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User's Guide and Description of the Perturbation Code Modules **DGRAD and TPERT**

E. T. Tomlinson
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COMPUTER SCIENCES DIVISION

USER'S GUIDE AND DESCRIPTION OF THE
PERTURBATION CODE MODULES DGRAD AND TPERT*

E. T. Tomlinson and R. A. Lillie**

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CONTENTS

ABSTRACT	1
1. INTRODUCTION	1
2. TPERT	1
TPERT INPUT	5
3. DGRAD	7
DGRAD INPUT	19
REFERENCES	11
APPENDIX	12

USER'S GUIDE AND DESCRIPTION OF THE PERTURBATION CODE MODULES DGRAD and TPERT

E. T. Tomlinson and R. A. Lillie

ABSTRACT

Two code modules, TPERT and DGRAD, are described, which when used in conjunction with the DOT IV discrete ordinate neutron transport code provide the user with the capability of performing perturbation calculations. The modules and their input are described. A sample problem is presented to aid in executing these modules.

1. INTRODUCTION

The movement and/or replacement of one material by another in a reactor core will cause a change in the system multiplication factor, k_{eff} . The magnitude of this change can be calculated either directly by recalculation of k_{eff} for the perturbed system or through the use of perturbation techniques. The methods incorporated in the code modules described in this report include first-order and exact perturbation theory based on both transport and diffusion theory approximations to the neutron transport equation. These modules were written as ancillary codes to the DOT IV discrete ordinates transport code. All input to these models is done using the free-form input routine FIDO.

2. TPERT

A perturbation code, TPERT, has been written to obtain exact and first-order reactivity changes. The purpose of this section is to provide a brief review of the expressions evaluated by TPERT and to

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provide a detailed description of the required input. TPERT couples with VIP¹ which generates adjoint-forward flux tables, i.e., $\phi^*\phi$ tables, using DOT-III² scalar flux tape information. (A slight modification of VIP will allow the use of DOT-IV scalar flux tapes.)³ The general scheme consists of passing the spatially integrated $\phi^*\phi$ tables from VIP into TPERT which in turn folds the $\phi^*\phi$ tables with the pertinent cross section changes.

The reactivity associated with a change in reactor composition, i.e., a perturbation, may be obtained from:

$$\Delta\rho = \langle\phi^*, (\Delta F/k - \Delta\Sigma + \Delta S)\phi'\rangle / \langle\phi^*, F'\phi'\rangle \quad (1)$$

where

$\Delta\rho$ = reactivity change

ΔF = change in fission operator

$\Delta\Sigma$ = change in total cross section operator

ΔS = change in scattering operator

k = unperturbed state eigenvalue

ϕ^* = unperturbed adjoint flux

ϕ' = perturbed forward flux

$F' = F + \Delta F$ = perturbed fission operator.

The brackets, i.e., $\langle \rangle$, in Equation (1) indicate integration over space, energy and angle. Equation (1) is normally called the exact perturbation equation since there are no approximations employed in its development. The first-order, or linear, approximation to Equation (1) may be obtained by simply substituting the unperturbed forward flux ϕ and the unperturbed fission operator F for ϕ' and F' , respectively.

This yields:

$$\Delta\rho = \langle\phi^*, (\Delta F/k - \Delta\Sigma + \Delta\sigma)\phi\rangle / \langle\phi^*, F_\phi\rangle . \quad (2)$$

The evaluation of the integrals in Equations (1) and (2) is carried out in two steps. The first step is performed by VIP and results in the generation of (L+1), where L is the order of scattering anisotropy, $\phi^*\phi$ tables for each region in which material changes occur or in which fissionable nuclides appear. These tables are ordered in a manner similar to ANISN formatted cross-section tables.

The terms which fold with the total cross section in TPERT are located in position IHT. These terms have the form⁴:

$$T_g = \sum_{L=0}^L \sum_m \sum_l (-1)^{l+1} (2l+1) j_{l,m,i,g}^* j_{l,m,i,g} v_i \quad (3)$$

where

$j_{l,m,i,g}^*$ = the DOT l_m^{th} adjoint flux moment in space cell i and group g

$j_{l,m,i,g}$ = the DOT forward flux moment.

v_i = volume of i^{th} space cell.

The terms which fold with the scattering and fission operators are stored in positions IHS through IHS+G-1 where G represents the total number of groups. These terms have the form⁴:

$$T_{l,g,g'} = \sum_l \sum_m (-1)^{l+1} j_{l,m,i,g}^* j_{l,m,g'} v_i . \quad (4)$$

For a given group g , the subscript g' may take on two values. In positions IHS through IHS+ g -1:

$$g' = g-k+1 \text{ for } k=1, \dots, g$$

and in positions IHS+ g through IHS+G-1:

$$g' = k \text{ for } k=g+1, \dots, G.$$

The second step in the evaluation of the integrals in Equations (1) and (2) is carried out by TPERT. This step consists of folding the terms represented by Equations (3) and (4) with the appropriate cross-section changes for each region. The folding process is described by the following:

$$\langle \phi^*, \frac{\Delta F}{k} \phi \rangle_r = \sum_g \sum_{g'} x_g \frac{\Delta \nu \Sigma_{fg'}}{k} T_{0,g,g'}, \quad (5a)$$

$$-\langle \phi^*, \Delta \Sigma \phi \rangle_r = \sum_g \Delta \Sigma_{Tg} T_g, \quad (5b)$$

and

$$\langle \phi^*, \Delta S \phi \rangle_r = \sum_g \sum_{g'} \sum_\ell \Delta \Sigma_{S\ell, g' \rightarrow g} T_{\ell, g, g'} \quad (5b)$$

where

x_g = fraction of fission neutrons born in group g ,

$\Delta \nu \Sigma_{fg'}$ = change in nu times the fission cross section in group g

$\Delta \Sigma_{Tg}$ = change in total cross section in group g ,

$\Delta \Sigma_{S\ell, g' \rightarrow g}$ = change in ℓ^{th} order scattering coefficient for scattering from group g' to group g .

In Equations (5), the subscript r has been introduced to denote different material regions. The perturbation denominators, i.e., $\langle\phi^*, F'\phi'\rangle$ and $\langle\phi^*, F\phi\rangle$ are evaluated by simply substituting $v\Sigma_{f'g'}$ or $v\Sigma_{fg}$ into Equation (5a) for $\Delta v\Sigma_{fg..}$. Summing the region contributions to $\Delta\rho$ completes the reactivity calculation.

TPERT INPUT

Title Card (18A4)

I\$S IHT - Position of total cross section

IHS - Position of self-scatter cross section

ITL - Cross-section table length

IGM - Number of energy groups

NR - Number of "VIP" regions (see Note 1)

ISCT - Order of scattering anisotropy

NMAT - Number of P_0 materials from tape (see Note 2)

NTAB - Logical unit number of VIP $\phi^*\phi$ tables

NCR - Logical unit number of cross-section tape

NDCR - Direct access logical unit number for cross-section storage (see Note 3)

NSRT - Logical unit for scratch disk (diffusion only)

JFLAG = 0 - use perturbed $v\Sigma_f$ denominator

1 - use unperturbed $v\Sigma_f$ denominator

ITOD = 0 - transport calculation (see Note 8)

1 - diffusion calculation

Terminate data block 1 with a T.

2** CHI (IGM) - Fission spectrum

3** VELS (IGM) - Group inverse velocities - fill with 1.0's if
inverse velocity folding is not desired (see Note 7)

4\$\$ MATID (NMAT)- Cross-section tape ID's for P_0 materials.

Arrays 5\$\$ through 10** apply to the following relationships for a given
VIP region:

$$\Sigma \text{ unperturbed} = U1 * \Sigma_1 + U2 * \Sigma_2$$

$$\Sigma \text{ perturbed} = P1 * \Sigma_1 + P2 * \Sigma_2$$

5\$\$ MAT1 (NR) - P_0 material numbers on direct access storage for
 Σ_1 cross sections by VIP region - use negative
number if region has fissionable material but no
perturbation.

6** U1 (NR) - Unperturbed multiplier for Σ_1 by VIP region

7** P1 (NR) - Perturbed multiplier for Σ_1 by VIP region

8\$\$ MAT2 (NR) - P_0 material numbers on direct access storage for
 Σ_2 cross sections by VIP region - use a zero if
only Σ_1 occurs in a region

9** U2 (NR) - Unperturbed multiplier for Σ_2 by VIP region

10** P2 (NR) - Perturbed multiplier for Σ_2 by VIP region

11** EIG - Unperturbed K_{eff}

BETA - Total delayed neutron fraction

DNORM - Perturbation integral denominator - enter 0.0
if code is to calculate

Terminate data block 2 with a T.

Note 1: Each region which contains a perturbation, i.e., change in
cross section, or which contains fissionable material is a
VIP region.

Note 2: TPERT, as presently programmed, will only accept cross sections
in ANISN library format - either on tape or disk.

Note 3: Direct access is used to store the cross sections in the same order as the ID's in the 4\$\$ array, e.g., if the ID of material M corresponds to the Nth entry in the 4\$\$ array, the P_0 number for this material is N in the 5\$\$ and 8\$\$ arrays.

Note 4: The number of words needed in COMMON/DATA in TPERT main is given by:

$$(3+2^{\times} ITL)*IGM+NMAT*(ISCT+2)+10*NR+40$$

Note 5: The number of tracks needed on logical unit NDCR is given by:

$$((ITL*TGM-1)/1800+1)*NMAT*(ISCT+1)$$

Note 6: To run multiple cases, simply supply a new title card and change the appropriate arrays. Be sure to include a terminator, e.g., T for both data blocks.

Note 7: TPERT will evaluate the quantity $\langle \phi^*, \frac{1}{\rho} \phi \rangle$ which is useful in certain time-dependent reactivity calculations.

Note 8: To run diffusion cases, it is necessary to set ISCT=1 in VIP and input the flux tapes generated by DGRAD.

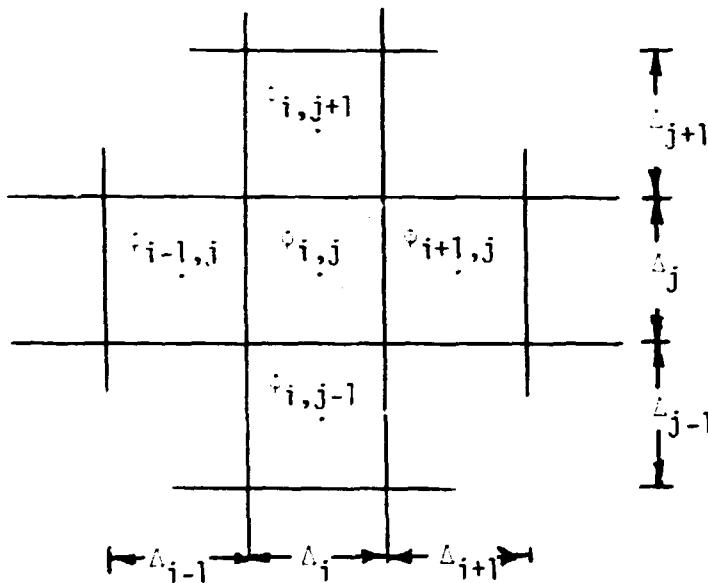
3. DGRAD

A module, DGRAD, was written to calculate the directional flux gradients from DOT III² diffusion theory flux tapes. DOT-IV³ scalar flux tapes can also be used if they are preprocessed in the RTFLUM⁴ module of the DOS⁵ system. The module, DGRAD, in conjunction with VIP and TPERT will allow the use of diffusion theory fluxes to obtain exact and first-order perturbation reactivity changes.

In order to calculate the reactivity associated with changes in reactor compositions using diffusion theory, it is necessary to fold not only the scalar fluxes with the appropriate cross sections, but also the average flux gradients with the diffusion coefficients. Since DOT

diffusion theory does not directly calculate these gradients, it was necessary to calculate the needed quantities external to the DOT code.

Consider the typical mesh cell with cell-centered fluxes



The flux on the left boundary of cell i, j , ϕ_{BL} can be calculated if the current across this boundary is assumed to be continuous.

$$2 D_{i-1,j} \frac{\phi_{BL} - \phi_{i-1,j}}{\Delta_{i-1}} = 2 D_{i,j} \frac{\phi_{i,j} - \phi_{BL}}{\Delta_i}$$

where $D_{i,j}$ is the diffusion coefficient for cell i,j . Solving for

$$\phi_{BL}$$

$$\phi_{BL} = \frac{D_{i,j} \phi_{i,j} \Delta_{i-1} + D_{i-1,j} \phi_{i-1,j} \Delta_i}{D_{i-1,j} \Delta_i + D_{i,j} \Delta_{i-1}} .$$

Similarly for the right boundary

$$\phi_{BR} = \frac{D_{i+1,j} \phi_{i+1,j}^i + D_{i,j} \phi_{i,j}^{i+1}}{D_{i,j}^i + D_{i+1,j}^i} .$$

The R direction gradient can then be obtained as follows

$$\nabla \phi_{i,j}^R = \frac{\phi_{BR} - \phi_{BL}}{\Delta_i} .$$

Similar arguments are used for the calculation of the Z direction gradients.

On the outer boundaries of the problem the following conditions are imposed

For reflected boundaries at

$$i=1 \quad \phi_{0,j} = \phi_{i,j} \quad j=1 \quad \phi_{i,0} = \phi_{i,1}$$

$$\Delta_{0,j} = \Delta_{i,j} \quad \Delta_{i,0} = \Delta_{i,1}$$

$$D_{0,j} = D_{i,j} \quad D_{i,0} = D_{i,1}$$

$$i=IM \quad \phi_{IM+1,j} = \phi_{IM,j} \quad j=JM \quad \phi_{i,JM+1} = \phi_{i,JM}$$

$$\Delta_{IM+1,j} = \Delta_{IM,j} \quad \Delta_{i,JM+1} = \Delta_{i,JM}$$

$$D_{IM+1,j} = D_{IM,j} \quad D_{i,JM+1} = D_{i,JM}$$

For non-return boundaries the flux is assumed to equal zero at the extrapolated boundary

$$i=1 \quad \phi_{0,j} = 0.0 \quad j=1 \quad \phi_{i,0} = 0.0$$

$$\Delta_{0,j} = 1.42089/\Sigma_{TR} \quad \Delta_{i,0} = 1.42089/\Sigma_{TR}$$

$$D_{0,j} = D_{i,j} \quad D_{i,0} = D_{i,1}$$

$$\begin{array}{ll}
 i=IM & :_{IM+1,j} = 0.0 \\
 & :_{IM+1,j} = 1.42089/\cdot_{TR} \\
 & D_{IM+1,j} = D_{IM,j} \\
 j=JM & :_{i,JM+1} = 0.0 \\
 & :_{i,JM+1} = 1.42089/\cdot_{TR} \\
 & D_{i,JM+1} = D_{i,JM}
 \end{array}$$

DGRAD INPUT

Title Card (20A4)

1\$S IFLX - 0/1 Forward/Adjoint
 IM - No. of Radial Intervals
 JM - No. of Axial Intervals
 MZ - No. of Material Zones
 ITL - Cross-Section Table length
 IHT - Position of the Transport Cross Section
 MT - Total Number of Materials
 IGM - No. of Energy Groups
 IBL - Left Boundary Condition 0=VAC 1=REF
 IBR - Right Boundary Condition
 IBT - Top Boundary Condition
 IBB - Bottom Boundary Condition
 IP1 - 0/1 Diffusion/Hybrid Output (see Note 2)
 NIN - Flux Input Unit
 NOUT - Flux Output Unit
 NSEC - Cross-Section Input Unit
 ISCRT - Scratch Unit
 IPRT - 0/1 Print/No Print Flux and Gradients

Data Block must be terminated with a T.

4** (IM+1) Radial Boundaries
 5** (JM+1) Axial Boundaries
 6\$\$ (IM*JM) Zone Number By Interval
 7\$\$ (MZ) Material By Zone

Data Block must be terminated with a T.

Note 1. To run multiple simply supply a new title card and input all the arrays and T's.

Note 2. If IP1 is set equal to zero the scalar flux and the flux gradients are output for the TPERT diffusion perturbation calculation. If IP1 is set equal to 1 the scalar flux and the partial currents are output for the VIP transport integral calculation. VIP is then run as if it were doing a normal P_1 transport problem. The latter option allows for including the P_1 scattering effects and implicit calculation of neutron leakage worths.

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1. R. L. Childs, "VIP, A Computer Program Using Two-Dimensional Discrete Ordinates Transport Calculations for Cross Section Sensitivity Analysis," UCCNG/CSD-1 (to be published).
2. W. A. Rhoades and F. R. Mynatt, *The DOT-III two-dimensional Discrete Ordinates Transport Code*, ORNL/TM-4280, 1973.
3. R. L. Childs, personal communication, 1977.
4. R. L. Childs, D. E. Bartine and W. W. Engle, Jr., "Perturbation Theory and Sensitivity Analysis for Two-Dimensional Shielding Calculations," *Trans. Am. Nucl. Soc.*, 21:543, June 1975.
5. W. A. Rhoades, personal communication, 1977.

A-1

APPENDIX

SAMPLE PROBLEM

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DGRAD

FURNACE UNAVAILABILITY

13 AMRAY 16 ENRILES READ
CT

0 14 FURNACES/AVAILABLE
0 20 UF RADIAL INFLUXES
0 20 UF AXIAL INTERVALS
420 UF MATERIAL UNITS
114 X-DRILL TIME UNITS
150 UF TRANSPORT ADRIVE
15 TOTAL NO. OF MATERIALS
2 JF ENERGY UNITS
1 LEFT SURFACE LUMINOSITY VAL 1.E-12
1 RIGHT SURFACE LUMINOSITY
100 TOP SURFACE LUMINOSITY
100 BOTTOM SURFACE LUMINOSITY
100 DIFFUSION COEFFICIENT
1 FLUX INPUT UNIT
1 FLUX OUTPUT UNIT
3 CRUSH SELECTION INPUT UNIT
4 SCRATCH UNIT NUMBER
1 PRINT/NU POINT

44 AMRAY 49 ENRILES READ & RADIAL INTERVAL BOUNDARIES
54 AMRAY 64 LNTRLS READ & AXIAL INTERVAL BOUNDARIES
68 AMRAY 6134 ENRILES READ & ZONE NUMBER BY INTERVAL
74 AMRAY 120 ENRILES READ & MATERIAL NUMBER BY ZONE

01 32905 NUMBER NECESSARY TO GO UNITS AVAILABLE
FLUX FURNACES 1 HAS 1 LEN MATERIAL UNITS UNITS NUUT
FLUX FOR GROUP 2 HAS 2 LEN MATERIAL UNITS UNITS NUUT
FLUX FOR GROUP 3 HAS 3 LEN MATERIAL UNITS UNITS NUUT
FLUX FOR GROUP 4 HAS 4 LEN MATERIAL UNITS UNITS NUUT
FLUX FOR GROUP 5 HAS 5 LEN MATERIAL UNITS UNITS NUUT
FLUX FOR GROUP 6 HAS 6 LEN MATERIAL UNITS UNITS NUUT
FLUX FOR GROUP 7 HAS 7 LEN MATERIAL UNITS UNITS NUUT
FLUX FOR GROUP 8 HAS 8 LEN MATERIAL UNITS UNITS NUUT
FLUX FOR GROUP 9 HAS 9 LEN MATERIAL UNITS UNITS NUUT
FLUX FOR GROUP 10 HAS 10 LEN MATERIAL UNITS UNITS NUUT

ADJOINT GRADIENTS

15 ARRAY 18 ENTRIES READ

OT

1 0/1 FORWARD/ADJOINT
 98 NU. OF RADIAL INTERVALS
 83 NU. OF AXIAL INTERVALS
 126 NU. OF MATERIAL ZONES
 14 X-SCL TABLE LENGTH
 5 POSITION OF TRANSPORT X-SCL
 18 TOTAL NU. OF MATERIALS
 9 NU. OF ENERGY GROUPS
 1 LEFT BOUNDARY CONDITION 0=VAL 1=REF
 0 RIGHT BOUNDARY CONDITION
 0 TOP BOUNDARY CONDITION
 0 BOTTOM BOUNDARY CONDITION
 1 0/1 DIFFUSION/HI OUTPUT
 10 FLUX INPUT UNIT
 11 FLUX OUTPUT UNIT
 3 CROSS SECTION INPUT UNIT
 4 SCRATCH UNIT NUMBER
 1 PRINT/NU PRINT

4* ARRAY 44 ENTRIES READ

5* ARRAY 84 ENTRIES READ

6* ARRAY 8134 ENTRIES READ

7* ARRAY 128 ENTRIES READ

OT

32903 WORKS NECESSARY 32900 WORKS AVAILABLE

FLUX FOR GROUP	1 HAS BEEN WRITTEN ON UNIT NUOT
FLUX FOR GROUP	2 HAS BEEN WRITTEN ON UNIT NUOT
FLUX FOR GROUP	3 HAS BEEN WRITTEN ON UNIT NUOT
FLUX FOR GROUP	4 HAS BEEN WRITTEN ON UNIT NUOT
FLUX FOR GROUP	5 HAS BEEN WRITTEN ON UNIT NUOT
FLUX FOR GROUP	6 HAS BEEN WRITTEN ON UNIT NUOT
FLUX FOR GROUP	7 HAS BEEN WRITTEN ON UNIT NUOT
FLUX FOR GROUP	8 HAS BEEN WRITTEN ON UNIT NUOT
FLUX FOR GROUP	9 HAS BEEN WRITTEN ON UNIT NUOT

INCORRECT STOP 123

DGRAD

A-3

VIP FOR R-Z DISRUPTED CORE ANALYSIS

18 ARRAY 11 ENTRIES READ

28 ARRAY 10 ENTRIES READ

JT

CONTROL PARAMETERS

1 ID -- PROBLEM IDENTIFICATION NUMBER (MUST BE POSITIVE)
28 IM -- NUMBER OF RADIAL INTERVALS
83 JM -- NUMBER OF AXIAL INTERVALS
128 IZM -- NUMBER OF ZONES (LARGEST ENTRY IN THE BS OR YS ARRAY)
1 ISCT -- MAXIMUM DEGREE OF LEGENDRE EXPANSION (MUST NOT EXCEED A03 IN DLT INPUT)
9 IGM -- NUMBER OF ENERGY GROUPS
1 IGE -- 0/1/2 X-Y / R-Z / R-THETA GEOMETRY
5 IHT -- TABLE POSITION OF TOTAL CROSS SECTION IN SWANLAKE PROBLEM
14 ITL -- CROSS SECTION TABLE LENGTH IN SWANLAKE PROBLEM
2 IFESS -- 1/2 NONFISSION SWANLAKE / FISSION SWANLAKE
6 IPRT -- 0/N NU EFFECT / PRINT THE (PHI*) (PHI) MATRIX FOR REGIONS 1 THROUGH N.

INPUT/OUTPUT PARAMETERS

0 NUF -- 0/N NU EFFECT / READ UNCOLLIDED FORWARD FLUX MOMENTS FROM UNIT N.
0 NUA -- 0/N NU EFFECT / READ UNCOLLIDED ADJOINT FLUX MOMENTS FROM UNIT N.
1 NFF -- LOGICAL UNIT FOR THE FORWARD SCALAR FLUX TAPE
2 NAF -- LOGICAL UNIT FOR THE ADJOINT SCALAR FLUX TAPE
5 NTF -- OUTPUT UNIT FOR THE (PHI*) (PHI) TAPE
5 NIN -- INPUT UNIT (NORMALLY 5)
6 NUU -- OUTPUT UNIT (NORMALLY 6)
30000 LBL -- BLKSIZE IN THE FBSAM DD STATEMENTS
10 NBL -- MAXIMUM NUMBER OF BLOCKS PER LOGICAL RECORD (FBSAM UNITS ONLY)
1 NERC -- 0/1 FOLLOW FBSAM LRKRN PROCEDURES / IGNORE FBSAM I/O ERRORS

THE MESH IS DIVIDED INTO 5 BLOCKS
66464 STORAGE LOCATIONS USED

28 ARRAY 84 ENTRIES READ

48 ARRAY 99 ENTRIES READ

88 ARRAY 6134 ENTRIES READ

98 ARRAY 128 ENTRIES READ

01

VIP

150

AIA

244

CASE 4 EXACT PI PERT

IS ARRAY

13 ENTRIES READ

TPERT

OT

2* ARRAY 9 ENTRIES READ

3* ARRAY 9 ENTRIES READ

4* ARRAY 17 ENTRIES READ

5* ARRAY 128 ENTRIES READ

6* ARRAY 128 ENTRIES READ

7* ARRAY 128 ENTRIES READ

8* ARRAY 128 ENTRIES READ

9* ARRAY 128 ENTRIES READ

10* ARRAY 128 ENTRIES READ

11* ARRAY 3 ENTRIES READ

OT

6-A

CASE 4 EXACT PI PERI

INPUT CONSTANTS

IHS	POSITION OF TOTAL CHUUS SECTION	5
ILS	POSITION OF SELF-SLATER CHUUS SECTION	6
ILL	CHUUS SECTION TABLE UNIT	14
IGM	NUMBER OF ENERGY CHUUS	15
NR	NUMBER OF VIP MATERIALS	16
ISCT	ORDER OF SCATTERING MATERIALS	17
NMAT	NUMBER OF PC INPUT MATERIALS	18
NTAB	LUGICAL UNIT NUMBER OF VIP PRIM-PRIM* VOLUME INTEGRATED TABLE	1
NCR	LUGICAL UNIT NUMBER OF INP CHUUS SECTION LIBRARY	2
NUCK	SIMUL ACCES LUGICAL UNIT NUMBER FOR CHUUS SECTION STORAGE	3
NSRT	SCRATCH DISK UNIT NUMBER	4
JFLAG	0/1 = USE PERTURBED DENUMINATOR/UNPERTURBED UNDENUMINATOR	5
ITUU	0/1 = TRANSFORM CALCULATION/DIFFUSION CALCULATION	6

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REACTIVITY CONTRIBUTION DUE TO CHANGE IN SCATTERING CROSS SECTION	=	-1.977310E-05
REACTIVITY CONTRIBUTION DUE TO CHANGE IN DIFFUSION COEFFICIENT	=	0.0
PERTURBATION INTEGRAL DENOMINATOR	=	3.744934E-08
TOTAL REACTIVITY CHANGE (DOLLARS)	=	1.302676E 00
INTEGRAL OVER INVERSE VELOCITY	=	4.721234E-06

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