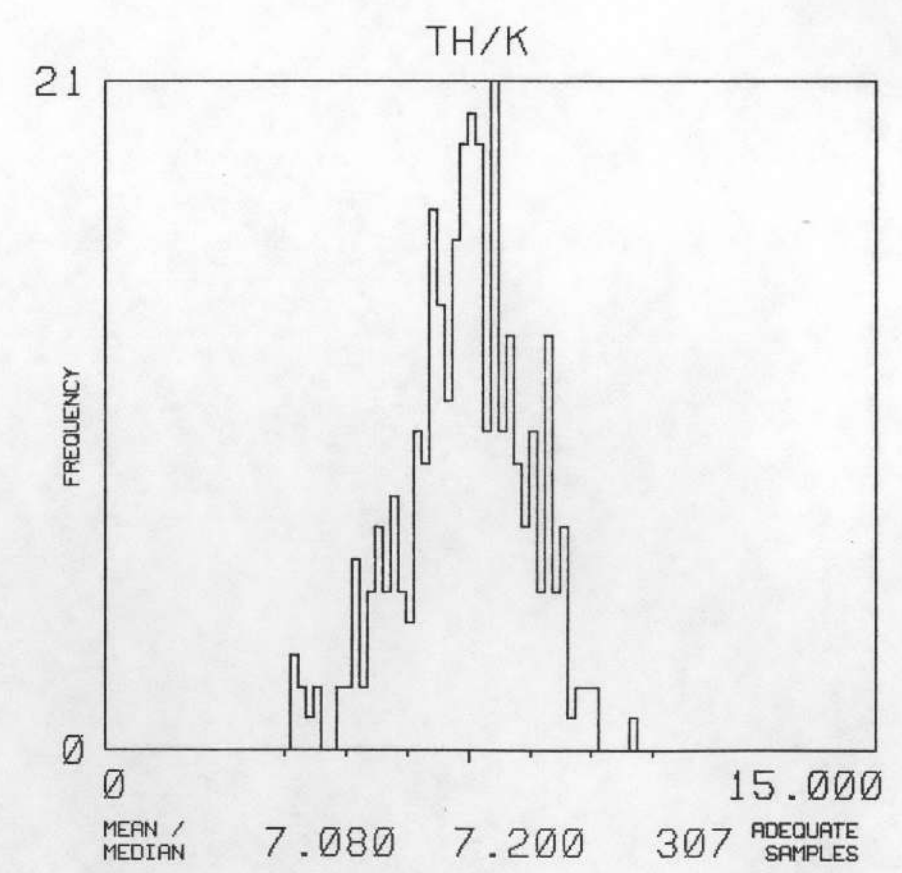
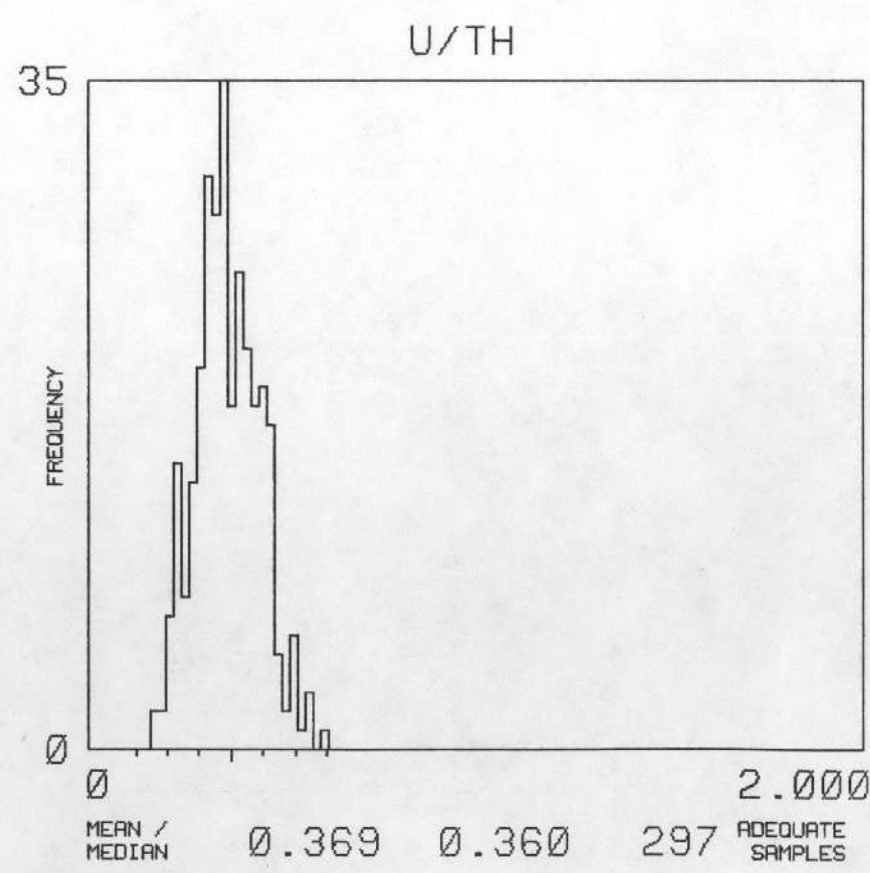
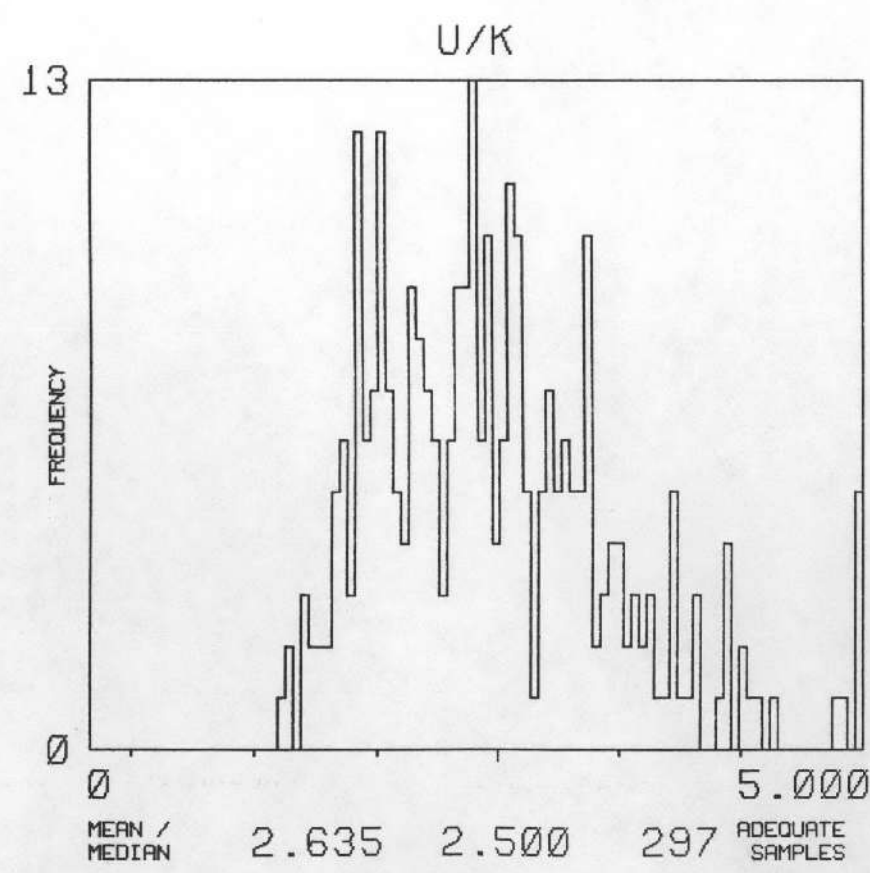
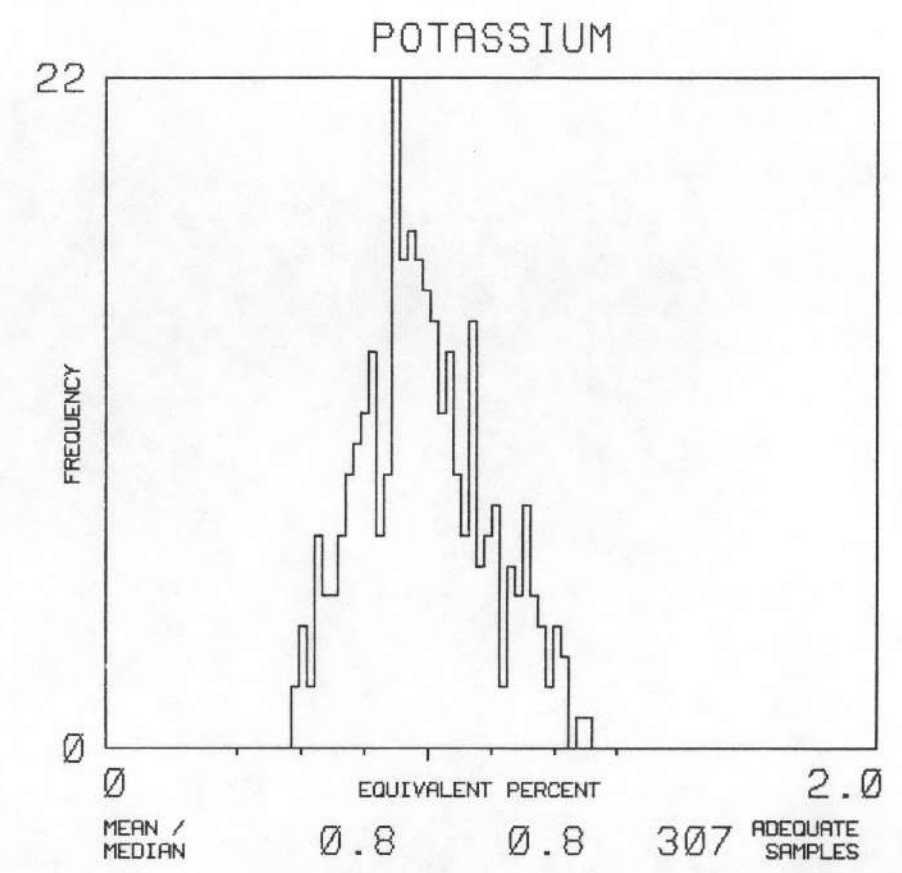
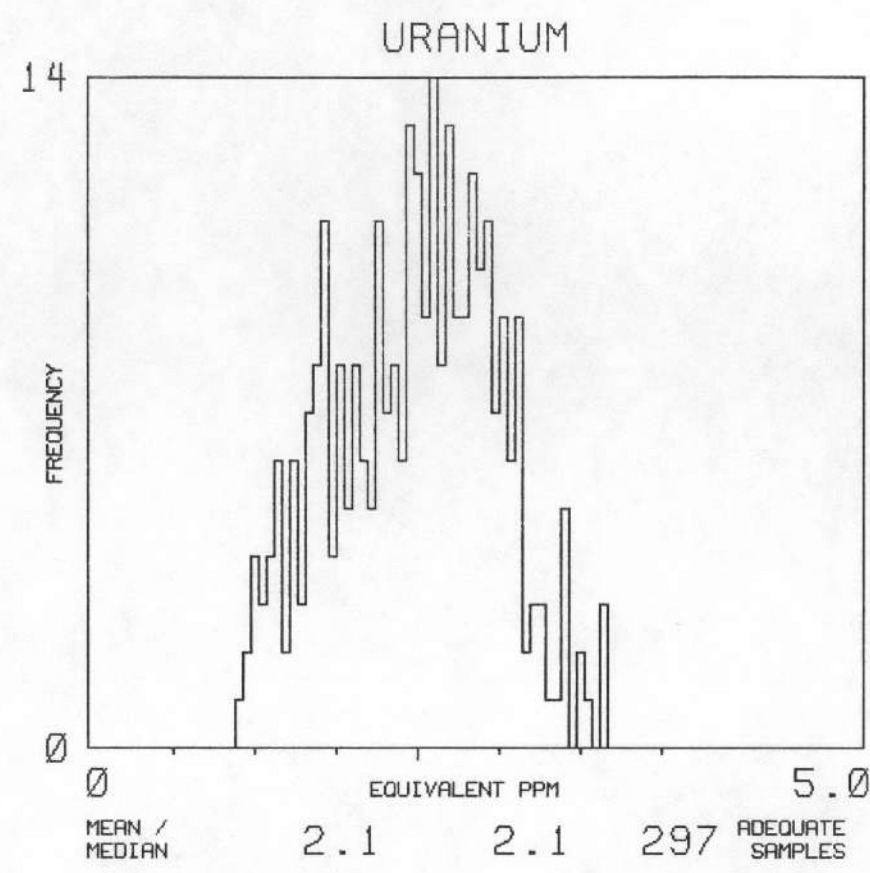
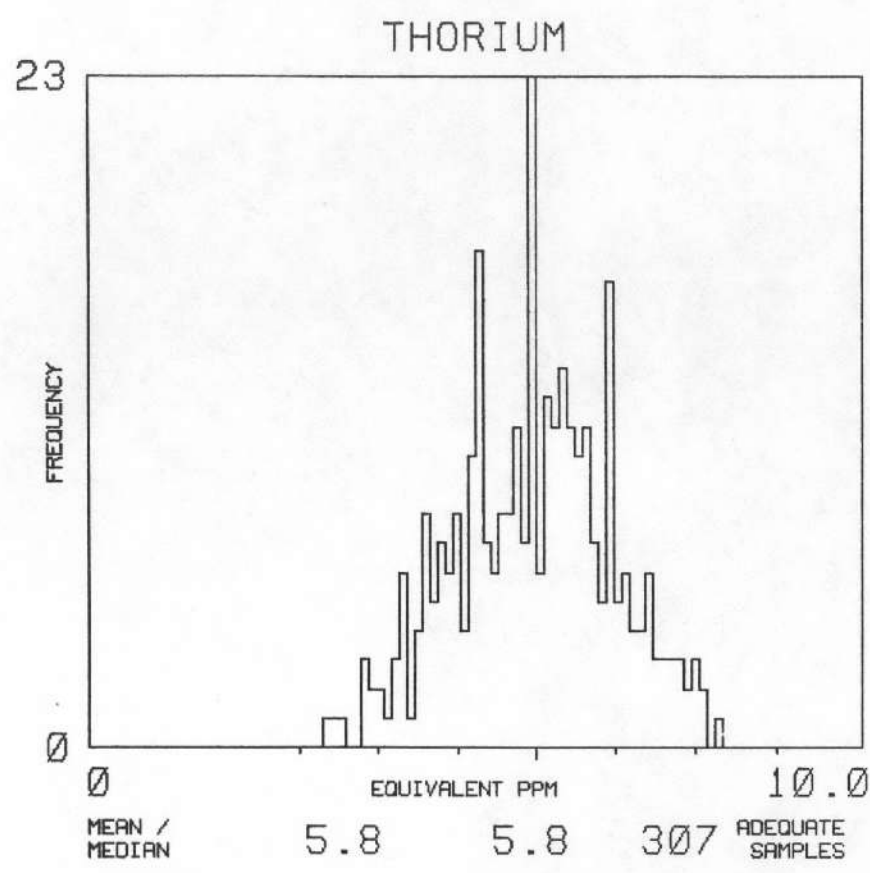
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VINCENNES

MAP UNIT : QSI

TOTAL NUMBER OF SAMPLES

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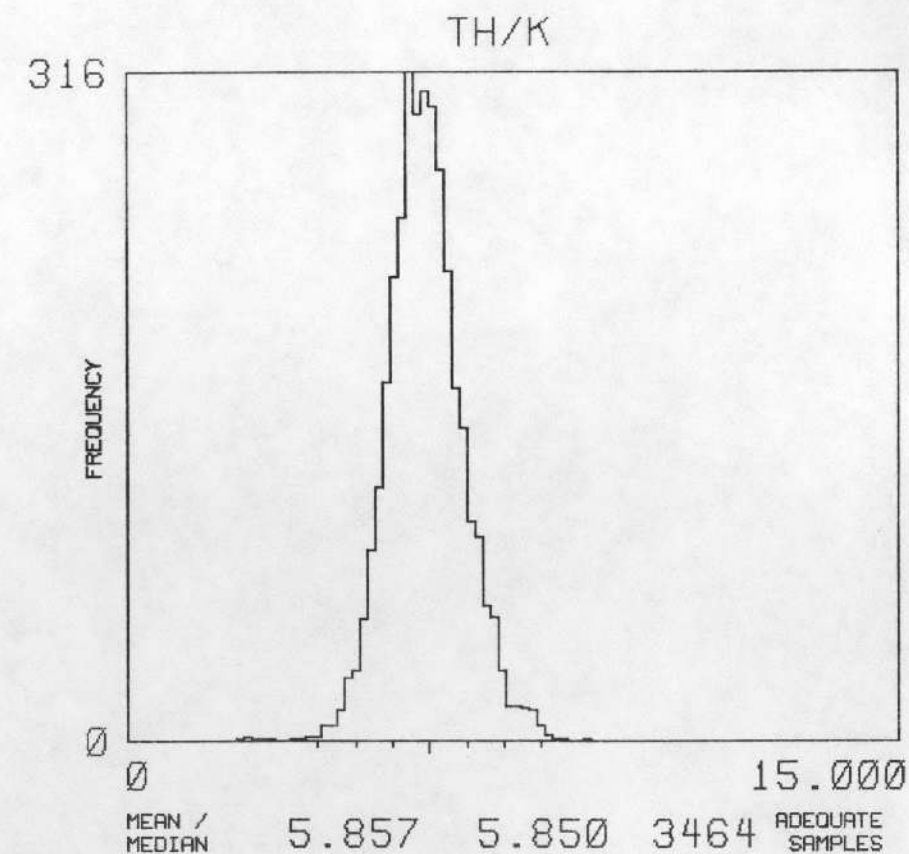
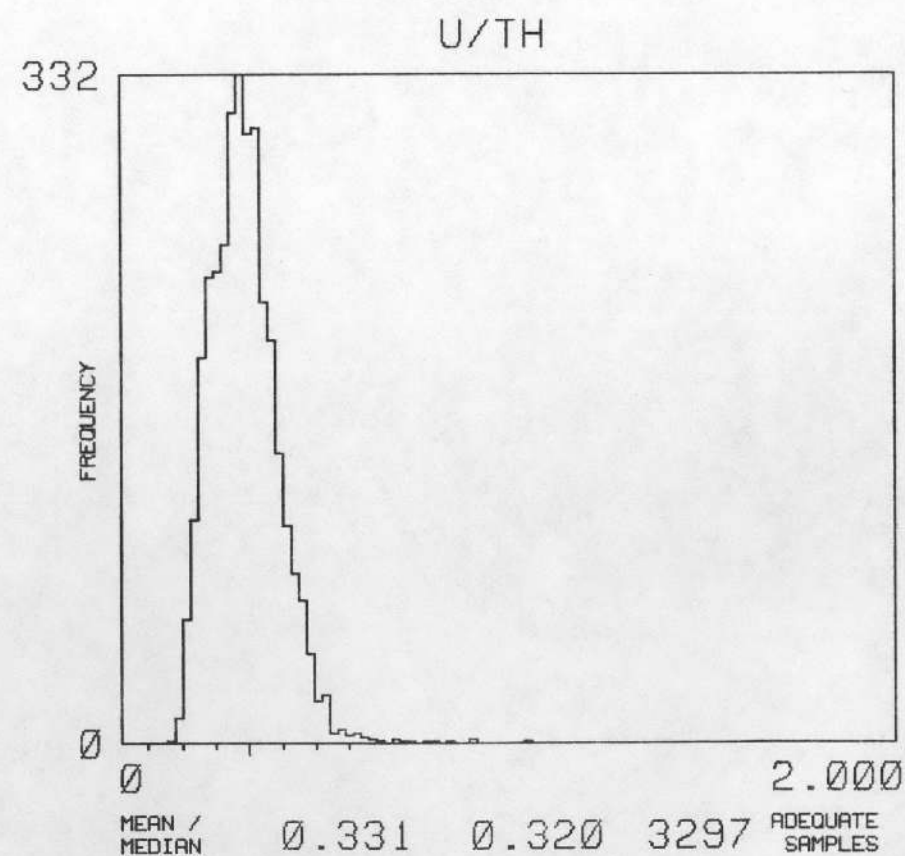
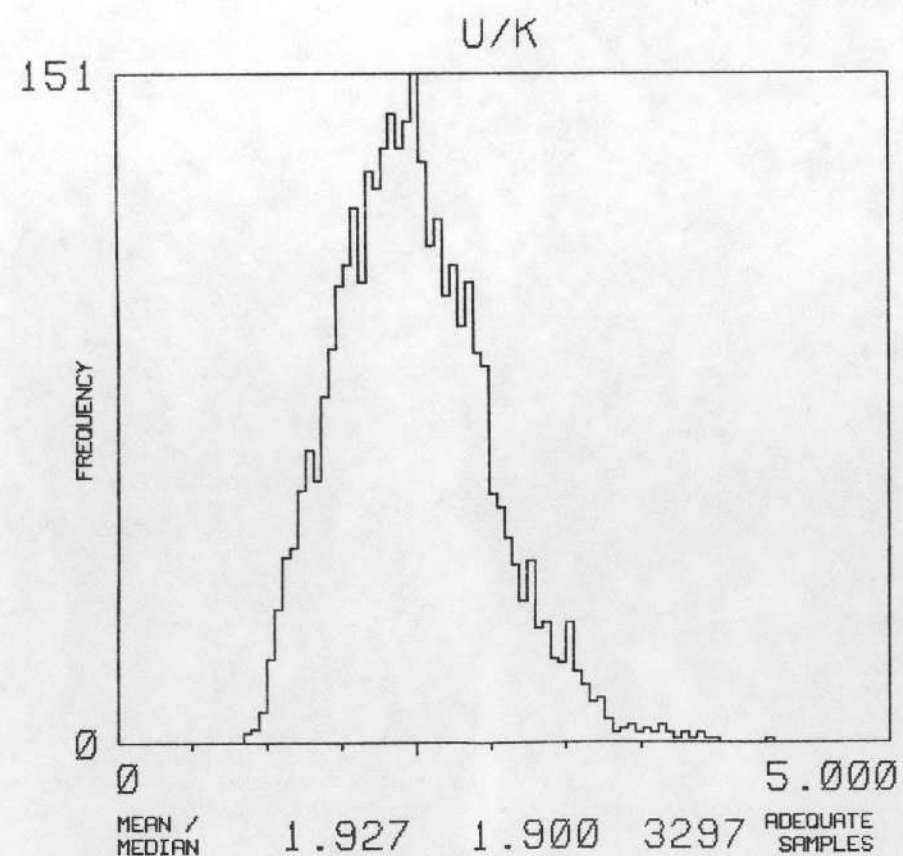
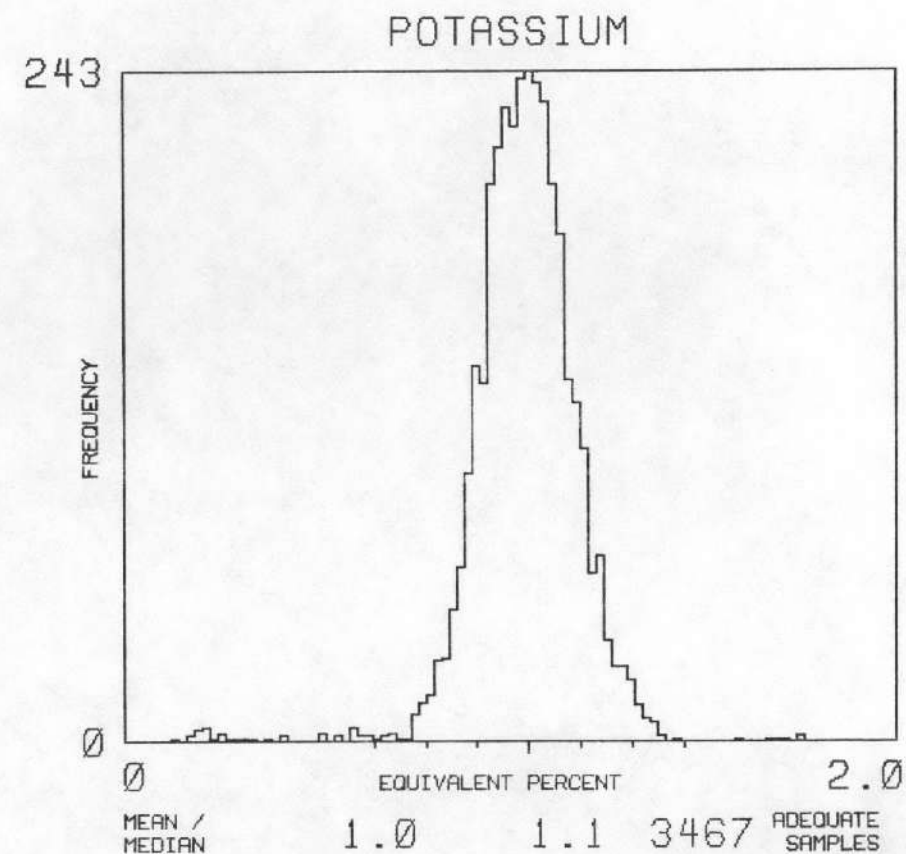
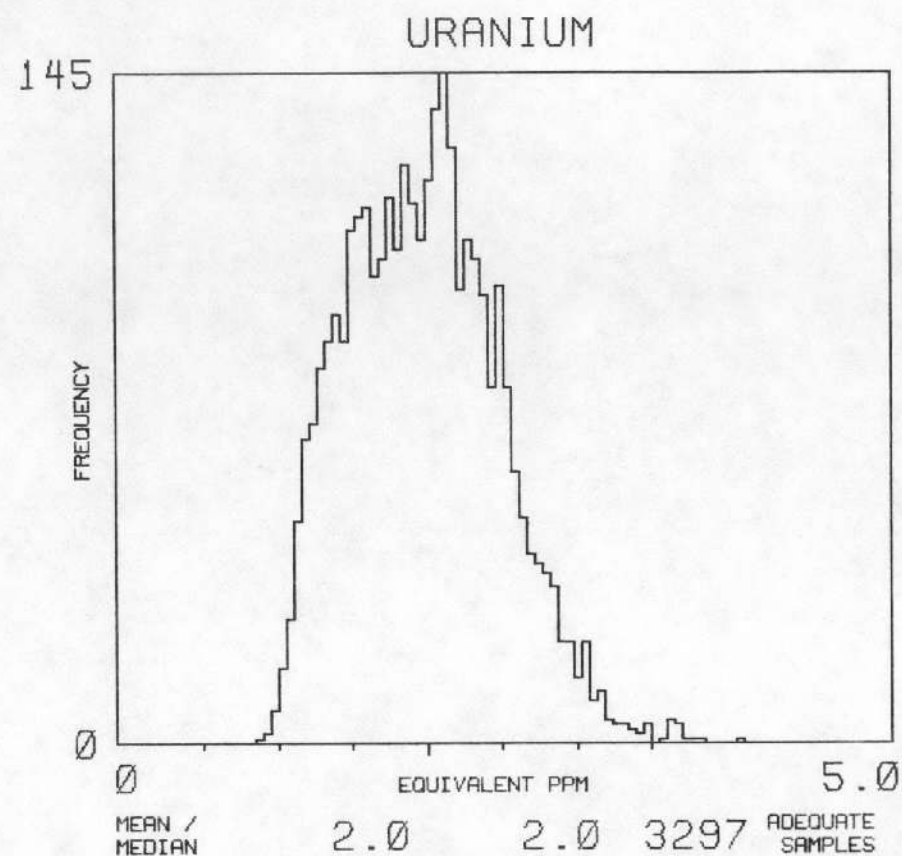
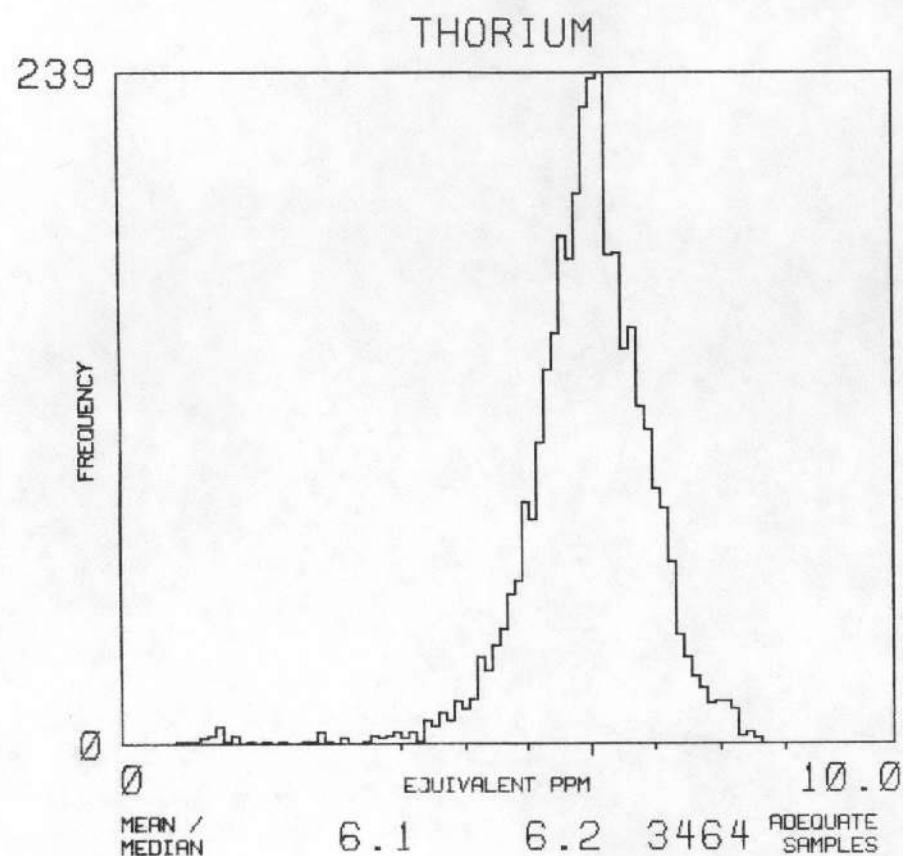


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VINCENNES

MAP UNIT : QTI

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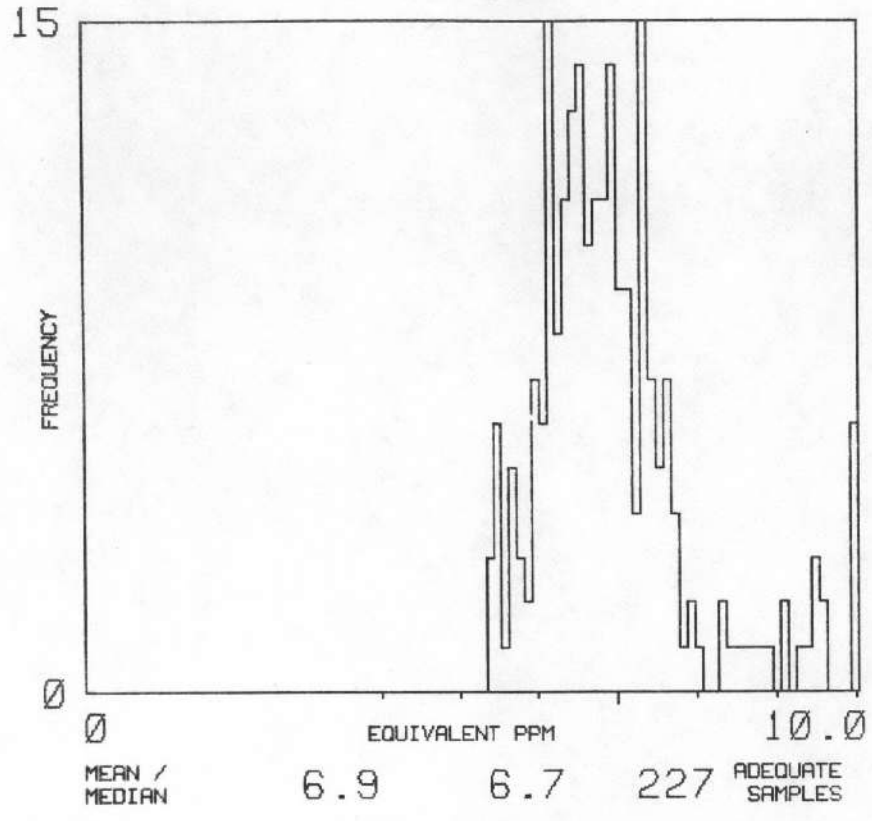
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VINCENNES

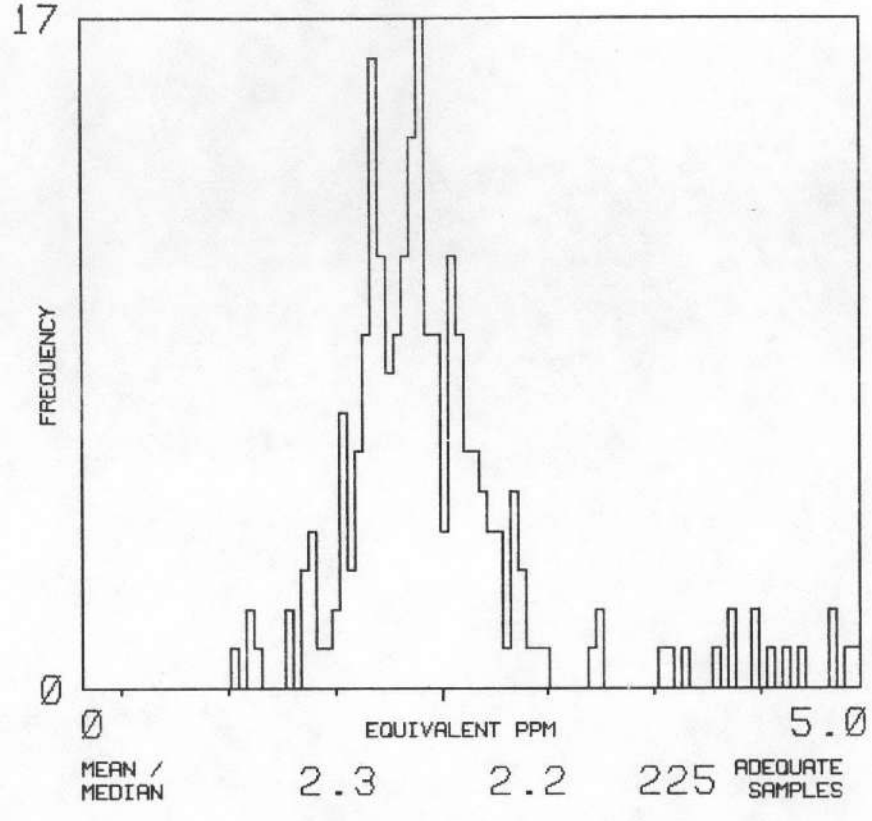
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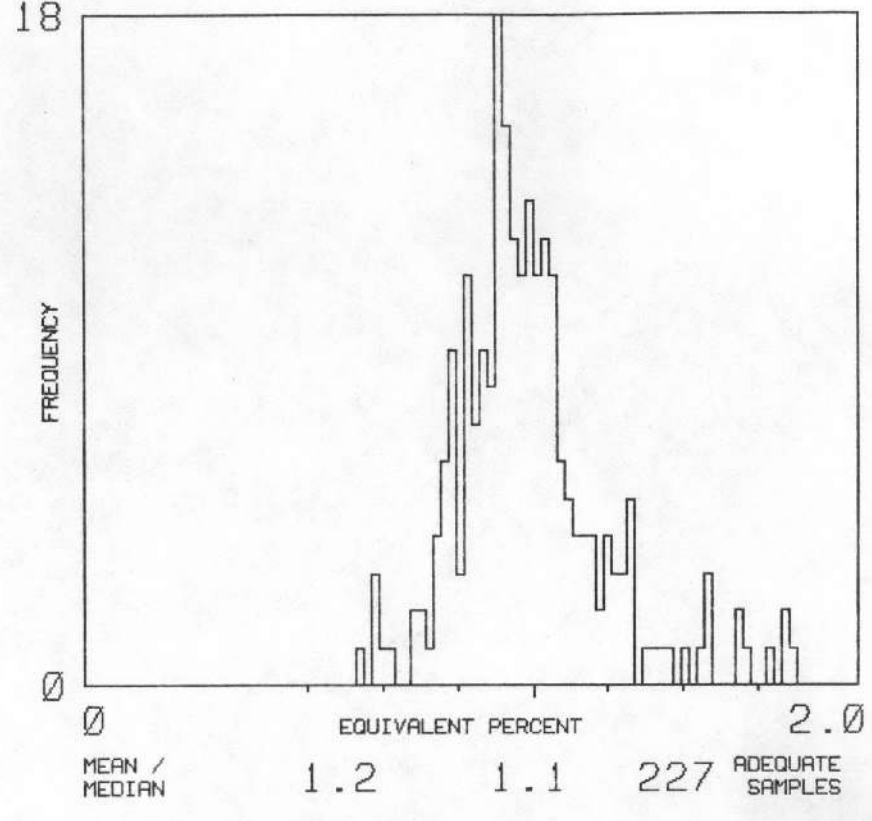
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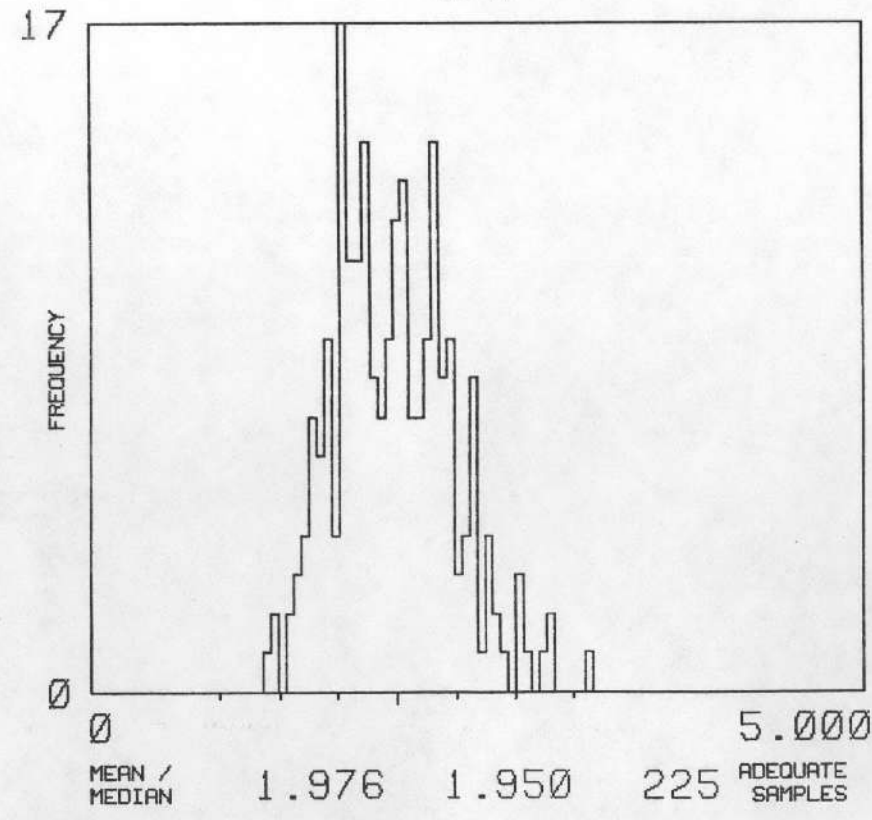
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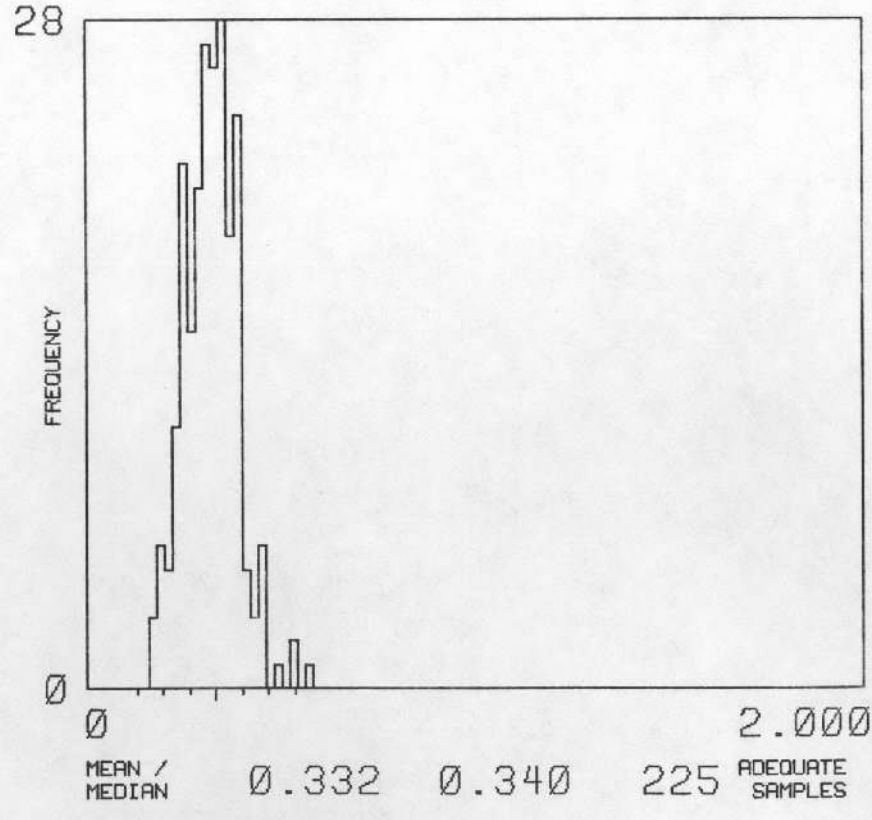
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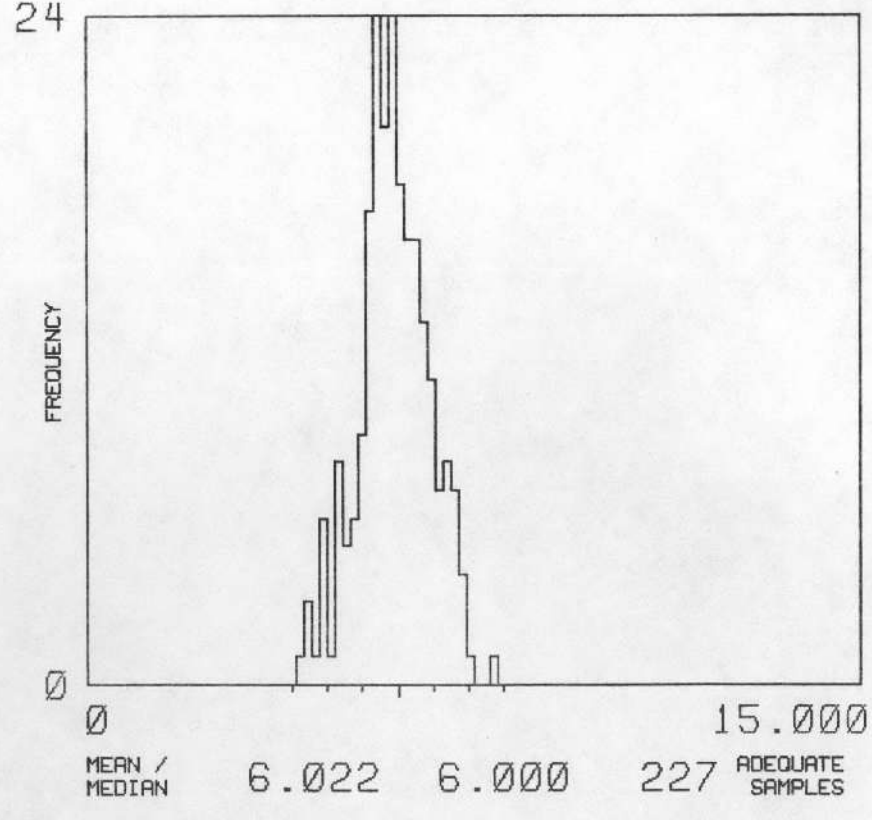
U/K



U/TH



TH/K



NJ 16-5

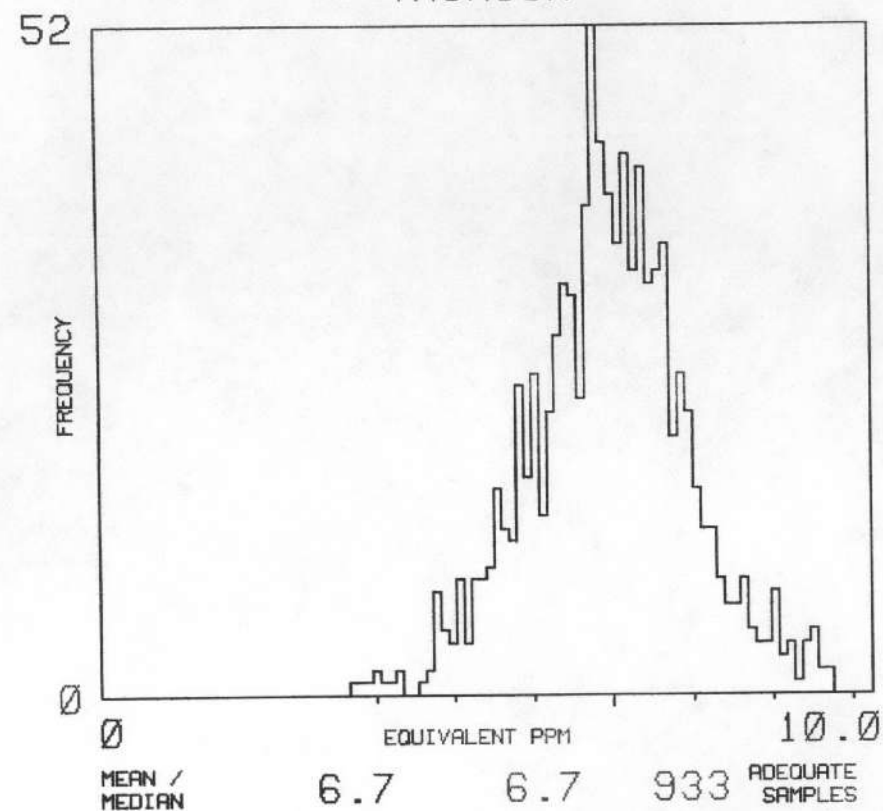
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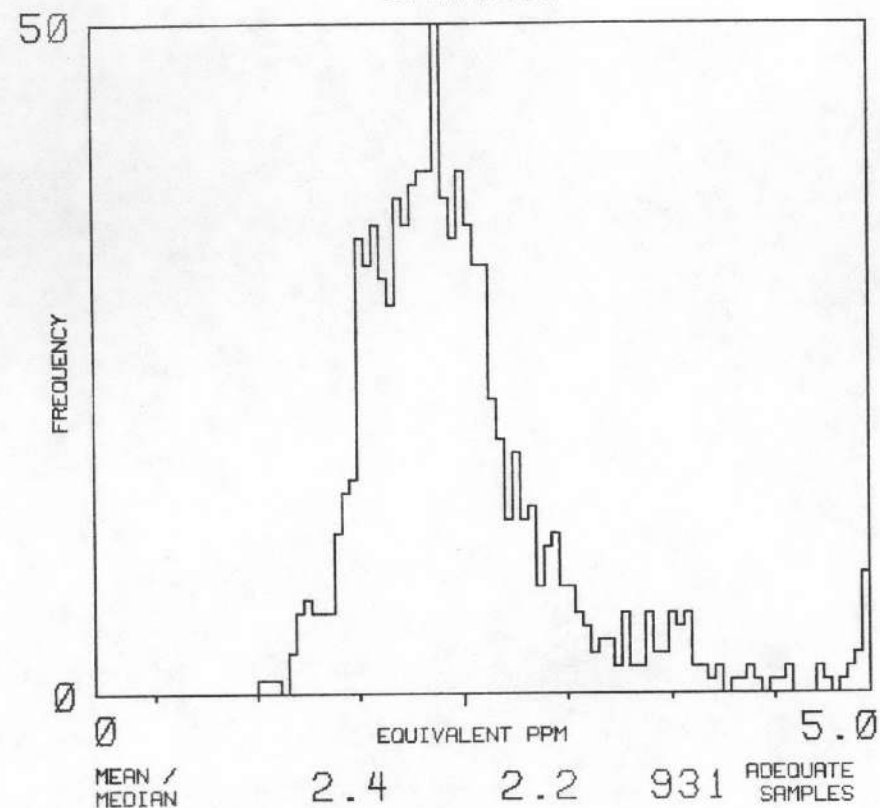
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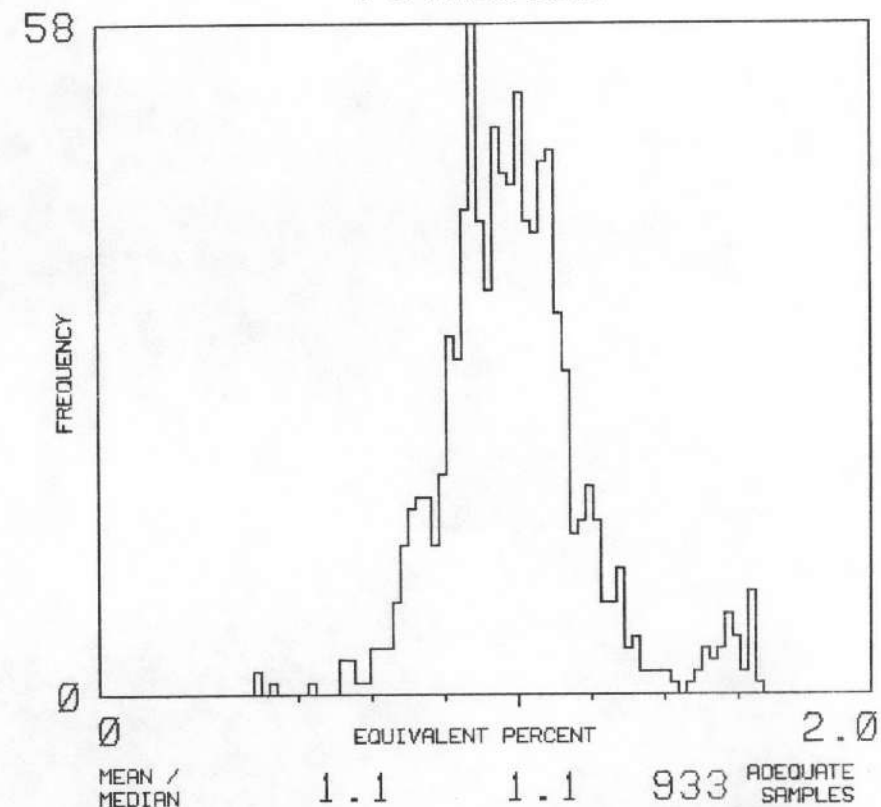
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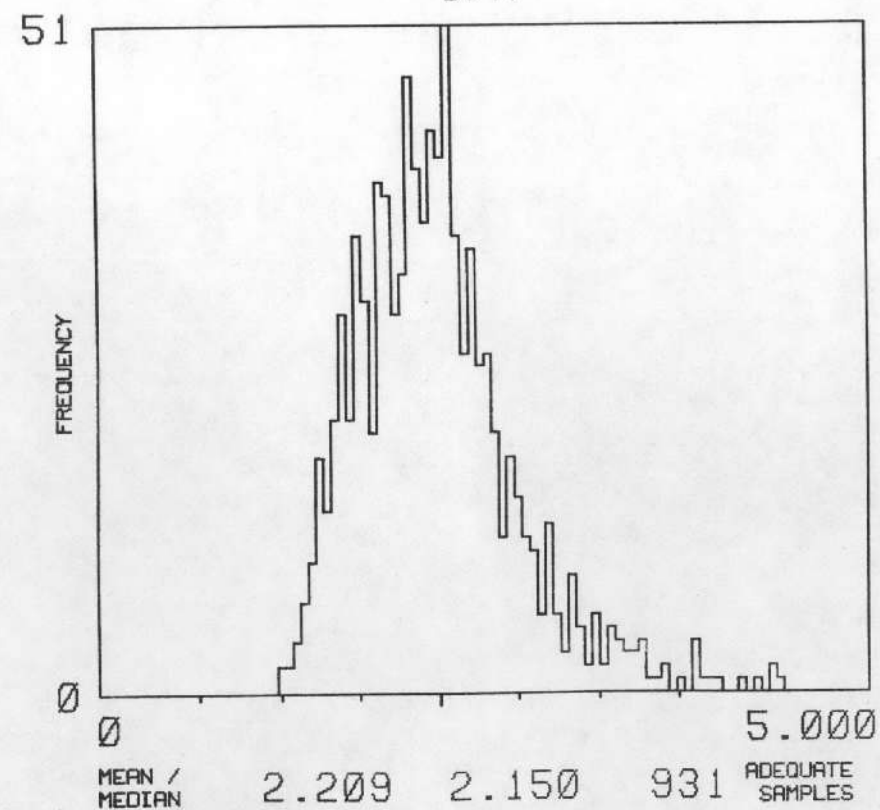
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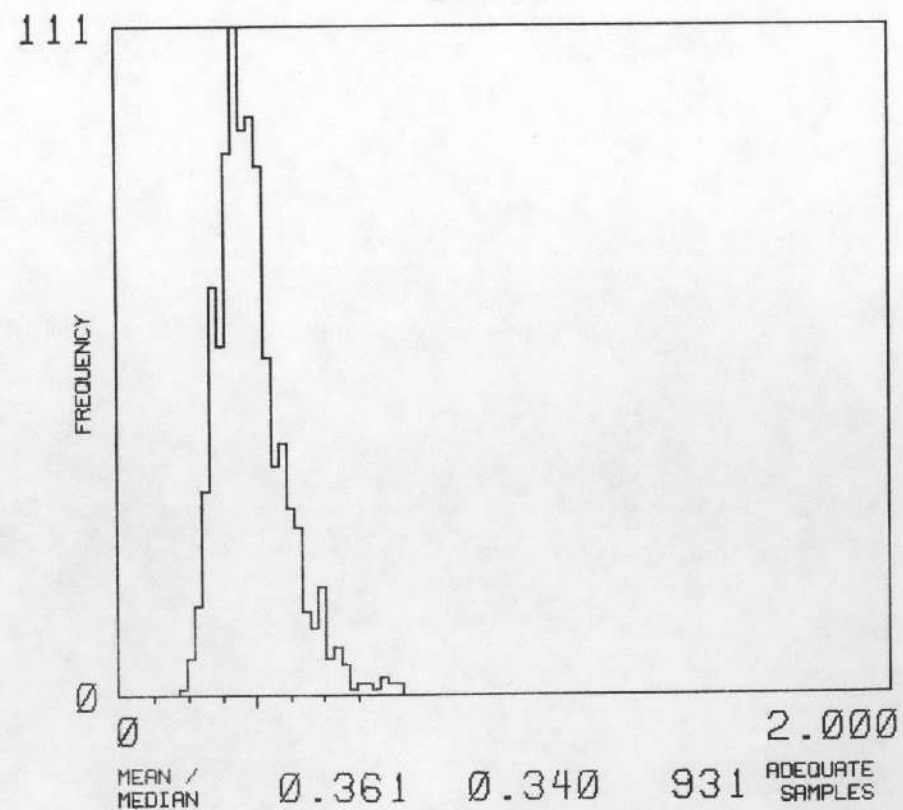
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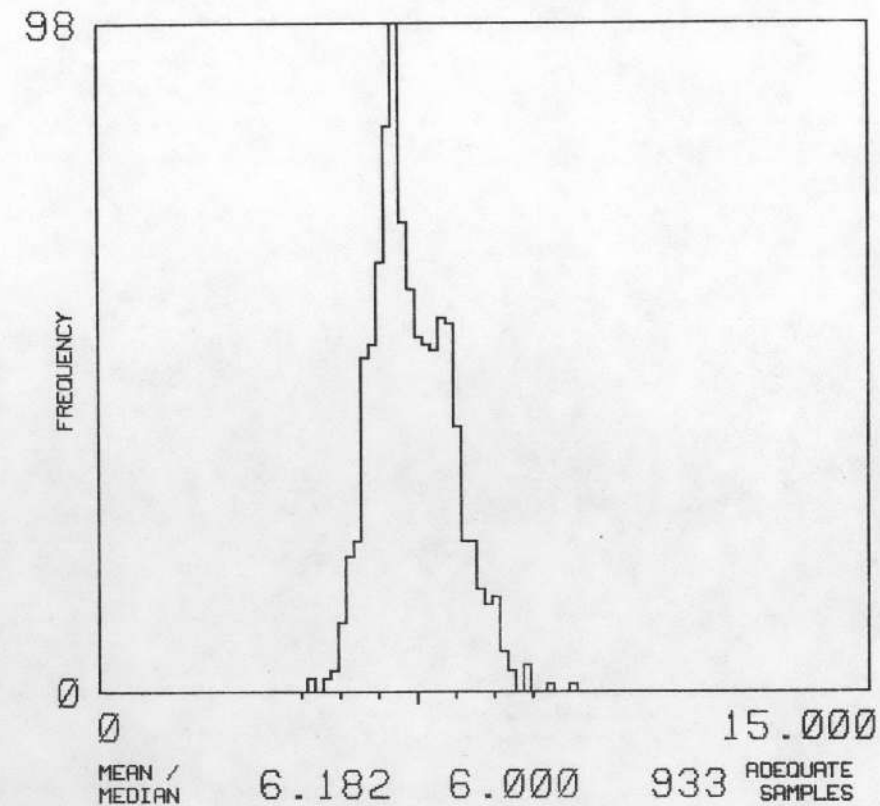
U/K



U/TH



TH/K

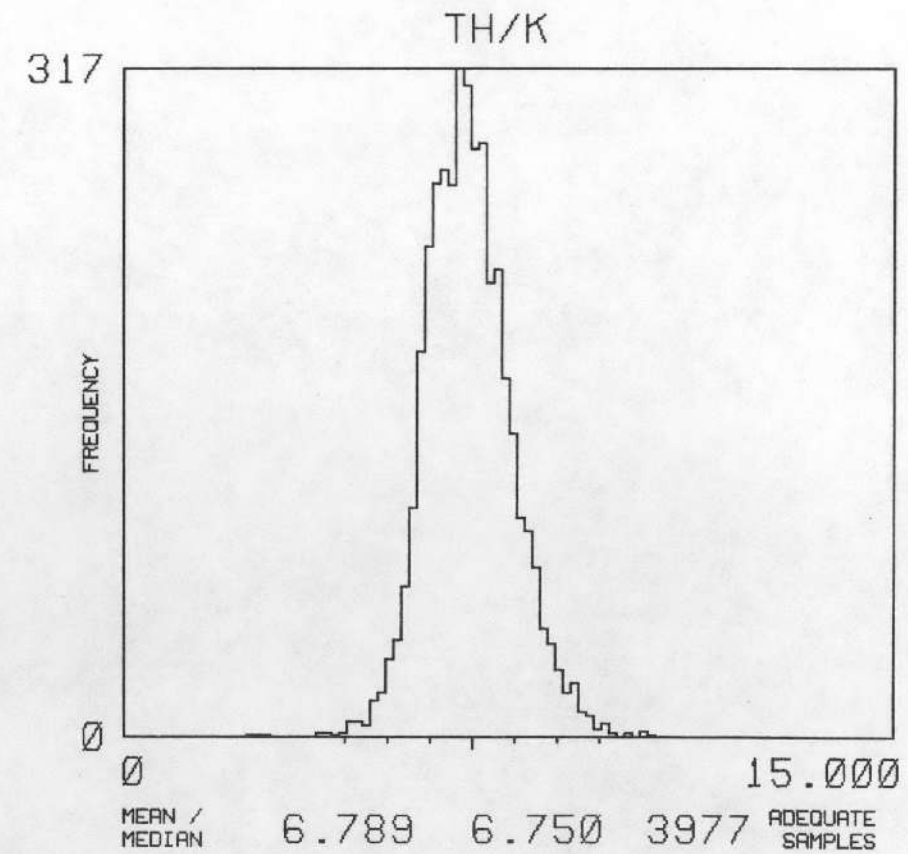
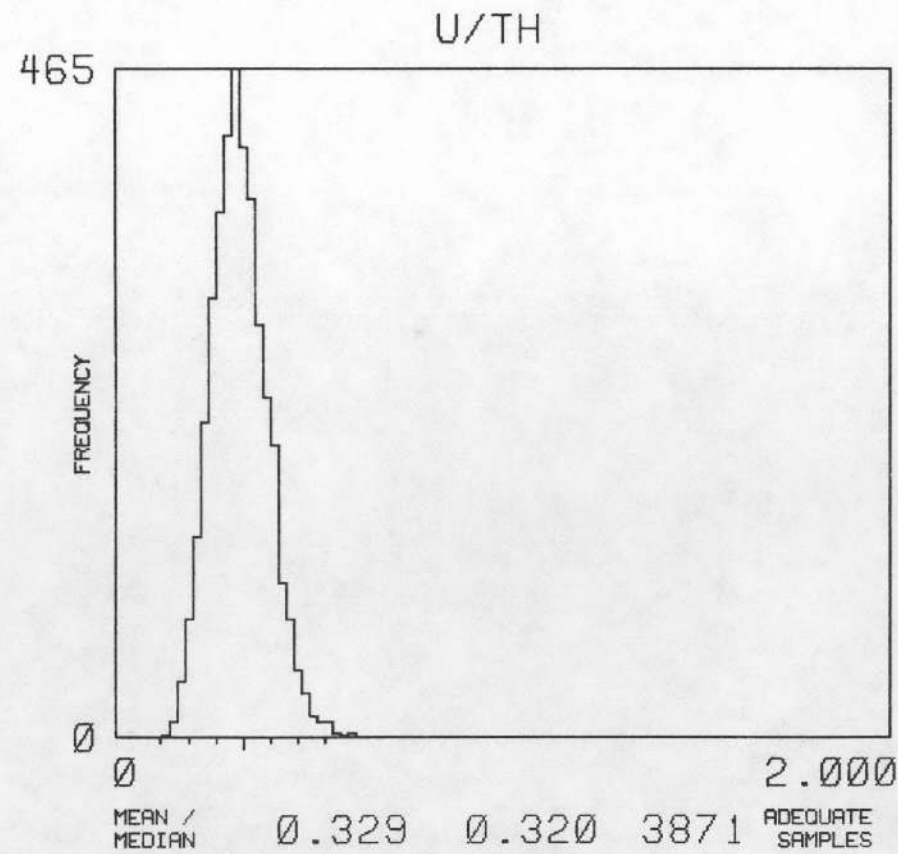
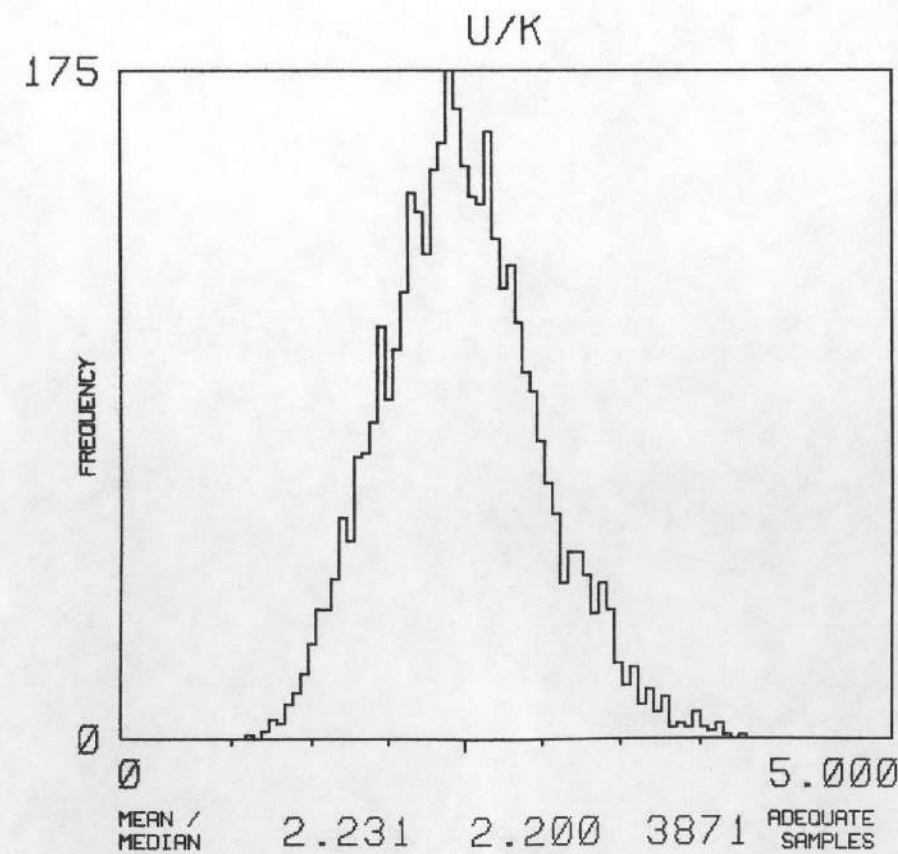
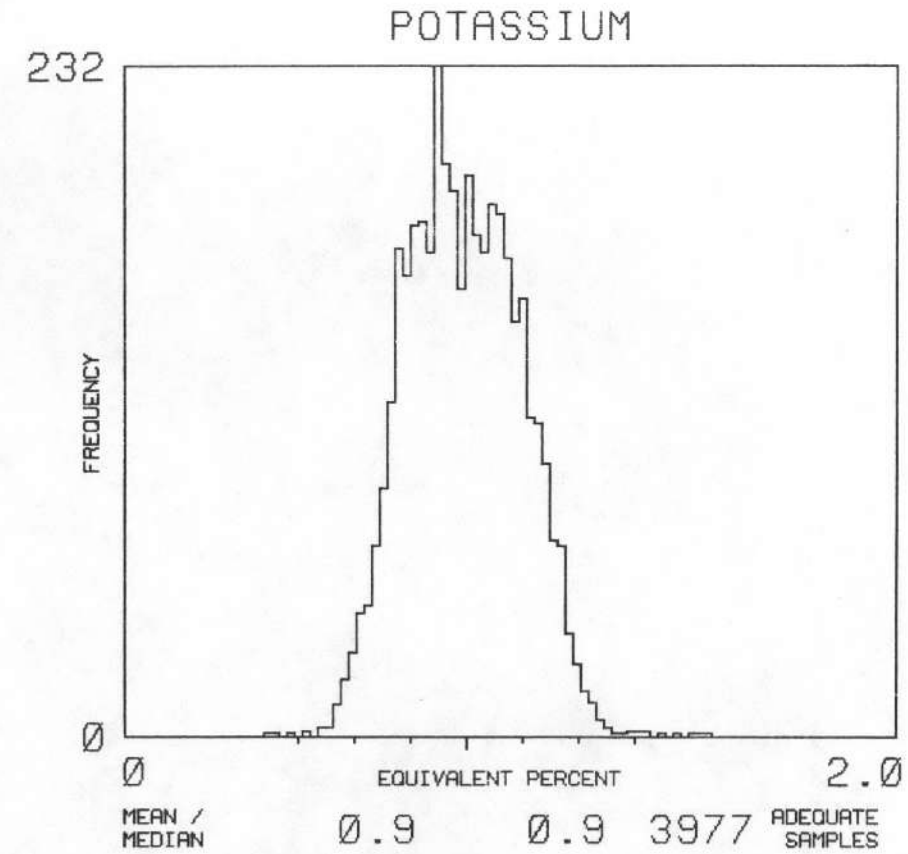
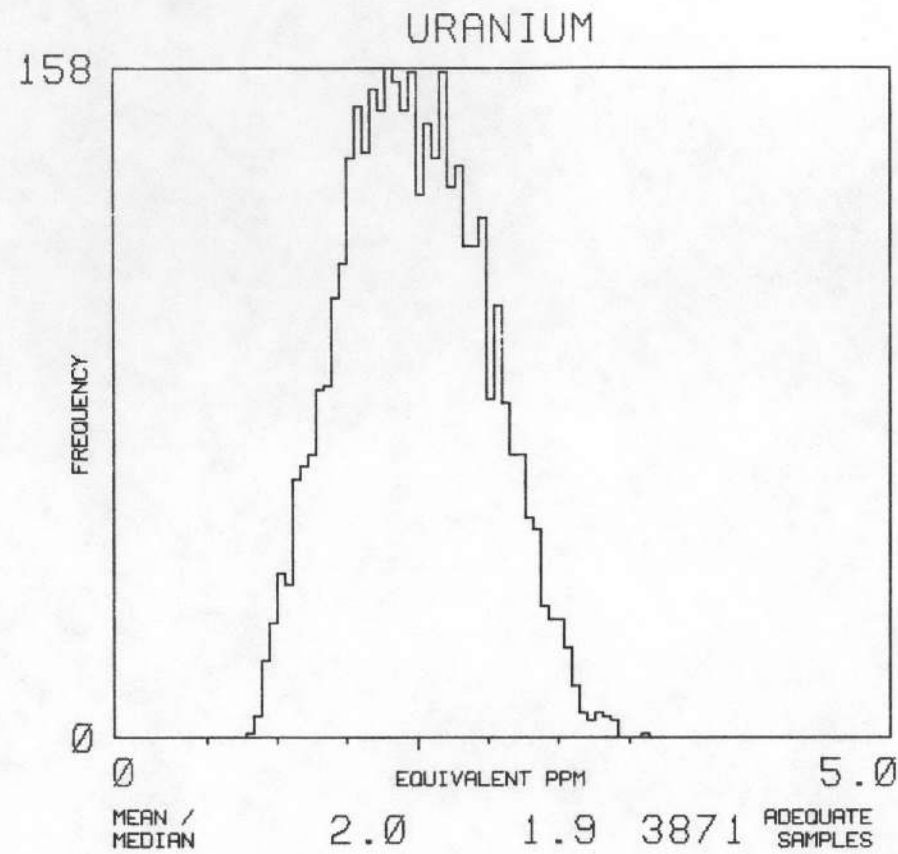
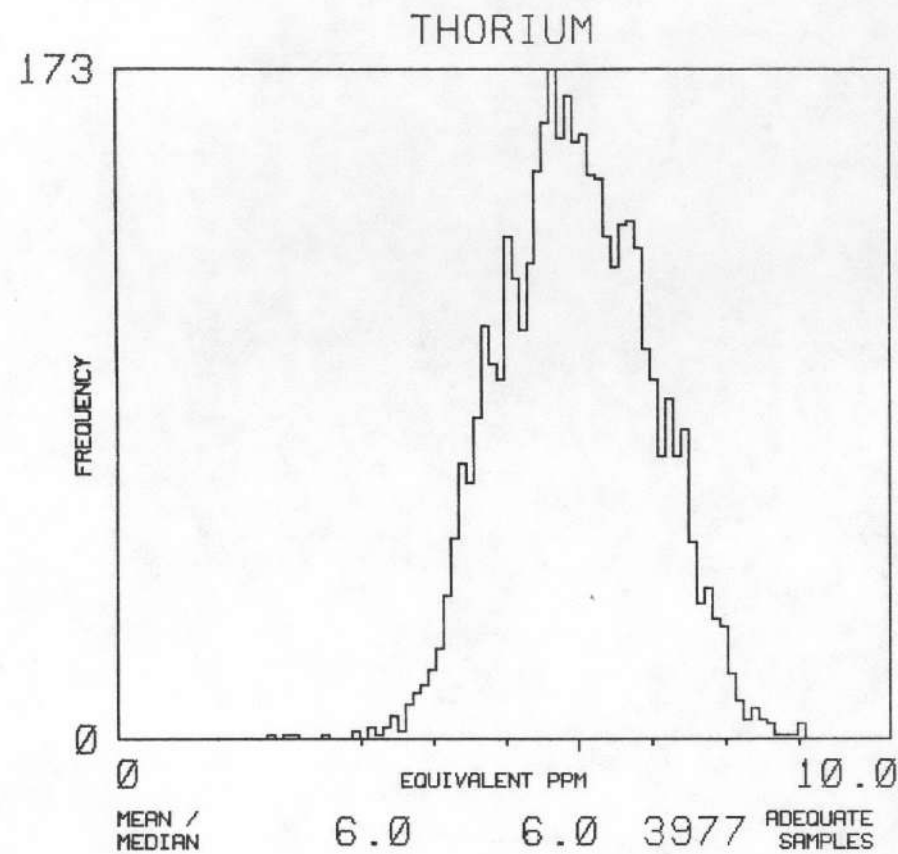


NJ 16-5

VINCENNES

MAP UNIT : PRC

TOTAL NUMBER OF SAMPLES 3977

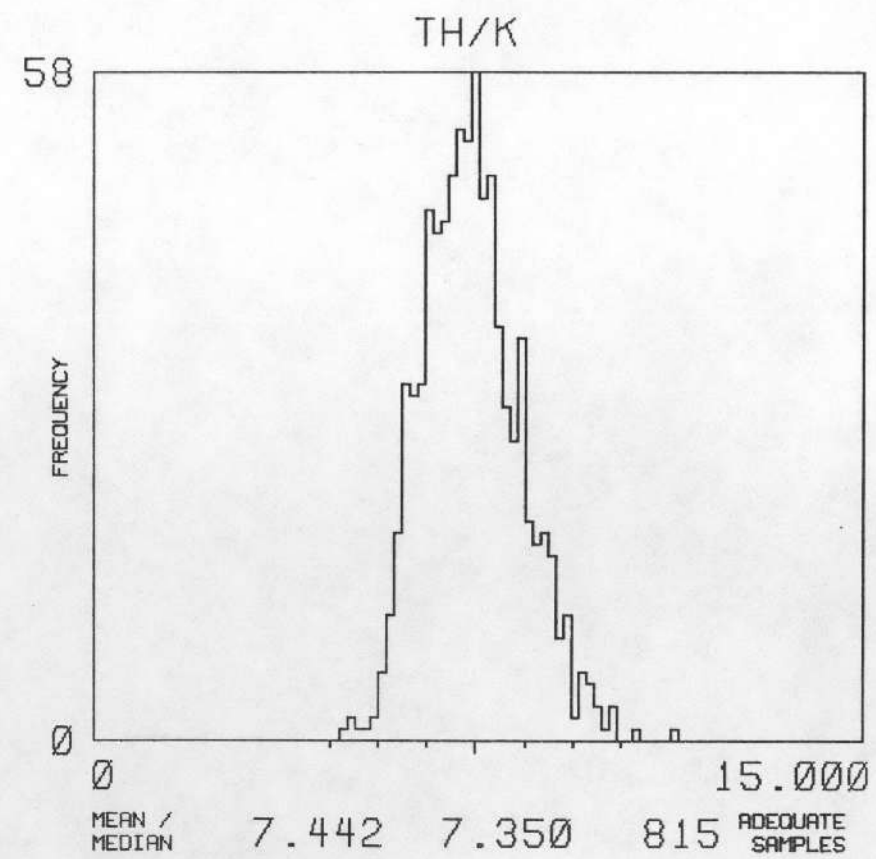
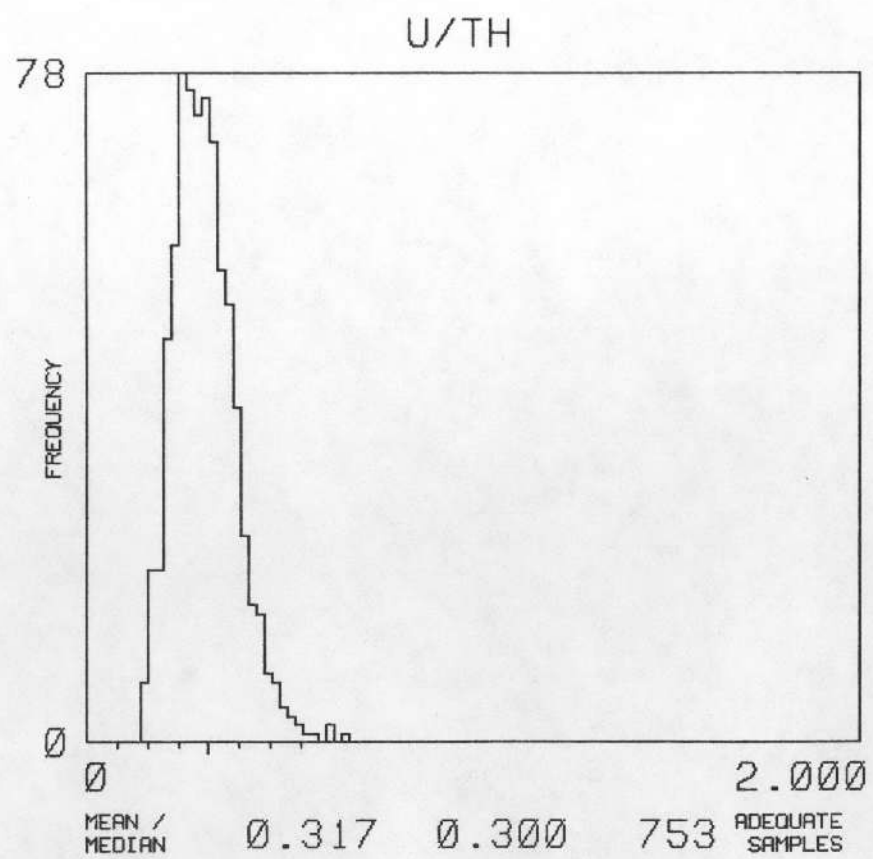
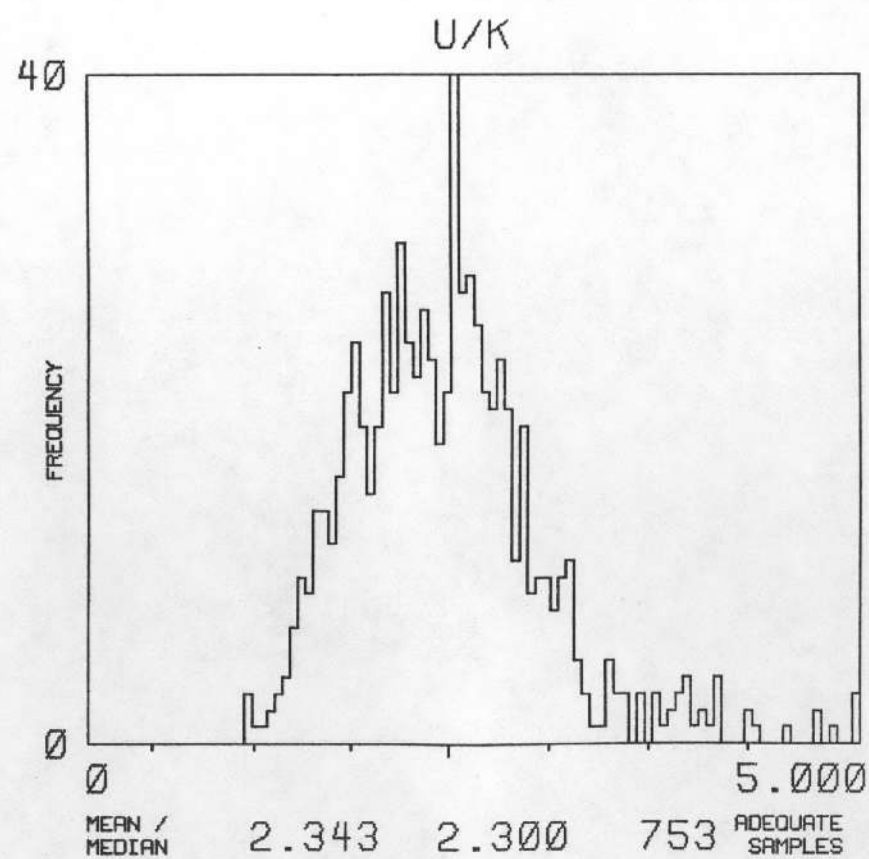
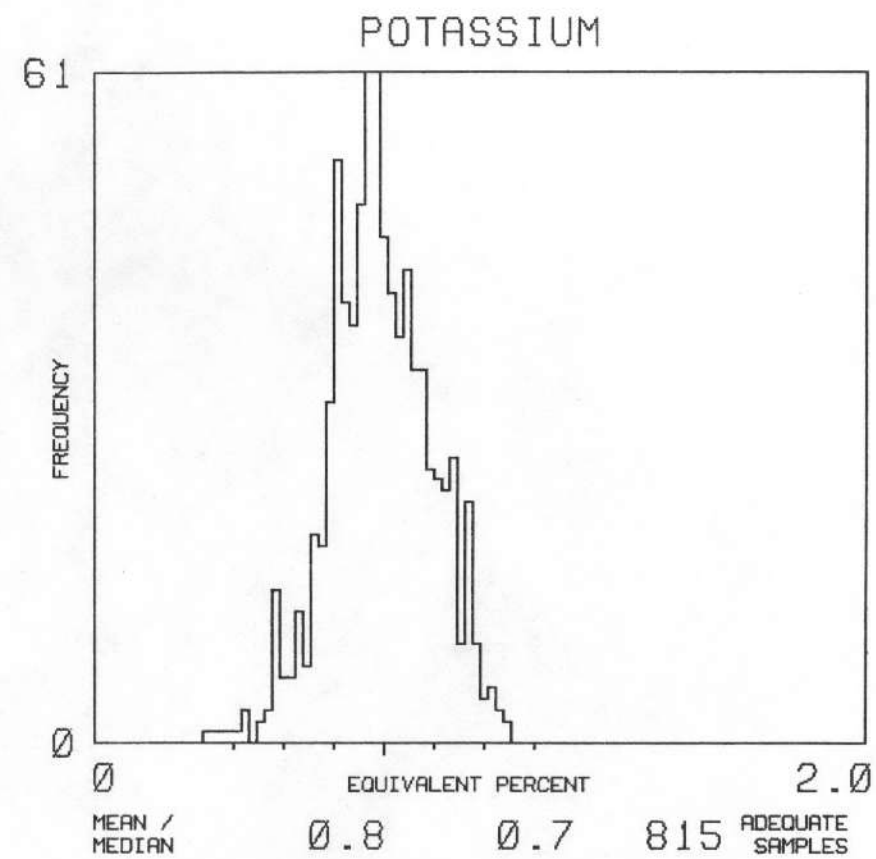
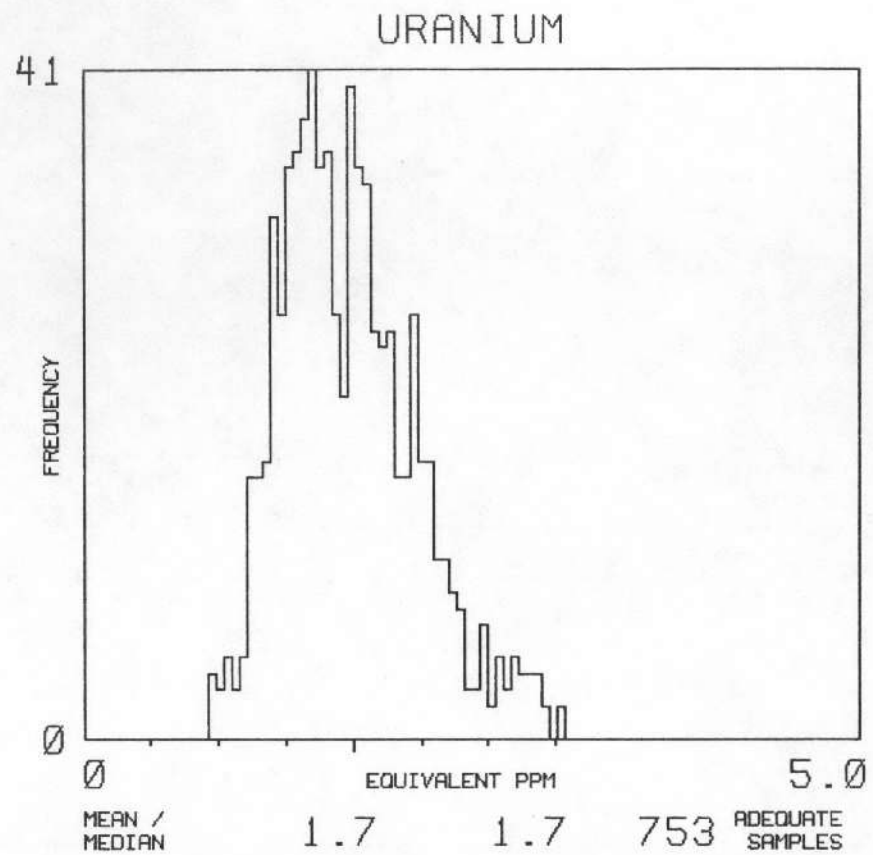
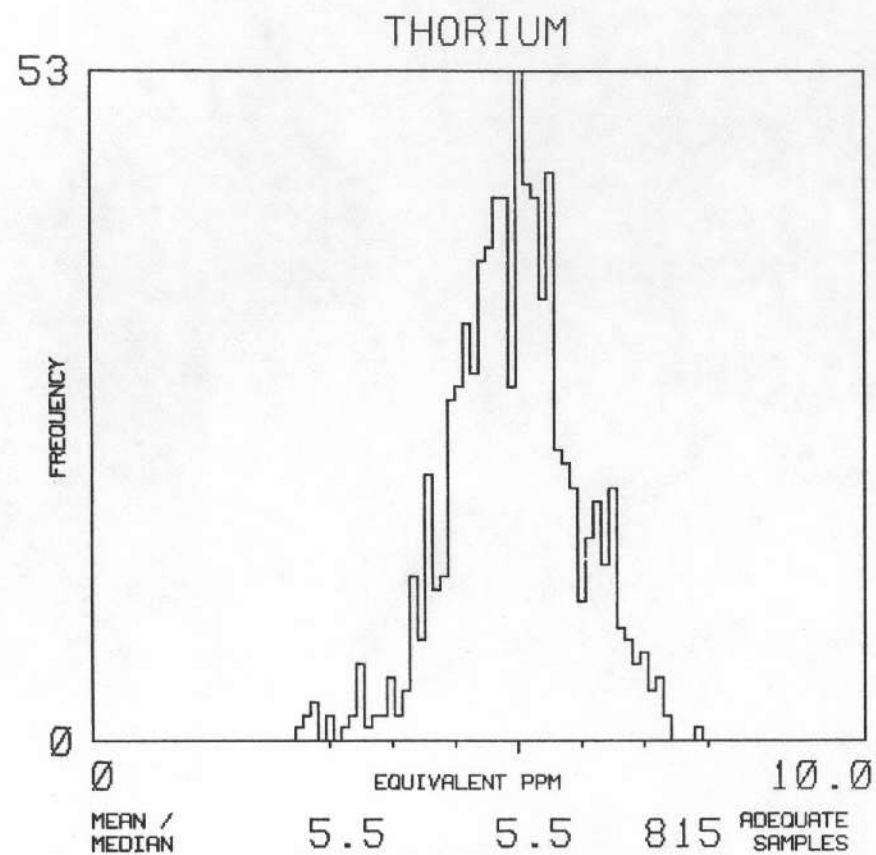


NJ 16-5

VINCENNES

MAP UNIT : MC

TOTAL NUMBER OF SAMPLES 815

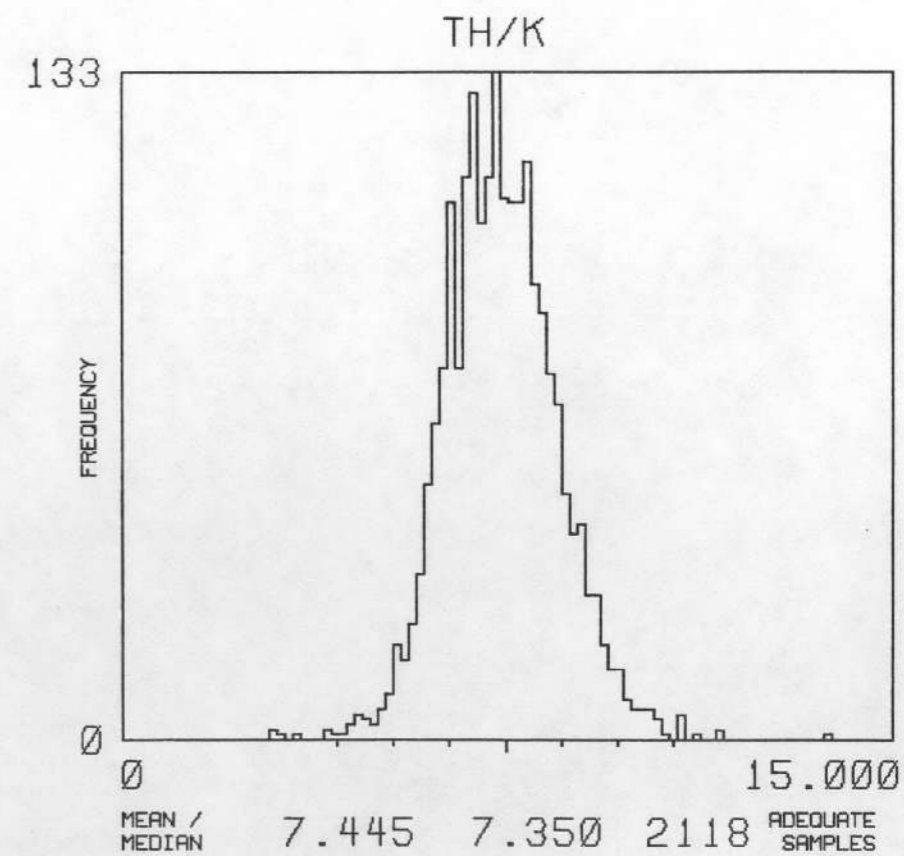
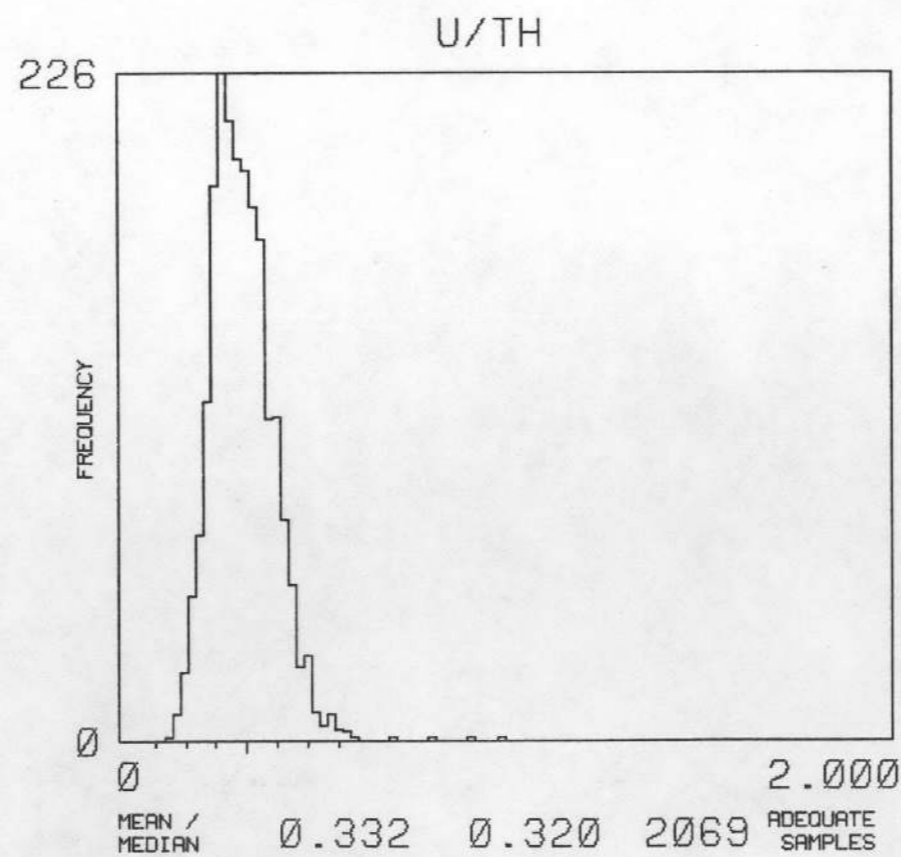
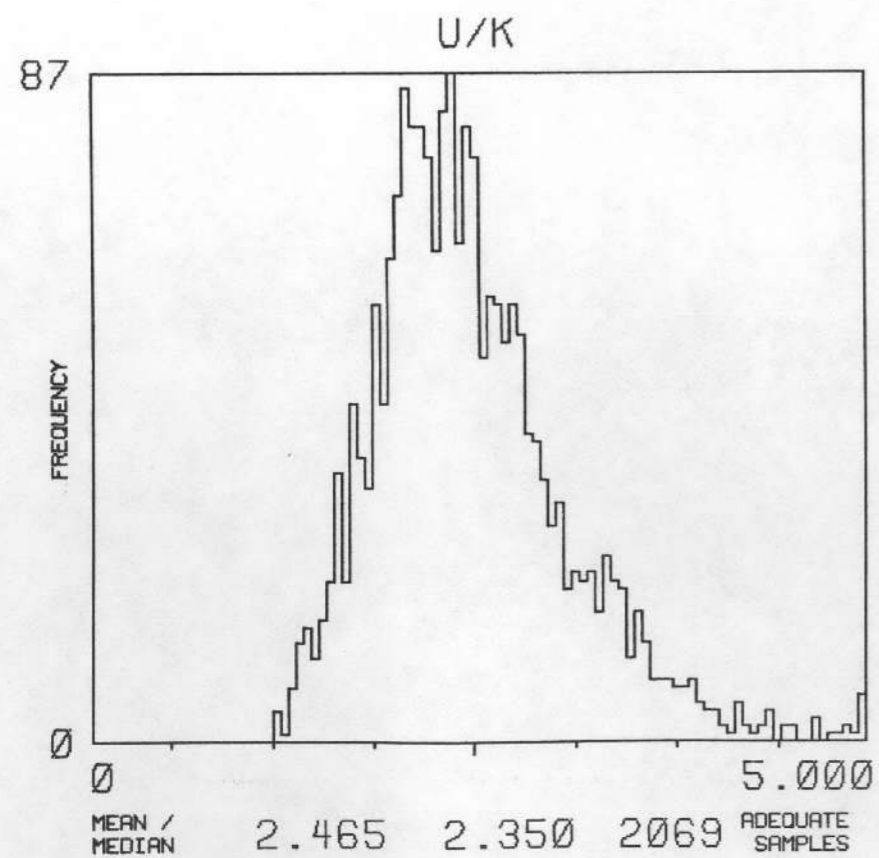
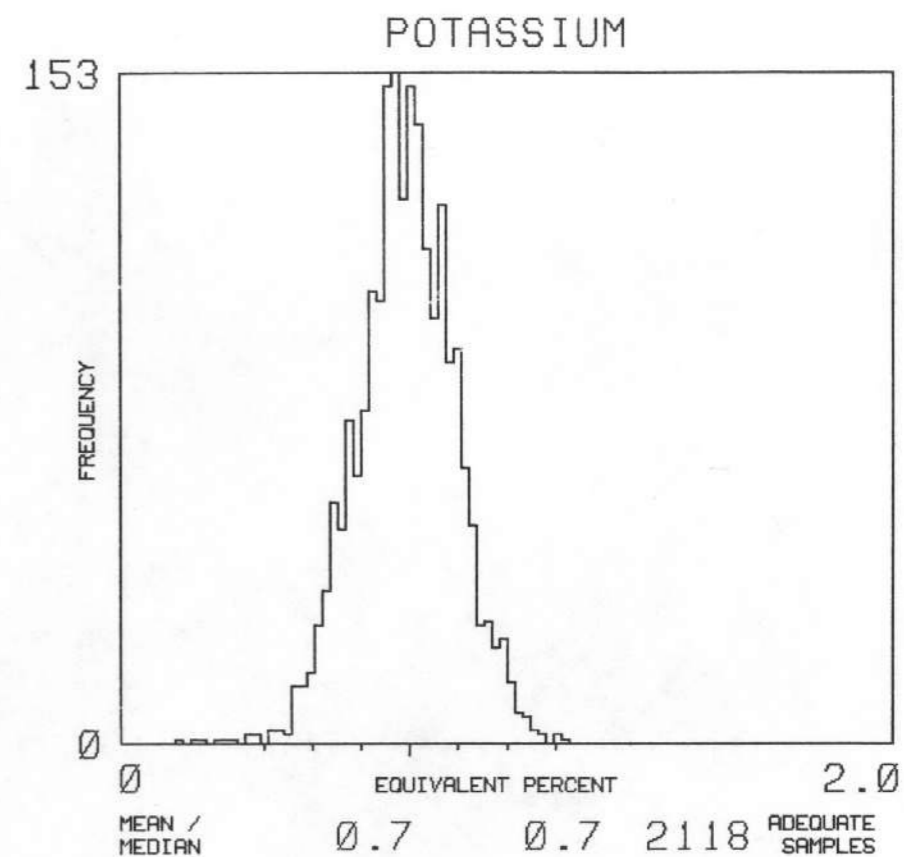
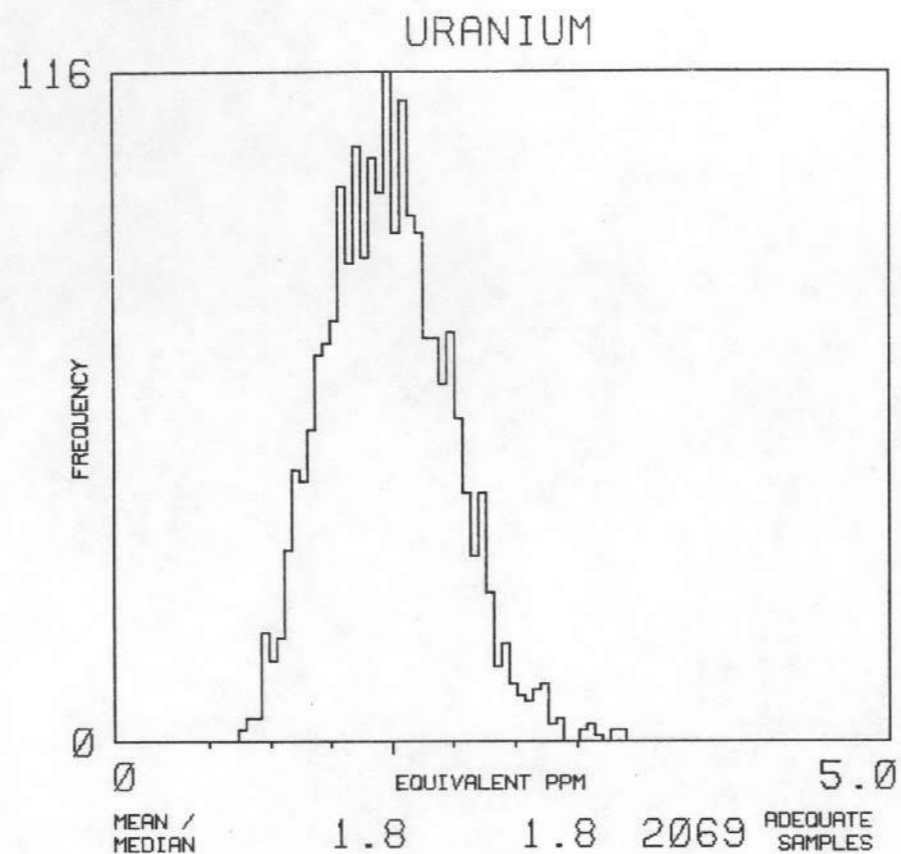
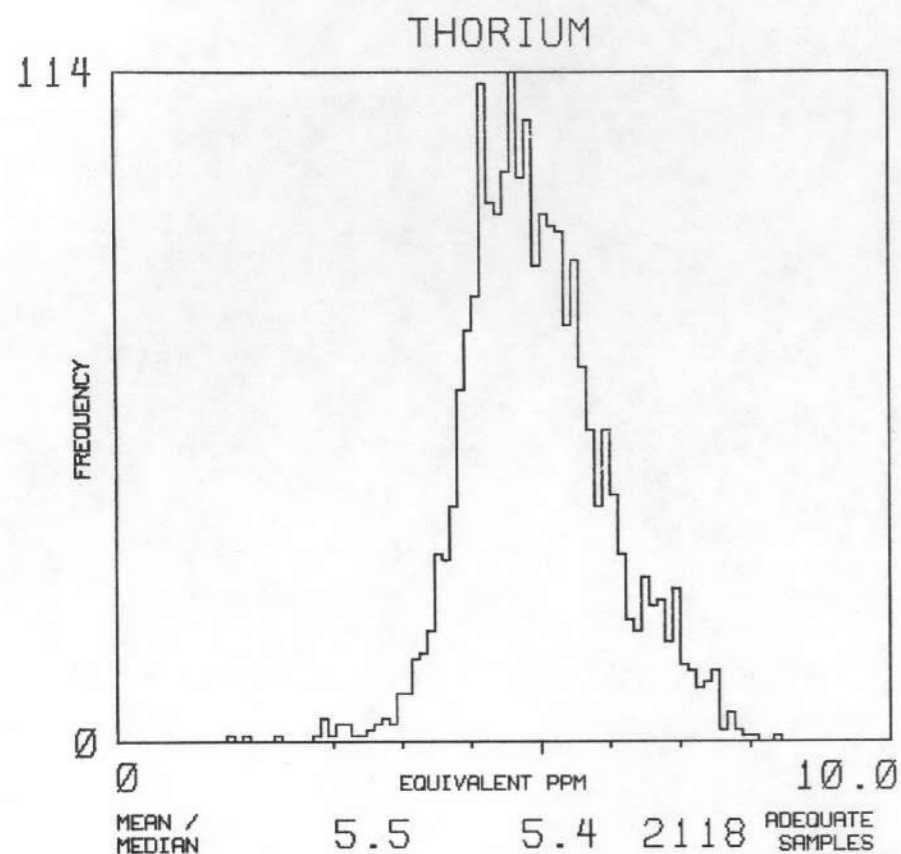


NJ 16-5

VINCENNES

MAP UNIT : MST

TOTAL NUMBER OF SAMPLES 2118

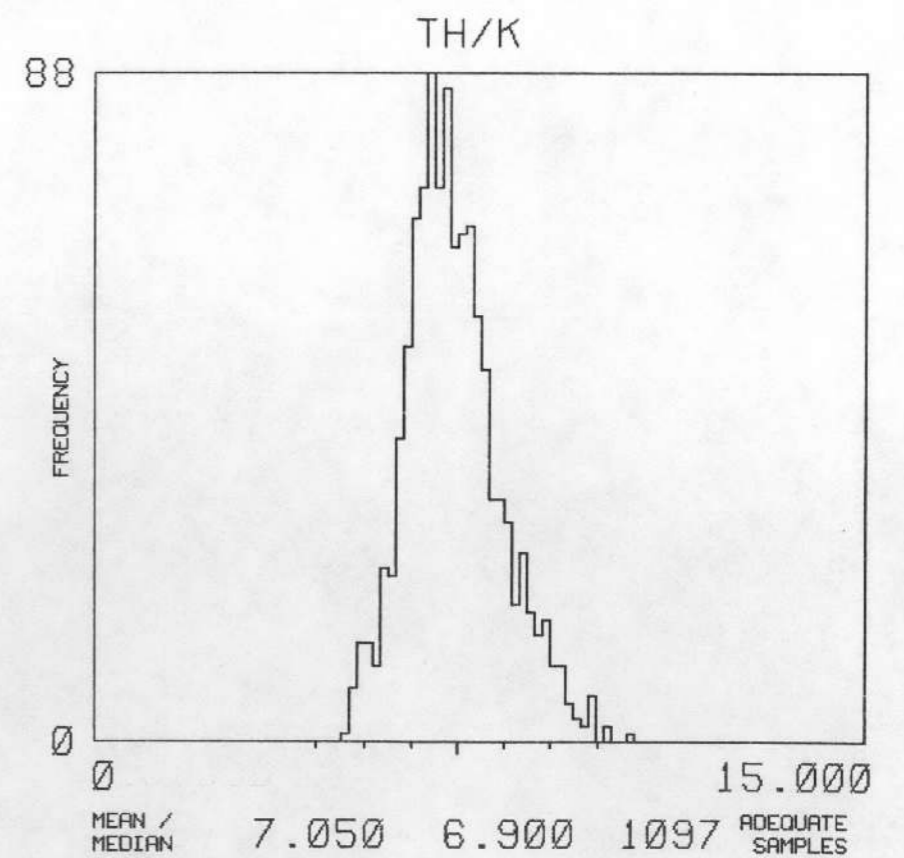
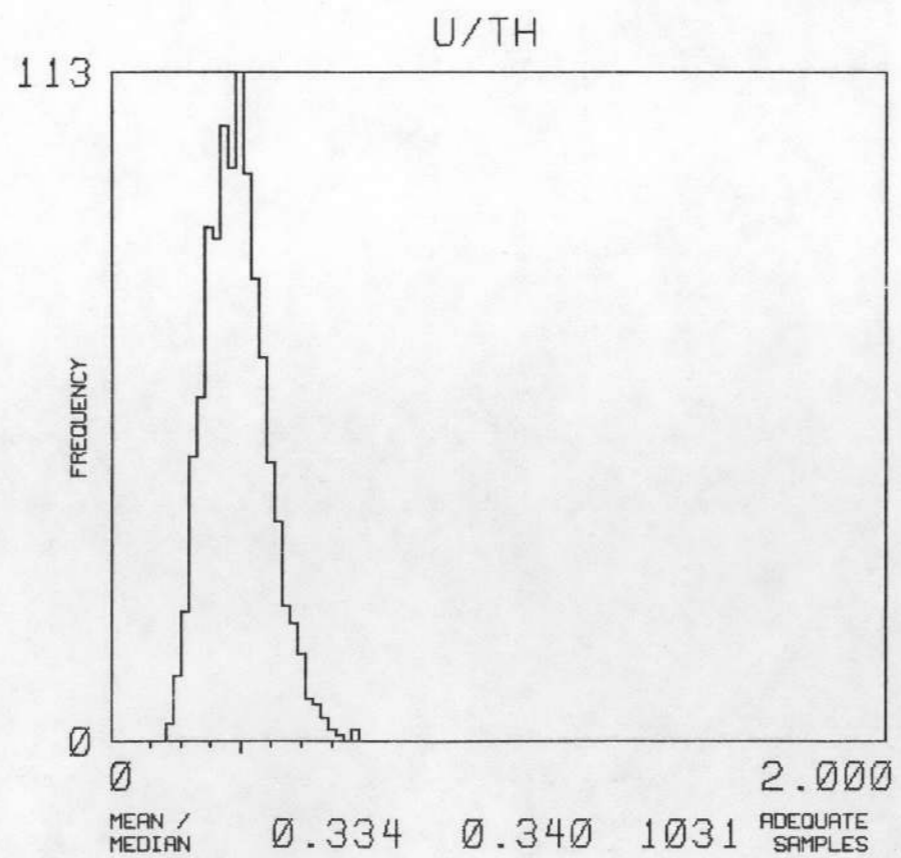
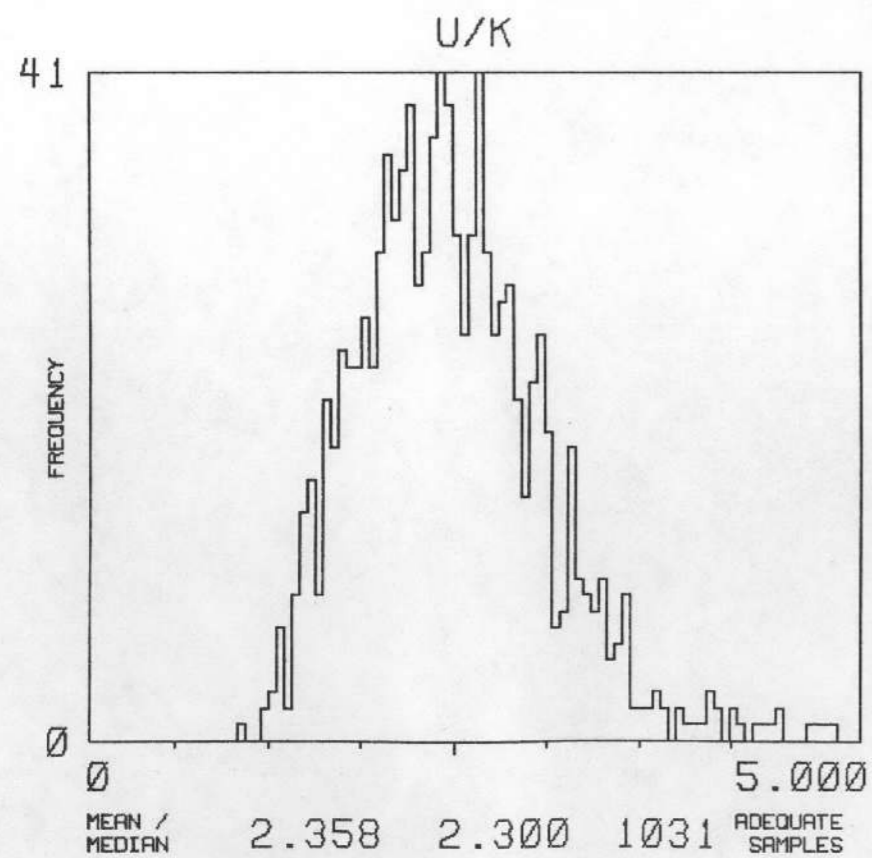
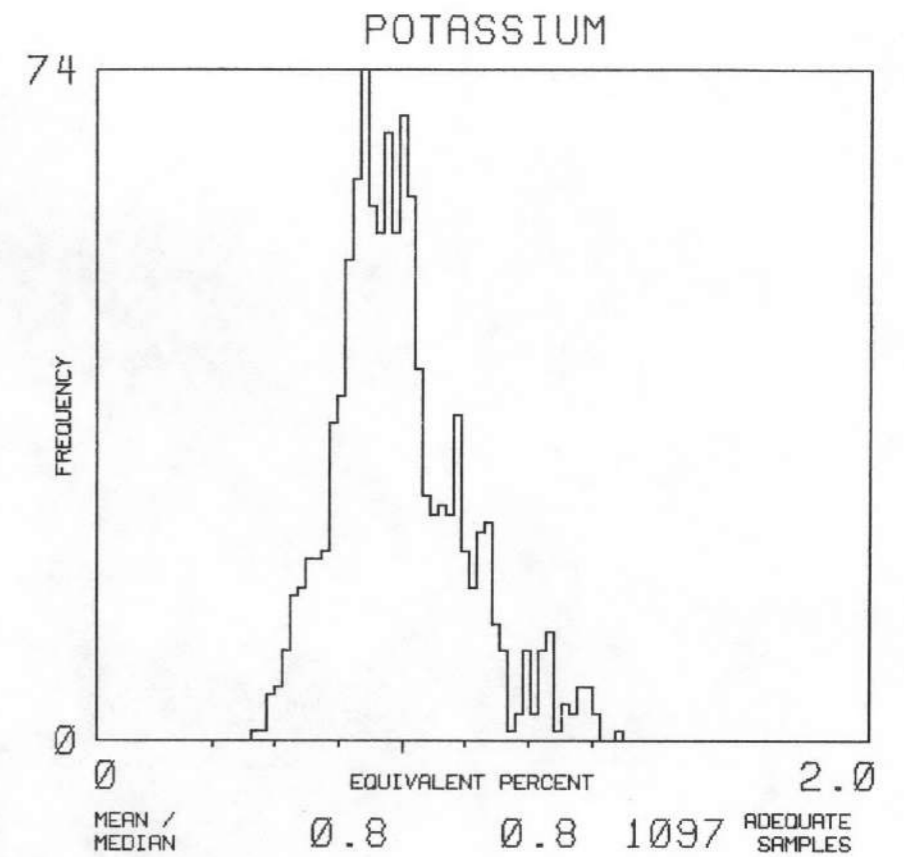
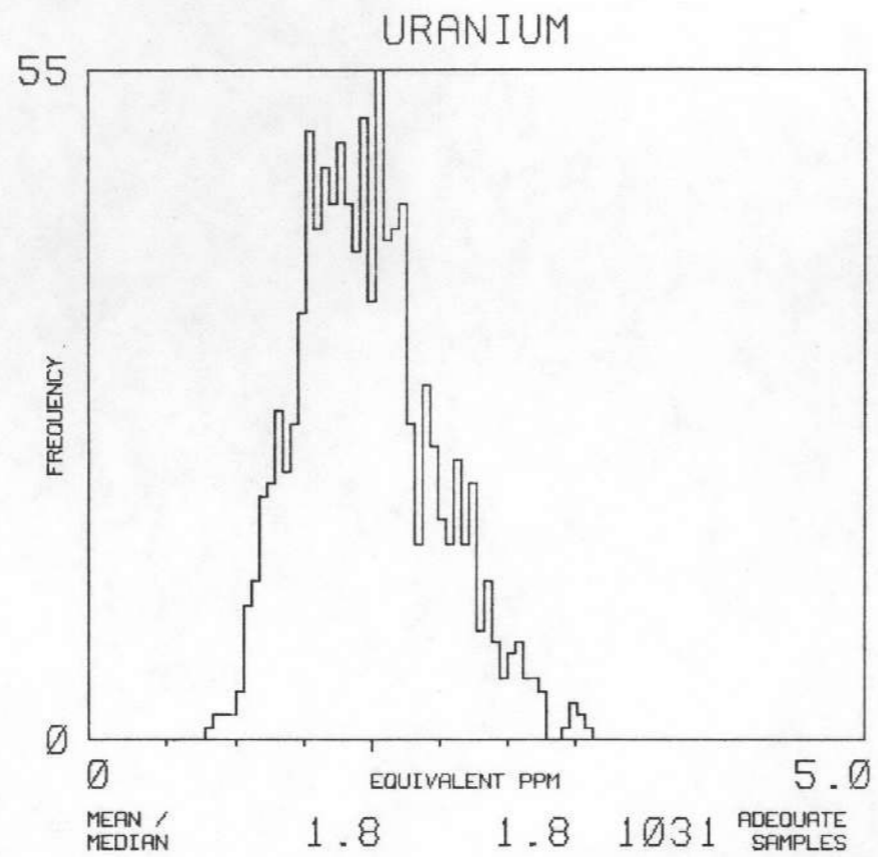
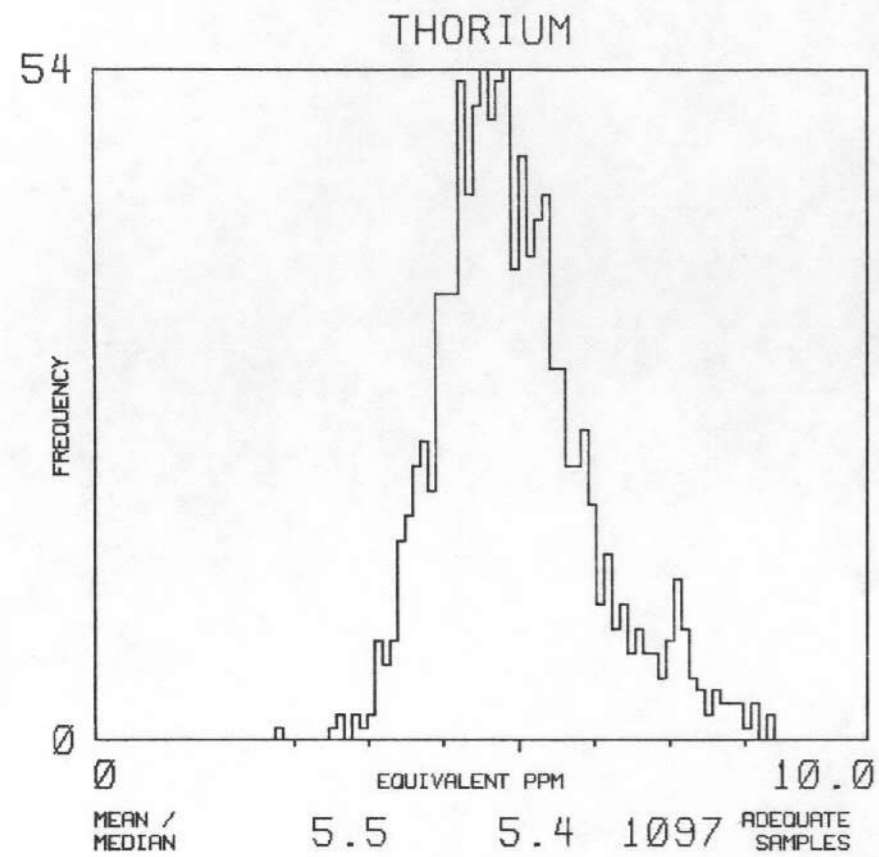


NJ 16-5

VINCENNES

MAP UNIT : MWB

TOTAL NUMBER OF SAMPLES 1097

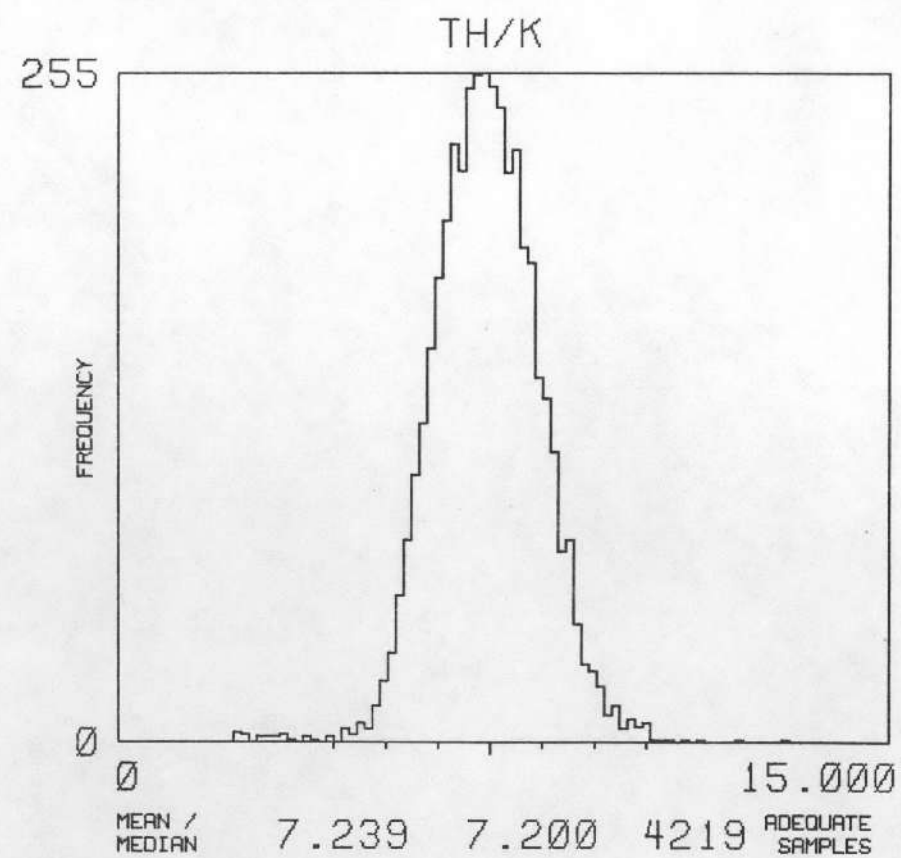
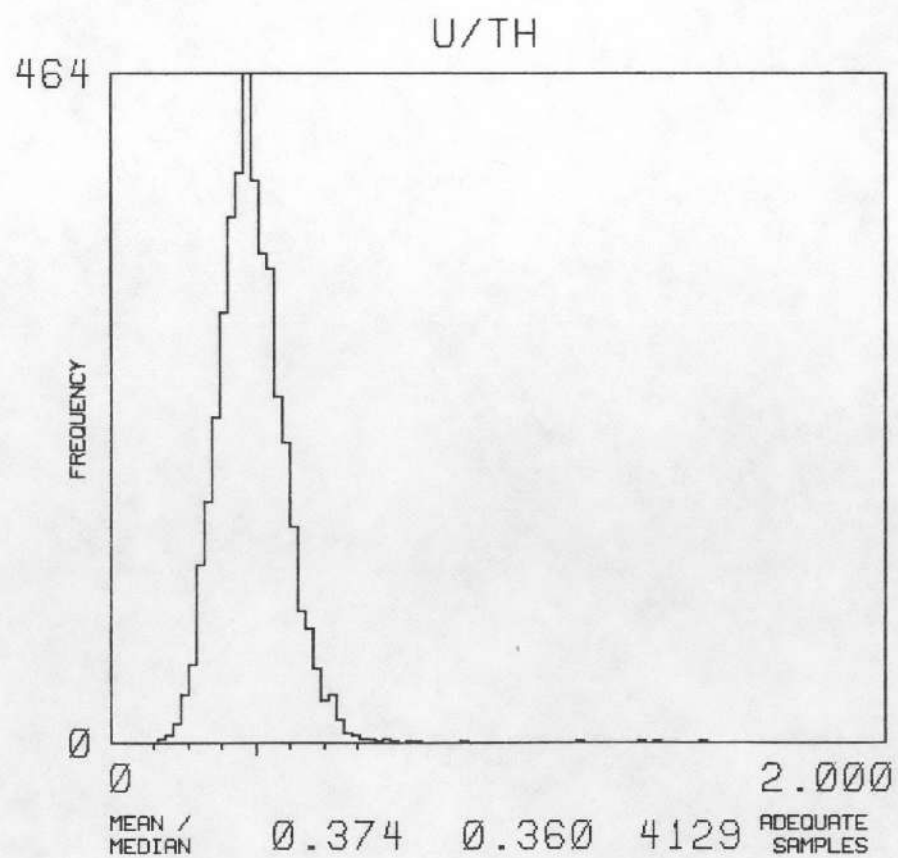
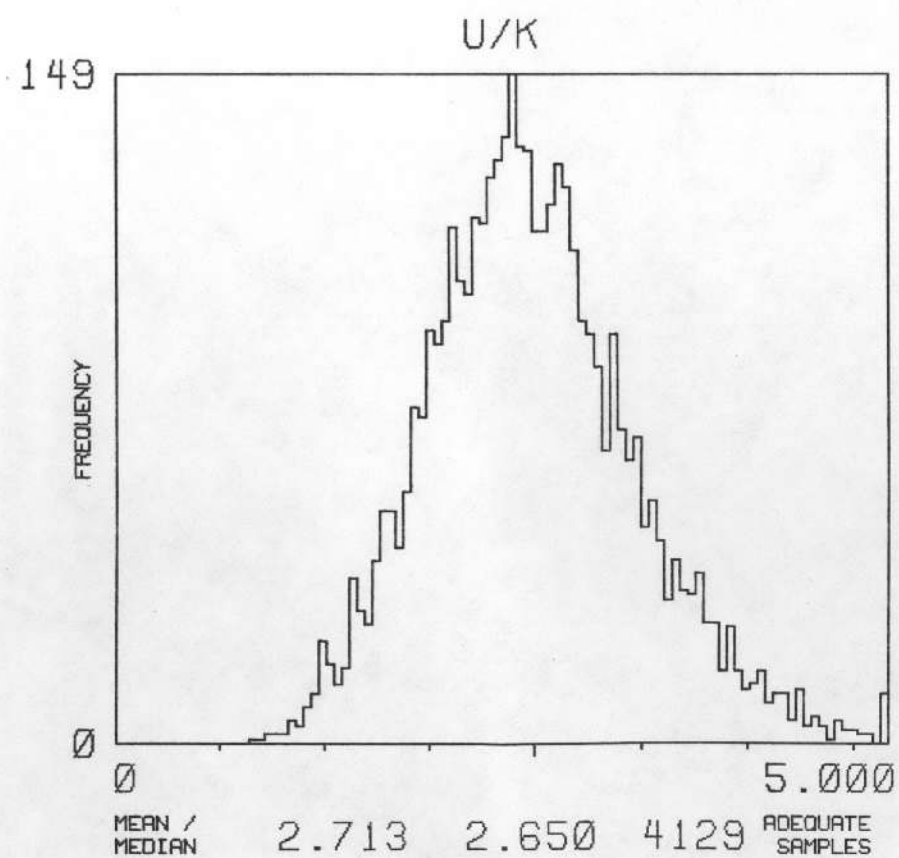
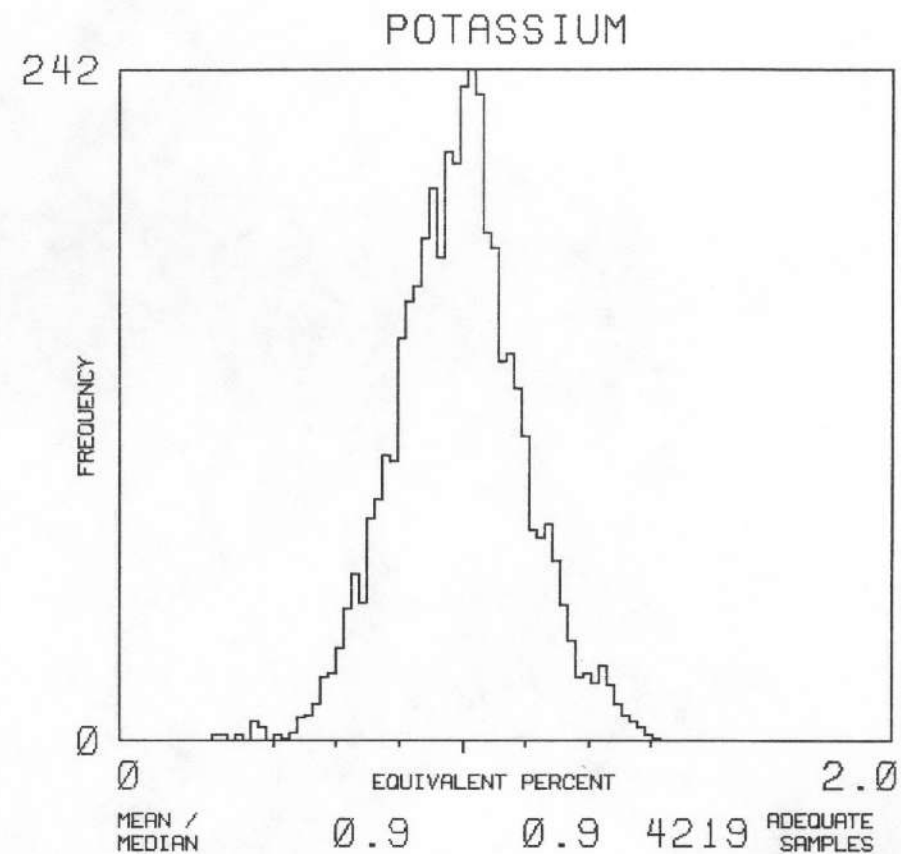
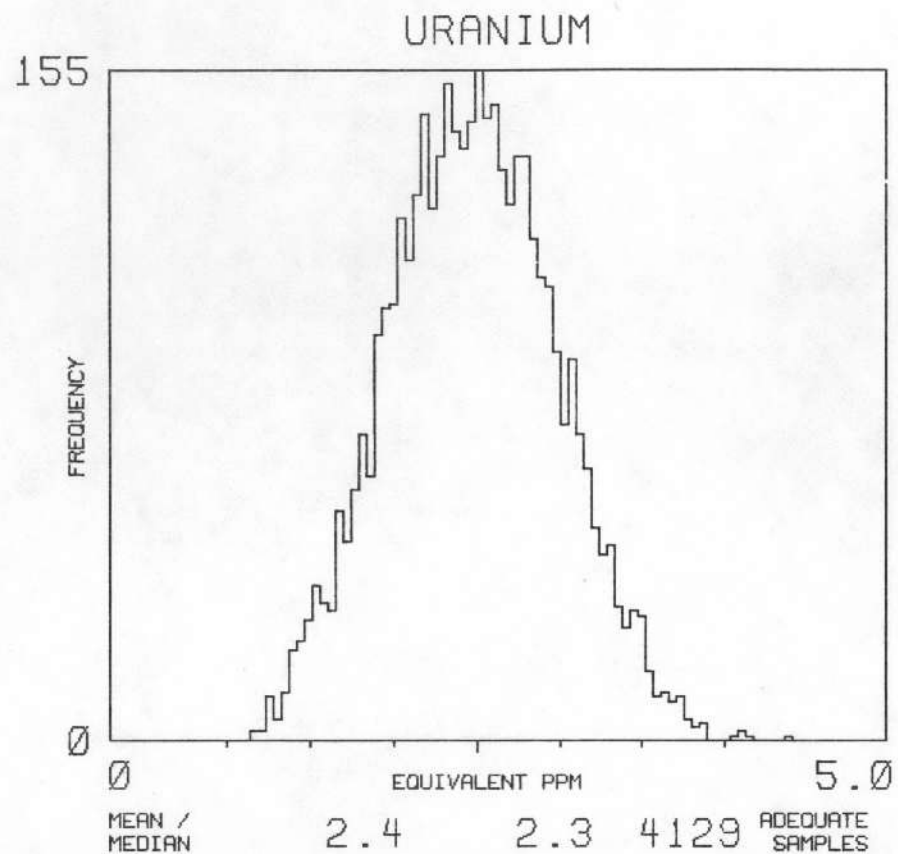
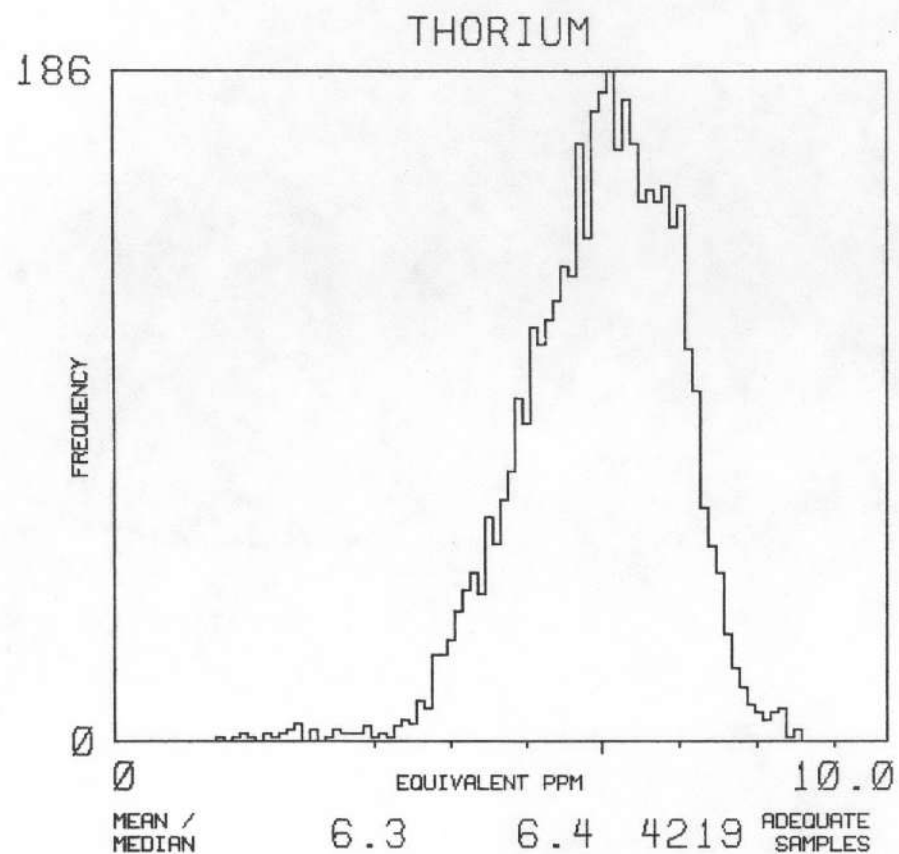


NJ 16-5

VINCENNES

MAP UNIT : MBR

TOTAL NUMBER OF SAMPLES 4219

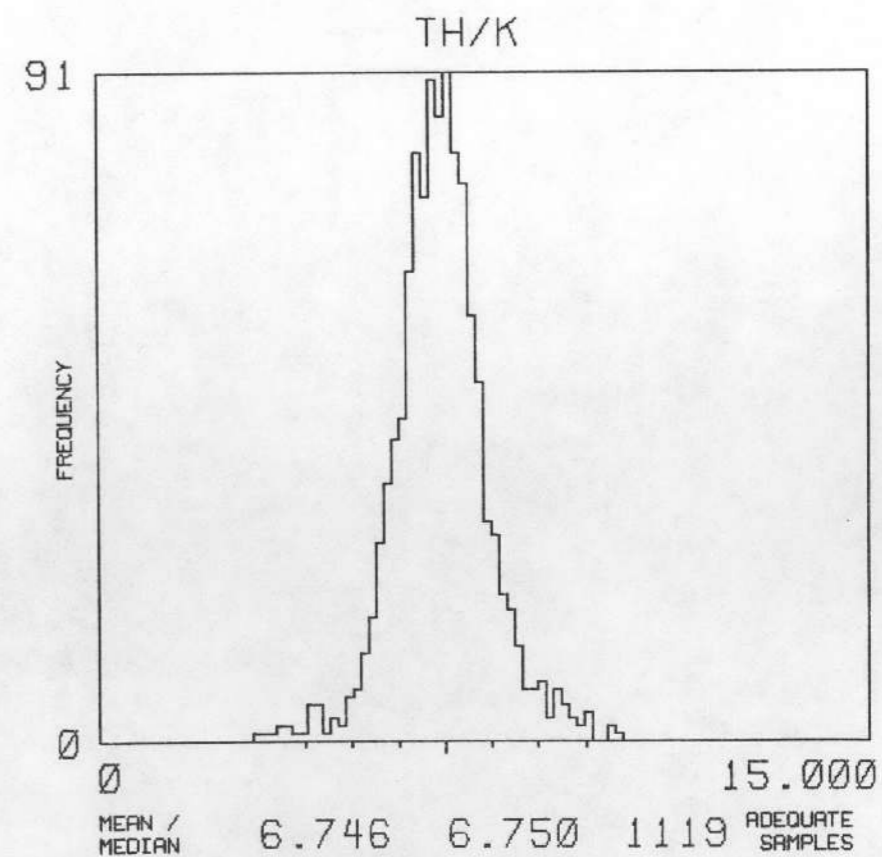
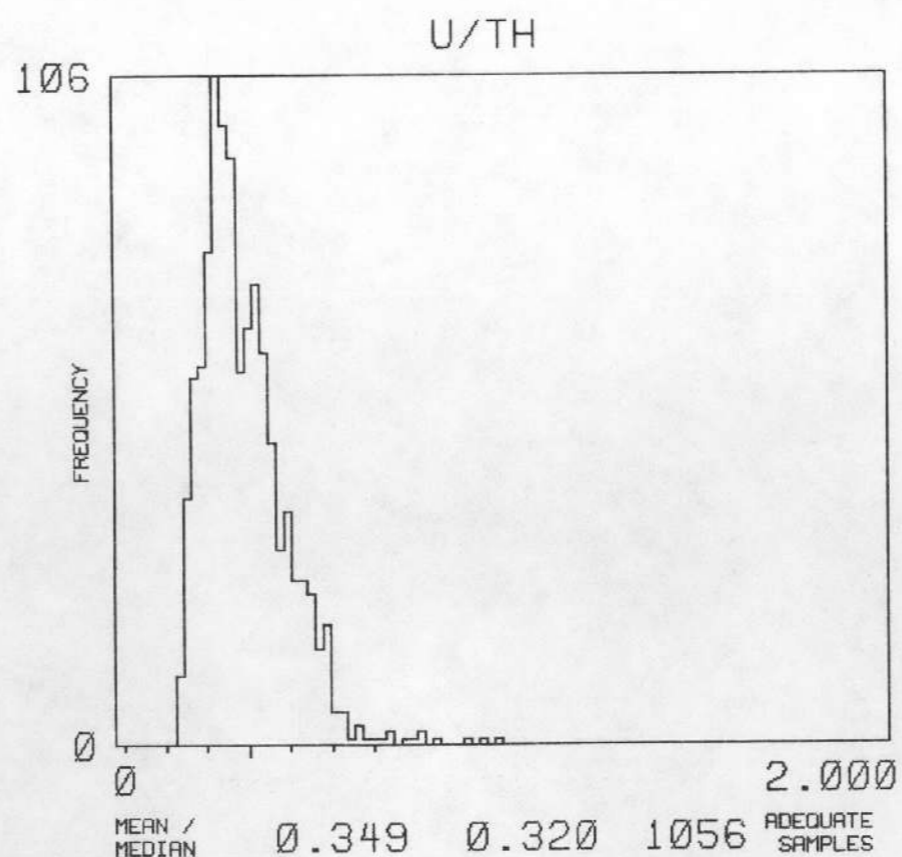
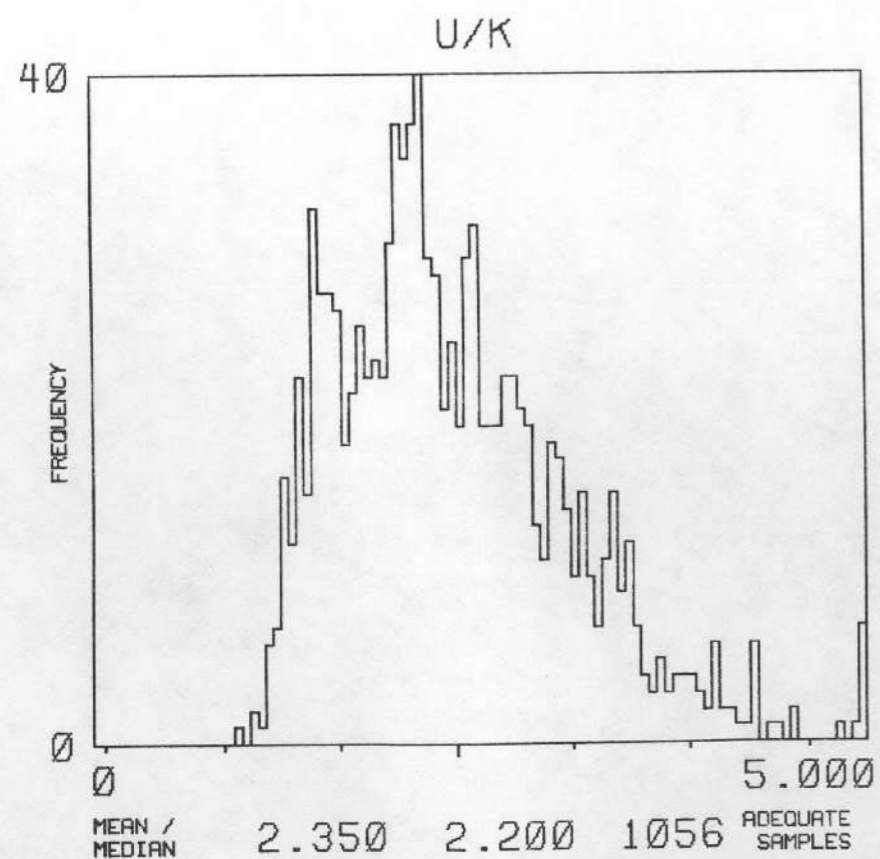
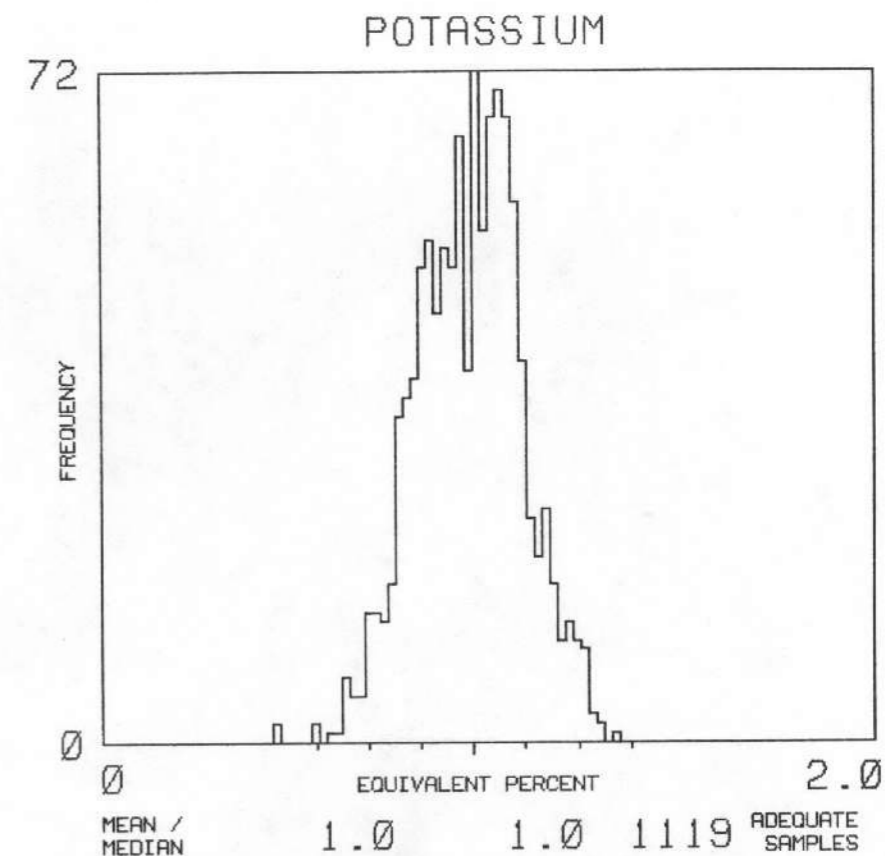
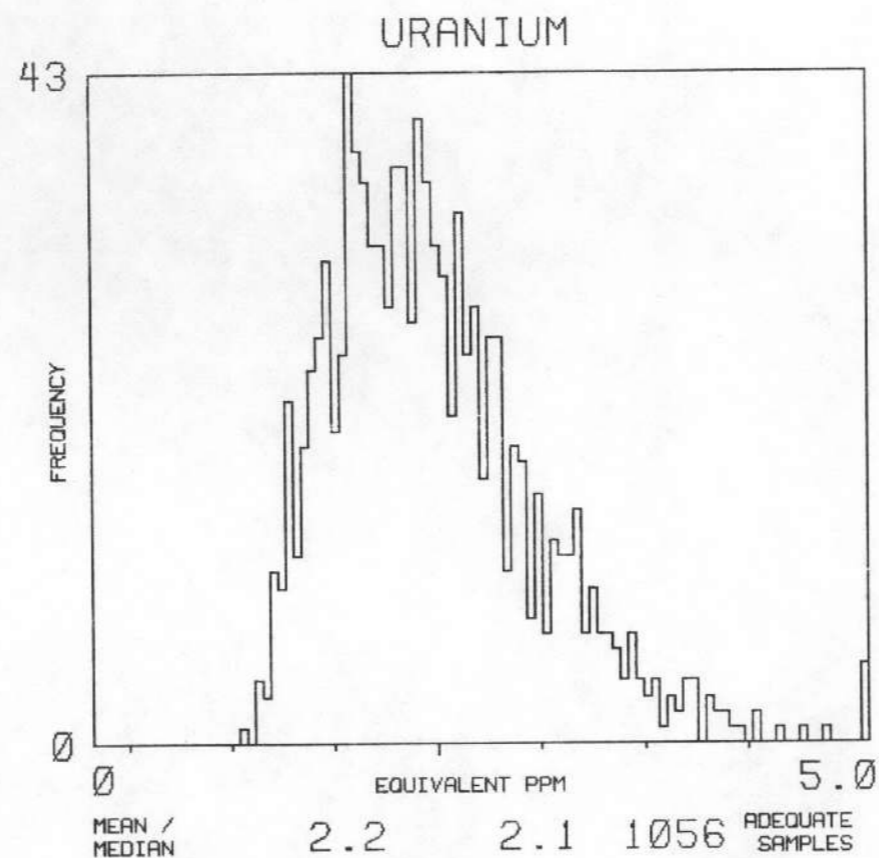
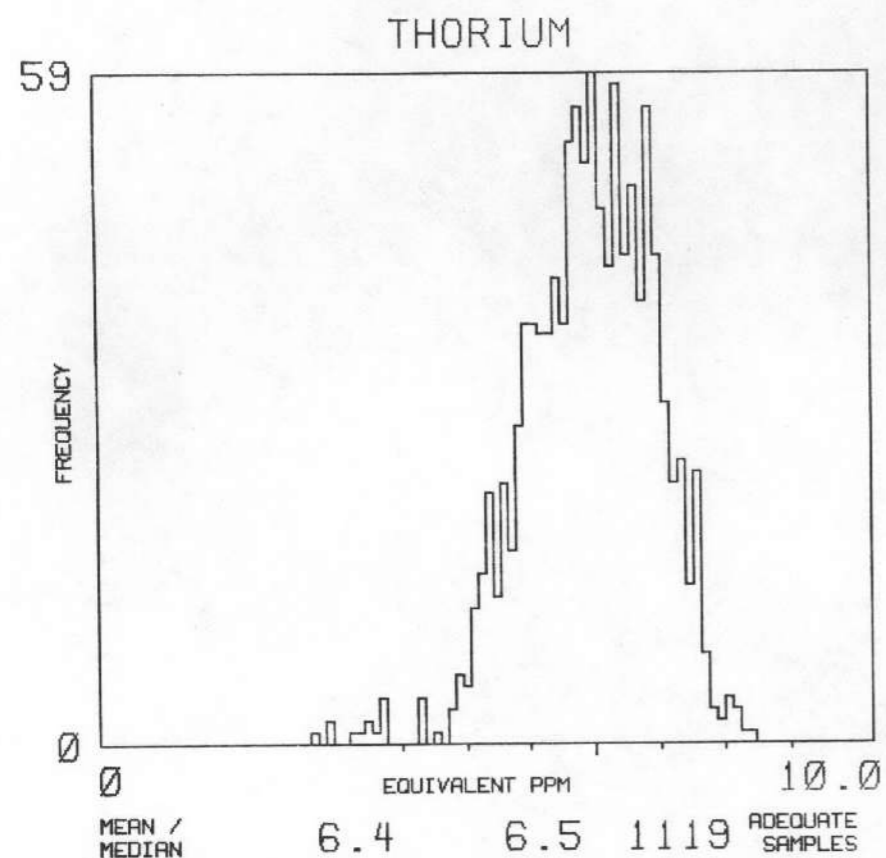


NJ 16-5

VINCENNES

MAP UNIT : MS

TOTAL NUMBER OF SAMPLES 1119

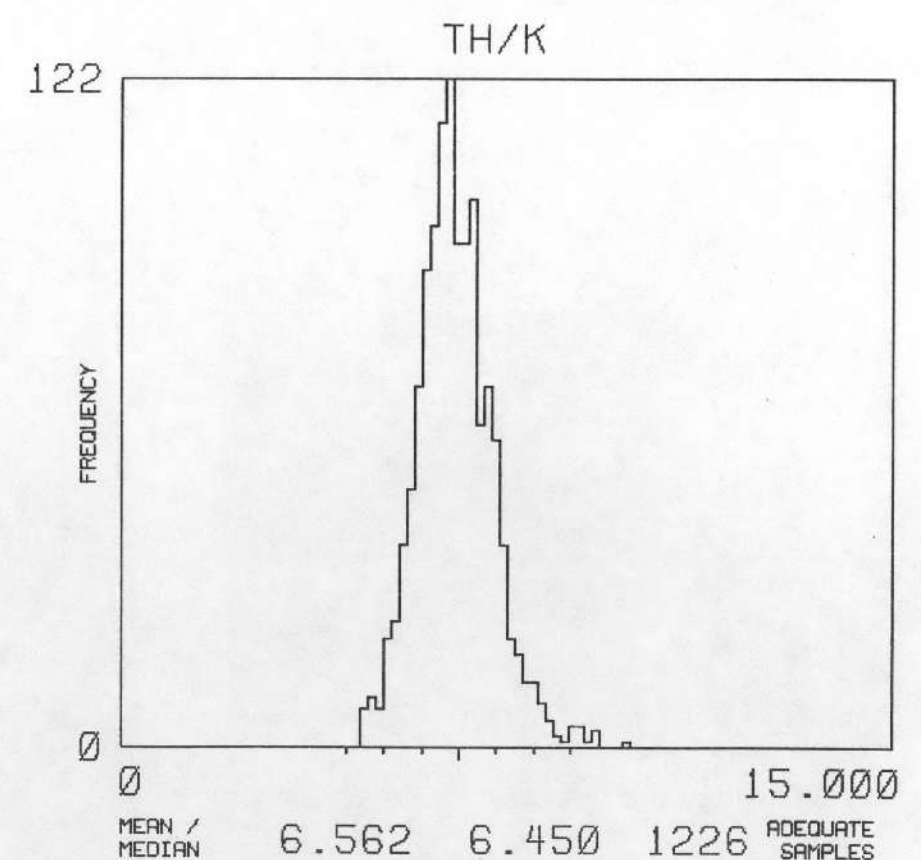
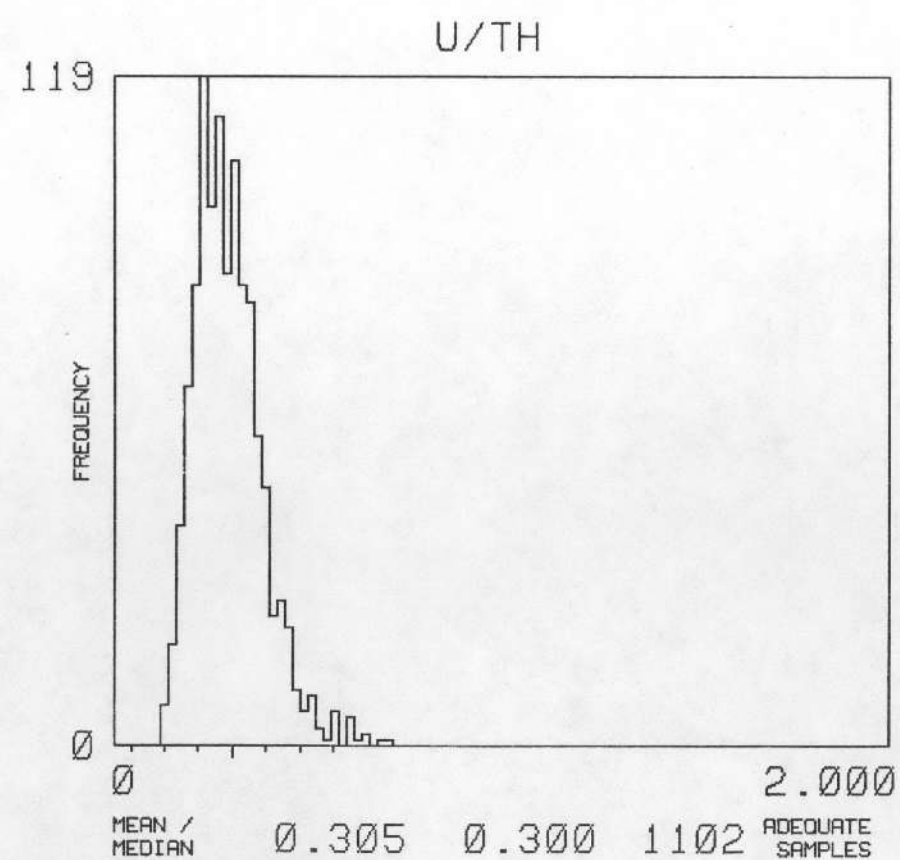
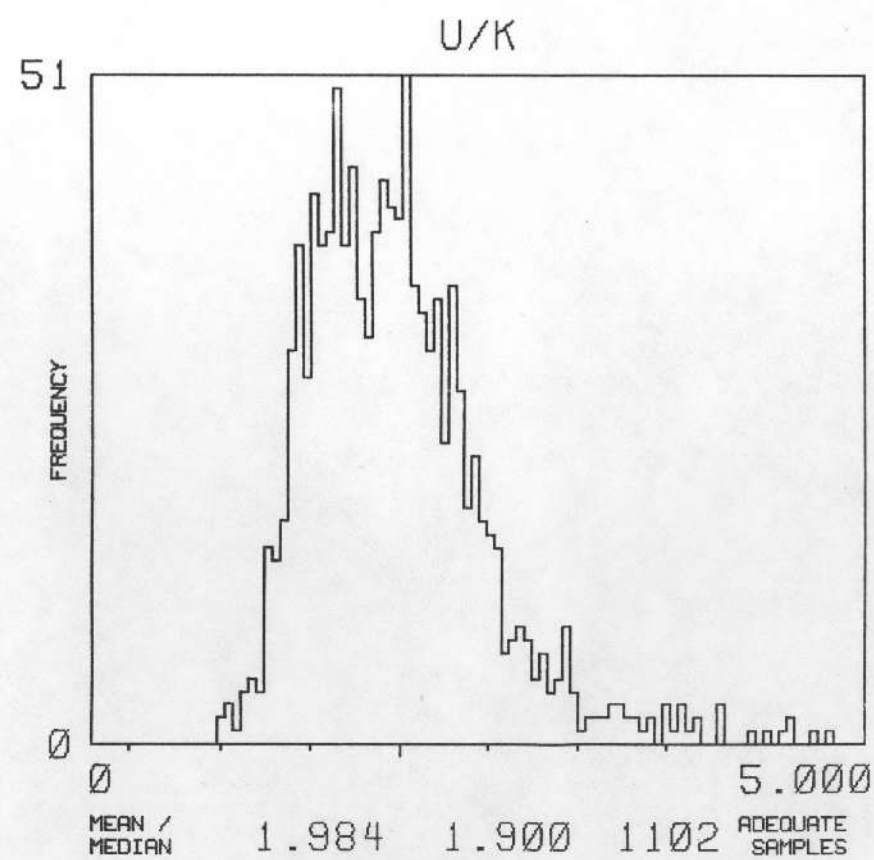
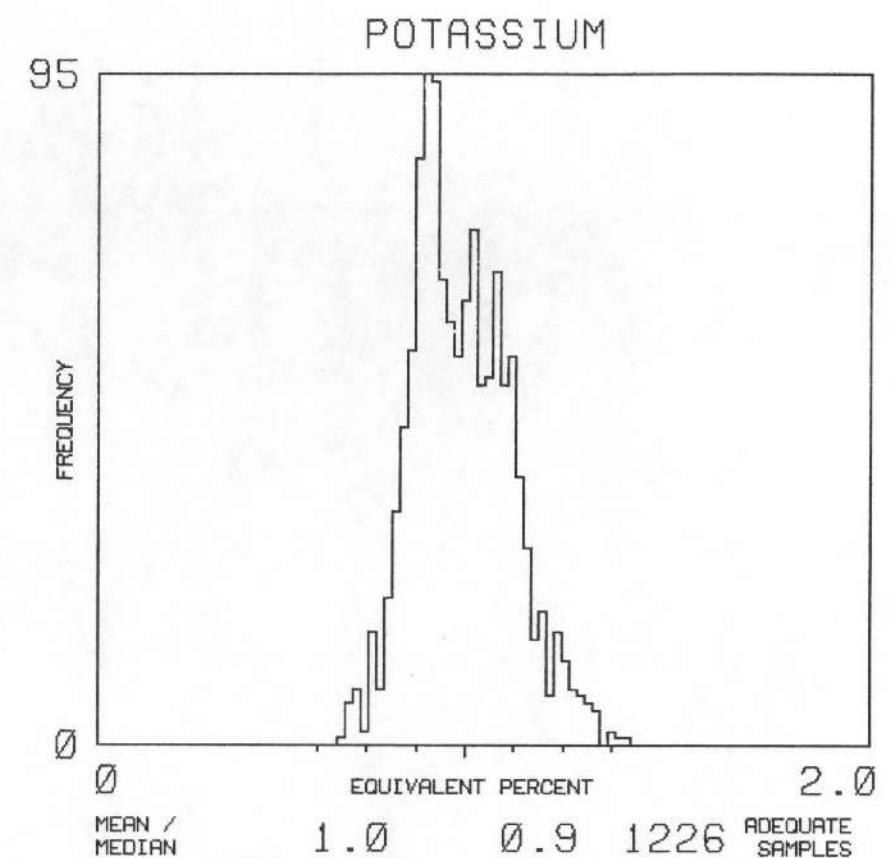
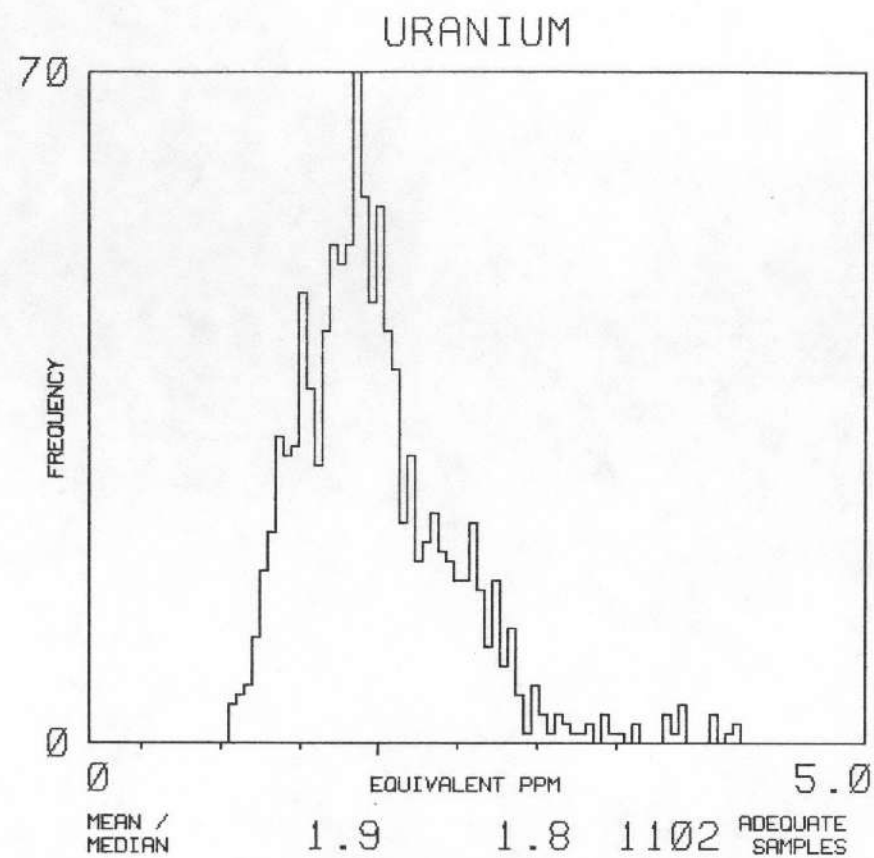
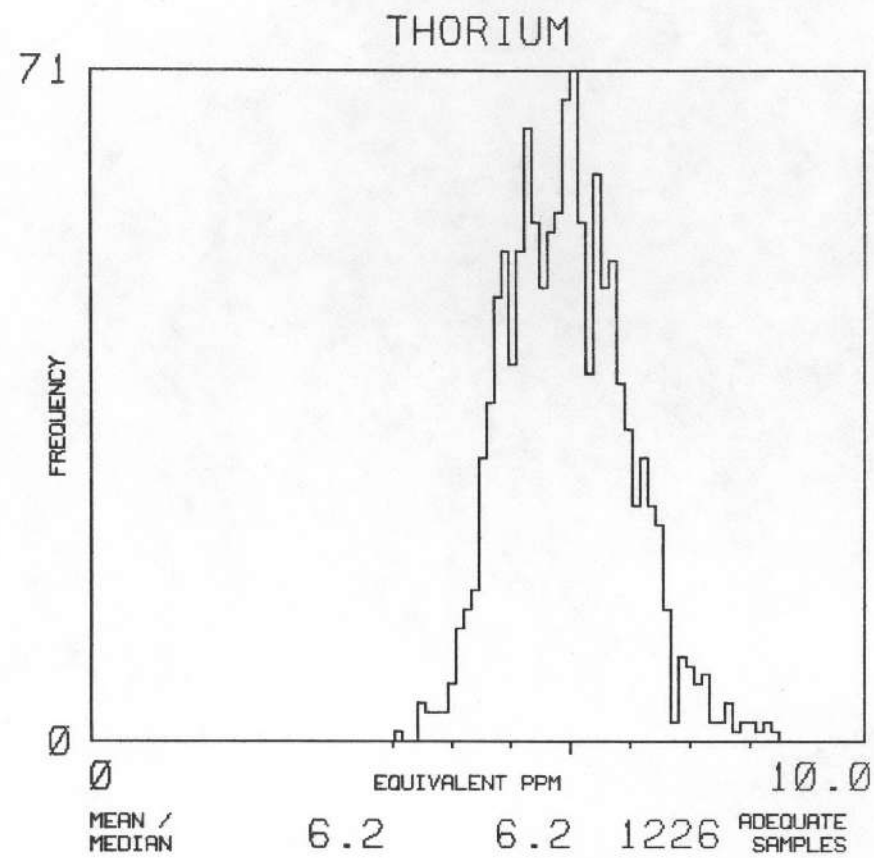


NJ 16-5

VINCENNES

MAP UNIT : MB

TOTAL NUMBER OF SAMPLES 1226



VINCENNES QUADRANGLE

Computer Map Unit Symbol Conversion Table

<u>Computer Map Unit Symbol</u>	<u>Geologic Map Unit Symbol</u>
QM	Qm
QC	QC
QPL	Qpl
QL	Ql
QCL	Qcl
QGV	Qgv
QGP	Qgp
QSI	Qsi
* QGK	Qgk
QTI	Qti
PMC	Pmc
PC	Pc
PRC	Prc
ME	Me
MST	Mst
MWB	Mwb
MBR	Mbr
MS	Ms
MB	Mb

NOTES:

On the following pages, histograms for each computer map unit are included in the same order as they appear on the above list.

Geologic descriptions of original geologic map units are in Appendix A.

Areas over water or cultural features were assigned separate map unit symbols and were removed from the data block during processing.

*Statistical analysis was not performed on these units due to there being an inadequate number of samples.

**APPENDIX G - Uranium Anomaly Summary and
Statistical Tables**

ANOMALY SUMMARY TABLE						PEAK PPM	NUMBER OF SAMPLES WITH A STANDARD DEVIATION OF :										
ANOMALY	FLIGHT	COMPUTER	MAP UNIT	AND NO.	ANOMALOUS SAMPLES IN UNIT		1	2	3	4	5	6	7	GT7			
51 C	800	QC	/	1QCL	/	3PRC	/	3	2.7	5	2	0	0	0	0	0	0
52 C	800	PRC	/	3	/	0	/	0	2.9	2	1	0	0	0	0	0	0
53 C	800	MST	/	1MC	/	3PRC	/	1QSI	3.2	4	2	2	0	0	0	0	0
54 C	800	PRC	/	3MST	/	1	/	0	2.8	1	2	1	0	0	0	0	0
55 C	800	MST	/	3MWB	/	1	/	0	2.8	3	1	0	0	0	0	0	0
56 C	800	MBR	/	2	/	0	/	0	3.7	1	0	1	0	0	0	0	0
57 C	800	MWB	/	1MBR	/	2	/	0	3.2	2	0	1	0	0	0	0	0
58 C	800	MS	/	2MBR	/	1	/	0	3.6	2	1	0	0	0	0	0	0
59 C	810	QC	/	1QL	/	1	/	0	3.7	0	1	1	0	0	0	0	0
60 C	810	PMC	/	1PC	/	4	/	0	4.7	1	0	4	0	0	0	0	0
61 C	810	PC	/	1QM	/	1QCL	/	2	4.5	1	1	2	0	0	0	0	0
62 C	810	PRC	/	3	/	0	/	0	2.8	2	1	0	0	0	0	0	0
63 C	810	PRC	/	1QC	/	1	/	0	3.4	1	0	1	0	0	0	0	0
64 C	810	MBR	/	6	/	0	/	0	3.5	3	3	0	0	0	0	0	0
65 C	820	QM	/	1PC	/	1QCL	/	1	3.2	2	1	0	0	0	0	0	0
66 C	820	QCL	/	1	/	0	/	0	3.6	0	0	1	0	0	0	0	0
67 C	820	MST	/	2MWB	/	1	/	0	3.2	0	1	1	1	0	0	0	0
68 C	830	PRC	/	5	/	0	/	0	2.7	3	2	0	0	0	0	0	0
69 C	830	QC	/	2	/	0	/	0	3.0	0	2	0	0	0	0	0	0
70 C	830	MBR	/	2	/	0	/	0	3.3	0	2	0	0	0	0	0	0
71 C	840	QL	/	2	/	0	/	0	3.1	0	2	0	0	0	0	0	0
72 C	840	QL	/	1	/	0	/	0	3.7	0	0	1	0	0	0	0	0
73 C	840	QL	/	1	/	0	/	0	3.7	0	0	1	0	0	0	0	0
74 C	840	QL	/	3QM	/	1	/	0	3.9	0	2	2	0	0	0	0	0
75 C	840	MBR	/	4	/	0	/	0	3.5	0	4	0	0	0	0	0	0
76 C	840	QC	/	1	/	0	/	0	3.4	0	0	1	0	0	0	0	0
77 C	1010	QL	/	5	/	0	/	0	3.8	1	3	1	0	0	0	0	0
78 C	1010	QL	/	4	/	0	/	0	2.9	2	2	0	0	0	0	0	0
79 C	1010	QTI	/	5	/	0	/	0	3.0	3	2	0	0	0	0	0	0
80 C	1030	QL	/	4	/	0	/	0	3.2	2	2	0	0	0	0	0	0
81 C	1030	PC	/	1QM	/	1	/	0	5.1	0	1	1	0	0	0	0	0
82 C	1030	PC	/	1QM	/	2	/	0	5.3	0	1	2	0	0	0	0	0
83 C	1040	PRC	/	4	/	0	/	0	2.7	3	1	0	0	0	0	0	0
84 C	1050	MST	/	1	/	0	/	0	2.8	0	0	1	0	0	0	0	0
85 C	1050	MST	/	4	/	0	/	0	2.4	3	1	0	0	0	0	0	0
86 C	1060	MBR	/	2	/	0	/	0	3.7	0	2	0	0	0	0	0	0
87 C	1060	MBR	/	3	/	0	/	0	3.2	2	1	0	0	0	0	0	0
88 C	1060	MBR	/	3	/	0	/	0	3.2	1	2	0	0	0	0	0	0

NOTES: M INDICATES THAT THE ANOMALY LIES OVER
A URANIUM MINE OR PROSPECT.

C INDICATES THAT THE ANOMALY LIES OVER A CULTURAL FEATURE.

W INDICATES POSSIBLE INTERFERENCE BY WEATHER PHENOMENA.

		MAP UNIT QM						
		-3	-2	-1	0	+1	+2	+3
POTASIMUM	DIST NORMAL	0.5737	0.7561	0.9385	1.1209	1.3033	1.4857	1.6681
URANIUM	DIST NORMAL	0.2309	1.0279	1.8249	2.6219	3.4189	4.2159	5.0129
THORIUM	DIST NORMAL	3.3092	4.4630	5.6168	6.7706	7.9244	9.0782	10.2320
U/K	DIST NORMAL	0.0390	0.8181	1.5972	2.3763	3.1554	3.9345	4.7136
U/TH	DIST NORMAL	-0.0364	0.1079	0.2522	0.3965	0.5408	0.6851	0.8294
TH/K	DIST NORMAL	4.0317	4.7092	5.3867	6.0642	6.7417	7.4192	8.0967

		MAP UNIT QC						
		-3	-2	-1	0	+1	+2	+3
POTASIMUM	DIST NORMAL	0.3313	0.5818	0.8323	1.0828	1.3333	1.5838	1.8343
URANIUM	DIST NORMAL	0.3458	0.8867	1.4276	1.9685	2.5094	3.0503	3.5912
THORIUM	DIST NORMAL	1.6745	3.0230	4.3715	5.7200	7.0685	8.4170	9.7655
U/K	DIST NORMAL	-0.1137	0.5464	1.2065	1.8666	2.5267	3.1868	3.8469
U/TH	DIST NORMAL	0.0424	0.1422	0.2420	0.3418	0.4416	0.5414	0.6412
TH/K	DIST NORMAL	1.4801	2.7966	4.1131	5.4296	6.7461	8.0626	9.3791

		MAP UNIT QPL						
		-3	-2	-1	0	+1	+2	+3
POTASIMUM	DIST NORMAL	0.7296	0.8497	0.9698	1.0899	1.2100	1.3301	1.4502
URANIUM	DIST NORMAL	0.2995	0.6942	1.0889	1.4836	1.8783	2.2730	2.6677
THORIUM	DIST NORMAL	-0.4258	0.9162	2.2582	3.6002	4.9422	6.2842	7.6262
U/K	DIST NORMAL	0.3029	0.6492	0.9955	1.3418	1.6881	2.0344	2.3807
U/TH	DIST NORMAL	0.0392	0.1621	0.2850	0.4079	0.5308	0.6537	0.7766
TH/K	DIST NORMAL	-0.0392	1.0700	2.1792	3.2884	4.3976	5.5068	6.6160

		MAP UNIT QL						
		-3	-2	-1	0	+1	+2	+3
POTASIMUM	DIST NORMAL	0.6802	0.8388	0.9974	1.1560	1.3146	1.4732	1.6318
URANIUM	DIST NORMAL	0.6509	1.1418	1.6327	2.1236	2.6145	3.1054	3.5963
THORIUM	DIST NORMAL	3.1554	4.2397	5.3240	6.4083	7.4926	8.5769	9.6612
U/K	DIST NORMAL	0.3913	0.8824	1.3735	1.8646	2.3557	2.8468	3.3379
U/TH	DIST NORMAL	0.0895	0.1713	0.2531	0.3349	0.4167	0.4985	0.5803
TH/K	DIST NORMAL	2.4770	3.5196	4.5622	5.6048	6.6474	7.6900	8.7326

		MAP UNIT QCL						
		-3	-2	-1	0	+1	+2	+3
POTASIMUM	DIST NORMAL	0.6115	0.7899	0.9683	1.1467	1.3251	1.5035	1.6819
URANIUM	DIST NORMAL	0.5927	1.0862	1.5797	2.0732	2.5667	3.0602	3.5537
THORIUM	DIST NORMAL	2.9159	4.0559	5.1959	6.3359	7.4759	8.6159	9.7559
U/K	DIST NORMAL	0.2827	0.8016	1.3205	1.8394	2.3583	2.8772	3.3961
U/TH	DIST NORMAL	0.0744	0.1590	0.2436	0.3282	0.4128	0.4974	0.5820
TH/K	DIST NORMAL	2.2894	3.3934	4.4974	5.6014	6.7054	7.8094	8.9134

		MAP UNIT QGV						
		-3	-2	-1	0	+1	+2	+3
POTASIMUM	DIST NORMAL	0.5671	0.7348	0.9025	1.0702	1.2379	1.4056	1.5733
URANIUM	DIST NORMAL	0.2689	0.7267	1.1845	1.6423	2.1001	2.5579	3.0157
THORIUM	DIST NORMAL	0.2327	1.5804	2.9281	4.2758	5.6235	6.9712	8.3189
U/K	DIST NORMAL	0.1020	0.5716	1.0412	1.5108	1.9804	2.4500	2.9196
U/TH	DIST NORMAL	0.0462	0.1550	0.2638	0.3726	0.4814	0.5902	0.6990
TH/K	DIST NORMAL	0.8306	1.8801	2.9296	3.9791	5.0286	6.0781	7.1276

MAP UNIT GGP

			-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL		0. 6262	0. 7288	0. 8314	0. 9340	1. 0366	1. 1392	1. 2418
URANIUM	DIST NORMAL		0. 7489	1. 0269	1. 3049	1. 5829	1. 8609	2. 1389	2. 4169
THORIUM	DIST NORMAL		2. 7857	3. 5450	4. 3043	5. 0636	5. 8229	6. 5822	7. 3415
U/K	DIST NORMAL		0. 6562	1. 0089	1. 3616	1. 7143	2. 0670	2. 4197	2. 7724
U/TH	DIST NORMAL		0. 1144	0. 1825	0. 2506	0. 3187	0. 3868	0. 4549	0. 5230
TH/K	DIST NORMAL		4. 3839	4. 7241	5. 0643	5. 4045	5. 7447	6. 0849	6. 4251

MAP UNIT GSI

			-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL		0. 3409	0. 5053	0. 6697	0. 8341	0. 9985	1. 1629	1. 3273
URANIUM	DIST NORMAL		0. 5557	1. 0802	1. 6047	2. 1292	2. 6537	3. 1782	3. 7027
THORIUM	DIST NORMAL		2. 7010	3. 7332	4. 7654	5. 7976	6. 8298	7. 8620	8. 8942
U/K	DIST NORMAL		0. 2652	1. 0552	1. 8452	2. 6352	3. 4252	4. 2152	5. 0052
U/TH	DIST NORMAL		0. 1228	0. 2050	0. 2872	0. 3694	0. 4516	0. 5338	0. 6160
TH/K	DIST NORMAL		3. 4985	4. 6924	5. 8863	7. 0802	8. 2741	9. 4680	10. 6619

MAP UNIT GTI

			-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL		0. 6430	0. 7777	0. 9124	1. 0471	1. 1818	1. 3165	1. 4512
URANIUM	DIST NORMAL		0. 5623	1. 0444	1. 5265	2. 0086	2. 4907	2. 9728	3. 4549
THORIUM	DIST NORMAL		3. 6107	4. 4423	5. 2739	6. 1055	6. 9371	7. 7687	8. 6003
U/K	DIST NORMAL		0. 4709	0. 9562	1. 4415	1. 9268	2. 4121	2. 8974	3. 3827
U/TH	DIST NORMAL		0. 0707	0. 1575	0. 2443	0. 3311	0. 4179	0. 5047	0. 5915
TH/K	DIST NORMAL		3. 6818	4. 4070	5. 1322	5. 8574	6. 5826	7. 3078	8. 0330

MAP UNIT PMC

			-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL		0. 5762	0. 7702	0. 9642	1. 1582	1. 3522	1. 5462	1. 7402
URANIUM	DIST NORMAL		0. 2516	0. 9368	1. 6220	2. 3072	2. 9924	3. 6776	4. 3628
THORIUM	DIST NORMAL		3. 8336	4. 8581	5. 8826	6. 9071	7. 9316	8. 9561	9. 9806
U/K	DIST NORMAL		0. 8237	1. 2079	1. 5921	1. 9763	2. 3605	2. 7447	3. 1289
U/TH	DIST NORMAL		0. 1285	0. 1963	0. 2641	0. 3319	0. 3997	0. 4675	0. 5353
TH/K	DIST NORMAL		3. 9843	4. 6635	5. 3427	6. 0219	6. 7011	7. 3803	8. 0595

MAP UNIT PC

			-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL		0. 5173	0. 7069	0. 8965	1. 0861	1. 2757	1. 4653	1. 6549
URANIUM	DIST NORMAL		0. 3824	1. 0503	1. 7182	2. 3861	3. 0540	3. 7219	4. 3898
THORIUM	DIST NORMAL		3. 5424	4. 5787	5. 6150	6. 6513	7. 6876	8. 7239	9. 7602
U/K	DIST NORMAL		0. 6547	1. 1728	1. 6909	2. 2090	2. 7271	3. 2452	3. 7633
U/TH	DIST NORMAL		0. 0962	0. 1844	0. 2726	0. 3608	0. 4490	0. 5372	0. 6254
TH/K	DIST NORMAL		3. 9318	4. 6820	5. 4322	6. 1824	6. 9326	7. 6828	8. 4330

MAP UNIT PRC

			-3	-2	-1	0	+1	+2	+3
POTASium	DIST NORMAL		0. 4523	0. 5971	0. 7419	0. 8867	1. 0315	1. 1763	1. 3211
URANIUM	DIST NORMAL		0. 5970	1. 0512	1. 5054	1. 9596	2. 4138	2. 8680	3. 3222
THORIUM	DIST NORMAL		3. 1168	4. 0691	5. 0214	5. 9737	6. 9260	7. 8783	8. 8306
U/K	DIST NORMAL		0. 7148	1. 2202	1. 7256	2. 2310	2. 7364	3. 2418	3. 7472
U/TH	DIST NORMAL		0. 1169	0. 1877	0. 2585	0. 3293	0. 4001	0. 4709	0. 5417
TH/K	DIST NORMAL		4. 3166	5. 1407	5. 9648	6. 7889	7. 6130	8. 4371	9. 2612

			MAP UNIT MC						
			-3	-2	-1	0	+1	+2	+3
POTASium	DIST	NORMAL	0.3588	0.4893	0.6198	0.7503	0.8808	1.0113	1.1418
URANIUM	DIST	NORMAL	0.4304	0.8653	1.3000	1.7347	2.1694	2.6041	3.0388
THORIUM	DIST	NORMAL	3.0533	3.8744	4.6955	5.5166	6.3377	7.1588	7.9799
U/K	DIST	NORMAL	0.4165	1.0586	1.7007	2.3428	2.9849	3.6270	4.2691
U/TH	DIST	NORMAL	0.0792	0.1584	0.2376	0.3168	0.3960	0.4752	0.5544
TH/K	DIST	NORMAL	4.6228	5.5626	6.5024	7.4422	8.3820	9.3218	10.2616

			MAP UNIT MST						
			-3	-2	-1	0	+1	+2	+3
POTASium	DIST	NORMAL	0.3701	0.4956	0.6211	0.7466	0.8721	0.9976	1.1231
URANIUM	DIST	NORMAL	0.6135	1.0083	1.4031	1.7979	2.1927	2.5875	2.9823
THORIUM	DIST	NORMAL	2.7789	3.6827	4.5865	5.4903	6.3941	7.2979	8.2017
U/K	DIST	NORMAL	0.4954	1.1520	1.8086	2.4652	3.1218	3.7784	4.4350
U/TH	DIST	NORMAL	0.0934	0.1729	0.2524	0.3319	0.4114	0.4909	0.5704
TH/K	DIST	NORMAL	4.1699	5.2617	6.3535	7.4453	8.5371	9.6289	10.7207

			MAP UNIT MWB						
			-3	-2	-1	0	+1	+2	+3
POTASium	DIST	NORMAL	0.2980	0.4616	0.6252	0.7888	0.9524	1.1160	1.2796
URANIUM	DIST	NORMAL	0.5048	0.9446	1.3844	1.8242	2.2640	2.7038	3.1436
THORIUM	DIST	NORMAL	2.5478	3.5277	4.5076	5.4875	6.4674	7.4473	8.4272
U/K	DIST	NORMAL	0.5507	1.1531	1.7555	2.3579	2.9603	3.5627	4.1651
U/TH	DIST	NORMAL	0.1006	0.1785	0.2564	0.3343	0.4122	0.4901	0.5680
TH/K	DIST	NORMAL	4.3252	5.2335	6.1418	7.0501	7.9584	8.8667	9.7750

			MAP UNIT MBR						
			-3	-2	-1	0	+1	+2	+3
POTASium	DIST	NORMAL	0.3989	0.5618	0.7247	0.8876	1.0505	1.2134	1.3763
URANIUM	DIST	NORMAL	0.7526	1.2882	1.8238	2.3594	2.8950	3.4306	3.9662
THORIUM	DIST	NORMAL	3.3522	4.3469	5.3416	6.3363	7.3310	8.3257	9.3204
U/K	DIST	NORMAL	0.6566	1.3421	2.0276	2.7131	3.3986	4.0841	4.7696
U/TH	DIST	NORMAL	0.1095	0.1975	0.2855	0.3735	0.4615	0.5495	0.6375
TH/K	DIST	NORMAL	4.2035	5.2153	6.2271	7.2389	8.2507	9.2625	10.2743

			MAP UNIT MS						
			-3	-2	-1	0	+1	+2	+3
POTASium	DIST	NORMAL	0.5563	0.6916	0.8269	0.9622	1.0975	1.2328	1.3681
URANIUM	DIST	NORMAL	0.2372	0.9013	1.5654	2.2295	2.8936	3.5577	4.2218
THORIUM	DIST	NORMAL	3.9056	4.7449	5.5842	6.4235	7.2628	8.1021	8.9414
U/K	DIST	NORMAL	0.0745	0.8331	1.5917	2.3503	3.1089	3.8675	4.6261
U/TH	DIST	NORMAL	0.0257	0.1335	0.2413	0.3491	0.4569	0.5647	0.6725
TH/K	DIST	NORMAL	4.0192	4.9282	5.8372	6.7462	7.6552	8.5642	9.4732

			MAP UNIT MB						
			-3	-2	-1	0	+1	+2	+3
POTASium	DIST	NORMAL	0.5693	0.6963	0.8233	0.9503	1.0773	1.2043	1.3313
URANIUM	DIST	NORMAL	0.3381	0.8481	1.3581	1.8681	2.3781	2.8881	3.3981
THORIUM	DIST	NORMAL	3.8627	4.6394	5.4161	6.1928	6.9695	7.7462	8.5229
U/K	DIST	NORMAL	0.2416	0.8224	1.4032	1.9840	2.5648	3.1456	3.7264
U/TH	DIST	NORMAL	0.0430	0.1302	0.2174	0.3046	0.3918	0.4790	0.5662
TH/K	DIST	NORMAL	4.3908	5.1146	5.8384	6.5622	7.2860	8.0098	8.7336

LINE BASED MEAN CONCENTRATIONS
AND RATIOS PER ROCK TYPE

	MAP UNIT QM														
	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	1.155	0.000	1.188	0.000	0.000	0.000	0.000	0.968	1.084	1.118	0.968	1.275	0.000	0.000	1.109
URANIUM	2.951	0.000	1.703	0.000	0.000	0.000	0.000	2.295	2.856	2.386	1.846	2.901	0.000	0.000	3.167
THORIUM	7.102	0.000	6.476	0.000	0.000	0.000	0.000	5.401	6.456	7.058	6.838	7.892	0.000	0.000	6.495
U/K	2.534	0.000	1.448	0.000	0.000	0.000	0.000	2.371	2.785	2.166	1.945	2.318	0.000	0.000	2.782
U/TH	0.414	0.000	0.271	0.000	0.000	0.000	0.000	0.430	0.473	0.344	0.272	0.371	0.000	0.000	0.481
TH/K	6.132	0.000	5.451	0.000	0.000	0.000	0.000	5.580	5.972	6.345	7.113	6.296	0.000	0.000	5.863
	1040	1050	1060												
POTASIAM	0.000	0.000	0.000												
URANIUM	0.000	0.000	0.000												
THORIUM	0.000	0.000	0.000												
U/K	0.000	0.000	0.000												
U/TH	0.000	0.000	0.000												
TH/K	0.000	0.000	0.000												

	MAP UNIT QC														
	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	1.078	1.133	1.078	0.880	1.138	1.210	1.040	0.925	1.169	1.008	0.926	0.975	1.123	1.285	1.304
URANIUM	2.239	1.887	1.748	1.573	2.264	2.037	2.049	1.946	1.985	1.728	2.018	2.219	1.835	1.827	2.039
THORIUM	5.265	5.622	5.248	5.140	5.862	5.803	5.896	5.296	6.010	5.384	5.594	6.343	5.617	5.741	6.582
U/K	2.109	1.668	1.665	1.741	2.056	1.692	2.052	2.261	1.695	1.858	2.158	2.307	1.559	1.418	1.578
U/TH	0.424	0.338	0.323	0.267	0.388	0.354	0.351	0.378	0.320	0.325	0.344	0.357	0.313	0.329	0.307
TH/K	4.959	5.045	4.935	6.008	5.276	4.861	5.832	5.860	5.223	5.742	6.157	6.570	5.056	4.420	5.055
	1040	1050	1060												
POTASIAM	0.958	1.035	1.129												
URANIUM	2.021	1.912	2.046												
THORIUM	5.877	6.037	6.797												
U/K	2.132	1.903	1.844												
U/TH	0.347	0.311	0.304												
TH/K	6.214	5.947	6.171												

MAP UNIT QPL

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	1.009	1.052	1.067	0.958	1.096	1.154	0.000	0.000	1.213	0.000	0.000	0.000	1.018	1.154	1.117
URANIUM	1.506	1.347	1.293	1.427	1.741	1.540	0.000	0.000	2.073	0.000	0.000	0.000	1.303	1.409	1.516
THORIUM	2.900	3.446	3.239	3.157	4.212	3.423	0.000	0.000	5.002	0.000	0.000	0.000	3.169	3.754	3.995
U/K	1.477	1.256	1.219	1.646	1.564	1.363	0.000	0.000	1.708	0.000	0.000	0.000	1.289	1.223	1.340
U/TH	0.508	0.385	0.446	0.351	0.413	0.462	0.000	0.000	0.422	0.000	0.000	0.000	0.416	0.390	0.346
TH/K	2.869	3.238	3.023	3.459	3.789	3.026	0.000	0.000	4.110	0.000	0.000	0.000	3.101	3.244	3.535

	1040	1050	1060
POTASIAM	0.000	0.000	0.000
URANIUM	0.000	0.000	0.000
THORIUM	0.000	0.000	0.000
U/K	0.000	0.000	0.000
U/TH	0.000	0.000	0.000
TH/K	0.000	0.000	0.000

MAP UNIT QL

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	1.108	1.152	1.161	1.154	1.279	1.176	1.138	1.214	1.208	1.143	1.178	1.110	1.227	1.139	1.003
URANIUM	2.241	1.961	1.941	1.518	2.371	2.091	2.249	2.275	2.098	2.086	2.117	2.219	2.246	1.986	2.321
THORIUM	5.454	5.932	5.780	6.039	6.563	5.886	6.052	6.019	6.458	6.230	6.792	7.057	6.651	5.882	6.977
U/K	2.027	1.684	1.726	1.327	1.869	1.787	1.999	1.887	1.744	1.844	1.839	2.033	1.857	1.765	2.351
U/TH	0.414	0.323	0.334	0.257	0.367	0.362	0.372	0.384	0.326	0.339	0.317	0.316	0.342	0.342	0.337
TH/K	4.920	5.112	5.012	5.232	5.144	5.045	5.349	4.949	5.369	5.469	5.853	6.472	5.444	5.199	6.978

	1040	1050	1060
POTASIAM	0.845	0.000	0.000
URANIUM	1.835	0.000	0.000
THORIUM	6.597	0.000	0.000
U/K	2.194	0.000	0.000
U/TH	0.281	0.000	0.000
TH/K	7.824	0.000	0.000

MAP UNIT QCL

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIUM	1.052	1.090	1.145	1.042	1.156	1.133	1.189	1.215	1.188	1.146	1.063	1.173	1.266	1.195	1.179
URANIUM	2.045	1.826	1.990	1.599	2.303	2.239	2.090	2.217	2.169	2.147	2.059	2.167	1.878	2.159	2.044
THORIUM	5.458	5.612	5.925	6.003	6.386	6.555	6.356	6.299	6.461	6.440	6.573	7.081	6.384	6.580	6.693
U/K	1.991	1.642	1.804	1.567	2.017	1.959	1.779	1.873	1.872	1.913	1.982	1.888	1.514	1.839	1.755
U/TH	0.371	0.319	0.328	0.272	0.366	0.340	0.332	0.360	0.339	0.332	0.317	0.310	0.300	0.332	0.303
TH/K	5.297	5.176	5.228	5.819	5.558	5.793	5.368	5.256	5.530	5.714	6.320	6.128	5.112	5.556	5.740

	1040	1050	1060
POTASIUM	0.982	0.975	0.922
URANIUM	2.236	2.130	2.132
THORIUM	6.714	5.940	6.283
U/K	2.323	2.266	2.471
U/TH	0.337	0.362	0.354
TH/K	6.910	6.243	6.918

MAP UNIT QGV

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIUM	0.000	1.070	1.140	0.921	1.110	1.186	0.000	0.000	0.000	0.000	0.765	0.861	0.000	1.120	1.126
URANIUM	0.000	1.593	1.815	1.320	1.713	1.774	0.000	0.000	0.000	0.000	1.709	2.301	0.000	1.397	1.760
THORIUM	0.000	4.153	5.142	3.156	3.699	4.358	0.000	0.000	0.000	0.000	4.671	5.217	0.000	4.190	4.902
U/K	0.000	1.460	1.581	1.486	1.538	1.498	0.000	0.000	0.000	0.000	1.910	2.676	0.000	1.248	1.500
U/TH	0.000	0.362	0.351	0.394	0.474	0.410	0.000	0.000	0.000	0.000	0.305	0.445	0.000	0.348	0.335
TH/K	0.000	3.882	4.455	3.435	3.322	3.629	0.000	0.000	0.000	0.000	6.068	6.070	0.000	3.737	4.352

	1040	1050	1060
POTASIUM	0.000	0.000	1.172
URANIUM	0.000	0.000	1.479
THORIUM	0.000	0.000	5.046
U/K	0.000	0.000	1.274
U/TH	0.000	0.000	0.283
TH/K	0.000	0.000	4.329

MAP UNIT QGP

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	0.000	0.969	0.000	0.000	0.000	0.948	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
URANIUM	0.000	1.581	0.000	0.000	0.000	1.745	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
THORIUM	0.000	5.283	0.000	0.000	0.000	5.259	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
U/K	0.000	1.646	0.000	0.000	0.000	1.873	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
U/TH	0.000	0.306	0.000	0.000	0.000	0.334	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
TH/K	0.000	5.433	0.000	0.000	0.000	5.574	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

	1040	1050	1060
POTASIAM	0.780	0.000	0.000
URANIUM	1.332	0.000	0.000
THORIUM	3.916	0.000	0.000
U/K	1.720	0.000	0.000
U/TH	0.342	0.000	0.000
TH/K	5.025	0.000	0.000

MAP UNIT QSI

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	0.744	0.000	0.798	0.786	1.110	0.948	0.900	0.687	0.740	0.824	0.860	0.000	0.000	0.000	0.000
URANIUM	2.121	0.000	1.499	0.985	2.629	2.198	2.031	2.666	1.800	2.359	2.117	0.000	0.000	0.000	0.000
THORIUM	5.204	0.000	4.810	5.648	7.287	6.044	6.809	5.812	5.260	5.936	5.946	0.000	0.000	0.000	0.000
U/K	2.830	0.000	2.063	1.276	2.390	2.347	2.298	3.944	2.466	2.963	2.535	0.000	0.000	0.000	0.000
U/TH	0.406	0.000	0.321	0.176	0.363	0.365	0.307	0.461	0.347	0.403	0.368	0.000	0.000	0.000	0.000
TH/K	7.076	0.000	6.250	7.184	6.579	6.533	7.624	8.506	7.104	7.344	6.927	0.000	0.000	0.000	0.000

	1040	1050	1060
POTASIAM	0.000	0.695	0.886
URANIUM	0.000	1.489	2.271
THORIUM	0.000	4.860	6.275
U/K	0.000	2.162	2.655
U/TH	0.000	0.309	0.361
TH/K	0.000	6.994	7.245

MAP UNIT QTI

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIU	1.027	1.028	1.052	0.960	1.088	1.051	1.157	0.000	0.000	0.000	0.000	0.000	1.053	0.000	1.154
URANIUM	1.995	1.841	1.666	1.605	2.251	2.410	2.013	0.000	0.000	0.000	0.000	0.000	2.089	0.000	2.091
THORIUM	5.722	5.912	6.175	5.917	6.370	6.362	6.100	0.000	0.000	0.000	0.000	0.000	6.254	0.000	6.231
U/K	1.954	1.807	1.617	1.664	2.091	2.285	1.775	0.000	0.000	0.000	0.000	0.000	2.002	0.000	1.824
U/TH	0.354	0.315	0.272	0.267	0.357	0.381	0.337	0.000	0.000	0.000	0.000	0.000	0.337	0.000	0.342
TH/K	5.605	5.764	5.948	6.179	5.877	6.014	5.302	0.000	0.000	0.000	0.000	0.000	5.961	0.000	5.407

	1040	1050	1060
POTASIU	0.000	0.000	1.009
URANIUM	0.000	0.000	2.064
THORIUM	0.000	0.000	7.121
U/K	0.000	0.000	2.046
U/TH	0.000	0.000	0.289
TH/K	0.000	0.000	7.052

MAP UNIT PMC

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIU	0.000	0.000	0.000	0.000	0.000	0.000	1.186	1.296	1.132	0.000	0.000	0.000	0.000	0.000	0.000
URANIUM	0.000	0.000	0.000	0.000	0.000	0.000	2.223	3.137	2.216	0.000	0.000	0.000	0.000	0.000	0.000
THORIUM	0.000	0.000	0.000	0.000	0.000	0.000	6.047	7.793	7.021	0.000	0.000	0.000	0.000	0.000	0.000
U/K	0.000	0.000	0.000	0.000	0.000	0.000	1.891	2.403	1.941	0.000	0.000	0.000	0.000	0.000	0.000
U/TH	0.000	0.000	0.000	0.000	0.000	0.000	0.367	0.401	0.313	0.000	0.000	0.000	0.000	0.000	0.000
TH/K	0.000	0.000	0.000	0.000	0.000	0.000	5.140	5.980	6.269	0.000	0.000	0.000	0.000	0.000	0.000

	1040	1050	1060
POTASIU	0.000	0.000	0.000
URANIUM	0.000	0.000	0.000
THORIUM	0.000	0.000	0.000
U/K	0.000	0.000	0.000
U/TH	0.000	0.000	0.000
TH/K	0.000	0.000	0.000

MAP UNIT PC

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIMUM	0.000	0.000	0.000	0.000	0.000	0.000	1.352	0.988	1.292	1.041	1.048	0.000	0.000	0.000	1.070
URANIUM	0.000	0.000	0.000	0.000	0.000	0.000	2.756	2.220	3.052	2.243	2.177	0.000	0.000	0.000	2.329
THORIUM	0.000	0.000	0.000	0.000	0.000	0.000	7.285	5.981	7.582	6.977	7.108	0.000	0.000	0.000	6.518
U/K	0.000	0.000	0.000	0.000	0.000	0.000	2.051	2.283	2.353	2.174	2.077	0.000	0.000	0.000	2.181
U/TH	0.000	0.000	0.000	0.000	0.000	0.000	0.379	0.374	0.403	0.324	0.306	0.000	0.000	0.000	0.359
TH/K	0.000	0.000	0.000	0.000	0.000	0.000	5.427	6.147	5.885	6.743	6.782	0.000	0.000	0.000	6.112

	1040	1050	1060
POTASIMUM	0.000	0.000	0.000
URANIUM	0.000	0.000	0.000
THORIUM	0.000	0.000	0.000
U/K	0.000	0.000	0.000
U/TH	0.000	0.000	0.000
TH/K	0.000	0.000	0.000

MAP UNIT PRC

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIMUM	0.840	0.813	0.819	0.864	0.871	0.917	0.929	0.942	0.911	0.915	0.885	0.796	0.000	0.000	0.000
URANIUM	1.626	1.581	1.622	1.344	2.112	2.015	2.130	2.166	1.973	2.133	2.081	1.916	0.000	0.000	0.000
THORIUM	5.193	5.024	5.449	5.461	5.609	6.084	5.809	6.276	6.145	6.610	6.307	6.015	0.000	0.000	0.000
U/K	1.997	1.982	2.018	1.566	2.477	2.229	2.323	2.347	2.187	2.358	2.369	2.429	0.000	0.000	0.000
U/TH	0.324	0.318	0.304	0.247	0.380	0.335	0.367	0.352	0.323	0.325	0.331	0.321	0.000	0.000	0.000
TH/K	6.198	6.217	6.687	6.329	6.565	6.712	6.344	6.684	6.801	7.283	7.193	7.616	0.000	0.000	0.000

	1040	1050	1060
POTASIMUM	0.887	0.807	0.000
URANIUM	1.886	1.916	0.000
THORIUM	5.821	5.986	0.000
U/K	2.138	2.385	0.000
U/TH	0.324	0.316	0.000
TH/K	6.596	7.475	0.000

MAP UNIT MC

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	0.000	0.000	0.000	0.000	0.000	0.000	0.798	0.714	0.815	0.747	0.750	0.747	0.000	0.000	0.000
URANIUM	0.000	0.000	0.000	0.000	0.000	0.000	2.062	2.114	1.735	1.620	1.737	1.850	0.000	0.000	0.000
THORIUM	0.000	0.000	0.000	0.000	0.000	0.000	5.302	5.257	5.904	5.284	5.541	5.736	0.000	0.000	0.000
U/K	0.000	0.000	0.000	0.000	0.000	0.000	2.610	2.990	2.121	2.213	2.356	2.495	0.000	0.000	0.000
U/TH	0.000	0.000	0.000	0.000	0.000	0.000	0.396	0.398	0.294	0.307	0.316	0.326	0.000	0.000	0.000
TH/K	0.000	0.000	0.000	0.000	0.000	0.000	6.647	7.415	7.334	7.179	7.440	7.730	0.000	0.000	0.000

	1040	1050	1060
POTASIAM	0.000	0.744	0.000
URANIUM	0.000	1.565	0.000
THORIUM	0.000	5.606	0.000
U/K	0.000	2.135	0.000
U/TH	0.000	0.282	0.000
TH/K	0.000	7.661	0.000

MAP UNIT MST

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	0.792	0.750	0.684	0.750	0.692	0.774	0.794	0.762	0.751	0.719	0.639	0.728	0.000	0.000	0.000
URANIUM	1.713	1.608	1.517	1.331	1.978	1.757	1.825	1.996	1.838	1.768	1.744	1.840	0.000	0.000	0.000
THORIUM	5.032	4.768	4.958	4.871	4.994	5.510	5.654	5.501	5.700	5.796	4.903	5.866	0.000	0.000	0.000
U/K	2.197	2.159	2.239	1.830	2.877	2.277	2.365	2.811	2.475	2.498	2.821	2.568	0.000	0.000	0.000
U/TH	0.345	0.344	0.309	0.264	0.399	0.320	0.327	0.379	0.327	0.307	0.362	0.317	0.000	0.000	0.000
TH/K	6.352	6.404	7.309	6.559	7.238	7.172	7.189	7.346	7.623	8.100	7.846	8.174	0.000	0.000	0.000

	1040	1050	1060
POTASIAM	0.768	0.775	0.000
URANIUM	1.607	1.808	0.000
THORIUM	4.994	5.603	0.000
U/K	2.106	2.352	0.000
U/TH	0.330	0.325	0.000
TH/K	6.530	7.311	0.000

MAP UNIT MS

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	0.893	0.984	1.029	0.950	1.023	0.929	0.938	0.897	0.803	0.000	0.762	0.000	0.000	0.000	0.000
URANIUM	3.197	2.050	1.727	1.844	2.631	2.199	2.938	2.668	1.942	0.000	1.624	0.000	0.000	0.000	0.000
THORIUM	5.908	6.724	6.048	6.232	6.742	6.401	6.585	7.157	6.381	0.000	5.872	0.000	0.000	0.000	0.000
U/K	3.569	2.121	1.697	1.934	2.578	2.386	3.138	3.056	2.457	0.000	2.105	0.000	0.000	0.000	0.000
U/TH	0.543	0.309	0.291	0.294	0.392	0.348	0.446	0.377	0.305	0.000	0.275	0.000	0.000	0.000	0.000
TH/K	6.627	6.887	5.950	6.619	6.612	6.906	7.070	8.076	8.080	0.000	7.698	0.000	0.000	0.000	0.000

	1040	1050	1060
POTASIAM	0.000	1.002	0.988
URANIUM	0.000	1.992	1.988
THORIUM	0.000	6.078	6.226
U/K	0.000	2.034	1.996
U/TH	0.000	0.334	0.317
TH/K	0.000	6.154	6.372

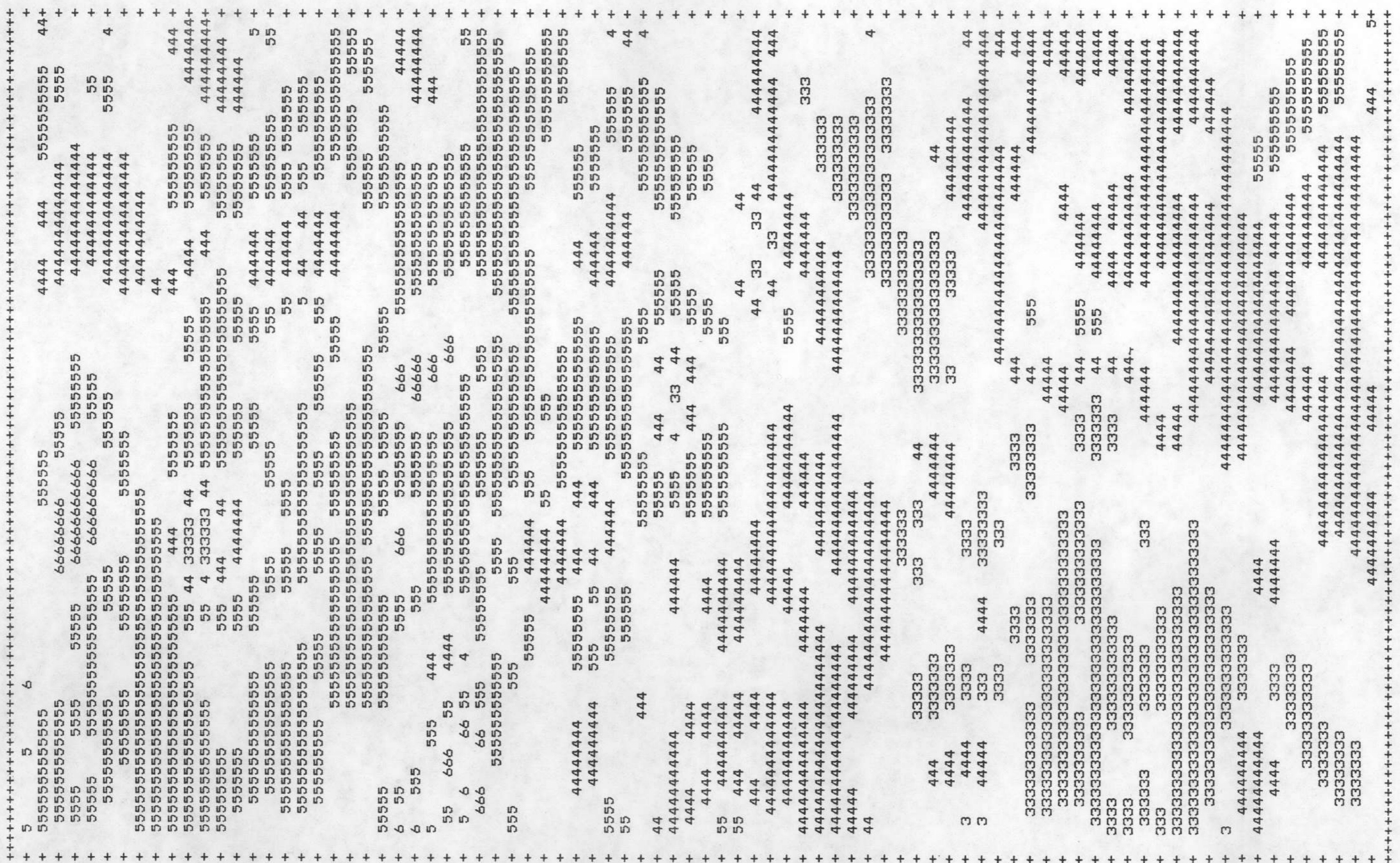
MAP UNIT MB

	730	740	750	760	770	780	790	800	810	820	830	840	1010	1020	1030
POTASIAM	0.938	0.970	0.868	0.949	0.000	0.000	0.864	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
URANIUM	2.037	1.815	1.894	1.443	0.000	0.000	2.634	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
THORIUM	6.025	6.410	5.672	6.392	0.000	0.000	6.706	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
U/K	2.188	1.886	2.228	1.505	0.000	0.000	3.055	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
U/TH	0.338	0.283	0.341	0.223	0.000	0.000	0.401	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
TH/K	6.462	6.705	6.581	6.768	0.000	0.000	7.756	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000

	1040	1050	1060
POTASIAM	0.000	1.019	1.008
URANIUM	0.000	1.922	1.788
THORIUM	0.000	6.530	6.510
U/K	0.000	1.945	1.779
U/TH	0.000	0.299	0.278
TH/K	0.000	6.447	6.491

APPENDIX H - Pseudo Contour Maps

VINCENNES



Potassium Pseudo-Contour Map - Vincennes Quadrangle

EXPLANATION		
PRINT CHARACTER		VALUE
0	LE	0.0000
1	0.0000	0.1250
2	0.1250	0.2500
3	0.2500	0.3750
4	0.3750	0.5000
5	0.5000	0.6250
6	0.6250	0.7500
7	0.7500	0.8750
8	0.8750	1.0000
9	1.0000	1.1250
GT	1.1250	1.2500

SCALE IN EQUIVALENT PERCENT



VINCENNES



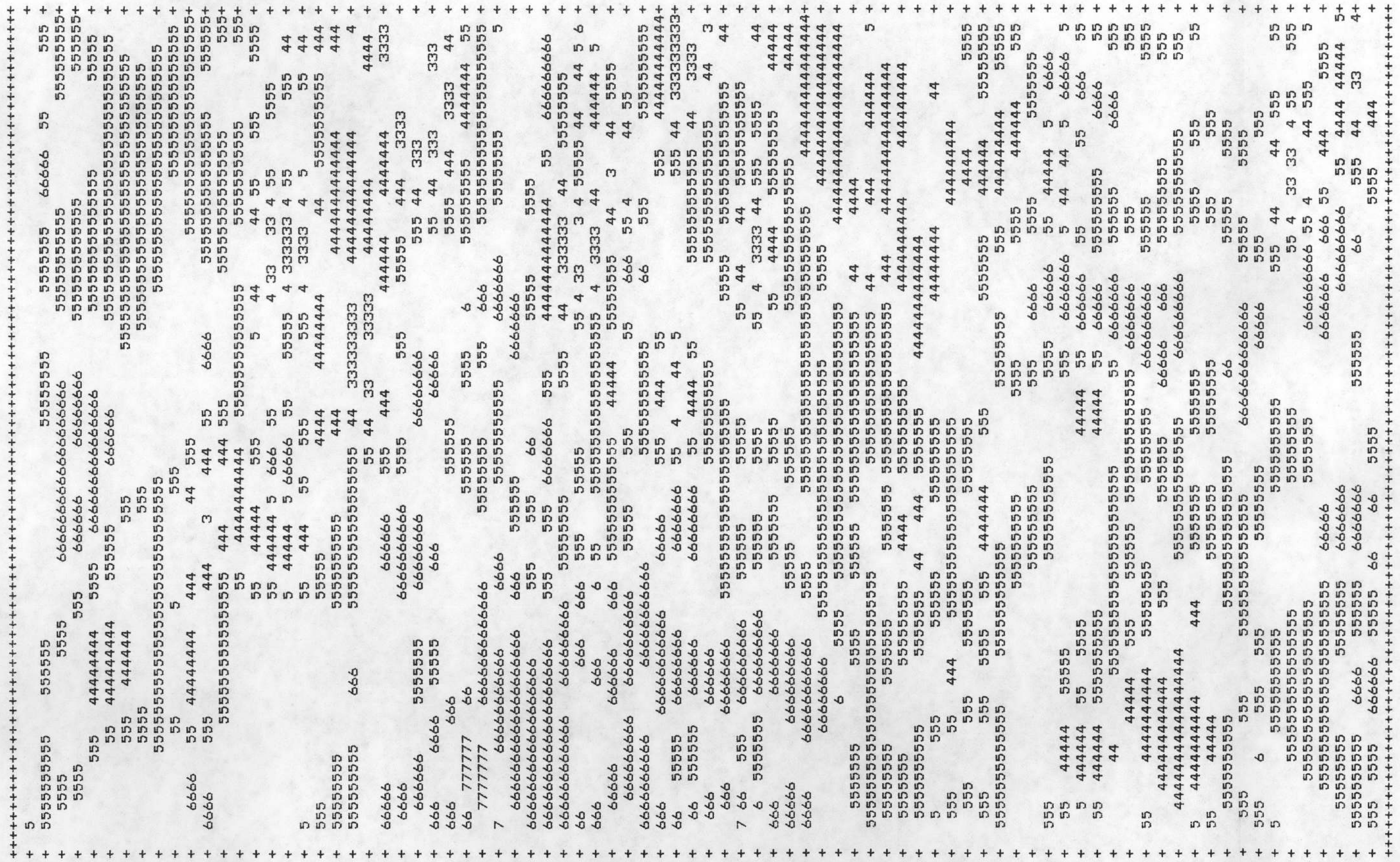
Uranium Pseudo-Contour Map - Vincennes Quadrangle



EXPLANATION	
PRINT CHARACTER	VALUE
0	LE 0.0000
1	0.0000 0.2500
2	0.2500 0.5000
3	0.5000 0.7500
4	0.7500 1.0000
5	1.0000 1.2500
6	1.2500 1.5000
7	1.5000 1.7500
8	1.7500 2.0000
9	2.0000 2.2500
	2.2500 2.5000
	2.5000 2.7500
	2.7500 3.0000
	3.0000 3.2500
	3.2500 3.5000
	3.5000 3.7500
	3.7500 4.0000
	4.0000 4.2500
	4.2500 4.5000
	GT 4.5000

SCALE IN EQUIVALENT PPM

VINCENNES



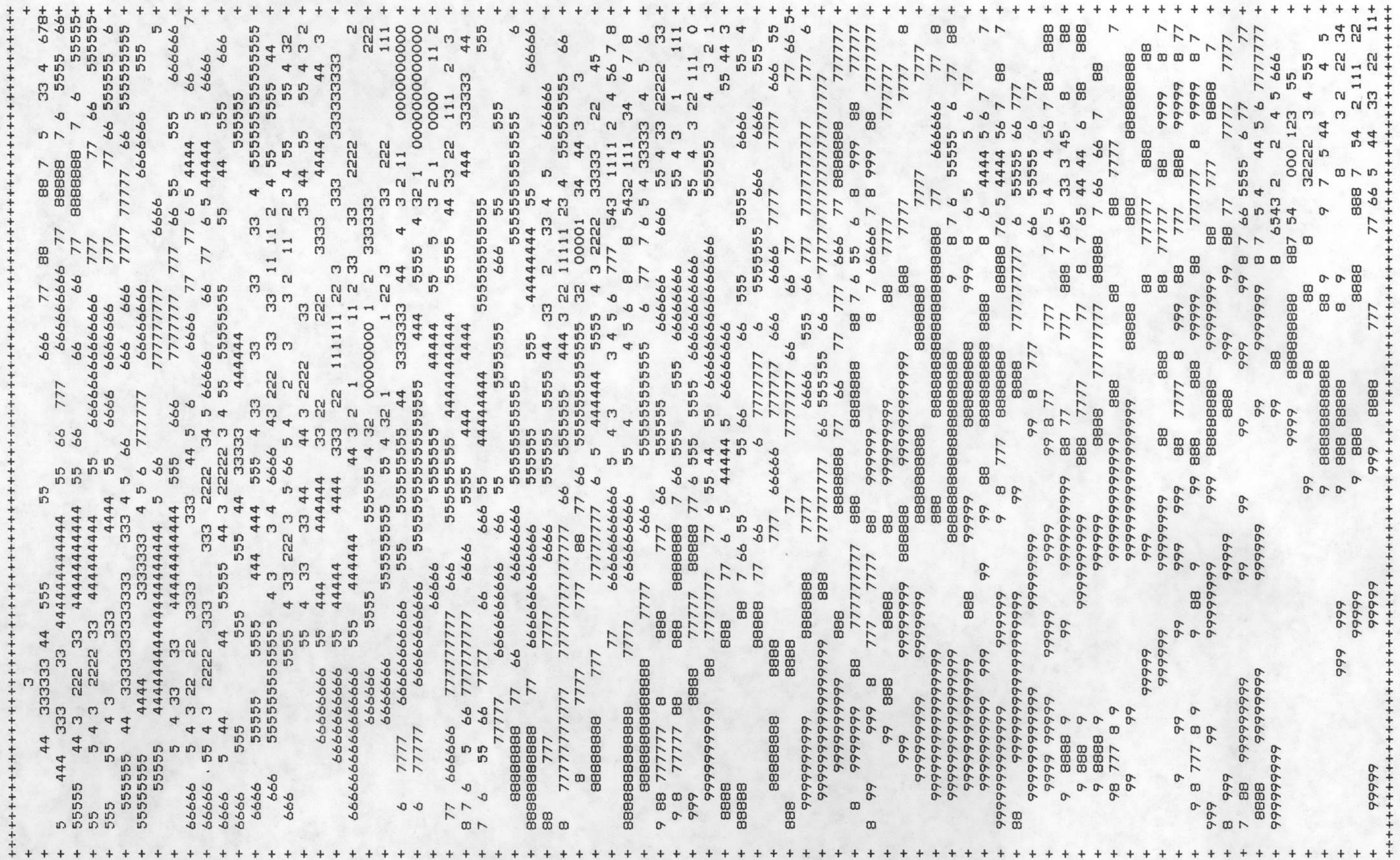
Thorium Pseudo-Contour Map - Vincennes Quadrangle

PRINT CHARACTER	VALUE
0	0.0000
1	0.6250
2	1.2500
3	1.8750
4	2.5000
5	3.1250
6	3.7500
7	4.3750
8	5.0000
9	5.6250
GT	11.2500



SCALE IN EQUIVALENT PPM

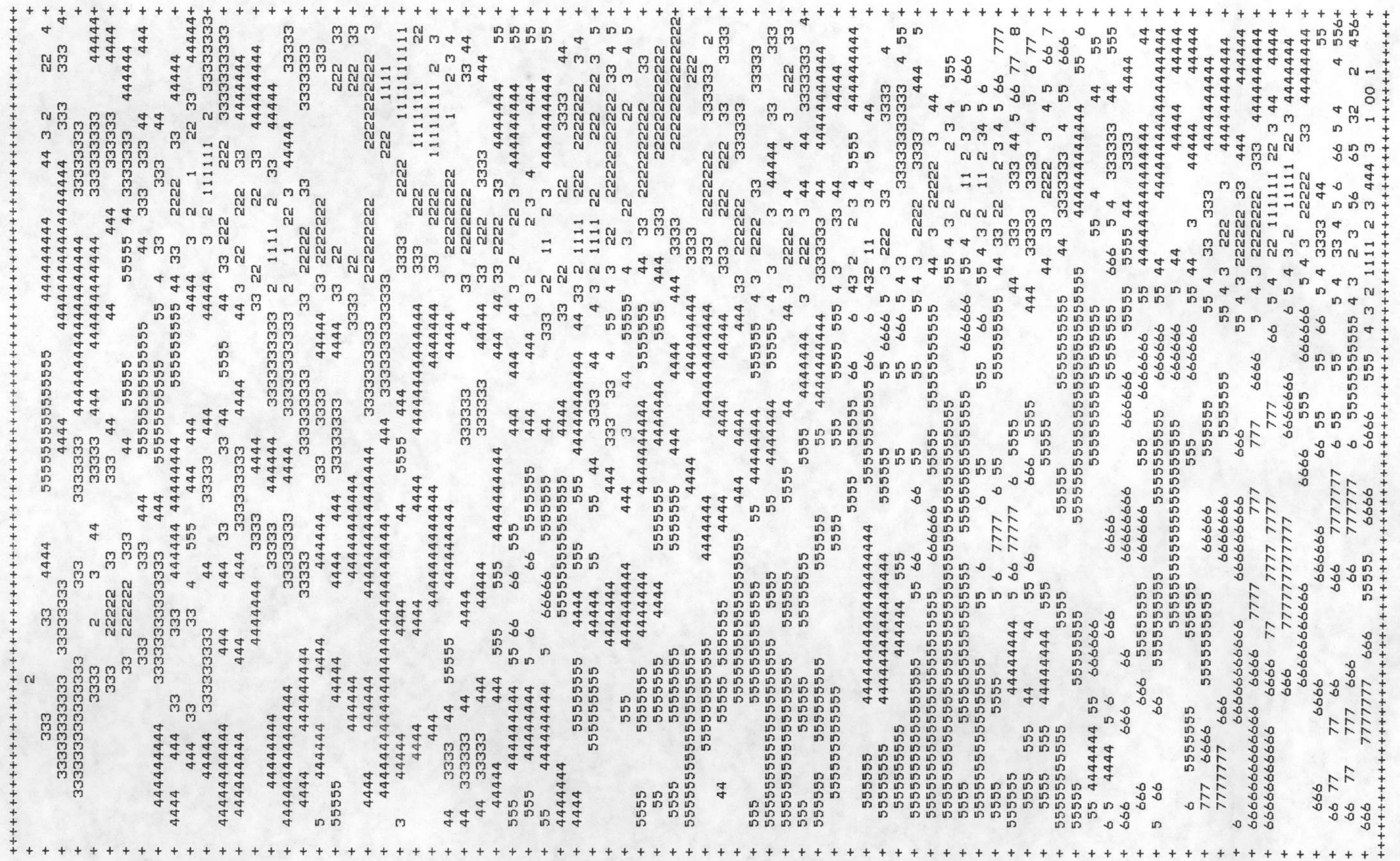
VINCENNES



PRINT CHARACTER	EXPLANATION	VALUE
0	LE	3.0000
1		3.2500
2		3.5000
3		3.7500
4		4.0000
5		4.2500
6		4.5000
7		4.7500
8		5.0000
9		5.2500
		5.5000
		5.7500
		6.0000
		6.2500
		6.5000
		6.7500
		7.0000
		7.2500
		7.5000
GT		7.5000

Thorium/Potassium Pseudo-Contour Map - Vincennes Quadrangle

VINCENNES

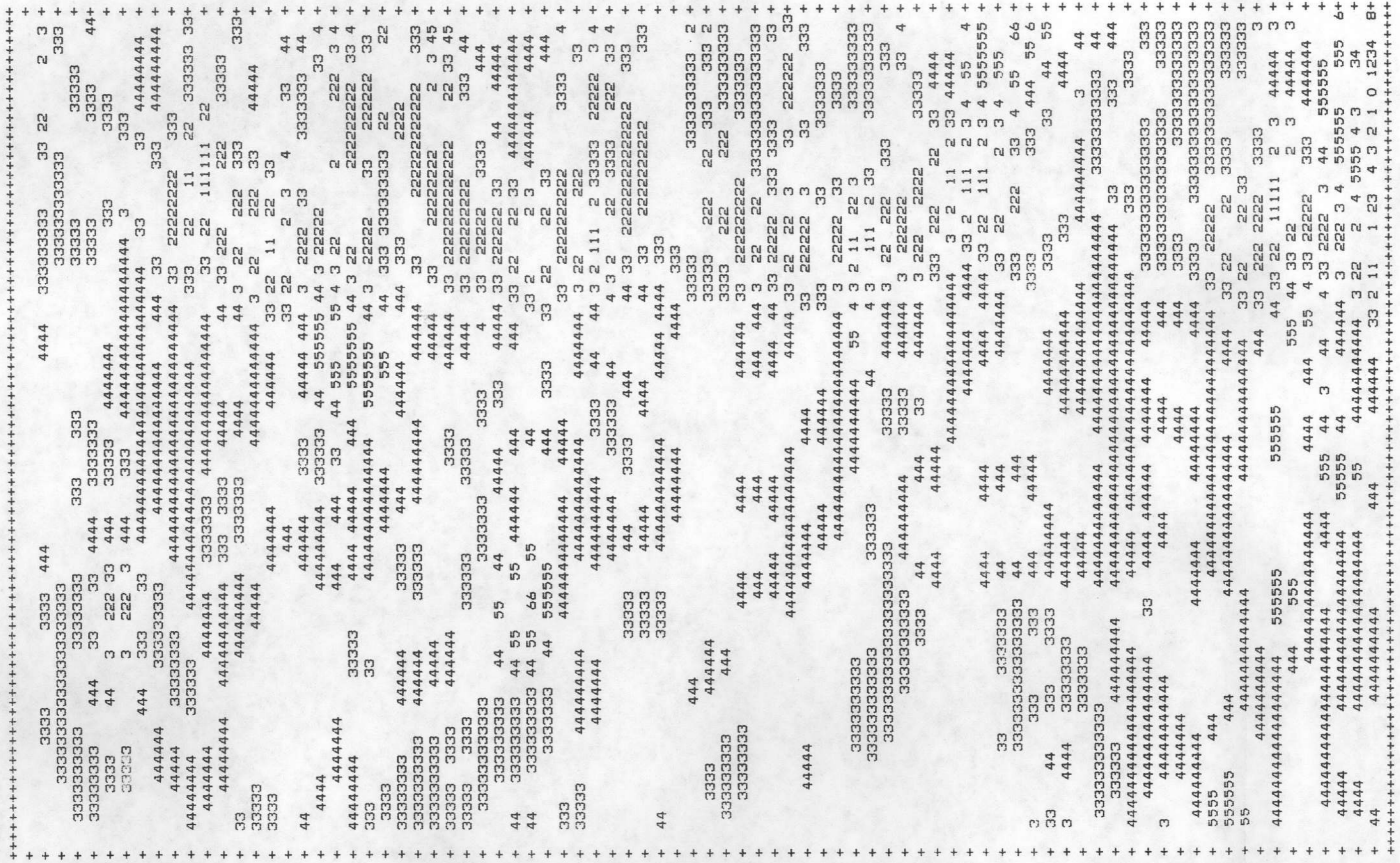


EXPLANATION

PRINT CHARACTER	VALUE
0	LE 0.0000
1	0.0000 0.2500
2	0.2500 0.5000
3	0.5000 0.7500
4	0.7500 1.0000
5	1.0000 1.2500
6	1.2500 1.5000
7	1.5000 1.7500
8	1.7500 2.0000
9	2.0000 2.2500
GT	2.2500 2.5000
	2.5000 2.7500
	2.7500 3.0000
	3.0000 3.2500
	3.2500 3.5000
	3.5000 3.7500
	3.7500 4.0000
	4.0000 4.2500
	4.2500 4.5000
	4.5000 4.7500
	4.7500 5.0000
	5.0000 5.2500
	5.2500 5.5000
	5.5000 5.7500
	5.7500 6.0000
	6.0000 6.2500
	6.2500 6.5000
	6.5000 6.7500
	6.7500 7.0000
	7.0000 7.2500
	7.2500 7.5000
	7.5000 7.7500
	7.7500 8.0000
	8.0000 8.2500
	8.2500 8.5000
	8.5000 8.7500
	8.7500 9.0000
	9.0000 9.2500
	9.2500 9.5000
	9.5000 9.7500
	9.7500 10.0000

Uranium/Potassium Pseudo-Contour Map - Vincennes Quadrangle

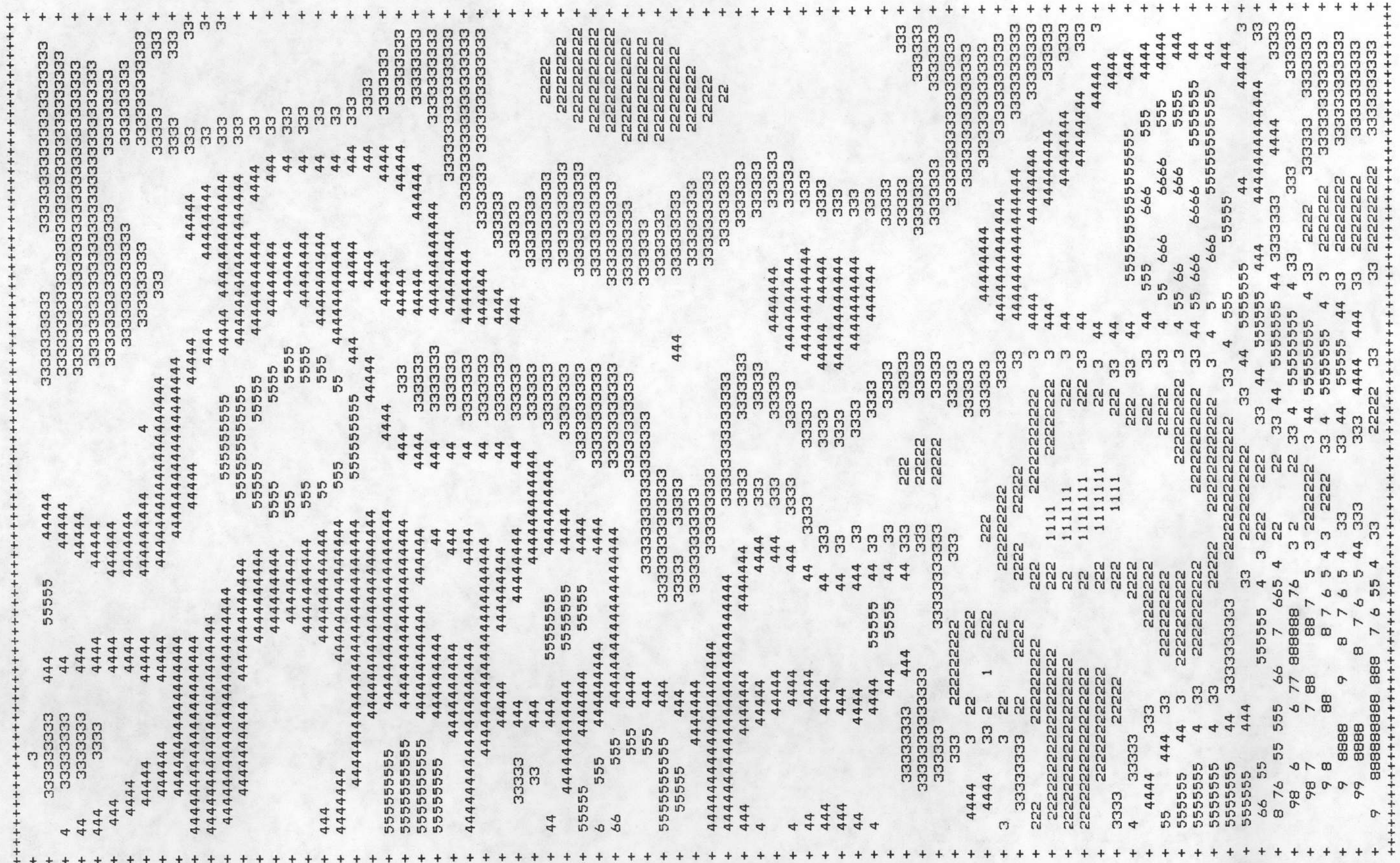
VINCENNES



PRINT CHARACTER	VALUE
0	0.0000
1	0.0500
2	0.1000
3	0.1500
4	0.2000
5	0.2500
6	0.3000
7	0.3500
8	0.4000
9	0.4500
GT	0.9000

Uranium/Thorium Pseudo-Contour Map - Vincennes Quadrangle

VINCENNES



EXPLANATION

PRINT CHARACTER	VALUE
0	LE-1200.0000
-1200.0000-1125.0000	
1-1125.0000-1050.0000	
-1050.0000 -975.0000	
2 -975.0000 -900.0000	
-900.0000 -825.0000	
3 -825.0000 -750.0000	
-750.0000 -675.0000	
4 -675.0000 -600.0000	
-600.0000 -525.0000	
5 -525.0000 -450.0000	
-450.0000 -375.0000	
6 -375.0000 -300.0000	
-300.0000 -225.0000	
7 -225.0000 -150.0000	
-150.0000 -75.0000	
8 -75.0000 0.0000	
0.0000 75.0000	
9 75.0000 150.0000	
GT 150.0000	

SCALE IN GAMMAS

Residual Magnetic Pseudo-Contour Map - Vincennes Quadrangle

1875
1876
1877
1878
1879