

Geology  
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NATIONAL URANIUM RESOURCE EVALUATION  
**AERIAL RADIOMETRIC AND MAGNETIC SURVEY**  
NATIONAL TOPOGRAPHIC MAP

**BISMARCK**

**NORTH DAKOTA**

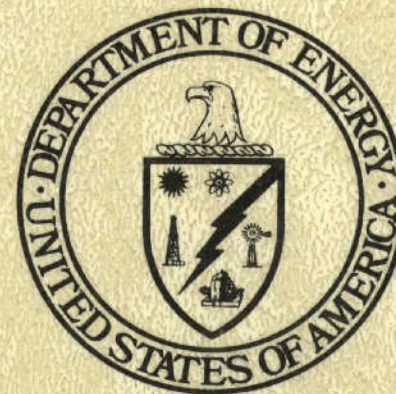
**FINAL REPORT**

1981



**Geodata International, inc.**

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PREPARED FOR U.S. DEPARTMENT OF ENERGY

Grand Junction Office, Colorado

UNDER CONTRACT NO. DE-AC13-76 GJO 1664

AND BENDIX FIELD ENGINEERING CORPORATION SUBCONTRACT NO. 80-459-S

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**GEOLOGY**

**GEOLOGICAL SURVEY OF WYOMING**

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AERIAL RADIOMETRIC AND MAGNETIC SURVEY

BISMARCK NATIONAL TOPOGRAPHIC MAP

NORTH DAKOTA

NEBRASKA-DAKOTAS PROJECT

PREPARED FOR THE U.S. DEPARTMENT OF ENERGY  
GRAND JUNCTION OFFICE  
GRAND JUNCTION, COLORADO

UNDER BENDIX FIELD ENGINEERING SUBCONTRACT NO. 80-459-S  
BY  
GEODATA INTERNATIONAL, INC.  
DALLAS, TEXAS

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ABSTRACT

*The results of analyses of the airborne gamma radiation and total magnetic field survey flown for the region identified as the Bismarck National Topographic Map NL14-4 is presented in this report. The airborne data gathered is reduced by ground computer facilities to yield profile plots of the basic uranium, thorium and potassium equivalent gamma radiation intensities, ratios of these intensities, aircraft altitude above the earth's surface, total gamma ray and earth's magnetic field intensity, correlated as a function of geologic units. The distribution of data within each geologic unit, for all surveyed map lines and tie lines, has been calculated and is included. Two sets of profiled data for each line are included, with one set displaying the above-cited data. The second set includes only flight line magnetic field, temperature, pressure, altitude data plus magnetic field data as measured at a base station. A general description of the area, including descriptions of the various geologic units and the corresponding airborne data, is included also.*



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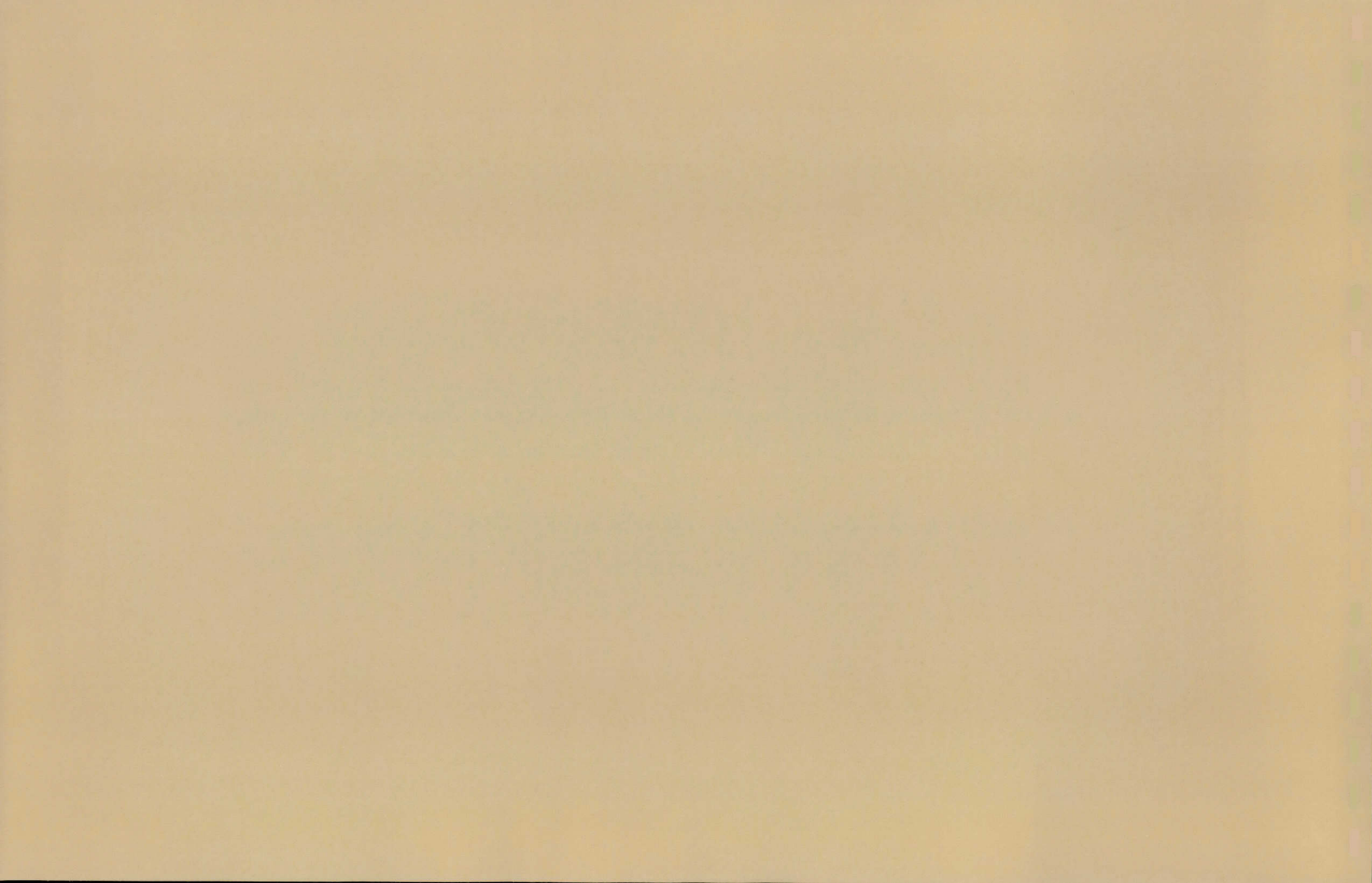
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# SECTION I

## INTRODUCTION







SECTION I.

INTRODUCTION

A. SURVEY AREA

Geodata International, Inc., Dallas, Texas, conducted an airborne gamma ray and total magnetic field survey for the Bismarck National Topographic Map Sheet as outlined in Figure I.1. This survey was performed from a fixed-wing aircraft, using a computer-controlled, large-volume radiation detector system to detect the gamma radiation flux emanating from the surface materials. Each map line was flown in an east-west direction with line lengths of 94.5 miles; each tie line was flown in a north-south direction with line lengths of 69.0 miles. Map lines and tie lines are located as shown in Figure II.1.

Sections I through IV of this report present information and results associated with this specific survey. Section V gives the data acquisition and the processing procedures which are generally applicable to any survey flown with the equipment described.

B. SUMMARY of MAP LOCATION, GEOLOGY and PHYSIOGRAPHY

The Bismarck map sheet area (Figure I.2) is located in southcentral North Dakota and bounded by longitudes 100°00' to 102°00' west, latitudes 46°00' to 47°00' north. The map region is included within two distinct sections of the Great Plains physiographic province; namely, the Glaciated Missouri Plateau section, and the Unglaciated Missouri Plateau section. The land surface is generally characterized as irregular and rolling. Elevations range from approximately 2,500 to 1,700 feet above sea level.

Deposition in the Bismarck map area has reportedly been affected by a synclinal basin, the Lemmon Syncline, since the Paleozoic Era. Fluctuations of the region with respect to sea level have been responsible for producing unconformable surfaces at the top of the Paleozoic sequence and elsewhere throughout the column. Most of the area was mantled with glacial detritus during the Pleistocene. Eolian and fluvial processes have continued to affect the region to the present time.

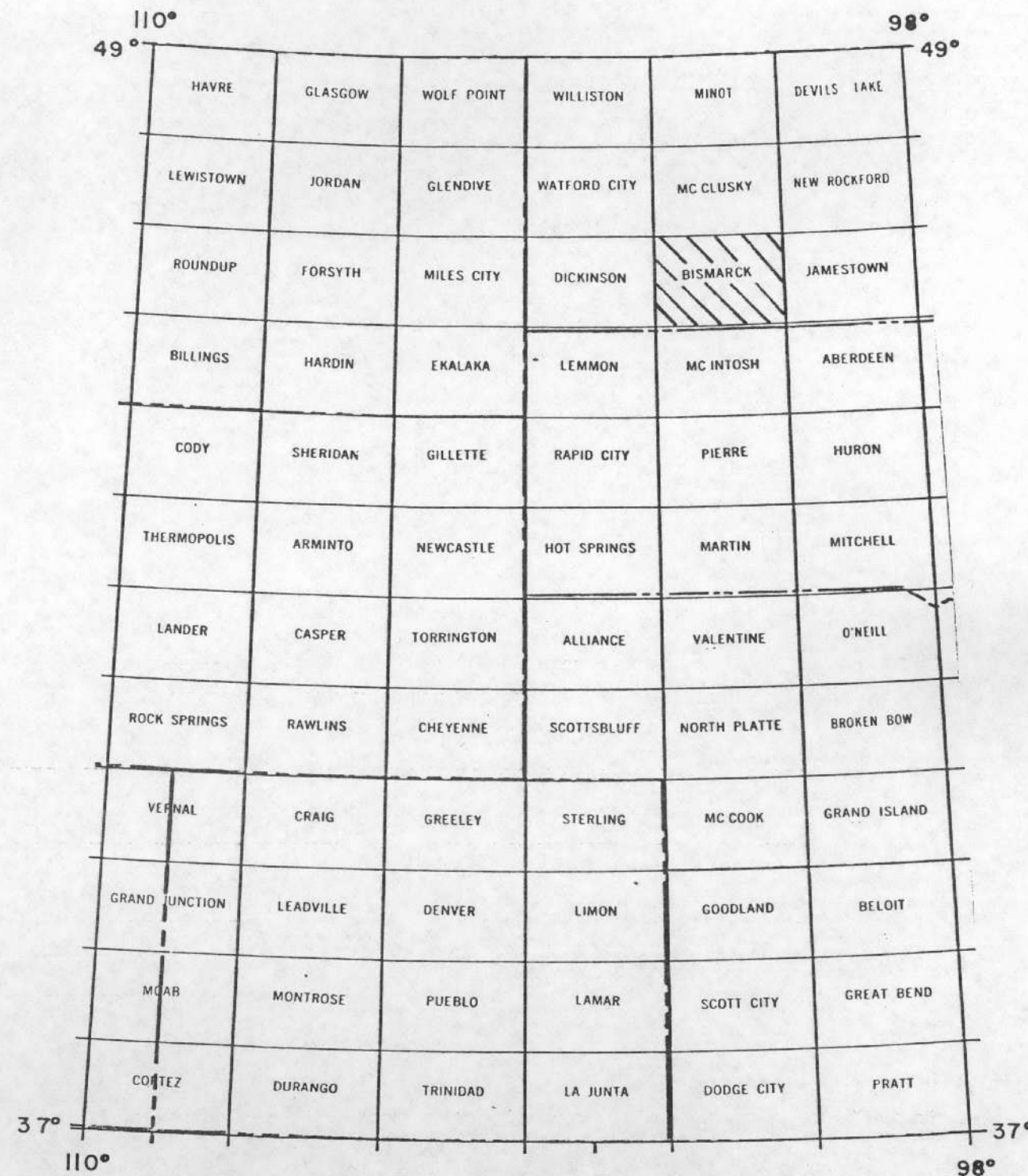
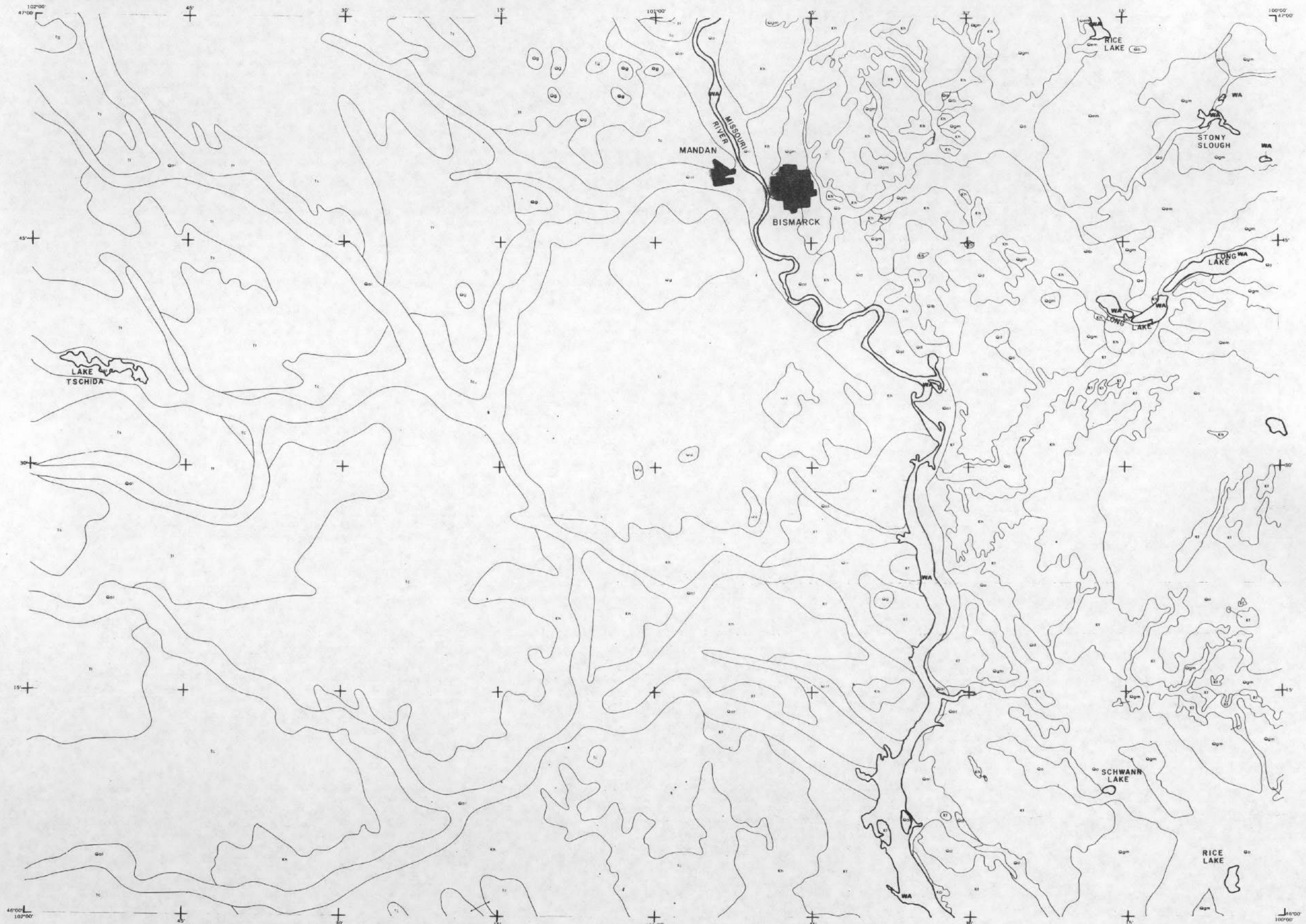


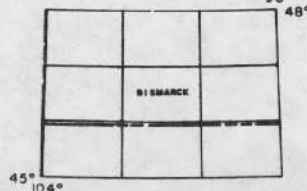
Figure I.1 Survey Index Map





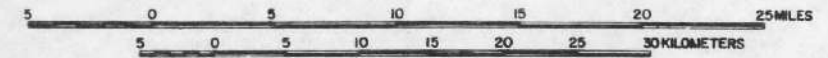
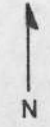
GEODATA INTERNATIONAL, INC.  
7035 John W. Carpenter Frwy., Dallas, Texas 75247

compiled by  
Martel Laboratories, Inc.



GEOLOGY BASE  
REF. NTMS, NL 14-4  
PREPARED FOR  
U.S. DEPARTMENT OF ENERGY

I-3



Bismarck, North Dakota  
Figure I.2 Geologic Base Map



# SECTION II

## FLIGHT OPERATIONS







## SECTION II.

### FLIGHT OPERATIONS

#### A. SURVEY TIME SUMMARY

The Bismarck map sheet was flown between July 26 and July 28, 1980. A detailed list of dates flown and lines flown on those dates, as well as average altitude and speed for those dates, appears in Appendix I.A.

#### B. LINE COORDINATE LOCATION

Doppler navigation system data have been used to locate the positions of the flight lines. These lines are positioned and verified by point locations, determined by visual sighting by the navigator or photographic recovery, and corresponding record numbers displayed by the on-board computer. The data are then plotted as solid lines with ticks every ten records, circles every fifty records, and record numbers every one hundred records. Record numbers and circles also appear at the end of each line. The points used for location reference (at least every 10 miles) are marked with an "X". The flight base is then photographed with the geologic base map to produce the composite map in Figure II.1.

#### C. TEST LINES

When conditions allow, two five-mile test lines are flown, one at the beginning of the day and one at the end of the day, over the same base. The data are used to check the repeatability of the system's measurements, and are presented in Appendix I.B.

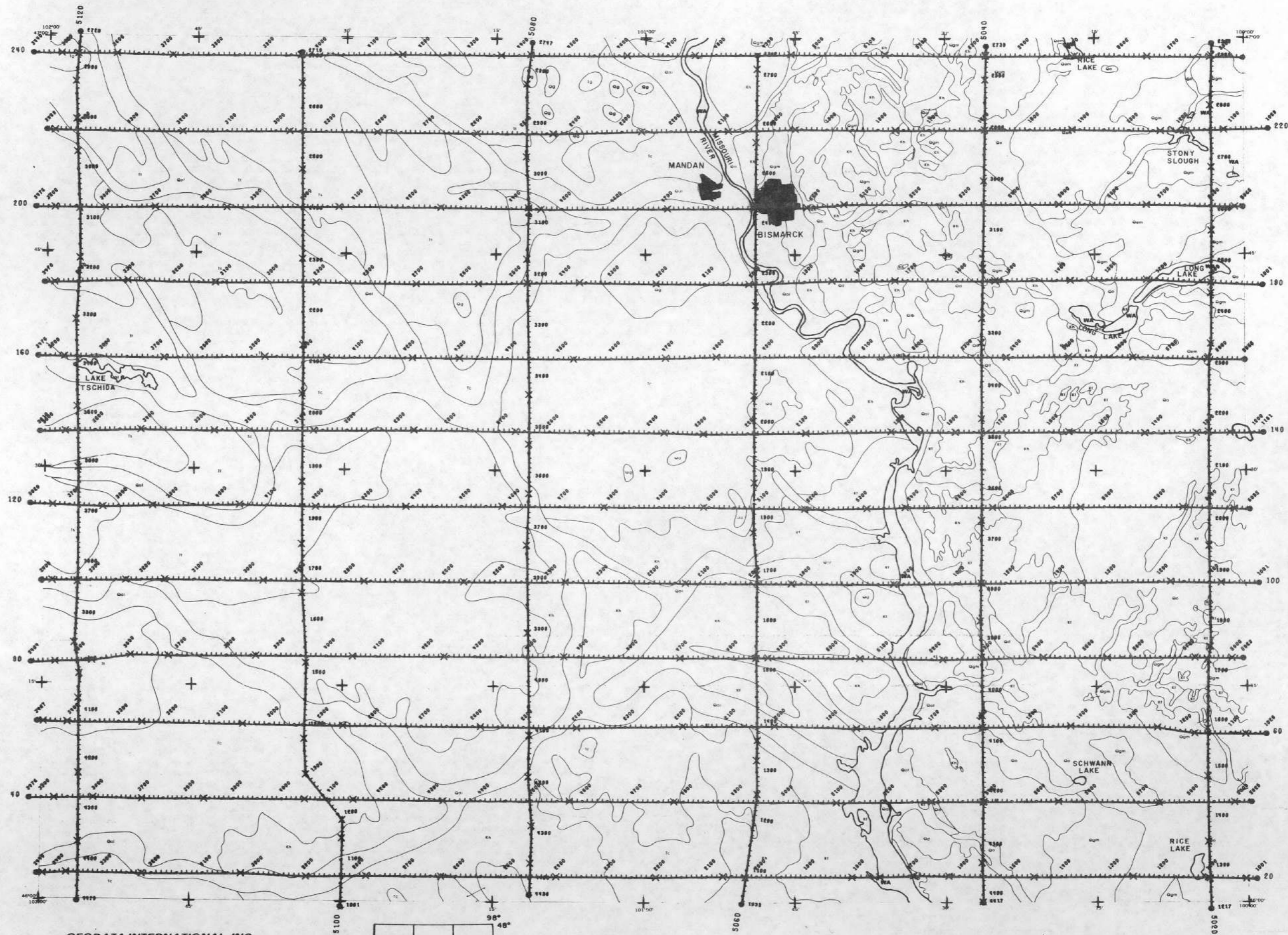
#### D. MAGNETIC DIURNAL CORRECTION - BASE STATION

A base station magnetometer is set up in the area to acquire data pertaining to the diurnal changes in the magnetic field. These data are analyzed to evaluate a diurnal correction to the magnetic data obtained by the aircraft. A list of these corrections appears in Appendix I.C.

#### E. ALTITUDE AND GROUND SPEED SUMMARY

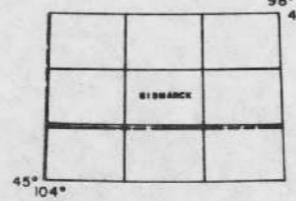
The average altitude and ground speed for each line is determined. A list by date appears in Appendix I.A, and is discussed in Section II.A. A list by flight line is given in Appendix I.E.





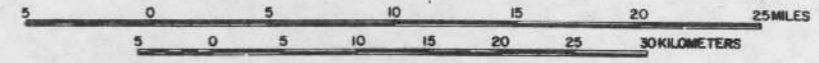
GEODATA INTERNATIONAL, INC.  
7035 John W. Carpenter Frwy., Dallas, Texas 75247

"x" INDICATES FILM VERIFIED POINTS



FLIGHT LINE BASE  
REF. NTMS, NL 14-4  
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II-2



# Bismarck, North Dakota

Figure II.1 NTMS Showing Flight Line Location



# SECTION III

GEOLOGY OF THE SURVEYED AREA







### SECTION III.

#### GEOLOGY of the SURVEYED AREA

##### A. LOCATION and GENERAL PHYSIOGRAPHY

The aerial radiometric and magnetic survey was conducted over a portion of southcentral North Dakota. The Bismarck National Topographic Map Sheet area (N.T.M.S., 1954) is bounded by longitudes 100°00' to 102°00' west and latitudes 46°00' to 47°00' north. The map region includes all or part of the following counties in North Dakota: Burleigh, Emmons, Grant, Kidder, Morton, and Sioux. A portion of the Standing Rock Indian Reservation is also included in the map sheet area.

The Bismarck Quadrangle lies mainly within the Glaciated Missouri Plateau section of the Great Plains province. The Unglaciated Missouri Plateau section of the map lies southwest of the Cannonball River. The northeastern corner of the area is described by Fenneman (1928) as the Coteau du Missouri, a morainal shelf of ancient, glacial-lake deposits.

Drainage in the Bismarck map area is accomplished chiefly by the Missouri River, which dissects the eastern two-thirds of the area and trends generally to the north. Flowing into the Missouri River from the west is the Cedar Creek River. A smaller stream, the Heart River, drains the northern half of the map sheet area into the Missouri Basin.

The land surface west of the Missouri River is irregular and rolling; it increases in elevation very gradually into the butte and mini-badlands area east of the Little Missouri River. It is deeply cut by the entrenched streams flowing from the west. Relatively flatter areas of land are used for agricultural purposes. Buttes and hills extend up to the escarpment west of the Missouri River. East of the river, however, the terrain flattens out considerably into a morainal plain with very rich soil. There are many lakes and dry lake beds present, remnants of glacial action.

The total relief in the map sheet area is approximately 800 feet. Elevations range from approximately 2,500 feet above sea level in the southwest to 1,700 feet in elevation in the eastern lake country.

##### B. GEOLOGY

The structural and depositional events of the Bismarck, North Dakota Quadrangle and surrounding regions are described by Darton (1909), Hancock (1922), Wilson et.al. (1951), Lemke (1960), Carlson

and Anderson (1965), and Frye (1969). These data are summarized as follows:

##### Paleozoic Era

There are no exposures of Paleozoic rock units in the Bismarck area, although much subsurface information has been collected from deep-well data. Since the inception of the Paleozoic Era, the map sheet area has been part of a synclinal depositional basin, the Lemmon Syncline. This basin is a subelement of a larger, deeper basin to the northwest, the Williston Basin.

Logs from wells drilled in the map sheet area record Cambrian rock at approximately 13,500 feet. The depositional basin began filling with clastics during the Ordovician, producing the Deadwood Formation beds. A predominantly carbonate sequence followed through the Mississippian Period.

In the map sheet area, the top of the Pennsylvanian is marked by an unconformable surface. Evaporites and clastics were deposited during the Permian. A major unconformity truncates the Paleozoic units (Walker, 1963).

##### Mesozoic Era

Slight subsidence of the map sheet area is reported by Hancock (1922) to have occurred during the Triassic. Predominantly marine rock units of the Jurassic and Lower to Middle Cretaceous are representative of eastward extensions of the Cordilleran seas.

Late Cretaceous deposition was affected by minor tectonic movements. The Pierre and Fox Hills formations of the Montana Group were deposited during this time. These two formations are the oldest units exposed in the map sheet area.

##### Cenozoic Era

The beginning of the Cenozoic Era in the map region is marked by the transitional, lignite-bearing Fort Union Group of which the Cannonball, Tongue River and Sentinel Butte formations are members. The group was thinly overlain by a member of the White River Group, the Golden Valley Formation.

Several advances of ice sheets from Canada during the Pleistocene were responsible for producing a relatively thick mantle of glacial detritus in the map area. Eolian and fluvial processes have continued to the present.

##### C. DESCRIPTION of the GEOLOGICAL MAP UNITS

A brief description of the outcropping geologic units of the Bismarck, North Dakota map sheet area (Figure I.2) is given, based on



the map compiled by Martel Laboratories, Inc. (1980), and data reported by Hancock (1922), Wilson, et.al. (1951), Lemke (1960), Finch (1967), Frye (1969) and Randich (1979).

### Cenozoic Era

#### Quaternary

##### Holocene-Recent

Qa1: Alluvium

Gravel, sand, silt, shale and clay, generally stratified, very permeable. Up to 150 feet in thickness at lower levels of the stream beds.

Qd: Dune Sand

In dune topography, fine, windblown, unconsolidated sand in spotty drifts and blowouts.

##### Pleistocene

Qo: Outwash-Channel Deposits

Gently undulating to nearly flat accumulations of stratified glacio-fluvial sand, clay, gravel and silt in generally elongated deposits.

Qem: End Moraines

Gently rolling to hummocky accumulations of drift, chiefly till, with moderate to high relief displaying linear patterns in places. Mostly till, small gravel, and sand.

Qgm: Ground Moraine

Moderately irregular deposits of small boulders, gravel, sand, stony clay till and humus, relatively impermeable; mantles part of the surface in the eastern and northeastern portion of map sheet area. 75 to 100 feet thick.

Qlb: Lacustrine Deposits

Very minor, isolated, irregular, glacial-lake deposits composed of sand, silts and clays. Generally stratified, with limited permeability.

Qg: Glacial Deposits

Isolated remnants of pre-Wisconsin glacial drift. The deposits are comprised of sand, gravel, cobbles and many boulders, granitic and gneissic. Up to 80 feet thick.

### Tertiary

#### Eocene

Tg: Golden Valley Formation

A very small outlier exposure of sandy, soft, permeable clay and sandstone. The unit is a member of the upper Fort Union Group. Pinches out in the far northwestern corner of the map. From 0 to 30 feet thick.

#### Paleocene

Ts: Sentinel Butte Formation

The deposit is comprised of interbedded fine sandstone, siltstone, claystone, shale and lignite. Light-colored sandstone and dark shales alternate with carbonaceous seams and lignites of different color and composition. Ranges up to 185 feet in thickness, thickening westward.

Tt: Tongue River Formation

The unit is well-exposed in the northwestern one-third of the map sheet area; interbedded very fine- to medium-grained sandstone, siltstone, claystone, limestone, shale and lignite. The basal sandstone portion of the Tongue River Formation is the most extensively exposed and contains abundances of petrified wood locally. Thin lenses of limestone (4 inches or less) are present in the siltstone and claystone beds.

Tc: Cannonball Formation

Widely exposed in the central portion of the map sheet area. The unit is comprised in part of glauconitic, friable, sandstone that is non-calcareous except for large concretions with calcium carbonate cement in matrix. The Cannonball Formation generally consists of siltstone, claystone and shale (largely carbonaceous). Lignite seams outcrop extensively in the lower part of the formation all along the northside of Cedar Creek and both banks of the Cannonball River. These seams are up to 11 feet thick.

### Mesozoic Era

#### Cretaceous

Kh: Hell Creek Formation

Predominantly sandstone (3 horizons) with unconsolidated fine clastics (quartzose) siltstone, shale and thin beds of lignite.



The sandstone contains much manganese minerals, siderite nodules and magnetite grains. The basal sandstone grades into lignitic and bentonitic shale with petrified wood. Average thickness is 290 feet (Randich, 1979).

Kf: Fox Hills Formation

Fine- to medium-grained sandstone, siltstone and shale. A relatively resistant sandstone bed at the top of the unit is responsible for producing benches and promontories. The bed comprises approximately one-third of the total formation thickness (maximum 390 feet). The remainder of the formation is composed of interbedded siltstone, fossilized shale with limonite concretions and a volcanic ash bed associated with a very dense bentonitic shale (Randich, 1979).

Kp: Pierre Shale

A very minor low-level exposure (approximately 100 feet thick) at the bottom of the Missouri River trench as it flows south out of the map sheet area. Contact between the overlying Fox Hills is transitional for 80 to 90 feet in most places and consists of a bentonitic shale. The formation itself is predominantly greyish-black shale with occasional fossils.

UNK: Unlabeled Geologic Unit

An unlabeled surface outcrop in the Bismarck map sheet area, of indeterminate age.

D. RADIOACTIVE MINERAL PROSPECTS in the SURVEYED AREA

Radioactive mineral-bearing ores are well distributed in several areas of southern and western North Dakota, adjoining the Crook County, Wyoming, and Black Hills outlier deposits.  $U_3O_8$  mineralization occurs in association with carbonaceous material in these units (Zeller and Schopf, 1959, and Vine, 1962). There are no reports of significant concentrations of uranium directly within the Bismarck map sheet area, however.



# SECTION IV

## RESULTS OF DATA ANALYSIS







## SECTION IV.

### RESULTS OF DATA ANALYSIS

#### A. DESCRIPTION OF STACKED DATA PROFILES

##### 1. Multivariable Radiometric Stacked Data Profiles

These profiles are presented at a horizontal scale of 1:500,000. The vertical scales are:

Altitude: 100 feet/div.; aircraft altitude above the surface

ETH(<sup>208</sup>Tl)\* 1.0 ppm/div; 7.15 c/s = 1 ppm/eTh

EU (<sup>214</sup>Bi)\* .50 ppm/div; 13.52 c/s = 1 ppm/eU

K (<sup>40</sup>K)\* .25 %/div; 98.06 c/s = 1%K

BiAir 5.0 c/s/div. 50.0 seconds averaged

Residual Magnetic Field 50.0 gammas/div. (See Sec.V.B.1)

GC (Count from 400 keV to 3.0 MeV) 400 c/s/div.

EU/ETH .05 /div.

EU/K .20 /div.

ETH/K .50 /div.

Geology Strip: An approximate six-mile width of the geology map, containing each line, is displayed above the profiles.

\* 7-second average weighted 1:2:3:4:3:2:1 is used and plotted at center.

##### 2. Residual Magnetic Field Profiles

Altitude: 100 feet/div.

Temperature: 1.0 °C/div.

Pressure: 3.0 mm of Hg/div.

Base Magnetic Field: 20.0 gammas/div.

Residual Magnetic Field: 10.0 gammas/div.

Geology Strip: An approximate six-mile width of the geology map, containing each line, is displayed above the profiles.

All profiles appear in Section IV.H.

#### B. SINGLE AND AVERAGE RECORD LISTINGS

Single and average record listings are provided on microfiche. Samples of each type are presented in Appendix III.

#### C. STATISTICAL PRESENTATION OF DATA BY GEOLOGIC TYPE

Tables IV.(1-6) contain the average value of each variable as a function of line number and geologic type. The tables are in order eTh, eU, K, eU/eTh, eU/K, eTh/K.

#### D. FREQUENCY DISTRIBUTION OF DATA FOR EACH GEOLOGIC TYPE

Table IV.7 contains the mean, standard deviation, and number of events for each geologic type encountered over the entire map sheet. Histograms for these data appear in Section IV.H.2.

#### E. DATA INTERPRETATION

##### 1. Analysis of Geologic Histograms

The radioactivity data is shown in histogram form with parts per million or percent plotted against number of events (Appendix I). The histograms for eTh and K were examined for conformity to a Gaussian curve. It is generally assumed that a geologic map unit, which encompasses a fairly homogeneous lithology, would have a unimodal distribution. Where map units vary significantly from a unimodal distribution, a further subdivision into more homogeneous lithologic types may be recommended. Table IV.8 shows the map units, which vary from a unimodal model, and for which separation of two or more distributions is feasible. Only units with excess of 200 events are considered.

##### 2. Discussion of Anomalies

###### Introduction

The eTh, eU, and eU/eTh (ratio) data were examined for anomalous values. An anomaly is defined by a minimum of two adjacent, two-standard deviation values, or a single, three-standard deviation value. The anomalies were listed by flight line in Table IV.9; by geologic map unit in Table IV.10; Table IV.10 is statistically summarized in Table IV.11. Only positive anomalies were examined for eTh and eU, but both positive and negative values were studied for the ratio anomaly.



Table IV.1 Geologic Unit Average Value as a Function of Map Line  
for eTh (PPM Times 10)

UNIT:	QAL	QD	QO	QEM	QGM	QLB	QG	TG	TS	TT	TC	KH	KF	KP	UNK
LINE															
ML 240:	66		61	58	66			80	71	70	68	67			
ML 220:	67		58	59	66		71		70	69	67	70			
ML 200:	67		57	59	62	65	61		74	74	65	54			
ML 180:	64	43	41	59	55	53	69		74	71	66	55			
ML 160:	71	57	44	50	47	55				73	67	57	46		
ML 140:	59		64						74	66	68	64	68		64
ML 120:	66		70				67		77	61	63	70	66		74
ML 100:	67		67							76	69	64	69		70
ML 80:	64	58	65		70					74	72	62	71		
ML 60:	67		56		73					67	71	60	68		
ML 40:	57		66		71						75	63	69		
ML 20:	68		65		77						70	64	64	57	
TL 5020:			59	57	63								62		
TL 5040:		48	61		66	39						60	71		
TL 5060:	60		70				68				64	63	61		
TL 5080:	58						68			66	71	62			
TL 5100:	65								71	67	66	66			
TL 5120:	66							79	73	71	67				

Table IV.2 Geologic Unit Average Value as a Function of Map Line  
for eU (PPM Times 10)

UNIT:	QAL	QD	QO	QEM	QGM	QLB	QG	TG	TS	TT	TC	KH	KF	KP	UNK
LINE															
ML 240:	16		16	15	16			23	18	17	15	18			
ML 220:	15		15	14	17		18		18	17	17	17			
ML 200:	18		16	14	17	15	19		19	20	15	13			
ML 180:	16	12	12	15	13	14	18		19	18	18	15			
ML 160:	18	16	9	13	13	13				19	16	15	12		
ML 140:	14		16						16	17	16	16	16		15
ML 120:	16		19				15		17	17	16	17	18		21
ML 100:	17		17							20	16	16	17		21
ML 80:	17	12	17		19					17	17	17	19		
ML 60:	19		16		19					20	17	18	18		
ML 40:	17		17		16						19	16	19		
ML 20:	18		15		22						18	18	17	12	
TL 5020:			14	12	15								15		
TL 5040:		11	14		17	8						15	18		
TL 5060:	16		16				15				15	17	18		
TL 5080:	15						17			17	17	17			
TL 5100:	16								17	17	16	18			
TL 5120:	18							21	19	18	17				

Table IV.3 Geologic Unit Average Value as a Function of Map Line for K (PC Times 100)

UNIT:	QAL	QD	QO	QEM	QGM	QLB	QG	TG	TS	TT	TC	KH	KF	KP	UNK
LINE															
ML 240:	151		144	135	142			169	156	155	152	146			
ML 220:	159		143	138	147		164		157	153	149	156			
ML 200:	156		143	138	148	150	139		162	161	150	127			
ML 180:	150	140	111	140	136	144	155		164	156	150	149			
ML 160:	158	148	142	142	139	149				170	160	145	140		
ML 140:	150		148						170	166	155	147	152		149
ML 120:	159		159				164		162	160	157	157	154		159
ML 100:	155		158							172	163	157	155		155
ML 80:	158	169	158		160					171	164	157	156		
ML 60:	153		160		158					172	163	154	162		
ML 40:	146		155		163						171	154	157		
ML 20:	163		148		164						162	150	156	143	
TL 5020:			145	141	146								156		
TL 5040:		148	158		155	139						149	164		
TL 5060:	137		154				160				157	152	151		
TL 5080:	153						157			153	161	153			
TL 5100:	160								160	163	165	152			
TL 5120:	165							177	166	169	179				

Table IV.4 Geologic Unit Average Value as a Function of Map Line for eU/eTh (Times 100)

UNIT:	QAL	QD	QO	QEM	QGM	QLB	QG	TG	TS	TT	TC	KH	KF	KP	UNK
LINE															
ML 240:	25		27	27	25			29	25	25	22	27			
ML 220:	23		26	25	27		25		27	25	26	25			
ML 200:	28		28	24	28	24	32		27	27	24	25			
ML 180:	25	28	32	25	24	26	26		26	26	27	27			
ML 160:	26	28	20	27	30	25				26	25	26	27		
ML 140:	24		25						22	26	24	25	24		23
ML 120:	24		28				22		23	28	26	25	28		29
ML 100:	26		25							27	24	25	25		31
ML 80:	26	20	26		27					23	24	27	27		
ML 60:	28		29		26					30	25	30	27		
ML 40:	30		25		22						26	26	28		
ML 20:	28		24		28						26	29	27	19	
TL 5020:			24	22	24								25		
TL 5040:		23	24		26	21						26	26		
TL 5060:	28		23				22				24	28	30		
TL 5080:	26						26			26	24	28			
TL 5100:	24								25	26	25	28			
TL 5120:	28							27	26	26	26				



Table IV.5 Geologic Unit Average Value as a Function of Map Line for eU/K (Times 1000)

UNIT:	QAL	QD	QO	QEM	QGM	QLB	QG	TG	TS	TT	TC	KH	KF	KP	UNK
LINE															
ML 240:	1108		1166	1164	1192			1419	1170	1163	1000	1242			
ML 220:	1007		1092	1082	1222		1096		1206	1126	1181	1142			
ML 200:	1225		1155	1075	1214	1047	1416		1242	1284	1046	1128			
ML 180:	1129	878	1224	1081	1011	980	1187		1184	1218	1223	1025			
ML 160:	1184	1087	655	972	1008	926				1145	1066	1048	920		
ML 140:	982		1093					977	1062	1067	1103	1073			1022
ML 120:	1016		1231				927	1101	1076	1043	1143	1207			1362
ML 100:	1148		1100						1191	1040	1027	1156			1418
ML 80:	1074	726	1131		1207				1027	1082	1097	1236			
ML 60:	1254		1014		1226				1179	1092	1202	1178			
ML 40:	1223		1093		989					1143	1099	1266			
ML 20:	1166		1072		1349					1146	1256	1148	774		
TL 5020:			1020	880	1072								1001		
TL 5040:		757	941		1114	611						1062	1150		
TL 5060:	1229		1097				971				999	1177	1230		
TL 5080:	1018						1131			1152	1072	1152			
TL 5100:	1005							1125	1100	1017	1267				
TL 5120:	1130							1200	1178	1124	974				

Table IV.6 Geologic Unit Average Value as a Function of Map Line for eTh/K (Times 1000)

UNIT:	QAL	QD	QO	QEM	QGM	QLB	QG	TG	TS	TT	TC	KH	KF	KP	UNK
LINE															
ML 240:	4400		4301	4336	4649			4754	4594	4571	4516	4608			
ML 220:	4226		4112	4303	4495		4339		4481	4521	4530	4517			
ML 200:	4334		4059	4359	4234	4342	4406		4576	4620	4381	4332			
ML 180:	4339	3098	3751	4232	4083	3706	4453		4529	4570	4449	3730			
ML 160:	4548	3844	3109	3582	3407	3684				4314	4226	3957	3320		
ML 140:	3990		4355					4369	3999	4434	4358	4515			4305
ML 120:	4198		4396				4077	4784	3804	4007	4492	4306			4651
ML 100:	4398		4279						4424	4299	4120	4491			4534
ML 80:	4078	3465	4158		4393				4373	4429	3953	4585			
ML 60:	4396		3494		4621				3944	4376	3947	4234			
ML 40:	4066		4289		4394					4412	4147	4396			
ML 20:	4194		4422		4750					4343	4298	4153	4375		
TL 5020:			4135	4040	4353								4017		
TL 5040:		3276	3899		4292	2814						4046	4332		
TL 5060:	4384		4564				4283				4135	4160	4095		
TL 5080:	3826						4319			4330	4408	4073			
TL 5100:	4114							4446	4158	4007	4364				
TL 5120:	4016							4458	4414	4219	3748				

eTh		eU		K		eU/eTh		eU/K		eTh/K		MAX. NO. EVENTS	GEOL. UNIT
$\sigma$	$\bar{x}$	$\sigma$	$\bar{x}$	$\sigma$	$\bar{x}$	$\sigma$	$\bar{x}$	$\sigma$	$\bar{x}$	$\sigma$	$\bar{x}$		
0.9723	6.6	0.3977	1.7	0.1851	1.6	0.0634	0.2686	0.2752	1.1297	0.5309	4.2299	3550.0	QAL
1.0036	4.8	0.4220	1.3	0.1188	1.5	0.0767	0.2691	0.2829	0.8905	0.5563	3.3138	370.0	QD
1.1329	6.2	0.4156	1.6	0.1884	1.5	0.0665	0.2615	0.2919	1.0705	0.5947	4.1192	3913.0	QO
0.6984	5.8	0.3236	1.5	0.0925	1.4	0.0623	0.2540	0.2497	1.0487	0.5524	4.1673	1384.0	QEM
0.8945	6.7	0.4138	1.8	0.1511	1.5	0.0575	0.2629	0.2571	1.1618	0.4630	4.4390	2430.0	QGM
1.0961	5.8	0.3556	1.4	0.1074	1.5	0.0546	0.2534	0.2378	0.9822	0.6637	3.9060	456.0	QLB
0.6517	6.8	0.2981	1.8	0.1225	1.5	0.0500	0.2670	0.2358	1.1699	0.4062	4.3855	482.0	QG
0.5819	8.0	0.2999	2.3	0.0948	1.7	0.0454	0.2893	0.2017	1.3368	0.4209	4.6433	122.0	TG
0.9334	7.3	0.3957	1.9	0.1481	1.6	0.0582	0.2602	0.2613	1.1650	0.5017	4.5025	3324.0	TS
0.9273	7.1	0.4009	1.9	0.1623	1.6	0.0608	0.2683	0.2587	1.1548	0.5109	4.3345	5139.0	TT
0.9140	6.9	0.3829	1.7	0.1429	1.6	0.0595	0.2526	0.2620	1.0754	0.5845	4.2872	8100.0	TC
0.8780	6.3	0.3769	1.7	0.1265	1.5	0.0641	0.2763	0.2634	1.1404	0.5521	4.1619	5559.0	KH
0.8804	6.8	0.4009	1.8	0.1246	1.6	0.0590	0.2728	0.2701	1.1776	0.5454	4.3327	3366.0	KF
1.8119	5.7	0.3054	1.2	0.4261	1.4	0.0413	0.1904	0.1474	0.7746	0.9852	4.3759	28.0	KP
0.7207	7.1	0.4224	2.0	0.1011	1.6	0.0551	0.2842	0.2640	1.2951	0.3733	4.5598	228.0	UNK

Table IV.7 Mean ( $\bar{x}$ ) and Standard Deviation ( $\sigma$ ) for Each Geologic Type.



TABLE IV.8 Geologic Units with Apparent Significant Variations from Unimodal Distributions, Based on the Analysis of the eTh Histograms\*

Geologic Unit	No. Events	eTh Recommended Split (equivalent ppm)
Qa1	3550	None
Qd	370	"
Qo	3913	"
Qem	1384	"
Qgm	2430	"
Q1b	456	"
Qg	482	"
Ts	3324	"
Kh	5558	"
Kf	3366	"
Unk	228	None

TABLE IV.9 SUMMARY OF ANOMALIES BISMARCK

		ETH	EU	EU/ETH
ML240	TS	3760- 3765	TS	3760- 3765
		4045- 4050		3790
	QEM	5580- 5585		4045- 4050
				( 4095- 4100)
			QAL	4615- 4620
			QU	4740
			QGM	5145
			QEM	5580- 5585
			QGM	( 5790- 5795)
ML220			TT	( 2535- 2540)
ML200	TT	3631- 3636	TT	3811
		3776- 3796	QG	4431- 4436
		3811		
	QAL	4586- 4591	QU	5106- 5111
ML180			QU	1086- 1091
				1111- 1116
				1206
			QLB	1486- 1491
			QU	1866- 1871
			TS	3316
ML160	TT	3626	QAL	3496- 3501
			TT	3931- 3936
			TC	4501- 4516
			QAL	5089- 5094
ML140	TC	2816- 2831	TC	2831- 2836
		2966- 2971		TS ( 3586- 3596)
ML120	TS	3680	QU	5745- 5750
				TT 3805
				4215- 4235
				TC 4255
				4265- 4270
			QU	6085
ML100	TC	2866- 2871	TT	3331- 3341
	TT	3019- 3029		QAL ( 2201)
ML80	KF	5554	QU	5454- 5459
			KF	5489
				5549- 5559
			QU	5804- 5809
ML60	KH	2523	KF	( 1688- 1693)

(...) DENOTES NEGATIVE ANOMALY

\*Recommended Splits on the Histograms are Given Only Where Such Splits Appear to be Obvious.

(TABLE IV.9 CONT'D)

		ETH		EU		EU/ETH	
ML60		TT	3308-	3318	KF	1743-	1748
					KH	2068	
						2403-	2413
					QAL	2433	
					TT	3308-	3318
						3328	
						3353	
ML40	TC	3661-	3666	TC	3790-	3805	
					4520-	4525	
				QO	5866-	5871	
					5880-	5885	
					QAL	5201	
ML20	QGM	1386-	1391	QO	1221-	1226	
				QGM	1401-	1416	
				KH	2376-	2381	
TL5020							
TL5040	QD	4313-	4318				
TL5060	KH	2548-	2553				
TL5080							
TL5100				TC	1636-	1641	
TL5120	TT	3844-	3854	TS	3029		
				TT	3819-	3834	
				TC	4164-	4169	
					4234-	4244	

(... ) DENOTES NEGATIVE ANOMALY

TABLE IV.10 Radioactivity Anomalies per Geologic Map Unit

Geologic Unit	eTh	eU	eU/eTh
<u>Quaternary</u>			
Qa1	0	3	3(1)
Qd	1	0	1
Qo	0	6	7
Qem	0	1	2
Qgm	1	1	1(1)
Q1b	0	0	1
Qg	0	0	1
<u>Tertiary</u>			
Ts	1	3	4(2)
Tt	3	7	9(1)
Tc	4	7	12
<u>Cretaceous</u>			
Kh	1	2	3
Kf	1	2	4(2)

(... ) denotes negative anomaly.



TABLE IV.11 Statistical Summary of Radioactivity Anomalies per Geologic Period(s)

Geologic Unit	eTh	eU	eU/eTh
<u>Quaternary</u>			
No. of Units w/ Anomalies	2	4	7
No. of Anomalies	2	11	16(2)
<u>Tertiary</u>			
No. of Units w/ Anomalies	3	3	3
No. Of Anomalies	8	17	25(3)
<u>Cretaceous</u>			
No. of Units w/ Anomalies	2	2	2
No. of Anomalies	2	4	7(2)
<u>Total Sample</u>			
No. of Units w/ Anomalies	7	9	12
No. of Anomalies	12	32	48(7)

(...) denotes negative anomaly.

Quaternary Geologic Units: Qal, Qd, Qo, Qem, Qgm, Qlb, Qg

eTh Anomalies

Approximately seventeen percent of the eTh anomalies reported from the Bismarck map sheet area are present in the units Qd and Qgm. The Quaternary units are exposed over roughly thirty percent of the map surface. Given the fact that the thorium ion is relatively insoluble and does not readily concentrate in surface waters, the anomalies are not considered to be significant.

eU and eU/eTh Anomalies

Thirty-four percent of the eU anomalies and thirty-three percent of the positive eU/eTh anomalies are recorded over the Quaternary units. Of these anomalies, well over one-third (54% and 44%, respectively) occur in the unit Qo. Twenty-eight percent of the negative ratio anomalies are present. There is one point of geographical coincidence between the Quaternary eU and eU/eTh anomalies; namely, ML240, stations 5580-5585 (Qem). The anomalies are probably not economically significant.

Tertiary Geologic Units: Ts, Tt, Tc

eTh Anomalies

Approximately sixty-seven percent of the eTh anomalies are found in the units Tc, Tt and, to a lesser extent, unit Ts. The Tertiary exposures comprise roughly forty percent of all outcrops in the Bismarck map area.

eU and eU/eTh Anomalies

Fifty-three percent of the eU anomalies and fifty-two percent of the positive eU/eTh anomalies are reported from the Tertiary units. Approximately forty-three percent of the negative ratio anomalies are found in the units. There are nine geographical coincidences of eU and eU/eTh anomalies: ML40, stations 3795-3805 and 4520-4525 (Tc); ML60, stations 3308-3318 (Tt); ML160, station 4506 (Tc); ML200, station 3811 (Tt); ML240, stations 3760-3765 and 4045-4050 (Ts); TL5100, stations 1636-1641 (Tc); and TL5120, stations 3824-3834 (Tt).

The loci of coincidental anomalies in these Fort Union Group members may yield significant concentrations of uranium, especially where the anomalies are associated with organic deposits.



Cretaceous Geologic Units: Kh, Kf

#### eTh Anomalies

Approximately seventeen percent of the eTh anomalies are recorded from Cretaceous exposures which make up roughly thirty percent of the map surface area.

#### eU and eU/eTh Anomalies

Approximately twelve and one-half percent of the eU anomalies and fourteen and one-half percent of the positive ratio anomalies are reported from the Cretaceous units. Twenty-eight percent of the negative ratio anomalies are present in the unit Kf. There are no coincidental anomalies within the Cretaceous exposures. The anomalies are presumably not economically significant.

#### Relationship between Radioactivity Anomalies and Known Radioactive Mineral Deposits

There are no reported radioactive mineral deposits directly within the Bismarck map sheet area (see Section III.D).

#### Relationship of Radioactivity Data to Cultural Features

Cultural features in the Bismarck map sheet area which may produce an effect on radioactivity data include the towns of Bismarck, Driscoll, Elgin, Flasher, Fort Yates, Glen Ullin, Hazelton, Linton, Mandan, New Salem, Selfridge and Strasburg. Major bodies of water include the Missouri River, the Geneva, Long, Magnuson, Rice, Schwahn, and Tschida lakes, the Strong Slough, and the Oahe Reservoir, as well as numerous intermittent lakes.

Water may have had a slight causative effect on the positive ratio anomalies associated with Long Lake: ML180, stations 1111-1116 and 1206 (Qo), and the positive ratio anomaly in the vicinity of the Missouri River: ML240, station 4740 (Qo).

#### Trends

#### eTh Anomalies

The eTh anomalies in the Bismarck map sheet area are roughly delimited into two loose clusters. The first is located in the southeastern corner of the map, and the second lies along the westcentral edge of the map sheet. The eTh anomalies are relatively scant in the map region.

#### eU Anomalies

Except for a paucity of eU anomalies in the northeastern corner of the map, the anomalies are relatively randomly distributed across the map region.

#### eU/eTh Anomalies

The eU/eTh anomalies are fairly uniformly distributed throughout the Bismarck map region, with the exception of the extreme southeastern edge of the map. Their distribution appears to be independent of structure or topography.

### 3. Summary and Recommendations

Over one-half of all eTh, eU and eU/eTh anomalies reported from the Bismarck map sheet area are recorded in the units Ts, Tt and Tc. The presence of relatively many geographically coincident anomalies within these Fort Union Group members seems to concur with known radioactive mineral deposits occurring in the Fort Union due west of the map region. Further, more detailed surveying is suggested.

### F. NATIONAL GAMMA RAY MAP SERIES (NGRMS)

The geologic base has been photographically screened to allow emphasis of the flight line locations and of the information regarding data analysis. These maps are used as the base for presenting statistical information on the six variables:

- \* eTh
- \* eU
- \* K
- \* eU/eTh Ratio
- \* eU/K Ratio
- \* eTh/K Ratio

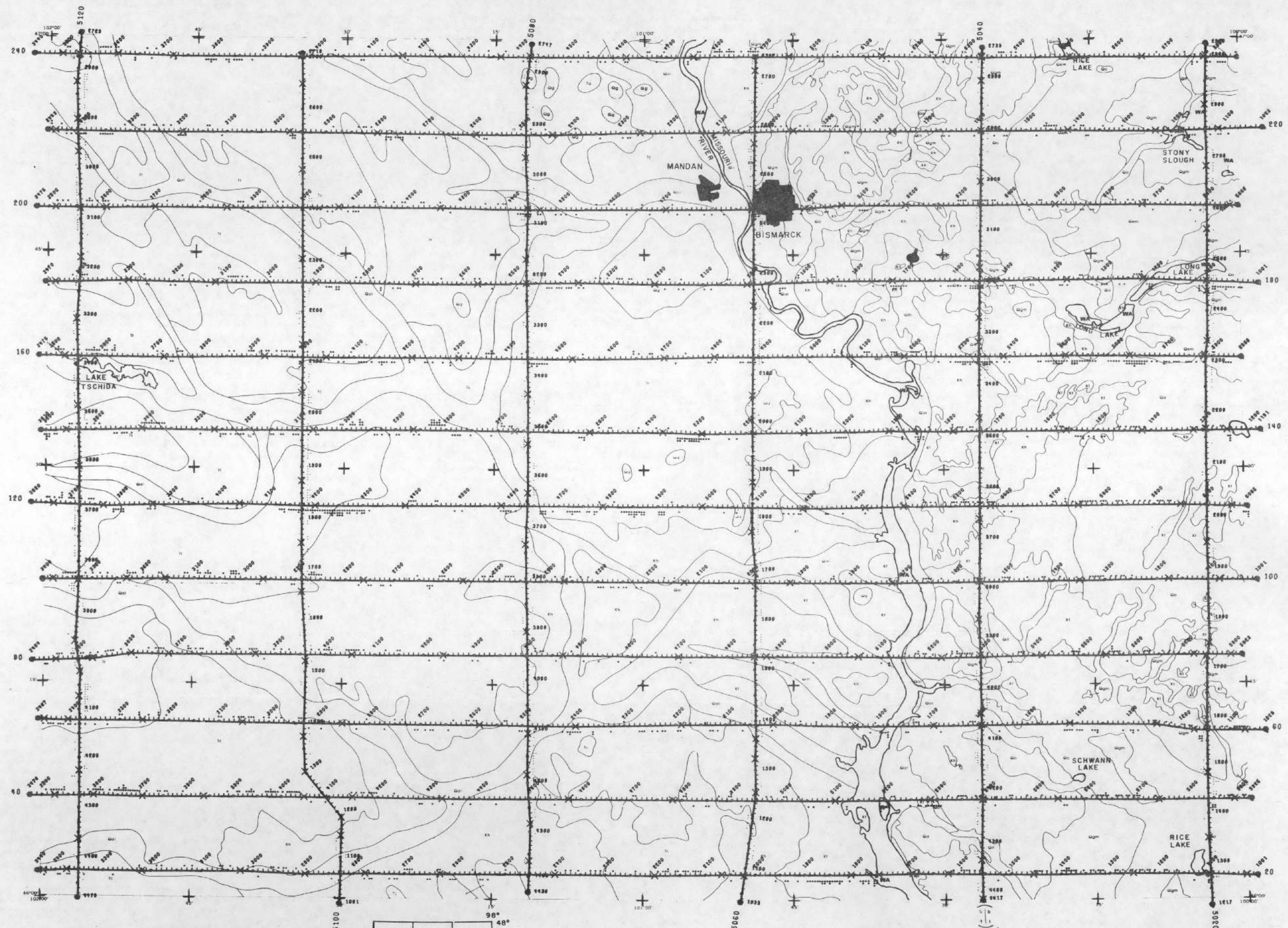
The six NGRMS sheets are presented in Figures IV. (1-6) of this report at a scale of 1:500,000 and as separate sheets at a scale of 1:250,000.

The statistical information is summarized on these maps through the utilization of one, two or three dots above or below the flight line at every fifth data point. One dot above the line indicates that the variable value at that point is between  $1\sigma$  and  $2\sigma$  greater than the mean value for that geologic type where  $\sigma$  values are determined for each geologic type based on all flight line data from the area, as is discussed further in Section V.B.4. Two dots indicate values between  $2\sigma$  and  $3\sigma$ , and three dots show values greater than  $3\sigma$ . Dots below the line indicate the variable values which are less than the mean value by 1, 2 or  $3\sigma$  in the same manner.



G. LINE PRINTER CONTOURS

Printer contours have been generated at a 1:500,000 scale for seven variables ( $eTh$ ,  $eU$ ,  $K$ ,  $eU/eTh$ ,  $eU/K$ ,  $eTh/K$ , and  $RMag$ , respectively). They appear in Appendix IV. Note that every alternate contour interval is composed of blanks to help delineate contour boundaries. Dots are used where the denominator value for a ratio is approaching zero, and to denote non-data areas.



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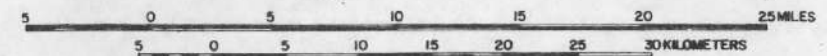
NATIONAL GAMMA RAY MAP SERIES

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ETH ± STANDARD DEVIATIONS  
REF. NTMS, NL 14-4  
PREPARED FOR  
U.S. DEPARTMENT OF ENERGY

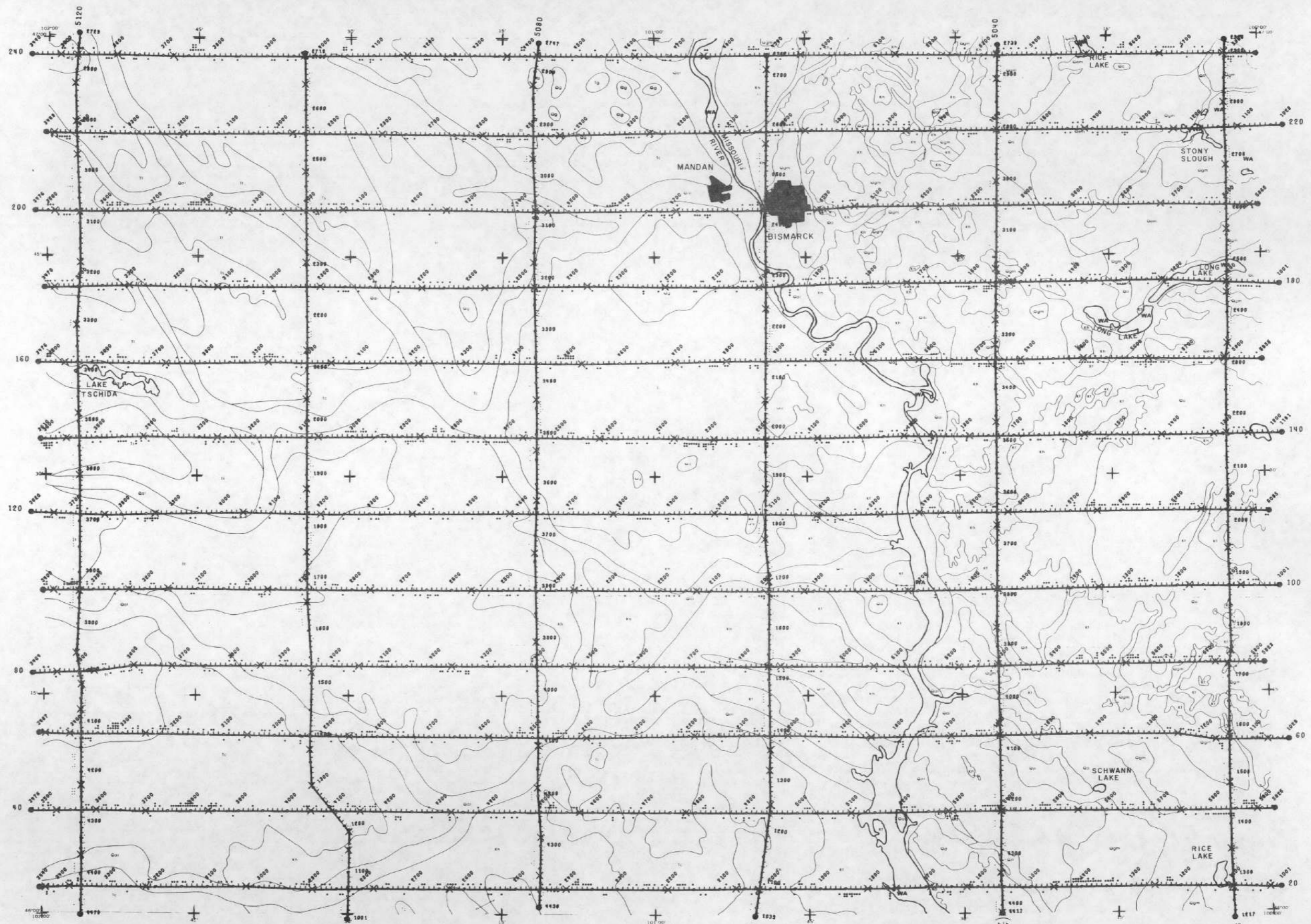
IV-16a



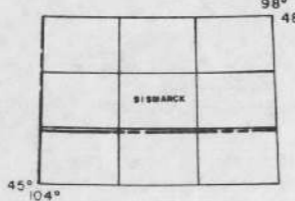
Bismarck, North Dakota

Figure IV.1 National Gamma Ray Map Series

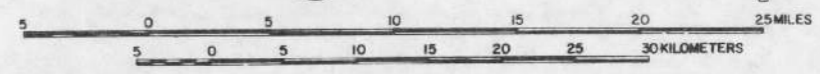




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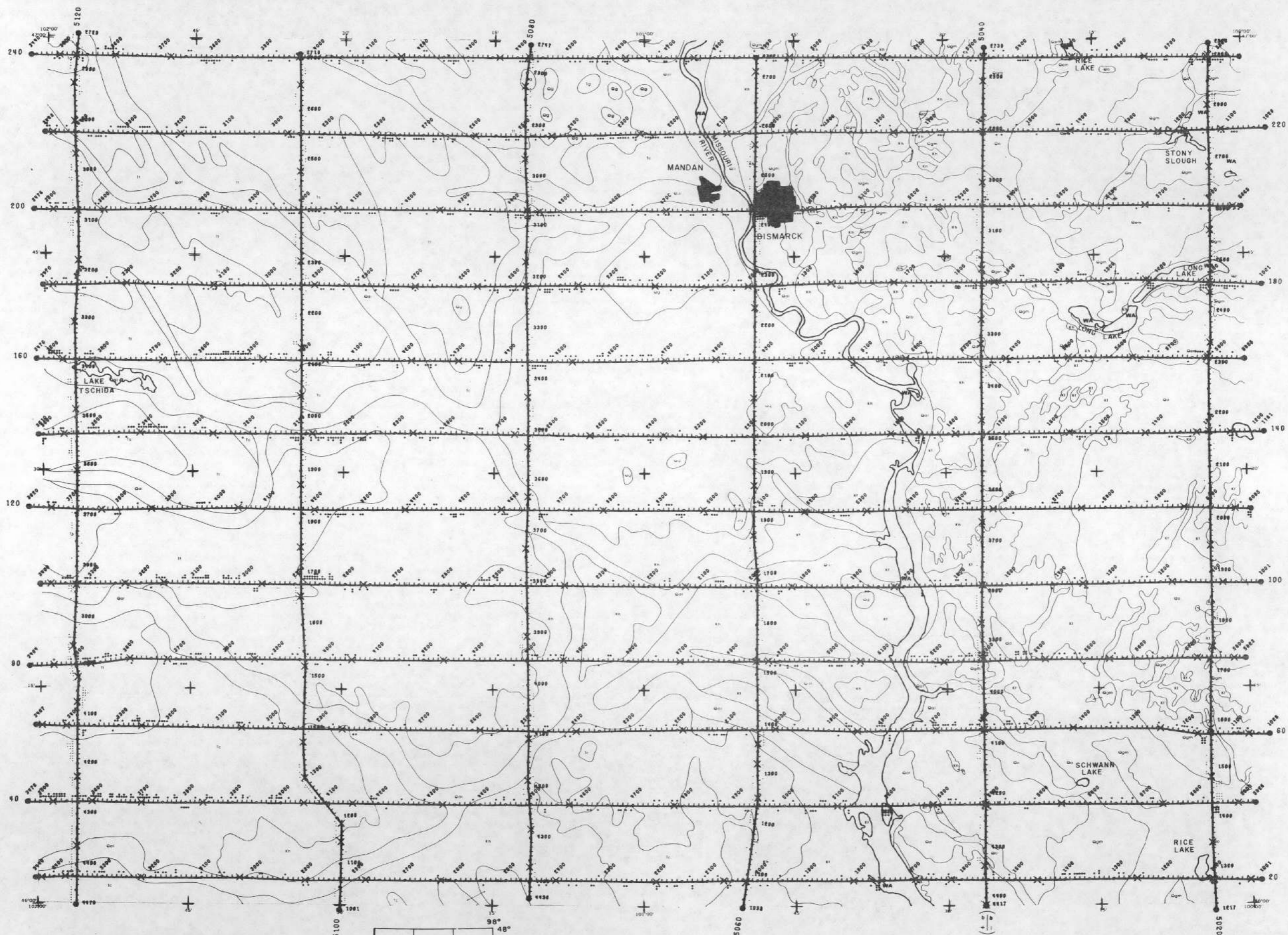


**Bismarck, North Dakota**

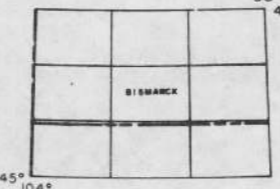
Figure IV.2 National Gamma Ray Map Series



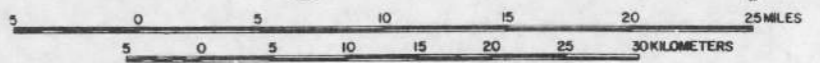




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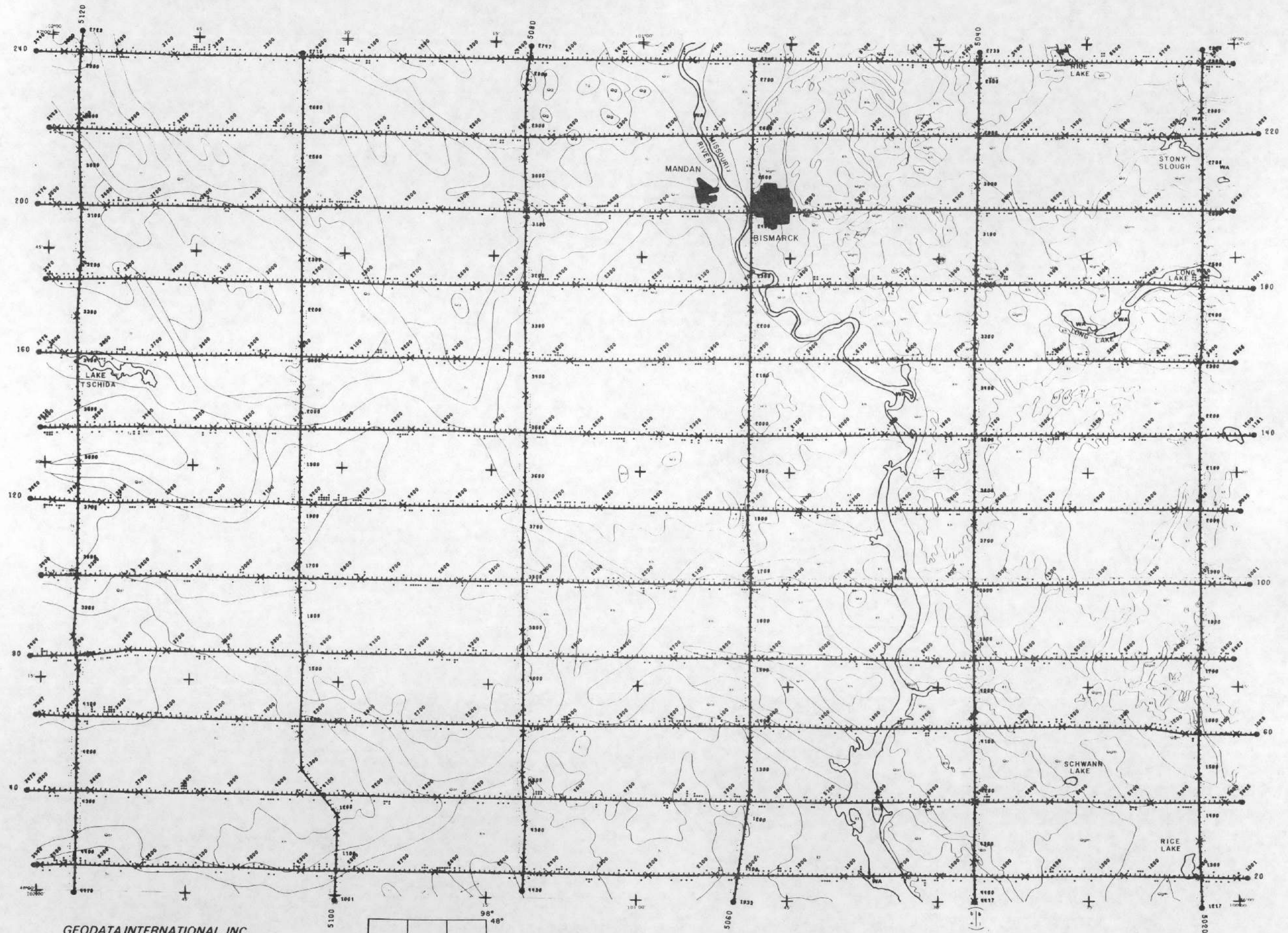


### Bismarck, North Dakota

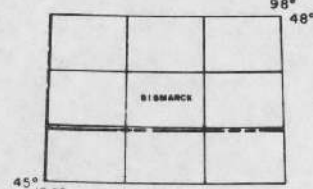
Figure IV.3 National Gamma Ray Map Series



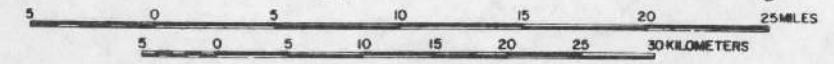




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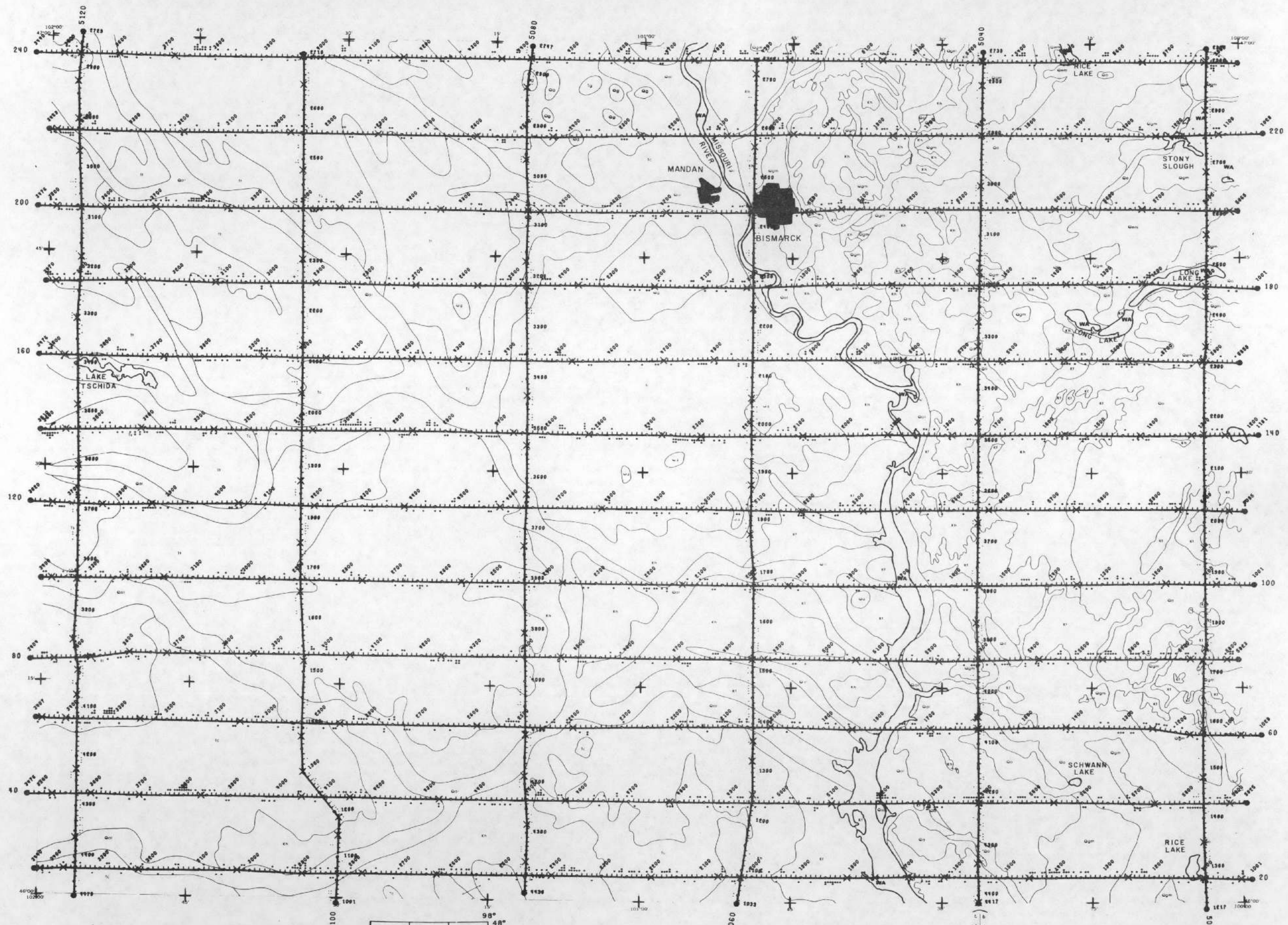


## Bismarck, North Dakota

Figure IV.4 National Gamma Ray Map Series



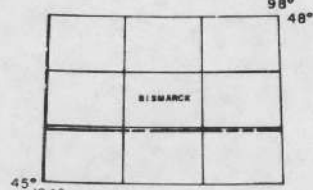




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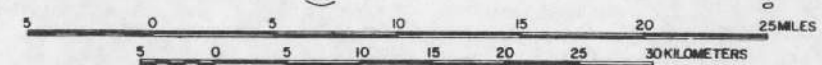
NATIONAL GAMMA RAY MAP SERIES

compiled by  
Martel Laboratories, Inc.



EU/K ± STANDARD DEVIATIONS  
REF. NTMS, NL 14-4  
PREPARED FOR  
U.S. DEPARTMENT OF ENERGY

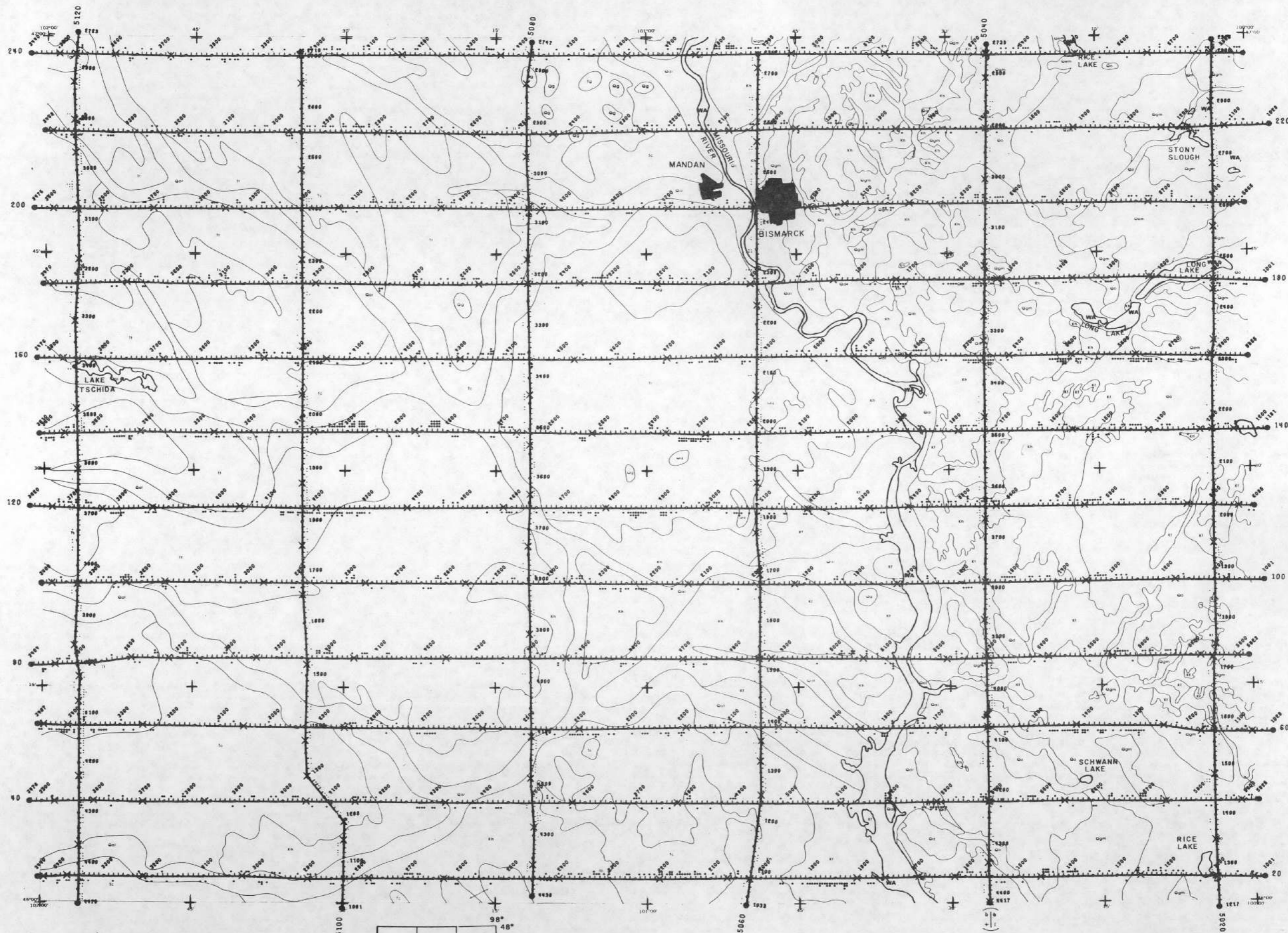
IV-16e



# Bismarck, North Dakota

Figure IV.5 National Gamma Ray Map Series

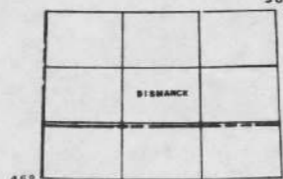




GEODATA INTERNATIONAL, INC.  
7035 John W. Carpenter Frwy., Dallas, Texas 75247

NATIONAL GAMMA RAY MAP SERIES

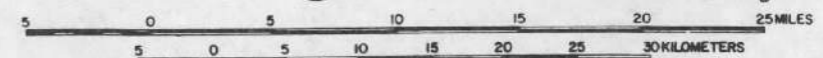
compiled by  
Martel Laboratories, Inc.



ETH/M - STANDARD DEVIATIONS  
REF. NTMS, NL 14-4

PREPARED FOR  
U.S. DEPARTMENT OF ENERGY

IV-16f

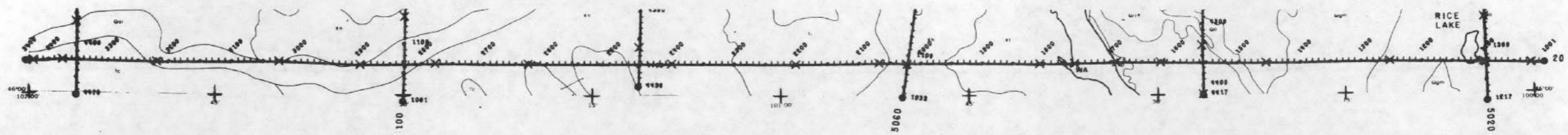


Bismarck, North Dakota

Figure IV.6 National Gamma Ray Map Series

H. STACKED DATA PROFILES AND GEOLOGIC HISTOGRAMS





ETH/K  
50 /DIV

EU/K  
20 /DIV

EU/ETH  
.5 /DIV

GC  
400 C/S/DIV

RMAG  
50 GAMMAS/DIV  
BASE = -450.0

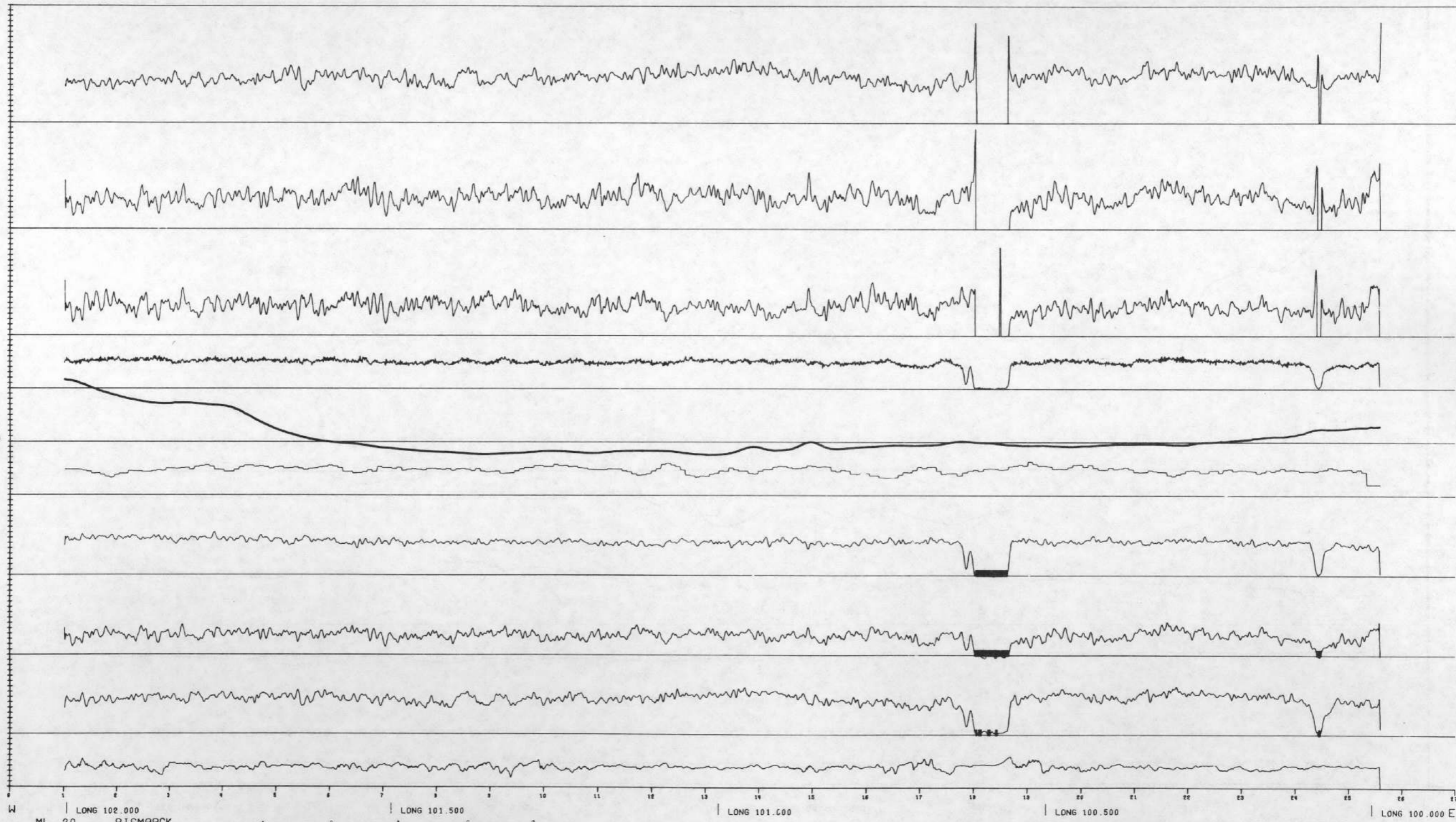
RIAIR  
5.0 C/S/DIV

K  
.25 PC/DIV

EU  
.50 PPM/DIV

ETH  
1.0 PPM/DIV

ALT  
100 FT/DIV



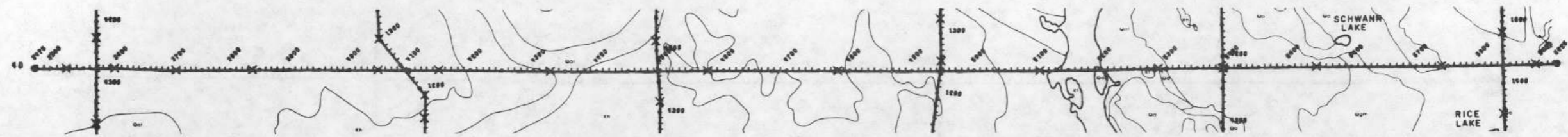
W | LONG 102.000 | LONG 101.500 | LONG 101.000 | LONG 100.500 | LONG 100.000 E

ML 20 BISMARCK









ETH/K  
.50 /DIV



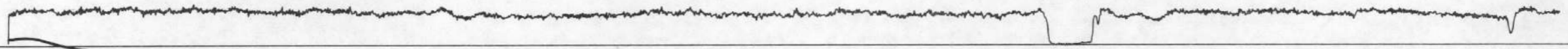
EU/K  
.20 /DIV



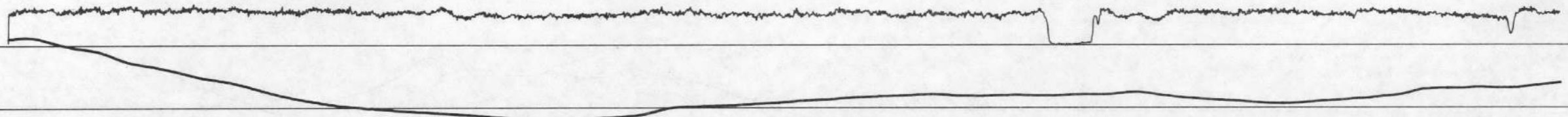
EU/ETH  
.05 /DIV



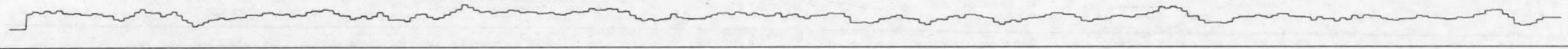
GC  
400 C/S/DIV



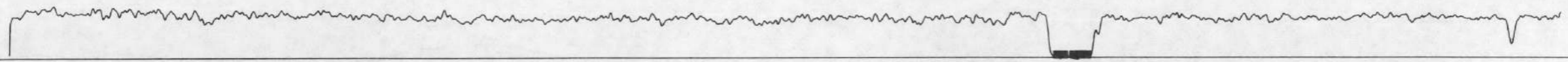
RMAG  
50 GAMMAS/DIV  
BASE = -450.0



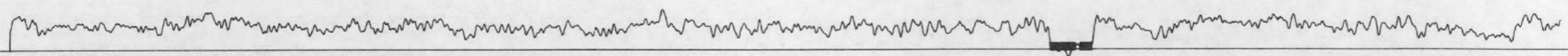
BIAIR  
5.0 C/S/DIV



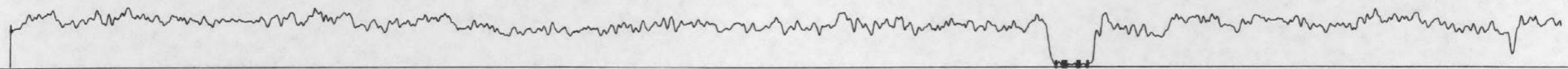
K  
.25 PC/DIV



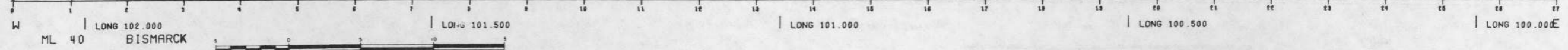
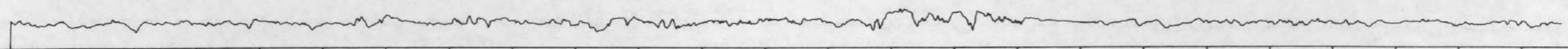
EU  
.50 PPM/DIV

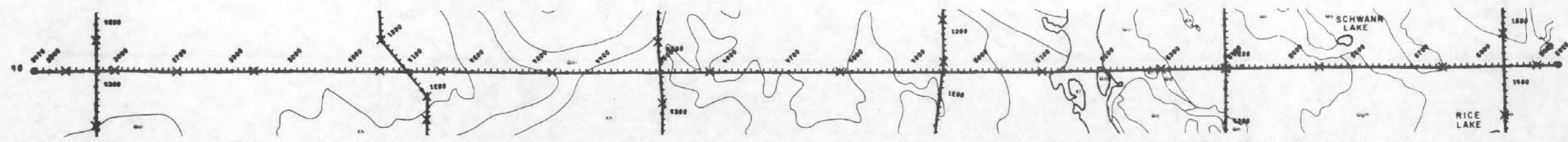


ETH  
1.0 PPM/DIV



ALT  
100 FT/DIV





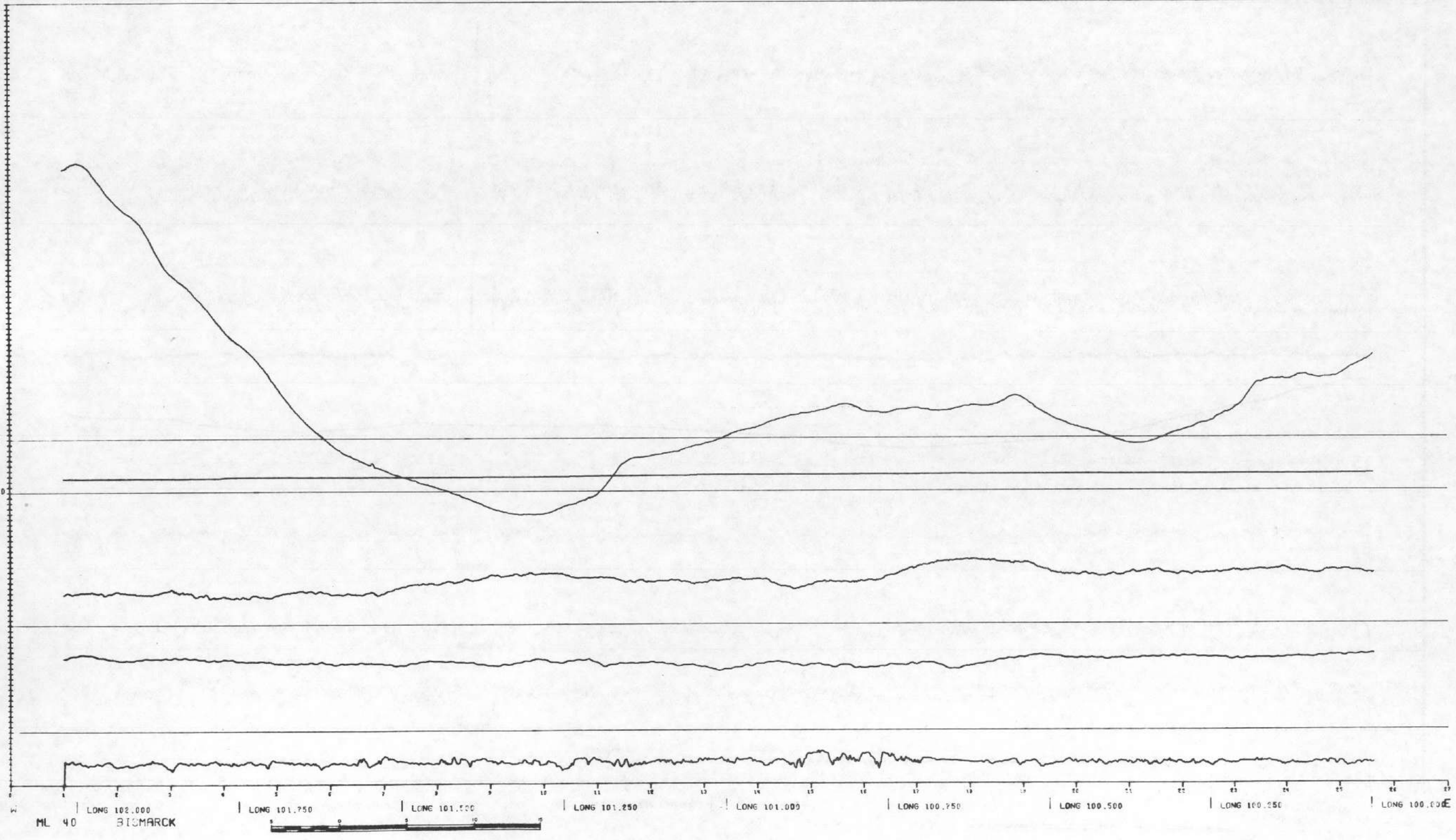
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
20 GAMMA/DIV  
BASE = 59320.0

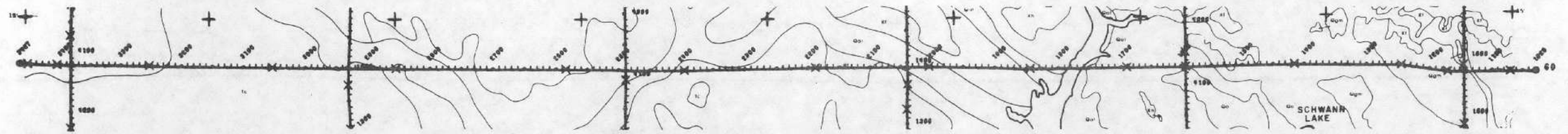
SP  
9 MM HG/DIV  
BASE = 660.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

ALT  
100 FT/DIV







ETH/K  
.50 /DIV

EU/K  
.20 /DIV

EU/ETH  
.05 /DIV

GC  
400 C/S/DIV

RMAG  
50 GAMMAS/DIV  
BASE = -150.0

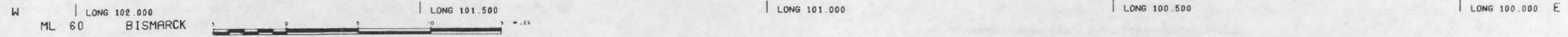
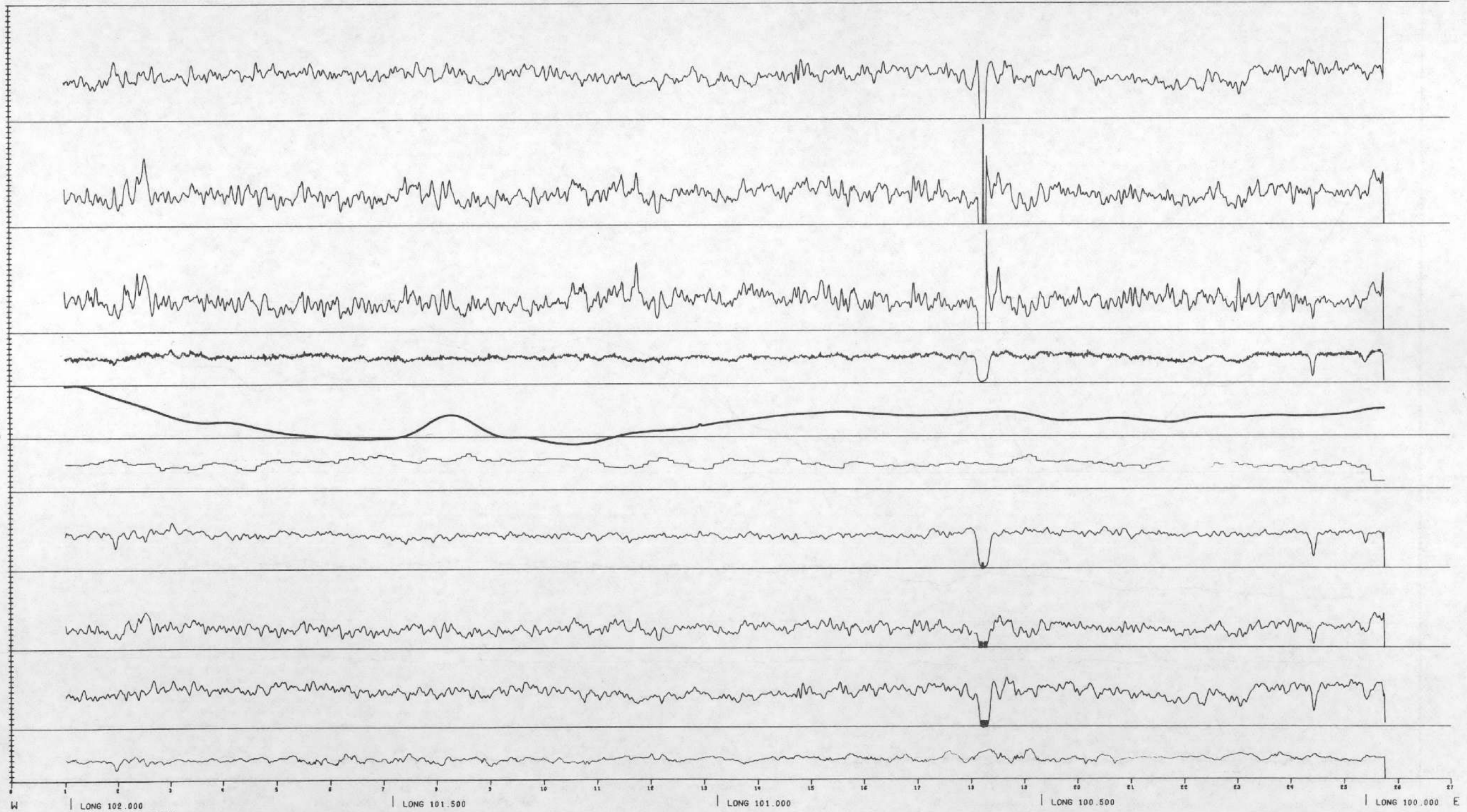
BIAIR  
5.0 C/S/DIV

K  
.25 PC/DIV

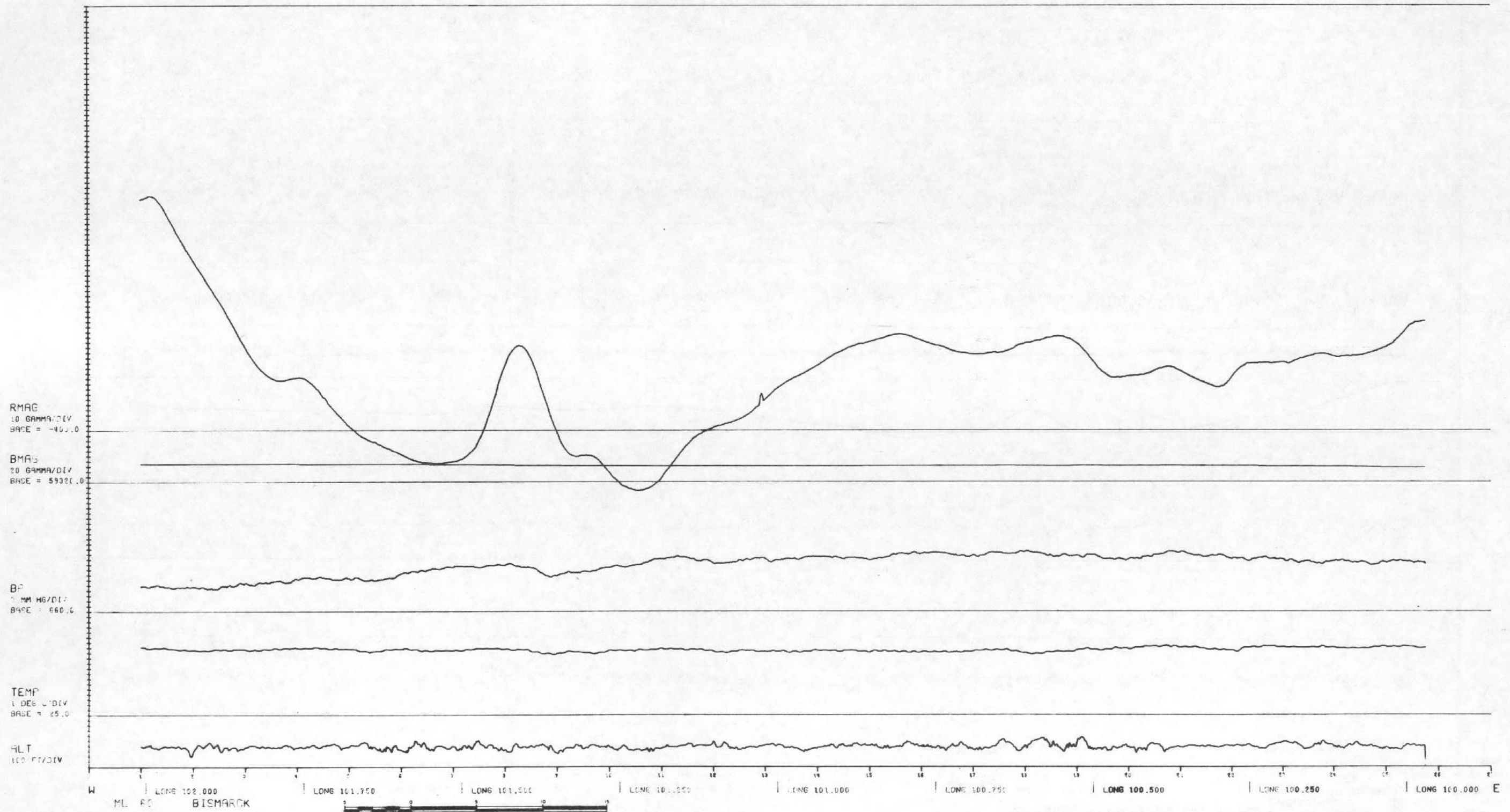
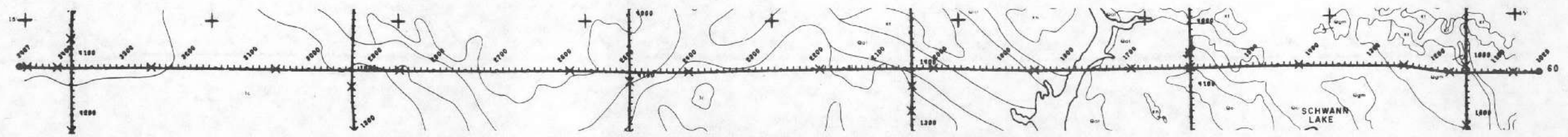
EU  
.50 PPM/DIV

ETH  
1.0 PPM/DIV

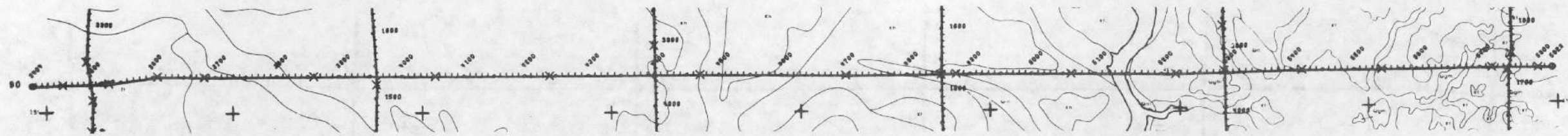
ALT  
100 FT/DIV



ML 60 BISMARCK







ETH/K  
50 /DIV

EU/K  
20 /DIV

EU/ETH  
05 /DIV

GC  
400 C/S/DIV

RMAG  
50 GAMMAS/DIV  
BASE = -450.0

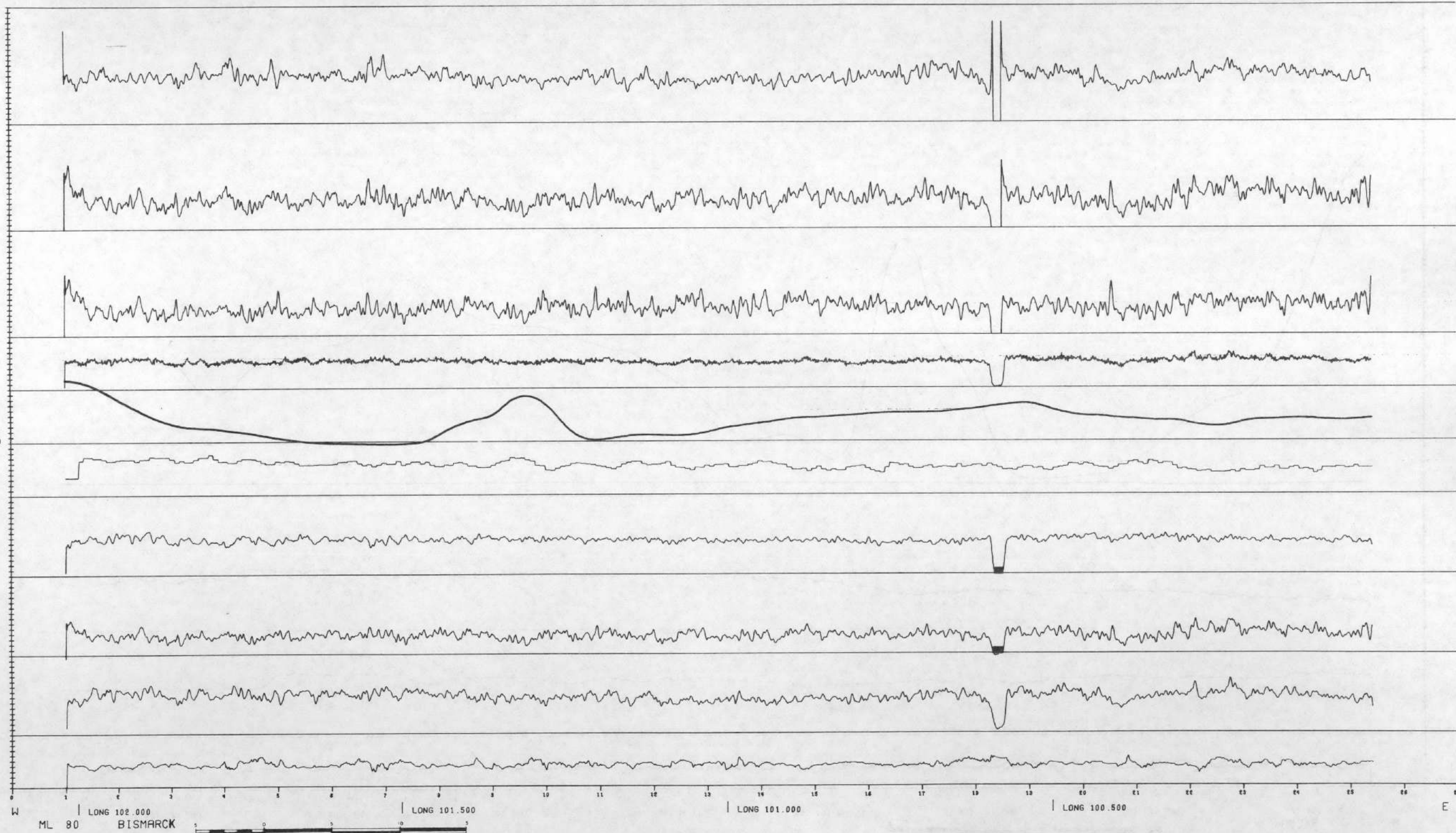
BIAIR  
5.0 C/S/DIV

K  
.25 PC/DIV

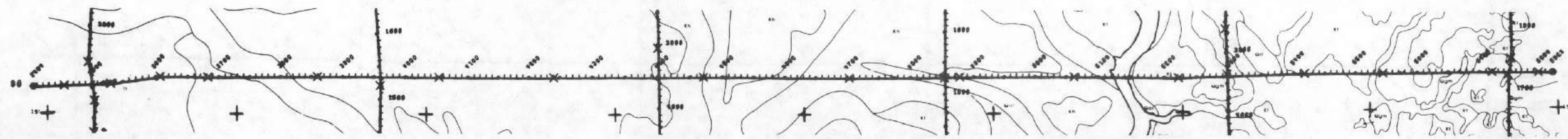
FU  
50 PPM/DIV

ETH  
1.0 PPM/DIV

ALT  
100 FT/DIV



W | LONG 102.000 | LONG 101.500 | LONG 101.000 | LONG 100.500 | E  
ML 80 BISMARCK



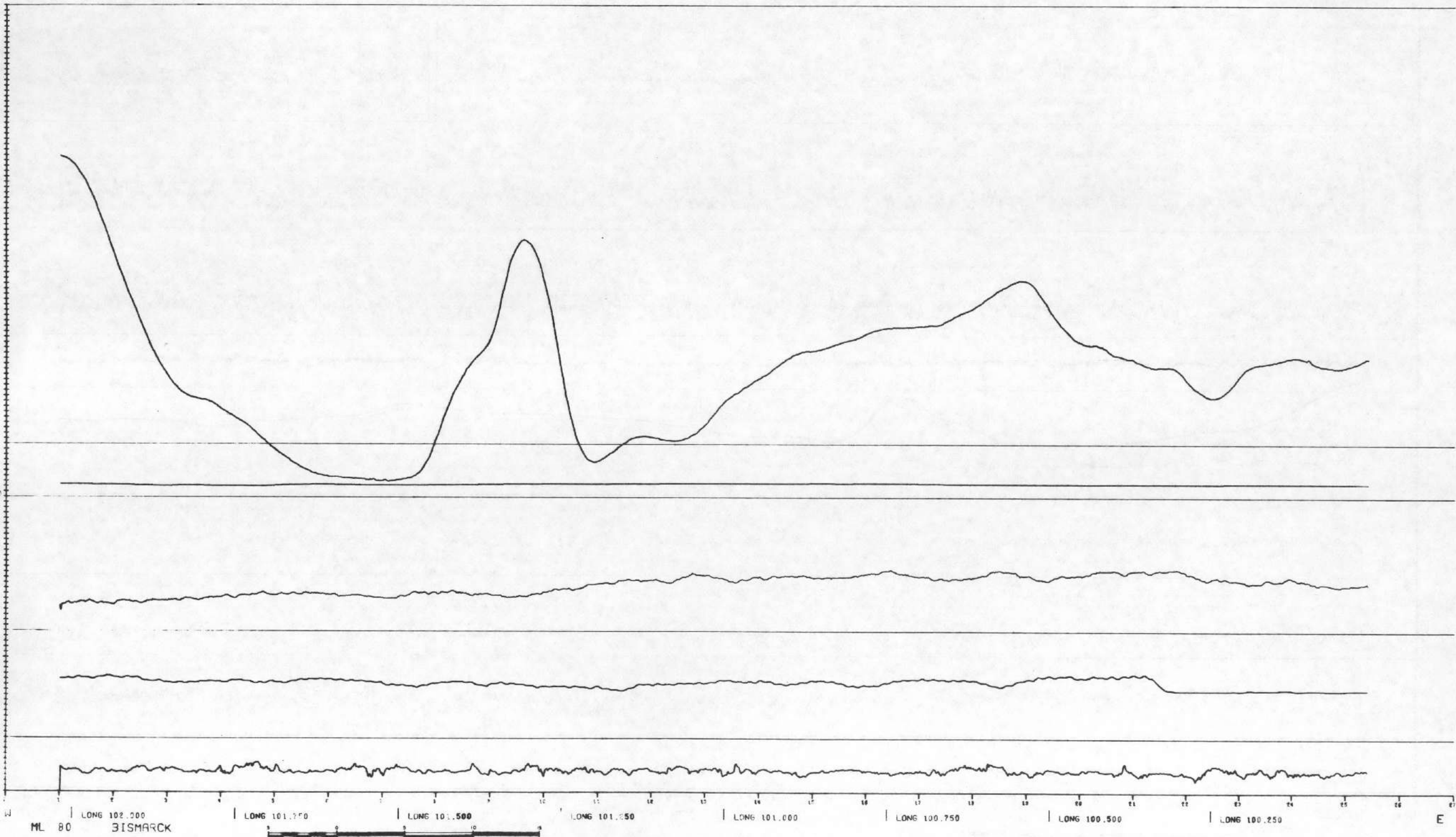
RMH  
10 GRAMS/DIV  
BASE = -100.0

BMA  
20 GRAMS/DIV  
BASE = 59320.0

BP  
3 MM HG/DIV  
BASE = 460.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

ALT  
100 FEET/DIV



ML 80 LONG 102.000 BISMARCK

LONG 101.750

LONG 101.500

LONG 101.250

LONG 101.000

LONG 100.750

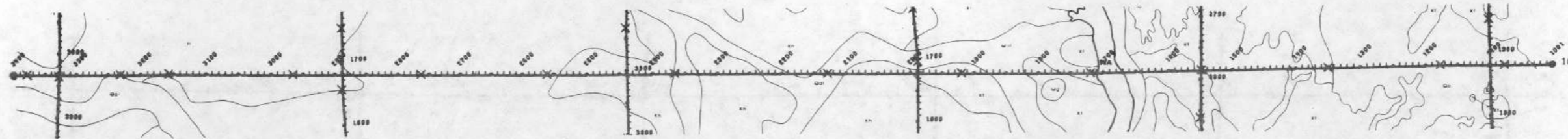
LONG 100.500

LONG 100.250

E







ETH/K  
.50 /DIV

EU/K  
.20 /DIV

EU/ETH  
.05 /DIV

GC  
400 C/S/DIV

RMAG  
50 GAMMAS/DIV  
BASE = -150.0

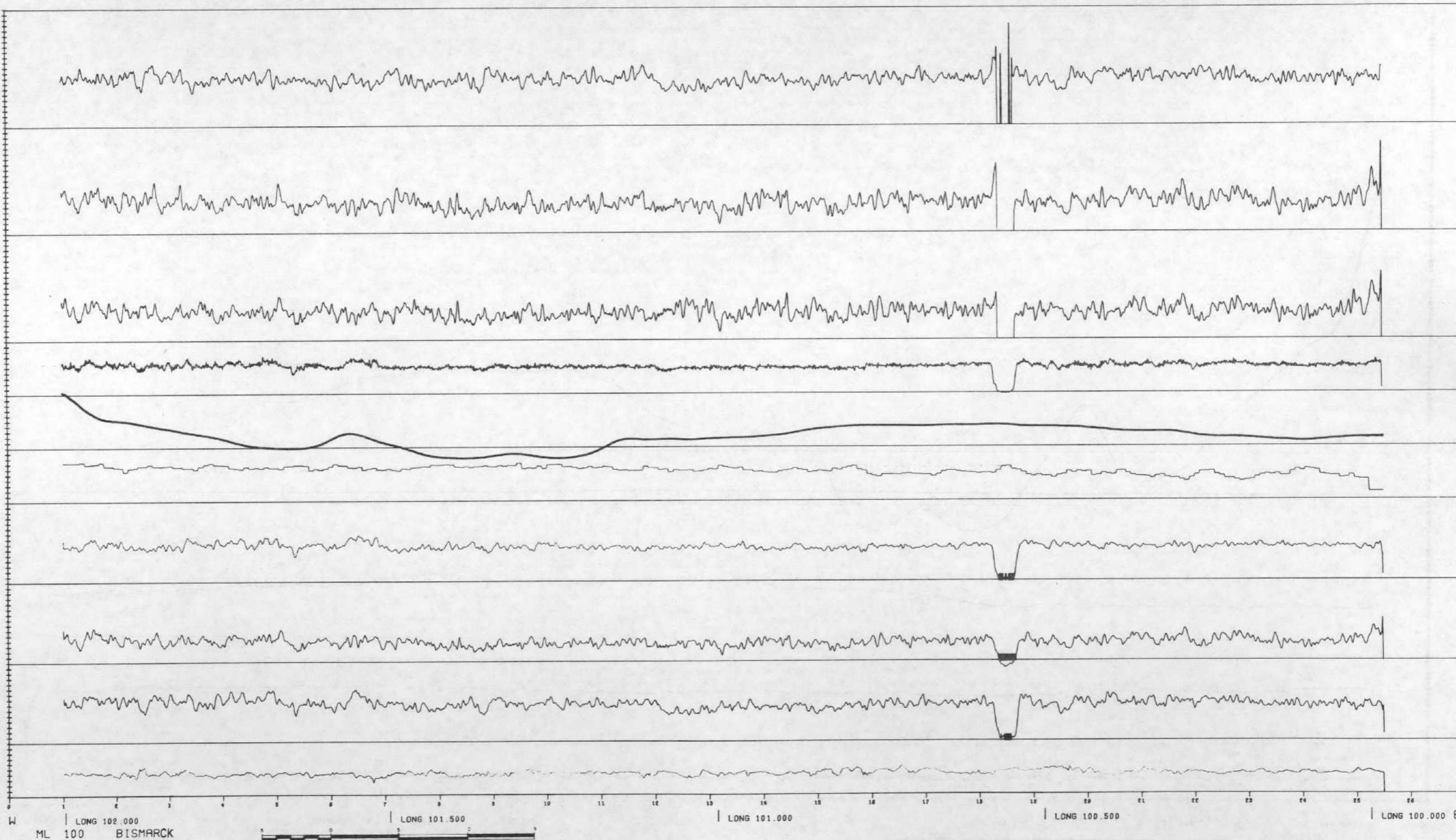
STAIR  
5.0 C/S/DIV

K  
.25 PC/DIV

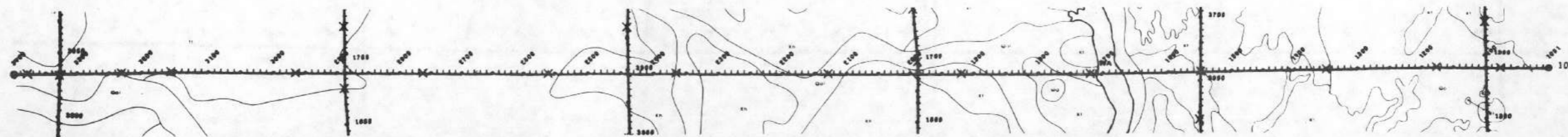
EU  
50 PPM/DIV

ETH  
1.0 PPM/DIV

ALT  
100 FT/DIV



W | LONG 102.000 | LONG 101.500 | LONG 101.000 | LONG 100.500 | LONG 100.000 E  
ML 100 BISMARCK



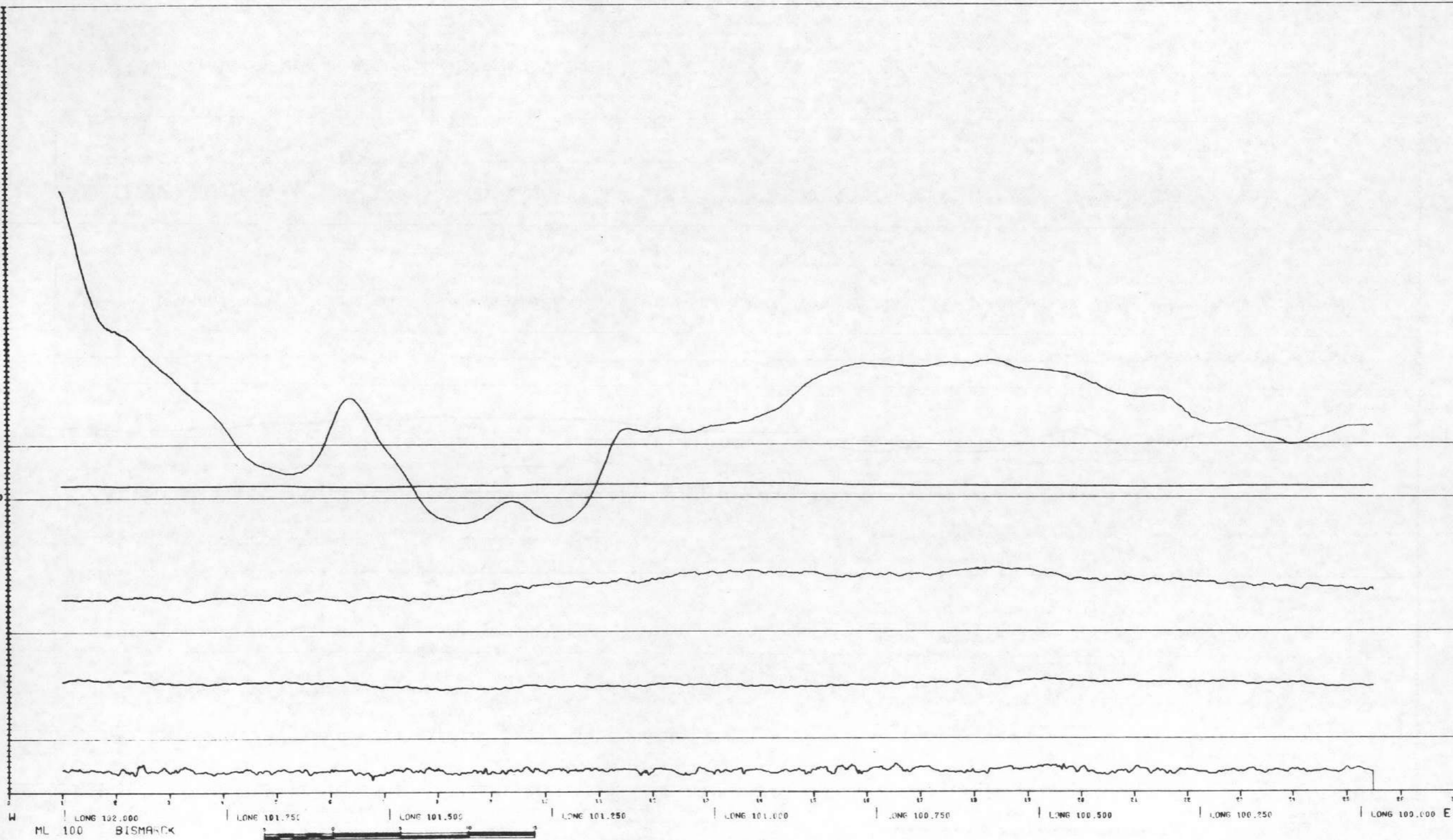
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
10 GAMMA/DIV  
BASE = 59320.0

BP  
3 MM HG/DIV  
BASE = 660.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

ALT  
100 FT/DIV

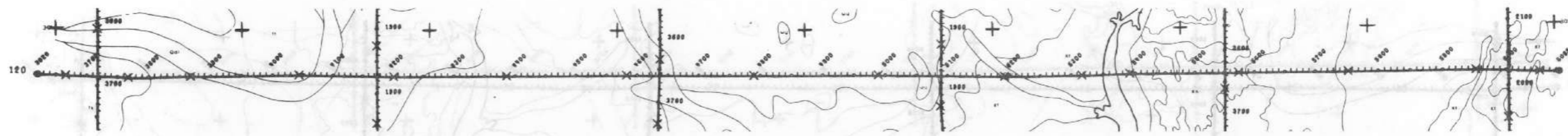


W | LONG 102.000 | LONG 101.750 | LONG 101.500 | LONG 101.250 | LONG 101.000 | LONG 100.750 | LONG 100.500 | LONG 100.250 | LONG 100.000 E

ML 100 BISMARCK







ETH/K  
.50 /DIV

EU/K  
.20 /DIV

EU/ETH  
.05 /DIV

GC  
400 C/S/DIV

RMAG  
30 GAMMAS/DIV  
BASE -450.0

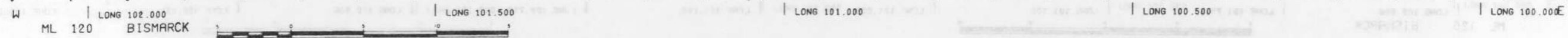
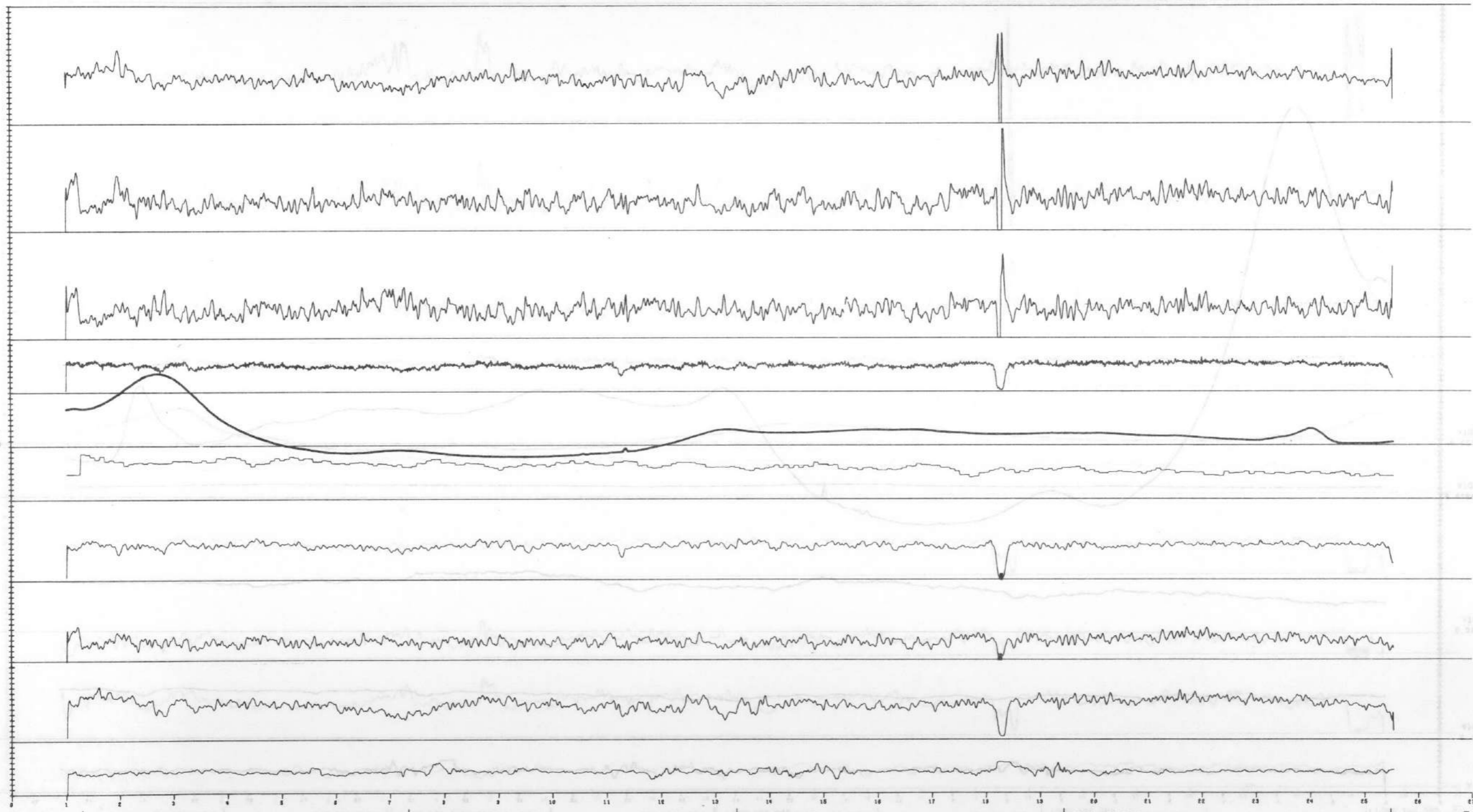
BIAIR  
5.0 C/S/DIV

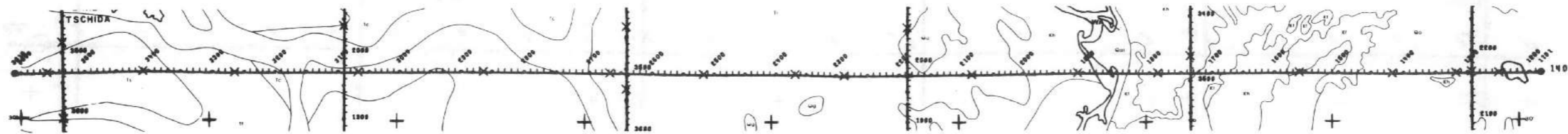
K  
.25 PC/DIV

EU  
.50 PPM/DIV

ETH  
1.0 PPM/DIV

ALT  
100 FT/DIV





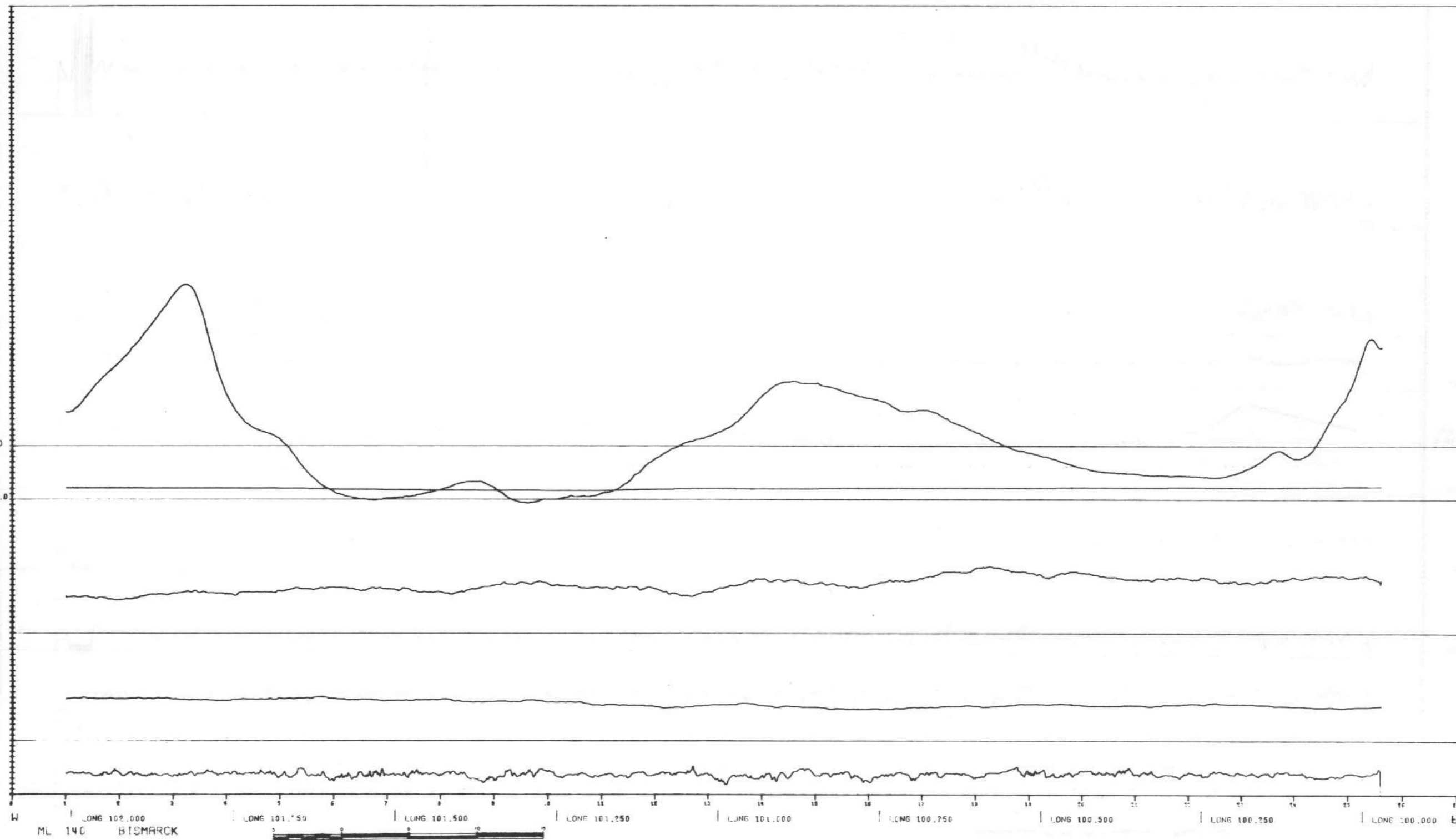
RMAG  
10 GAMMA/DIV  
BASE = -100.0

BMAG  
20 GAMMA/DIV  
BASE = 53320.0

BP  
3 MM HG/DIV  
BASE = 660.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

ALT  
100 FT/DIV

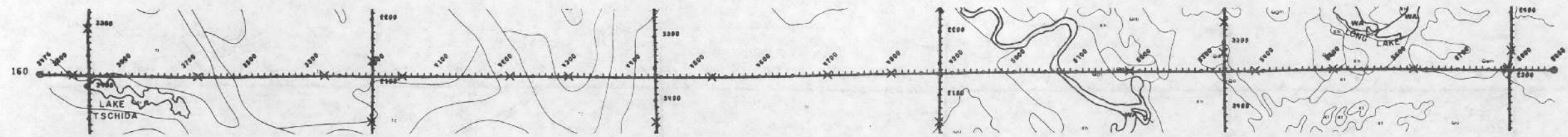


W 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 E  
LONG 102.000 LONG 101.750 LONG 101.500 LONG 101.250 LONG 101.000 LONG 100.750 LONG 100.500 LONG 100.250 LONG 100.000

ML 140 BISMARCK







ETH/K  
50 /DIV

EU/K  
20 /DIV

EU/ETH  
.05 /DIV

GC  
400 C/S/DIV

RMAG  
50 GAMMAS/DIV  
BASE = -450.0

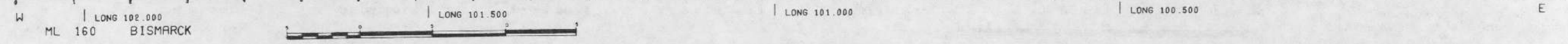
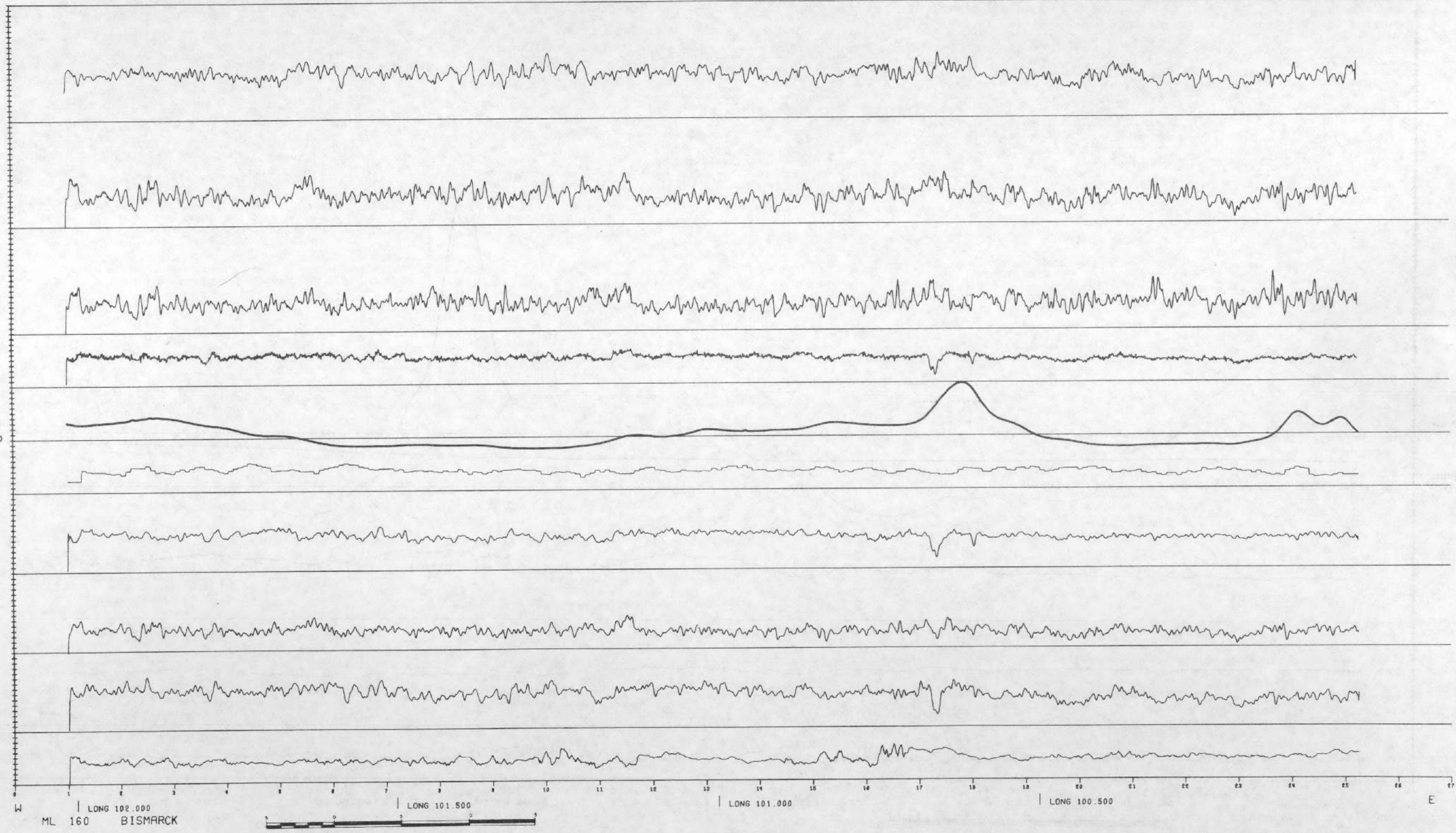
BIAIR  
5.0 C/S/DIV

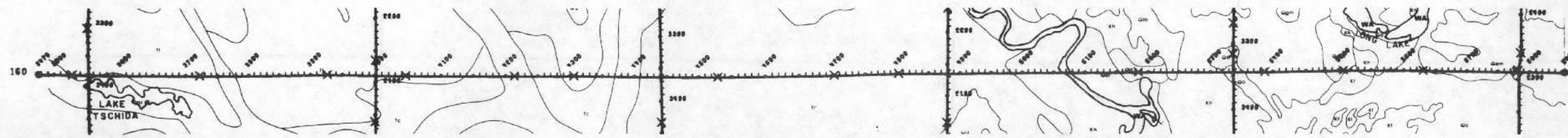
K  
.25 PC/DIV

EU  
50 PPM/DIV

ETH  
1.0 PPM/DIV

ALT  
100 FT/DIV





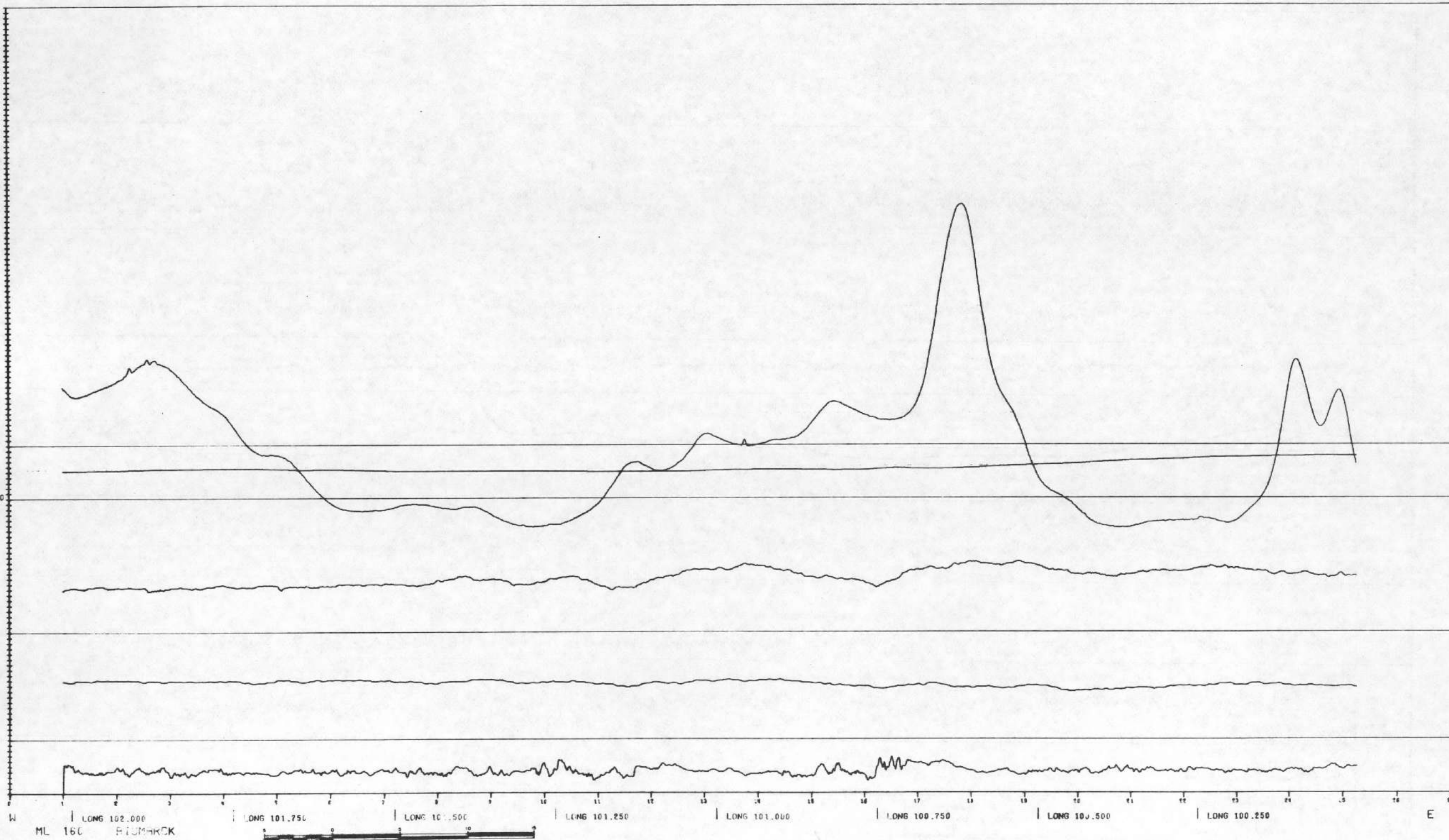
RMAG  
10 GAMMA/DIV  
BASE = -100.0

BMAG  
20 GAMMA/DIV  
BASE = 53320.0

BP  
3 MM HG/DIV  
BASE = 650.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

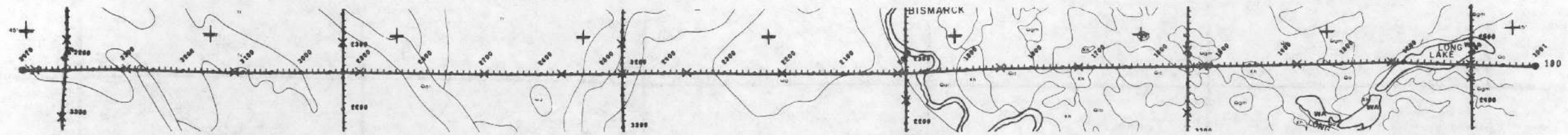
ALT  
100 FT/DIV



W | LONG 102.000 | LONG 101.750 | LONG 101.500 | LONG 101.250 | LONG 101.000 | LONG 100.750 | LONG 100.500 | LONG 100.250 | E

ML 160 BISMARCK





ETH/K  
.50 /DIV

EU/K  
.20 /DIV

EU/ETH  
.05 /DIV

GC  
400 C/S/DIV

RMAG  
50 GAMMAS/DIV  
BASE = -150.0

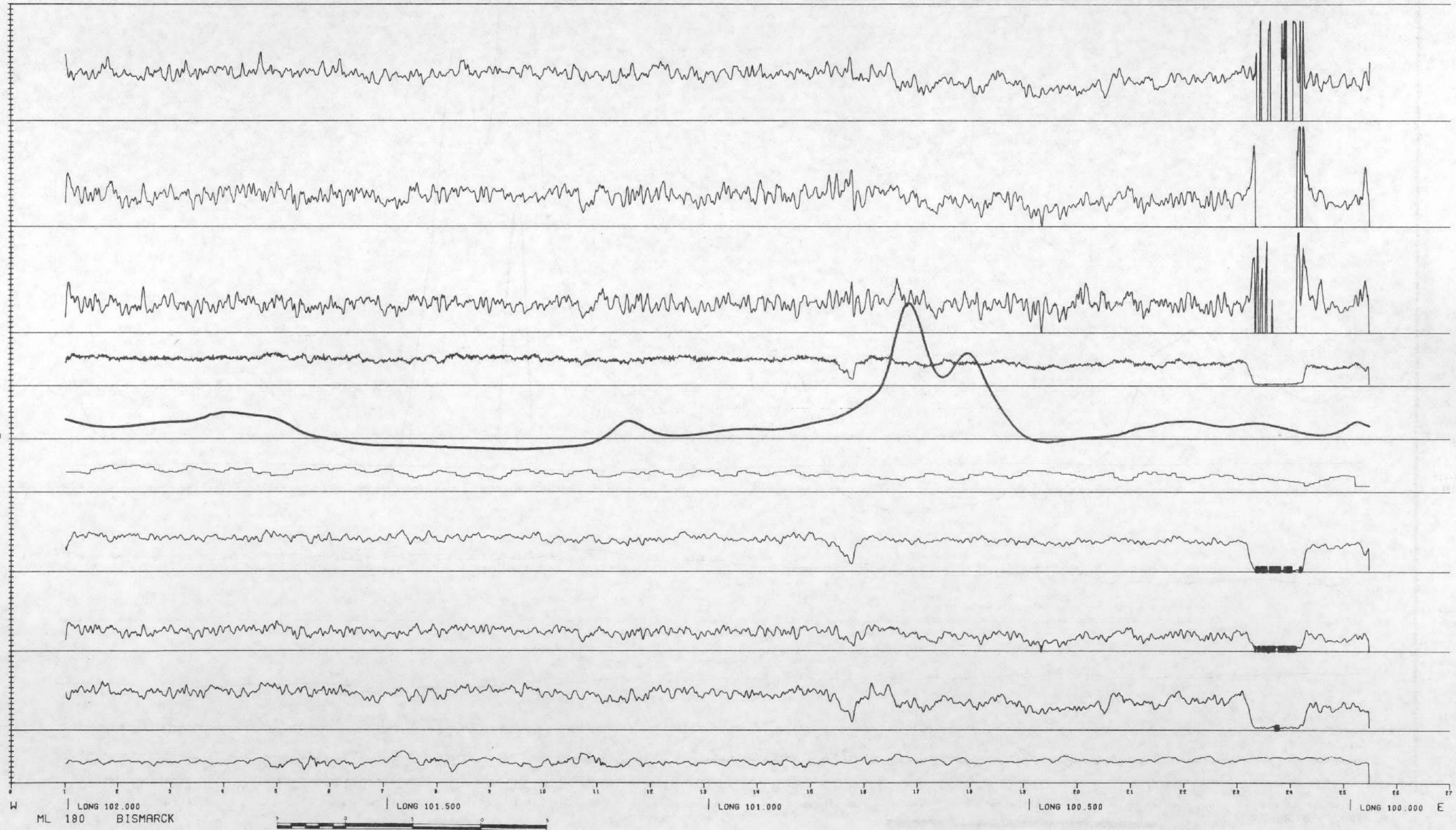
BIAIR  
5.0 C/S/DIV

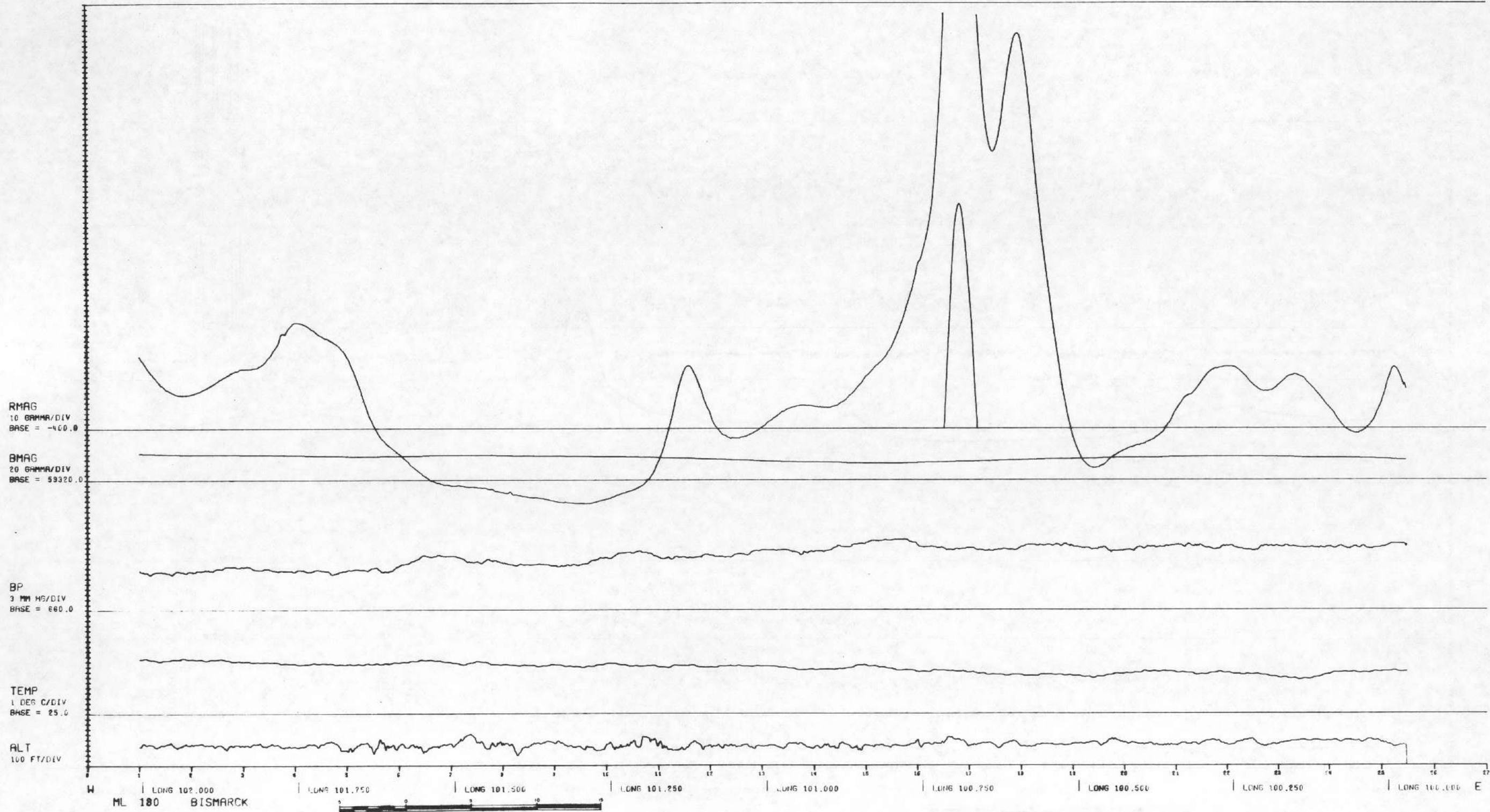
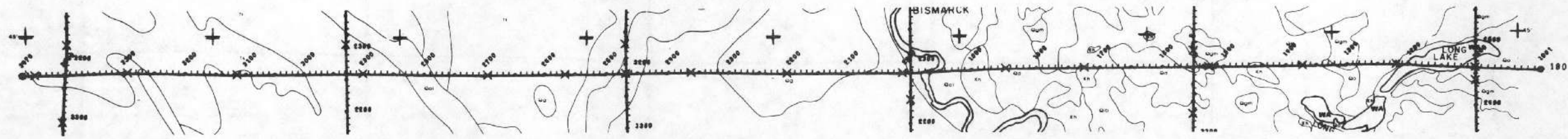
K  
.25 PC/DIV

EU  
.50 PPM/DIV

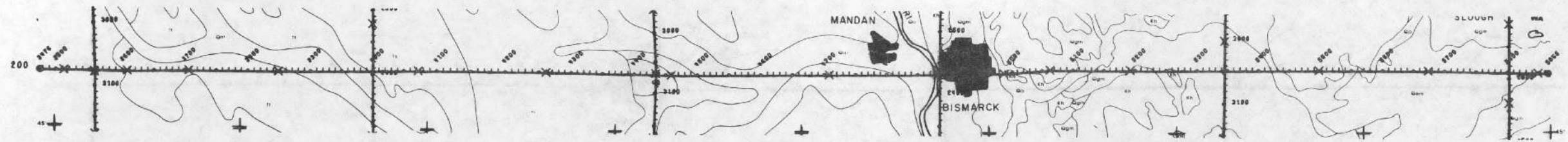
ETH  
1.0 PPM/DIV

ALT  
100 FT/DIV









ETH/K  
50 / DIV

EU/K  
20 / DIV

EU/ETH  
.05 / DIV

GC  
400 C/S/DIV

RMAG  
50 GAMMAS/DIV  
BASE = -450.0

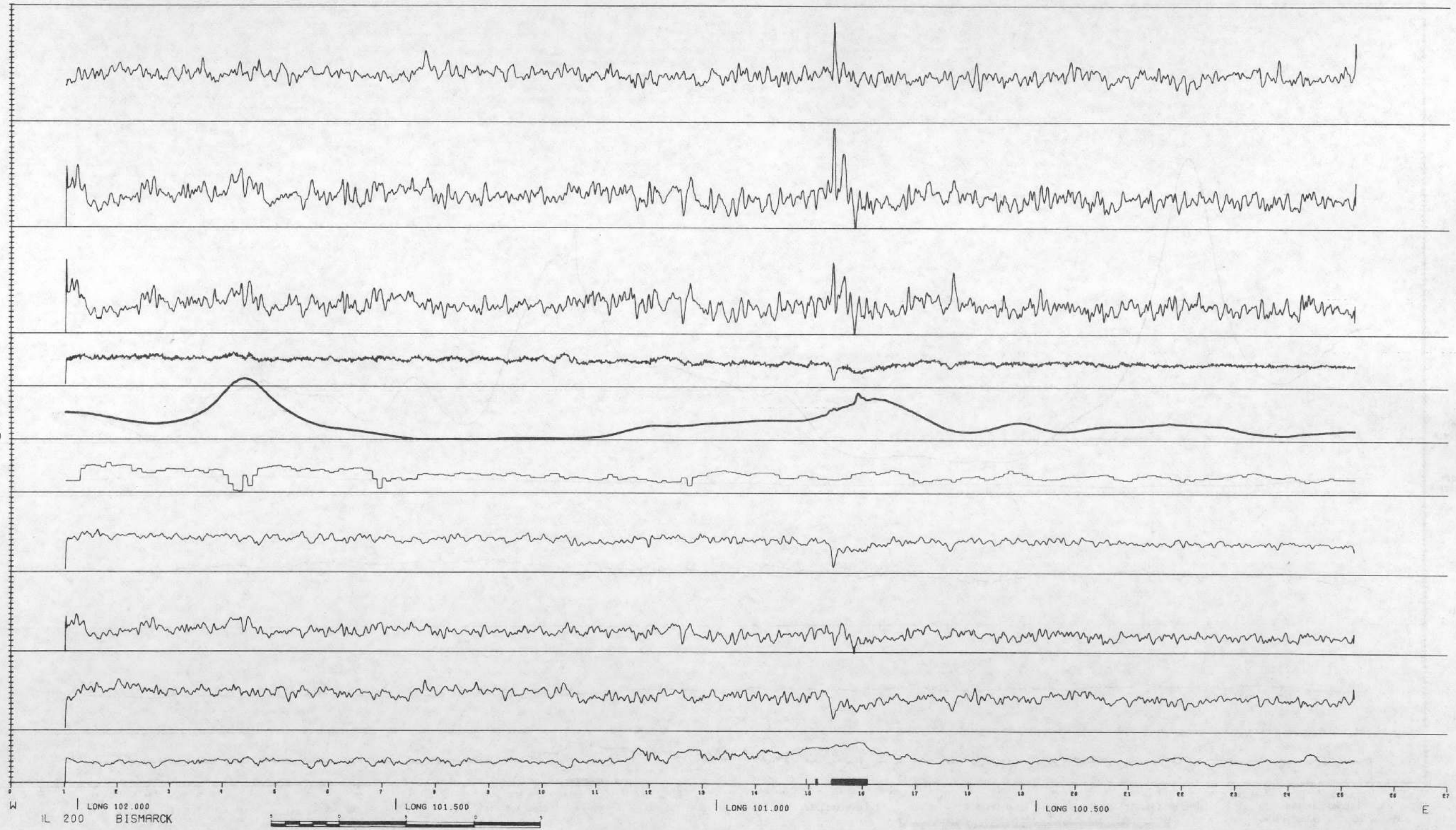
BIAIR  
5.0 C/S/DIV

K  
.25 PC/DIV

EU  
.50 PPM/DIV

ETH  
1.0 PPM/DIV

HIT  
100 FT/DIV



W | LONG 102.000  
IL 200 BISMARCK

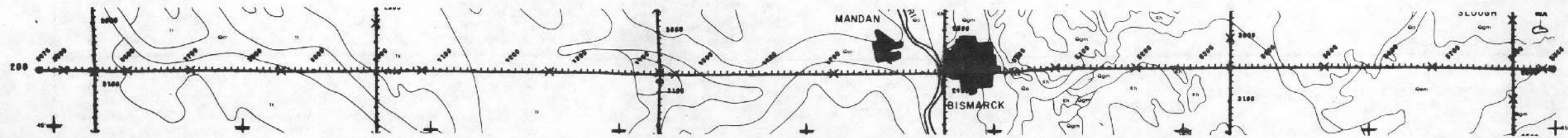


LONG 101.500

LONG 101.000

LONG 100.500

E



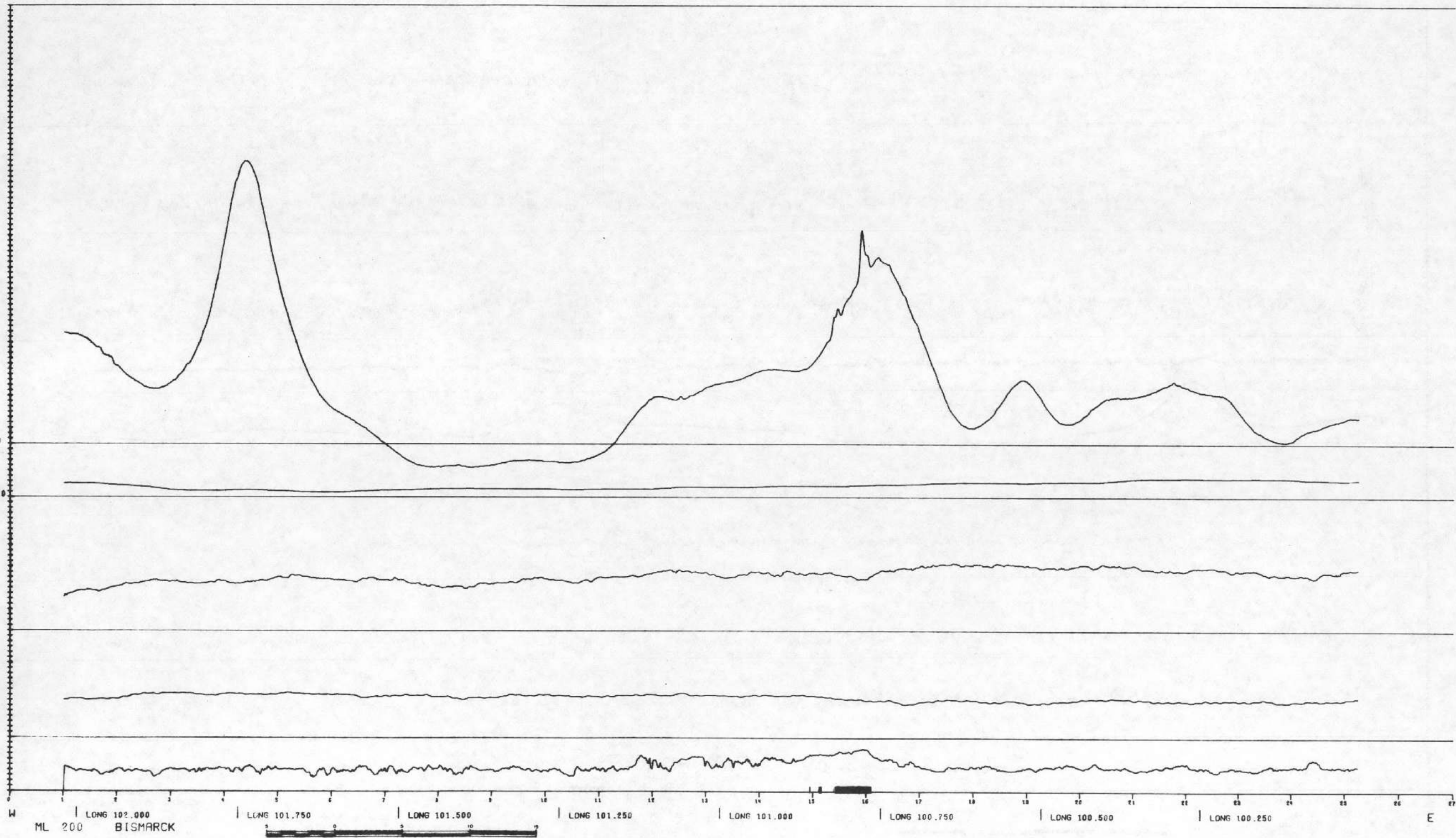
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
20 GAMMA/DIV  
BASE = 59320.0

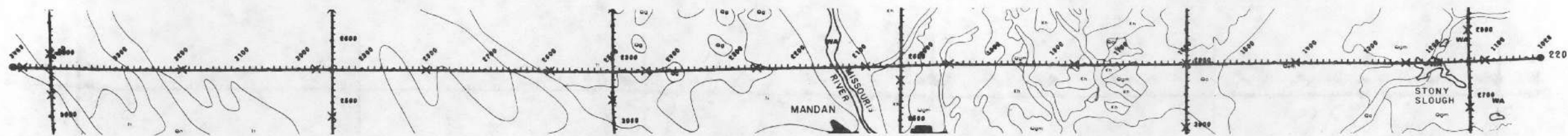
BP  
3 MM HG/DIV  
BASE = 660.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

ALT  
10 FT/DIV







ETH/K  
50 /DIV



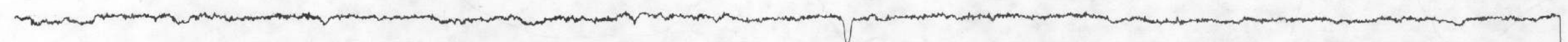
EU/K  
20 /DIV



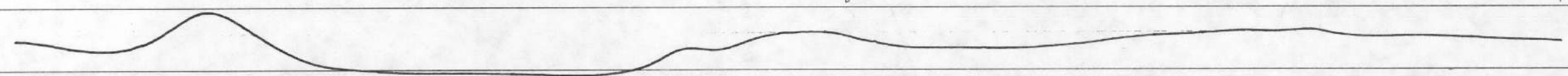
EU/ETH  
.05 /DIV



GC  
400 C/S/DIV



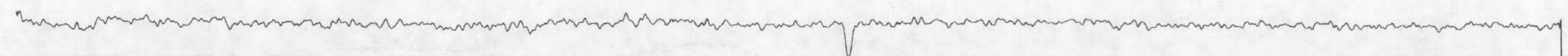
RMAG  
50 GAMMAS/DIV  
BASE = -450.0



BIAIR  
5.0 C/S/DIV



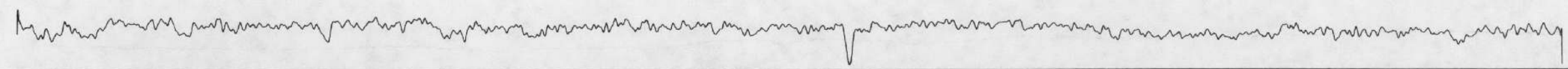
K  
.25 FC/DIV



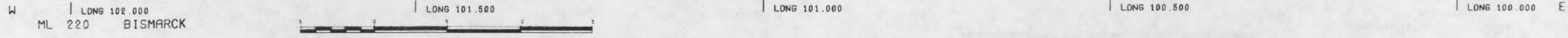
EU  
50 PPM/DIV



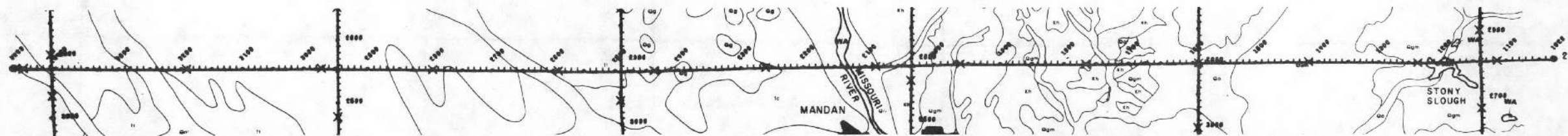
ETH  
1.0 PPM/DIV



ALT  
100 FT/DIV



ML 220 BISMARCK



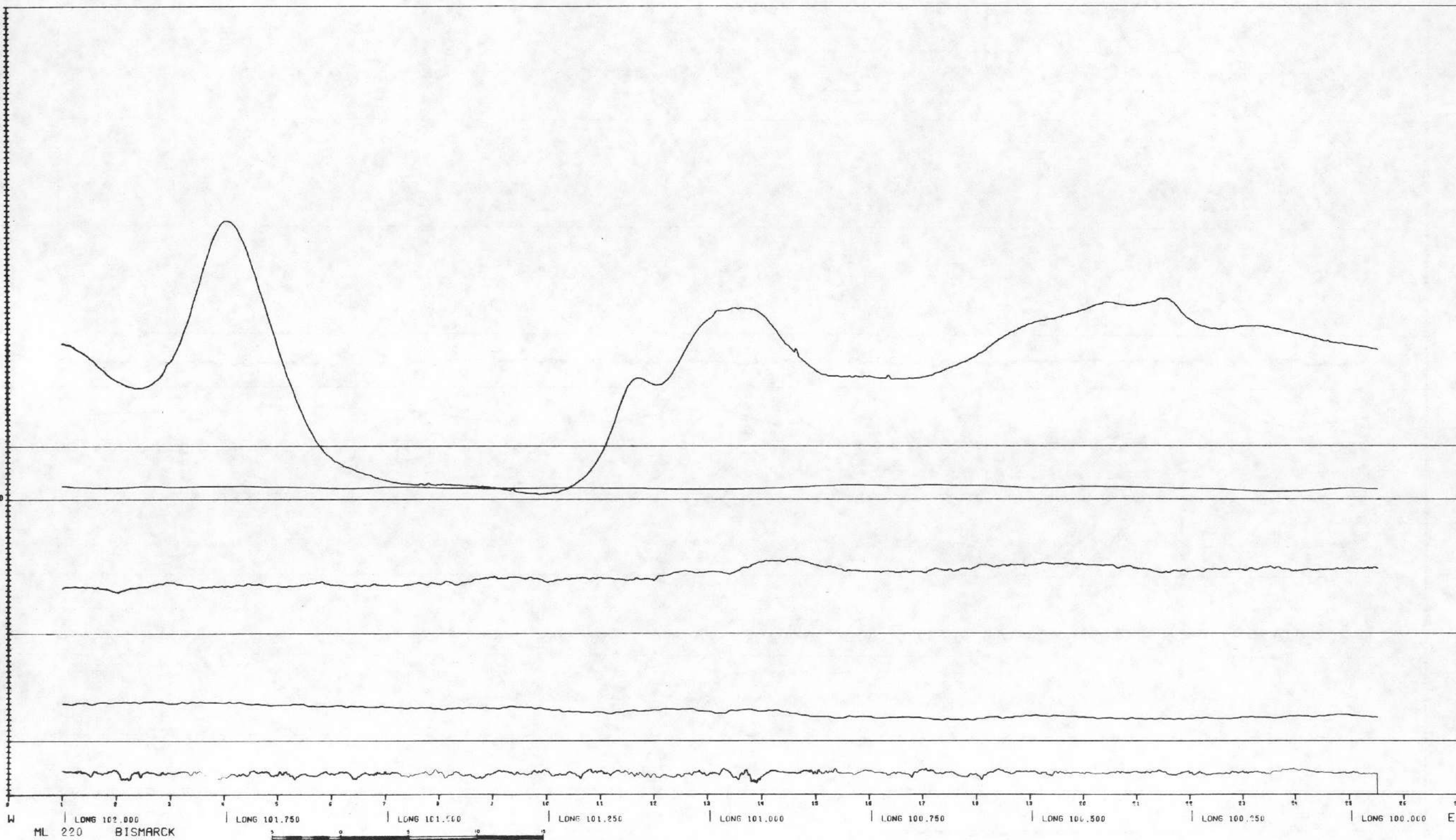
RMG  
10 GAMMA/DIV  
BASE = -400.0

BMG  
20 GAMMA/DIV  
BASE = 59320.0

BP  
3 MM HG/DIV  
BASE = 660.0

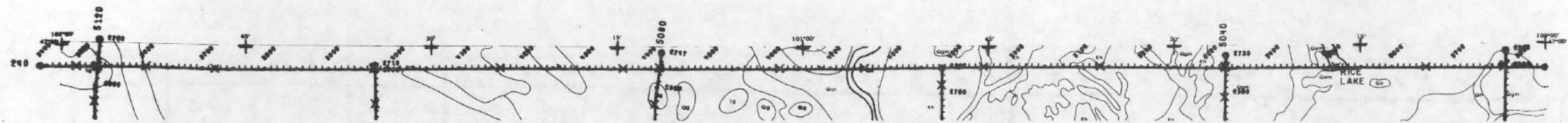
TEMP  
1 DEG C/DIV  
BASE = 25.0

ALT  
100 FT/DIV

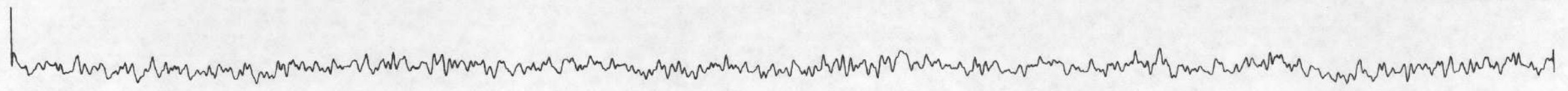


ML 220 BISMARCK

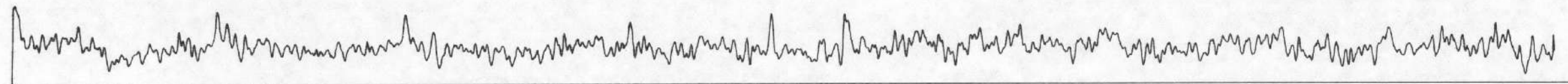




ETH/K  
50 /DIV



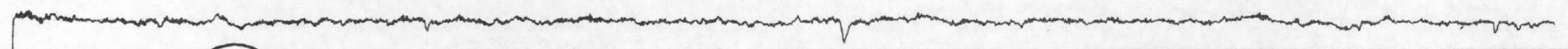
EU/K  
.20 /DIV



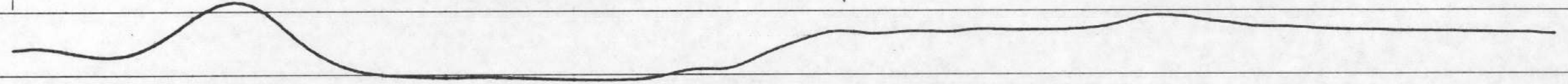
EU/ETH  
.05 /DIV



GC  
400 C/S/DIV



RMAG  
50 GAMMAS/DIV  
BASE = -450.0



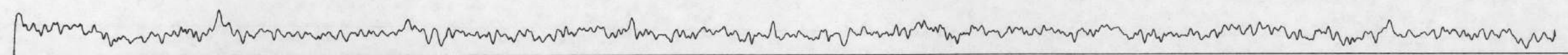
BIAIR  
5.0 C/S/DIV



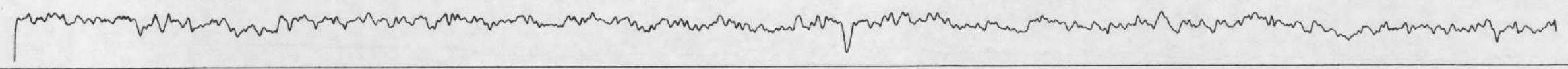
K  
.25 PC/DIV



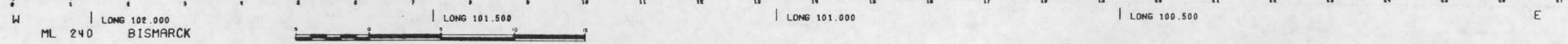
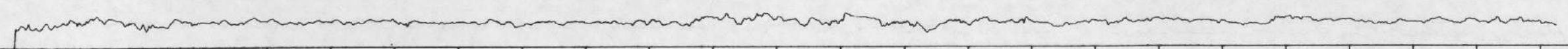
EU  
.50 PPM/DIV



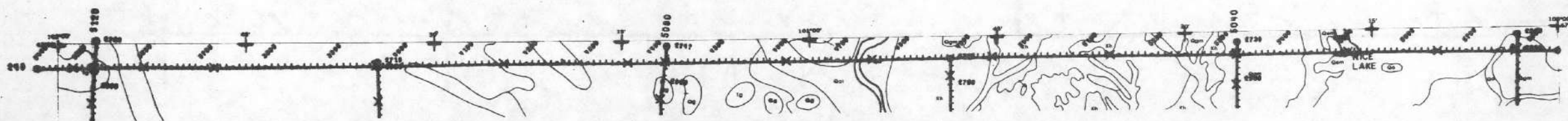
ETH  
1.0 PPM/DIV



ALT  
100 FT/DIV



ML 240 BISMARCK



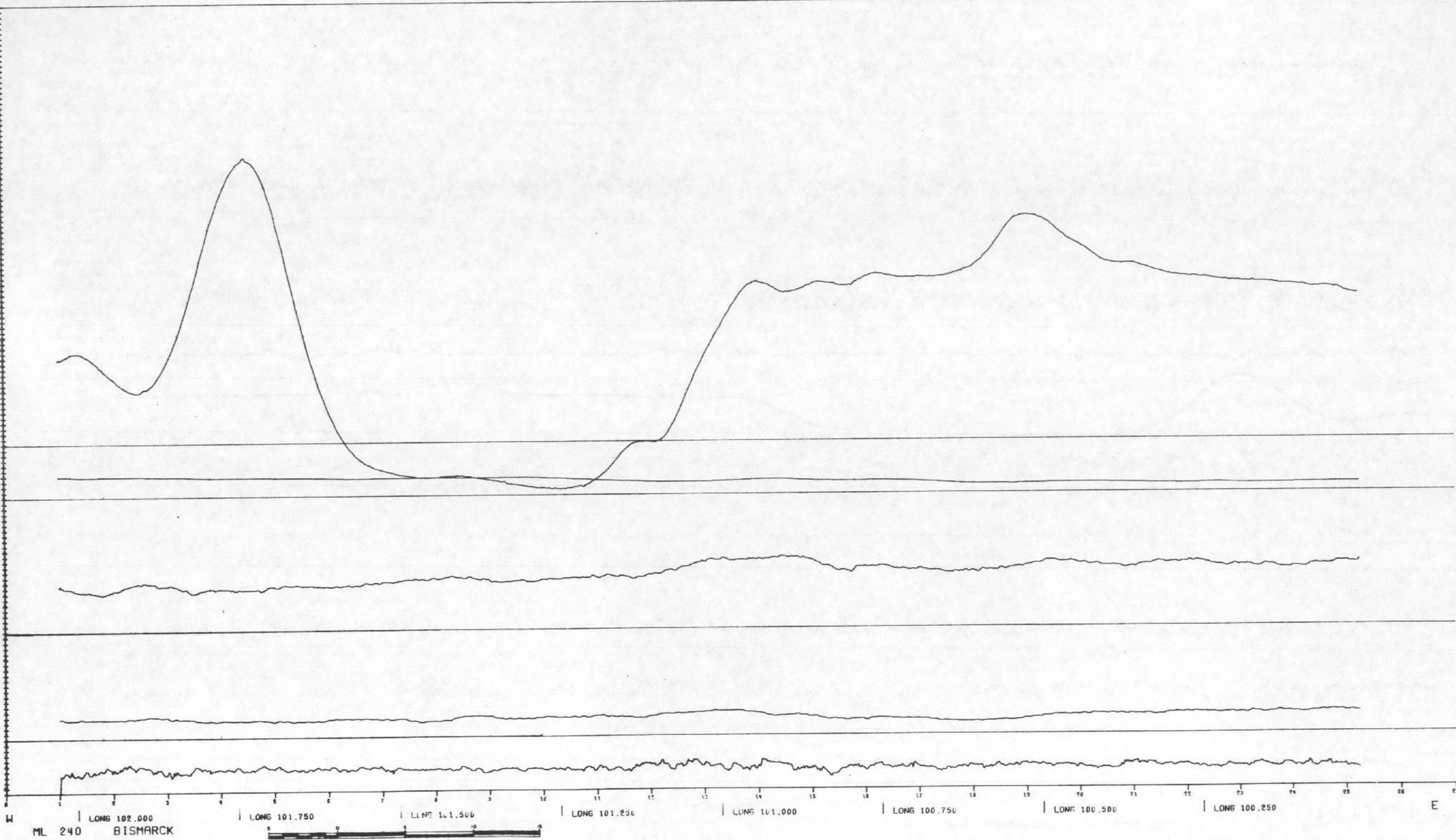
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
20 GAMMA/DIV  
BASE = 53220.0

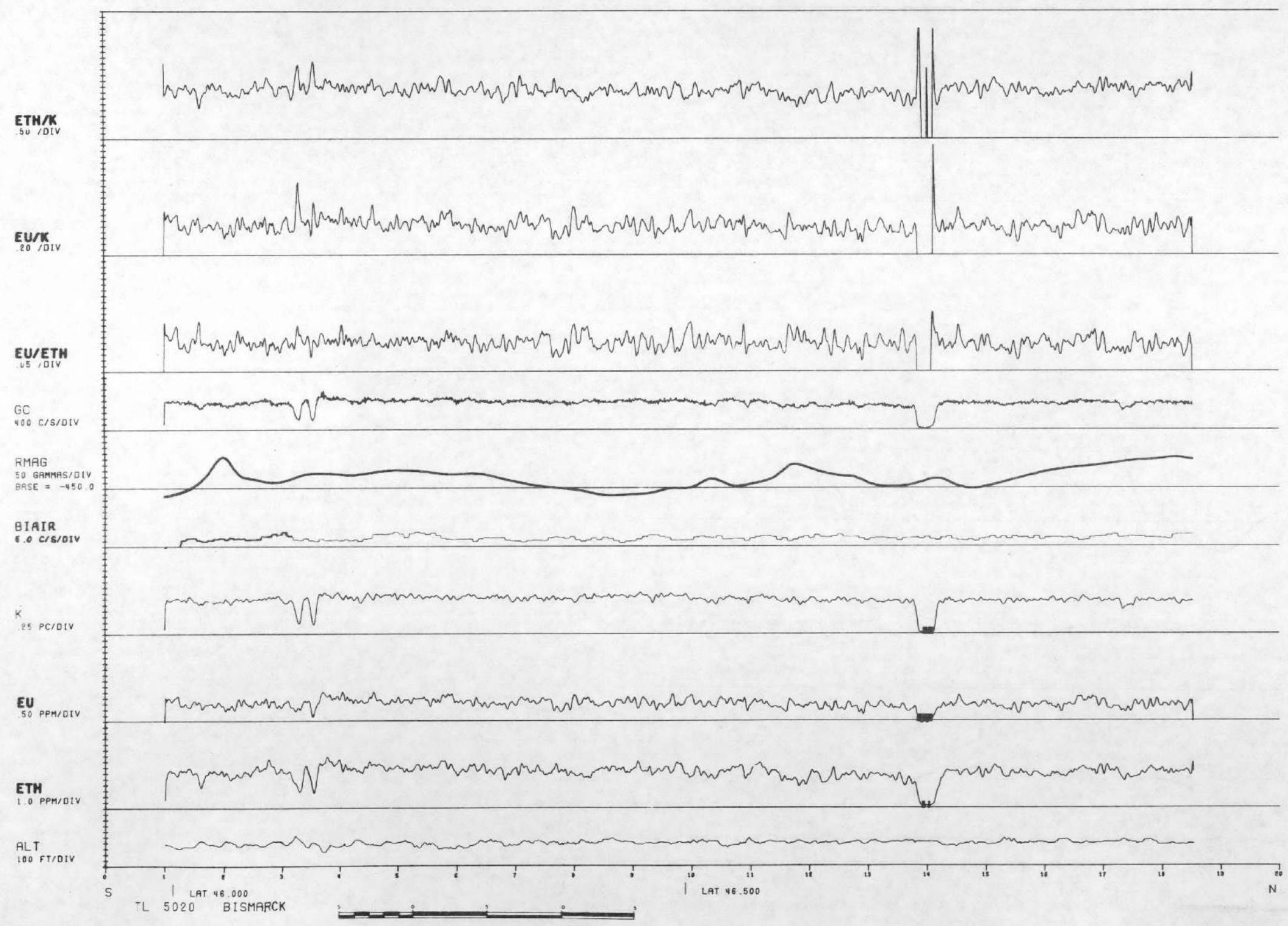
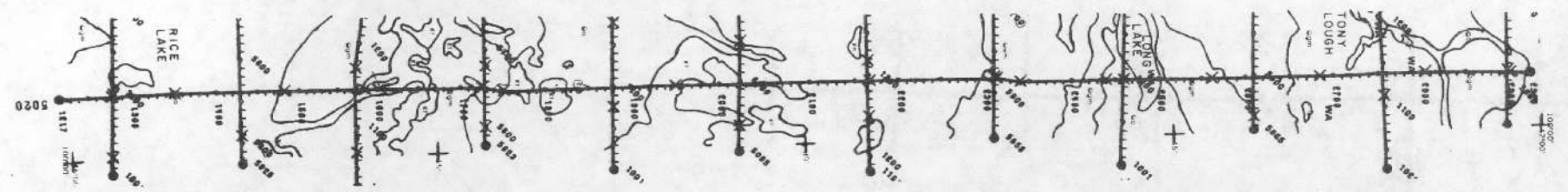
BP  
3 MM HG/DIV  
BASE = 600.0

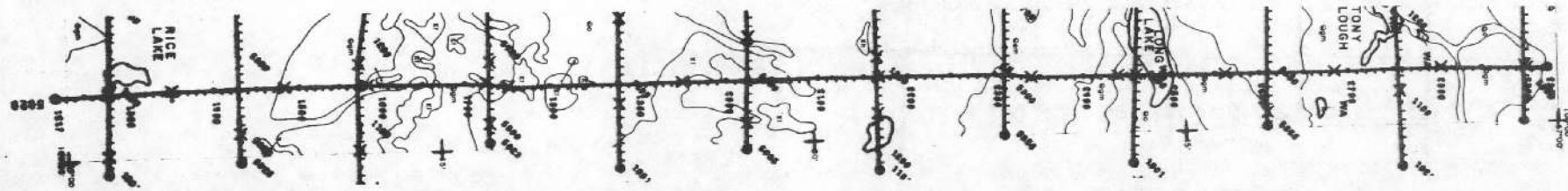
TEMP  
1 DEG C/DIV  
BASE = 25.0

ALT  
100 FT/DIV









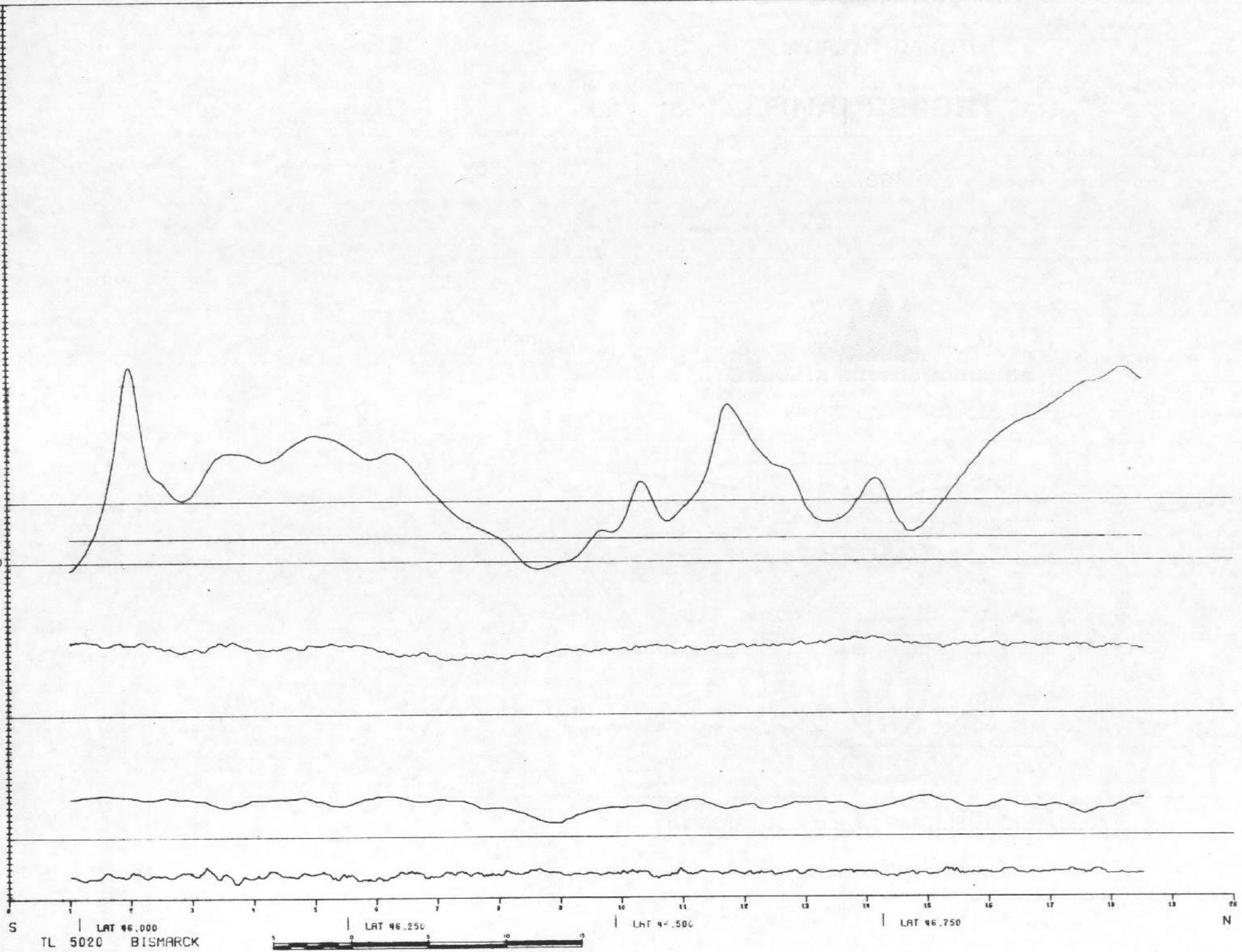
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
20 GAMMA/DIV  
BASE = 53320.0

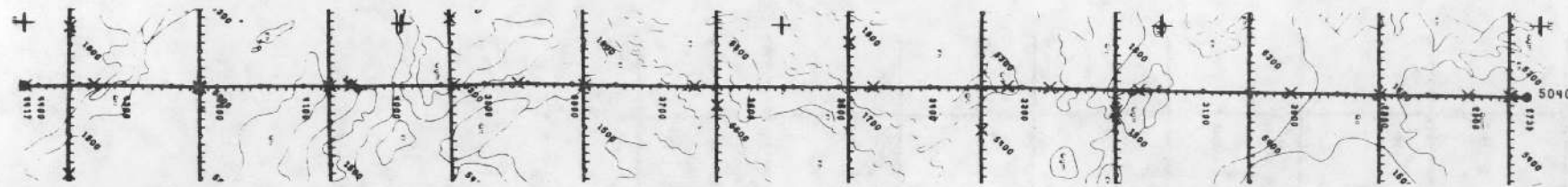
BP  
3 MM HG/DIV  
BASE = 660.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

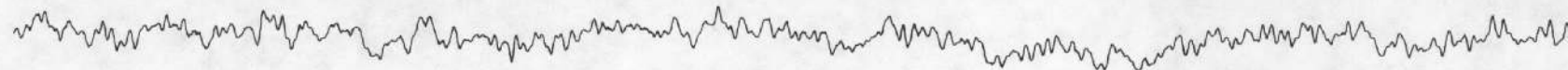
ALT  
100 FT/DIV







ETH/K  
.50 /DIV



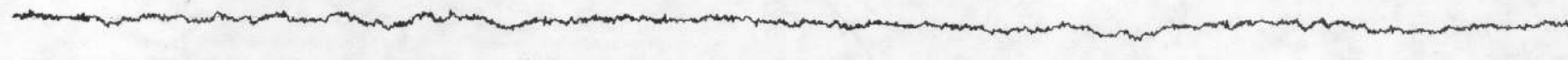
EU/K  
.20 /DIV



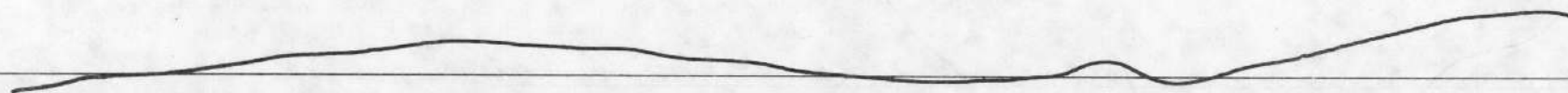
EU/ETH  
.05 /DIV



GC  
400 C/S/DIV



RMAG  
50 GAMMAS/DIV  
BASE = -450.0



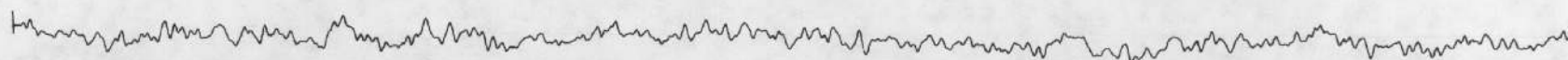
BIAIR  
5.0 C/S/DIV



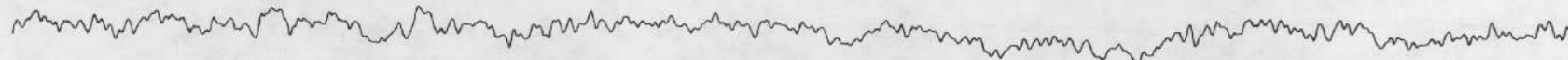
K  
.25 PC/DIV



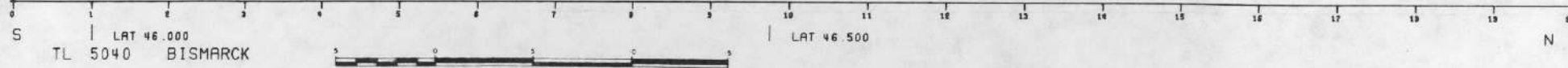
EU  
.50 PPM/DIV



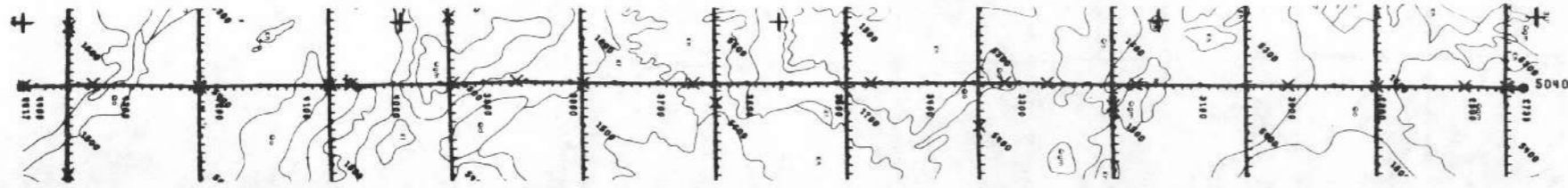
ETH  
1.0 PPM/DIV



ALT  
100 FT/DIV



TL 5040 BISMARCK



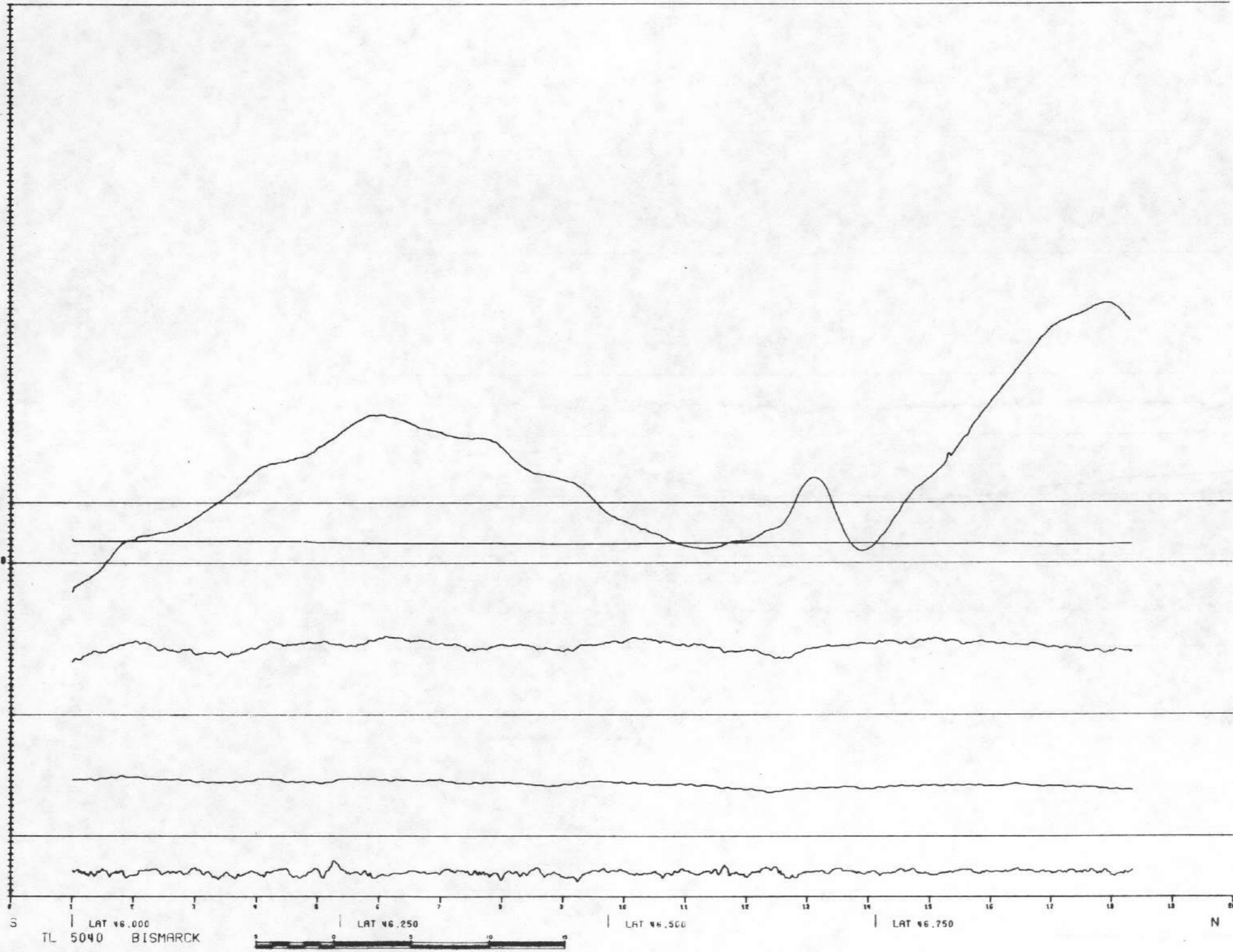
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
20 GAMMA/DIV  
BASE = 59320.0

BP  
3 MM HG/DIV  
BASE = 660.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

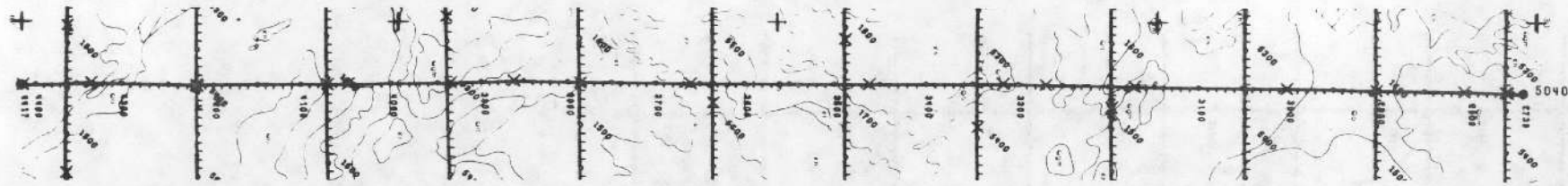
ALT  
100 FT/DIV



S | LAT 46.000 | LAT 46.250 | LAT 46.500 | LAT 46.750 | N  
TL 5040 BISMARCK







ETH/K  
50 /DIV

EU/K  
20 /DIV

EU/ETH  
.05 /DIV

GC  
400 C/S/DIV

RMAG  
50 GAMMAS/DIV  
BASE = -450.0

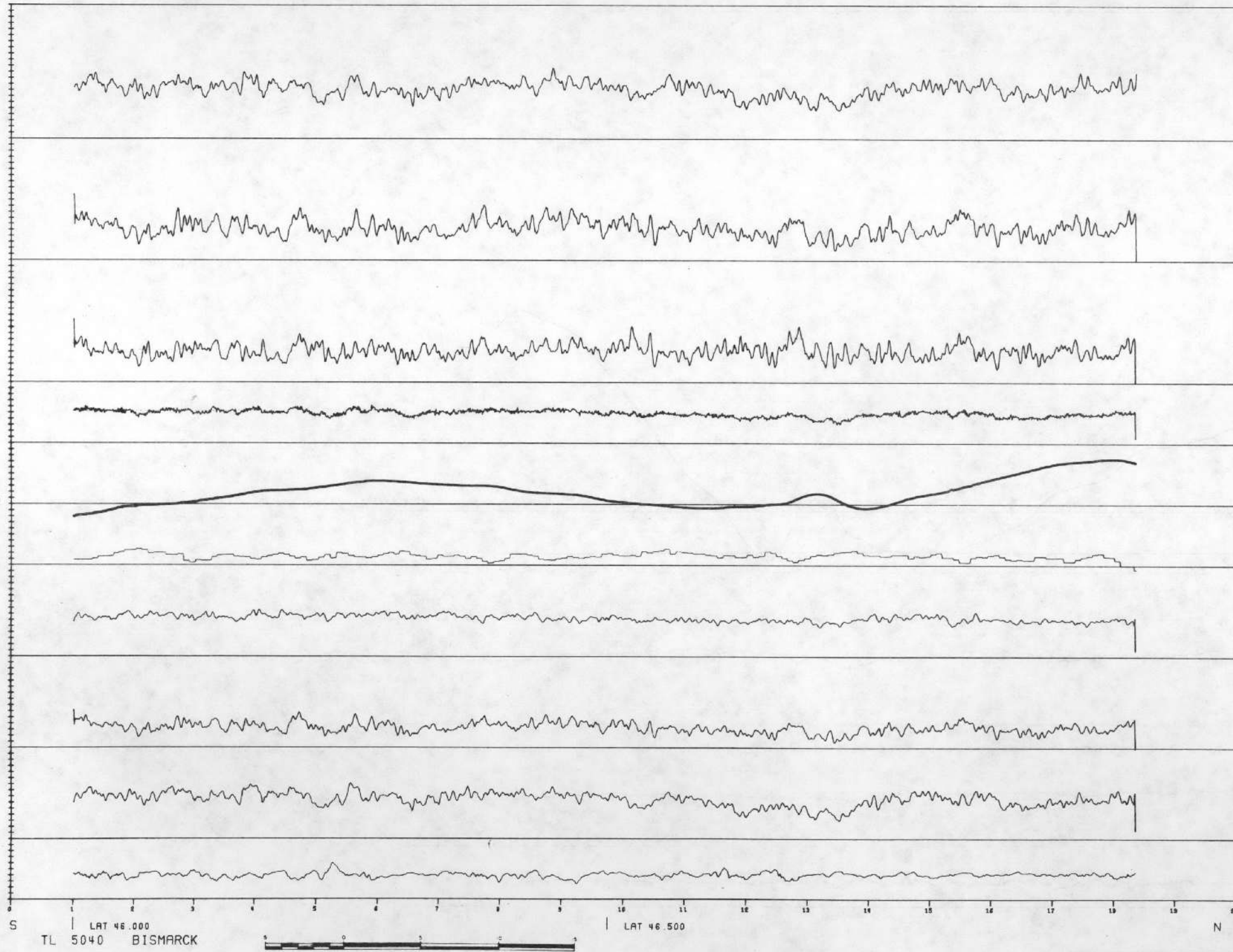
BIRIR  
5.0 C/S/DIV

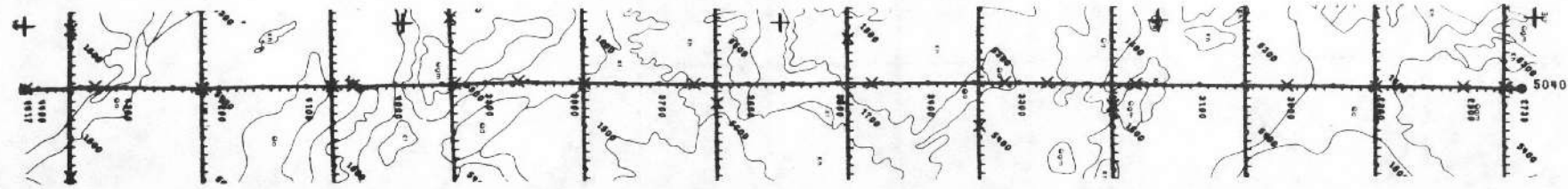
K  
.25 PC/DIV

EU  
.50 PPM/DIV

ETH  
1.0 PPM/DIV

ALT  
100 FT/DIV





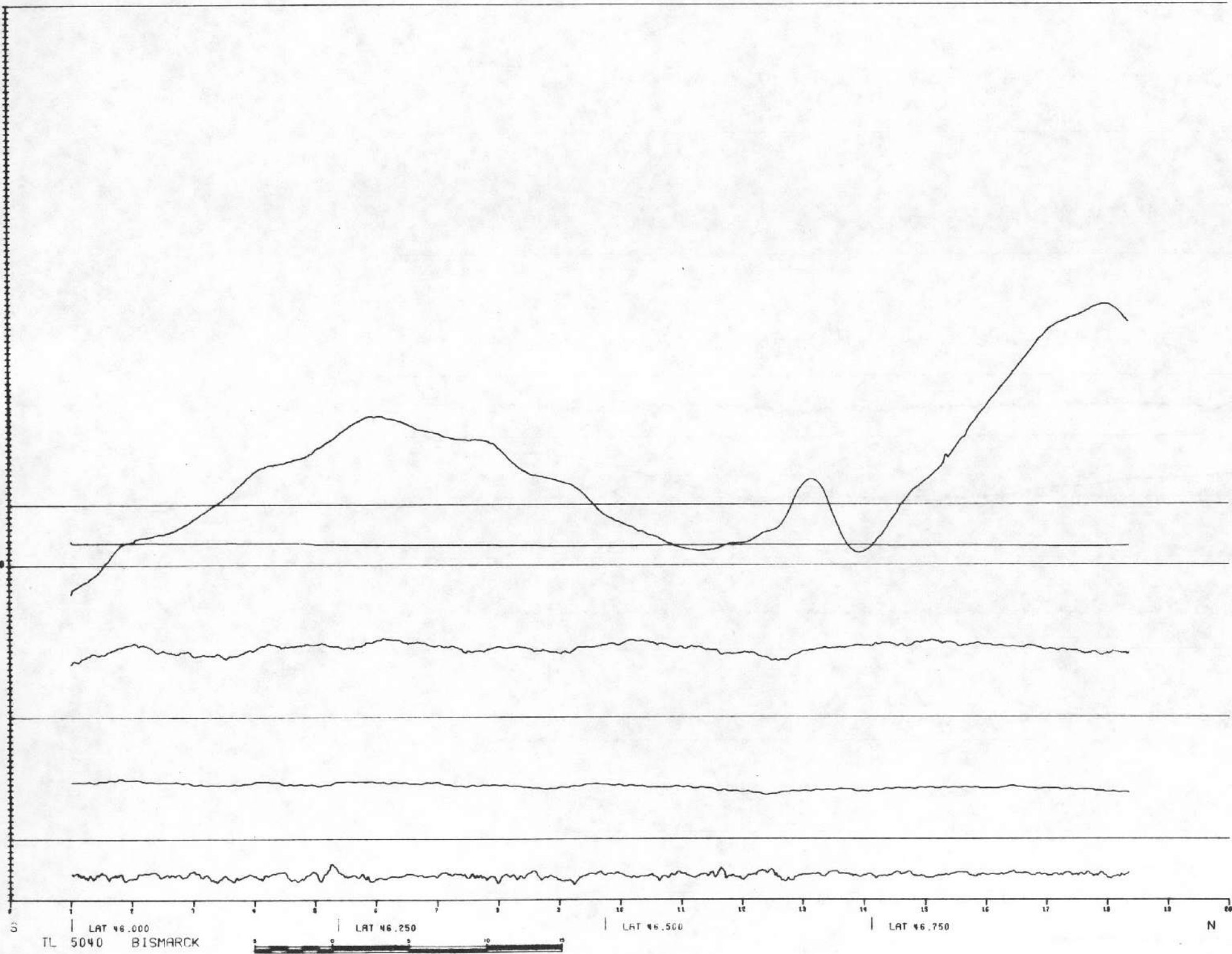
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
20 GAMMA/DIV  
BASE = 59320.0

BP  
3 MM HG/DIV  
BASE = 660.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

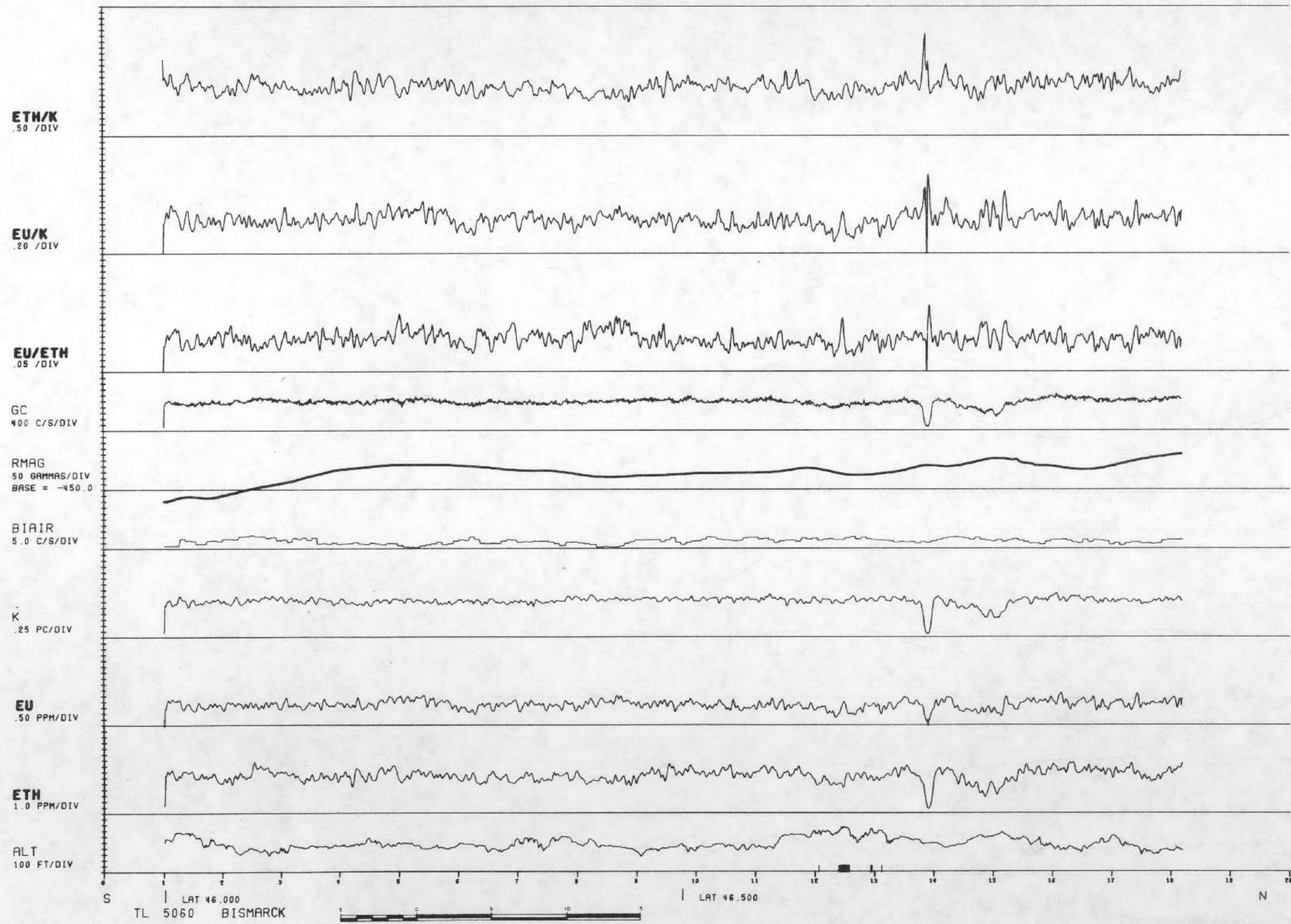
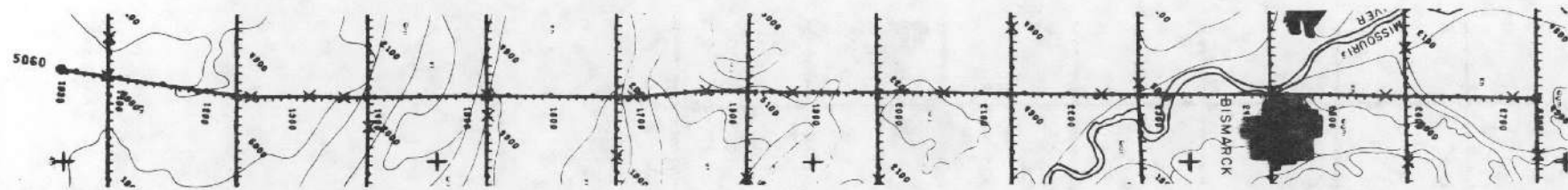
ALT  
100 FT/DIV

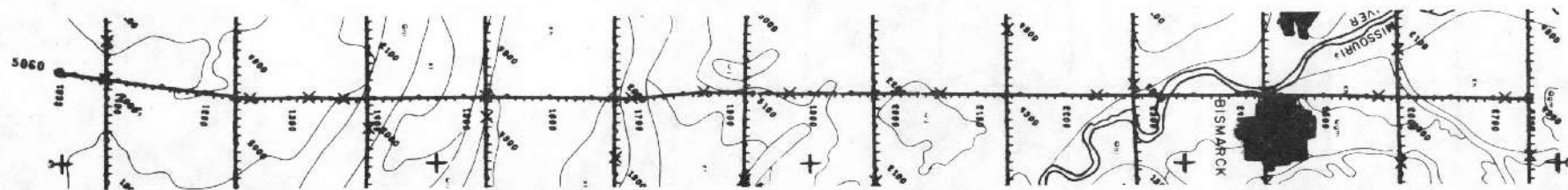


TL 5040 BISMARCK









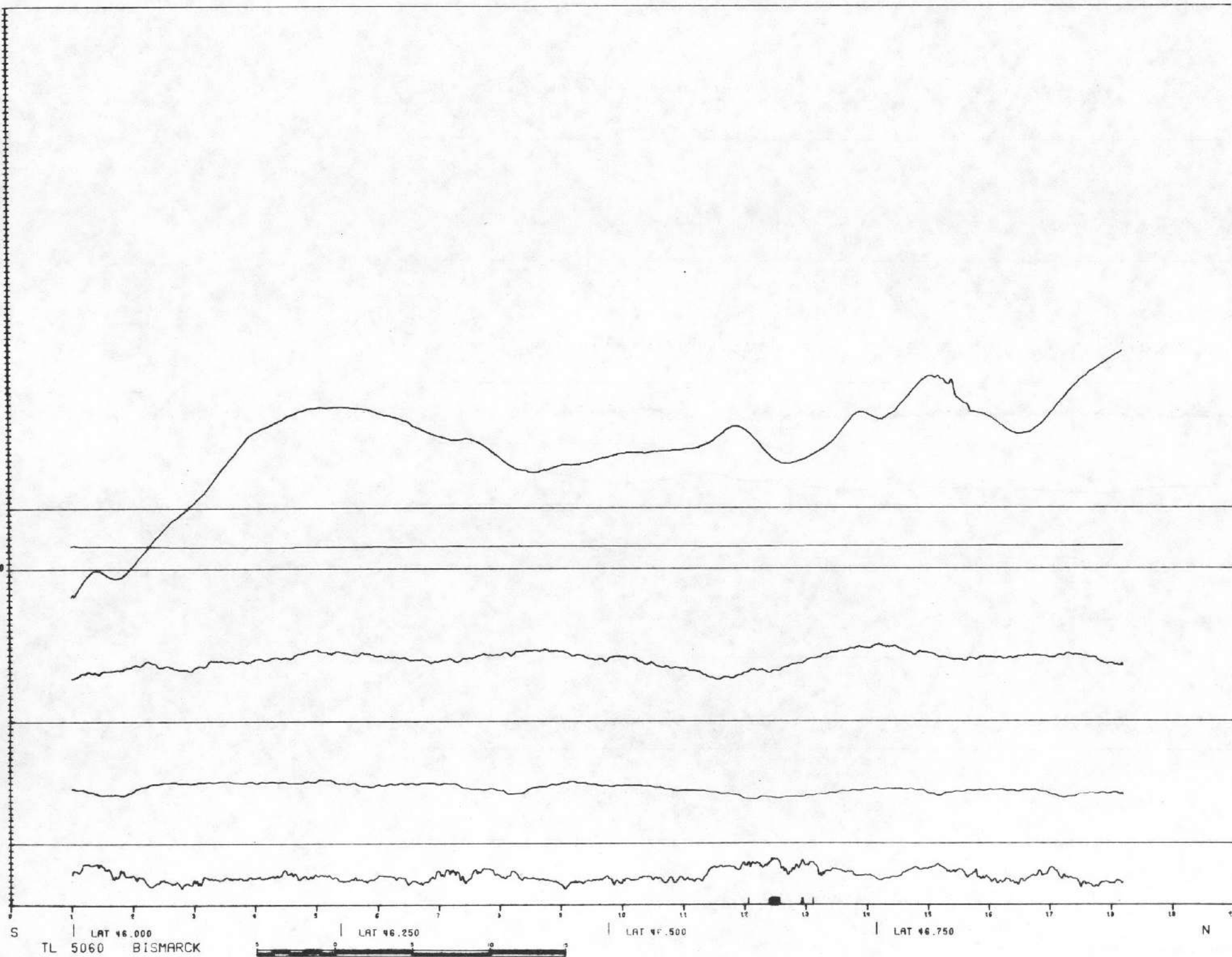
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
20 GAMMA/DIV  
BASE = 59320.0

BP  
3 MM HG/DIV  
BASE = 660.0

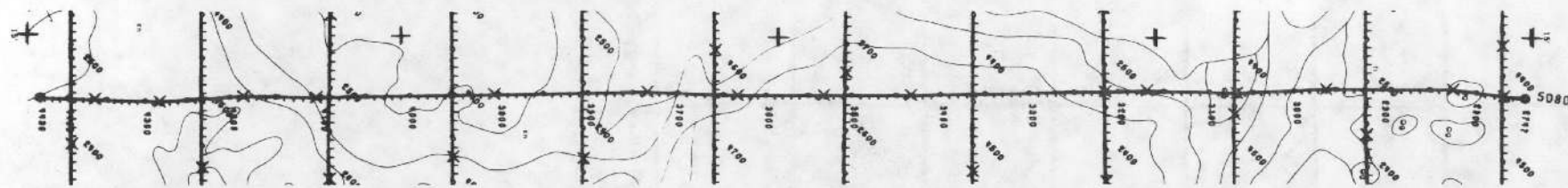
TEMP  
1 DEG C/DIV  
BASE = 25.0

ALT  
100 FT/DIV



TL 5060 BISMARCK

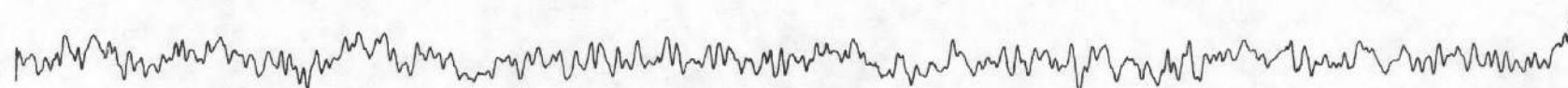




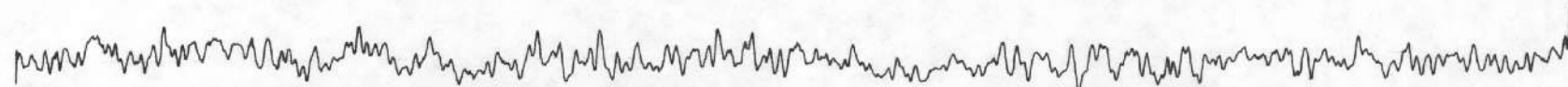
ETH/K  
.50 /DIV



EU/K  
.20 /DIV



EU/ETH  
.05 /DIV



GC  
400 C/S/DIV



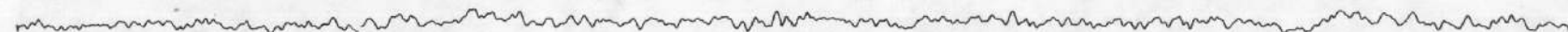
RMAG  
50 GAMMAS/DIV  
BASE = -450.0



BIAIR  
5.0 C/S/DIV



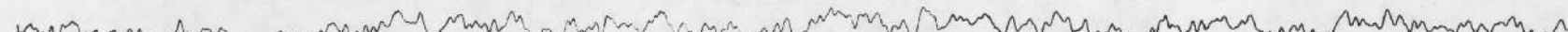
K  
.25 PC/DIV



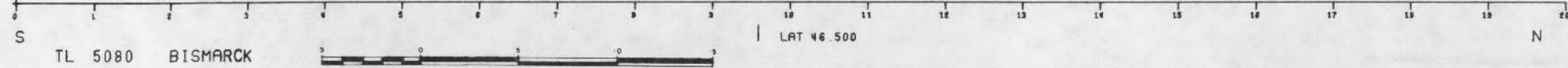
EU  
.50 PPM/DIV

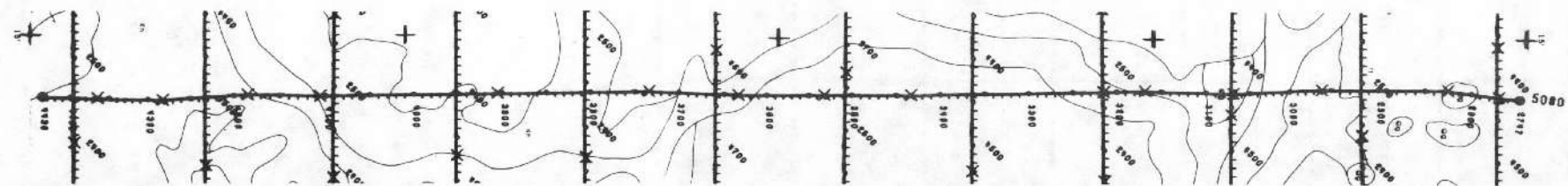


ETH  
1.0 PPM/DIV



ALT  
100 FT/DIV





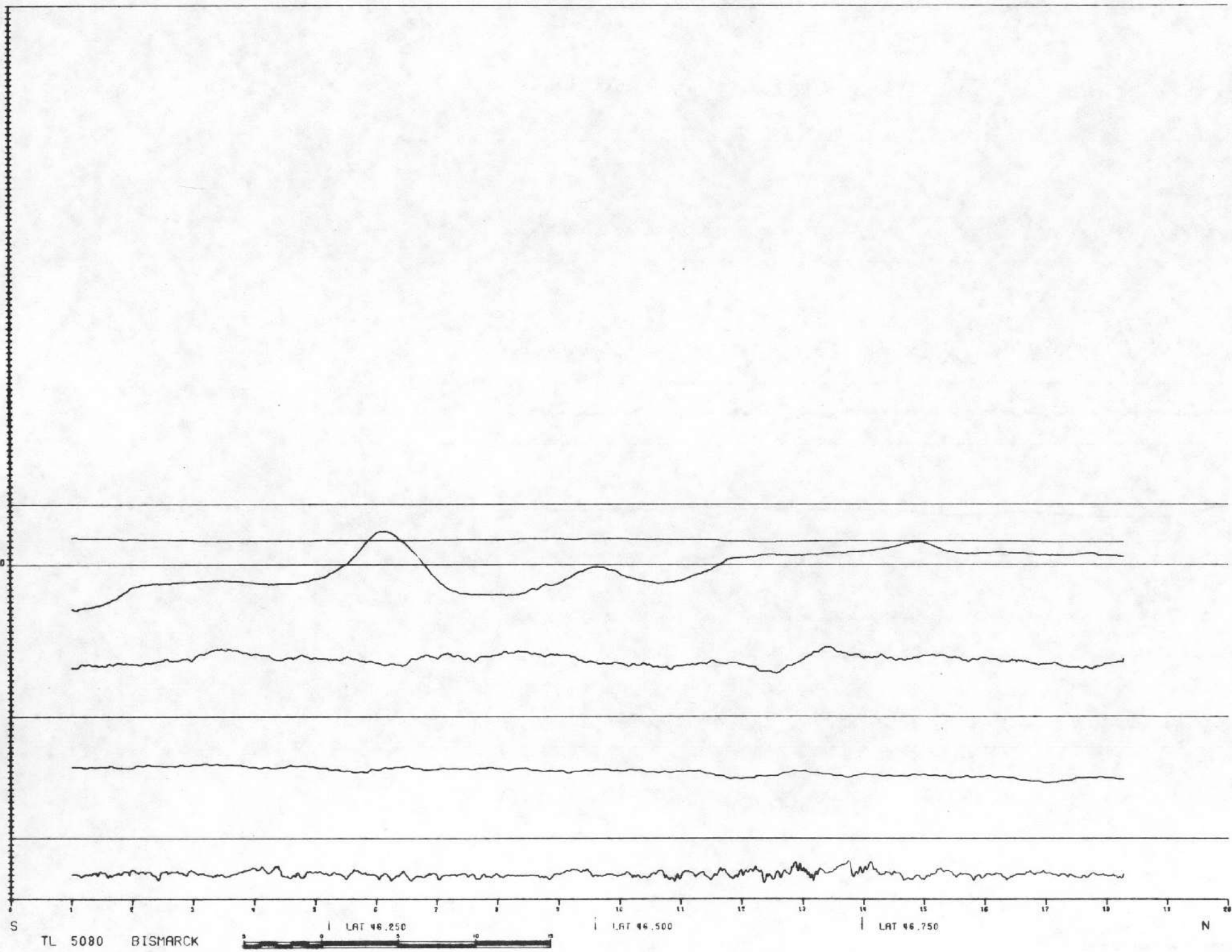
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
20 GAMMA/DIV  
BASE = 59320.0

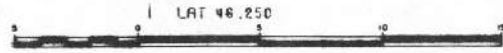
BP  
3 MM HG/DIV  
BASE = 660.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

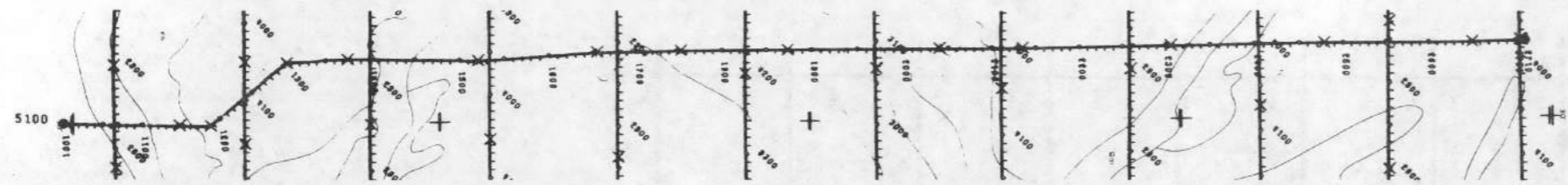
ALT  
100 FT/DIV



TL 5080 BISMARCK







ETH/K  
.50 /DIV

EU/K  
.20 /DIV

EU/ETH  
.05 /DIV

GC  
400 C/S/DIV

RMAG  
50 GAMMAS/DIV  
BASE = -450.0

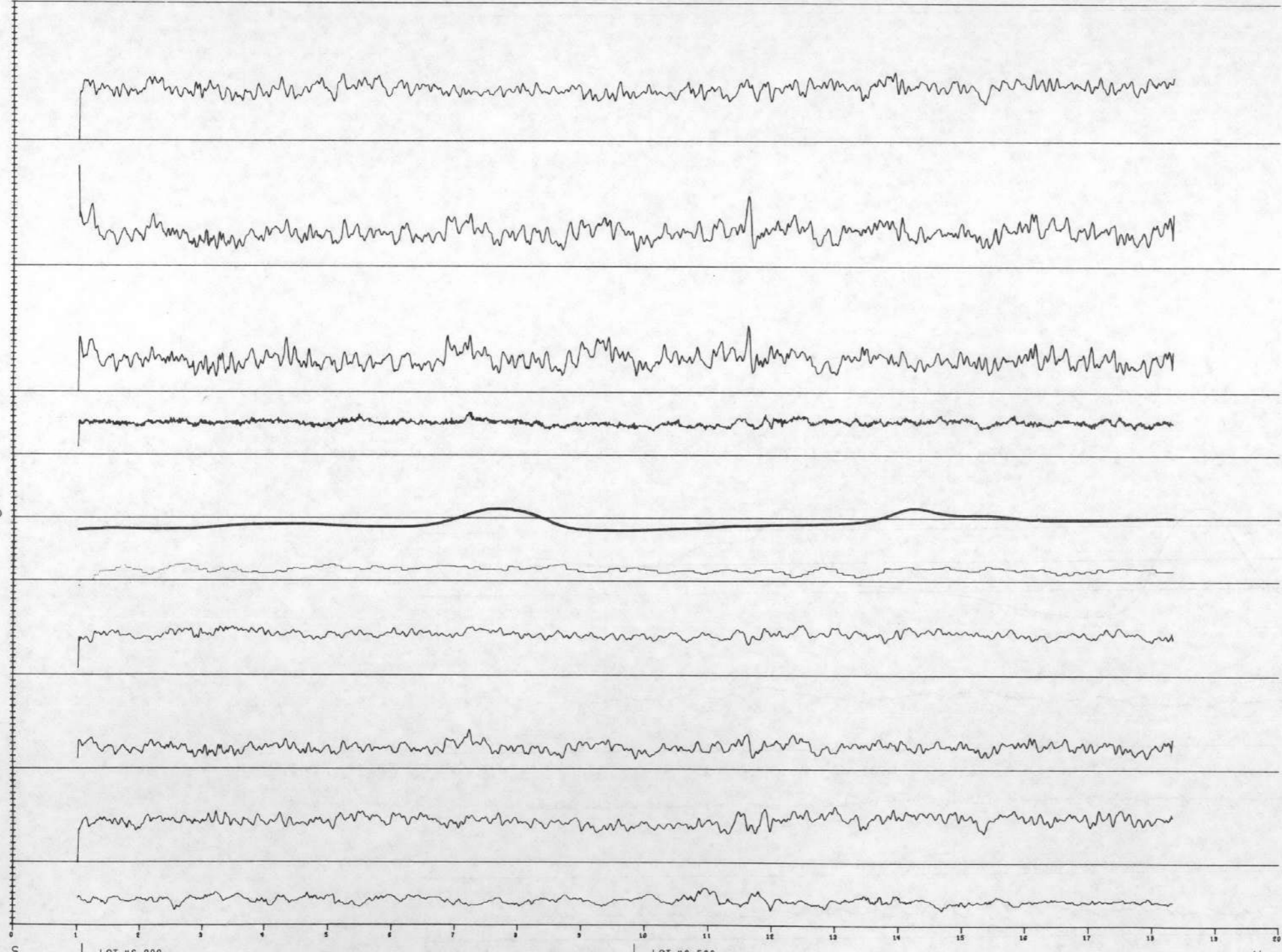
PAIR  
5.0 C/S/DIV

K  
.25 PC/DIV

EU  
.50 PPM/DIV

ETH  
1.0 PPM/DIV

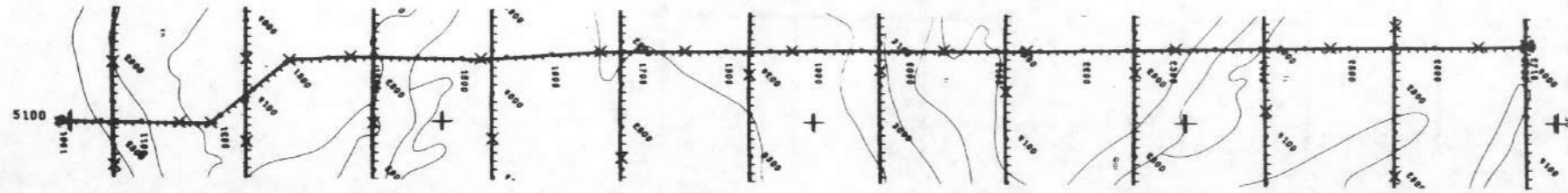
FLT  
100 FT/DIV



S | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | N

TL 5100 BISMARCK | LAT 46.000 | LAT 46.500





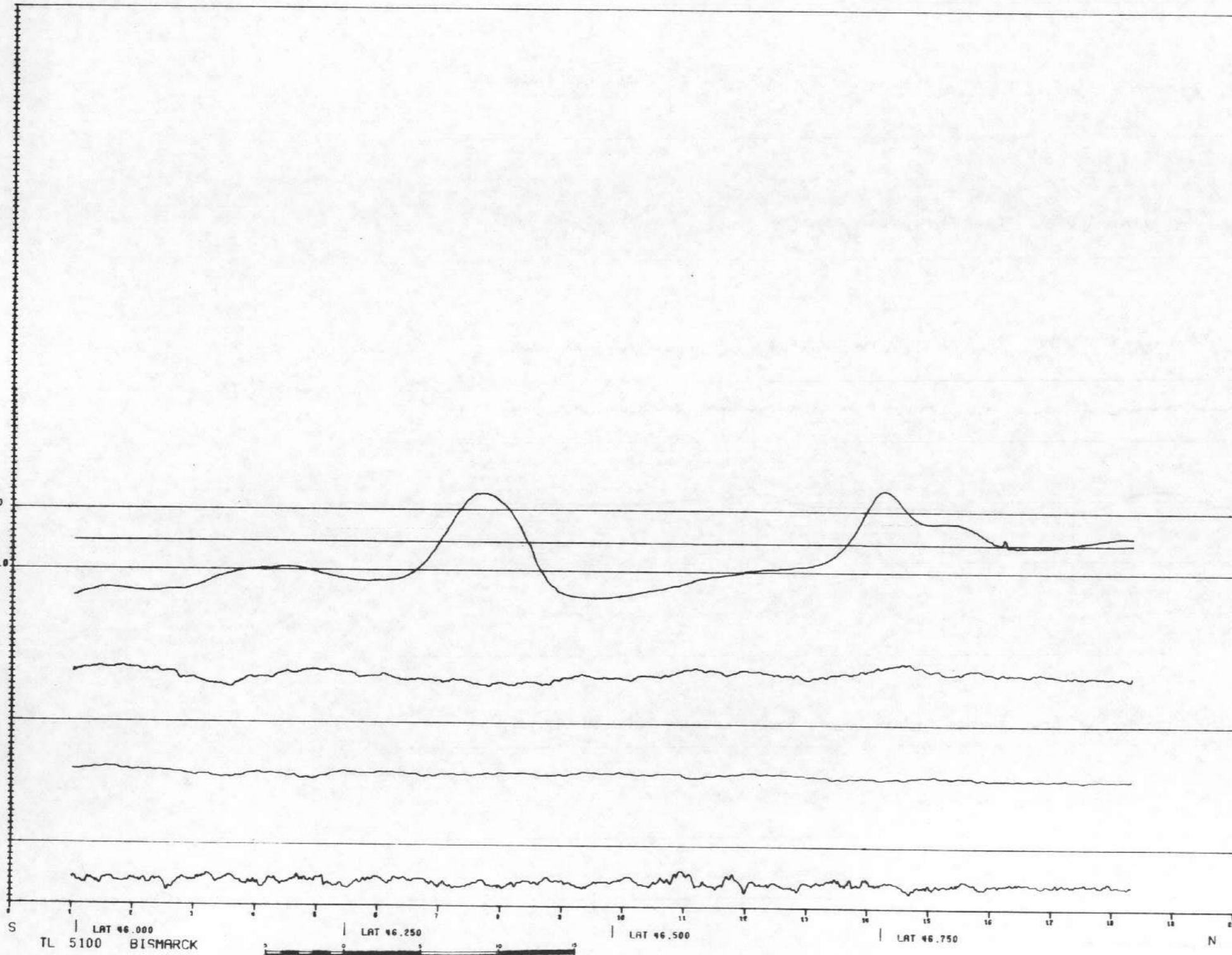
RMAG  
10 GAMMA/DIV  
BASE = -400.0

BMAG  
20 GAMMA/DIV  
BASE = 59320.0

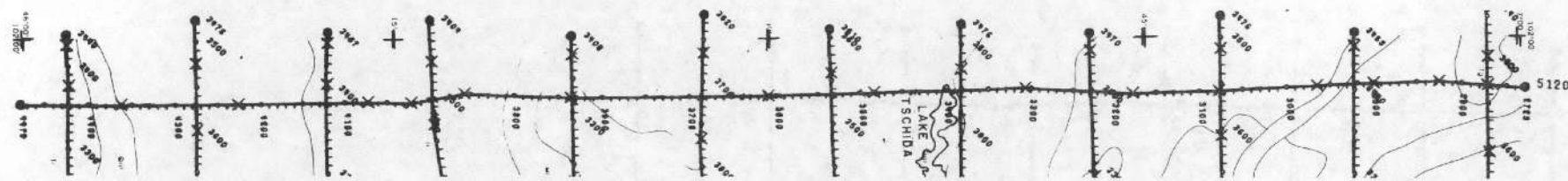
BP  
3 MM HG/DIV  
BASE = 660.0

TEMP  
1 DEG C/DIV  
BASE = 25.0

ALT  
100 FT/DIV







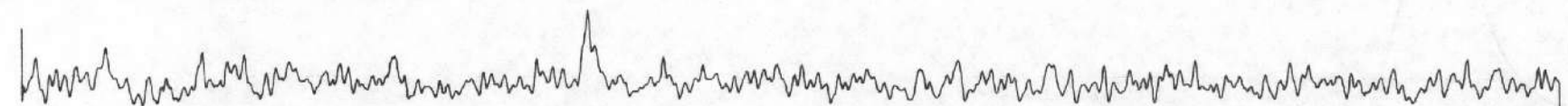
ETH/K  
.50 /DIV



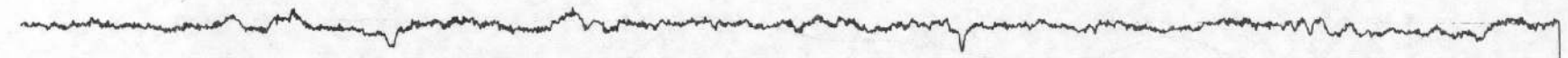
EU/K  
.20 /DIV



EWETH  
.05 /DIV



GC  
400 C/S/DIV



RMAG  
50 GAMMAS/DIV  
BASE = -450.0



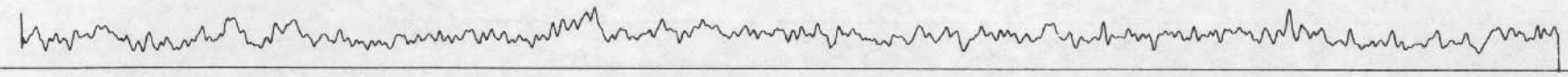
B: AIR  
5.0 C/S/DIV



K  
.25 PC/DIV



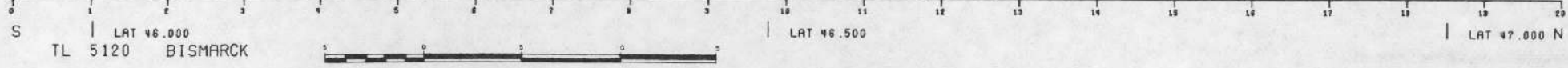
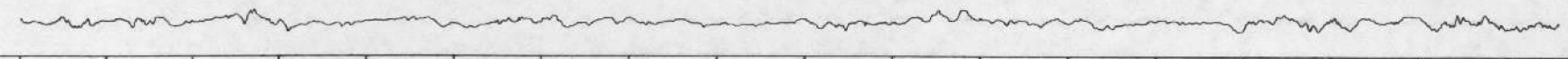
EU  
.50 PPM/DIV

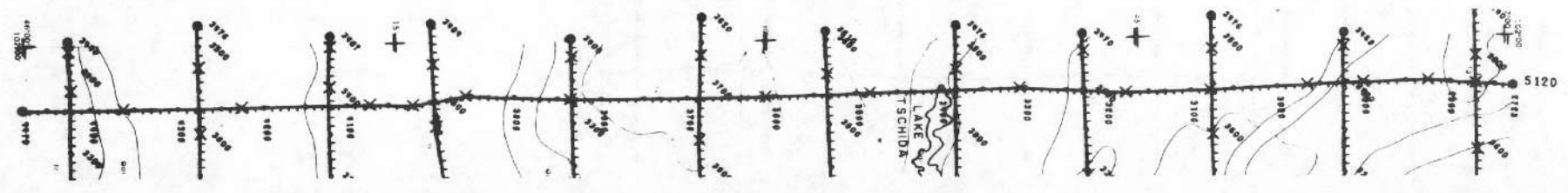


ETH  
1.0 PPM/DIV



ALT  
100 FT/DIV





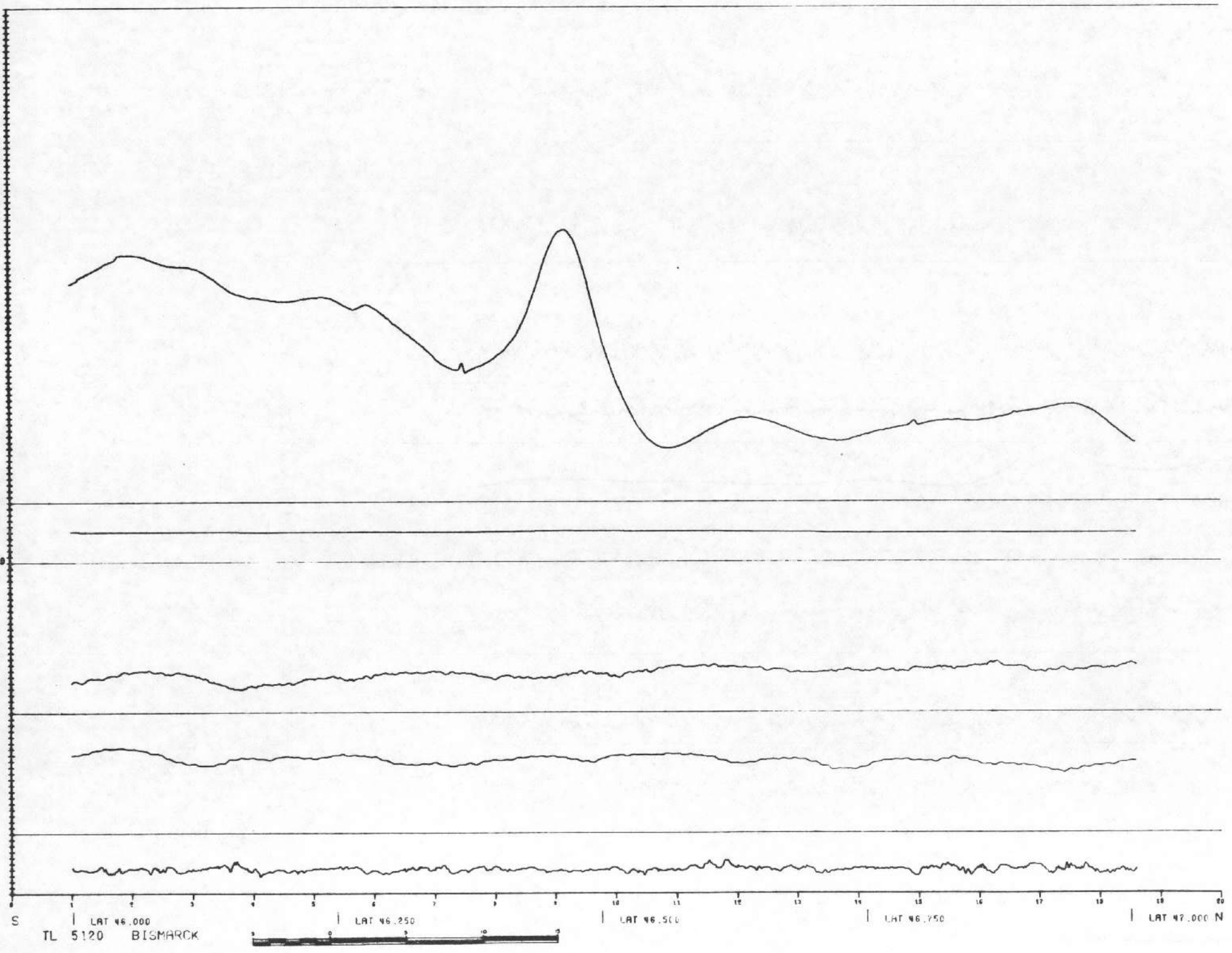
RMAG  
10 GAMMA/DIV  
BASE = -100.0

BMAG  
20 GAMMA/DIV  
BASE = 5920.0

BP  
3 MM HG/DIV  
BASE = 660.0

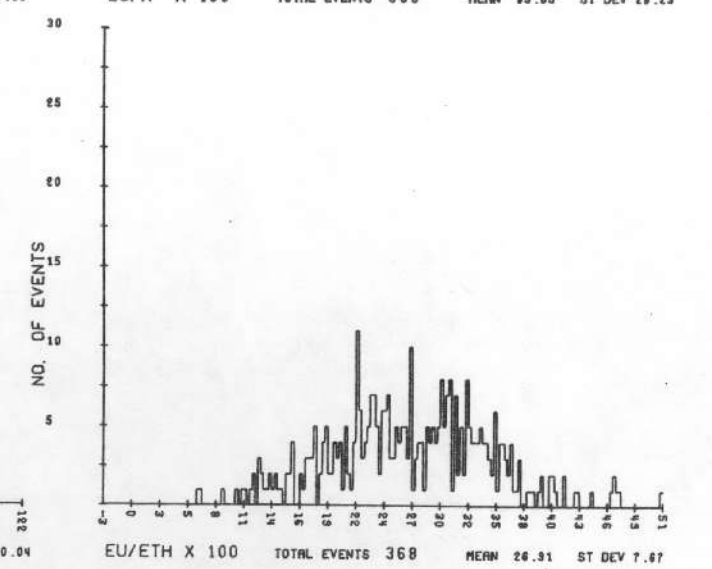
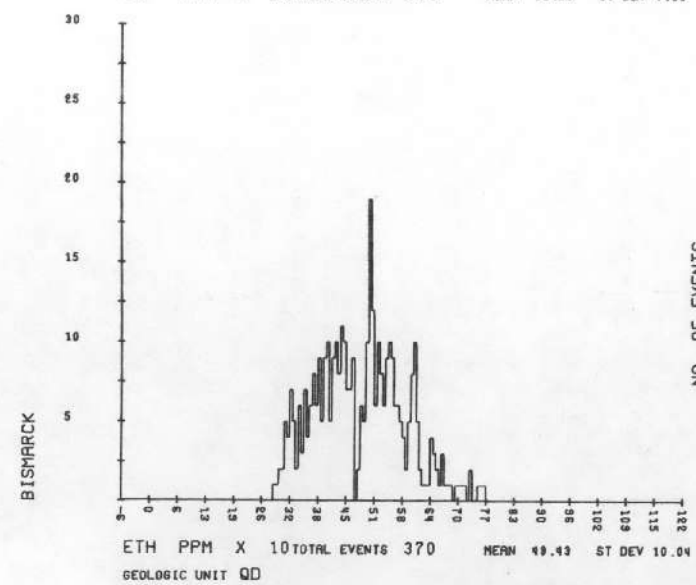
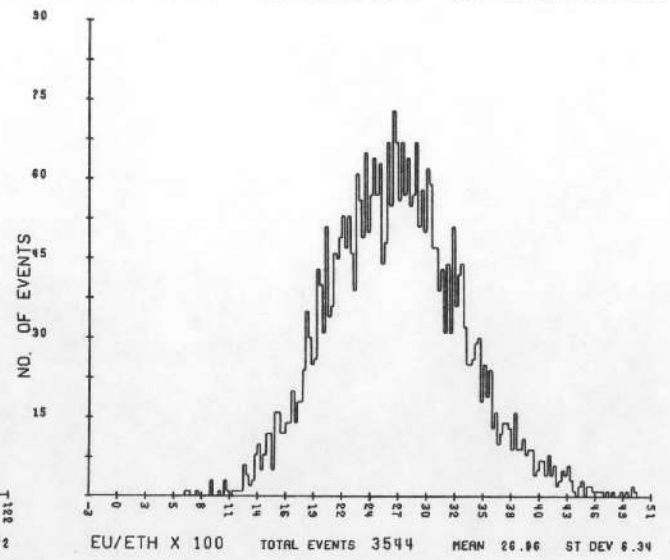
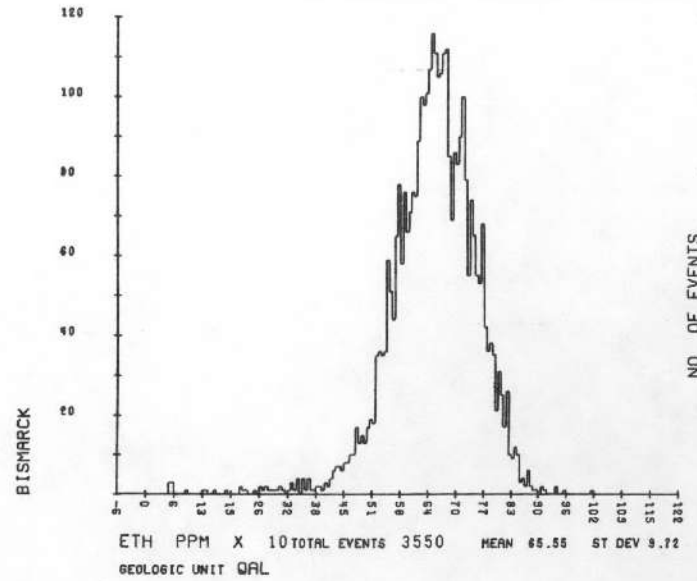
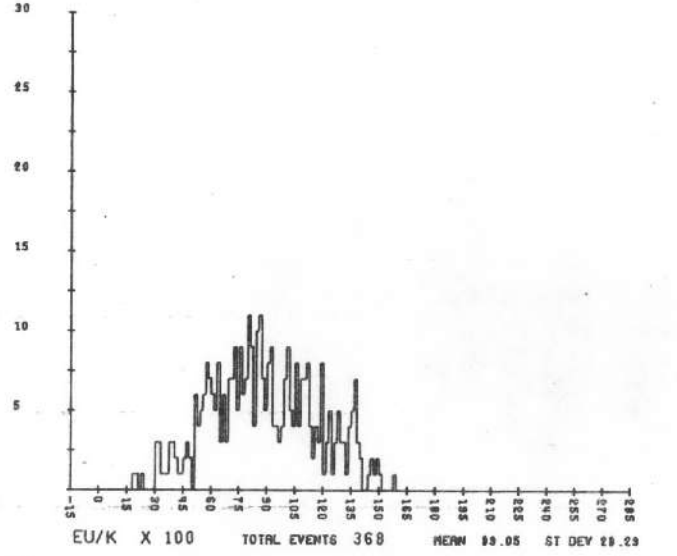
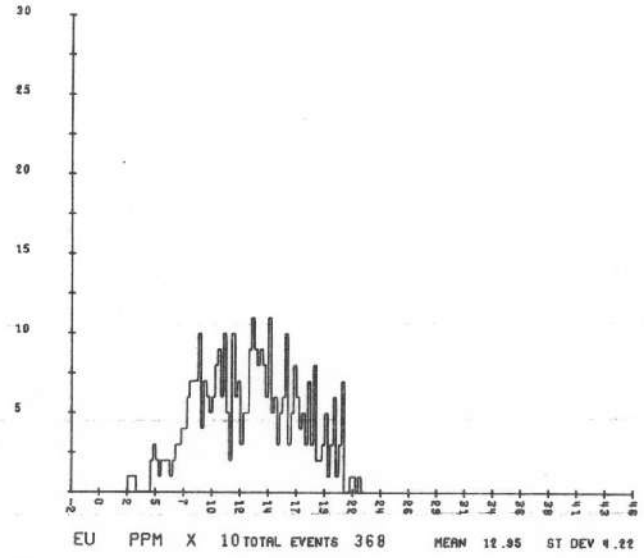
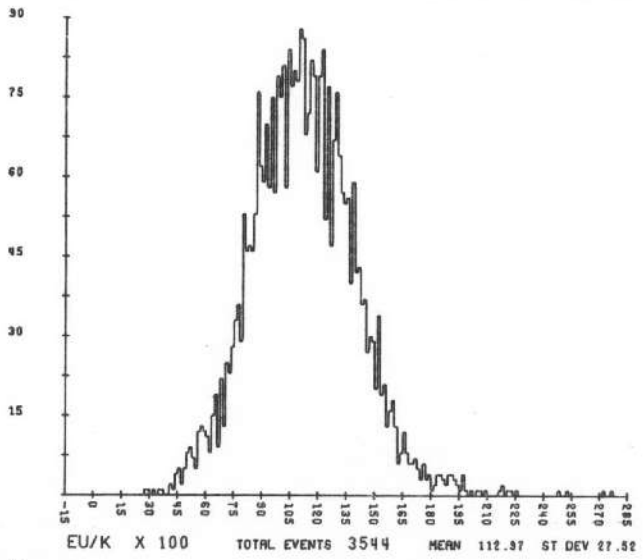
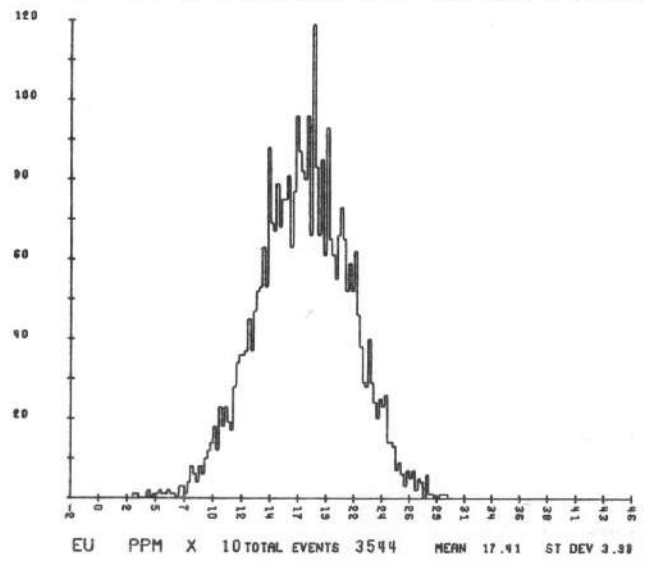
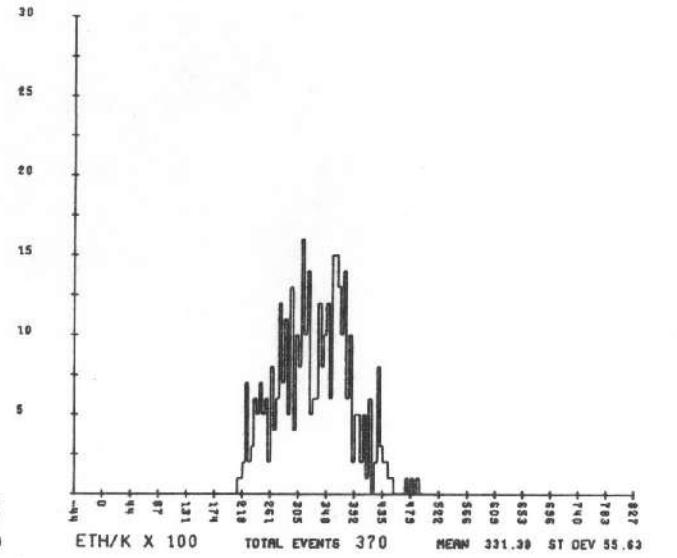
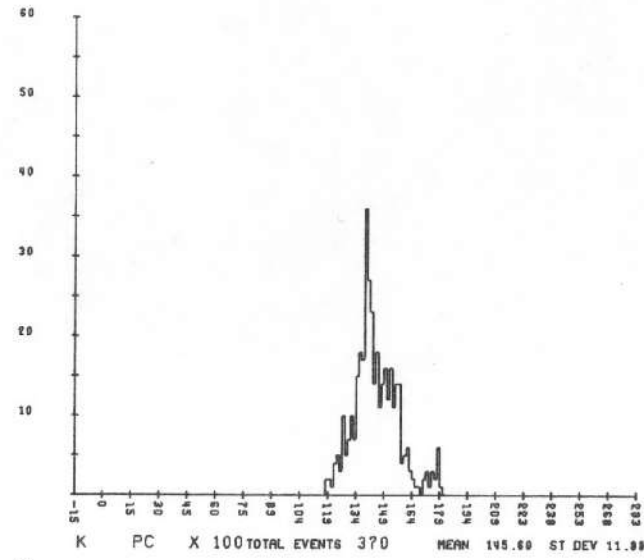
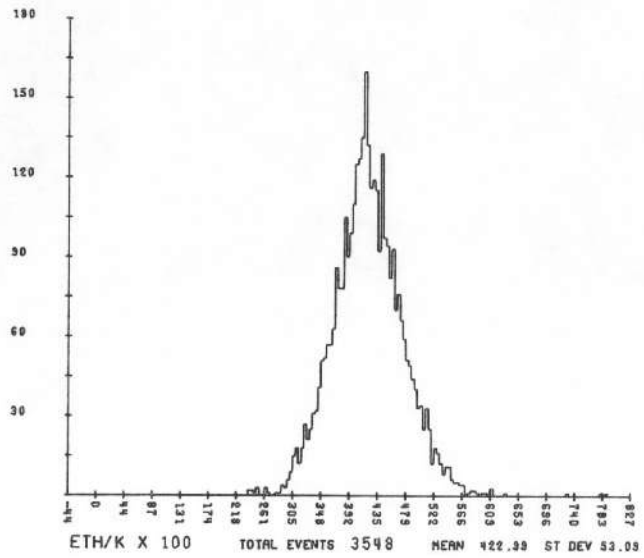
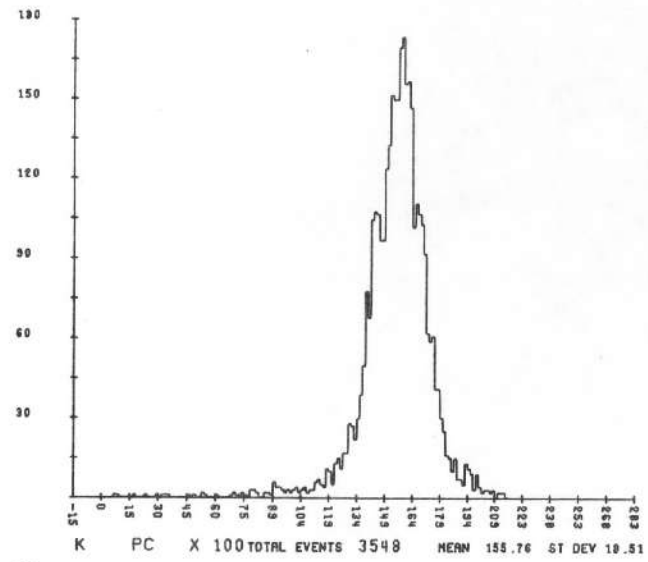
TEMP  
1 DEG C/DIV  
BASE = 25.0

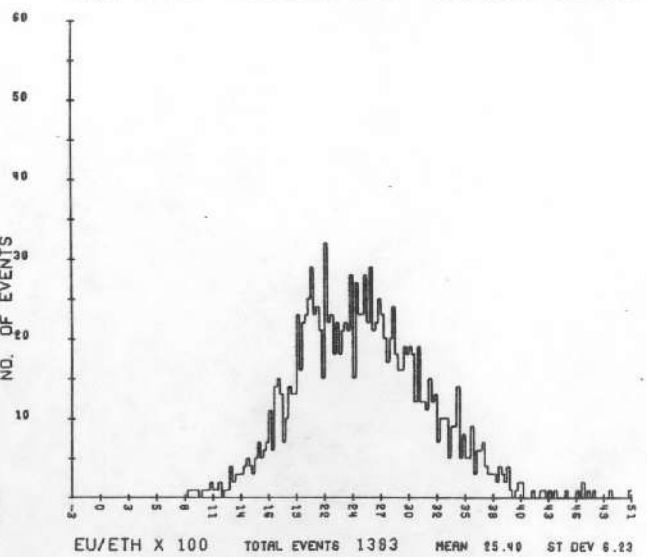
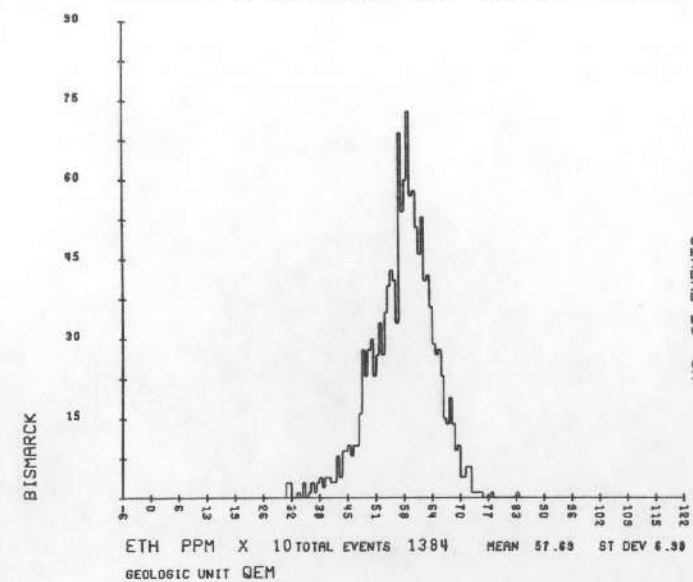
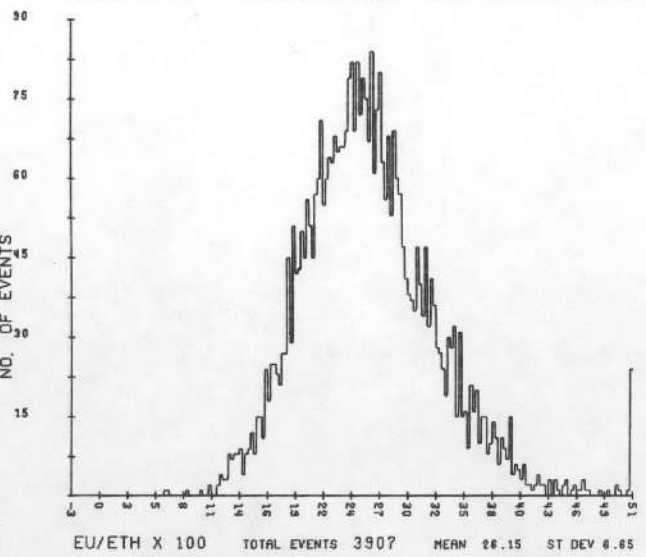
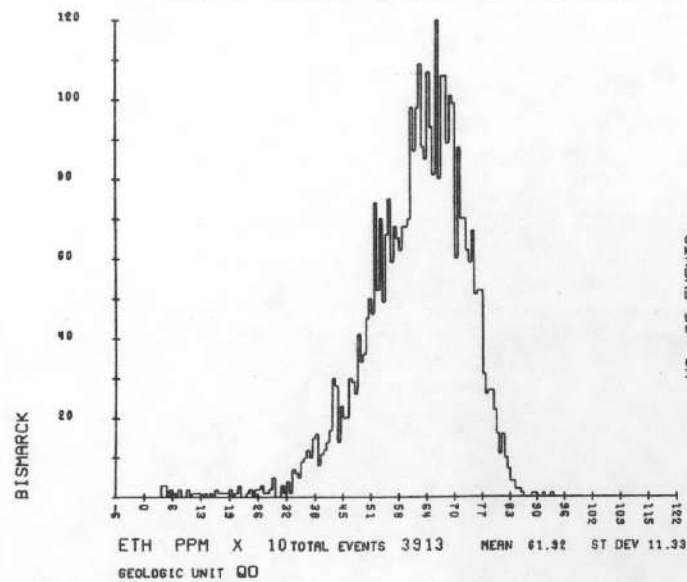
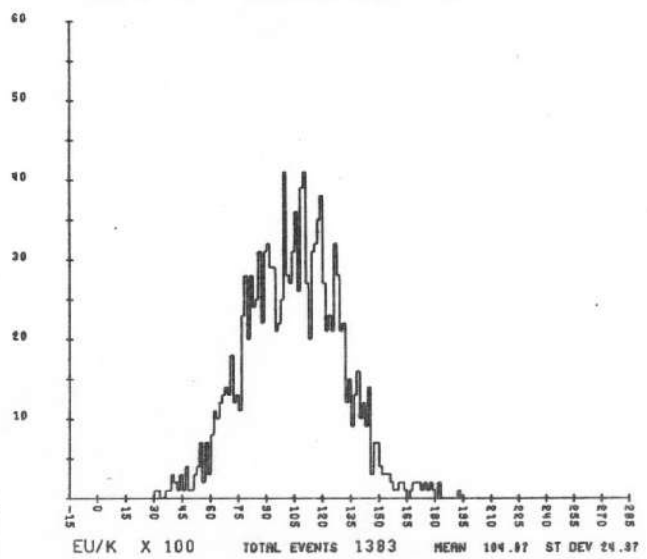
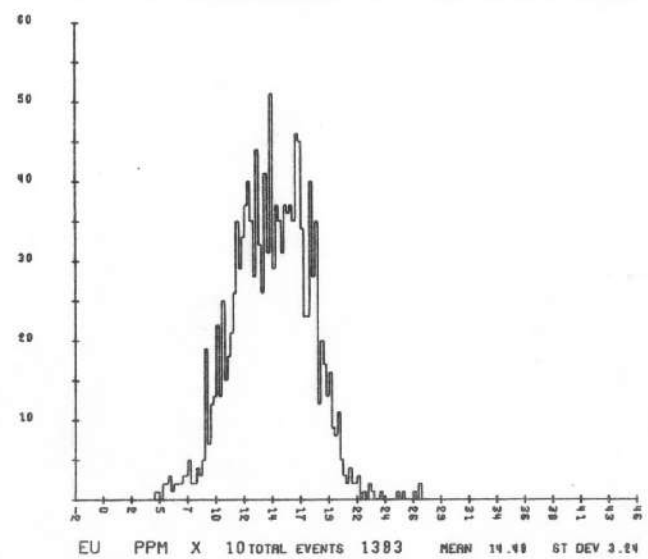
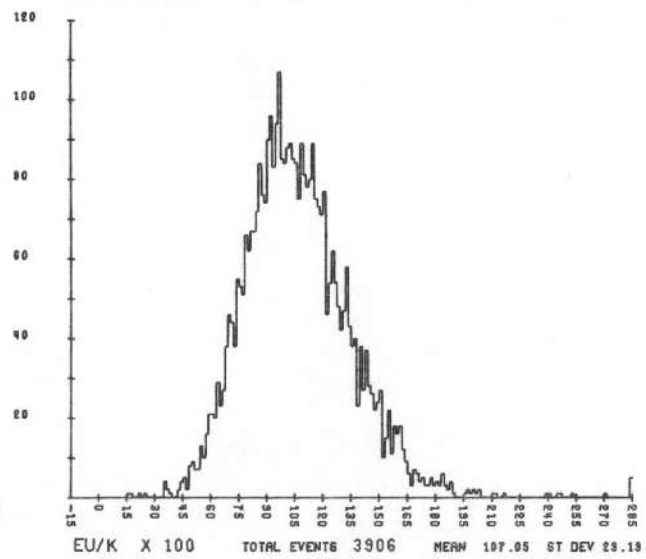
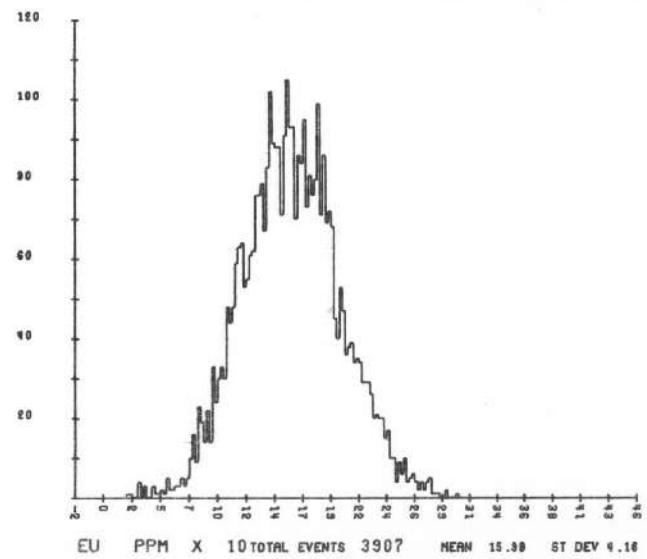
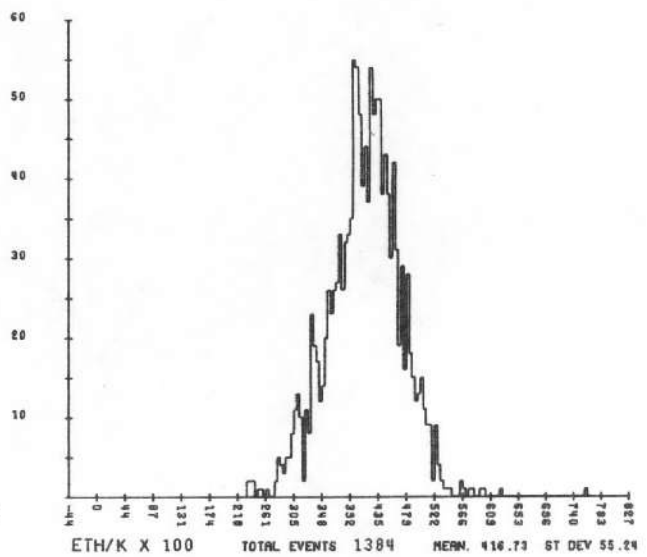
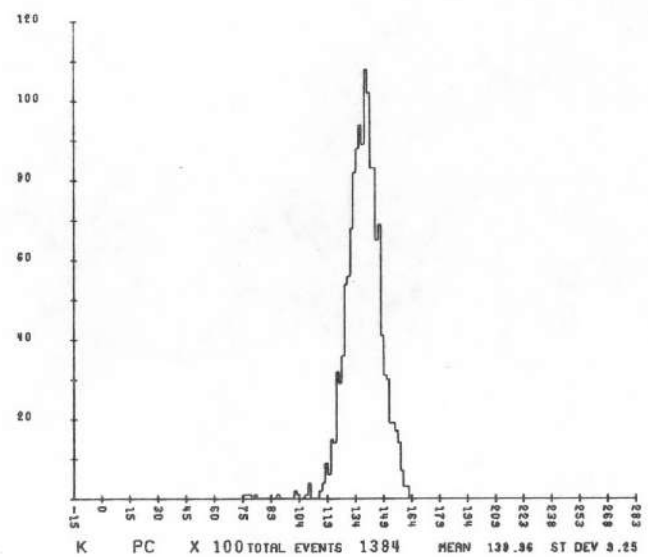
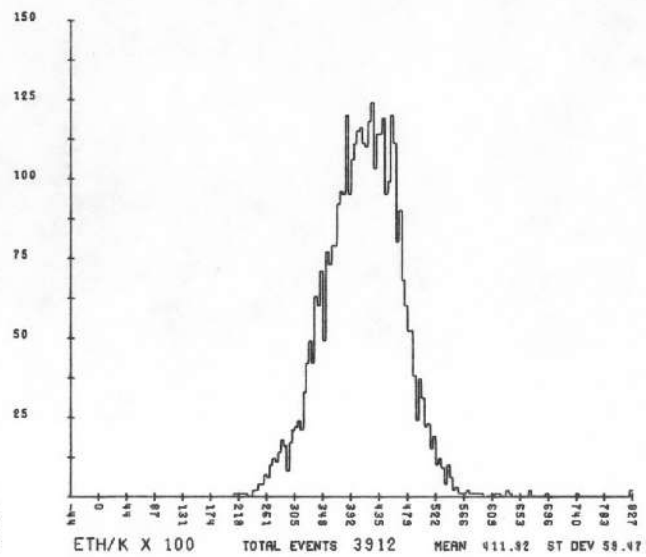
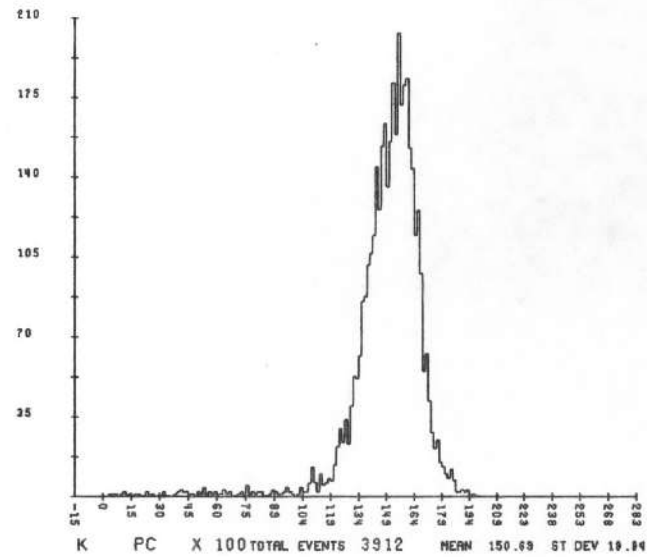
ALT  
100 FT/DIV



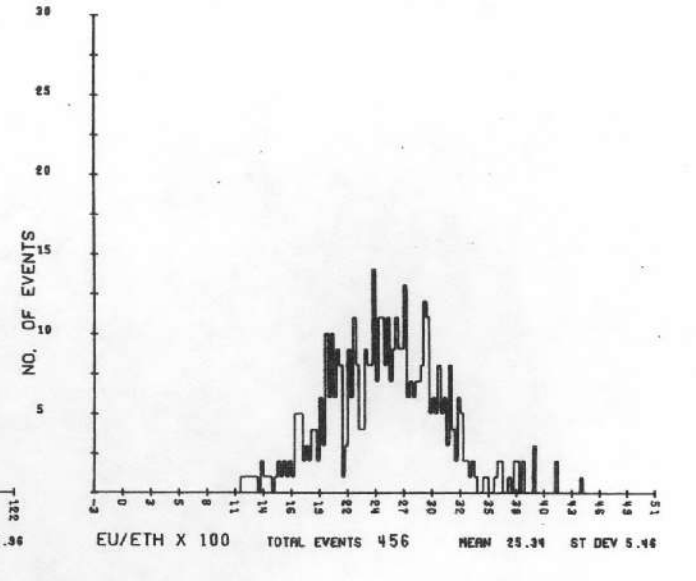
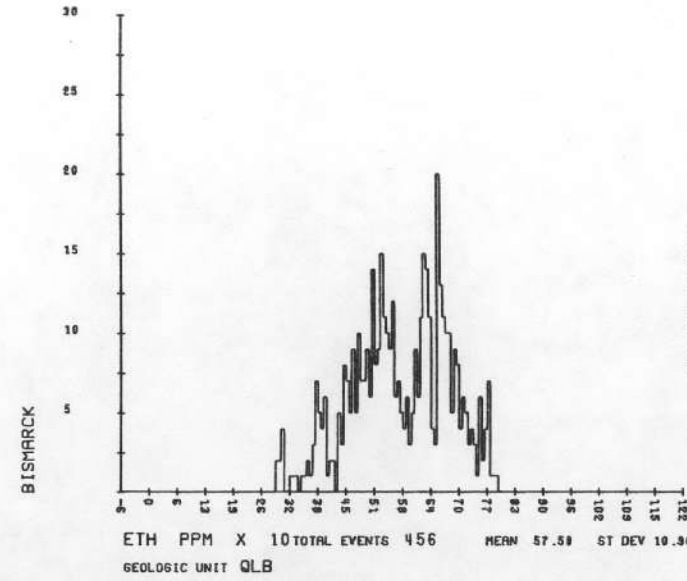
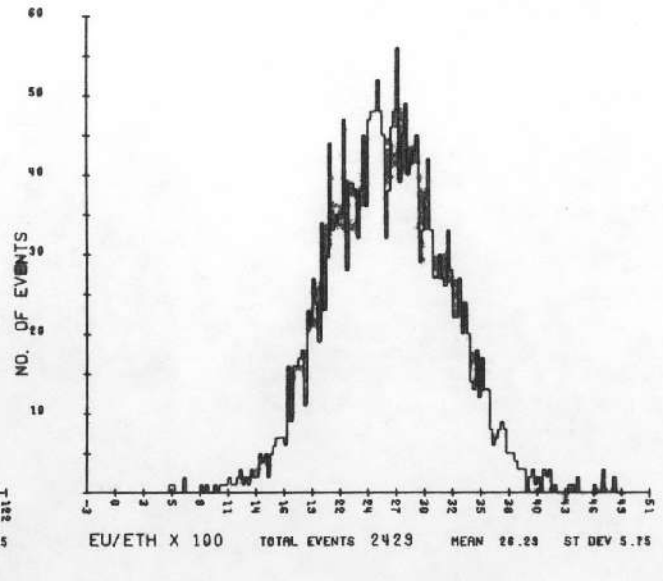
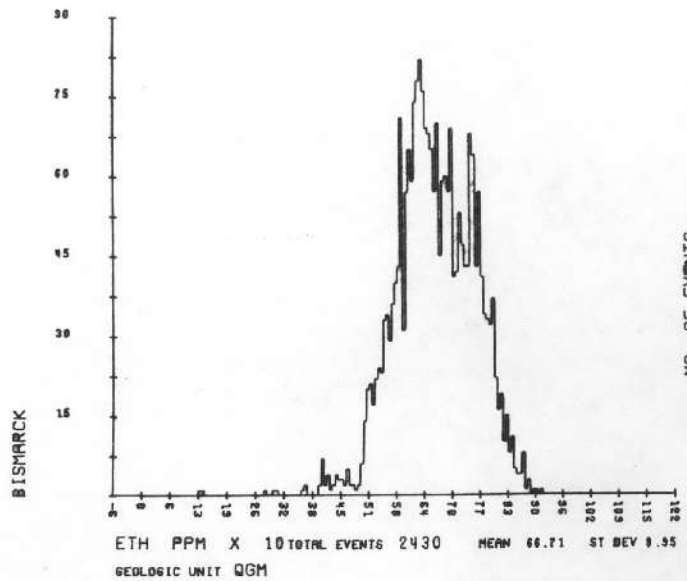
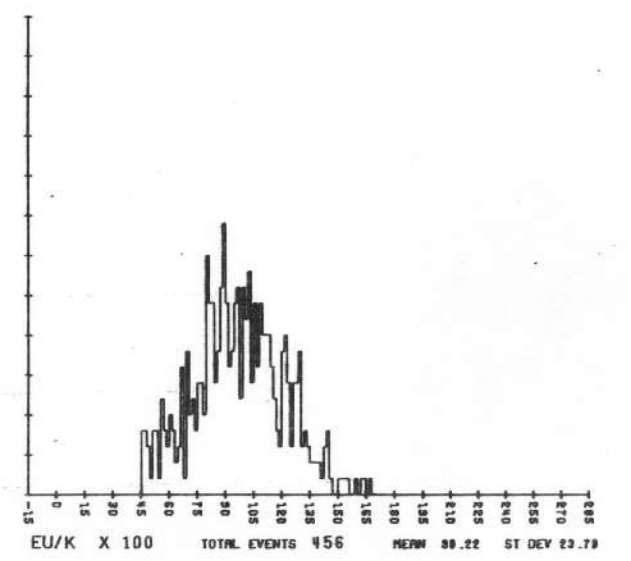
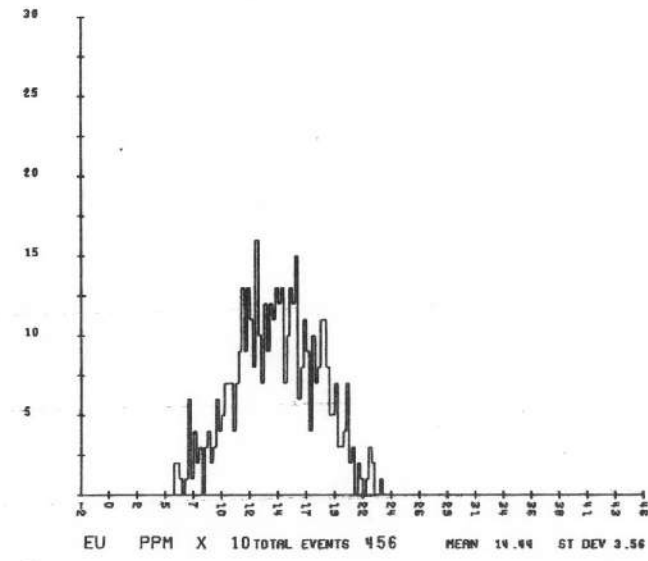
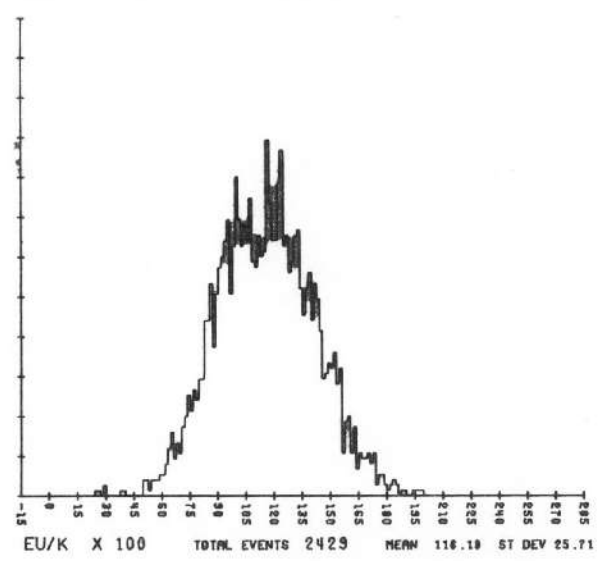
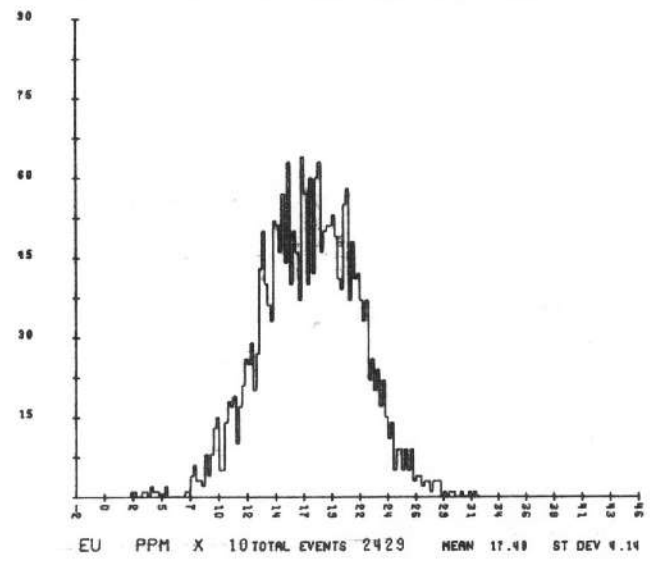
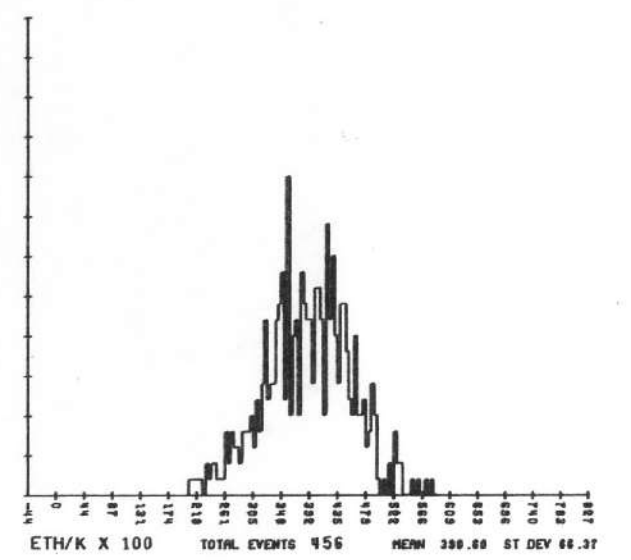
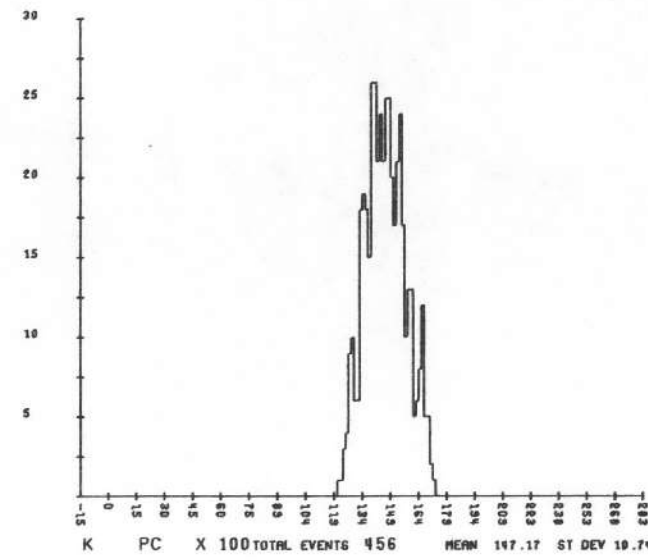
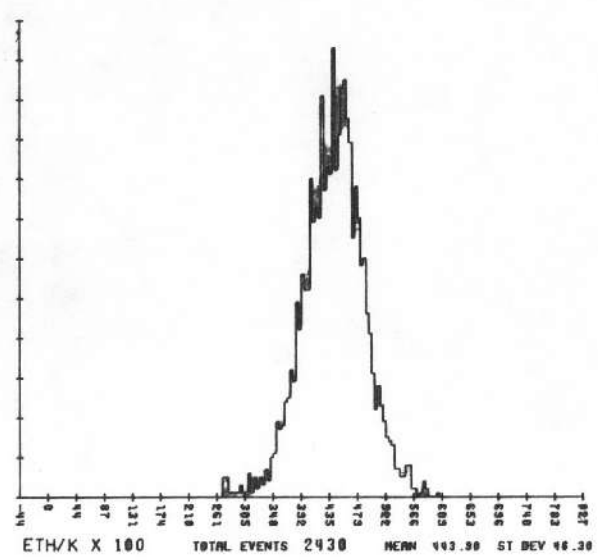
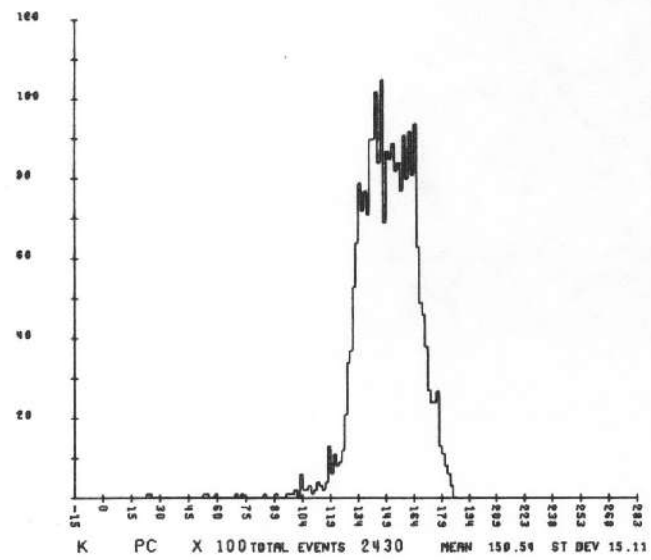
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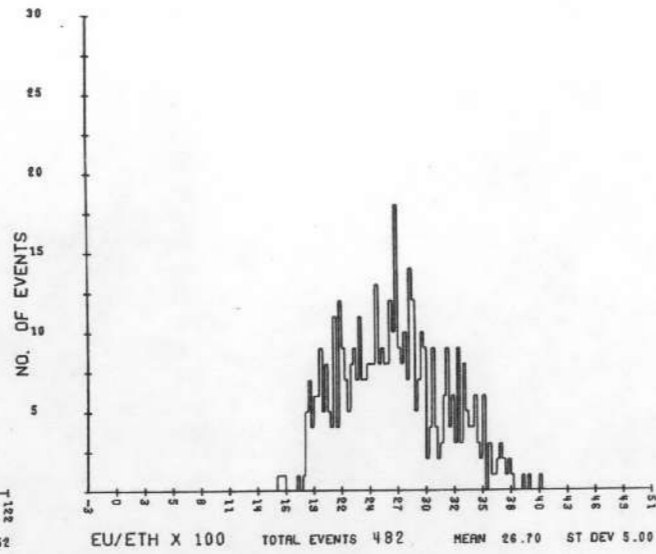
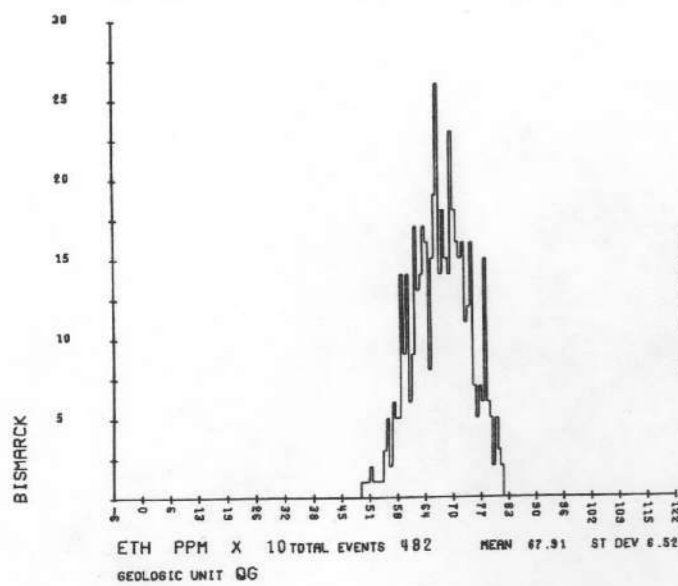
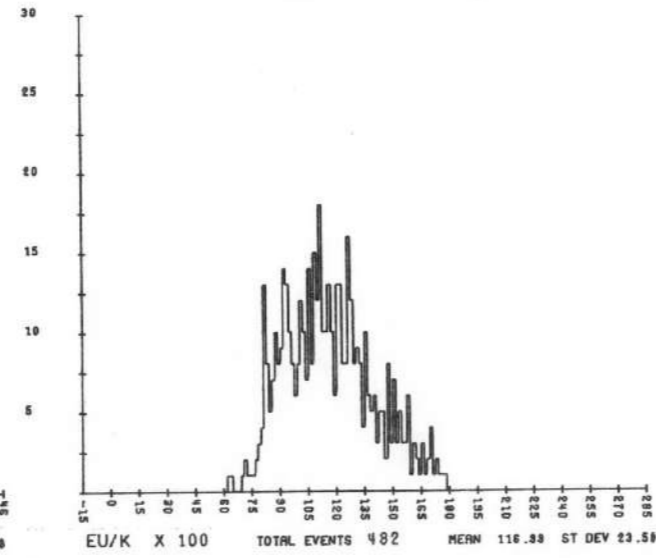
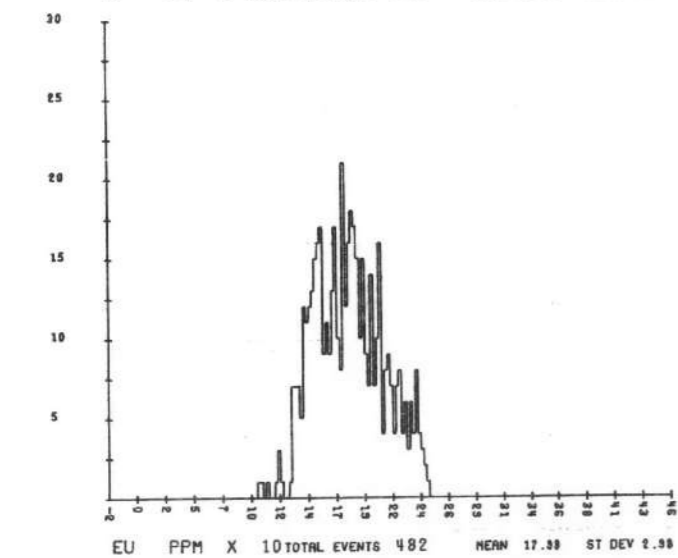
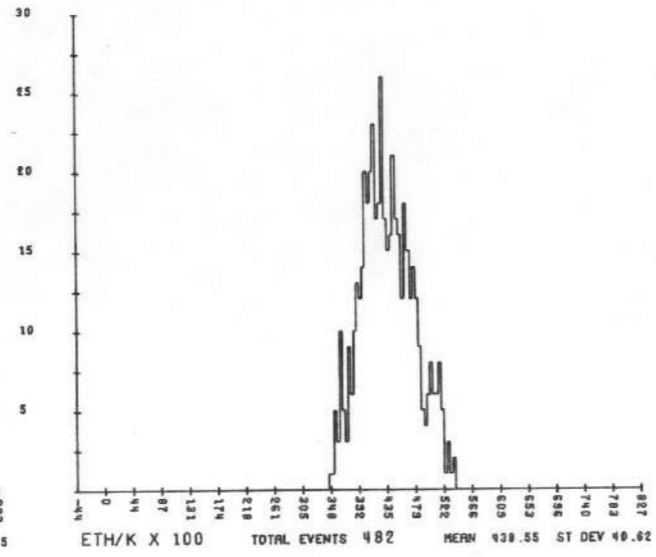
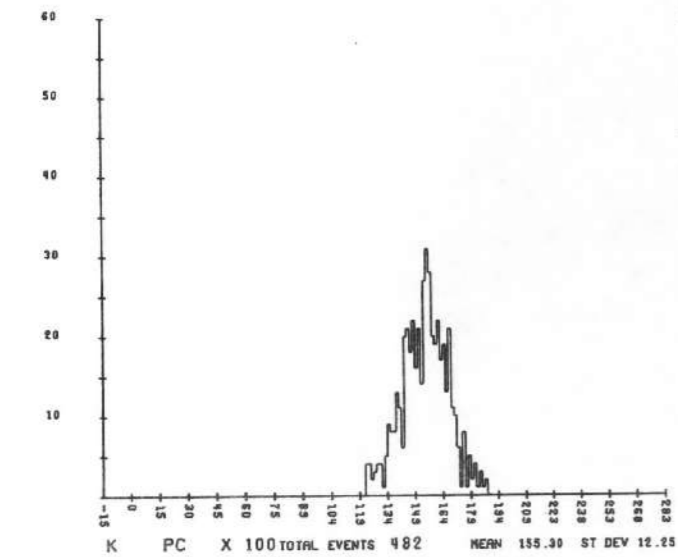




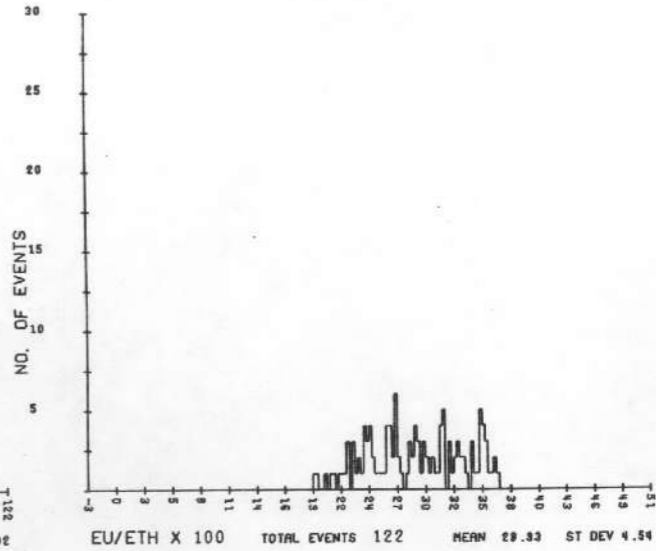
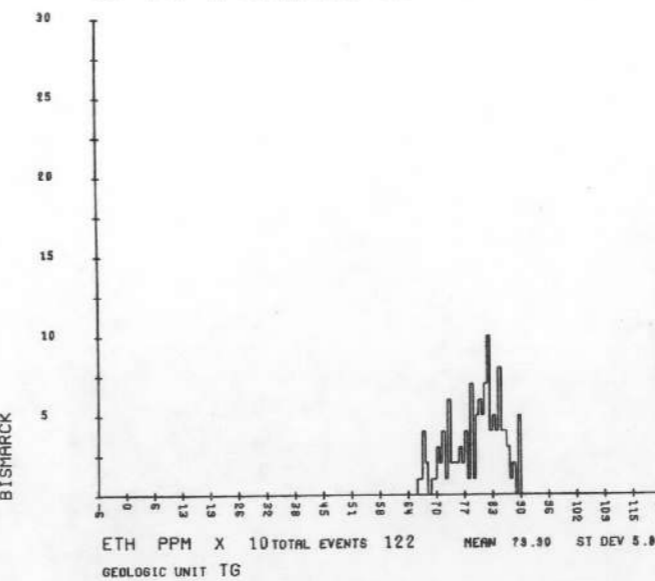
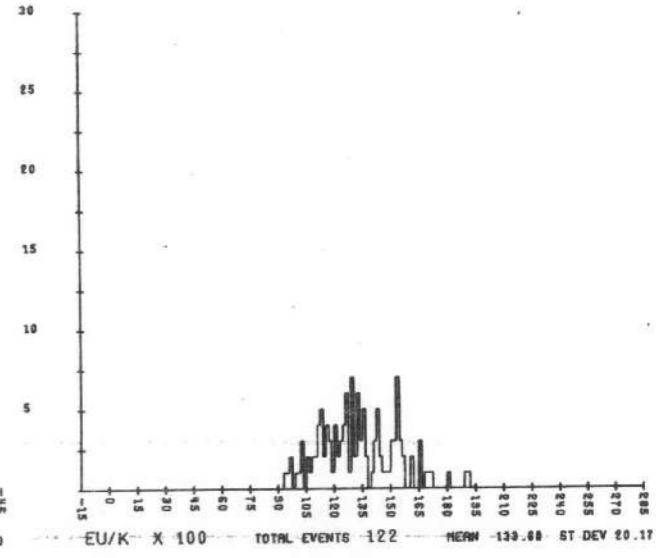
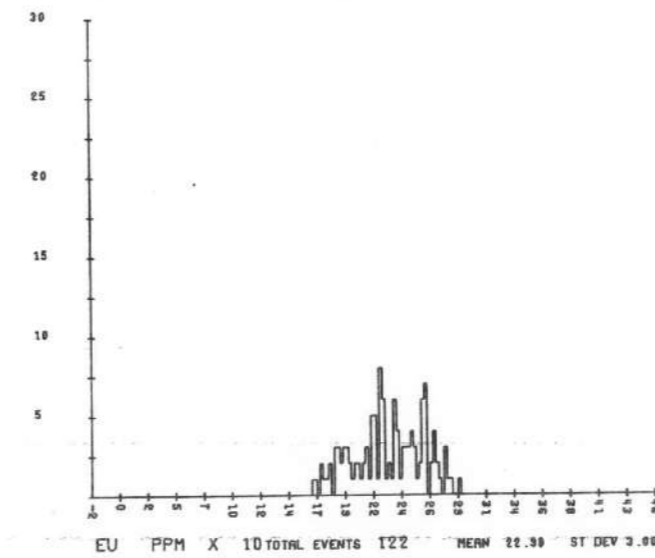
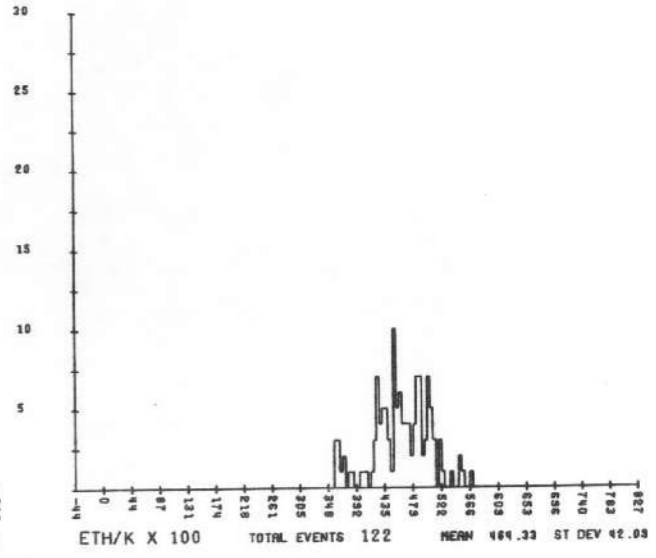
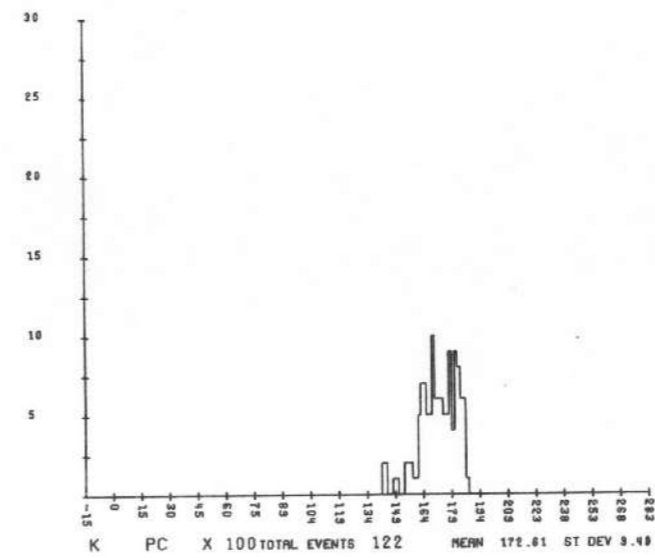






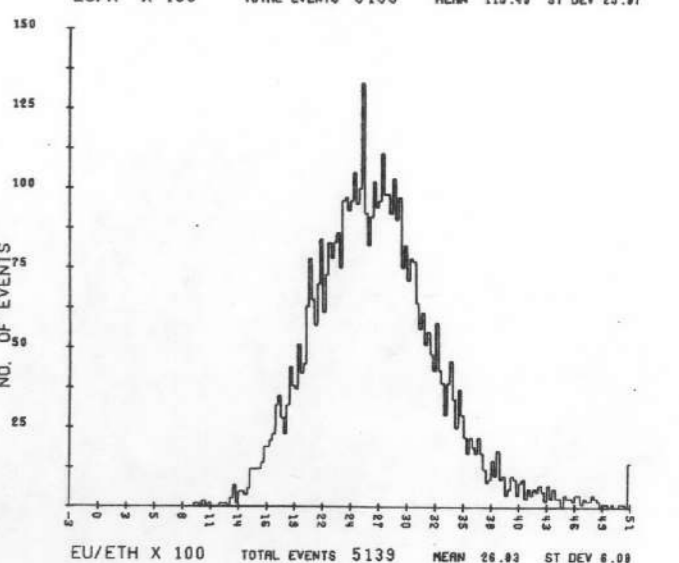
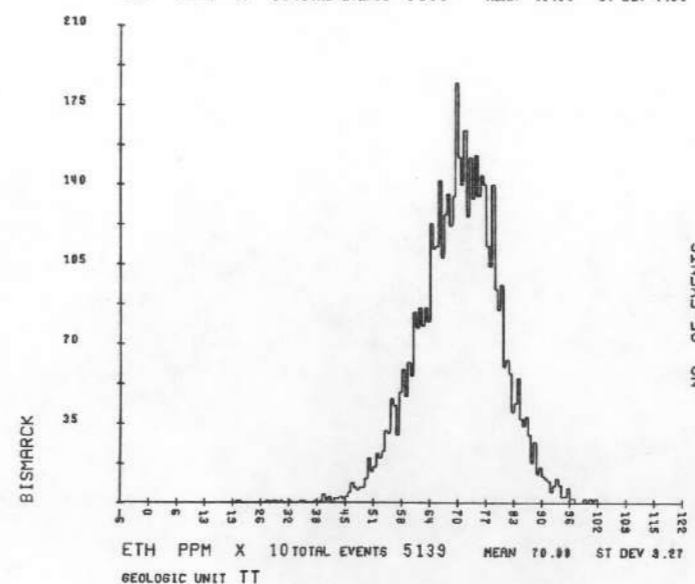
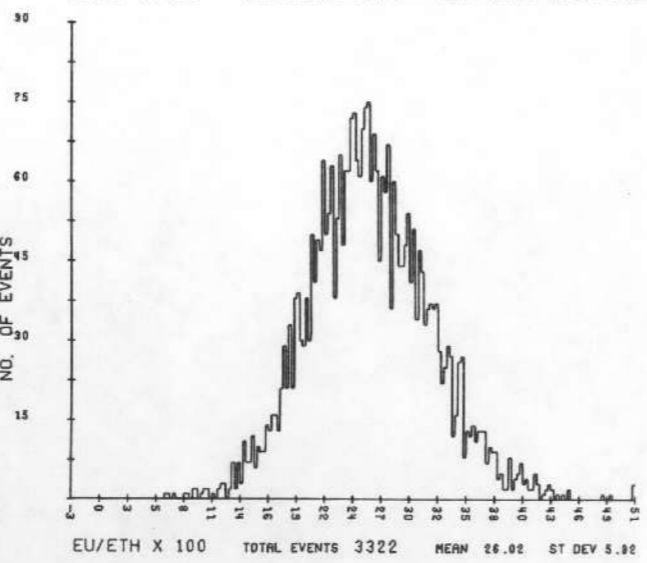
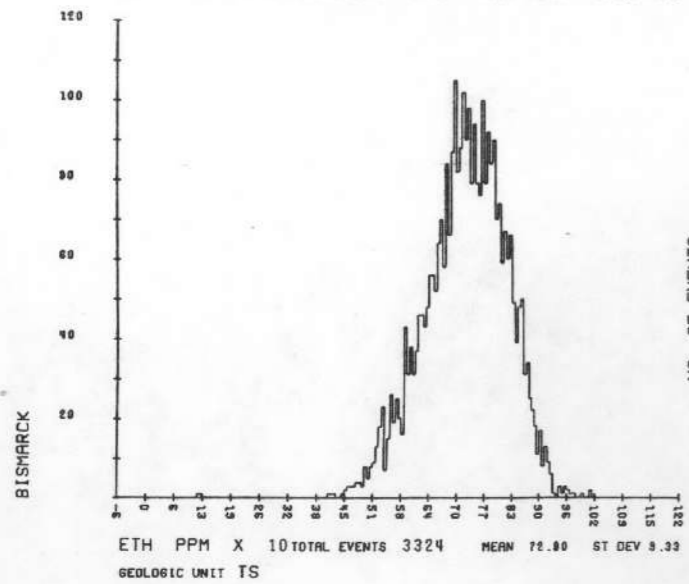
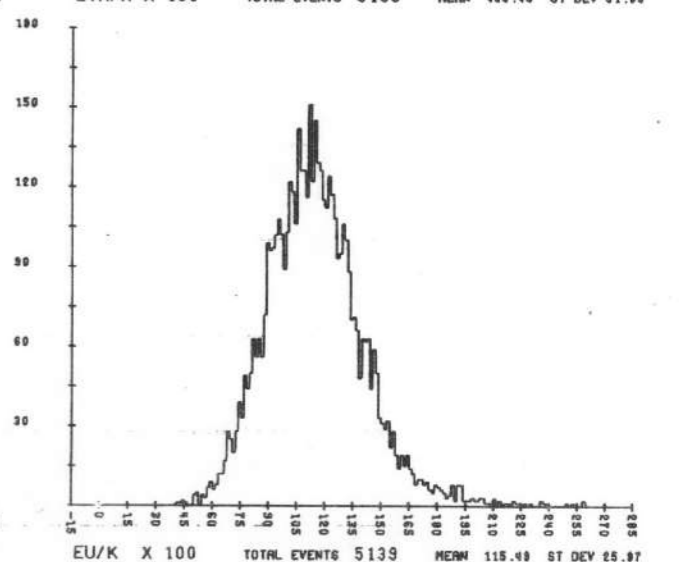
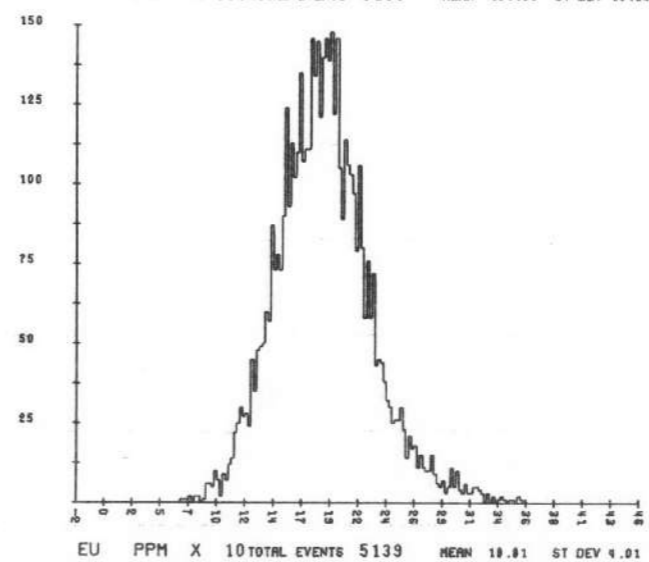
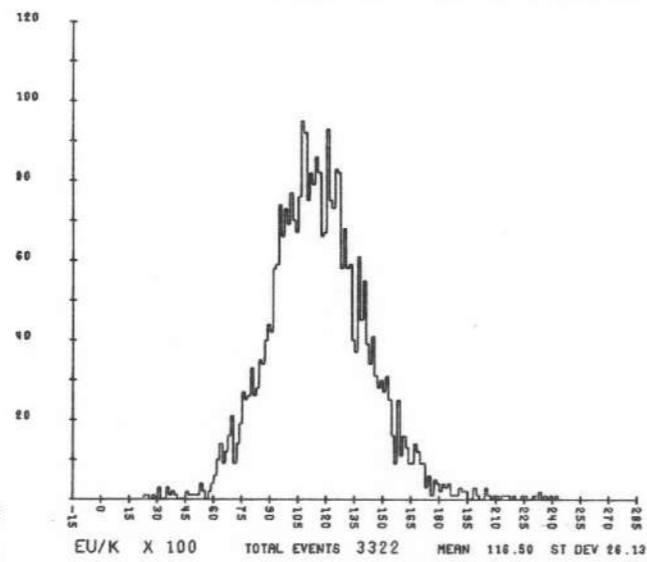
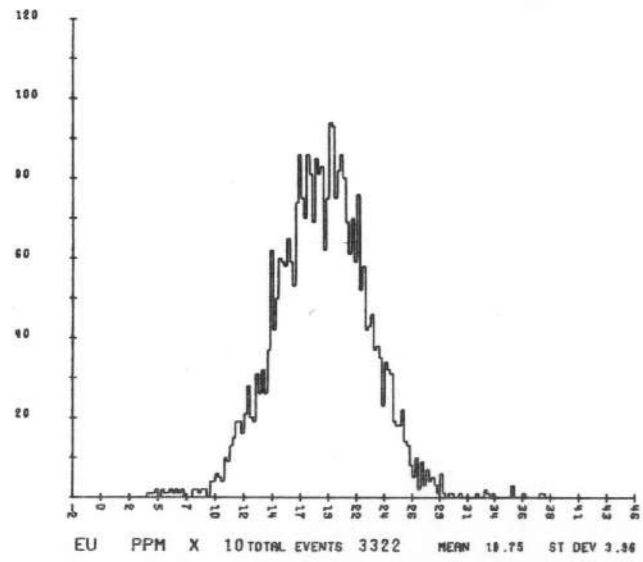
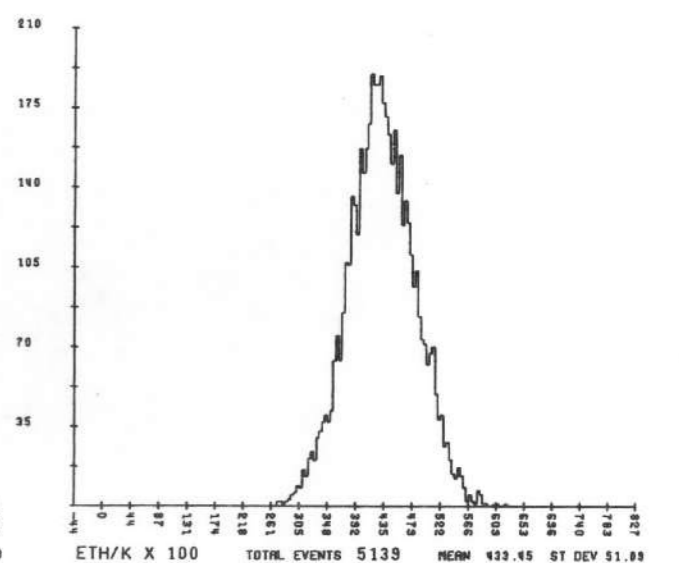
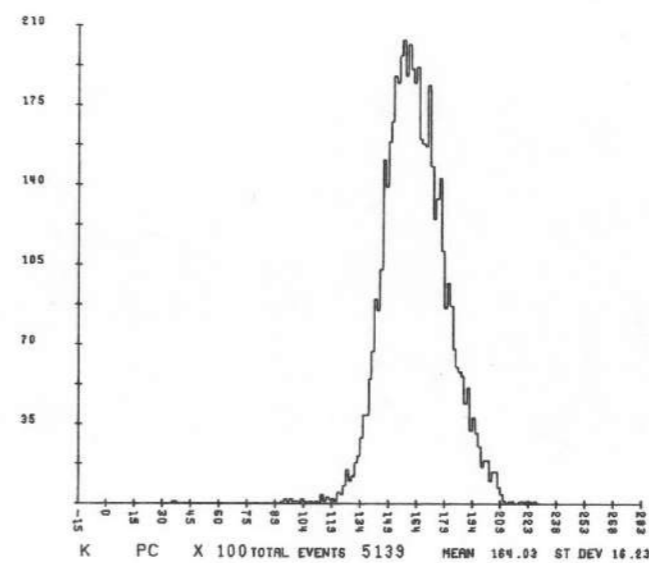
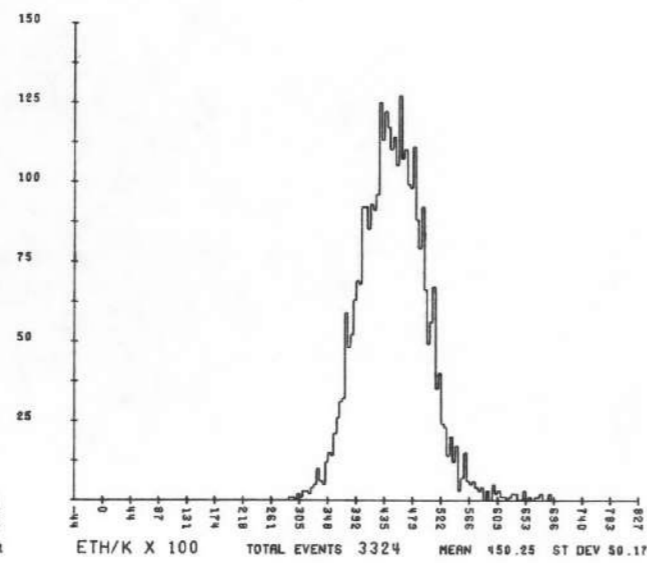
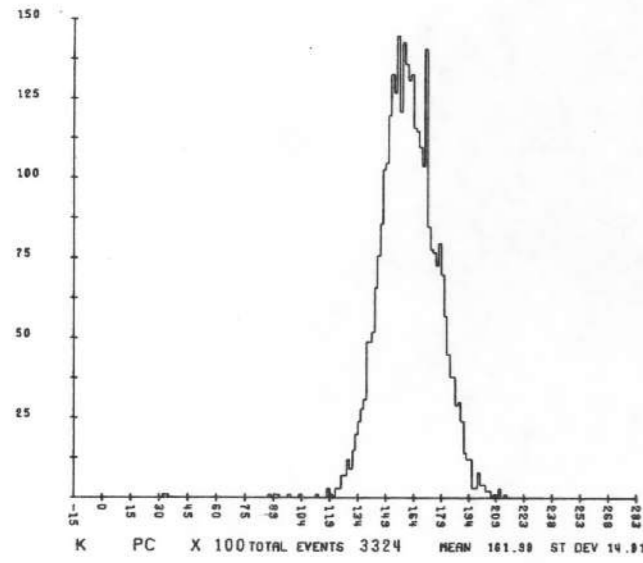


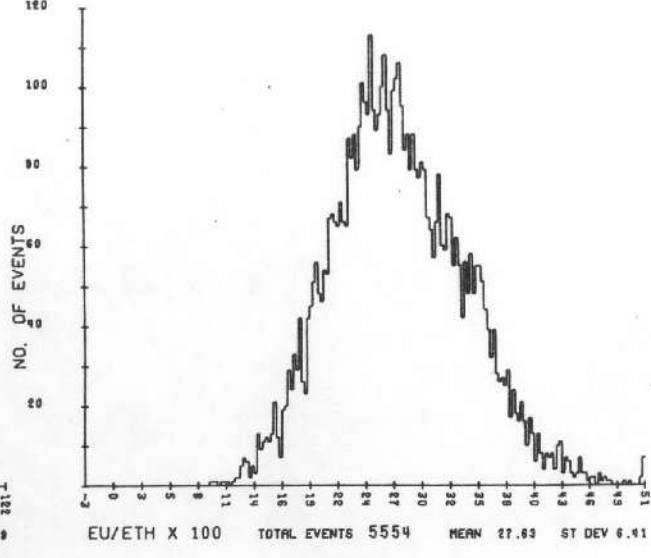
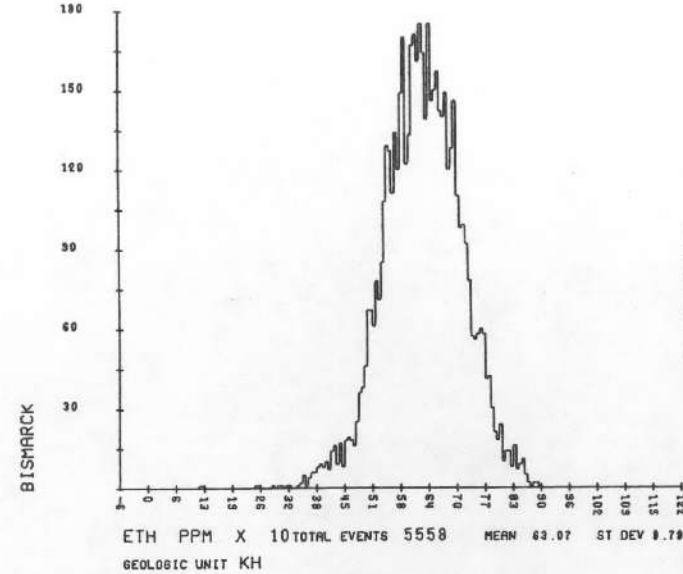
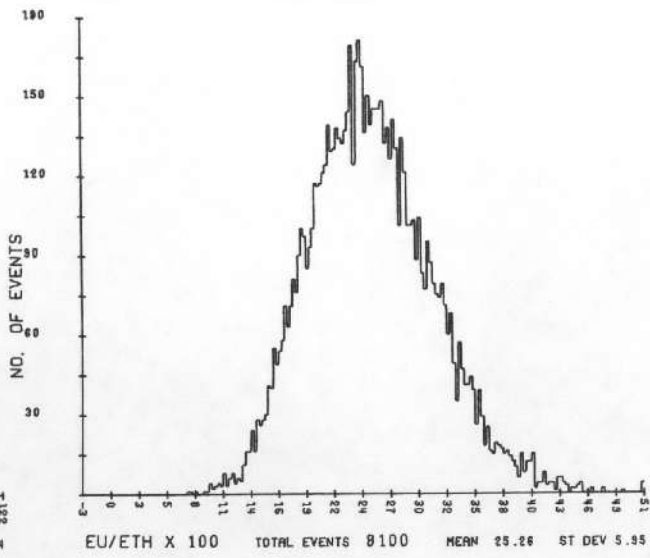
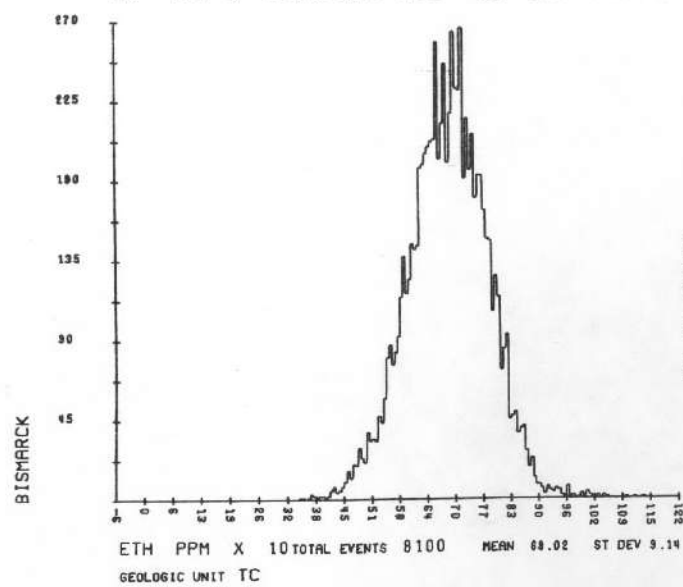
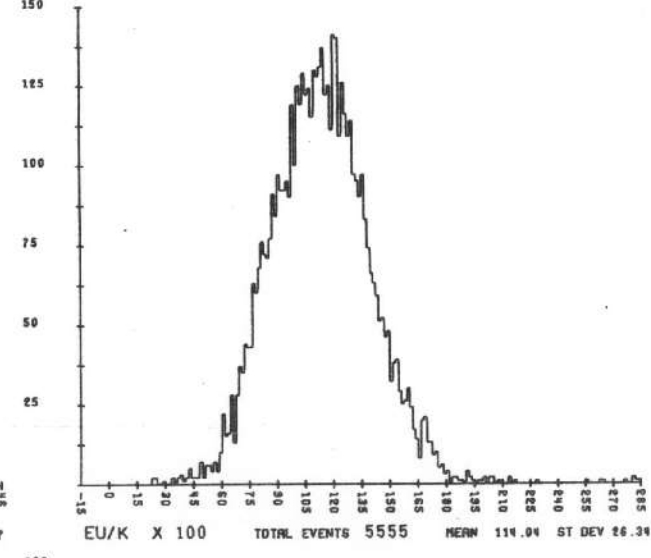
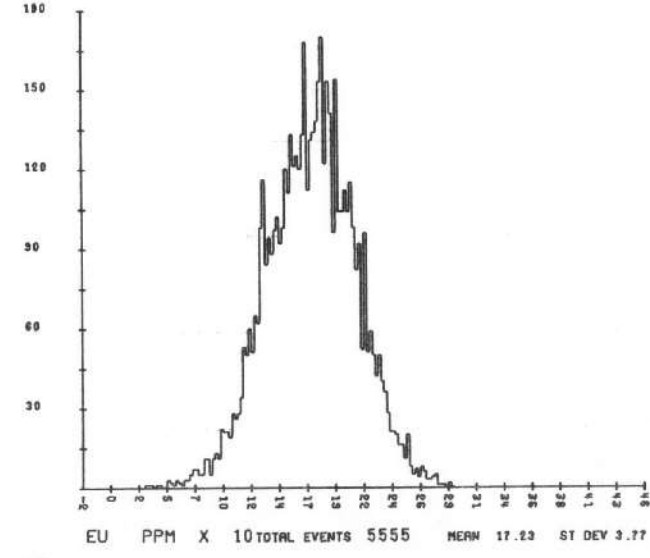
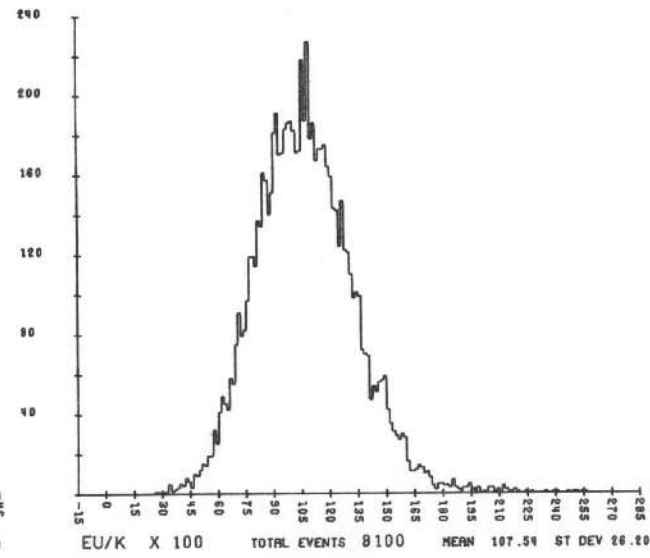
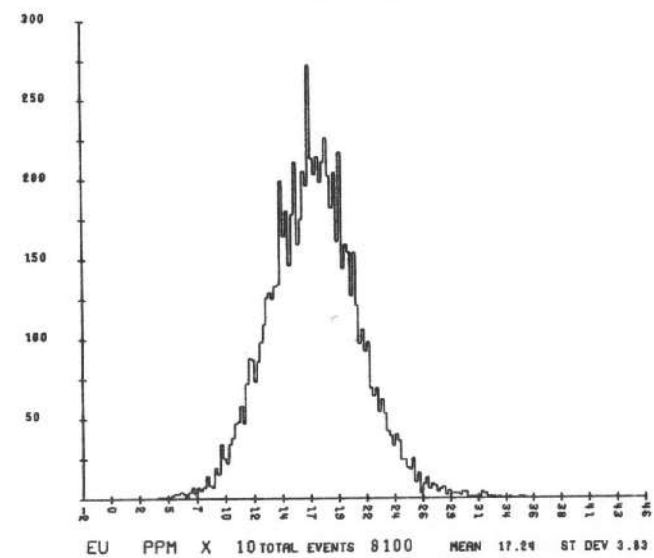
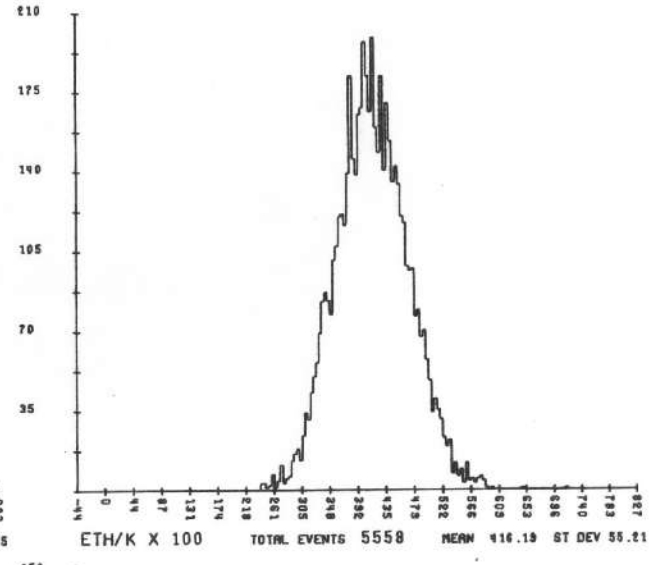
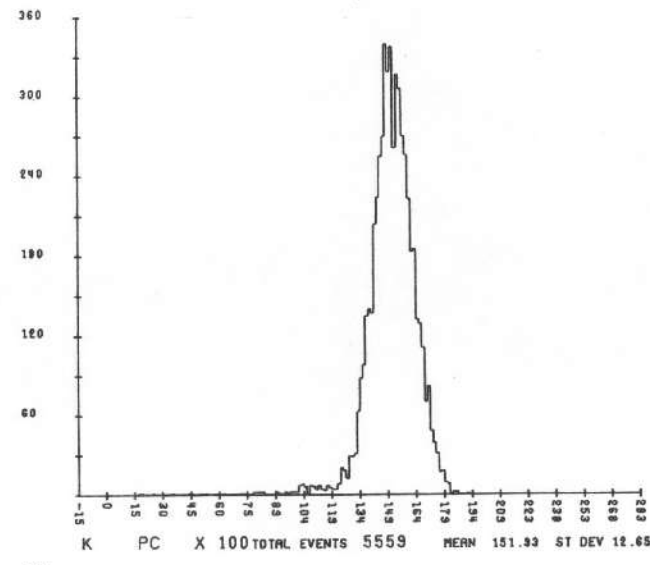
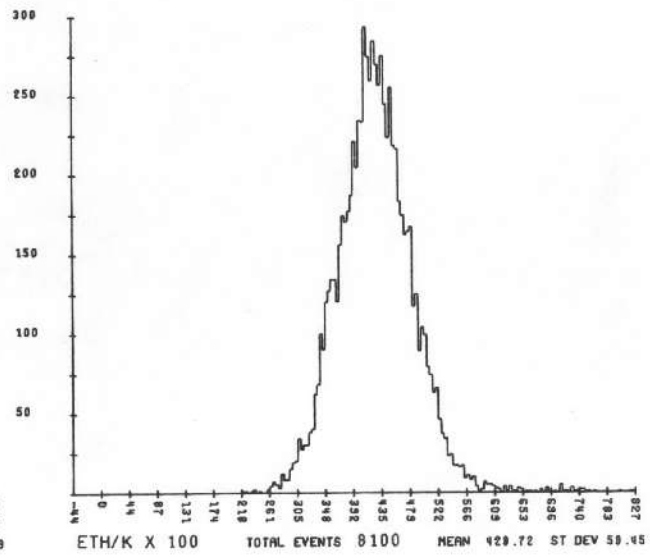
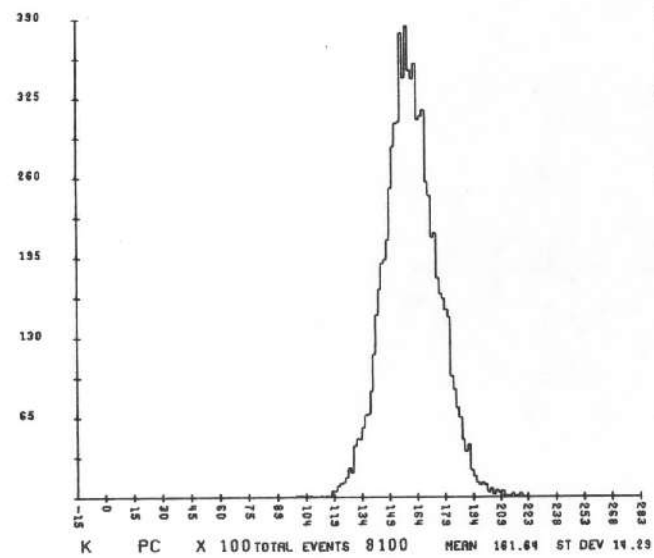
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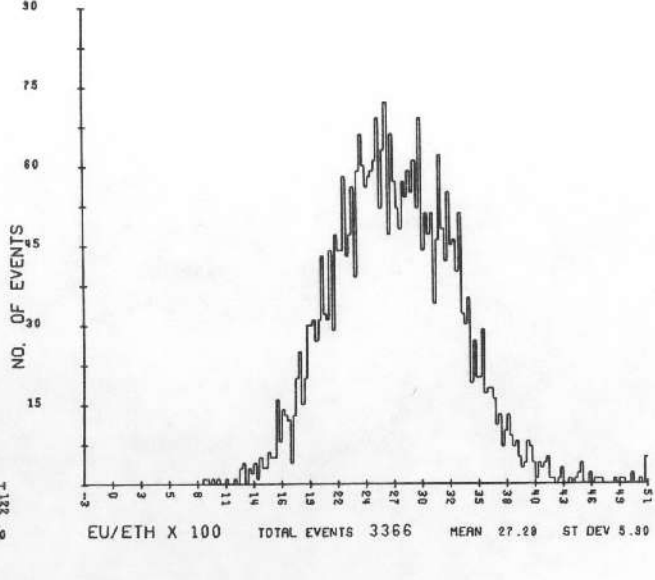
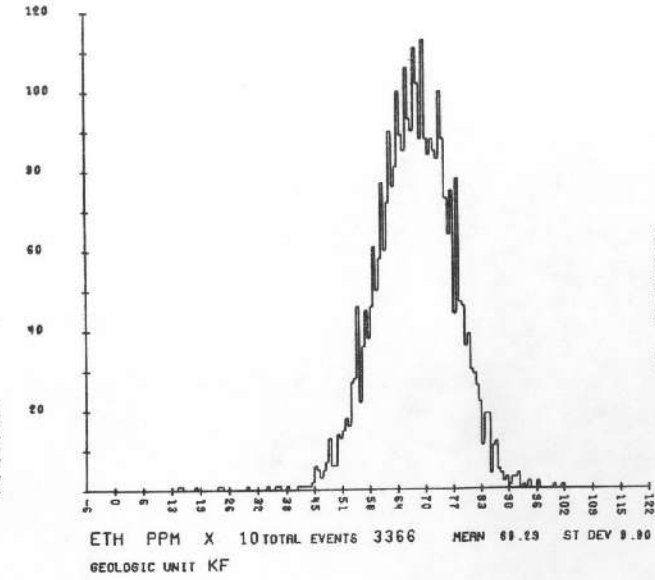
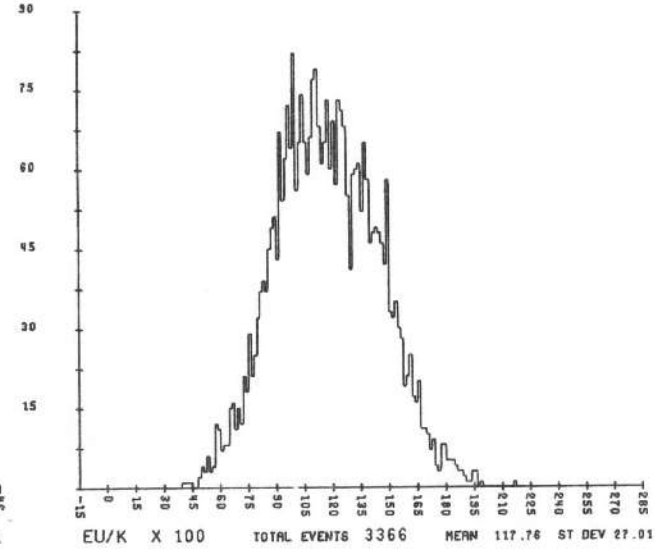
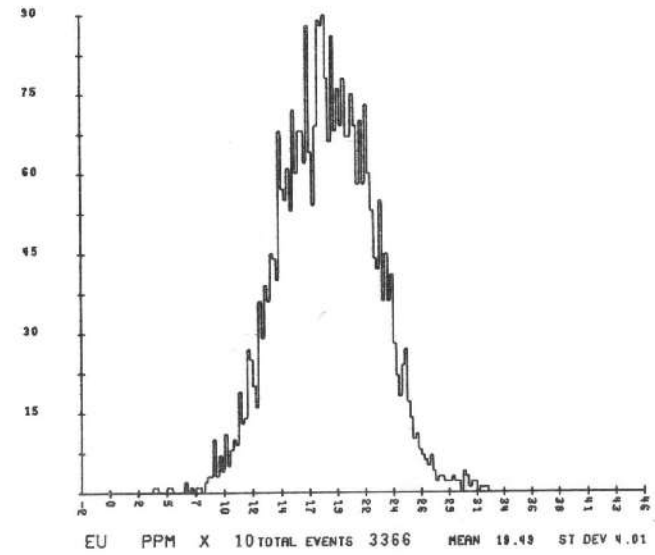
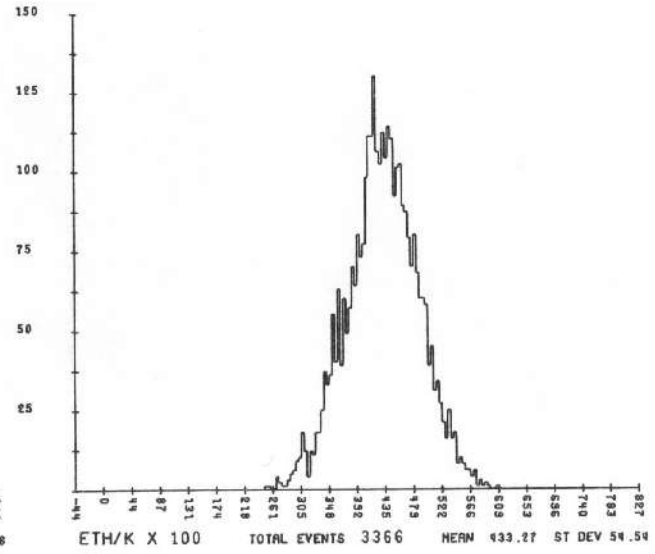
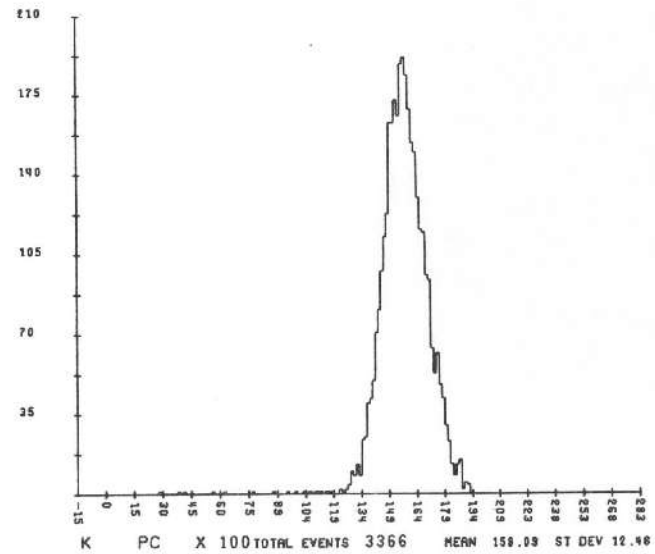
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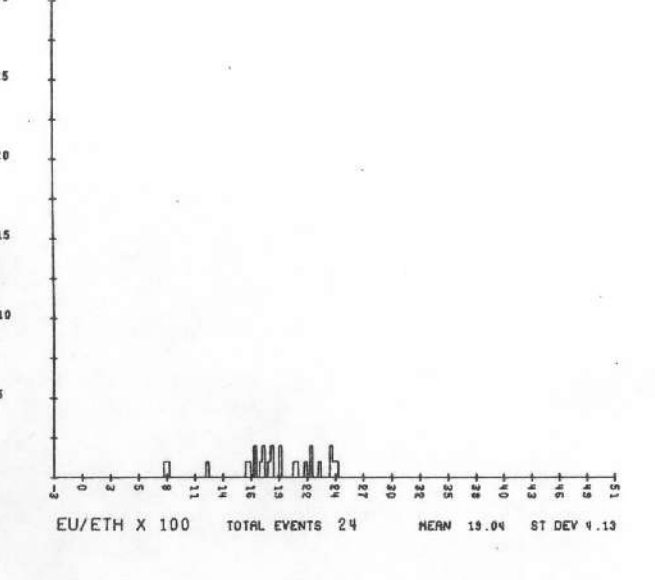
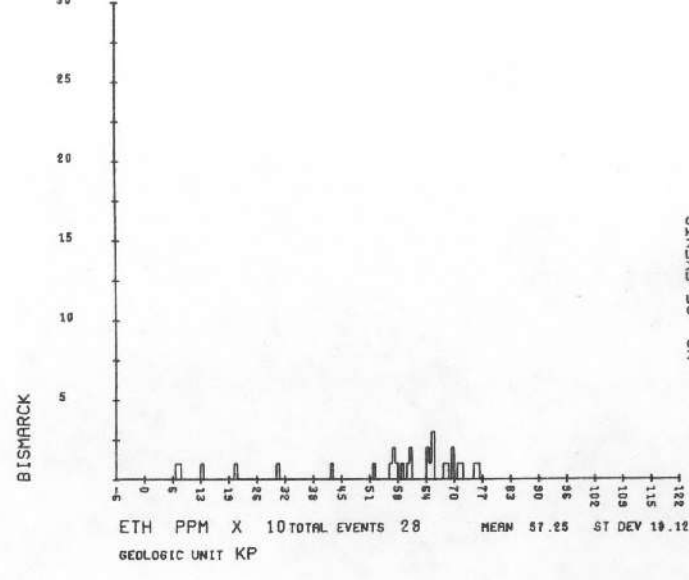
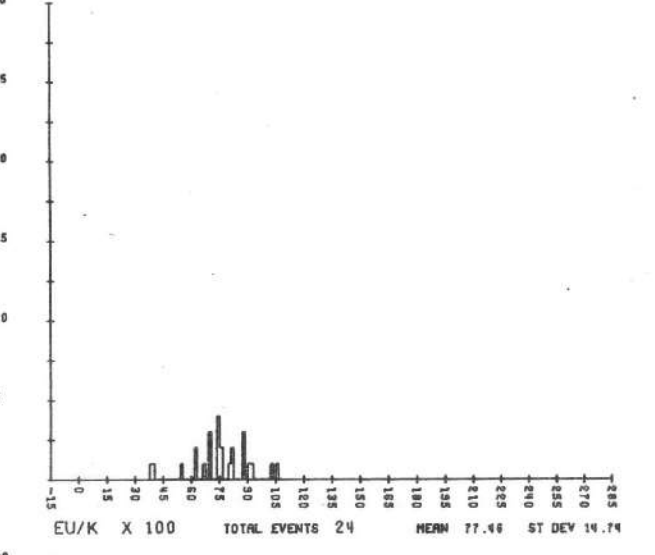
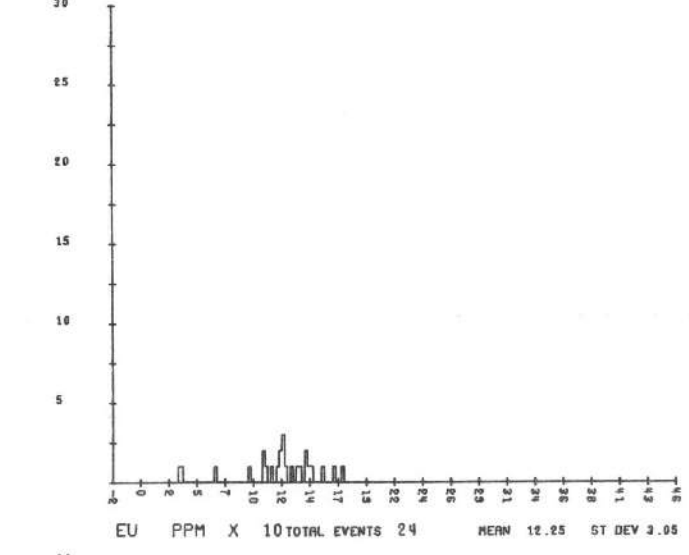
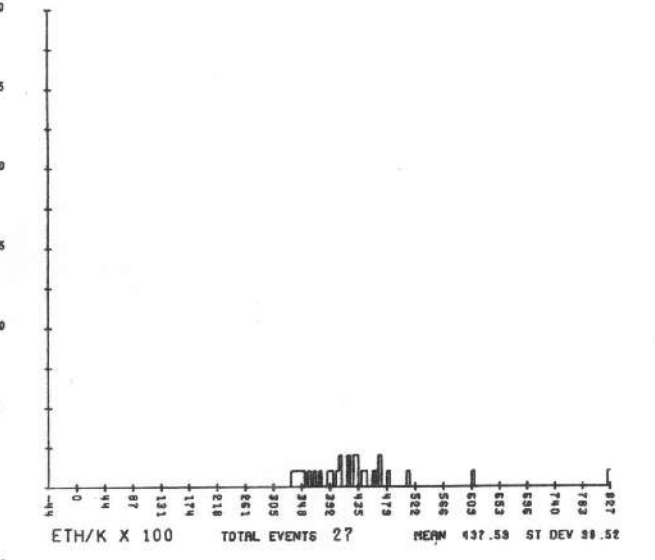
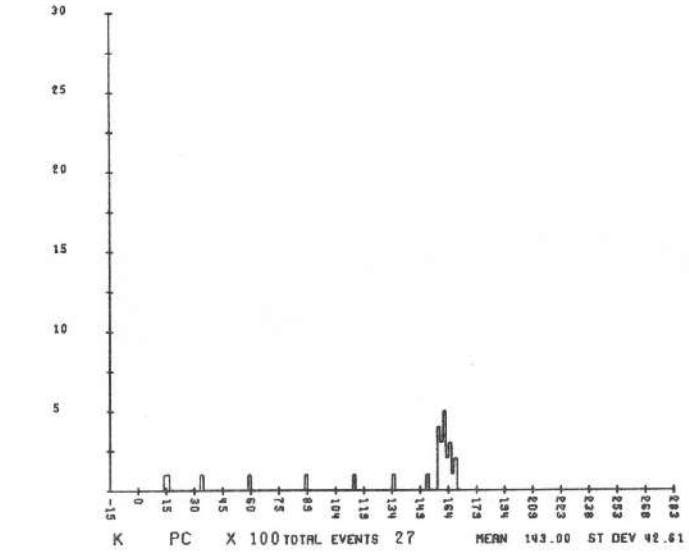




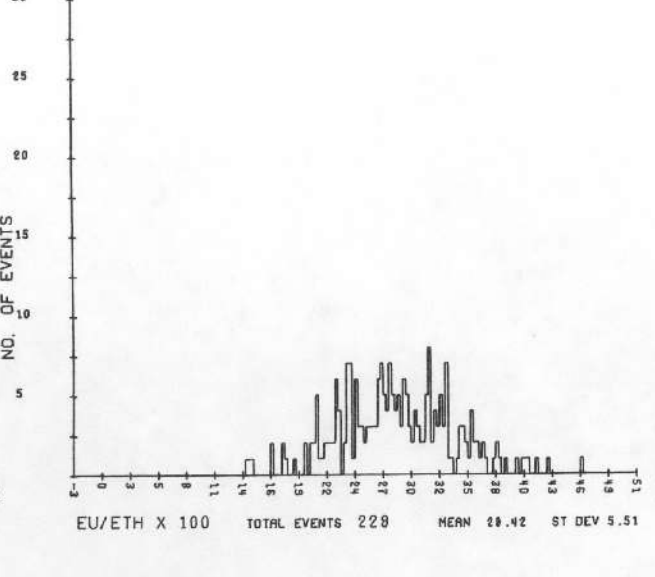
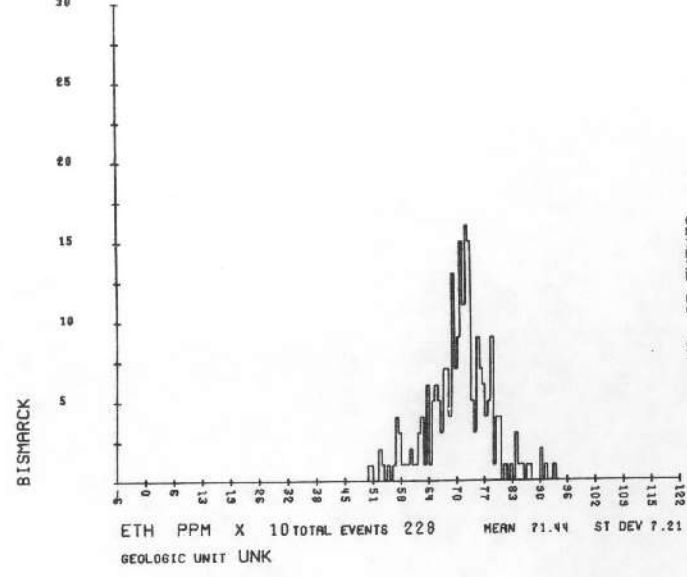
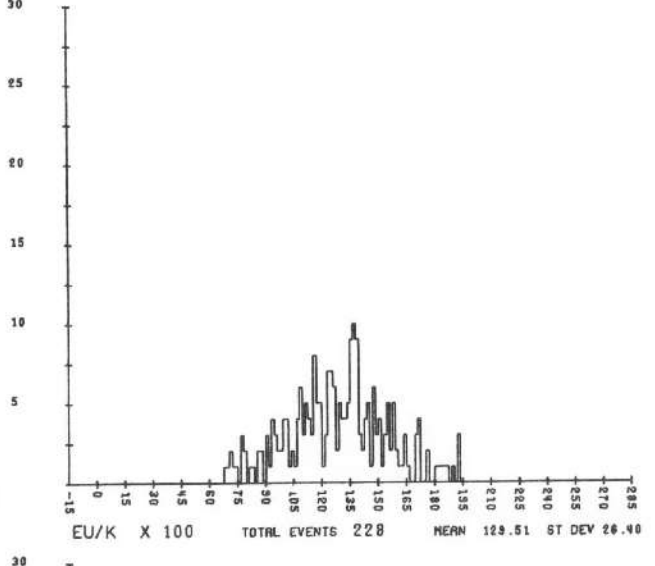
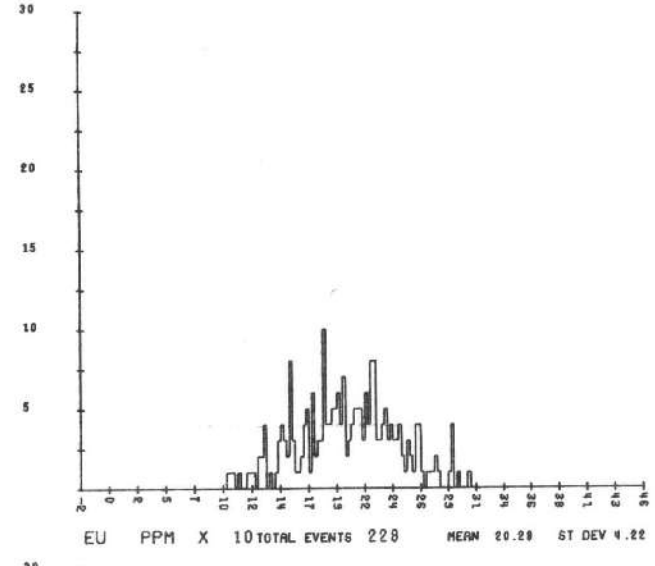
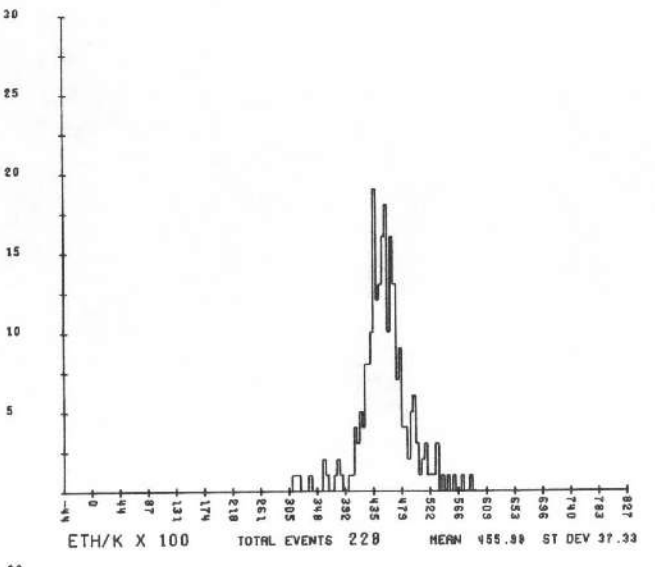
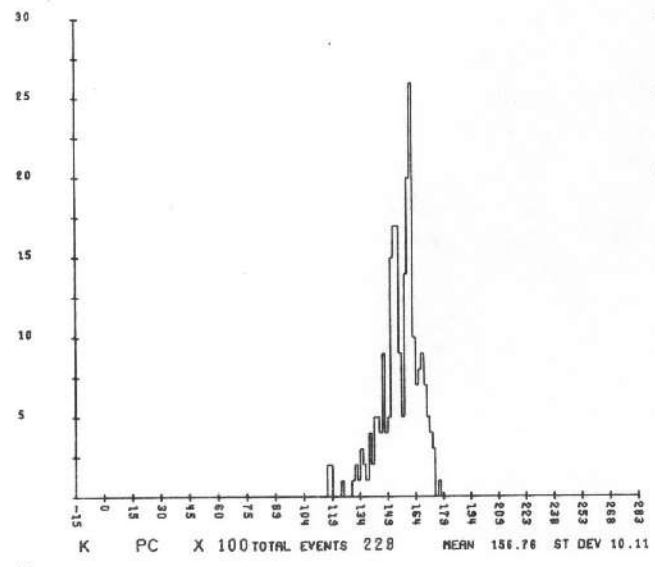




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# SECTION V

GEODATA DATA AQUISITION AND PROCESSING





## SECTION V.

### GEODATA DATA ACQUISITION AND PROCESSING

#### A. DATA ACQUISITION SYSTEM

A brief description of the computer-linked Geodata Data Acquisition System (GDAS), used in the present survey, is presented here. The five primary components of the GDAS, which are mounted aboard a Douglas Super DC-3 aircraft, Figure V.1, are:

- 1) An array of nine (9) 11½" dia. by 4" thick NaI(Tl) detectors;
- 2) a NOVA mini-computer system
- 3) a Collins ALT-50 radar altimeter system;
- 4) a proton precession magnetometer; and
- 5) a Bendix DRA-12C doppler navigation system.

The nine-crystal detector array has been calibrated to measure the gamma radiation spectrum between 0-6 MeV. The contents of the 3 to 6 MeV interval is monitored in order to reduce the contributions of the cosmic events in the 0-3 MeV interval, which is of primary interest in this survey. Eight of the nine detectors are mounted to measure the  $4\pi$  solid angle gamma radiation spectrum emanating from the earth's surface. The ninth detector, which is partially shielded underneath by a 3.5-inch lead plate, is situated to measure the  $^{214}\text{Bi}$  radiation incoming from the upper  $2\pi$  solid angle.

Each crystal detector has an estimated volume of 415.5 cubic inches, resulting in a total volume for the entire  $4\pi$  system of 3324 cubic inches. The estimated volume to velocity ratio for this system is 23.7, where the average speed for the DC3-S is approximately 140 mph.

The energy resolution of the GDAS as calculated from the  $^{137}\text{Cs}$  662 keV photopeak was 10.7%, where each individual crystal was 9.0% or better. Automatic digital gain calibration for the eight detector array and the single detector system was accomplished by stabilizing on the  $^{40}\text{K}$  photopeak data.

The NOVA computer, shown in the system block diagram of Figure V.2, is the control center of the GDAS. The data is gathered by the computer for every one-second period in a manner giving no dead time when readout to the magnetic tapes for storage. Two magnetic tape recorders are used; one to record the total spectral data and the computer tabulated results (LDT), and the other to record only the computer tabulated results (CDT).

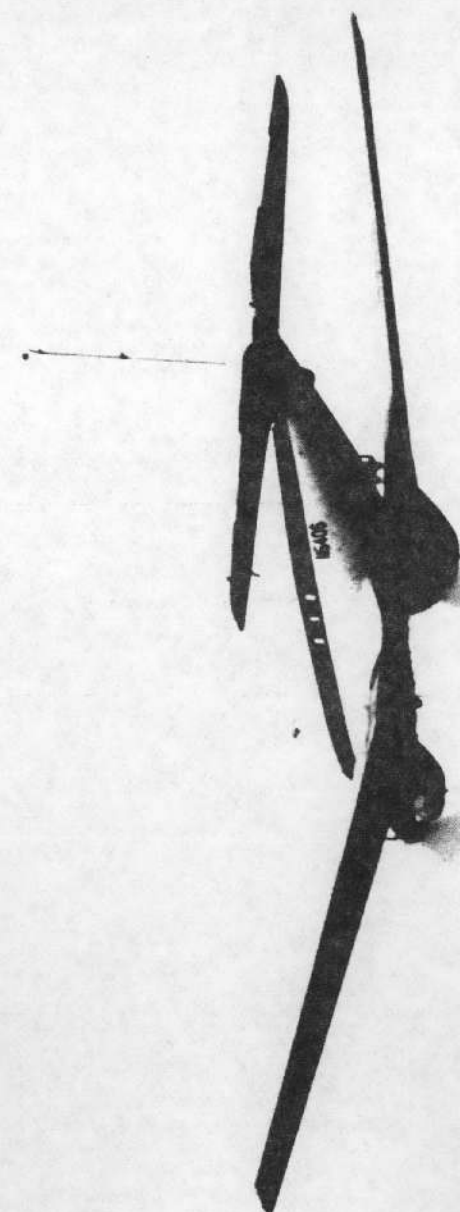


Figure V.1 Survey Aircraft



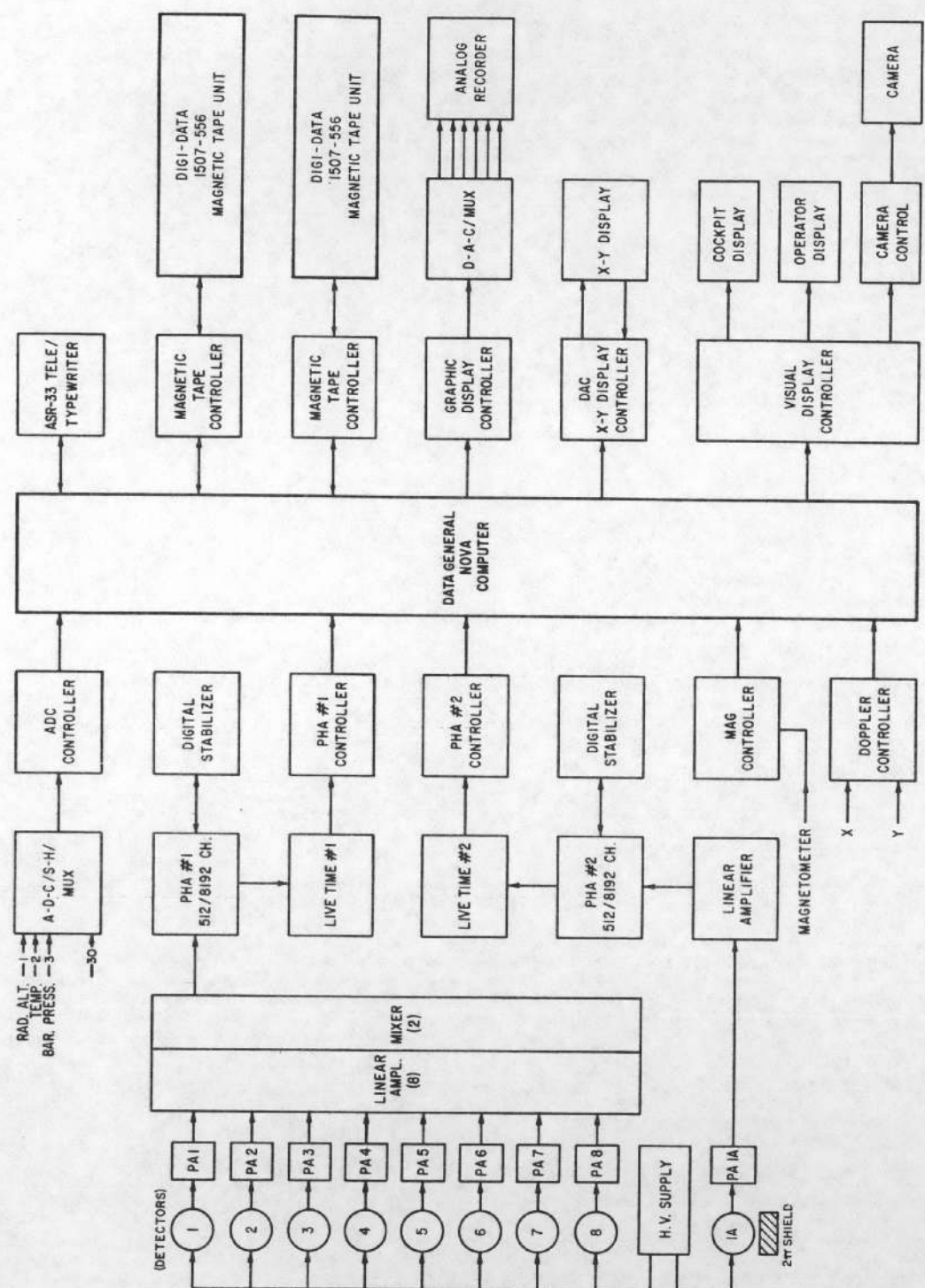


Figure V.2 System Block Diagram

Digital-to-analog conversion of the resultant intensities, their ratios and the magnetic field data are plotted on multi-track paper, allowing immediate examination for anomalous data.

The spectral data from the single detector system gathers and records the  $2\pi$  spectral data every nine seconds. This  $2\pi$  data is necessary to determine the amount of atmospheric  $^{214}\text{Bi}$  radiation in the  $4\pi$  spectral data. A third segment of the computer's core gathers and sums the total  $2\pi$  and  $4\pi$  gamma radiation spectra for each flight line, which can then be plotted as shown in Figure V.3 (EOFL spectrum).

Due to the dependence of the gamma ray data on altitude, a highly accurate radar altimeter is used. The Collins ALT-50 system is designed to make a series of 8 measurements per second, where the resulting altitude is the average.

Since the gathered data are dependent on the current ambient temperature and pressure readings, a Senso-Tek barometric pressure sensor and a Hy-Col thermocouple sensor were used to monitor conditions outside the aircraft.

A proton precession magnetometer sensor, having a 0.25 gamma readout resolution and less than a 1.0 gamma noise envelope, is sampled every second to yield a measurement of the total intensity of the earth's magnetic field below the aircraft. The sensor is carried as a "bird" on a 100-foot cable in order to minimize the magnetic effects of the aircraft.

A Bendix DRA-12C navigation system with a  $\pm 100\text{th}$ /nautical mile accuracy provides a doppler navigation cross-track and along-track analog signal to be recorded each second onto magnetic tape. Two other methods are used to properly locate the aircraft's track: visual sightings and photography. The first method is employed by the navigator, who marks flight map location reference points with computer-displayed record numbers. The second method is a 35mm film that records a continuous, recoverable track which has a 20% overlap/frame at an elevation of 400 feet.

There are three basic operating modes of the GDAS that the operator can manipulate:

- 1) CALIBRATE, which allows proper gain calibration for the detectors;
- 2) OPERATE, which allows data to be collected, summed and recorded; and
- 3) PLAYBACK, which allows the operator to examine the newly acquired data.



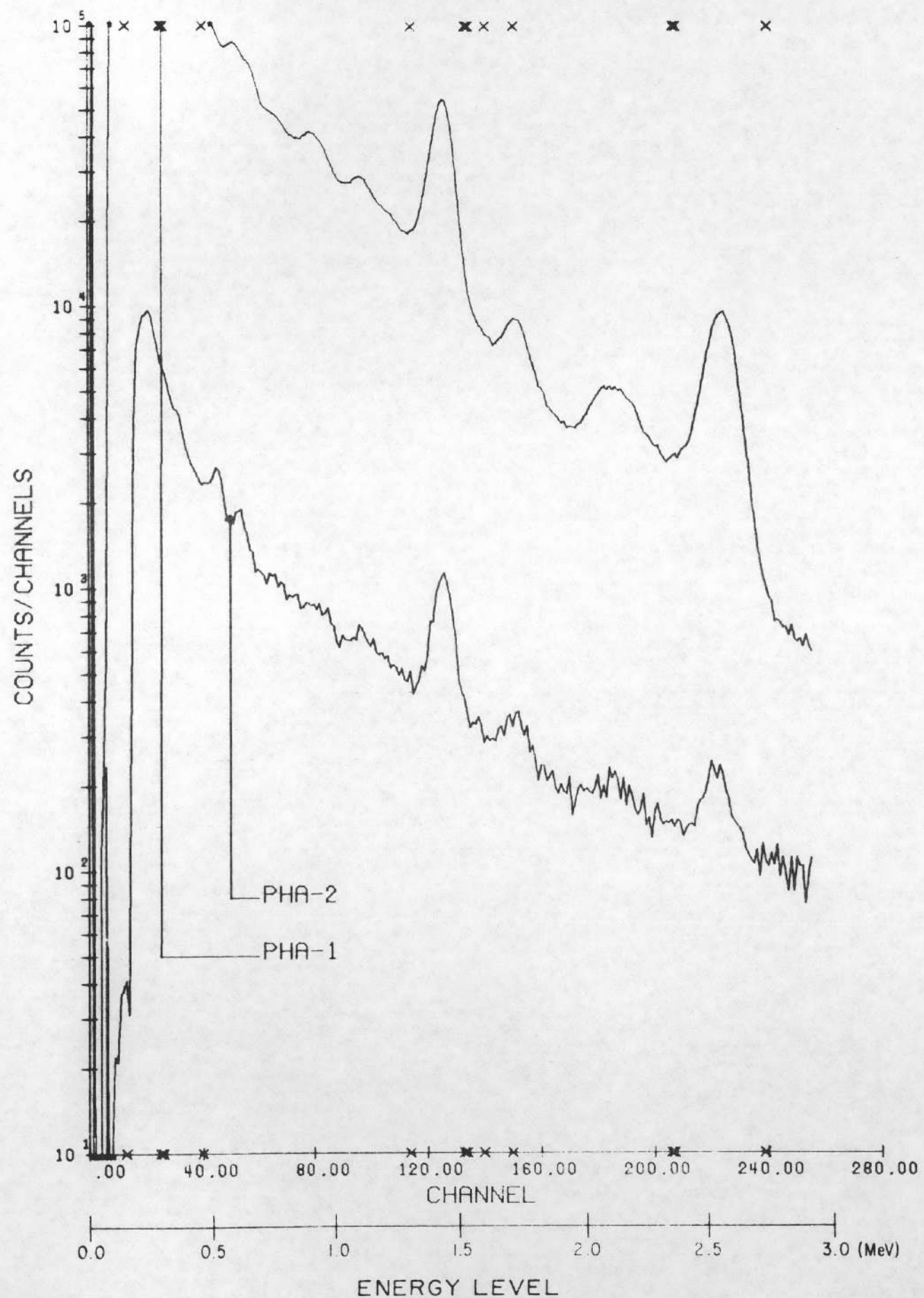


Figure V.3 Typical End-of-Flight-Line Spectral Plot  
V-5

## B. DATA PROCESSING

### 1. Data Reduction

The field data tapes produced by the data acquisition system (Section V.A) contain the  $4\pi$  and  $2\pi$  gamma radiation spectra, measured between 0 to 6 MeV. The resulting gamma ray spectra are composite spectra of the several different isotopes that emit gamma rays within the detectors' energy range. The method used in this work to determine the concentrations of the different isotopes monitored is discussed in this section.

In this work, there are four different isotopes which contributed to the resultant composite spectra under consideration. In order of the highest to lowest energy emitter, they are: cosmic,  $^{208}\text{Tl}$ ,  $^{214}\text{Bi}$  and  $^{40}\text{K}$  counting rates.

Isotope	Energy Interval (MeV)
Cosmic	3.0 to 6.0
$^{208}\text{Tl}$	2.410 to 2.796
$^{214}\text{Bi}$	1.661 to 1.860
$^{40}\text{K}$	1.357 to 1.556

Due to the occurrence of Compton scatter at all gamma ray energy intervals, a  $4 \times 4$  matrix method approach is used to "spectrally strip" the group summed counting rates into their individual counting rates attributed only to the isotope associated with that energy interval.

This matrix method approach is theoretically applicable to a spectrum containing any number of isotopic gamma rays. For convenience, the four isotopes will be denoted as: COS, TL, BI and K. The channel group sum for each energy interval can be considered to consist of fractional components of each of its constituents. For instance, one can write for the TL channel group sum:

$$a\text{COS} + 1.0\text{TL} + f\text{BI} + 0.0\text{K} = \text{MTL}$$

where MTL is the channel group sum count;

and the coefficients, which are known as Compton coefficients, for each variable represent the responses of the data gathering system to each isotope over the entire energy spectrum.

Similarly, equations can be written for the energy interval group sums for MCOS, MBI and MK, as shown below in matrix notation by



$$\begin{bmatrix} 1.0 & 0.0 & 0.0 & 0.0 \\ a & 1.0 & f & 0.0 \\ b & \alpha & 1.0 & g \\ c & \beta & \gamma & 1.0 \end{bmatrix} \begin{bmatrix} \text{COS} \\ \text{TL} \\ \text{BI} \\ \text{K} \end{bmatrix} = \begin{bmatrix} \text{MCOS} \\ \text{MTL} \\ \text{MBI} \\ \text{MK} \end{bmatrix}$$

where each element of the 4 x 4 matrix is a Compton coefficient. By inverting the 4 x 4 matrix and multiplying on the left by the channel group sum matrix, the resulting column matrix, whose elements are COS, TL, BI and K, represents the counts in each energy interval attributed only to the indicated isotope source.

Table V.1 contains the data reduction parameters, coefficients and backgrounds used in this survey. The listed Compton coefficients were determined from data acquired during high altitude flights and from "known" test pad data concentrations in Grand Junction, Colorado.

The resulting reduced counting rates for COS, TL, BI and K must then be normalized with respect to the measured live time counting rate of the data acquisition system. This is necessary in order to restore the linear relationship between the photopeak counts and the source's intensity. This procedure is accomplished by dividing the reduced counts by the live time, LTC1:

thus,

$$\begin{aligned} \text{COS1} &= \text{COS/LTC1} \\ \text{TL1} &= \text{TL/LTC1} \\ \text{BI1} &= \text{BI/LTC1} \\ \text{K1} &= \text{K/LTC1} \end{aligned}$$

The next step in the data processing involves the subtraction of the background counts present on board the aircraft. The background counts, which exist in the aircraft and its equipment, are determined from high altitude data where the data acquisition is free from all ground sources and atmospheric  $^{214}\text{Bi}$  contamination. The background counts, denoted as  $B_{\text{TL}}$ ,  $B_{\text{BI}}$  and  $B_{\text{K}}$ , used in this work are listed in Table V.1. During the processing, the backgrounds are checked by observing the resulting counting rates over large bodies of water, where the rates would have near-zero intensities. The gross count's background counting rate,  $B_{\text{GC}}$ , over channels 35-239, is also given in Table V.1.

After the backgrounds have been subtracted from the live time corrected photopeak counts, thus

$$\overline{\text{TLI}} = \text{TL1} - B_{\text{TL}}$$

$$\overline{\text{BII}} = \text{BI1} - B_{\text{Bi}}$$

$$\overline{\text{KI}} = \text{K1} - B_{\text{K}}$$

The resulting counting rates for  $\overline{\text{TLI}}$  and  $\overline{\text{KI}}$  represent the counts contributed only by the sources below the aircraft on the earth's surface. In the case of  $\overline{\text{BII}}$ , an additional source of  $^{214}\text{Bi}$  radiation, which is caused by atmospheric  $^{214}\text{Bi}$ , BIAIR, is still eminent.

The  $2\pi$  detector system data is used to determine the magnitude of the BIAIR to be subtracted. Since the predominate variable source affecting the  $2\pi$  detector is the atmospheric  $^{214}\text{Bi}$ , it is possible to utilize most of the  $2\pi$  spectrum in the BIAIR determination, and thereby produce some improvement in the statistical error. The energy interval used for the  $2\pi$  crystal is between 1.05 to 2.79 MeV. Within this interval, the aircraft's background,  $B_{2\pi}$ , and its Compton coefficient,  $C_{2\pi}$ , have been determined from the high altitude data. (See Table V.1.)

The BIAIR associated with the unshielded detector array is determined, using the shielded detector by the relation:

$$\text{BIAIR} = \frac{G(x)}{(1 - k_2 G(x))} [\text{VC} - C_{2\pi} \cdot \text{COS1} - B_{2\pi} - \text{RVALM}]$$

where

- $G(x)$  is the relationship between the  $4\pi$  and  $2\pi$  solid angles, the channel group sums and the number of detectors in the detector arrays;
- $\text{VC}$  is the  $2\pi$  total count group sum of channels 91-239, c/s;
- $\text{COS1}$  is the  $4\pi$  cosmic count, greater than 3.0 MeV, c/s;

and,

$$\text{RVALM} = k_1 \overline{\text{TLI}} + k_2 \overline{\text{BII}} + k_3 \overline{\text{KI}}$$



where  $k_1, k_2, k_3$  are constant factors that correct for the penetration/spill of the emanated surface radiation. These penetration/spill constants are dependent on the amount of lead shielding used on the  $2\pi$  crystal. The values used in this work are listed in Table V.1.

$\overline{TLI}$ ,  $\overline{BII}$  and  $\overline{KI}$  have already been defined as the  $4\pi$  reduced data counting rates, c/s.

Finally, the  $^{214}\text{Bi}$  counting rate caused only by the surface sources is given by

$$\text{BISUR} = \overline{BII} - \text{BIAIR}$$

Briefly summarizing,  $\overline{TLI}$ , BISUR and  $\overline{KI}$  are the counting rates as measured at the height of the aircraft. All interfering counts from cosmic, backgrounds and atmospheric  $^{214}\text{Bi}$  have been removed.

Since the various counting rates are dependent upon the height of the aircraft above the surface terrain, it is necessary to correct the associated isotope's counting rate to an altitude of 400 feet above the surface terrain. This is accomplished through the equations indicated below:

$$\text{TLS} = \overline{TLI} \cdot e^{-\mu_1(400 - \frac{\rho}{\rho_0} x)}$$

$$\text{BIS} = \text{BISUR} \cdot e^{-\mu_2(400 - \frac{\rho}{\rho_0} x)}$$

$$\text{KS} = \overline{KI} \cdot e^{-\mu_3(400 - \frac{\rho}{\rho_0} x)}$$

and

$$\text{GC(gross count)} = (\overline{\text{GC}} - B_{\text{GC}} - S \cdot \text{BIAIR}) \cdot e^{-\mu_4(400 - \frac{\rho}{\rho_0} x)}$$

where

$\overline{\text{GC}}$  is the live time corrected gross count, channels 35-239,

S is the ratio of the BI data, channels 35-239 to channels 143-159,

$B_{\text{GC}}$  is the gross count background,

TLI, BIS, KS are the respective photopeak's counting rates at 400 feet;

$\rho_0$  is the air density at standard temperature and pressure; 0.001293 gm/cc

$\rho$  is the air density at the time the survey data was flown;

$\mu_1, \mu_2, \mu_3, \mu_4$  are the respective linear attenuation coefficients;

x is the aircraft's height above the surface terrain in feet.

The attenuation coefficients and other constants used in the altitude normalization are listed in Table V.1.

After each flight line of data has undergone the above data reduction, the average values for each radiation variable and variable ratios for each of the flight lines were plotted to demonstrate the consistency of the average values and that a smooth flow continues from day to day, and from the start to the finish of each day.

Diurnal variations of the magnetic field base station intensity were measured and applied to the field data. (See Section II.D and Appendix I.C.) The magnetic heading corrections for the aircraft and its equipment used in this survey were determined by flying a predetermined path at a survey altitude in first an east to west direction, then in a west to east direction. The same procedure is used on a north to south path. Based on the data obtained in this fashion, see Table V.1, the heading corrections were removed from all the data. The magnetic field data were then IGRF corrected to give the residual magnetic field. The International Geomagnetic Reference Field subtracted was provided by the U.S. Geological Survey with reference to the IAGA Bulletin #38, "Grid Values and Charts by the IGRF 1975.0", National Technical Information Service Report #PB265483.

The system sensitivities at 400 feet used in this survey are shown in Table V.1.

## 2. Description of Data Processing

The processing flow chart representative of the work performed in this survey is shown in Figure V.4.

As stated in Section V.A., the original field data tapes were recorded to contain the various tag words,  $4\pi$  and  $2\pi$  spectral



TABLE V-1: DATA REDUCTION PARAMETERS AND CONSTANTS - N540S - 1980

AIRCRAFT BACKGROUNDS				COSMIC CORRECTION RATIOS	
Detector	Parameter	Window	Value (CPS)	Parameter	Value
Terrestrial (4π)	B <sub>K</sub>	Potassium	29.98	c	0.2069
	B <sub>Bi</sub>	Uranium	9.40	b	0.1651
	B <sub>Tl</sub>	Thorium	5.83	a	0.2202
	B <sub>GC</sub>	Gross	286.69	-	-
Atmospheric (2π)	B <sub>2π</sub>	Uranium	8.33	C <sub>2π</sub>	0.2232

DERIVED STRIPPING COEFFICIENTS AND RATIOS			
Coefficient	Value	Coefficient	Value
α	0.2755	k <sub>1</sub>	0.030
β	0.4058	k <sub>2</sub>	0.0
γ	0.8595	k <sub>3</sub>	0.0
f	0.0693	S	17.5
g	0.0156	-	-

LINEAR ABSORPTION COEFFICIENTS		
Radio Element	Parameter	Value (x10 <sup>-3</sup> per ft.)
Potassium	μ <sub>1</sub>	2.448
Uranium	μ <sub>2</sub>	1.329
Thorium	μ <sub>3</sub>	1.899
Gross	μ <sub>4</sub>	1.430

MAGNETIC HEADING CORRECTION	
Flight Direction	Correction (gammas)
West to East	+3.56
East to West	-3.56
North to South	-1.0
South to North	+1.0

RADIOELEMENT	SYSTEM SENSITIVITIES AT 400 FEET
Potassium (cps/%K)	98.05
Uranium (cps/ppm eU)	13.52
Thorium (cps/ppm eTh)	7.15

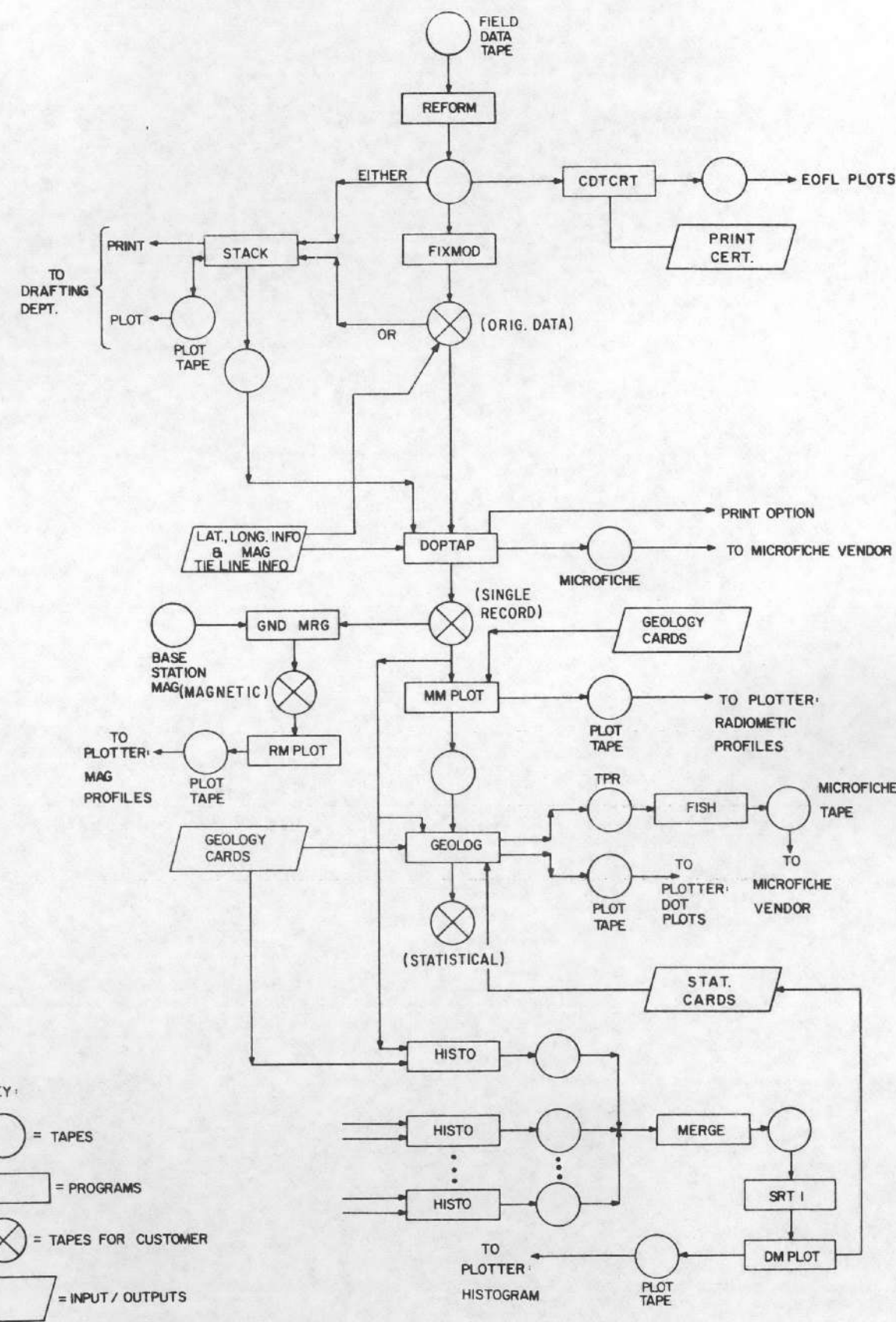


Figure V.4 Data Reduction Flow Chart



data and the trailer record sums for each flight line. The purpose of the REFORM program is to sum the raw spectral data (LDT) into the proper group sum energy intervals for each second for each line. The CDTPLT program is a data certification program that produces the EOFL spectral plots, Figure V.3, and profiles of each of the channel group sums, which are plotted as a function of each line's record numbers.

A brief summary of each program and its uses is given below:

<u>PROGRAM</u>	<u>FUNCTION</u>
REFORM	Produces energy group sums and EOFL spectra.
FIXMOD	Primary processing for "spectral stripping" matrix reduction, live time normalization, background and BIAIR subtraction, and altitude corrections.
STACK	Flight path recovery to produce record location map at a scale of 1:250,000.
DOPTAP	Single record processing with latitude/longitude positioning, IGRF and single point statistical adequacy computations, and magnetic heading corrections.
GNDMRG	Merges aircraft magnetometer and ground magnetometer in proper time sequence and applies diurnal corrections to the field data.
VARPLT	Produces radiometric and magnetic stacked profile plot tapes.
HISTO, MERGE, and SORT1	Preliminary programs to prepare/sort data as a function of geologic type for the entire area.
HISPLT	Produces geological histograms, mean and standard deviation tables, and plot tape for the entire area.
GEODOT	Produces plot tape for standard deviation "dot plots" related to geologic type.
FICHE	Produces average record and single record reduced data listings and microfiche tapes, which are sent to microfiche vendor.
CUSTOMER	Produces all customer required tapes.

### 3. Data Presentation

The surveyed area was positioned geographically to completely cover the specific National Topographic Map. Each topographic map has been used as the flight base, and sufficient geographical and 15' location information has been shown. The flight line pattern has been superpositioned onto these created base maps, where the standard deviation levels for each independent variable and each ratio of these variables have been plotted (NGRMS), based on the data contained within the total map area. Every fifth data point along each map line has its standard deviation value shown at the location of that value. Therefore, there are six NGRMS sheets which indicate the location and magnitude of anomalous data.

The multivariable map line profile, which represents 10 variables as a function of their latitude and longitude location for each line, is presented at a scale of 1:500,000. Each profile presents:

1. Aircraft altitude above the surface
2. eTh ( $^{208}\text{Tl}$  from  $^{232}\text{Th}$  decay series)
3. eU ( $^{214}\text{Bi}$  from  $^{238}\text{U}$  decay series)
4. K ( $^{40}\text{K}$  from natural potassium)
5. BIAIR (atmospheric  $^{214}\text{Bi}$ )
6. Residual magnetic field
7. Gross count (greater than 400 keV)
8. eU/eTh ( $^{214}\text{Bi}/^{208}\text{Tl}$ ) ratio
9. eU/K ( $^{214}\text{Bi}/^{40}\text{K}$ ) ratio
10. eTh/K ( $^{208}\text{Tl}/^{40}\text{K}$ ) ratio
11. Geologic data, including aircraft flight path

The residual magnetic field map line profile, which represents five variables as a function of their latitude and longitude location for each line, plus geologic data at a scale of 1:500,000, is presented as:

1. Aircraft altitude
2. Atmospheric temperature
3. Atmospheric pressure
4. Residual magnetic field data
5. Magnetic field base line station data
6. Geological data, including aircraft flight path

The output of these various computations supplies, beyond two profile sets, the following data:

- \* Histograms of the radiation data distribution within each geologic unit.



- \* Histograms of the average velocity distribution for each one-second record for each map and tie line.
- \* Histograms of the average altitude distribution for each one-second record for each map and tie line.
- \* Tables giving the average radiation concentration of each geologic unit for each flight line.
- \* Average radiation concentration for each variable as a function of flight line, including the atmospheric  $^{214}\text{Bi}$ .
- \* Set of maps showing the standard deviation data as a function of location and radiation variable.
- \* Printer plot contour maps of eTh, eU, K, eU/K, eU/eTh, eTh/K and the magnetics at a scale of 1:500,000.

#### 4. Statistical Analysis Procedures

It is necessary to exclude from the statistical analysis all variables which have too low a counting rate to be statistically valid, and data which were obtained at altitudes above 1,000 feet. To this end, a statistical adequacy test was run on all data for each data record. If a given value of T $\ell$ , Bi or K failed the test, that variable value, and any ratio value associated with it, were not used in the statistical determinations of mean and standard deviation values. In addition, such values are indicated on the radiometric profiles by a vertical (tick) mark along the base line for the variable, and are flagged in the single record and averaged record listings (microfiche). The ratio values are set to zero in the Radiometric Profile Plots. The flags in the listings appear under the heading AKUT for altitude,  $^{40}\text{K}$ ,  $^{214}\text{Bi}$  and  $^{208}\text{Tl}$ , respectively. The flags are zero for statistically valid data, and one for rejected data in the case of K, U and T. For altitude (A), a zero indicates altitudes to 700 feet, a one (1) indicates altitudes between 700 and 1,000 feet, and a two (2) indicates altitudes above 1,000 feet.

The tests used to reject data were as follows:

$$\begin{array}{lll}
 (1) \quad \overline{T\ell I} < 1.5 & \sqrt{\overline{T\ell w} - \overline{T\ell I}} & = 1.5\sigma T \\
 (2) \quad \text{BISUR} < 1.5 & \sqrt{\overline{Bi w} - \text{BISUR}} & = 1.5\sigma B \\
 (3) \quad \overline{KI} < 1.5 & \sqrt{\overline{K w} - \overline{KI}} & = 1.5\sigma K
 \end{array}$$

where the "w" subscript refers to the respective window counting rates from the raw data and  $\overline{T\ell I}$ , BISUR and  $\overline{KI}$  have previously been defined. If any of the above inequalities were true, the associated variable was flagged, and that value was rejected in all statistical determinations.

The values of the radicals in the above equations, which are indicated as  $\sigma T$ ,  $\sigma B$ ,  $\sigma K$  and the barred values, were calculated on the basis of a single record value for determining flags in the single record listings and the 7-point weighted values for determining flags in the averaged records listings.

The mean value and standard deviations were calculated assuming the data to have a normal distribution within a geologic type. The equation used in determining the variance is:

$$\sigma^2 = \frac{1}{N-1} \left\{ \sum_{i=1}^N x_i^2 - N\bar{x}^2 \right\}$$

where N is the number of statistically valid samples for a given geologic type,  $x_i$  is the value of the variable for sample number i, and  $\bar{x}$  is the mean value of the variable for the geologic type. Values from the entire survey of the area are used in these computations.



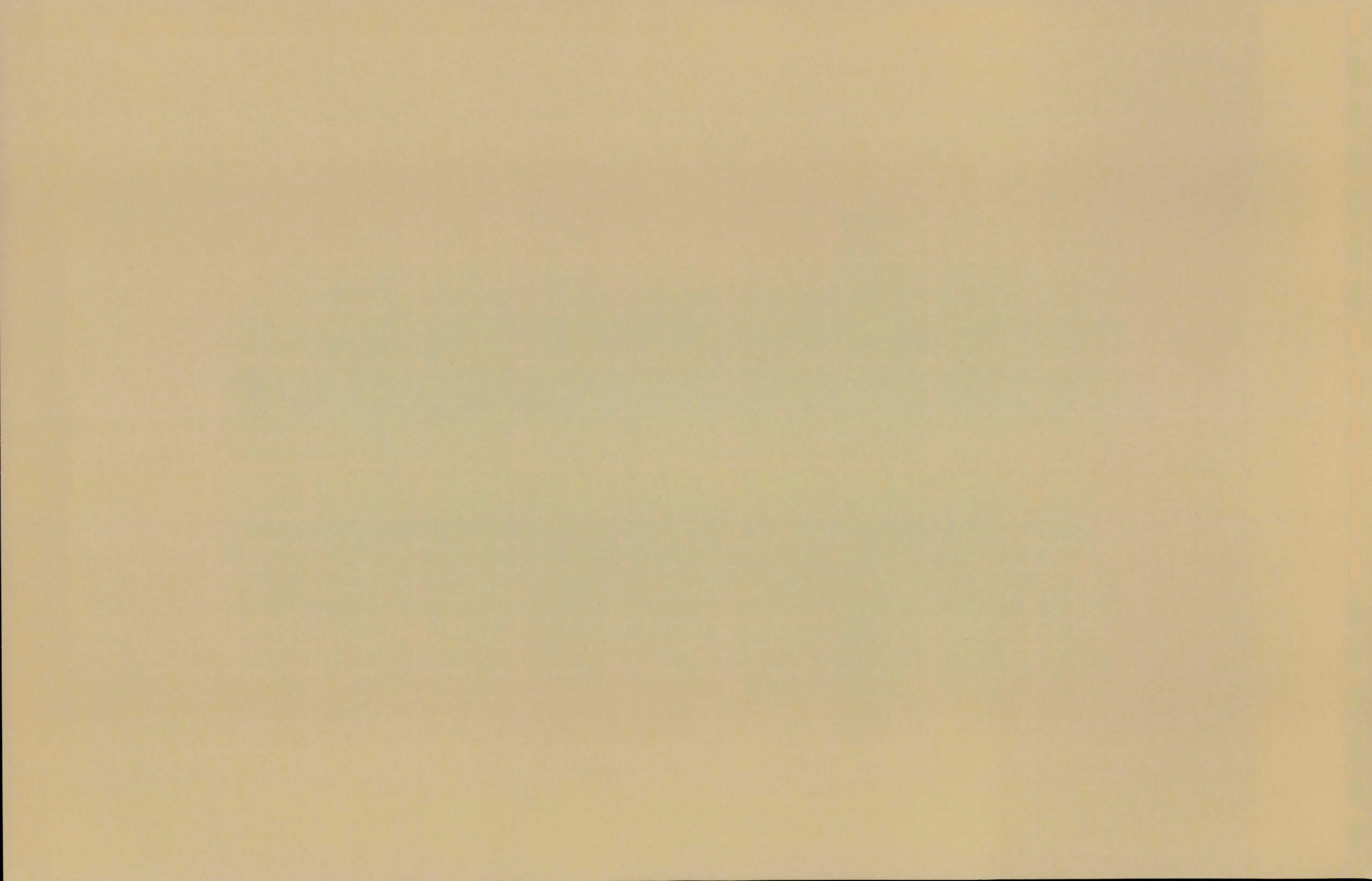
# APPENDICES

I PRODUCTION SUMMARY

II TAPE FORMAT STATEMENTS

III COMPUTER LISTINGS

IV LINE PRINTER CONTOURS







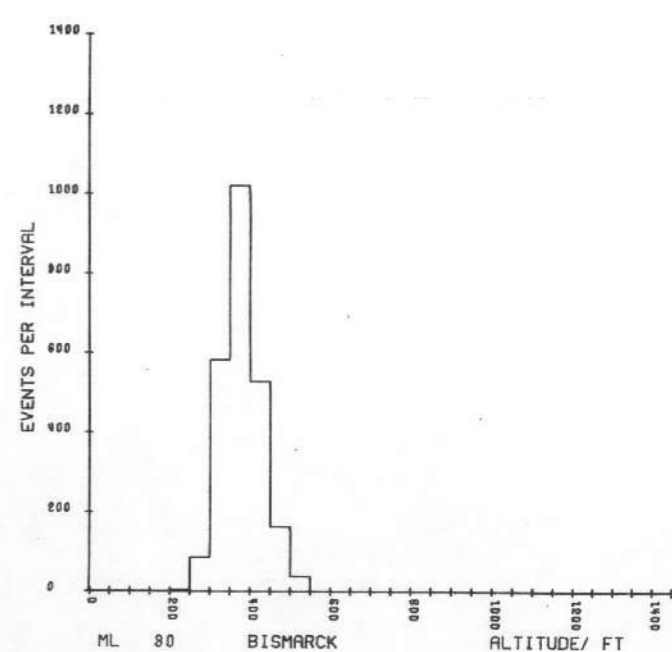
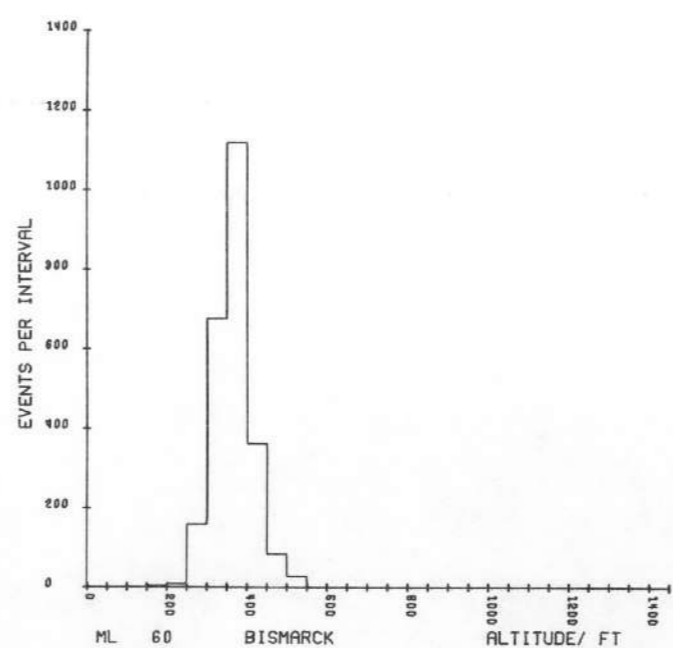
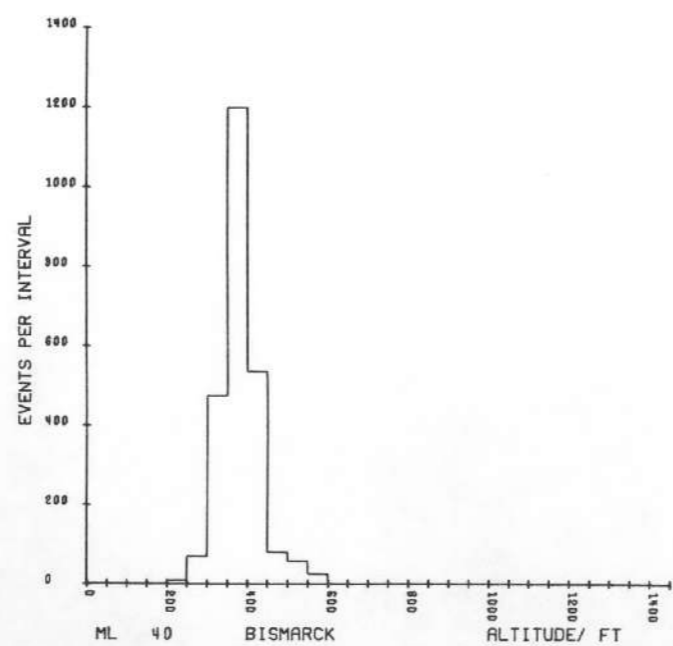
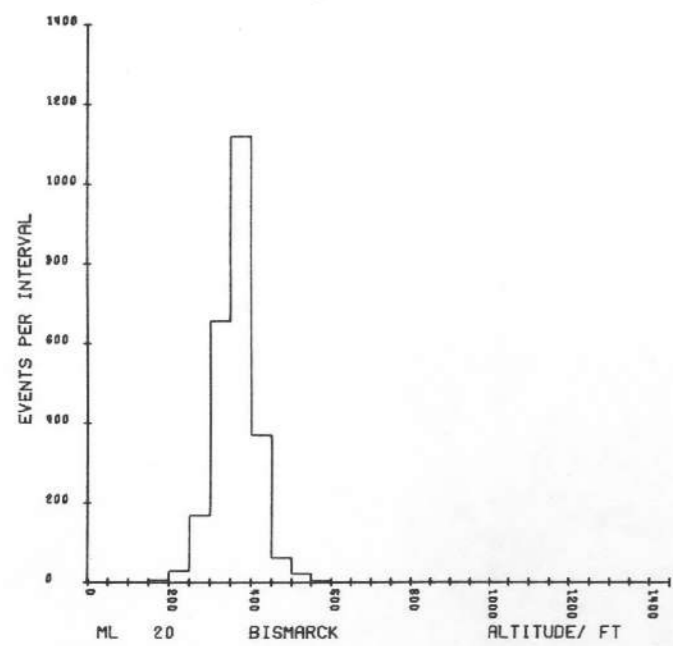
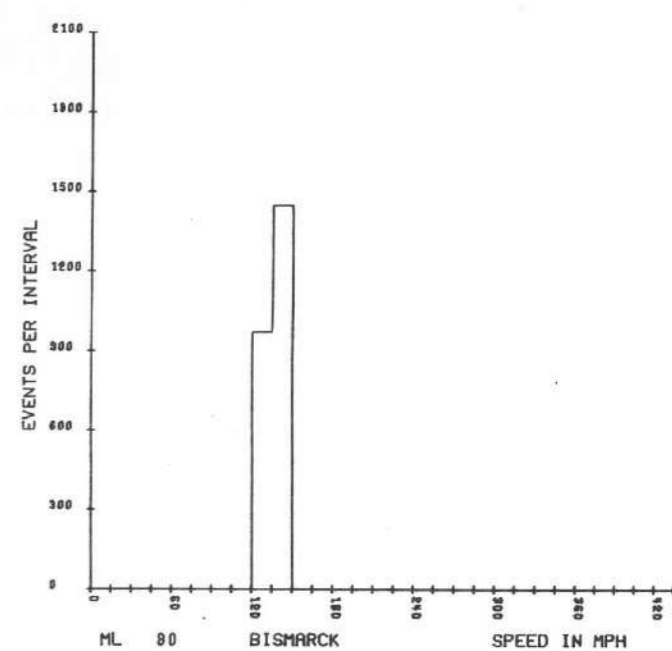
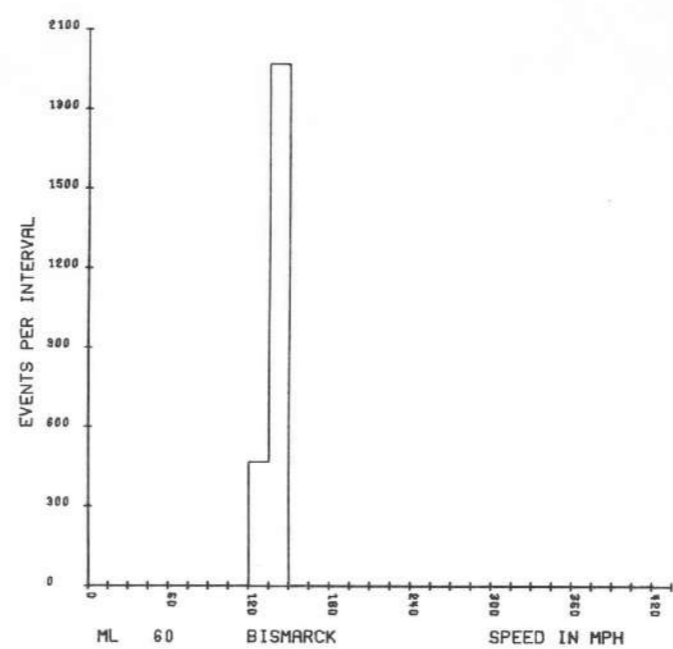
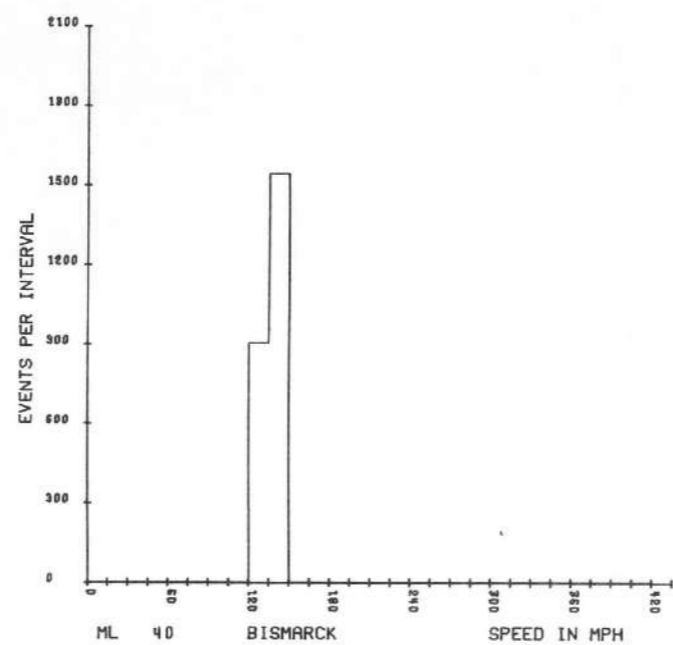
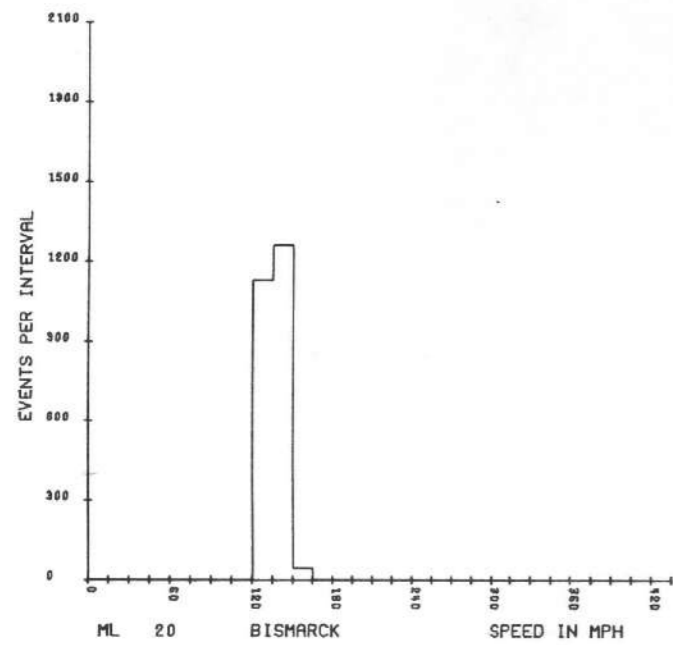
## AI.C DIURNAL CORRECTIONS TO LINE DATA

LINE	DIURNAL CORRECTIONS IN GAMMAS	LINE	DIURNAL CORRECTIONS IN GAMMAS	LINE	DIURNAL CORRECTIONS IN GAMMAS	AI.D.	EXPLANATORY NOTES
ML 240	15	ML 160	-49	ML 80	17		No difficulties were encountered during the processing of the Bismarck quad.
ML 220	23	ML 140	26	ML 60	3		
ML 200	23	ML 120	23	ML 40	9		
ML 180	-19	ML 100	22	ML 20	-12		
TL 5020	-11	TL 5060	-6	TL 5100	-26		
TL 5040	1	TL 5080	-13	TL 5120	-30		

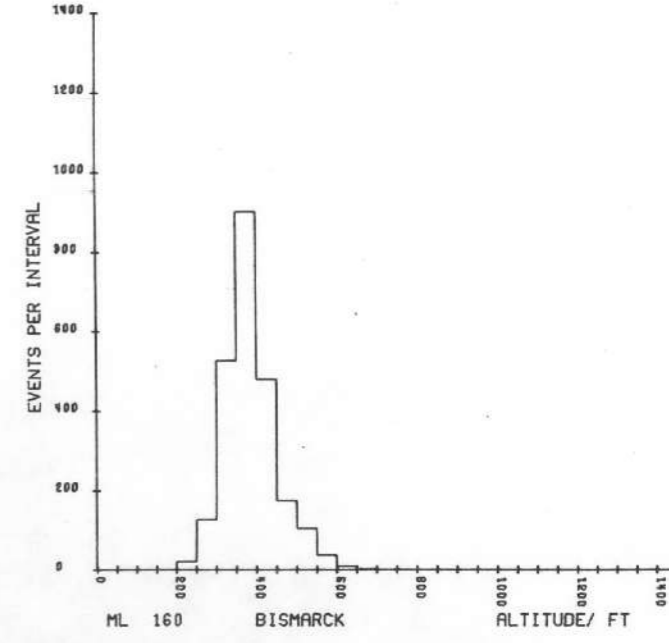
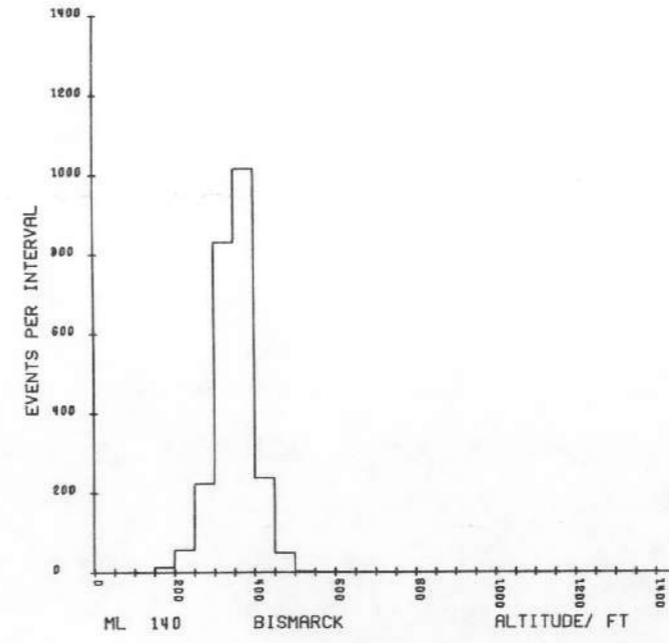
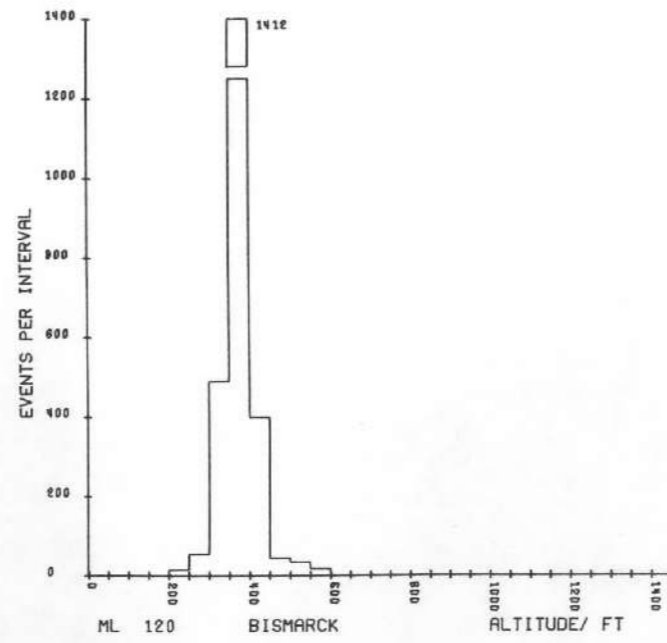
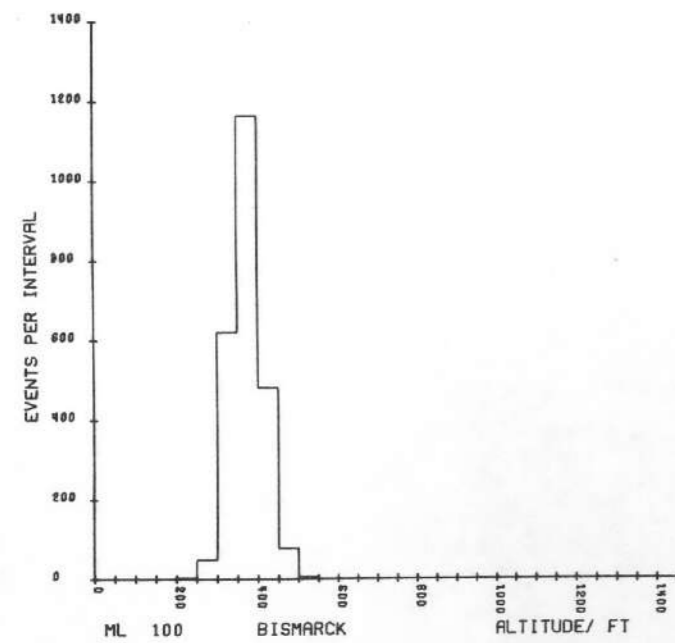
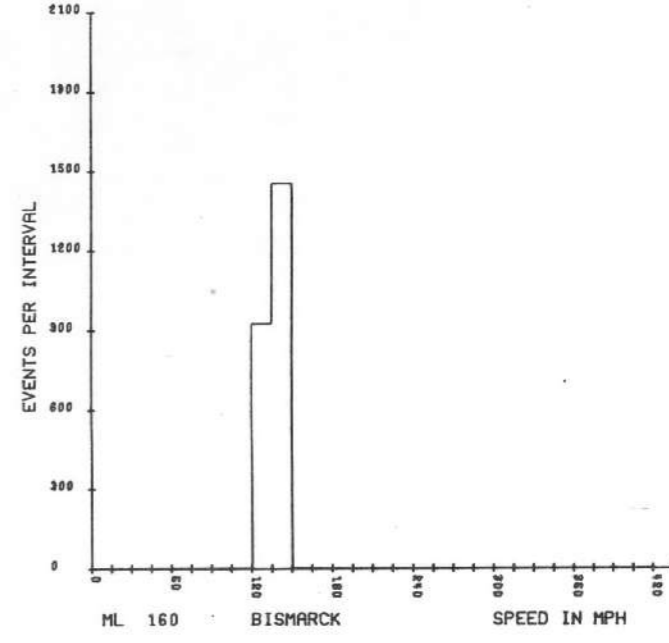
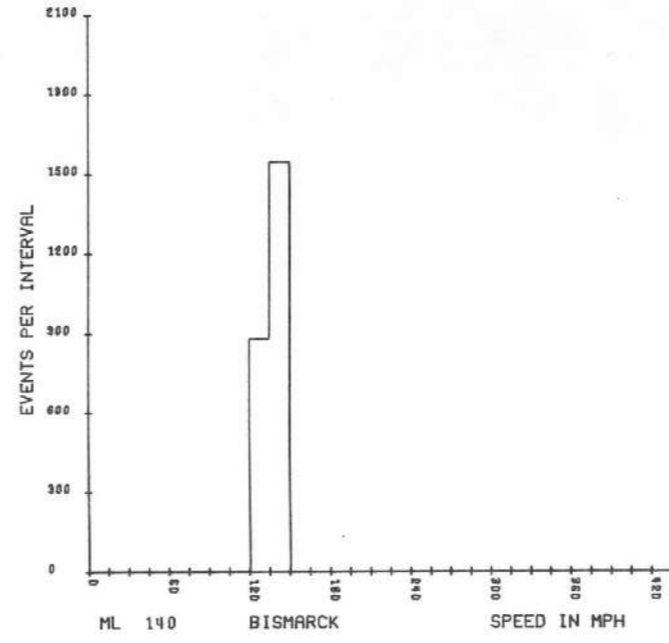
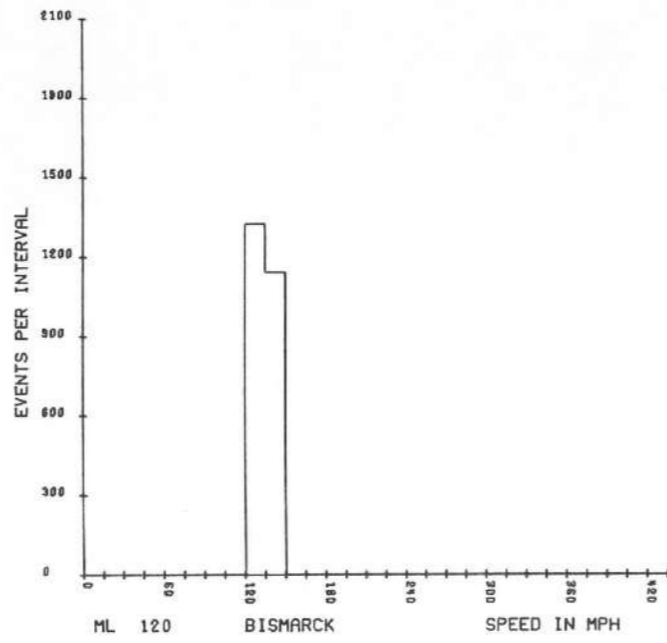
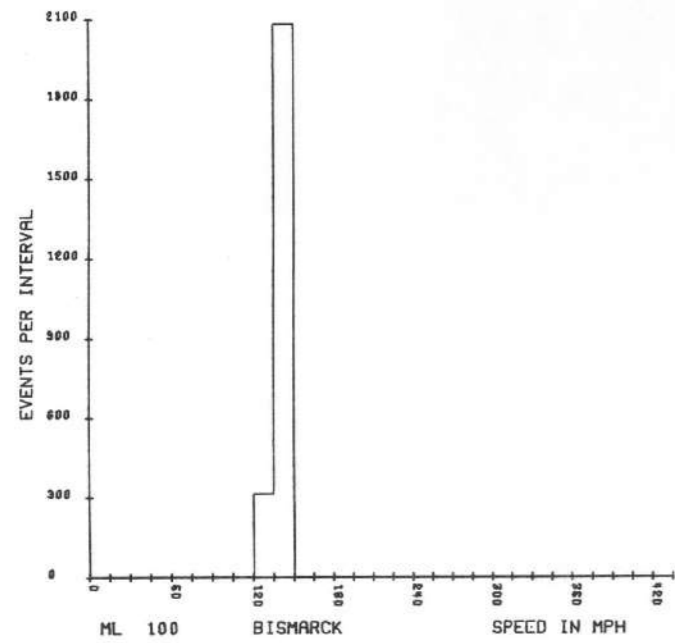


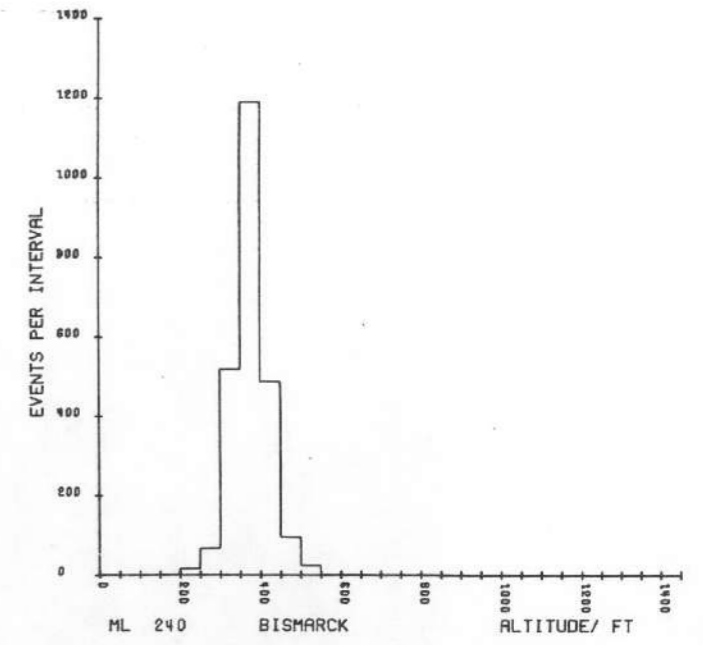
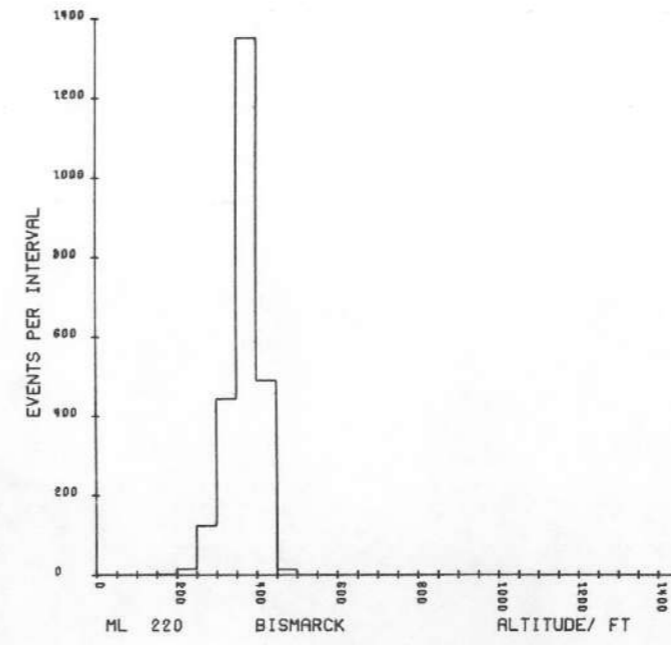
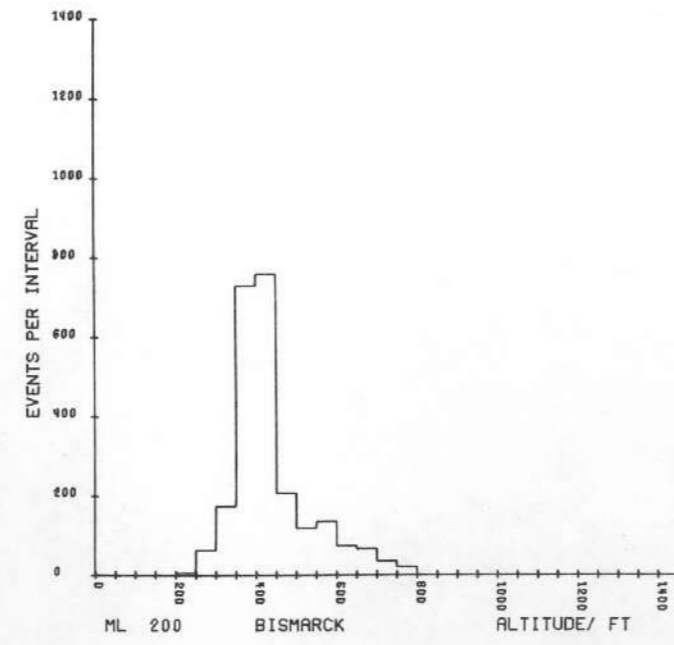
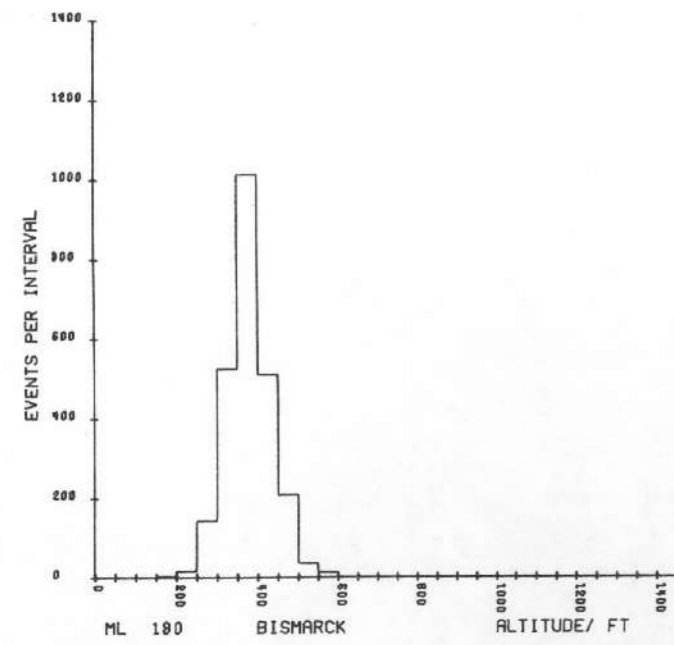
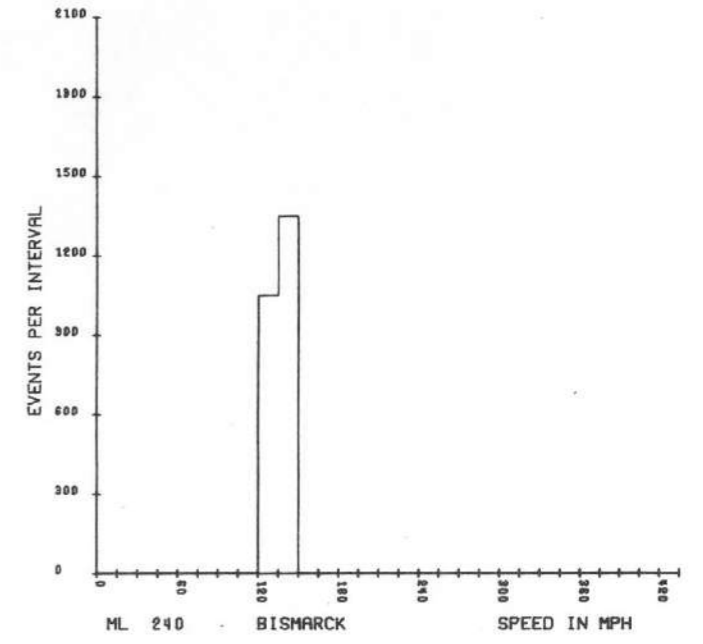
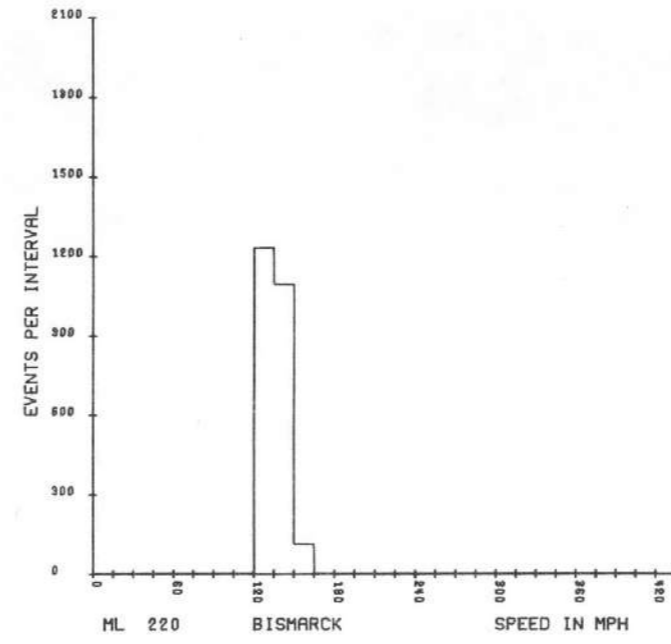
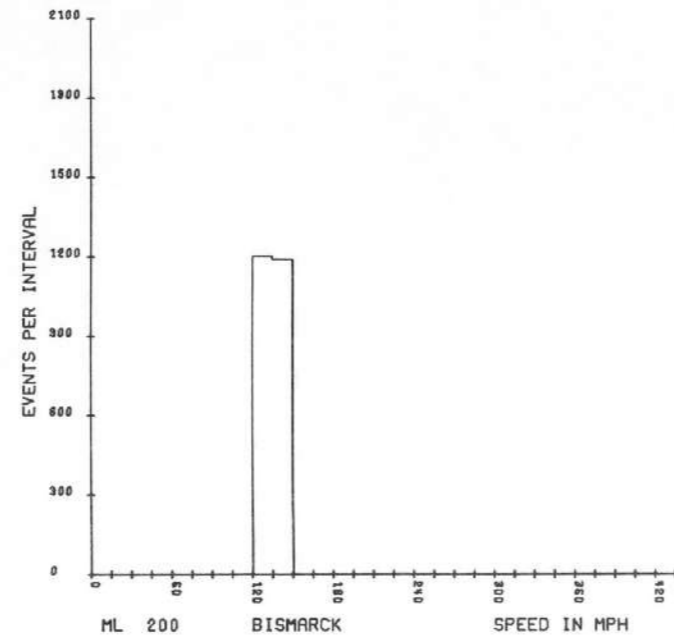
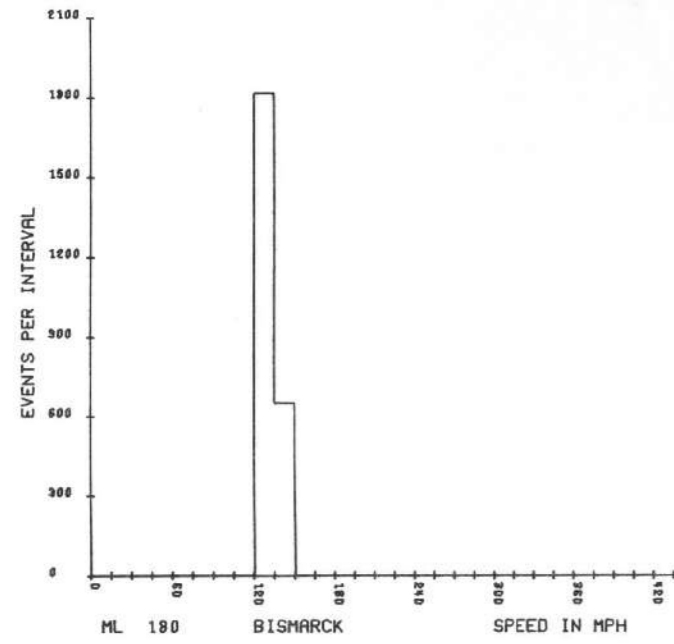
## AI.E AVERAGE SPEED AND ALTITUDE DATA SUMMARY

LINE	AVERAGE SPEED (MPH)	ALTITUDE (FEET)	LINE	AVERAGE SPEED (MPH)	ALTITUDE (FEET)
ML 20	143	389	ML 200	142	461
ML 40	144	407	ML 220	143	395
ML 60	147	391	ML 240	143	401
ML 80	144	404	TL 5020	147	389
ML 100	148	398	TL 5040	147	401
ML 120	142	400	TL 5060	144	472
ML 140	145	376	TL 5080	146	416
ML 160	144	410	TL 5100	146	398
ML 180	139	404	TL 5120	144	397

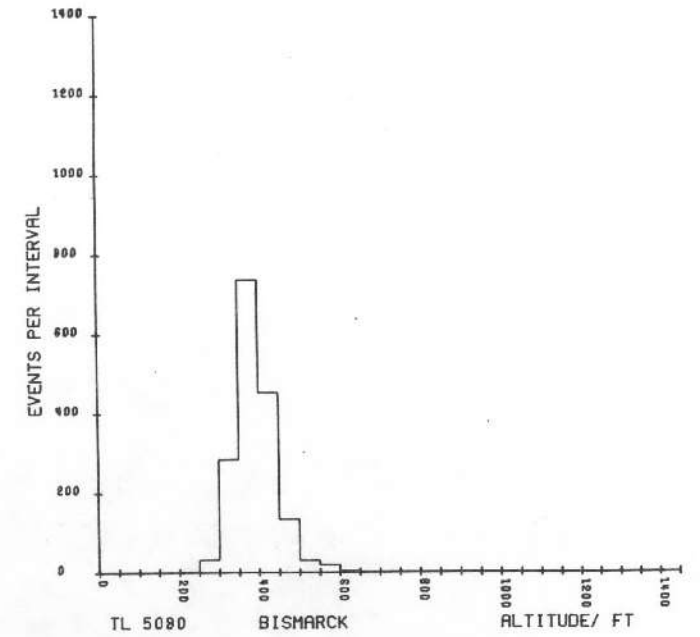
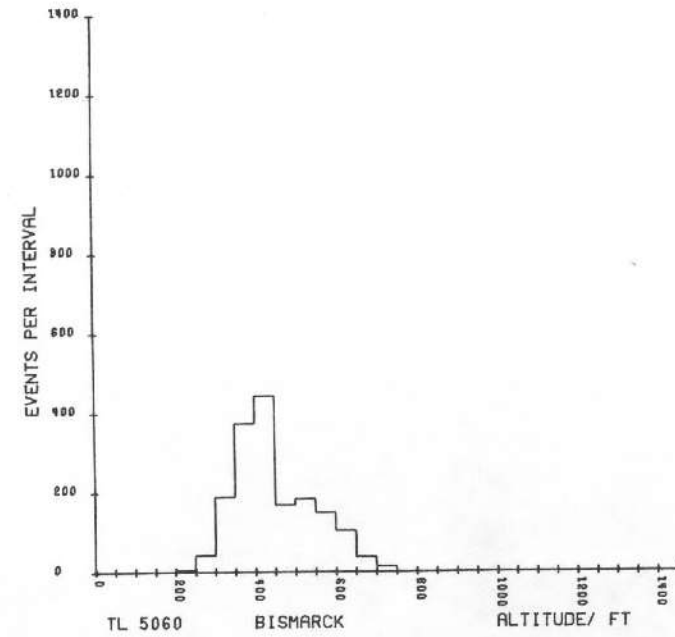
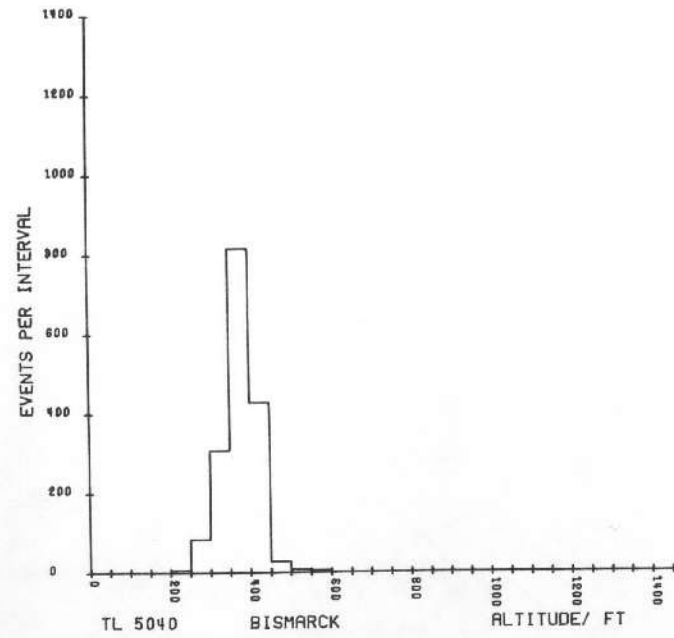
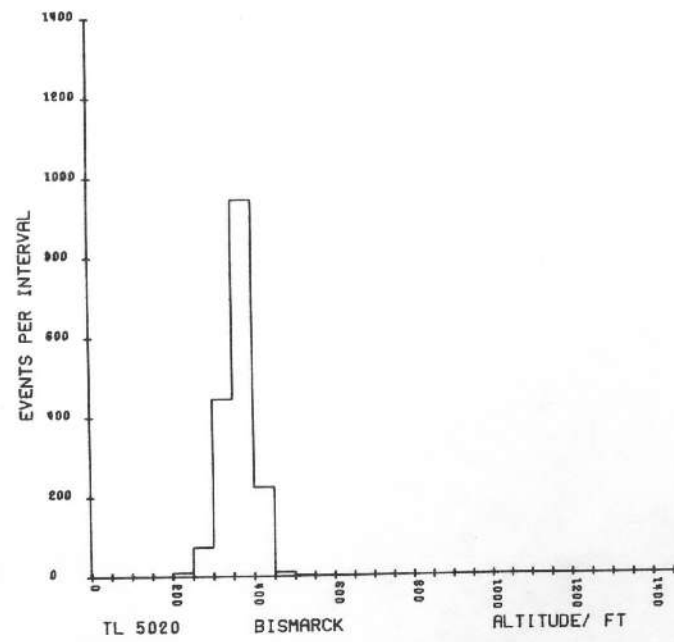
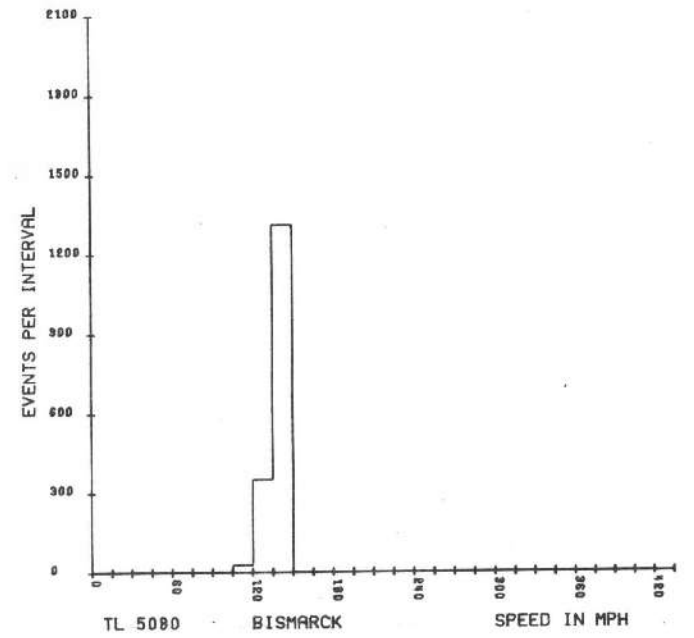
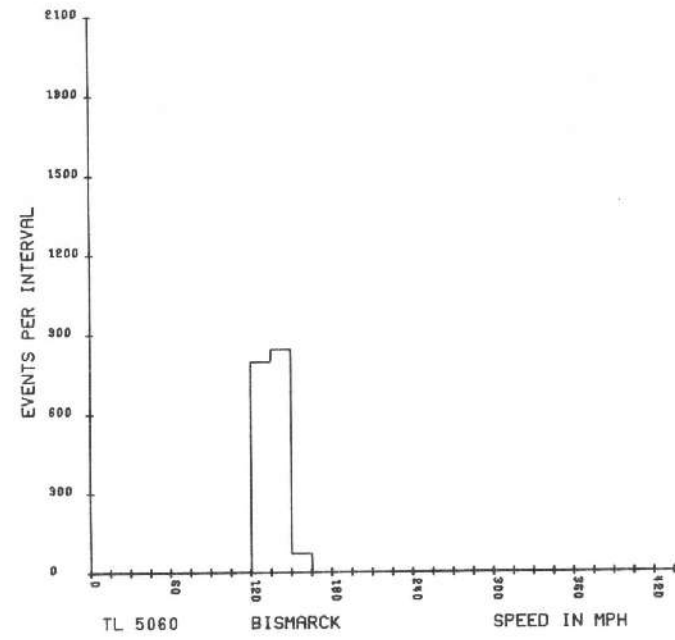
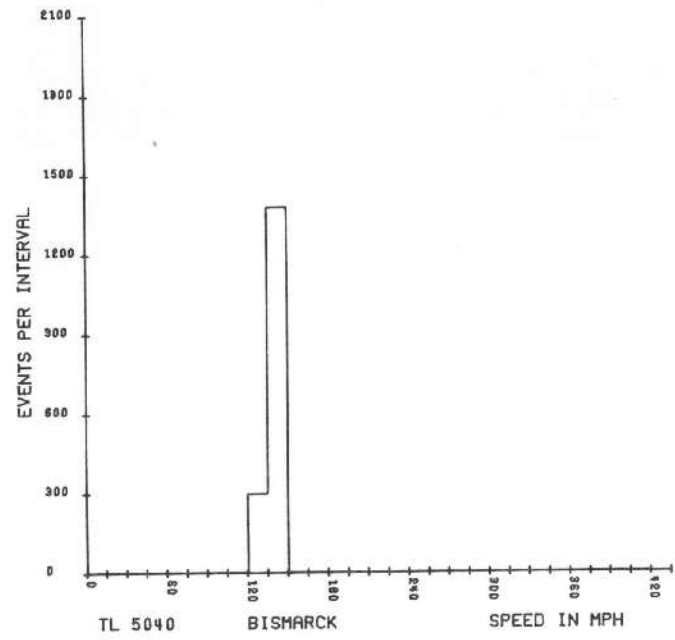
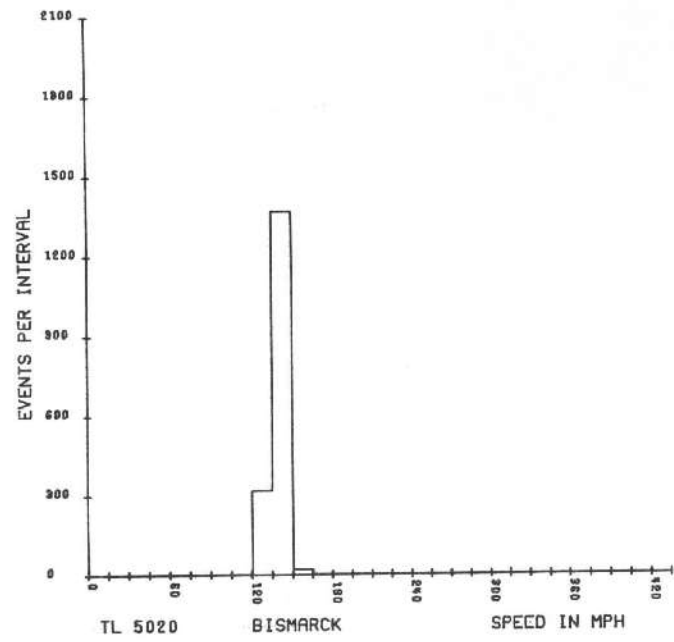


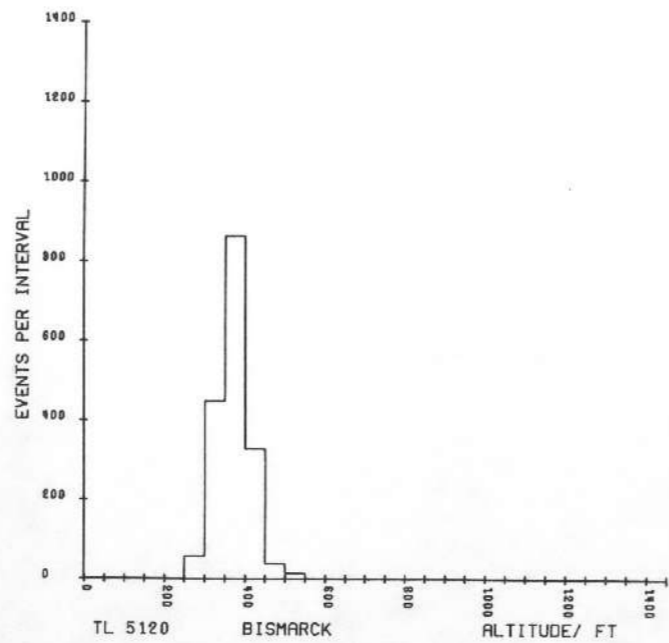
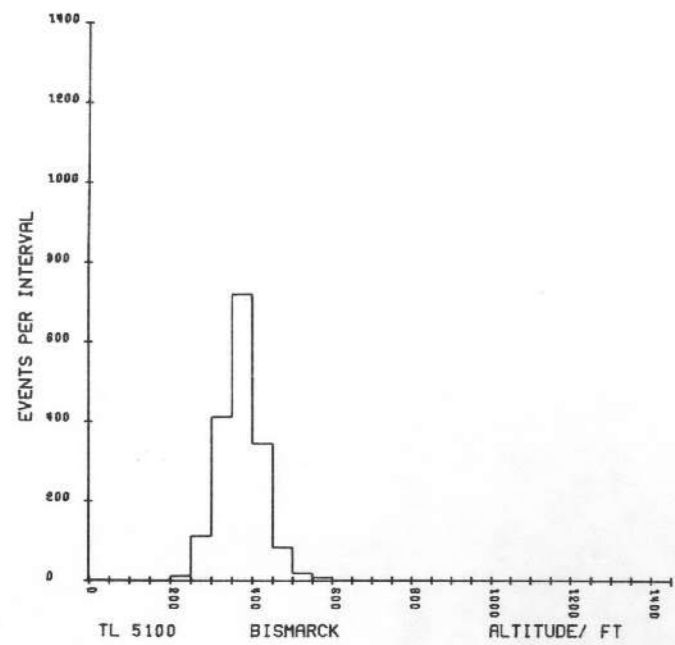
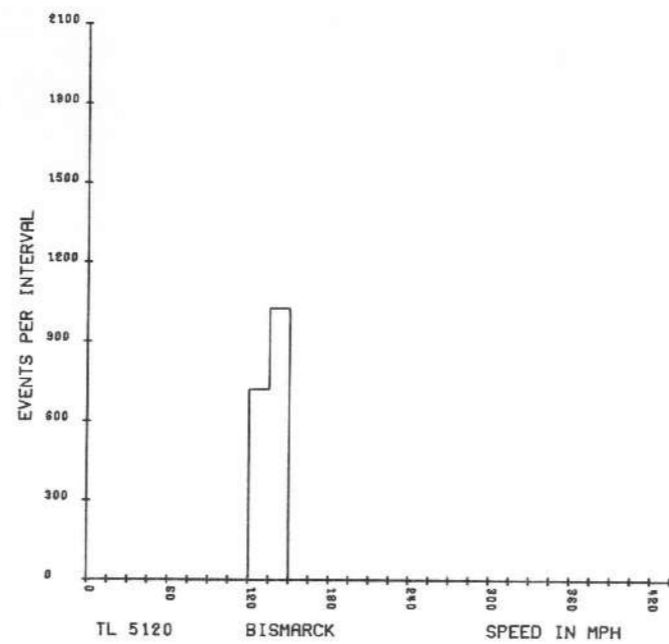
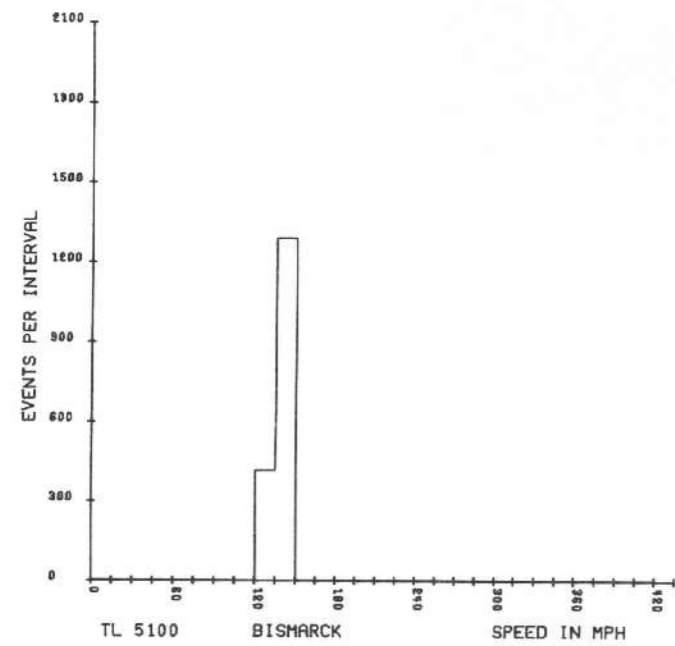














APPENDIX II

TAPE FORMAT STATEMENTS

A. DESCRIPTION OF DATA TAPES

A1. General

All data tapes are 9-track, 800 BPI (NRZI), odd parity, EBCDIC code. Each tape contains a gum label giving the survey project name, month and year of survey, tape type, subcontractor name, date tape created, tape reel count, tape recording characteristics, block size in Bytes and location of tape format information.

The general description for each of the tape types is as follows:

<u>Block Number</u>	<u>Description</u>
1	Format Description
2	Tape Identification
3	First Data Block
4	Second Data Block
.	.
.	.
.	Last Data Block
EOF	

A2. Raw Spectral Data Tapes

Block Size (Physical Record): 6600 characters  
 Logical Record, Data : 1100 characters

1. Format Description Block (Block 1)

The Format Description utilizes 4248 characters. The remaining 2352 characters of this block are blanks.

<u>Line Number</u>	<u>Character Number</u>
	12345678901234567890123456789012345678901234567890123456789012
1	01 0978 (DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)
2	
3	RAW SPECTRAL DATA TAPE
4	
5	FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK ON TAPE)
6	
7	ITEM    FORMAT    DESCRIPTION
8	1        A40        QUADRANGLE NAME AS PROJECT IDENTIFICATION
9	2        A20        NAME OF SUBCONTRACTOR
10	3        I4         APPROXIMATE DATE OF SURVEY (MONTH, YEAR)

Line Number	Character Number		
11	4	I1	AERIAL SYSTEM IDENTIFICATION CODE
12	5	A20	AIRCRAFT IDENTIFICATION BY TYPE AND FAA NUMBER
13	6	I3	BFEC CALIBRATION REPORT NUMBER
14	7	F6.3	4PI SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS
15			
16	8	F6.3	2PI SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS
17			
18	9	I3	NUMBER OF CHANNELS (0-3 MEV) FOR 4PI SYSTEM
19	10	I3	NUMBER OF CHANNELS (0-3 MEV) FOR 2PI SYSTEM
20	11	I3	NUMBER OF FLIGHT LINES ON THIS TAPE
21	12	I4	FIRST FLIGHT LINE NUMBER ON THIS TAPE
22	13	I6	FIRST RECORD NUMBER OF FIRST FLIGHT LINE
23	14	I3	JULIAN DATE (DAY OF YEAR) FIRST FLIGHT LINE WAS COLLECTED
24			
25	15-17	I4,I6,I3	REPEAT OF ITEMS 12-14 FOR SECOND FLIGHT LINE ON THIS TAPE
26			
27	*	*	*
28	*	*	*
29	*	*	*
30	306-308	I4,I6,I3	REPEAT OF ITEMS 12-14 FOR 99TH FLIGHT LINE ON THIS TAPE
31			
32			
33			FORMAT FOR RAW SPECTRAL DATA RECORD (THIRD THRU LAST BLOCK ON TAPE)
34			
35	ITEM	FORMAT	DESCRIPTION
36	1	I1	AERIAL SYSTEM IDENTIFICATION CODE
37	2	I4	FLIGHT LINE NUMBER
38	3	I6	RECORD IDENTIFICATION NUMBER
39	4	I6	GMT TIME OF DAY (HHMMSS)
40	5	F8.4	LATITUDE TO FOUR DECIMAL PLACES IN DEGREES
41	6	F8.4	LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
42	7	F6.1	TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
43	8	F7.1	TOTAL MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
44			
45	9	A8	SURFACE GEOLOGIC MAP UNIT CODE
46	10	I4	QUALITY FLAG CODES
47	11	F4.1	OUTSIDE AIR TEMPERATURE TO ONE DECIMAL PLACE IN DEGREES CELSIUS
48			
49	12	F5.1	OUTSIDE AIR PRESSURE TO ONE DECIMAL PLACE IN MMHG
50	13	F5.3	LIVE TIME COUNTING PERIOD TO THREE DECIMAL PLACES IN SECONDS
51			
52	14	I4	SUMMED RAW OUTPUT FROM COSMIC CHANNELS (3-6 MEV) IN COUNTS
53			
54	15	I4	RAW OUTPUT FROM CHANNEL 1 IN COUNTS
55	16	I4	RAW OUTPUT FROM CHANNEL 2 IN COUNTS
56	*	*	*
57	*	*	*
58	*	*	*
59	270	I4	RAW OUTPUT FROM CHANNEL 256 IN COUNTS
-	-	-	2352 BLANK CHARACTERS

## 2. Tape Identification Block (Block 2)

The information and format for this block are indicated in lines 8 through 30 of the Format Description Block A2.1, and 1396 characters are produced. The remaining 5204 characters in this block are blanks.

If fewer than 99 flight lines exist, the unused flight line information, 13 characters per flight line, is filled with 9's through the 99th flight line.

## 3. Raw Spectral Data Blocks

The information and format for the logical records in these blocks are indicated in lines 36 through 59 of the Format Description Block A2.1. One logical record contains 1100 characters. There are six such logical records per 6600 character physical record or block.

The  $2\pi$  data logical record is recorded after the corresponding  $4\pi$  data collection intervals at a frequency dependent on the  $2\pi$  system data collection interval. For example, if the  $4\pi$  data collection interval is 1 second and the  $2\pi$  data collection interval is 10 seconds, then 10 records of  $4\pi$  data are recorded followed by 1 record of the  $2\pi$  data which was collected during the preceding 10 seconds. The format for the  $2\pi$  data is identical to that of the  $4\pi$  data, except for lines 40 through 49 of the Format Description Block given above. These variables are expressed in the  $2\pi$  record as all nines in the format specified for I and F fields, and all zeros for A fields.

## A3. Single-Record Reduced Data Tapes

Block Size (Physical Record): 6900 characters  
 Logical Record, Data : 138 characters

### 1. Format Description Block (Block 1)

The Format Description utilizes 6768 characters. The remaining 132 characters of this block are blanks.

Line Number	Character Number	
1	02 0978	(DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)
2		
3		SINGLE RECORD REDUCED DATA TAPE
4		
5		FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)
6		



Line Character Number  
Number 12345678901234567890123456789012345678901234567890123456789012

Line Number	ITEM	FORMAT	DESCRIPTION
7			
8	1	A40	QUADRANGLE NAME AS PROJECT IDENTIFICATION
9	2	A20	NAME OF SUBCONTRACTOR
10	3	I4	APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
11	4	I1	NUMBER OF AERIAL SYSTEMS USED TO COLLECT DATA FOR THIS QUADRANGLE
12			
13	5	I1	AERIAL SYSTEM IDENTIFICATION CODE FOR FIRST SYSTEM
14	6	A20	AIRCRAFT IDENTIFICATION BY TYPE AND FAA NUMBER FOR FIRST SYSTEM
15			
16	7	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN CPS PER PERCENT K FOR FIRST SYSTEM
17			
18	8	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT U
19			
20	9	F6.1	NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT TH
21			
22	10	I6	BLANK FIELD (999999)
23	11	F6.3	4PI-SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS FOR FIRST SYSTEM
24			
25	12	F6.3	2PI-SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS FOR FIRST SYSTEM
26			
27	13	I3	NUMBER OF CHANNELS (0-3 MEV) IN 4PI SYSTEM FOR FIRST AERIAL SYSTEM
28			
29	14	I3	NUMBER OF CHANNELS (0-3 MEV) IN 2PI SYSTEM FOR FIRST AERIAL SYSTEM
30			
31	15-24	(SAME)	REPEAT OF ITEMS 5-14 FOR SECOND AERIAL SYSTEM
32	*	*	*
33	*	*	*
34	*	*	*
35	*	*	*
36			
37	85-94	(SAME)	REPEAT OF ITEMS 5-14 FOR NINTH AERIAL SYSTEM
38	95	I3	NUMBER OF FLIGHT LINES ON THIS TAPE
39	96	I4	FIRST FLIGHT LINE NUMBER ON THIS TAPE
40	97	I6	FIRST RECORD NUMBER OF FIRST FLIGHT LINE
41	98	I3	JULIAN DATE (DAY OF YEAR) FIRST FLIGHT-LINE DATA WAS COLLECTED
42			
43	99-101	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR SECOND FLIGHT LINE ON THIS TAPE
44	*	*	*
45	*	*	*
46	*	*	*
47			
48	390-392	I4,I6,I3	REPEAT OF ITEMS 96-98 FOR 99TH FLIGHT LINE ON THIS TAPE
49			
50			
51			
52	FORMAT FOR SINGLE RECORD REDUCED DATA RECORD (THIRD THRU LAST BLOCK)		
53			
54	ITEM	FORMAT	DESCRIPTION
55	1	I1	AERIAL SYSTEM IDENTIFICATION CODE
56	2	I4	FLIGHT LINE NUMBER
57	3	I6	RECORD IDENTIFICATION NUMBER
58	4	I6	GMT TIME OF DAY (HHMMSS)
59	5	F8.4	LATITUDE TO FOUR DECIMAL PLACES IN DEGREES

Line Character Number  
Number 12345678901234567890123456789012345678901234567890123456789012

Line Number			
60	6	F8.4	LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
61	7	F6.1	TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
62	8	F7.1	RESIDUAL (IGRF REMOVED) MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
63			
64	9	A8	SURFACE GEOLOGIC MAP UNIT CODE
65	10	I4	QUALITY FLAG CODES
66	11	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN PERCENT K
67			
68	12	F4.1	UNCERTAINTY IN TERRESTRIAL POTASSIUM TO ONE DECIMAL PLACE IN PERCENT K
69			
70	13	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
71			
72	14	F4.1	UNCERTAINTY IN TERRESTRIAL URANIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
73			
74	15	F6.1	APPARENT CONCENTRATION OF TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
75			
76	16	F4.1	UNCERTAINTY IN TERRESTRIAL THORIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
77			
78	17	F6.1	URANIUM-TO-THORIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
79			
80	18	F6.1	URANIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
81			
82	19	F6.1	THORIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
83			
84	20	F8.1	GROSS GAMMA (0.4-3.0 MEV) COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
85			
86	21	F6.1	UNCERTAINTY IN GROSS GAMMA COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
87			
88	22	F5.1	ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
89			
90	23	F4.1	UNCERTAINTY IN ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
91			
92	24	F4.1	OUTSIDE AIR TEMPERATURE TO ONE DECIMAL PLACE IN DEGREES CELSIUS
93			
94	25	F5.1	OUTSIDE AIR PRESSURE TO ONE DECIMAL PLACE IN MMHG

2. Tape Identification Block (Block 2)

The information and format for this block are indicated in lines 8 through 49 of the Format Description Block A3.1, and 1922 characters are produced. The remaining 4978 characters of this block are blanks.

If less than nine aerial systems are used, the space allocated for additional systems is filled with 9's in the format specified for each item using I and F fields, and with zeros for A fields.

Similarly, if fewer than 99 flight lines exist, the unused flight line information, 13 characters per flight line, is filled with 9's through the 99th flight line.



3. Single Record Reduced Data Blocks

The information and format for the logical records in these blocks are indicated in lines 55 through 94 of the Format Description Block A3.1. One logical record contains 138 characters. There are 50 such logical records per 6900 character physical record or block.

The data appearing in locations specified by lines 68, 72, 76, 86 and 90 of the Format Description Block A3.1 are 9's in the format specified in each case.

A4. Statistical Analysis Data Tapes

Block Size (Physical Record): 8000 characters  
 Logical Record, Data : 160 characters

1. Format Description Block (Block 1)

The Format Description utilizes 7560 characters. The remaining 440 characters are blanks.

Line Number	Character Number	
1	03 0978	(DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)
2		
3		STATISTICAL ANALYSIS DATA TAPE
4		
5		FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)
6		
7	ITEM	FORMAT DESCRIPTION
8	1	A40 QUADRANGLE NAME AS PROJECT IDENTIFICATION
9	2	A20 NAME OF SUBCONTRACTOR
10	3	I4 APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
11	4	I1 NUMBER OF AERIAL SYSTEMS USED TO COLLECT DATA FOR THIS QUADRANGLE
12		
13	5	I1 AERIAL SYSTEM IDENTIFICATION CODE FOR FIRST SYSTEM
14	6	A20 AIRCRAFT IDENTIFICATION BY TYPE AND FAA NUMBER FOR FIRST SYSTEM
15		
16	7	F6.1 NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN CPS PER PERCENT K
17		
18		
19	8	F6.1 NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT U
20		
21		
22	9	F6.1 NOMINAL ALTITUDE SYSTEM SENSITIVITY RELATIVE TO TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN CPS PER PPM EQUIVALENT TH
23		
24		
25	10	I6 BLANK FIELD (999999)
26	11	F6.3 4PI-SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS FOR FIRST SYSTEM
27		
28	12	F6.3 2PI-SYSTEM DATA COLLECTION INTERVAL TO THREE DECIMAL PLACES IN SECONDS FOR FIRST SYSTEM
29		

Line Number	Character Number	
30	13 I3	NUMBER OF CHANNELS (0-3 MEV) IN 4PI SYSTEM FOR FIRST AERIAL SYSTEM
31		
32	14 I3	NUMBER OF CHANNELS (0-3 MEV) IN 2PI SYSTEM FOR FIRST AERIAL SYSTEM
33		
34	15-24 (SAME)	REPEAT OF ITEMS 5-14 FOR SECOND AERIAL SYSTEM
35	* *	*
36	* *	*
37	* *	*
38	85-94 (SAME)	REPEAT OF ITEMS 5-14 FOR NINTH AERIAL SYSTEM
39	95 I3	NUMBER OF FLIGHT LINES ON THIS TAPE
40	96 I4	FIRST FLIGHT LINE NUMBER ON THIS TAPE
41	97 I6	FIRST RECORD NUMBER OF FIRST FLIGHT LINE
42	98 I3	JULIAN DATE (DAY OF YEAR) FIRST FLIGHT LINE DATA WAS COLLECTED
43		
44	99-101 I4,I6,I3	REPEAT OF ITEMS 96-98 FOR SECOND FLIGHT LINE ON THIS TAPE
45		
46	* *	*
47	* *	*
48	* *	*
49	390-392 I4,I6,I3	REPEAT OF ITEMS 96-98 FOR 99TH FLIGHT LINE ON THIS TAPE
50		
51		
52		FORMAT FOR STATISTICAL ANALYSIS DATA RECORD (THIRD THRU LAST BLOCK)
53		
54	ITEM	FORMAT DESCRIPTION
55	1	I1 AERIAL SYSTEM IDENTIFICATION CODE
56	2	I4 FLIGHT LINE NUMBER
57	3	I6 RECORD IDENTIFICATION NUMBER
58	4	I6 GMT TIME OF DAY (HHMMSS)
59	5	F8.4 LATITUDE TO FOUR DECIMAL PLACES IN DEGREES
60	6	F8.4 LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
61	7	F6.1 TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
62	8	F7.1 RESIDUAL (IGRF REMOVED) MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
63		
64	9	A8 SURFACE GEOLOGIC MAP UNIT CODE
65	10	I5 QUALITY FLAG CODES
66	11	F6.1 AVERAGED CONCENTRATION OF TERRESTRIAL POTASSIUM (K-40) TO ONE DECIMAL PLACE IN PERCENT K
67		
68	12	F4.1 UNCERTAINTY IN TERRESTRIAL POTASSIUM TO ONE DECIMAL PLACE IN PERCENT K
69		
70	13	F5.1 POTASSIUM STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
71		
72	14	F6.1 AVERAGED CONCENTRATION OF TERRESTRIAL URANIUM (BI-214) TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
73		
74	15	F4.1 UNCERTAINTY IN TERRESTRIAL URANIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
75		
76	16	F5.1 URANIUM STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
77		
78	17	F6.1 AVERAGED CONCENTRATION OF TERRESTRIAL THORIUM (TL-208) TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
79		
80	18	F4.1 UNCERTAINTY IN TERRESTRIAL THORIUM TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
81		



Line Number	Character Number	
82	19	F5.1 THORIUM STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
83		
84	20	F8.1 GROSS GAMMA (0.4-3.0 MEV) COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
85		
86	21	F6.1 UNCERTAINTY IN GROSS GAMMA COUNT RATE TO ONE DECIMAL PLACE IN COUNTS PER SECOND
87		
88	22	F5.1 ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
89		
90	23	F4.1 UNCERTAINTY IN ATMOSPHERIC BI-214 4PI CORRECTION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
91		
92	24	F6.1 AVERAGED URANIUM-TO-THORIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
93		
94	25	F5.1 URANIUM-TO-THORIUM RATIO STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
95		
96	26	F6.1 AVERAGED URANIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
97		
98	27	F5.1 URANIUM-TO-POTASSIUM RATIO STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
99		
100		
101	28	F6.1 AVERAGED THORIUM-TO-POTASSIUM RATIO TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
102		
103	29	F5.1 THORIUM-TO-POTASSIUM RATIO STANDARD DEVIATION FROM THE MEAN TO ONE DECIMAL PLACE AND ALGEBRAICALLY SIGNED
104		
105		

2. Tape Identification Block (Block 2)

The information and format for this block are indicated in lines 8 through 49 of the Format Description Block A4.1, and 1922 characters are produced. The remaining 6078 characters of this block are blanks.

If less than nine aerial systems are used, the space allocated for additional systems is filled with 9's in the format specified for each item using I and F fields, and with zeros for A fields.

Similarly, if fewer than 99 flight lines exist, the unused flight line information, 13 characters per flight line, is filled with 9's through the 99th flight line.

3. Statistical Analysis Data Blocks

The information and format for the logical records in these blocks are indicated in lines 55 through 103 of the Format Description Block A4.1. One logical record contains 160 characters. There are 50 such logical records per 8000 character physical record or block.

The data appearing in locations specified by lines 68, 74, 80, 86 and 90 of the Format Description Block A4.1 are 9's in the format specified in each case.

File 2: Statistical Analysis Summary

Block Size (Physical Record): 7000 characters  
 Logical Record (Data) : 140 characters

1. Format Description Block (Block 1)

The Format Description utilizes 4320 characters. The remaining 2680 characters are blanks.

Line Number	Character Number	
1	05 0978	(DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODE)
2		
3		STATISTICAL ANALYSIS SUMMARY TAPE (OR FILE)
4		
5		FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)
6		
7	ITEM	FORMAT DESCRIPTION
8	1	A40 QUADRANGLE NAME AS PROJECT IDENTIFICATION
9	2	A20 NAME OF SUBCONTRACTOR
10	3	I4 APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
11	4	I6 NUMBER OF GEOLOGIC MAP UNITS USED FOR THIS QUADRANGLE
12		
13		
14		FORMAT FOR STATISTICAL ANALYSIS SUMMARY DATA RECORD (THIRD THRU LAST BLOCK)
15		
16		
17	ITEM	FORMAT DESCRIPTION
18	1	A8 SURFACE GEOLOGIC MAP UNIT IDENTIFYING CODE
19	2	I6 TOTAL RECORDS FOR GEOLOGIC MAP UNIT
20	3	I6 NUMBER OF POTASSIUM RECORDS COMPUTED FOR GEOLOGIC UNIT
21		
22	4	F6.1 POTASSIUM CONCENTRATION MEAN TO ONE DECIMAL PLACE IN PERCENT K
23		
24	5	F6.1 POTASSIUM CONCENTRATION STANDARD DEVIATION TO ONE DECIMAL PLACE IN PERCENT K
25		
26	6	A3 POTASSIUM CONCENTRATION DISTRIBUTION CODE
27	7	I6 NUMBER OF URANIUM RECORDS COMPUTED FOR GEOLOGIC UNIT
28	8	F6.1 URANIUM CONCENTRATION MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
29		
30	9	F6.1 URANIUM CONCENTRATION STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U
31		
32	10	A3 URANIUM CONCENTRATION DISTRIBUTION CODE
33	11	I6 NUMBER OF THORIUM RECORDS COMPUTED FOR GEOLOGIC UNIT
34	12	F6.1 THORIUM CONCENTRATION MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
35		
36	13	F6.1 THORIUM CONCENTRATION STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH
37		



Line Number	Character Number	Description
38	14 A3	THORIUM CONCENTRATION DISTRIBUTION CODE
39	15 I6	NUMBER OF URANIUM-TO-THORIUM RATIO RECORDS COMPUTER FOR GEOLOGIC UNIT
40		
41	16 F6.1	URANIUM-TO-THORIUM RATIO MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
42		
43	17 F6.1	URANIUM-TO-THORIUM RATIO STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PPM EQUIVALENT TH
44		
45		
46	18 A3	URANIUM-TO-THORIUM RATIO DISTRIBUTION CODE
47	19 I6	NUMBER OF URANIUM-TO-POTASSIUM RATIO RECORDS COMPUTED FOR GEOLOGIC UNIT
48		
49	20 F6.1	URANIUM-TO-POTASSIUM RATIO STANDARD DEVIATION TO ONE IN PPM EQUIVALENT U PER PERCENT K
50		
51	21 F6.1	URANIUM-TO-POTASSIUM RATIO STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT U PER PERCENT K
52		
53	22 A3	URANIUM-TO-POTASSIUM RATIO DISTRIBUTION CODE
54	23 I6	NUMBER OF THORIUM-TO-POTASSIUM RATIO RECORDS COMPUTED FOR GEOLOGIC UNIT
55		
56	24 F6.1	THORIUM-TO-POTASSIUM RATIO MEAN TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
57		
58	25 F6.1	THORIUM-TO-POTASSIUM RATIO STANDARD DEVIATION TO ONE DECIMAL PLACE IN PPM EQUIVALENT TH PER PERCENT K
59		
60	26 A3	THORIUM-TO-POTASSIUM RATIO DISTRIBUTION CODE

2. Tape Identification Block (Block 2)

The information and format for this block are indicated in lines 8 through 11 of the Format Description Block A6.1, and 70 characters are produced. The remaining 6930 characters of this block are blanks.

3. Statistical Analysis Summary Data Blocks

The information and format for the logical records in these blocks are indicated in lines 18 through 60 of the Format Description Block A6.1. One logical record contains 140 characters. There are 50 such logical records per 7000 character physical record or block.

A5. Magnetic Data Tapes

Block Size (Physical Record): 8000 characters  
 Logical Record (Data) : 80 characters

1. Format Description Block (Block 1)

The Format Description utilizes 3384 characters. The remaining 4616 characters are blanks.

Line Number	Character Number	Description
1	04 0978	(DATA TAPE TYPE AND FORMAT SPECIFICATION DATE CODES)
2		
3		MAGNETIC DATA TAPE
4		
5		FORMAT FOR TAPE IDENTIFICATION BLOCK (SECOND BLOCK)
6		
7	ITEM	FORMAT DESCRIPTION
8	1	A40 QUADRANGLE NAME AS PROJECT IDENTIFICATION
9	2	A20 NAME OF SUBCONTRACTOR
10	3	I4 APPROXIMATE DATE OF SURVEY (MONTH, YEAR)
11	4	I3 NUMBER OF FLIGHT LINES ON THIS TAPE
12	5	I4 FIRST FLIGHT LINE ON THIS TAPE
13	6	I6 FIRST RECORD NUMBER OF FIRST FLIGHT LINE
14	7	I3 JULIAN DATE (DAY OF YEAR) FIRST FLIGHT LINE DATA WAS COLLECTED
15		
16	8	F8.4 LATITUDE OF GROUND BASE STATION TO FOUR DECIMAL PLACES IN DEGREES FOR FIRST FLIGHT LINE
17		
18	9	F8.4 LONGITUDE OF GROUND BASE STATION TO FOUR DECIMAL PLACES IN DEGREES FOR FIRST FLIGHT LINE
19		
20	10-14	(SAME) REPEAT OF ITEMS 5-9 FOR SECOND FLIGHT LINE ON THIS TAPE
21		
22	*	*
23	*	*
24	*	*
25	495-499	(SAME) REPEAT OF ITEMS 5-9 FOR 99TH FLIGHT LINE ON THIS TAPE
26		
27		
28		FORMAT FOR MAGNETIC DATA RECORD (THIRD THRU LAST BLOCK)
29		
30	ITEM	FORMAT DESCRIPTION
31	1	I1 AERIAL SYSTEM IDENTIFICATION CODE
32	2	I4 FLIGHT LINE NUMBER
33	3	I6 RECORD IDENTIFICATION NUMBER
34	4	I6 GMT TIME OF DAY (HHMMSS)
35	5	F8.4 LATITUDE TO FOUR DECIMAL PLACES IN DEGREES
36	6	F8.4 LONGITUDE TO FOUR DECIMAL PLACES IN DEGREES
37	7	F6.1 TERRAIN CLEARANCE TO ONE DECIMAL PLACE IN METERS
38	8	F5.1 OUTSIDE AIR PRESSURE TO ONE DECIMAL PLACE IN MMHG
39	9	A8 SURFACE GEOLOGIC MAP UNIT CODE
40	10	F7.1 TOTAL MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
41		
42	11	F7.1 RESIDUAL (IGRF REMOVED) MAGNETIC FIELD INTENSITY TO ONE DECIMAL PLACE IN GAMMAS
43		
44	12	F7.1 DIURNAL MAGNETIC INTENSITY VARIATION TO ONE DECIMAL PLACE IN GAMMAS
45		
46	13	F7.1 MAGNETIC DEPTH-TO-BASEMENT TO ONE DECIMAL PLACE IN METERS (IF REQUIRED)
47		



2. Tape Identification Block (Block 2)

The information and format for this block are indicated in lines 8 through 25 of the Format Description Block A5.1, and 2938 characters are produced. The remaining 5062 characters of this block are blanks.

If fewer than 99 flight lines exist, the unused flight line information, 29 characters per flight line, is filled with 9's through the 99th flight line in the format indicated.

3. Magnetic Data Blocks

The information and format for the logical records in these blocks are indicated in lines 31 through 46 of the Format Description Block A5.1. One logical record contains 80 characters. There are 100 such logical records per 8000 character physical record or block.

If the magnetic depth-to-basement is not required, this item is expressed as 99999.9.

B. DESCRIPTION OF LISTINGS

B1. Single record reduced data listings: include the following information on Microfiche:

<u>ITEM</u>	<u>DESCRIPTION</u>
REC	Sequential record number
Lat	Location Y in latitude
Long	Location X in longitude
RMag	Residual magnetic field, gammas
Alt	Surface altitude
GEO UNIT	Geologic Type
AKUT	A=Altitude; K=Potassium; U=Uranium T=Thorium - Results of statistical adequacy test
COS	Cosmic c/s
BIAIR	Airborne <sup>214</sup> Bi, 4π data, c/s
GC	Gross count, .4 MeV - 2.8 MeV
eTh	ppm
eU	ppm
K	%
eU:eTh	Ratio
eU:K	Ratio
eTh:K	Ratio
TEMP	Outside Air Temperature (°C)
BP	Atmospheric Pressure (mm Hg)

B2. Averaged record data listings: include the following information on Microfiche:

<u>ITEM</u>	<u>DESCRIPTION</u>
REC	Sequential Record number
GEO UNIT	Geologic type
AKUT	A=Altitude; K=Potassium; U=Uranium; T=Thorium - Results of statistical adequacy test
Long	Longitude of X location of geologic type
Lat	Latitude of Y location of geologic type
RMag	Residual magnetic field, gammas
COS	Cosmic, 4π
BIAIR	Atmospheric Bi, 4π, c/s
GC	Gross count, c/s

ITEMDESCRIPTION

eTh  
Rank  
eU  
Rank  
K  
Rank  
eU/eTh  
Rank  
eU/K  
Rank  
eTh/K  
Rank

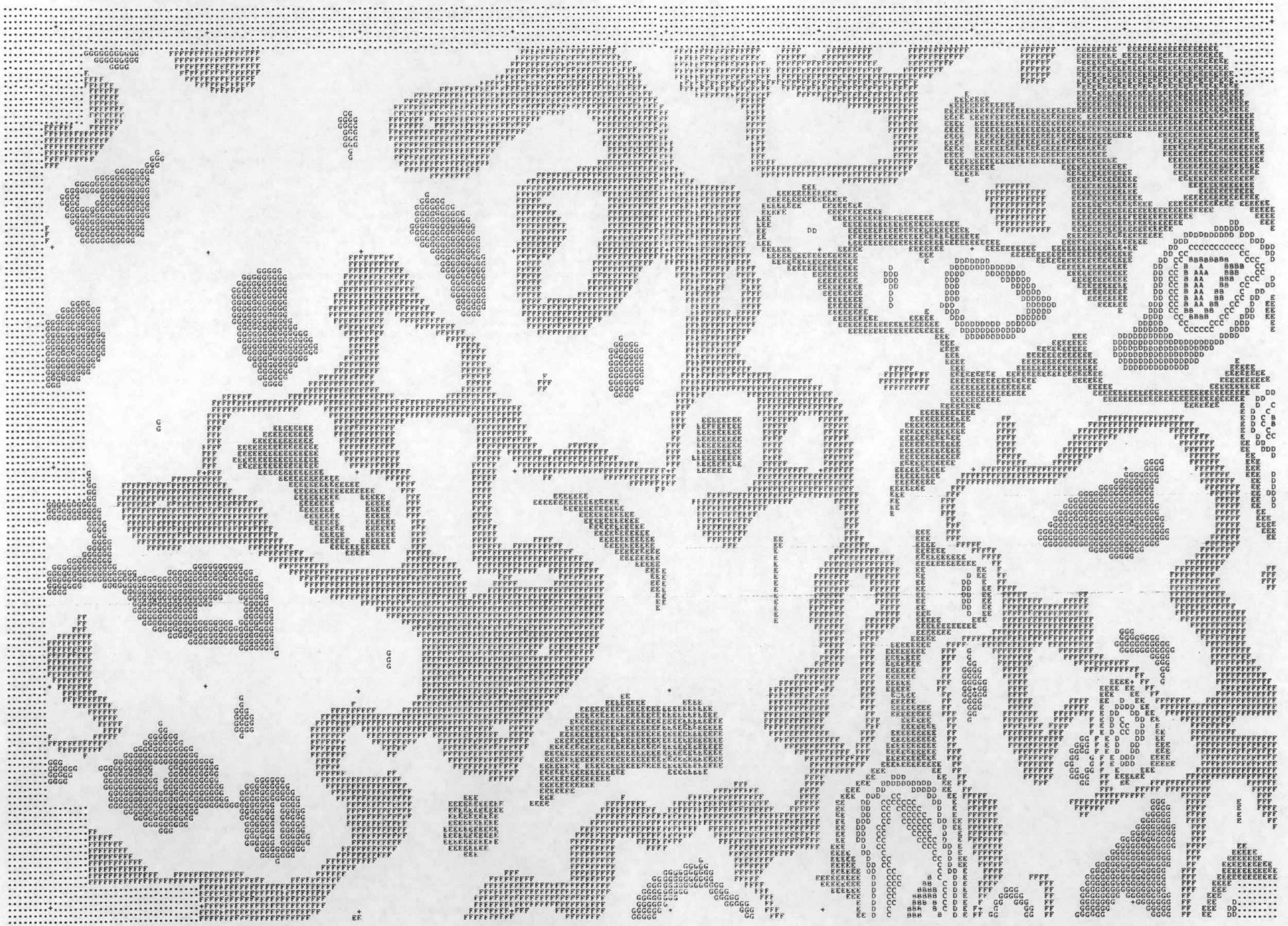
eTh value, ppm  
eTh standard deviation rank  
eU value, ppm  
eU standard deviation rank  
K value, %  
K standard deviation rank  
Ratio value  
eU/eTh standard deviation rank  
Ratio value  
eU/K standard deviation rank  
Ratio value  
eTh/K standard deviation rank



1GEODATA INT. INC.		SINGLE REC LISTING				1980																						
BISMARCK		NM 14-04				MAPLINE		240																				
1	RCN	GEUNIT	AKUT	LAT	LONG	RMAG	COS	GC	BLAIR	ALT	TEMP	BP	ETH	EU	K	EU/ETH	EU/K	ETH/K										
3440	ZNA	0000	46.9798	102.0285	-301.7	40	2097	10.1	390	28.8	690.9	7.0	3.0	1.2	0.43	2.48	5.71											
3441	ZNA	0010	46.9799	102.0276	-243.8	13	232	10.1	-61	28.4	685.3	1.3	0.1	0.1	0.12	1.45	12.34											
3442	ZNA	0000	46.9799	102.0267	-241.9	40	2185	10.1	322	28.7	684.8	6.6	1.9	1.4	0.29	1.40	4.77											
3443	ZNA	0000	46.9799	102.0259	-241.5	45	2242	10.1	311	28.7	683.8	6.6	3.8	1.2	0.59	3.22	5.51											
3444	ZNA	0000	46.9799	102.0250	-241.5	40	2319	10.1	301	28.8	685.3	7.8	3.3	1.2	0.42	2.68	6.45											
3445	ZNA	0000	46.9799	102.0242	-242.8	49	2334	10.1	300	28.8	684.3	8.3	2.9	1.2	0.35	2.40	6.86											
3446	ZNA	0000	46.9799	102.0233	-242.2	45	2388	10.1	297	28.7	686.3	7.3	3.8	1.5	0.52	2.55	4.92											
3447	ZNA	0000	46.9799	102.0224	-241.8	44	2518	10.1	312	28.7	683.8	9.4	3.4	1.5	0.36	2.22	6.13											
3448	ZNA	0000	46.9799	102.0216	-241.4	35	2656	10.1	332	28.6	684.8	8.0	4.5	1.4	0.57	3.21	5.66											
3449	ZNA	0000	46.9799	102.0207	-241.0	49	2462	10.1	347	28.6	683.3	8.5	3.4	1.4	0.40	2.40	6.02											
3450	ZNA	0000	46.9799	102.0199	-240.8	46	2319	10.1	370	28.5	684.3	7.0	2.5	1.8	0.36	1.43	3.99											
3451	ZNA	0000	46.9799	102.0190	-240.2	34	2555	10.1	380	28.4	683.3	9.1	3.7	1.7	0.41	2.15	5.27											
3452	ZNA	0000	46.9799	102.0181	-238.8	40	2343	10.1	367	28.4	683.3	6.6	5.2	1.2	0.79	4.16	5.28											
3453	ZNA	0000	46.9799	102.0173	-238.6	58	2362	10.1	365	28.4	684.3	7.6	2.4	1.3	0.31	1.89	6.02											
3454	ZNA	0000	46.9799	102.0164	-238.2	48	2764	10.1	363	28.4	684.3	8.3	2.6	2.1	0.31	1.21	3.85											
3455	ZNA	0000	46.9799	102.0155	-237.6	53	2646	10.1	352	28.4	682.8	9.5	1.8	1.8	0.19	1.04	5.33											
3456	ZNA	0000	46.9799	102.0147	-237.2	53	2260	10.1	330	28.4	684.3	7.8	2.3	1.5	0.24	1.54	5.26											
3457	ZNA	0000	46.9800	102.0138	-236.5	52	2537	10.1	317	28.4	684.3	6.7	3.5	1.9	0.52	1.79	3.46											
3458	ZNA	0000	46.9800	102.0130	-235.9	47	2623	10.1	314	28.4	683.8	9.7	2.1	1.7	0.22	1.23	5.53											
3459	ZNA	0000	46.9800	102.0121	-235.2	45	2343	10.1	325	28.4	683.8	6.9	3.5	1.4	0.51	2.47	4.87											
3460	ZNA	0000	46.9800	102.0112	-234.8	63	2637	10.1	355	28.4	683.3	9.8	2.9	1.9	0.29	1.54	5.22											
3461	ZNA	0000	46.9800	102.0104	-234.4	48	2405	10.1	399	28.4	683.3	6.4	1.5	2.1	0.23	0.70	3.05											
3462	ZNA	0000	46.9800	102.0095	-233.8	67	2761	10.1	400	28.4	684.3	10.9	1.8	1.8	0.16	0.96	5.91											
3463	ZNA	0000	46.9800	102.0086	-233.6	62	2551	10.1	364	28.4	683.3	9.4	2.7	1.6	0.29	1.77	6.05											
3464	ZNA	0000	46.9800	102.0078	-232.2	64	2626	10.1	332	28.4	683.3	7.7	1.9	1.9	0.25	1.01	4.03											
3465	ZNA	0000	46.9800	102.0069	-231.8	40	2601	10.1	309	28.4	683.8	9.8	2.4	1.8	0.24	1.31	5.42											
3466	ZNA	0000	46.9800	102.0061	-231.4	53	2837	10.1	316	28.4	683.3	7.7	2.9	2.1	0.37	1.37	3.66											
3467	ZNA	0000	46.9800	102.0052	-231.3	47	2312	25.9	304	28.4	682.8	6.4	1.3	1.8	0.21	0.76	3.67											
3468	ZNA	0000	46.9800	102.0043	-231.0	34	2287	25.9	306	28.4	683.3	6.3	2.1	1.9	0.33	1.07	3.25											
3469	ZNA	0000	46.9800	102.0035	-230.9	46	2726	25.9	310	28.4	682.8	9.7	3.9	1.7	0.41	2.37	5.84											
3470	ZNA	0000	46.9800	102.0026	-231.2	42	2186	25.9	304	28.4	682.8	6.6	3.8	1.6	0.57	2.33	4.05											
3471	ZNA	0000	46.9800	102.0017	-231.3	42	2402	25.9	320	28.4	680.7	7.7	1.2	1.8	0.15	0.67	4.39											
3472	ZNA	0000	46.9800	102.0009	-231.4	50	2395	25.9	339	28.4	682.8	5.5	3.8	1.8	0.69	2.13	3.07											
3473	TG	0000	46.9801	102.0000	-231.3	44	2510	25.9	340	28.4	682.3	8.1	2.1	1.8	0.26	1.17	4.60											
3474	TG	0000	46.9801	101.9992	-231.6	48	2330	25.9	324	28.5	682.3	6.6	2.9	1.6	0.44	1.84	4.19											
3475	TG	0000	46.9801	101.9983	-230.7	48	2523	25.9	315	28.6	682.3	11.7	1.1	2.0	0.09	0.56	5.88											
3476	TG	0000	46.9801	101.9974	-230.8	40	2433	27.3	303	28.6	682.8	8.3	2.1	2.0	0.25	1.03	4.11											
3477	TG	0000	46.9801	101.9966	-230.9	52	2212	27.3	297	28.7	682.3	5.0	2.1	1.7	0.43	1.27	2.99											
3478	TG	0000	46.9801	101.9957	-231.0	50	2424	27.3	293	28.7	681.2	9.2	3.2	1.7	0.34	1.83	5.32											
3479	TG	0000	46.9801	101.9948	-231.1	47	2187	27.3	284	28.7	682.8	8.1	2.2	1.5	0.27	1.44	5.27											
3480	TG	0000	46.9801	101.9940	-231.2	51	2231	27.3	300	28.7	681.7	8.4	1.9	1.5	0.23	1.26	5.49											
3481	TG	0000	46.9801	101.9931	-231.3	48	2206	27.3	322	28.7	681.7	8.1	1.7	1.7	0.21	0.98	4.65											
3482	TG	0000	46.9801	101.9923	-231.7	39	2372	27.3	313	28.7	680.7	8.5	0.9	1.9	0.10	0.46	4.38											
3483	TG	0000	46.9801	101.9914	-232.0	33	1937	27.3	332	28.6	681.7	8.4	1.8	1.2	0.22	1.50	6.80											
3484	TG	0000	46.9801	101.9905	-232.6	57	2384	27.3	368	28.6	681.7	8.4	3.0	1.6	0.35	1.80	5.11											
3485	TG	0000	46.9801	101.9897	-233.0	40	1944	25.5	362	28.5	683.3	6.6	1.6	1.5	0.25	1.06	4.36											
3486	TG	0000	46.9801	101.9888	-233.8	52	2146	25.5	391	28.5	682.3	7.4	3.1	1.6	0.42	1.97	4.69											
3487	TG	0000	46.9801	101.9880	-234.2	36	2223	25.5	405	28.5	681.2	7.4	2.4	1.6	0.33	1.50	4.54											
3488	TG	0000	46.9801	101.9871	-234.8	40	2281	25.5	409	28.5	681.2	8.7	3.3	1.5	0.38	2.16	5.63											
3489	TG	0000	46.9802	101.9862	-235.4	32	2217	25.5	402	28.5	681.2	7.3	2.8	1.7	0.39	1.65	4.27											
3490	TG	0000	46.9802	101.9854	-236.0	39	2348	25.5	406	28.5	682.3	7.8	2.2	2.0	0.28	1.10	3.90											
3491	TG	0000	46.9802	101.9845	-236.6	51	2323	25.5	396	28.5	681.2	7.4	2.1	1.9	0.28	1.10	3.93											
3492	TG	0000	46.9802	101.9836	-236.8	51	2618	25.5	352	28.5	681.2	10.8	1.6	2.0	0.14	0.79	5.50											
3493	TG	0000	46.9802	101.9828	-237.4	40	2253	25.5	336	28.5	682.8	10.2	1.7	1.4	0.17	1.19	7.15											
3494	TG	0000	46.9802	101.9819	-238.0	56	2390	24.6	325	28.5	681.7	7.7	3.6	1.7	0.47	2.17	4.60											
3495	TG	0000	46.9802	101.9811	-238.6	54	2468	24.6	317	28.5	682.3	8.7	1.1	1.8	0.13	0.63	4.94											
3496	TG	0000	46.9802	101.9802	-239.2	55	2259	24.6	317	28.6	681.2	7.0	2.9	1.5	0.41	1.90	4.60											

1GEODATA INT. INC.		AVERAGE REC LISTING				1980														
BISMARCK		NM 14-04				MAPLINE		240												
1	RCN	GEUNIT	AKUT	LAT	LONG	RMAG	CUS	GC	BLAIR	ETH RANK	EU RANK	K RANK	EU/ETH RANK	EU/K RANK	ETH/K RANK					
3440	ZNA	0000	46.9798	102.0285	-301.7	40	2097	10.1	7.0+ 0	3.0+ 1	1.2- 0	0.43+ 0	2.48+ 2	5.71+ 1						
3441	ZNA	0010	46.9799	102.0276	-243.8	13	232	10.1	1.3- 2	0.1- 3	0.1- 3	0.12- 2	1.45- 0	12.34+ 8						
3442	ZNA	0000	46.9799	102.0267	-241.9	40	2185	10.1	6.6+ 0	1.9- 0	1.4- 0	0.29- 0	1.40- 0	4.77+ 0						
3443	ZNA	0000	46.9799	102.0259	-241.5	45	2242	10.1	6.4+ 0	2.7+ 0	1.1- 0	0.43+ 0	2.45+ 1	5.76+ 1						
3444	ZNA	0000	46.9799	102.0250	-241.5	40	2319	10.1	7.1+ 0	3.0+ 1	1.2- 0	0.42+ 0	2.48+ 2	5.89+ 1						
3445	ZNA	0000	46.9799	102.0242	-242.8	49	2334	10.1	7.8+ 1	3.3+ 1	1.3- 0	0.43+ 0	2.54+ 2	5.91+ 1						
3446	ZNA	0000	46.9799	102.0233	-242.2	45	2388	10.1	8.0+ 1	3.5+ 1	1.4- 0	0.44+ 0	2.58+ 2	5.86+ 1						
3447	ZNA	0000	46.9799	102.0224	-241.8	44	2518	10.1	8.2+ 1	3.6+ 1	1.4+ 0	0.43+ 0	2.47+ 2	5.73+ 1						
3448	ZNA	0000	46.9799	102.0216	-241.4	35	2656	10.1	8.2+ 1	3.6+ 1	1.5+ 0	0.44+ 0	2.41+ 1	5.51+ 1						
3449	ZNA	0000	46.9799	102.0207	-241.0	49	2462	10.1	8.1+ 1	3.6+ 1	1.5+ 0	0.45+ 0	2.37+ 1	5.32+ 0						
3450	ZNA	0000	46.9799	102.0199	-240.8	46	2													





Alt-1 Line Printer Contour

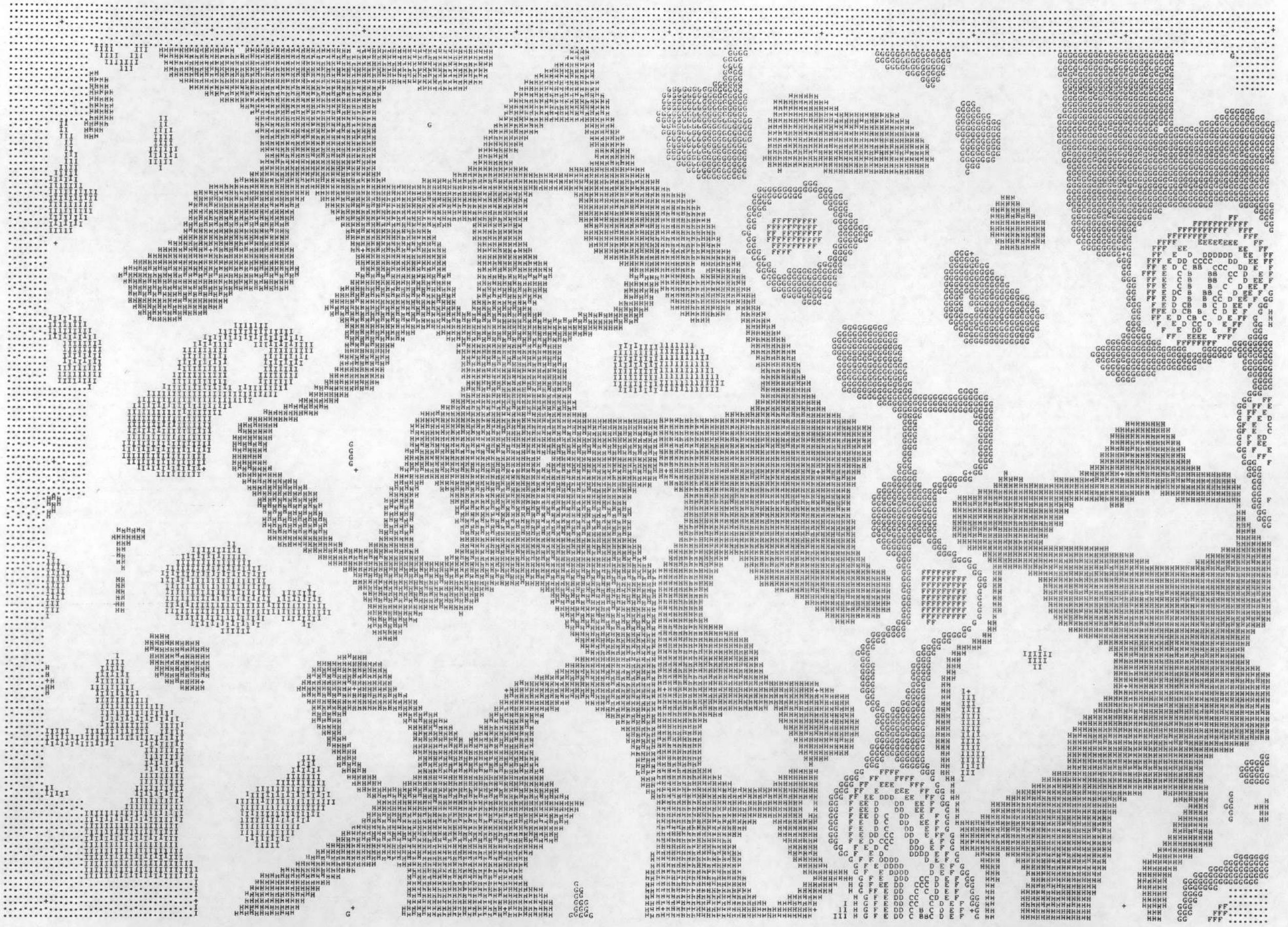
GEODATA INTERNATIONAL, INC.  
DALLAS, TEXAS

4.200	2.50<C< 3.00	3.50<C< 4.00	4.50<C< 5.00	5.50<C< 6.00	6.50<C< 7.00
	7.50<C< 8.00				







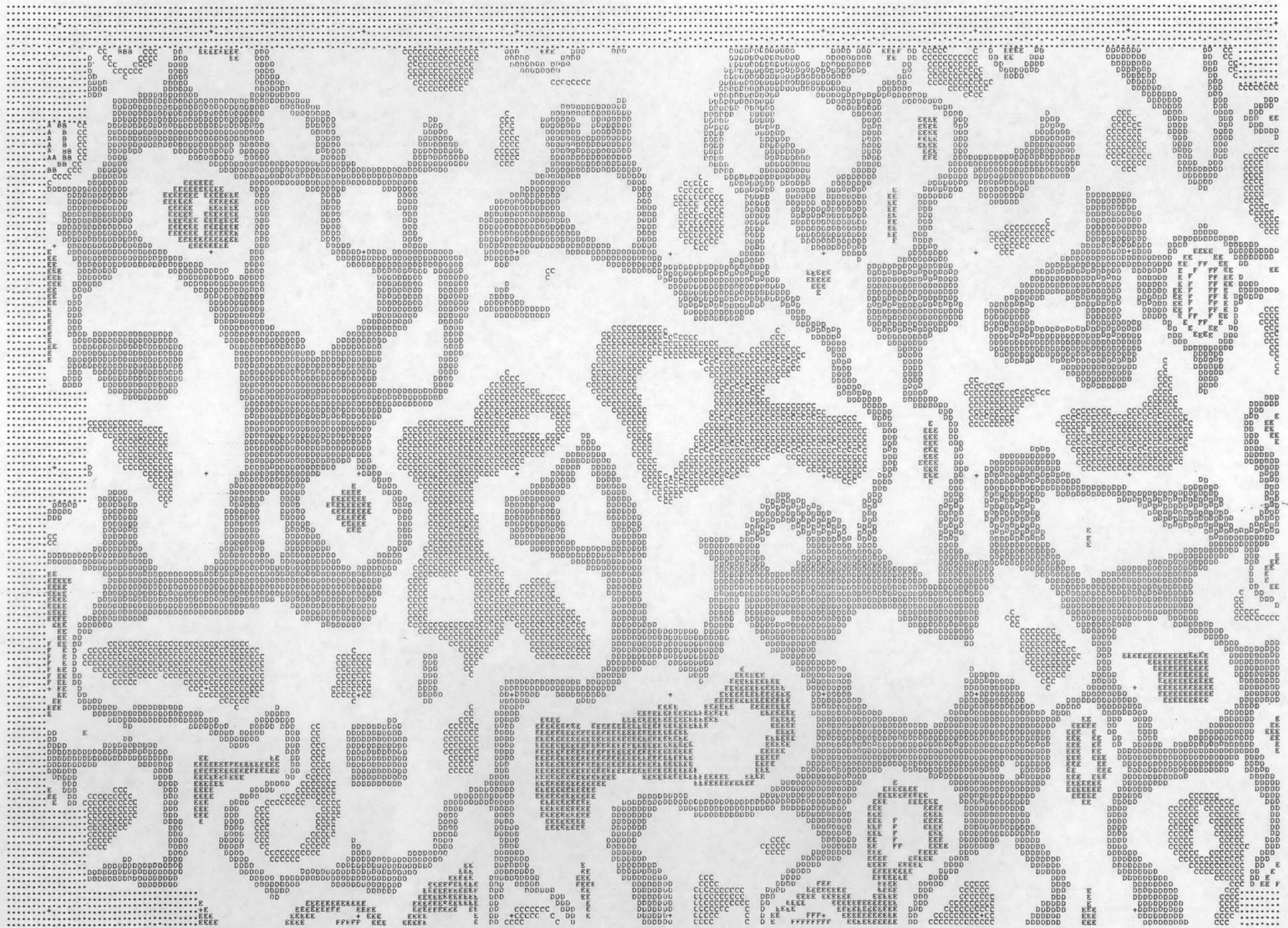


ATV-3 Line Printer Contour

GEODATA INTERNATIONAL, INC.  
DALLAS, TEXAS

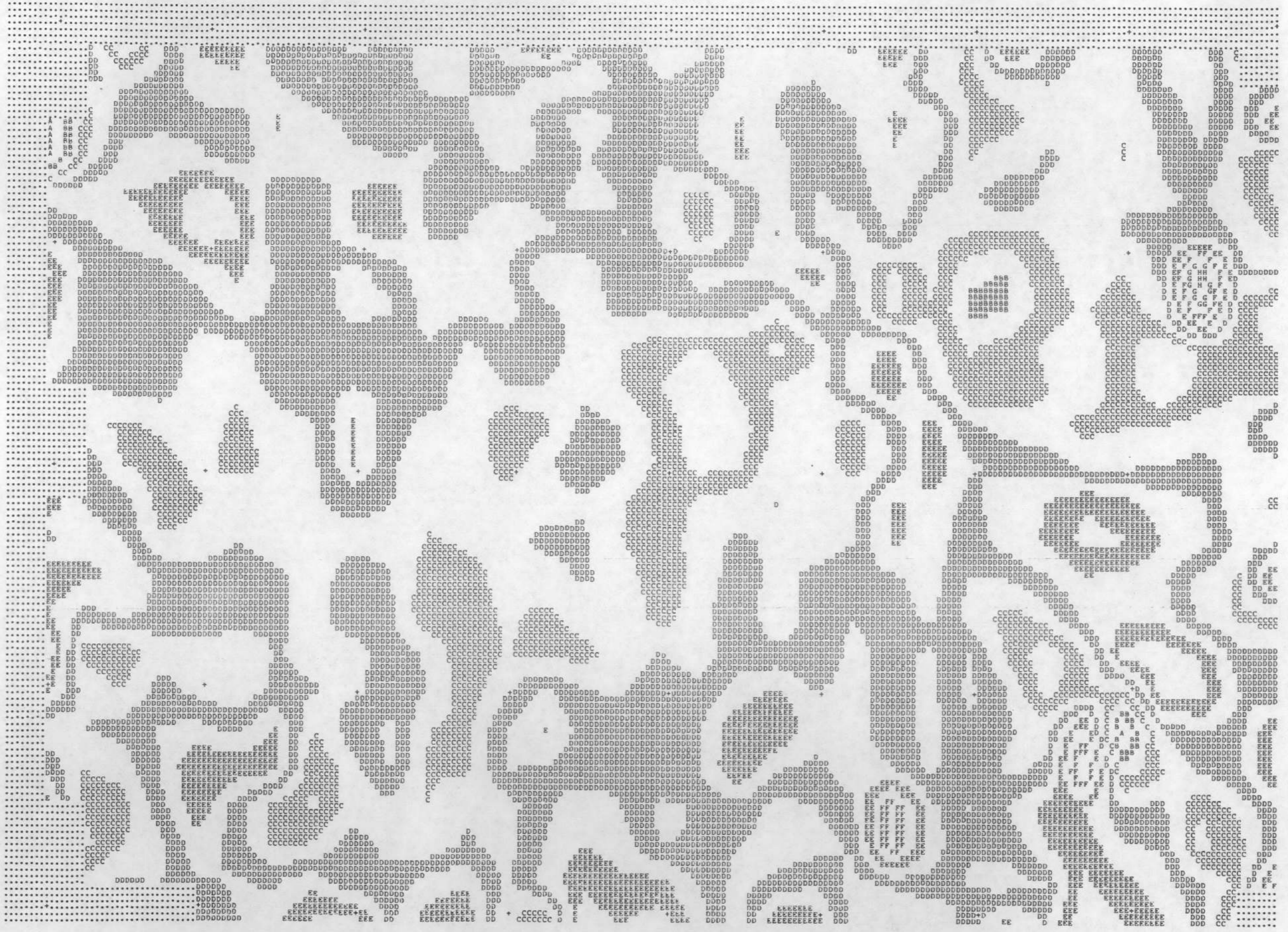
A < 0.360	0.450 < B < 0.540	0.630 < C < 0.720	0.810 < D < 0.900	0.990 < E < 1.080	1.170 < F < 1.260
	1.350 < G < 1.440	1.530 < H < 1.620	1.710 < I < 1.800		





AIW-4 Line Printer Contour



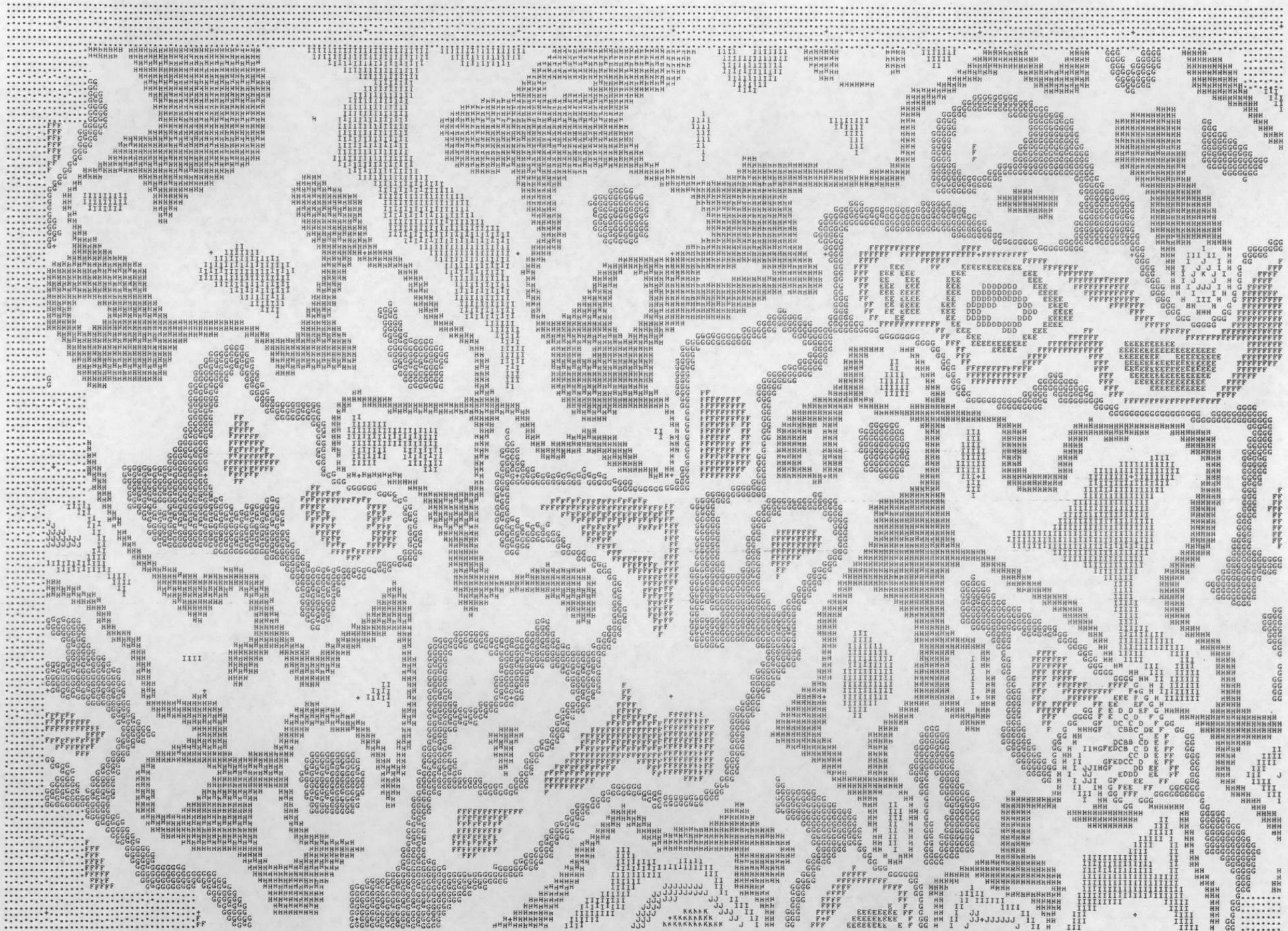


ATI-5 Line Printer Contour

GEODATA INTERNATIONAL, INC.  
DALLAS, TEXAS

A< 0.50 0.70< 0.80 0.90<< 1.00 1.10<<< 1.20 1.30<<<< 1.40 1.50<<<<< 1.60



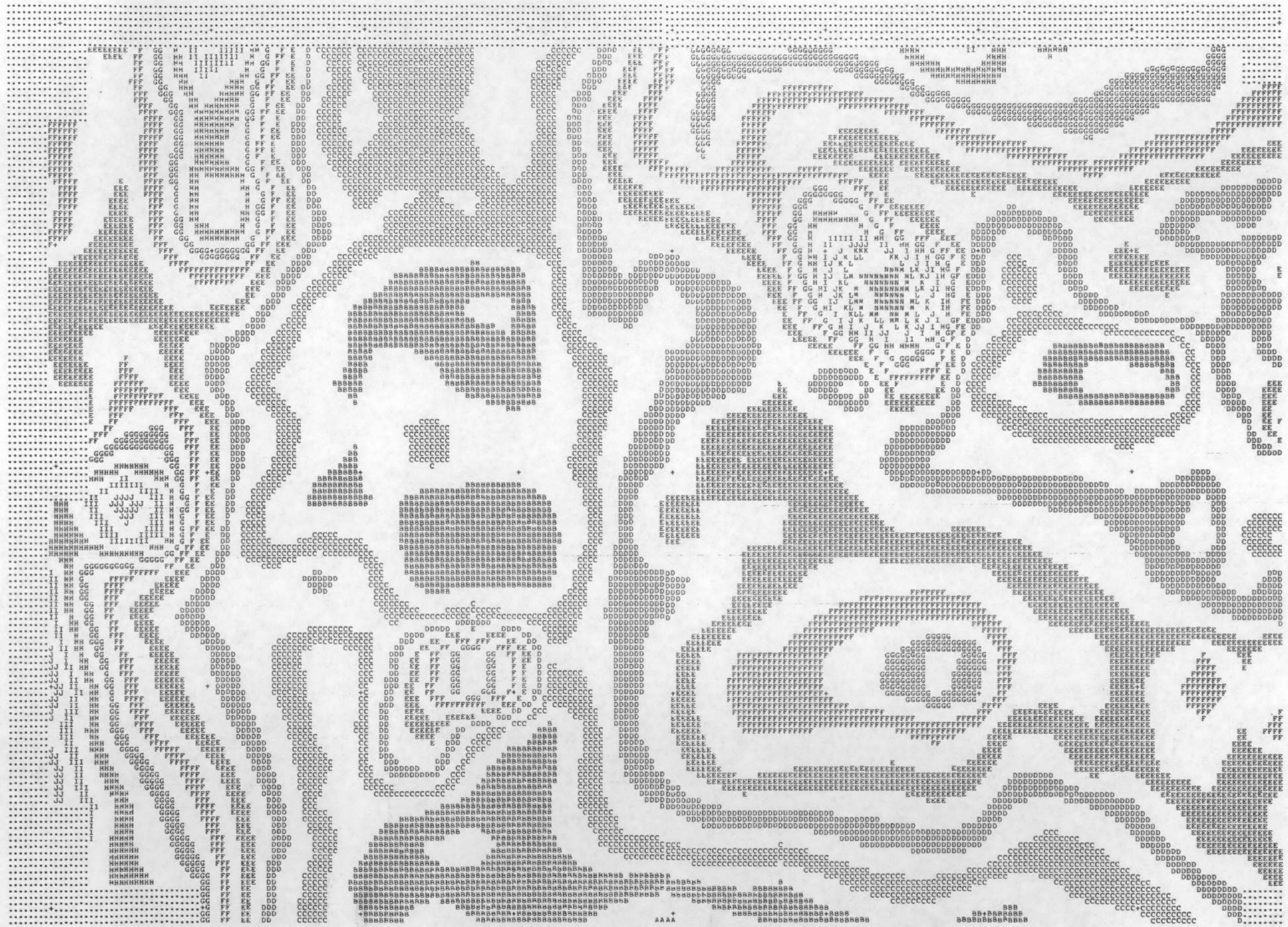


Line Printer Contour

GEDATA INTERNATIONAL, INC.  
DALLAS, TEXAS

A < 2.24	2.40 < 2.56	2.72 < 2.88	3.04 < 3.20	3.36 < 3.52	3.68 < 3.84
	4.00 < 4.16	4.32 < 4.48	4.64 < 4.80	4.96 < 5.12	5.28 < 5.44





Line Printer Contour

GLD DATA INTERNATIONAL, INC.  
 DALLAS, TEXAS

AK < 00.	-560, <K < 520.	-480, <K < 440.	-400, <K < 360.	-320, <K < 280.	-240, <K < 200.
	-160, <K < 120.	-80, <K < 40.	0, <K < 40.	80, <K < 120.	160, <K < 200.
	240, <K < 280.	320, <K < 360.	400, <K < 440.		



## BIBLIOGRAPHY

- Andrews, D.A., 1936, Suggested Fort Union-Lance Correlations in Montana and the Dakotas; Wash. Acad. Sci. Journ., Vol. 26, pp. 387-389.
- Ballard, W.W., 1969, Red River Formation of Northeast Montana and Northwest North Dakota; U.S. Geol. Surv. Bull. No. 906-B, pp. 40-57.
- Collins, S.G., 1954, Geology of the Dakota Badlands; So. Dak. Geol. Surv. Rep. No. 17, pp. 26-42.
- Carlson, C.G., and Freer, T.F., 1975, Geology of Benson and Pierce Counties, North Dakota; No. Dak. Geol. Surv. Bull. No. 59-4, pp. 18-29.
- Carlson, C.G., and Anderson, S.B., 1965, Sedimentary and Tectonic History of North Dakota Part of the Williston Basin; Amer. Assoc. Pet. Geol. Bull. Vol. 49, 11, pp. 1846-1863.
- Darton, N.H., 1909, Geology of the Central Great Plains; U.S. Geol. Surv. Prof. Paper No. 32, pp. 351-373.
- Fenneman, N.M., 1928, Physiographic Divisions of the United States; Amer. Assoc. Geol. Ann., Vol. 24, pp. 460-520.
- Finch, W.I., 1967, Geology of Epigenetic Uranium Deposits in Sandstones of the United States; U.S. Geol. Surv. Prof. Paper No. 538, pp. 68-96.
- Frye, C.I., 1969, Stratigraphy of the Hell Creek Formation in the Dakotas; No. Dak. Geol. Surv. Bull. No. 54, pp. 92-111.
- Hancock, E.T., 1922, New Salem Lignite Field, North Dakota; U.S. Geol. Surv. Bull. No. 726, pp. 7-16.
- Lemke, R.W., and Kaye, C.D., 1953, Geologic Map of Bonbells Quadrangle, North Dakota; U.S. Geol. Surv. Open File Map, Scale 1:48,000.
- Lemke, R.W., 1960, Geology of the Souris River Area, North Dakota; U.S. Geol. Surv. Prof. Paper No. 325, pp. 38-55.
- Lloyd, E.R., 1914, Cannonball Lignite Field, Morton County, North Dakota; U.S. Geol. Surv. Bull. 541, pp. 24-37.
- Martel Laboratories, Inc., 1980, Geology of the Bismarck Quadrangle; Prepared in accordance with Specification No. 1125-C for the U.S. Dept. of Energy, Map, Scale 1:250,000.

(Bibliography Cont'd.)

- N.T.M.S., 1954, National Topographic Map Series, Bismarck, North Dakota Quadrangle; U.S. Geol. Surv. NL14-4, Ltd. Rev. 1976, Map, Scale 1:250,000.
- Randich, P.G., 1979, Geology and Ground Water Studies of Grant and Souix Counties, North Dakota; No. Dak. Geol. Surv. Bull. No. 67-Pt.III, pp. 1-41.
- Vine, J.D., 1962, Geology of Uranium in Coaly Carbonaceous Rocks; U.S. Geol. Surv. Prof. Paper 356-D, pp. 113-170.
- Walker, G.W., and Osterwald, F.W., 1963, Geology of Uranium-Bearing Veins in Conterminous United States; U.S. Geol. Surv. Prof. Paper No. 455-A, pp. 16-46.
- Wilson, R.D., et.al., 1951, Composition and Properties of the Pierre Shale and Equivalent Rocks, Northern Great Plains Region; U.S. Geol. Surv. Prof. Paper No. 106-B, pp. 10-32, 78-112.
- Zeller, G.D., and Schopf, E., 1959, Core Drilling for Uranium Ores, Harding and Butte Counties, South Dakota, and Bowman County, North Dakota; No. Dak. Geol. Surv. Bull. No. 1055-C, pp. 31-42.





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