KELVIN RARE GAS ~~TIME-OF-FLIGHT~~ PROGRAM

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TABLE OF CONTENTS

I.	Theory and Methods for TOF Calibration	1
II.	Time of Flight Program KELVIN Description and Directions for Use	14
III.	KELVIN Program Listing with Sample Output	17

I. Theory and Methods for TOF Calibration.

The purpose of this appendix is to explain in detail the procedure for performing time-of-flight (TOF) calibration measurements. The result of the calibration measurements is to assign a correct length (L) to the path the molecules travel in a particular experimental configuration. In conjunction with time information (t) a velocity distribution (L/t) can then be determined.

To measure the flight path from the interaction zone or TOF wheel to the ionizer a known velocity distribution is used as calibrant. The standard practice is to use the rare gas nozzle distributions which are defined by assuming a Maxwellian velocity distribution superimposed on the bulk flow velocity. Because the electron bombardment ionizer is sensitive to number density, the velocity dependence of the assumed number density distribution is important. From standard texts¹ a Maxwellian velocity distribution is

$$\frac{1}{e} \frac{M}{2kT_s} \left(v_x^2 + v_y^2 + v_z^2 \right) dv_x dv_y dv_z \quad (1)$$

where T_s is the source temperature. For our model, this is the distribution an observer would see moving at the flow velocity where T_s is the terminal beam temperature (usually $\leq 10^\circ\text{K}$ for rare gases). However, the observations made in the laboratory frame distort the distribution because of the constraints imposed on the molecular trajectories by the defining apertures.

Let the +z direction be along the beam centerline. For practical measurements the nozzle can be treated as a point source^{2a, 2b} and the detector as a circular disk of radius r at a distance L from the nozzle. The flow velocity is $v_z \hat{z}$ so the laboratory frame velocity is $v_x \hat{x} + v_y \hat{y} + (v_z + v_F) \hat{z}$ where (v_x, v_y, v_z) is the velocity in the mass flow frame of reference. The detector aperture limits the transverse velocity perpendicular to the beam axis by $(v_{\text{transverse}})/(v_z + v_F) \leq \frac{r}{L}$. The laboratory number density distribution of velocities (v_L) is then

$$e^{-\beta v_z^2} dv_z \int_0^{\frac{r}{L}(v_z+v_F)} e^{-\beta \rho^2} d\rho = e^{-\beta (v_L - v_F)^2} \left(e^{-\beta v_L^2 r^2 / L^2} - 1 \right) dv_L \quad (2)$$

where $\rho = \sqrt{v_x^2 + v_y^2}$, $\beta = \frac{M}{2kT_s}$ and $v_L = v_z + v_F$. For a standard detector arrangement, $\frac{r}{L} \approx \frac{0.005}{5}$ and the expression (2) can be expanded as

$$e^{-\beta (v_L - v_F)^2} \left(1 - \beta v_L^2 \frac{r^2}{L^2} + \frac{\beta^2}{2} \left(\frac{v_L r}{L} \right)^4 + \dots - 1 \right) \quad (3)$$

The speed ratio is defined as $\sqrt{\beta} v_F = \alpha$ so (3) becomes

$$e^{-\beta (v_L - v_F)^2} \left(\alpha^2 \left(\frac{v_L}{v_F} \right)^2 \left(\frac{r}{L} \right)^2 - \alpha^4 \left(\frac{v_L}{v_F} \right)^4 \left(\frac{r}{L} \right)^4 + \dots \right)$$

When the exponential term is maximized ($v_L = v_F$), the second term in the

power series expansion will be negligible when $\frac{\alpha^2}{2} \left(\frac{v_L}{v_F} \frac{r}{L} \right)^2 = \frac{\alpha^2}{2} \left(\frac{r}{L} \right)^2 \leq 0.01$. This holds for typical $\frac{r}{L}$ values when $\alpha \leq 100$. For all beams except high pressure He beams or H₂ seeded beams, the speed ratios are usually much less than this value. For speed ratios near 100, the distributions are then sufficiently narrow with respect to the dwell time and ionizer resolution that the width cannot be directly measured with the present flight lengths, so the approximation can be used for all α .

In conclusion, the observed velocity distribution is proportional to

$$v_L^2 e^{-\beta(v_L - v_F)^2} dv_L \quad (4)$$

when $\alpha^2 \left(\frac{v_L}{v_F} \right)^2 \left(\frac{r}{L} \right)^2 \leq 0.01$. This expression agrees with that derived by Habets^{2b} using somewhat different arguments. To compare with the result from the multichannel scaler (MCS) the Jacobian from velocity to time is $dv_L = \frac{v_L^2}{L} dt$. The number density distribution experimentally measured is then

$$\frac{v_L^4}{L} e^{-\beta(v_L - v_F)^2} dt \quad (5)$$

with $v_L = \frac{L}{t}$ and t regarded as the independent variable.

The procedure is to use (4) with known rare gas expansion conditions so that v_F and β can be determined. By using the time location of the observed peak (t_p) in the velocity distribution (4), the effective length L to the ionizer can be determined by $L = v_p^* t_p$.

The direct output from the MCS can be used to obtain a good first approximation to L. First, the total time offset must be measured.

The time offset is given by

$$t_{\text{offset}} = t_E - t_{\text{ion}} - t_{\text{trigger}} + t_D + t_W$$

where t_E is the electronic offset given by the time between the leading edge of the trigger pulse at the MCS trigger input and the maximum of the photodiode signal, t_{ion} is the ion flight time to be described below, t_{trigger} is the width of the trigger pulse sent to the MCS and t_D is a deliberate offset to displace the TOF for long flight paths. t_{wheel} is the time delay resulting from the offset between the peak of the photodiode signal and when the wheel slit is centered on the detector slit. t_{wheel} is measured by rotating the wheel clockwise and counterclockwise and averaging the two results. The t_{trigger} delay results from the design of MCS. The 1 MHz internal clock is disabled for the duration of the trigger pulse, so the clock begins to decrement the dwell time counter within 50 nsecs after the end of the trigger pulse. The ion flight time is determined by measuring the difference in mass peaks originating from a common molecule. The use of multiply charged rare gas ions has been observed to result in incorrect (over-estimation) of ion flight times. D. Krajnovich has used CF_3I in He to obtain narrow velocity distributions with mass fragments over a large range. The possible source of error in this method is the translational

energy released in fragmentation which could distort the measurement. A comparison of the fragment distribution widths will indicate if this is important. The various mass fragment peaks can be used to fit the expression $C\sqrt{M}$. For 75 volt ions and 250 volt extraction voltage the canonical value for C is 3 $\mu\text{secs}/\sqrt{\text{amu}}$.

The predicted maximum velocity from eqn. (5) is

$$V_P = \frac{V_F}{2} + \frac{V_F}{2} \sqrt{1 + \frac{4}{8V_F^2}} \quad \text{or} \quad V_F = \frac{V_P^2 - 1.0/8}{V_P} \quad (6)$$

where

$$V_F \text{ (cm/sec)} = 2.039 \times 10^4 \sqrt{\frac{T_{\text{nozzle}}(^{\circ}\text{K}) - T_{\text{terminal}}(^{\circ}\text{K})}{M(\text{amu})}}$$

The nozzle temperature is measured with a thermocouple using an ice bath reference. The terminal temperature is obtained from the half width of the velocity distribution by

$$T_{\text{terminal}}(^{\circ}\text{K}) = 8.679 \times 10^{-9} m(\text{amu}) (\Delta v(\text{cm/sec}))^2 \quad (7)$$

where

$$\Delta v = \frac{L \cdot \Delta t}{t_{1/2} \cdot t_0 \cdot t_{\text{Dwell}}}$$

L is the flight length to be determined and can be guessed by previous

knowledge for an initial correction. Δt is the number of channels between the maximum and half height of the distribution, $t'_{1/2}$ is the half height channel number corrected for the offset time, t'_0 is the peak channel number corrected for the offset time, and t_D is the dwell time. Using these values $L(\text{cm}) = V_p(\text{cm/sec}) * t'_0(\text{sec})$. The agreement between L values determined from Ar, Kr, Xe expansions should be $\pm 0.3\%$.

To compare the accuracy of this direct method the more accurate fitting by the KELVIN program was used to iterate on T_{terminal} and L until agreement was found. The results are reported in Table 1.

The source of errors which can bias the above procedure which are within experimental control are the purity of rare gas used for calibration and the count rate limitations of the MCS. The first effect can be quite noticeable because several minutes after flowing a new rare gas it is still possible to detect a clean TOF at the preceeding mass. The experimentalist should wait until all traces of the old gas disappear. Gas cylinders can contain impurities when they are low in pressure. A cursory mass scan at atmospheric and rare gas peaks during the purge time can check for this source of contamination.

The second effect cannot be solved by using the average observed count rate on the count rate meter, since most of the signal is arriving in a small time interval, roughly $1/200$ of the rate meter duty cycle. The MCS scalers are rated at ~ 30 MHz with a minimum data pulse width of 20 nanoseconds. For 1% accuracy in the largest channel the count rate should not exceed 1 MHz.

An additional source of bias was thought to be the manner in which the dual scalers toggle back and forth as the channels advance. If a data pulse is present at the transition from one channel to the next, then depending on its width four alternatives are possible. First, if the data pulse is short, then the partial pulse transmitted to either scaler will be too short to trigger the counters. Conversely, if each portion is sufficiently long then the pulse will be counted twice. The intermediate range is when one half of the pulse is sufficient and the other not to trigger the corresponding counter. These effects were empirically investigated using a digital delay generator/pulse generator arrangement to measure the delay between a single data pulse relative to the trigger pulse with an accuracy of 10 nanoseconds. The results are shown in Fig. 1. From these measurements it is seen that for pulse widths greater than 30 nanoseconds, the multiple counting dominates. However, the effect of the problem is not significant except for very large total counts. The reason for this is as follows.

Assume the data in channels $i, i+1$ is fit by a linear equation to be determined below. If C_i, C_{i+1} are the total counts in these channels, then

$$Y = \frac{(C_{i+1} + C_i)}{2t_i t_d} X + \frac{C_{i+1} + C_i}{2t_d} + \frac{(C_i - C_{i+1})t_i}{t_d^2}$$

where t_i is the i^{th} channel time, t_d the dwell time, and

$$C_{i+1} = \int_{t_i}^{t_{i+1}} y dx; \quad C_i = \int_{t_{i-1}}^{t_i} y dx.$$

The number of counts centered about the channel transition in a time interval 2Δ is

$$\int_{t_{i-\Delta}}^{t_{i+\Delta}} y dx = \frac{\Delta(C_{i-1} + C_i)}{t_p} = \frac{\Delta}{t_p} \bar{N}.$$

Consequently, for $\Delta = 30$ nanoseconds, $t_D = 2$ microseconds the correction is $4.5 \times 10^{-3} \bar{N}$ where 30% overcounting has been assumed. This compares with the statistical error $\sqrt{\bar{N}} = \bar{N} * 4.5 \times 10^{-3}$ when $N = 5 \times 10^5$ counts. With longer dwell times the effect is even less important.

The behavior on the 1 microsecond dwell time scale is not nearly as good as the 2 microsecond results and should be avoided. The data presented here refers to one particular MCS unit and may not be transferable to other units.

The imperfect gas correction to the enthalpy for Ar at 1000 torr, 288°K amounts to $\sim 0.2\%^{2b}$ and can be neglected here in determining V_o (Eqn. 6) from the nozzle temperature. Condensation effects will perturb the terminal temperature and velocity by the heat of condensation added to the flow and by ionizer fragmentation to the monomer mass. This can be checked by observing higher polymer masses, and lowering the pressure if necessary.

Several studies^{2b} have shown that a two component velocity distribution gives a much improved fit to the data. This was not investigated but the systematic differences observed in the calculated and experimental data here are similar to those reported by the above studies using a one component distribution. For chemical accuracy, the one component fit is adequate.

The assumption of the one component distribution was tested indirectly by attempting a direct deconvolution of the measured distribution. For every channel, a narrow velocity distribution ($R = 10^6$) centered on that channel was convoluted over the ionizer and shutter functions. The spread of this "delta function" input into adjacent channels defines a matrix C which takes the true channel distribution into the observed one. The inverse of this matrix $C^{-1} = D$ will then relate the observed channel space distribution to the true distribution free of ionizer and shutter effects. This deconvoluted distribution can then be transferred simply to a velocity distribution. In Fig. 2 is shown the results for two rather different expansions, a high pressure He beam and a He/N_2 anti-seeded beam. The high pressure beam shows that the distribution is completely contained within the convolution effects. The large oscillations are a result of the narrow distribution and the change in sign of adjacent entries of the inverse matrix, D . A simple two channel average removes this effect noticeably. The anti-seeded distribution shows no significant difference between the measured and deconvoluted results. This is a consequence of the broadness of the distribution. The direct deconvolution

result is not as useful as the trial and fit method because the information is not as compact as the simple two parameter fit. It is useful as a guide to the magnitude of the broadening induced by the measurements.

For laser photofragmentation experiments the distance from the collision zone to the TOF wheel must be added onto the TOF distance. This is done by measuring the distance with the transit while the wheel is spinning to reduce the warp error caused by the 5 mil stainless steel wheel material.

The effect of emission current and extractor voltage effect the modeling of the detection process by a nonuniform electron distribution which can shield the ions from the extraction field or ionize the neutral species nonuniformly. These can be experimentally measured by using a narrow He beam whose experimental width is dominated by the ionizer. Until this behavior is known, a more accurate deconvolution of the TOF spectra is not warranted.

REFERENCES

1. F. Reif, Fundamentals of Statistical and Thermal Physics, p. 264, McGraw-Hill (1965).
2. (a) U. Bossel, R. David, M. Faubel, K. Winkelmann, Rarefied Gas Dynamics, p. 235.
(b) A. Habets, "Supersonic Expansion of Argon into Vacuum", Ch. 2,5 Thesis, University of Eindhoven, Holland, 1977.

Table 1. Comparison of computer fitted parameters with those obtained by iteratively solving Equations 6,7 in the text.

	Computer Fit			Iterative Fit					
	L(cm)	β	$v_0 (10^4 \text{ cm/sec})$	First Iteration			Second Iteration		
				L	β	v_0	L	β	v_0
Ar	16.46	2.751	5.517	16.75	2.662	5.616	16.544	2.740	5.536
Kr	16.46	5.136	3.807	16.75	4.970	3.875	16.512	5.115	3.820
Xe	16.46	8.111	3.058	16.75	7.838	3.113	16.477	8.067	3.068

FIGURE CAPTIONS

Fig. 1. Transition effects in the dual scalars (a) 25 nanosecond data pulse width, 2 microsecond dwell time. (b) 40 nanosecond data pulse width, 2 microsecond dwell time. (c) 50 nanosecond data pulse width, 2 microsecond dwell time. (d) 40 nanosecond data pulse width, 3 microsecond dwell time. ▲ total counts in channels 10 and 11. ■ total counts in channel 10. ● total counts in channel 11.

Fig. 2. (a) Deconvoluted He beam. — Initial data. ● Deconvoluted data. ▲ Deconvoluted with 2 channel average. (b) Deconvoluted He/N₂ beam. ● Initial data. ▲ Deconvoluted data (displaced by one channel).

XBL 813-8538

Fig. 1

-13b-

XBL 813-8537

Fig. 2

II. Time of Flight Program KELVIN and Directions for use.

This section describes the salient features of the program KELVIN used to fit time of flight data to deduce velocity distributions. The current version draws heavily on its predecessor written by J. Valentini. Its basic difference is to improve efficiency in the calculation by using a digital filter devised by R. Sparks. It also has an improved search procedure to find the best fit parameters.

The nominal structure is to simulate the effects of the finite ionizer length and slit widths on a measured velocity distribution by calculating a shutter function for the channel space slit overlap which is used as a digital filter. This is applied to the trial velocity distribution which has been convoluted for the ionizer length. The ionizer is treated as a simple sum of 10 identical point ionizers with slightly different lengths from the collision zone. Using a Marquardt algorithm, the parameters are varied until one of three criteria is satisfied.

- 1) The change in parameters is less than 0.005 of their respective magnitudes.
- 2) The value of χ^2 has reached a value such that the data has been fit to the 90% confidence limit.
- 3) Twenty complete iterations have occurred without either 1) or 2) occurring.

KELVIN can analyze any number of time of flights. Each velocity distribution needs the same number of input cards. The final data set

is followed by a blank card. To use the program which is stored on disk, use the following control cards.

JOB CARD

USER PR

FETCHPS, VDW, LGO/RR, KELOBJ.

LGO.

EXIT.

DUMP, 0.

GRUMP.

7/8/9

Input cards needed for each velocity distribution (all numbers F10.1 format, except where noted).

Card

1. Title
2. Mass (amu), channel width (μ sec), nominal neutral flight length (cm), ionizer length (cm), channel offset (channels).
3. Beginning channel number, ending channel number (215).
4. Wheel frequency (Hz), wheel diameter (cm), wheel slit width (mm), collimating slit width (mm).
5. etc. Data (8F10.1)

Output consists of the title with a list of the parameters used, followed by the input data, and the shutter function in channel space. Offset has the opposite effect from the ion flight time, i.e. offset is directly added to the channel number.

The intermediate reduced standard deviations and parameter changes are listed with each iteration.

The final parameters are listed along with the number of iterations, calculated data, and the change in the fitted parameters that would produce a χ^2 greater than at the minimum.

A graph of the two distributions is also produced.

The parametrized velocity distribution has the form

$$P(v) \sim v^2 e^{-\beta(v-v_0)^2}$$

where v_0 is the mass flow velocity, and $\beta = 1/(\text{ALPHA})^2$, where alpha is the average relative velocity in the mass flow frame of reference. The speed ratio is the dimensionless number $\sqrt{\beta} * v_0$. The flow velocity is in units of 10,000 cm/sec.

```

1      PROGRAM KELVIN(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)
      COMMON/PAIR/CHAN,LNID,DL,RCHAN,ECHAN,MCHAN,MASS,MAXP,OFFSET
      COMMON/TRIP/NIOT,HZ,DIA,SA,SD,TRP1(9),TRISZ,ITRSHF,ITLAG
      DIMENSION EXPT(255),SIGCAL(255),SIGCA1(255),SIGCA2(255)
      DIMENSION YPL1(256),YPL2(256),XPL(256)
      REAL MASS,LNID
      INTEGER RCHAN,ECHAN,MCHAN

10     C      INPUT DATA
      C
      C      1003 CALL INDATA(EXPT,META,VZRO)
      C
      C      FITTING ROUTINE TAKEN FROM "DATA REDUCTION AND ERROR ANALYSIS
      C      FOR THE PHYSICAL SCIENCES" BY PHILIP R. BEVINGTON.
15     C      PROGRAM 11-5 CURFIT WHICH IS A MARQUARDT ALGORITHM FOR A NON-
      C      LINEAR LEAST SQUARES FIT WITH IMPROVED STABILITY NEAR A MINIMUM.
      C      WAS THE MODEL FOR THIS PROCEDURE.
      C      ALL CALCULATIONS ARE PERFORMED WITH VZRO IN KILOMETERS PER SECOND.
      C      OUTPUT IS IN UNITS OF 10**4 CM/SEC
20     C
      C      CALCULATE FIRST ATTEMPT AT A FIT WITH TRIAL VALUES.
      C
      C      SF=0.
25     C      CALL VELO(BETA,VZRO,SIGCAL,SIGCA1,SIGCA2)
      C      CALL FITT(SIGCAL,EXPT,SF,DCI
      C      ILOW=MCHAN-ITRSHF
      C      IHIGH=ECHAN-ITRSHF
30     C      IFIT=10
      C      FLAND=,001
      C      CH=FLOAT(MCHAN-4-2*ITRSHF)
      C      WRITE(6,100)
      C      1000 FORMAT(1X,INTERMEDIATE VALUES=,/)
35     C      DO 1000 JCYC=1,IFIT
      C
      C      DFDV IS THE FIRST DERIVATIVE WITH RESPECT TO PEAK VELOCITY.
      C      DFD0 IS THE FIRST DERIVATIVE WITH RESPECT TO PEAK WIDTH.
40     C
      C      W IS THE WEIGHTING FACTOR.
      C      B1 AND B2 IS THE BETA MATRIX.
      C      A11,A12,A22 IS THE ALPHA MATRIX
      C
      C      B1=0.
      C      B2=0.
45     C      A11=0.
      C      A12=0.
      C      A22=0.
      C      SUM=0.
50     C
      C      DO LOOP ONLY EXTENDS OVER CHANNELS WHICH AREN'T TRUNCATED BY THE
      C      SHUTTER FUNCTION.
      C
      C      DO 1001 I=ILOW,IHIGH
      C      DFDV=SIGCA2(I)*SF
      C      DFDV=SIGCA1(I)*SF
55

```

```

      M=1./EXPT(I)
      D=EXP(TT)-SIGCAL(I)
      DM=DM
      O1=B1+DM*DFDV
      B2=B2+DM*DFDB
      A11=A11+DFDV*DFDV*DM
      A22=A22+DFDB*DFDB*DM
      A12=A12+DFDV*DFDB*DM
      1001 SUM=SUM+DM*DM
      65
      C
      C CALCULATE THE CHI SQUARED ERROR.
      C NOTE THAT THERE ARE FOUR PARAMETERS IN THE FIT TO THE DATA.
      C THESE ARE THE  $\sigma$  LEVEL, THE SCALE FACTOR, THE PEAK WIDTH AND
      C VELOCITY.
      70
      C
      C CH11=SUM/CH
      C
      C ADJUST PARAMETERS AS NECESSARY
      C A1 AND A2 IS THE CURVATURE MATRIX. A1INV AND A2INV ITS INVERSE.
      C FLAMDA IS THE FACTOR WHICH DETERMINES THE EXTENT OF THE GRADIENT
      C INFLUENCE ON THE SEARCH.
      71
      C
      C A1=1.+FLAMDA
      C DEN2=SQRT(A1+A22)
      C A2=A12/DEN2
      C DEN1=A1*A1-A2*A22
      C A1INV=A1/DEN1
      C A2INV=A2/DEN1
      C DVZRO=RI*A1INV/ABS(A11+B2*A2INV/DEN2
      C DBETA=B1+A2INV/DEN2
      80
      C
      C IF DBETA IS FORCED TO GO NEGATIVE, THEN THE DISTRIBUTION IS
      C NARROW RELATIVE TO THE SHUTTER FUNCTION. DBETA IS HALVED UNTILL
      C THE VALUE OF DBETA IS POSITIVE. IFLAG IS SET TO 1 SINCE THE MORE
      C ACCURATE INTEGRATION OVER THE CHANNEL WIDTH IS NECESSARY FOR THIS
      C CASE.
      90
      C
      C
      C
      C
      221 IF DBETA*DBETA<225,225,220
      225 IFLAG=1
      C DBETA=DBETA/2.
      C GOTO 221
      C
      C CALCULATE THE DISTRIBUTION AT THE NEW VALUE OF BETA AND VZRO.
      100
      C
      C F=0.
      C CALL VELOC(BETA,DBETA,VZRO+DVZRO,SIGCAL,SIGCAL1,SIGCAL2)
      C CALL FIT(SIGCAL,EXPT,SF,DCI)
      C SUM=0.
      C DO 1010 1=1LOW,1HIGH
      105 1010 SUM=SUM+EXP(TT)-SIGCAL(TT)*F2/EXPT(T)
      C CH12=SUM/CH
      C WRITE(6,216) CH12,DBETA/103.,DVZRO/10.
      216 FORMAT(15X,'STANDARD DEVIATION=',E12,3,5X,'DBETA=',E12,4,5X,'DVZP=',
      C 1,E12,4)
      110
      C

```

```

C IF THE NEW VALUE OF CHISQR2 IS LARGER THAN THE OLD VALUE, MAKE
C THE GRADIENT CONTRIBUTION 10 TIMES LARGER AND TRY AGAIN.
C
115 90 IF(CHI1-CHI2) 95,101,101
FLANDA=10.*FLANDA
GOTO 71
C
C STEP FITTING IF PARAMETERS OPTIMIZED
C
120 C A IS THE NUMBER OF STANDARD DEVIATIONS EACH CALCULATED POINT
C DIFFERS FROM THE DATA ON THE AVERAGE
C
101 A=SQRT(SUM/FLDATINCHAN-2*ITRSHF)
VZRO=VZRO+DVZRO
BETA=BETA+DBETA
FLANDA=FLANDA/10.
C
C THE SEARCH ENDS IF 10 ITERATIONS HAVE HAPPENED WITHOUT THE
C FOLLOWING CONDITIONS HAVING BEEN SATISFIED.
130 C IF THE VALUES OF BETA AND VZRO ARE CHANGING LESS THAN .005
C OF THEIR PREVIOUS VALUE, OR THE DATA HAS BEEN FIT WITHIN THE 90
C PER CENT CONFIDENCE LIMIT, I.E. AS2.
C
135 IF(4.LE.2.) GOTO 1002
IF(1ABS(DRBTAL-LE, (.005*BETA/11.AND.1ABS(DVZRO-LE,1.005*VZRO))1)
1 GOTO 1002
1000 CONTINUE
JCYC=JCYC-1
140 1002 WRITE(6,301)
FORMAT(1X,*,FINAL PARAMETER VALUES*,/1
WRITE(6,1210)BETA/100.,VZRO*10.,VZRO*SQRT(BETA)/10./SQRT(BETA),
JCYC,A
1210 FORMAT(1X,*,BETA=*,E12.4,3X,*,VZRO=*,E12.4,2X,*,SPEED RATIO=*,E12.4,
12X,*,ALPHA=*,E12.4,2X,*,ITERATIONS=*,13,2X,*,AVERAGE DEVIATION=*,E4.1
1)
145 IF(JCYC.EQ.17) WRITE(6,219)
219 FORMAT(5X,*,C A U T I O N----- THE FULL NUMBER OF ITERATIONS HAS
1 OCCURED WITHOUT CONVERGENCE,/)
150 1000=SQRT(A2HW/A22)
ENETA=SQRT(ALNVA/AL1)
VZRO=SQRT(ALNVA/AL1)
WRITE(6,217) ENETA/100.,ENZRO*10.
217 FORMAT(1X,*,ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA
1 AND VZRO=*,E12.4,5X,E12.4)
C
155 C PLOT DATA
C
C
WRITE(6,205)
NPIS=ECHAN-BCHAN-2*ITRSHF
XSTEP=5./FLDATINPIS)
160 J=1
OC=EXPT(INCHAN+3)
EPL(1)=0.
TI=9.9/(EXPT(MAXE)-OC)
WRITE(6,206)11,SIGCAL(11),I=1LOW,1HIGH
165 DO 1005 I=LOW,HIGH

```

PROGRAM RELVIN 76/75 DPT=2

APL1111-100011-001011
 V12111-11001111-001111
 J=11

APL1111-110011-110011

1005 CONTINUE

205 FORWATC/LOC=CC, CALLED D131, R1RUI D10N 4,1

206 FORWATC/LOC=CC, CALLED D131, R1RUI D10N 4,1

207 GO TO 1003

END

SYMBOLIC REFERENCE MAP (R-1)

ENTRY POINTS
 1123 RELVIN

VARIABLES	SN	TYPE	RELOCATION
1700 A	REAL		
1673 AINV	REAL		
1655 A12	REAL		
1674 A2INV	REAL		
1692 B1	REAL		
1650 CH	REAL		
1666 CH1	REAL		
1664 D	REAL		
1693 D12	REAL		
1602 D1V	REAL		
2 DL	REAL		
1665 DM	REAL		
4 ECHM	INTEGER		
1707 E1V	REAL		
1646 F1T	INTEGER		
1645 HIGH	INTEGER		
31 ITRASHF	INTEGER		
1705 J	INTEGER		
1 INV	INTEGER		
1703 MPTS	REAL		
3 SA	REAL		
1642 3F	REAL		
2705 STGC1	REAL		
1671 SUN	REAL		
1693 W	REAL		
4703 XPL	REAL		
3703 YPL1	REAL		
1667 A1	REAL		
1654 A11	REAL		
1671 A2	REAL		
1656 A22	REAL		
1640 BETA	REAL		
1659 D	REAL		
1677 CH12	REAL		
1676 DETA	REAL		
1672 DE41	REAL		
1663 D1V8	REAL		
1675 DM20	REAL		
1701 E1E1A	REAL		
1702 EV2E0	REAL		
1647 FLAYDA	REAL		
1630 IFLAG	INTEGER		
1644 ILOW	INTEGER		
30 ITR512	INTEGER		
1651 JCVC	INTEGER		
6 MESS	REAL		
11 OFFSET	REAL		
4 S8	REAL		
2306 STGCAL	REAL		
3304 STGC42	REAL		
5 TSP	REAL		
1640 WIDTH	REAL		
1706 X5TEP	REAL		
4303 YPL2	REAL		
TRIP	TRIP		
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FILE NAMES	MODE	445	OUTPUT	0	TAPES	445	TAPES	EXT
EXTERNALS	TYPE	ARGS						
FIT		4			INDATA	3		
LPPLT		7			SJRT	REAL	1	LIBRARY
VELO		5						
INLINE FUNCTIONS	TYPE	ARGS						
AMS	REAL	1	INTRIN		FLOAT	REAL	1	INTRIN
STATEMENT LABELS								
1207 71			0 95		INACTIVE		1764 101	
1614 205	FMT		1623 206	FMT			1470 216	FMT
1970 217	FMT		1550 219	FMT			1240 220	
1225 221			0 225		INACTIVE		1466 300	FMT
1911 301	FMT		0 1000				3 1001	
1312 1002			1127 1003				0 1005	
0 1010			1527 1210	FMT				
LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES								
1150 1000	JCYC		34 137	1408	EXT REFS	EXIT5	NOT INVER	
1155 1001	1		33 64	219	DPT			
1245 1010	1		104 106	38	INSTACK			
1304 1005	1		164 166	78	EXT REFS			
1402 1005	1		165 170	50	INSTACK			
COMMON BLOCKS LENGTH								
PAR			9					
TRI			27					
STATISTICS								
PROGRAM LENGTH			44158	2317				
BUFFER LENGTH			6660	438				
SCM LABELED COMMON LENGTH			448	36				
610008 SCM USED								

```

1      SUBROUTINE FIT(SIGCAL,EXPT,SCALE,DC)
      C
      C      SCALES THE CALCULATED AND OBSERVED TOF SPECTRA
      C
5      DIMENSION SIGCAL(255),EXPT(255)
      COMMON/TRIP/MID,HZ,DIA,SA,SR,TRP(10),ITRSIZ,ITRSHF,IFLAG
      COMMON/PAR/CHAN,LMID,DL,BCHAN,ECHAN,NCHAN,MASS,MAKF,OFFSET
      INTEGER BCHAN,ECHAN
      ILOW=BCHAN+ITRSHF
      IHIGH=ECHAN-ITRSHF
      BCHAN=0.
      XINV=0.
      X=0.
      Y=0.
      VX=0.
      VYX=0.
15     C
      C      LEAST SQUARES LOOP
      C
20     DO 30 I=ILOW,IHIGH
      Y=Y+SIGCAL(I)
      XINV=XINV+1./EXPT(I)
      YX=YX+SIGCAL(I)/EXPT(I)
      YX=YX+SIGCAL(I)*SIGCAL(I)/EXPT(I)
      BCHAN=BCHAN+1.
      X=X+EXPT(I)
      C
      C      CONTINUE
      C
30     DELTA=XINV*YX-VX*VX
      DC=(BCHAN*YX-VX*Y I/DELTA
      SCALE=(XINV*Y-BCHAN*YX)/DELTA
      C
      C      FINALLY SCALE THE DATA
      C
35     DO 40 I=BCHAN,ECHAN
      SIGCAL(I)=SIGCAL(I)*SCALE*DC
      C
      C      CONTINUE
      C
      C      RETURN
      C
      C      END

```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
3 FIT

VARIABLES	SN	TYPE	RELOCATION						
3 BCHAN	INTEGER	PAR	0	CHAN	REAL	PAR			
0 DC	REAL	F.P.	56	DELTA	REAL				
2 DIA	REAL	TRIP	2	DL	REAL	PAR			
4 ECHAN	INTEGER	PAR	0	EXPT	REAL	ARRAY			
1 HZ	REAL	TRIP	55	I	INTEGER				
32 IFLAG	INTEGER	TRIP	46	IHIGH	INTEGER				

SUBROUTINE FIT

76/76

DP1-2

FTM 4.8*508/345

02 JAN 81 13.09.96

PAGE

2

VARIABLES	SN	TYPE	RELOCATION				
45 ILON		INTEGER		31	LYSSH	INTEGER	TRIP
30 ITRSZ		INTEGER	TRIP	1	LNUD	INTEGER	PAR
6 MASS		INTEGER	PAR	7	MARE	INTEGER	PAR
9 NCHAN		INTEGER	PAR	10	DPFSET	REAL	PAR
47 ACHAN		REAL		3	SA	REAL	TRIP
4 SA		REAL	TRIP	0	SCALE	REAL	FoP.
0 SIGCAL		REAL	ARRAY	5	TRP	REAL	ARRAY TRIP
0 WIDTH		REAL	TRIP	51	X	REAL	
50 XINV		REAL		52	Y	REAL	
53 YX		REAL		56	YX	REAL	
STATEMENT LABELS							
0	30			0	40		
LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES							
19	30	1	20 27	128	INSTACK		
41	40	1	34 36	38	INSTACK		
COMMON BLOCKS LENGTH							
	TRIP		27				
	PAR		9				
STATISTICS							
	PROGRAM LENGTH		576	47			
	SCN LABELED COMMON LENGTH		448	36			
	810008 SCN USED						

```

1      SUBROUTINE BIG(SIGCAL,MAX)
      C
      C      FINDS THE MAXIMUM IN A YDF SPECTRUM
      C
      COMMON/PAF/CHAN,LMID,DL,BCHAN,ECHAN,NCHAN,MASS,MAXE,OFFSET
      INTEGER NCHAN,ECHAN
      DIMENSION SIGCAL(255)
      MAX=0
      SIGMAX=0.0
      DO 1 I=NCHAN,ECHAN
      IF (SIGCAL(I) .LT. SIGMAX) GO TO 1
      SIGMAX=SIGCAL(I)
      MAX=I
1      CONTINUE
      IF (MAX .EQ. 0) WRITE (*,255)
      255 FORMAT('D NO MAXIMUM FOUND')
      RETURN
      END

```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS

3 BIG

VARIABLES	SM	TYPE	RELOCATION	D	CHAN	REAL	PAR
3	BCHAN	INTEGER	PAR	0	CHAN	REAL	PAR
2	DL	REAL	PAR	4	ECHAN	INTEGER	PAR
30	I	INTEGER	PAR	1	LMID	INTEGER	PAR
6	MASS	INTEGER	PAR	0	MAX	INTEGER	F.P.
7	MAXE	INTEGER	PAR	5	NCHAN	INTEGER	PAR
10	OFFSET	REAL	PAR	3	SIGCAL	REAL	F.P.
27	SIGMAX	REAL					ARRAY

FILE NAMES

TAPED

MODE

FMT

STATEMENT LABELS

15 1

25 255 FMT

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
11	1	1	10 14	30	INSTACK

COMMON BLOCKS

PAR

9

STATISTICS

PROGRAM LENGTH	318	25
SCN LABELED COMMON LENGTH	118	9
610008 SCN USED		

```

1      SUBROUTINE TRAPI
COMMON/TRIP/WIDTH,M,DELSA,SB,TAP(10),ITRSIZ,ITRSHF,ILAG
DATA PI,CON/3.14159265,10000./

5      C
C      DEFINITION OF INPUT PARAMETERS
C      SA=WHEEL SLIT WIDTH IN MILLIMETERS
C      SB=DETECTOR SLIT WIDTH IN MILLIMETERS
C      WIDTH=CHANNEL TIME IN MICROSECONDS
10     C      DIA=DIAMETER FROM CENTER OF WHEEL TO DETECTOR SLIT IN CM.
C      T=ONE HALF THE NUMBER OF CHANNELS PER MILLIMETER TRAVEL OF WHEEL
C      TT=HALF THE NUMBER OF SLITS FOR BASE OF TRAPEZOID
C      TA=HALF THE NUMBER OF SLITS FOR THE TOP OF TRAPEZOID
C      IT=INTEGRAL VERSION OF IT
C      ITA=INTEGRAL VERSION OF TA
15     C      ITRSZ=NUMBER OF CHANNELS AFFECTED BY DIGITAL FILTER
C      ITRSHF      (ITRSZ=2+ITRSHF+1)

C      T=CON/PI*DELSA*HZ*2.*WIDTH
C      TI=I(SA*SB)

20     C      SA=MIN(LA,SB)
C      YA=TI-SA*TO*2.
C      IT=INT(TT-.5)
C      ITA=INT(TA-.5)

25     C      CHECK IF BASE OF TRAPEZOID LESS THAN ONE CHANNEL WIDE
C
C      IF(TT.EQ.0) GOTO 90
C      ITRSZ=1+2*(TT+1)
C      ITRSHF=TT+1

30     C      CHECK IF TOP OF TRAPEZOID MORE THAN ONE CHANNEL WIDE
C
C      IF(TA.GE.0) GOTO 40

35     C      TRAPEZOID CORNER OCCURS WITHIN THE FIRST CHANNEL
C      TRP(10)=(TI-TA*TA-.25)/(TT-TA)

C      CHECK IF TRAPEZOID BASE OCCURS WITHIN FIRST CHANNEL
40     C
C      IF(ITT.EQ.0) GOTO 30
C      TRAPEZOID EDGE SPREAD OVER ITT CHANNELS

45     C      DO 20 I=1,ITT
C      TRP(10:I)=(TT-FLD*IT(I))/(TT-TA)
C      TRP(10-I)=TRP(10+I)

20     C      CHANNEL WHERE EDGE HITS BASE

50     C
C      TRP(11+ITT)=(TT-.5-FLD*IT(1))*2/(2.*(TT-TA))
C      TRP(9-ITT)=TRP(11+ITT)
C      GOTO 75

30     C
C      CASE WHERE TOP OF TRAPEZOID AT LEAST ONE CHANNEL WIDE.
55     C

```

```

      A...101=1.0
      C
      L      DOES TOP OF TRAPEZOID EXTEND OVER MORE THAN ONE CHANNEL?
      C
60      C      IF (ITTA.EQ.0.) GOTO 50
      C
      C      IF SO THAN ALL THESE CHANNELS HAVE UNIT AREA
      C
65      C      DO 45 I=1,ITA
      C      TRP(I*ITA)=1.0
      C      TRP(I*ITA)=1.0
      C
45      C      IS EDGE OF TRAPEZOID CONTAINED WITHIN ONE CHANNEL.
      C
70      C      IF (ITT.EQ.ITA) GOTO 70
      C
      C      AREA FOR CORNER OF TRAPEZOID.
      C
75      C      YERN=FLOAT(ITTA)*.5-YA
      C      TRP(I*ITA)=1.-TERM*TERM/(2*(ITT-YA))
      C      TRP(I*ITA)=TRP(I*ITA)
      C
80      C      CHANNELS WITH EDGE OF TRAPEZOID, BUT NO CORNERS
      C
      C      CHECK IF THERE ARE PURE EDGE CHANNELS
      C
85      C      IF (I2+ITA-ITT.GT.0) GOTO 60
      C      ILOW=2+ITA
      C      DO 55 I=ILOW,ITT
      C      TRP(I*ITA)=ITT-FLOAT(I)/ITT-YA
      C      TRP(I*ITA)=TRP(I*ITA)
      C
90      C      CHANNEL WHERE EDGE HITS BASE
      C
60      C      TRP(I*ITA)=ITT-.5-FLOAT(ITT)*.5/(2*(ITT-YA))
      C      TRP(I*ITA)=TRP(I*ITA)
      C      GOTO 75
      C
95      C      CASE WHERE EDGE CONTAINED IN ONE CHANNEL
      C
70      C      TRP(I*ITA)=ITA+YB-1+.5-FLOAT(ITA)
      C      TRP(I*ITA)=TRP(I*ITA)
      C      GOTO 75
      C
100      C      CASE WHERE ALL OF TRAPEZOID IN ONE CHANNEL
      C
90      C      TRP(I*ITA)=1.0
      C      IYASTZ=1
      C      IYASHF=0
      C
105      C      NORMALIZE SO TRAPEZOID HAS UNIT AREA
      C
110      C      SUM=0.0

```

```

      AREA=IA*II
      ILUM=10-ITRASHF
      IHIGH=10-ITRASHF
      DO 77 J=ILUM,IHIGH
      TRP(I)=TRP(I)/AREA
      SUM=SUM+TRP(I)
      WRITE(6,103)
115      77  FORWAT(11)
      WRITE(6,100)
120      1000 FORWAT(1H,*,SHUTTER FUNCTION TRAPEZOID=, 2X,19F4.1)
      RETURN
      END

```

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

120 1 57CD 120 FIELD WIDTH OF A CONVERSION DESCRIPTOR SHOULD BE AS LARGE AS THE NIVINJM SPECIFIED FOR THAT DESCRIPTION

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS

1 TRAP1

VARIABLES

SN TYPE

RELOCATION

201	AREA	REAL		146	CON	REAL	
2	DIA	REAL	TRIP	1	HZ	REAL	TRIP
203	I	INTEGER		32	IFLAG	INTEGER	TRIP
210	IHIGH	INTEGER		205	ILOW	INTEGER	
202	ITA	INTEGER		31	ITRASHF	INTEGER	TRIP
30	ITRASHF	INTEGER	TRIP	201	IT	INTEGER	
145	PI	REAL		3	SA	REAL	TRIP
4	SB	REAL	TRIP	206	SUM	REAL	
176	T	REAL		203	TA	REAL	
204	TEAR	REAL		5	TRP	REAL	ARRA: TRIP
177	TI	REAL		7	WIDTH	REAL	TRIP

FILE NAMES

MODE

TAPE4

FMT

INLINE FUNCTIONS

TYPE

ARGS

ARINI

REAL

0

INTRIN

FLOAT

REAL

1

INTRIN

INT

INTEGER

1

INTRIN

STATEMENT LABELS

0 20

37 30

44 40

0 45

55 40

0 55

76 60

105 70

121 75

0 77

115 90

152 103

FMT

STATEMENT LABELS				
160	1000	FMT		
LOOPS	LABEL	INDEX	FROM-TO	LENGTH
13	20	1	55 47	40
53	45	1	45 07	20
72	55	1	06 08	40
127	77	1	119 116	30
				INSTACK

COMMON BLOCKS	LENGTH
3	27

STATISTICS	
PROGRAM LENGTH	2118
COMMON LENGTH	137
SCN LABELED COMMON LENGTH	338
61000R SCN USED	27

CARD UP	
---------	--

120	
-----	--

COMMON BLOCKS	
---------------	--

ENTRY POINTS	
--------------	--

COMMON BLOCKS	
---------------	--

VARIABLES	
-----------	--

201	001	01			
-----	-----	----	--	--	--

2	213	121			
---	-----	-----	--	--	--

201	1	011			
-----	---	-----	--	--	--

210	10112	111 2			
-----	-------	-------	--	--	--

202	11A	101			
-----	-----	-----	--	--	--

11	11 11	111			
----	-------	-----	--	--	--

105	01	11			
-----	----	----	--	--	--

5	21	11			
---	----	----	--	--	--

106	1	11			
-----	---	----	--	--	--

229	1112	111			
-----	------	-----	--	--	--

112	11	11			
-----	----	----	--	--	--

FILE NAME	
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22	
----	--

PROGRAM NAME	
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```

1 SUBROUTINE HALF(EXPT,H)
COMMON/PPAR/CHAN,LHID,DL,BCHAN,ECHAN,NCHAN,MASS,YAXE,OFFSET
DIMENSION EXPT(255)
REAL MASS,LHID
INTEGER NCHAN,ECHAN,NCHAN

```

```

C CALCULATE CHANNEL NUMBER OF APPROXIMATE HALF HEIGHT
C
C

```

```

13 ASSUME DC LEVEL GIVEN BY THE COUNTS IN THE THIRD CHANNEL
DC=EXPT(NCHAN+3)
C

```

```

15 NAXE IS THE CHANNEL NUMBER OF THE PEAK OF THE DISTRIBUTION
H=EXPT(NAXE)*DC/72
DO 10 I=BCHAN,NAXE
C

```

```

20 ASSUME FIRST CHANNEL WHOSE SIGNAL IS LARGER THAN THE CALCULATED
HALF HEIGHT IS THE CORRECT CHANNEL
C

```

```

IF(EXPT(I))>H THEN GOTO 10
TI=EXPT(I)-EXPT(I-1)
B=EXPT(I)+EXPT(I-1)-TI*FLOAT(2*I-1)
B=B/2

```

```

H=H-B/71
GOTO 20

```

```

10 CONTINUE
RETURN
END

```

SYMBOLIC REFERENCE MAP (R=I)

ENTRY POINTS

3 HALF

VARIABLES	SM	TYPE	RELOCATION				
35 B	REAL	PEAL	PAR	3	BCHAN	INTEGER	PAR
0 CHAN	REAL	PEAL	PAR	32	DC	REAL	
2 DL	REAL	PEAL	PAR	4	ECHAN	INTEGER	PAR
0 EXPT	REAL	ARRAY	F.P.	0	H	REAL	F.P.
31 I	INTEGER			1	LHID	INTEGER	PAR
4 MASS	REAL		PAR	7	NAXE	INTEGER	PAR
5 NCHAN	INTEGER		PAR	10	OFFSET	REAL	PAR
34 TI	REAL						

IN THE FUNCTIONS TYPE ARG
 FLOAT REAL 1 INTRIN

SUBROUTINE HALF

76/76 OPT=2

FIN 4.81508/045

02 JAN 61 13.09.56

PAGE 2

STATEMENT LABELS

20 10

27 20

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXITS
16	10	1	17 28	138	DPT	

COMMON BLOCKS	LENGTH
PAR	9

STATISTICS

PROGRAM LENGTH	368	30
SCM LABELED COMMON LENGTH	110	9
61000R SCM USED		

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
J INDATA

VARIABLES

343	BC	SM	TYPE	REALLOCATION	3	BCMAN	INTEGER	PAR
0	BETA	REAL		F.P.	0	CHAN	REAL	PAR
2	DIA	REAL		TRIP	2	DL	REAL	PAR
344	EC	INTEGER			4	ECMAN	INTEGER	PAR
0	EXPT	REAL	ARRAY	F.P.	346	H	REAL	
1	HZ	REAL		TRIP	345	I	INTEGER	
32	IFLAG	INTEGER		TRIP	31	IFASHF	INTEGER	TRIP
30	IRAST	INTEGER		TRIP	1	LMIG	REAL	PAR
6	MASS	REAL		PAR	7	MAKE	INTEGER	PAR
9	MCHAN	INTEGER		PAR	10	OFFSET	REAL	PAR
3	SA	REAL		TRIP	4	SH	REAL	TRIP
350	TITLE	REAL	ARRAY		5	TPP	REAL	ARRAY
347	VLEN	REAL			5	VIRD	REAL	F.P.
0	WIDTH	REAL		TRIP				

FILE NAMES

TAPES	FMF	NDDE	FMF	FMF
-------	-----	------	-----	-----

EXTERNALS

STG	TYPE	ARGS	HELP	2
-----	------	------	------	---

INLINE FUNCTIONS

FLOAT	REAL	TYPE	ARGS	INTRIN	4
-------	------	------	------	--------	---

STATEMENT LABELS

198	100	FMF	175	101	FMF	135	102	FMF
306	103	FMF	251	104	FMF	211	203	FMF
274	201	FMF	209	204	FMF	313	205	FMF
269	211	FMF	330	215	FMF			

LOOPS

LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS
-------	-------	---------	--------	------------	----------

COMMON BLOCKS

PAR	LENGTH
-----	--------

STATISTICS

PROGRAM LENGTH	376R	254
SCM LABELED COMMON LENGTH	448	36
410008 SCM USED		

```

1      SUBROUTINE LPLT (X1,Y1,NPT1,K2,Y2,NPT2,NB)
      DIMENSION IPA(120),X(1300),Y(1300),X2(1300),Y2(130)
      DIMENSION C(1500),X(1300),Y(1300),V(1300)
      DATA I1,I2,I3,I4,I5,I0,I18 / 1M,1M2,1M3,1M4,1M5,1M0,1M /
      DATA LB,I1,LN,LP / 1M,1M1,1M-,1M+ /
      DATA DX,DY / 3.025,0.125 /
      NRI(10,2001)
2001  FCGPAT (1M)
      IF (NO .EQ. 0) GOTO 20
      IF (NO .EQ. 1) LND=L1
      IF (NO .EQ. 2) LND=L2
      IF (NO .EQ. 3) LND=L3
      IF (NO .EQ. 4) LND=L4
      GOTO 21
      15      20  CONTINUE
      LND=L5
      WRITE (6,2001)
2003  FORMAT (1M F)
      21  CONTINUE
      DO 1 I=1,NPT1
      IF (X(I)) .LT. DB1 X(I)=DB1
      IF (Y(I)) .LT. -3.*DY Y(I)=-3.*DY
      X(I)=INT((X(I)+DB1)/(2.*DB1))
      Y(I)=INT((Y(I)+3.*DY)/(2.*DY))+4
25      1  CONTINUE
      DO 13 I=1,NPT2
      IF (X(I)) .LT. DB1 X(I)=DB1
      IF (Y(I)) .LT. -3.*DY Y(I)=-3.*DY
      X(I)=INT((X(I)+DB1)/(2.*DB1))
      Y(I)=INT((Y(I)+3.*DY)/(2.*DY))+4
30      10  CONTINUE
      DO 2 I=1,18
      IPA(I)=LB
      CONTINUE
      35      2  DO 7 N=1,57
      N2=60-N+1
      DO 3 I=1,120
      IPA(I)=LB
      CONTINUE
      40      3  IPA(20)=L1
      IF ((FLOAT(N2)/8.-N2/8) .GT. 1.E-6) GOTO 5
      IPA(19)=LM
      IPA(20)=LM
      IF (N2 .NE. 16) GOTO 5
45      4  DO 4 I=21,120
      IPA(I)=LM
      IF ((FLOAT(I)/10.-I/10) .LE. 1.E-6) IPA(I)=LP
      CONTINUE
      5  CONTINUE
      50      DO 6 I=1,NPT1
      IF (Y(I)) .NE. N2) GOTO 6
      IPA(20,X(I))=L0
      CONTINUE
      6  DO 12 I=1,NPT2
      IF (Y(I)) .NE. N2) GOTO 12

```

```

      END=20+IX211
      IF (IPAI(ND) .EQ. LR) IPAI(ND)=LR
      IF (IPAI(ND) .EQ. LD) IPAI(ND)=LD
      IF (IPAI(ND) .EQ. LK) IPAI(ND)=LK
60      CONTINUE
      WRITE (6,2000) (IPAI(I),I=1,L201)
      CONTINUE
2000  FORMAT (120a11)
65      RETURN
      END

```

SYMBOLIC REFERENCE MAP (R=1)

ENTRY POINTS
9 LPP1

VARIABLES	SN	TYPE	RELOCATION						
221 DX		REAL		222 DY		REAL			
252 I		INTEGER		255 INQ		INTEGER			
256 IPA		INTEGER	ARRAY	446 IX1		INTEGER	ARRAY		
1576 IX2		INTEGER	ARRAY	1122 IV1		INTEGER	ARRAY		
2252 IV2		INTEGER	ARRAY	214 LA		INTEGER			
215 LB		INTEGER		216 LI		INTEGER			
217 LM		INTEGER		251 LND		INTEGER			
219 LO		INTEGER		220 LP		INTEGER			
212 LS		INTEGER		206 LI		INTEGER			
207 L2		INTEGER		210 L3		INTEGER			
211 L4		INTEGER		251 N		INTEGER			
0 MD		INTEGER	F.P.	0 NPT1		INTEGER		F.P.	
0 NPT2		INTEGER	F.P.	254 NI		INTEGER			
0 X1		REAL	ARRAY	3 X2		REAL	ARRAY	F.P.	
0 V1		REAL	ARRAY	3 Y2		REAL	ARRAY	F.P.	

FILE NAMES
TYPE6 FMT

INLINE FUNCTIONS	TYPE	ARGS	INTRIN	INT	INTEGER	INTRIN
FLOAT	REAL	1				

SYMBERY LABELS

0 1			0 2		0 3
0 4		131 5		157 6	
0 7		0 10		177 12	
32 20		35 21		241 2003	FMT
226 2001	FMT	233 2003	FMT		

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
45	1	I	20 25	168	OPT
73	10	I	26 31	168	OPT
113	2	I	32 34	28	INSTACK
117	7	N	35 42	688	EXT REFS NOT INNER

SUBROUTINE LPPLT

76776

OPT=2

FIN 4.0-508/045

02 JAN 81 11.00.55

PAGE

3

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
129	3	1	37 59	20	INSTACK
142	4	1	45 48	78	INSTACK
155	6	1	50 53	38	INSTACK
165	12	1	54 60	118	OPT

STATISTICS

PROGRAM LENGTH

2731R

1497

61000B SCH USED

-35-

```

1      SUBROUTINE VELO(BETA,VZRO,SIGCAL,SIG1,SIG2)
      C
      C CALCULATES THE TOP SPECTRA AVERAGED OVER THE IONIZER LENGTH AND
      C SHUTTER FUNCTION
5      C
      C COMMON/PAIR/CHAN,LHID,DL,BCHAN,ECHAN,NCHAN,MASS,MAKE,OFFSET
      C COMMON/TRIP/WIDTH,HZ,BJA,SA,SB,TRP(19),ITRSHF,IFLAG
      C DIMENSION SIGTEN(255),SIGCAL(255)
      C DIMENSION SIGCAL(255),SIGCA2(255),SIG1(255),SIG2(255)
      C REAL MASS,LHID,L
      C INTEGER BCHAN,ECHAN
      C N=3
      C
      C ZERO ARRAYS
15      C
      C SIGCAL, SIGCA2 CONTAIN THE ANALYTICAL DERIVATIVES OF THE DISTRIBUTION
      C WITH RESPECT TO VZRO AND BETA RESPECTIVELY. THE SHUTTER
      C CONVOLUTED RESULTS ARE RETURNED IN SIG1, SIG2.
      C
      C DO 5 I=1,255
20      C
      C SIGCAL(I)=0.
      C SIGTEN(I)=0.
      C SIGCA1(I)=0.
      C SIGCA2(I)=0.
      C SIG1(I)=0.
      C SIG2(I)=0.
25      C
      C 3
      C CONVOLVE
      C ILOW=BCHAN+ITRSHF
      C IHIGH=ECHAN-ITRSHF
      C
      C 30
      C NINT IS THE GRID SIZE FOR THE SIMPSON'S RULE INTEGRATION
      C OVER CHANNEL WIDTH. IF THE BEAM WIDTH IS VERY NARROW, THEN
      C SET IFLAG=1 AND THIS INTEGRATION IS PERFORMED, ELSE USE IFLAG=0
      C AND THE ROUTINE IS ROUGHLY 6 TIMES FASTER.
      C NINT SHOULD PROBABLY BE ODD.
      C 35
      C SEE *INTRODUCTION TO NUMERICAL ANALYSIS BY HILDEBRAND, SECOND
      C ED., PG. 93.
      C THE CURRENT VALUE OF NINT IS CHOSEN SUCH THAT IF A FINER GRID
      C IS NEEDED, THEN THE SIMULATION OF THE EXPERIMENT BY THIS PROGRAM
      C IS PROBABLY MORE IN ERROR.
      C
      C 40
      C NINT=11
      C
      C DIVIDE IONIZER INTO NINT INTERVALS
      C NOTE THAT NINT SHOULD BE ODD
      C
      C 45
      C NION=11
      C
      C THESE CONSTANTS ARE USED IN THE INTERVALS FOR THE IONIZER INTEGRATION
      C AND THE CHANNEL WIDTH INTEGRATION.
      C
      C 50
      C
      C S2=FLOAT(NINT-1)
      C NID=NINT-2
      C NHID=(NION+1)/2
      C S=FLOAT(NION-1)
      C C1=CHAN*.1
      C
      C 55

```


C2=CHAN*10(-5)

THE 40 DD LOOP TREATS EACH POINT IN THE IONIZER EQUALLY, AND
MODELS THE EXPERIMENT BY NIM INDEPENDENT AND SLIGHTLY DISPLACED
IONIZERS.

DD 40 I=1,NION

C=LHID+FLOAT(NMID)*DL/5

DD 35 J=0,CHAN,ECHAN

IF(I*LAG-EQ.0) GOTO 30

THE DD LOOP PERFORMS THE SIMPSON'S RULE INTEGRATION

T1 IS THE LEFT EDGE OF THE CHANNEL.

T1=C*(I*DATEJ-1)+OFFSET

V1=L/T1

X1=V1**N*EXP(-BETA*(V1-VZRO)**2)/T1

W1=0.

W2=0.

W=0.

DT IS THE STEP LENGTH IN TIME SPACE FOR THE INTEGRATION
OVER THE CHANNEL WIDTH

DT=C1/52

DD 25 K=1,M2*2

T2=T1+DT

T3=T2+DT

V2=L/T2

V3=L/T3

X2=V2**N*EXP(-BETA*(V2-VZRO)**2)/T2

X3=V3**N*EXP(-BETA*(V3-VZRO)**2)/T3

W=0.014.*X2*X3

W1=W1+X1*2.*BETA*(V1-VZRO)*X2*0.8.*BETA*(V2-VZRO)*X3*2.*BETA*(V3-VZRO)

T1=T3

W2=W2-X1*(V1-VZRO)**2-X3*(V3-VZRO)**2-4.*X2*(V2-VZRO)**2

X1=X3

T1=T3

CONTINUE

SIGTEM(J)=SIGTEM(J)+W*DT/3.

DERIVATIVE OF INTENSITY WITH RESPECT TO VZRO.

SIGCAL(J)=SIGCAL(J)+W1*DT/3.

DERIVATIVE OF INTENSITY WITH RESPECT TO BETA.

SIGCZ(J)=SIGCZ(J)+W2*DT/3.

GOTO 35

APPROXIMATE THE AREA OF THE VELOCITY DISTRIBUTION IN THIS CHANNEL
BY ITS VALUE AT THE MIDPOINT.

V=C1*(I*DATEJ)+V*FFSET1+C2

CALCULATE THE VELOCITY OF THE PARTICLE DEFLECTED IN CHANNEL J
IF IT WAS IONIZED AT THIS DISTANCE L FROM THE COLLISION ZONE

V=L/T

```

C
C USING THE GIVEN VELOCITY DISTRIBUTION, CALCULATE THE RELATIVE
C AMOUNT EXPECTED TO HAVE THIS VELOCITY
115 C C=V0*EXP(-BETA*(V-VZD)**2) /I
C DERIVATIVE OF INTENSITY WITH RESPECT TO VZD,
C SIGCAL(J)=SIGCAL(J)+2.*BETA*(V-VZD)*C
C DERIVATIVE OF INTENSITY WITH RESPECT TO BETA,
C SIGCAZ(J)=SIGCAZ(J)+C*(V-VZD)**2
120 C SIGTEM(J)=SIGTEM(J)+C
C CONTINUE
40 C CONTINUE
C DO 60 J=JLOW,JHIGH
125 C
C CONVOLVE NOW OVER THE SHUTTER FUNCTION USING THE TRAP ARRAY AS A
C DIGITAL FILTER
C
C ITENP=I0-I
C JLOW=I-ITRSHF
C JHIGH=I+ITRSHF
130 C DO 55 J=JLOW,JHIGH
C R=J-ITENP
C SIG1(I)=SIG1(I)+TRP(R)*SIGCAL(J)
C SIG2(I)=SIG2(I)+TRP(R)*SIGCAZ(J)
135 C SIGAL(I)=SIGCAL(I)+TRP(R)*SIGTEM(J)
C 55 C CONTINUE
C RETURN
C END

```

SYMBOLIC REFERENCE MAP (IN=1)

ENTRY POINTS

3 VELO

VARIABLES	SN	TYPE	RELOCATION				
3 BECHAN		INTEGER	PAR	0 BETA	REAL		F.P.
307 C		REAL		2 CHAN	REAL		PAR
264 CI		REAL		265 C2	REAL		
2 DIA		REAL	TRIP	2 OL	REAL		PAR
275 DI		REAL		4 ECHAN	INTEGER		PAR
1 HI		REAL	TRIP	293 I	INTEGER		
32 IFLAG		INTEGER	TRIP	255 IHIGH	INTEGER		
234 ILOW		INTEGER	TRIP	310 ITENP	INTEGER		TRIP
31 ITRSHF		INTEGER		30 ITRSI2	INTEGER		
266 J		INTEGER		312 JHIGH	INTEGER		
311 JLOW		INTEGER		276 K	INTEGER		
251 L		REAL		1 LMI0	REAL		PAR
6 MASS		REAL	PAR	7 MAXE	INTEGER		PAR
252 N		INTEGER		5 NCHAN	INTEGER		PAR
256 NINT		INTEGER		257 NI0N	INTEGER		
262 NMID		INTEGER		261 NI2	INTEGER		

SUBROUTINE VELO

7676

OPT=2

FIN 4.R=538/045

J2 JAN 81 13.09.56

PAGE

4

VARIABLES	SH	TYPE	RELOCATION	PAR	263	5	REAL	TRIP
10 OFFSET	REAL							
3 SA	REAL				4	58	REAL	
0 SIGCAL	REAL	ARRAY	F.P.	712	SIGCAL	REAL	ARRAY	
1311 SIGCA2	REAL	ARRAY	F.P.	313	SIGTEM	REAL	ARRAY	
0 SIG1	REAL	ARRAY	F.P.	0	SIG2	REAL	ARRAY	F.P.
260 S2	REAL			305	1	REAL		
5 TRP	REAL	ARRAY	TRIP	267	13	REAL		
277 T2	REAL			303	13	REAL		
306 V	REAL			3	VZRO	REAL		F.P.
270 V1	REAL			301	V2	REAL		
302 V3	REAL			274	W	REAL		
0 WIDTH	REAL		TRIP	272	W1	REAL		
271 W2	REAL			271	X1	REAL		
303 X2	REAL			304	X3	REAL		
EXTERNALS	TYPE	ARGS						
EXP	REAL	1	LIBRARY					
INLINE FUNCTIONS	TYPE	ARGS						
FLGAT	REAL	1	INTRIN					
STATEMENT LABELS								
0 5				0	25		156	30
204 15				0	40		3	55
0 60								
LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES			
13 5	I		19 26	48	INSTAC4			
35 40	I		62 122	1548		EXT REFS	NOT INNER	
49 35	J		66 121	1448		EXT REFS	NOT INNER	
72 25	K		81 94	538		EXT REFS		
220 60	I		123 136	168		NOT INNER		
223 55	J		131 135	78	INSTAC4			
COMMON BLOCKS	LENGTH							
PAR	9							
TRIP	27							
STATISTICS								
PROGRAM LENGTH			17276	983				
SCM LABELED COMMON LENGTH			448	36				
610008 SCM USED								

LOAD MAP.

LINK - RKY 6300/7300 8.4

02 JAN 81 11.09.57

PAGE 1

FL REQUIRED TO LOAD 33600
 FL REQUIRED TO RUN 21600
 INITIAL TRANSFER TO KELVIN 1267

BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE
/PAR/	100	11	
/TRIP/	111	33	
KELVIN	144	530	LGO
FILE	5447	57	LGO
BIG	5526	31	LGO
TRAPI	5557	211	LGO
HALF	5770	36	LGO
INDATA	6026	376	LGO
IMPLY	6424	2731	LGO
VELD	11345	1727	LGO
/STP.END/	13304	1	
/ECL.C./	13305	26	
/OLIMNT/	13333	1	
/QJDSFL/	13334	2	
/QASAFGL/	13336	1	
/QCOMP./	13337	1	
/Q8-IO./	13340	171	
FTNLIB	13531	1	FTNLIB
CIN	13532	13	FTNLIB
COMID	13545	60	FTNLIB
ENDJ	13625	2	FTNLIB
EXP	13627	75	FTNLIB
EXPMSG	13722	16	FTNLIB
RECMK	13740	31	FTNLIB
FLTY	14001	156	FTNLIB
FLTYUT	14157	314	FTNLIB
FRAP	14473	406	FTNLIB
FORST	15155	662	FTNLIB
/QOVERL7/	15763	1	
FORUFL	15764	16	FTNLIB
F.OPEN	16002	120	FTNLIB
F.READF	16122	170	FTNLIB
F.WRTF	16312	122	FTNLIB
GET1F	16434	43	FTNLIB
GETFP	16477	60	FTNLIB
INCOM	16537	262	FTNLIB
INPC	17041	234	FTNLIB
KODEP	17275	516	FTNLIB
KRAREP	20033	435	FTNLIB
OUTCOM	20470	242	FTNLIB
OUTC	20732	155	FTNLIB
QZMTRY	21107	31	FTNLIB
RDO	21140	23	FTNLIB
SPA	21163	11	FTNLIB

LOAD MAP.

LINK - RAY 6300/7033 8.4

PAGE 7

BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE
SOFT.	21174	32	FINAL18
SYSAID	21229	1	FINAL18
SYSAID	21253	3	FINAL18
SYSAID	21253	7	FINAL18
SYSLST	21272	62	FINAL18
SYSLST	21354	2	FINAL18
SYSLST	21356	10	FINAL18
SYSLST	21425	1	FINAL18
SYSLST	21425	66	FINAL18
SYSLST	21513	63	FINAL18

41 13F BENZENE DIMER CALIBRATION

MASS = 40.000

CHANNEL WIDTH = 2.2 MICROSECONDS BEGINNING CHANNEL = 81, ENDING CHANNEL = 253; FLIGHT LENGTH = 16.66 CM; SOURCE LENGTH = 1.22 CM.

OFFSET = -8.4 CHANNELS

WHEEL FREQ. = 4000. HZ; WHEEL DIAMETER = 17.3 CM; SLOT WIDTH = .76 MM; DETECTOR APERTURE = .13 MM

INPUT DISTRIBUTION

81	120.0	82	122.0	83	142.0	84	144.0	85	114.0	86	128.0	87	139.0	88	120.0
89	126.0	90	139.0	91	136.0	92	132.0	93	131.0	94	150.0	95	140.0	96	127.0
97	135.0	98	137.0	99	138.0	100	147.0	101	124.0	102	142.0	103	140.0	104	177.0
105	133.0	106	143.0	107	121.0	108	144.0	109	143.0	110	138.0	111	134.0	112	134.0
113	131.0	114	162.0	115	155.0	116	144.0	117	157.0	118	149.0	119	166.0	120	164.0
121	200.0	122	179.0	123	211.0	124	225.0	125	258.0	126	289.0	127	268.0	128	340.0
129	368.0	130	364.0	131	454.0	132	528.0	133	619.0	134	698.0	135	817.0	136	914.0
137	1081.0	138	1290.0	139	1462.0	140	1671.0	141	1993.0	142	2171.0	143	2481.0	144	2652.0
145	291.0	146	3182.0	147	3539.0	148	3837.0	149	4129.0	150	4295.0	151	4501.0	152	4570.0
153	4759.0	154	4751.0	155	4895.0	156	4780.0	157	4812.0	158	4694.0	159	4592.0	160	4356.0
161	4230.0	162	3901.0	163	3776.0	164	3507.0	165	3342.0	166	3024.0	167	2746.0	168	2546.0
169	2334.0	170	2122.0	171	1894.0	172	1775.0	173	1575.0	174	1444.0	175	1266.0	176	1219.0
177	1048.0	178	956.0	179	873.0	180	800.0	181	743.0	182	643.0	183	622.0	184	589.0
185	492.0	186	502.0	187	502.0	188	418.0	189	391.0	190	364.0	191	389.0	192	378.0
193	327.0	194	271.0	195	278.0	196	241.0	197	262.0	198	237.0	199	251.0	200	234.0
201	220.0	202	209.0	203	233.0	204	233.0	205	221.0	206	216.0	207	144.0	208	221.0
209	202.0	210	223.0	211	192.0	212	204.0	213	194.0	214	193.0	215	196.0	216	189.0
217	185.0	218	181.0	219	161.0	220	221.0	221	159.0	222	233.0	223	188.0	224	169.0
225	173.0	226	174.0	227	159.0	228	149.0	229	185.0	230	166.0	231	175.0	232	173.0
233	157.0	234	167.0	235	177.0	236	165.0	237	152.0	238	170.0	239	160.0	240	146.0
241	157.0	242	147.0	243	135.0	244	167.0	245	187.0	246	174.0	247	138.0	248	160.0
249	136.0	250	126.0	251	148.0	252	161.0	253	119.0	254	143.0	255	155.0		

SHUTTER FUNCTION TRAPEZOID .214.971.214

INTERMEDIATE VALUES

STANDARD DEVIATION = .559E+01 DBETA = -.2113E+00 DVZRO = -.6386E-01
STANDARD DEVIATION = .564E+01 DBETA = -.2192E-01 DVZRO = -.1980E-01
STANDARD DEVIATION = .563E+01 DBETA = -.1229E-01 DVZRO = .179JE-03

FINAL PARAMETER VALUES

BETA = .2751E+01 VZRO = .3517E+01 SPEED RATIO = .9152E+01 ALPHA = .6329E+00 ITERATION = 3 AVERAGE DEVIATION = 2.3
ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA AND VZRO = .6804E-02 .1410E-02

CALCULATED DISTRIBUTION

82	160.9	81	150.9	84	160.9	85	160.9	86	163.9	87	160.9	88	153.9	89	160.9
90	163.9	91	160.9	92	160.9	93	160.9	94	163.9	95	163.9	96	163.9	97	160.9
98	160.9	99	160.9	100	160.9	101	160.9	102	160.9	103	160.9	104	160.9	105	160.9

194	160.9	107	160.9	108	162.9	109	153.9	112	160.9	113	160.9
195	160.9	108	160.9	109	162.9	110	153.9	113	160.9	114	160.9
196	160.9	109	160.9	110	162.9	111	153.9	114	160.9	115	160.9
197	160.9	110	160.9	111	162.9	112	153.9	115	160.9	116	160.9
198	160.9	111	160.9	112	162.9	113	153.9	116	160.9	117	160.9
199	160.9	112	160.9	113	162.9	114	153.9	117	160.9	118	160.9
200	160.9	113	160.9	114	162.9	115	153.9	118	160.9	119	160.9
201	160.9	114	160.9	115	162.9	116	153.9	119	160.9	120	160.9
202	160.9	115	160.9	116	162.9	117	153.9	120	160.9	121	160.9
203	160.9	116	160.9	117	162.9	118	153.9	121	160.9	122	160.9
204	160.9	117	160.9	118	162.9	119	153.9	122	160.9	123	160.9
205	160.9	118	160.9	119	162.9	120	153.9	123	160.9	124	160.9
206	160.9	119	160.9	120	162.9	121	153.9	124	160.9	125	160.9
207	160.9	120	160.9	121	162.9	122	153.9	125	160.9	126	160.9
208	160.9	121	160.9	122	162.9	123	153.9	126	160.9	127	160.9
209	160.9	122	160.9	123	162.9	124	153.9	127	160.9	128	160.9
210	160.9	123	160.9	124	162.9	125	153.9	128	160.9	129	160.9
211	160.9	124	160.9	125	162.9	126	153.9	129	160.9	130	160.9
212	160.9	125	160.9	126	162.9	127	153.9	130	160.9	131	160.9
213	160.9	126	160.9	127	162.9	128	153.9	131	160.9	132	160.9
214	160.9	127	160.9	128	162.9	129	153.9	132	160.9	133	160.9
215	160.9	128	160.9	129	162.9	130	153.9	133	160.9	134	160.9
216	160.9	129	160.9	130	162.9	131	153.9	134	160.9	135	160.9
217	160.9	130	160.9	131	162.9	132	153.9	135	160.9	136	160.9
218	160.9	131	160.9	132	162.9	133	153.9	136	160.9	137	160.9
219	160.9	132	160.9	133	162.9	134	153.9	137	160.9	138	160.9
220	160.9	133	160.9	134	162.9	135	153.9	138	160.9	139	160.9
221	160.9	134	160.9	135	162.9	136	153.9	139	160.9	140	160.9
222	160.9	135	160.9	136	162.9	137	153.9	140	160.9	141	160.9
223	160.9	136	160.9	137	162.9	138	153.9	141	160.9	142	160.9
224	160.9	137	160.9	138	162.9	139	153.9	142	160.9	143	160.9
225	160.9	138	160.9	139	162.9	140	153.9	143	160.9	144	160.9
226	160.9	139	160.9	140	162.9	141	153.9	144	160.9	145	160.9
227	160.9	140	160.9	141	162.9	142	153.9	145	160.9	146	160.9
228	160.9	141	160.9	142	162.9	143	153.9	146	160.9	147	160.9
229	160.9	142	160.9	143	162.9	144	153.9	147	160.9	148	160.9
230	160.9

KA TOP CALIBRATION BENZENE DIMER

MASS = 84.000

CHANNEL WIDTH = 3.3 MICROSECONDS BEGINNING CHANNEL = 81 ENDING CHANNEL = 2241 FLIGHT LENGTH = 13.36 CM IONIZER LENGTH = 1.22 CM

OFFSET = -8.3 CHANNELS

WHEEL FREQ. = 250. HZ WHEEL DIAMETER = 17.3 CM SLOT WIDTH = .76 MM DETECTOR APERTURE = .13 MM

INPUT DISTRIBUTION

81	182.0	82	203.0	83	177.0	84	185.0	85	198.0	86	163.0	87	194.0	88	187.0
89	180.0	90	182.0	91	199.0	92	181.0	93	172.0	94	180.0	95	181.0	96	192.0
97	179.0	98	198.0	99	183.0	100	155.0	101	191.0	102	183.0	103	186.0	104	211.0
105	213.0	106	232.0	107	202.0	108	193.0	109	226.0	110	216.0	111	276.0	112	216.0
113	255.0	114	267.0	115	264.0	116	286.0	117	284.0	118	355.0	119	422.0	120	518.0
121	572.0	122	667.0	123	786.0	124	931.0	125	1104.0	126	1346.0	127	1468.0	128	1773.0
129	2212.0	130	2628.0	131	3064.0	132	3570.0	133	4174.0	134	4807.0	135	5687.0	136	6300.0
137	7224.0	138	8055.0	139	8988.0	140	9823.0	141	10811.0	142	11458.0	143	12322.0	144	13102.0
145	13986.0	146	14136.0	147	14622.0	148	14864.0	149	15118.0	150	15340.0	151	15056.0	152	14772.0
153	14448.0	154	14133.0	155	13776.0	156	12895.0	157	12512.0	158	11704.0	159	10895.0	160	10211.0
161	9439.0	162	8741.0	163	8145.0	164	7428.0	165	6833.0	166	6114.0	167	5586.0	168	5241.0
169	4507.0	170	4121.0	171	3660.0	172	3267.0	173	2916.0	174	2629.0	175	2353.0	176	2123.0
177	1885.0	178	1678.0	179	1504.0	180	1355.0	181	1232.0	182	1097.0	183	1009.0	184	864.0
185	886.0	186	785.0	187	685.0	188	575.0	189	431.0	190	346.0	191	248.0	192	145.0
193	458.0	194	446.0	195	426.0	196	404.0	197	378.0	198	361.0	199	370.0	200	344.0
201	317.0	202	309.0	203	328.0	204	316.0	205	327.0	206	216.0	207	338.0	208	277.0
209	291.0	210	272.0	211	304.0	212	301.0	213	306.0	214	307.0	215	278.0	216	298.0
217	261.0	218	295.0	219	267.0	220	299.0	221	262.0	222	257.0	223	294.0	224	257.0

SHUTTER FUNCTION TRAPEZOID .232,535,232

INTERMEDIATE VALUES

STANDARD DEVIATION =	.159E+02	DBETA =	-.1666E+00	OVZRO =	-.4632E-01
STANDARD DEVIATION =	.132E+02	DBETA =	.1602E+00	OVZRO =	.1765E-02
STANDARD DEVIATION =	.125E+02	DBETA =	-.8631E-01	OVZRO =	-.3139E-03
STANDARD DEVIATION =	.123E+02	DBETA =	-.4598E-01	OVZRO =	-.1631E-03
STANDARD DEVIATION =	.122E+02	DBETA =	-.2309E-01	OVZRO =	-.8122E-04

FINAL PARAMETER VALUES

BETA = .5136E+01 VZRO = .3807E+01 SPEED RATIO = .8527E+01 ALPHA = .4413E+00 ITERATIONS = 5 AVERAGE DEVIATION = 3.4

ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN REIA AND VZRO = .6373E-02 .5458E-01

CALCULATED DISTRIBUTION

82	236.4	83	236.4	84	236.4	85	236.4	86	236.4	87	236.4	88	236.4	89	236.4
90	236.4	91	236.4	92	236.4	93	236.4	94	236.4	95	236.4	96	236.4	97	236.4
98	236.4	99	236.4	100	236.4	101	236.4	102	236.4	103	236.4	104	236.4	105	236.4
106	236.4	107	236.4	108	236.5	109	236.5	110	236.7	111	237.0	112	237.6	113	236.8
114	240.8	115	244.3	116	250.2	117	259.7	118	274.7	119	297.0	120	331.5	121	380.5

122	449.6	123	544.4	124	671.5	125	830.5	126	1051.3	127	1318.7	128	1647.0	129	2042.1
130	2538.1	131	3047.3	132	3659.5	133	4361.9	134	5088.6	135	5891.0	136	6737.8	137	7619.2
138	8506.9	139	9396.4	140	10265.8	141	11097.1	142	11871.2	143	12576.5	144	13208.9	145	13774.1
146	14182.1	147	14450.1	148	14644.1	149	14723.9	150	14671.1	151	14453.8	152	14166.2	153	13787.9
154	13579.1	155	13100.7	156	12564.4	157	11981.5	158	11351.5	159	10721.3	160	10085.1	161	9404.2
162	8746.9	163	8100.6	164	7471.4	165	6864.4	166	6291.7	167	5732.4	168	5212.7	169	4725.0
170	4272.9	171	3953.6	172	3667.7	173	3414.1	174	3191.3	175	2996.3	176	2814.9	177	1996.9
178	1783.5	179	1592.8	180	1422.9	181	1272.1	182	1134.6	183	1020.8	184	917.1	185	826.1
186	746.3	187	676.7	188	615.9	189	563.1	190	517.2	191	477.5	192	443.1	193	413.4
194	387.8	195	365.8	196	346.9	197	330.6	198	316.7	199	304.7	200	294.5	201	285.8
202	276.4	203	272.0	204	268.6	205	262.3	206	256.1	207	254.8	208	252.0	209	249.5
210	247.6	211	245.8	212	244.4	213	243.1	214	242.1	215	241.2	216	240.5	217	239.8
218	239.3	219	238.8	220	238.5	221	238.1	222	237.9	223	237.6				

KE 13F CALIBRATION DATA SHEET

MASS = 131.000

CHANNEL WIDTH = 3.0 MICROSECONDS; BEGINNING CHANNEL = 121; ENDING CHANNEL = 255; CHANNEL LENGTH = 134 CM; TONER LENGTH = 1.00 CM

OFFSET = 81 CHANNELS

WHEEL FREQ. = 240. MZ; WHEEL DIAMETER = 17.3 CM; SLOT WIDTH = .26 MM; DEFLECTION APERTURE = .25 MM

INPUT DESCRIPTION

121	159.0	122	101.0	123	134.0	124	125.0	125	125.0	126	121.0	127	126.0	128	131.0
129	137.0	130	111.0	131	121.0	132	107.0	133	112.0	134	129.0	135	141.0	136	133.0
137	147.0	138	121.0	139	146.0	140	153.0	141	172.0	142	152.0	143	171.0	144	157.0
145	207.0	146	225.0	147	218.0	148	288.0	149	272.0	150	324.0	151	379.0	152	404.0
153	478.0	154	533.0	155	611.0	156	721.0	157	816.0	158	944.0	159	1040.0	160	1243.0
161	1404.0	162	1625.0	163	1907.0	164	2228.0	165	2459.0	166	2845.0	167	3231.0	168	3543.0
169	3914.0	170	4418.0	171	4804.0	172	5330.0	173	5681.0	174	6252.0	175	6677.0	176	7219.0
177	7590.0	178	8057.0	179	8385.0	180	8736.0	181	9111.0	182	9467.0	183	9751.0	184	9754.0
185	10031.0	186	10047.0	187	10101.0	188	10347.0	189	10634.0	190	9693.0	191	9737.0	192	9316.0
193	9100.0	194	8035.0	195	8610.0	196	8144.0	197	7732.0	198	7410.0	199	6496.0	200	6659.0
201	6066.0	202	5758.0	203	5474.0	204	5051.0	205	4674.0	206	4411.0	207	4334.0	208	3775.0
209	3457.0	210	3133.0	211	2898.0	212	2727.0	213	2457.0	214	2156.0	215	2064.0	216	1861.0
217	1770.0	218	1557.0	219	1436.0	220	1308.0	221	1166.0	222	1111.0	223	1070.0	224	904.0
225	835.0	226	761.0	227	720.0	228	617.0	229	546.0	230	601.0	231	558.0	232	484.0
233	478.0	234	410.0	235	398.0	236	354.0	237	345.0	238	345.0	239	312.0	240	307.0
241	250.0	242	281.0	243	240.0	244	227.0	245	272.0	246	234.0	247	242.0	248	109.0
249	215.0	250	253.0	251	184.0	252	215.0	253	214.0	254	201.0	255	145.0		

SHUTTER FUNCTION TRAPEZOID .23F.535.235

INTERMEDIATE VALUES

STANDARD DEVIATION*	.120E+02	BETA*	-.3945E+00	DELTA*	-.4264E-01
STANDARD DEVIATION*	.053E+01	BETA*	.2512E+00	DELTA*	.1343E-02
STANDARD DEVIATION*	.877E+01	BETA*	.1445E+00	DELTA*	.4059E-03
STANDARD DEVIATION*	.851E+01	BETA*	.8279E-01	DELTA*	.2121E-03
STANDARD DEVIATION*	.847E+01	BETA*	.4546E-01	DELTA*	.1110E-03
STANDARD DEVIATION*	.845E+01	BETA*	.2478E-01	DELTA*	.6039E-04

FINAL PARAMETER VALUES

BETA* = .811E+01 VZRO* = .3956E+01 SPEED RATIO* = .8710E+01 ALPHA* = .4511E+03 ITERATIONS* = 6 AVERAGE DEVIATION* = 7.9
ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA AND VZRO* = .1309E-01 .4787E-03

CALCULATED DISTRIBUTION

122	158.0	123	158.0	124	158.0	125	158.0	126	154.0	127	154.0	128	156.0	129	158.0
130	158.0	131	156.0	132	158.0	133	154.0	134	154.0	135	154.0	136	154.0	137	156.0
138	158.0	139	158.0	140	158.0	141	154.0	142	160.0	143	161.0	144	163.0	145	167.0
146	171.0	147	174.0	148	180.0	149	203.0	150	222.0	151	247.0	152	281.0	153	306.0
154	383.0	155	454.0	156	544.0	157	651.0	158	786.0	159	941.0	160	1126.0	161	1335.0

162	1386.6	163	1861.0	164	2160.5	165	2530.7	166	2841.3	167	3274.1	168	3709.3	169	4146.1
170	4612.0	171	5081.0	172	5566.6	173	6059.2	174	6571.3	175	6994.8	176	7450.8	177	7946.1
178	8446.1	179	8631.6	180	8917.0	181	9160.2	182	9455.1	183	9682.5	184	9720.2	185	9701.8
186	9875.7	187	9904.9	188	9737.4	189	9675.6	190	9472.1	191	9281.0	192	8955.4	193	8195.7
194	8275.7	195	8004.9	196	7737.4	197	7475.6	198	7238.1	199	6851.3	200	6398.1	201	4135.7
202	5781.9	203	5431.2	204	5080.9	205	4757.6	206	4357.4	207	3947.5	208	3570.4	209	3137.3
210	3175.2	211	3021.1	212	2781.8	213	2557.4	214	2184.5	215	2152.3	216	1870.4	217	1837.3
218	1846.9	219	1701.9	220	1722.6	221	1752.2	222	1147.3	223	1042.3	224	950.0	225	884.0
228	793.0	229	725.1	230	653.6	231	608.7	232	556.3	233	514.4	234	474.5	235	439.7
238	369.5	239	318.1	240	284.7	241	253.7	242	217.8	243	214.9	244	276.0	245	261.9
248	190.2	249	186.1	250	182.6	251	179.5	252	176.8	253	174.7	254	169.9	255	164.7

BENZENE MONOMER 3.21 MVOLT VOZZLF, 400 TORR TOTAL/HE, 23 CENT, BATH

MASS = 78.000

CHANNEL WIDTH = 2.0 MICROSECONDS; BEGINNING CHANNEL = 40; ENDING CHANNEL = 160; FLIGHT LENGTH = 10.56 CM; IONIZER LENGTH = 1.03 CM;

OFFSET = -11. CHANNELS

WHEEL FREQ. = 401. HZ; WHEEL DIAMETER = 17.3 CM; SLOT WIDTH = .76 MM; DETECTOR APERTURE = .13 MM

INPUT DISTRIBUTION

49	18.0	50	75.0	51	75.0	52	10.0	53	16.0	54	57.0	55	66.0	56	68.0
57	87.0	58	74.0	59	79.0	60	77.0	61	75.0	62	79.0	63	91.0	64	83.0
65	69.0	66	67.0	67	76.0	68	59.0	69	76.0	70	59.0	71	73.0	72	63.0
73	75.0	74	77.0	75	66.0	76	78.0	77	81.0	78	91.0	79	82.0	80	109.0
81	15.0	82	195.0	83	317.0	84	457.0	85	711.0	86	1112.0	87	1837.0	88	2557.0
89	3665.0	90	4967.0	91	6611.0	92	8097.0	93	10000.0	94	11831.0	95	13085.0	96	14750.0
97	15231.0	98	15667.0	99	15533.0	100	15081.0	101	14185.0	102	13187.0	103	11811.0	104	10414.0
105	9063.0	106	7611.0	107	6589.0	108	5695.0	109	4884.0	110	3827.0	111	3170.0	112	2498.0
113	2167.0	114	1774.0	115	1475.0	116	1277.0	117	1054.0	118	861.0	119	689.0	120	600.0
121	507.0	122	475.0	123	472.0	124	397.0	125	317.0	126	289.0	127	284.0	128	265.0
129	243.0	130	221.0	131	199.0	132	193.0	133	167.0	134	182.0	135	168.0	136	151.0
137	139.0	138	137.0	139	43.0	140	22.0	141	18.0	142	138.0	143	174.0	144	105.0
145	105.0	146	99.0	147	91.0	148	98.0	149	136.0	150	99.0	151	117.0	152	99.0
153	96.0	154	84.0	155	89.0	156	76.0	157	101.0	158	71.0	159	99.0	160	97.0

SHUTTER FUNCTION TRAPEZOID -214, 572, 214

INTERMEDIATE VALUES

STANDARD DEVIATION = .260E+02 DBETA = -.1736E+00 DVZRO = -.3996E-01

STANDARD DEVIATION = .2449E+02 DBETA = -.2752E-01 DVZRO = -.7949E-02

STANDARD DEVIATION = .2478E+02 DBETA = -.1179E-01 DVZRO = -.1637E-02

STANDARD DEVIATION = .247E+02 DBETA = -.5391E-02 DVZRO = -.6681E-03

FINAL PARAMETER VALUES

BETA = .1145E+01 VZRO = .9230E+01 SPEED RATIO = .9876E+01 ALPHA = .9366E+00 TRAJECTORY = 4 AVERAGE DEVIATION = 4.9

ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA AND VZRO = .1792E-02 .1504E-02

CALCULATED DISTRIBUTION

50	84.3	51	84.3	52	84.3	53	84.3	54	84.3	55	84.3	56	84.3	57	84.3
58	84.3	59	84.3	60	84.3	61	84.3	62	84.3	63	84.3	64	84.3	65	84.3
66	84.3	67	84.3	68	84.3	69	84.3	70	84.3	71	84.3	72	84.3	73	84.3
74	84.3	75	84.4	76	84.6	77	85.3	78	87.5	79	93.1	80	106.3	81	135.2
82	189.1	83	300.7	84	486.8	85	787.3	86	1242.1	87	1889.2	88	2757.0	89	3856.7
90	5172.8	91	6665.1	92	8264.3	93	9883.0	94	11414.3	95	12764.8	96	13655.6	97	14002.0
98	14968.0	99	14957.7	100	14113.5	101	13953.6	102	13019.0	103	11948.0	104	10745.8	105	9499.2
106	8261.0	107	7076.0	108	5976.1	109	4981.6	110	4103.1	111	3324.6	112	2696.5	113	2194.6
114	1812.0	115	1351.1	116	1061.7	117	832.4	118	652.7	119	513.1	120	405.7	121	323.8
122	261.7	123	215.1	124	180.2	125	156.4	126	135.3	127	121.2	128	111.0	129	103.5

130	98.1	131	74.2	132	91.3	133	80.1	134	87.2	135	81.6	80.1	137	85.6
138	85.2	139	84.5	140	85.7	141	84.6	142	84.5	143	85.4	84.4	145	84.6
146	86.3	147	84.3	148	86.3	149	84.3	150	84.3	151	84.3	84.3	153	84.3
154	84.3	155	84.3	156	86.3	157	84.3	158	84.3	159	84.3			

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BENZENE DIMER, 3,21 - 402214.000 HRR TOTAL/ME, 23 BATH

MASS = 156.000

CHANNEL WIDTH = 2.0 MICROSECONDS BEGINNING CHANNEL = 73, ENDING CHANNEL = 160, FLIGHT LENGTH = 16.40 CM, IONIZER LENGTH = 1.07 CM,

OFFSET = -16. CHANNELS

WHEEL FREQ. = 401. HZ; WHEEL DIAMETER = 17.3 CM; SLOT WIDTH = .76 MM; DETECTOR APERTURE = .13 MM

INPUT DISTRIBUTION

73	16977.0	74	16978.0	75	16630.0	76	16864.0	77	16914.0	78	16997.0	79	16831.0	80	16723.0
81	16772.0	82	16762.0	83	16958.0	84	16884.0	85	17061.0	86	16711.0	87	16738.0	88	16928.0
89	16996.0	90	16929.0	91	16758.0	92	16937.0	93	17063.0	94	16926.0	95	17086.0	96	17351.0
97	17605.0	98	18060.0	99	18474.0	100	19351.0	101	20346.0	102	21415.0	103	22369.0	104	22475.0
105	23726.0	106	24662.0	107	24775.0	108	24815.0	109	24846.0	110	24720.0	111	23882.0	112	22627.0
113	21604.0	114	20922.0	115	20278.0	116	19784.0	117	19104.0	118	18616.0	119	18386.0	120	17984.0
121	17925.0	122	17360.0	123	17526.0	124	17506.0	125	17143.0	126	17013.0	127	17117.0	128	17744.0
129	17110.0	130	17043.0	131	17078.0	132	16999.0	133	16915.0	134	16877.0	135	16842.0	136	17152.0
137	16755.0	138	16947.0	139	16952.0	140	17003.0	141	16899.0	142	16943.0	143	16959.0	144	16932.0
145	16789.0	146	16655.0	147	17036.0	148	16878.0	149	16873.0	150	16658.0	151	16878.0	152	16744.0
153	17208.0	154	16804.0	155	16523.0	156	17133.0	157	16923.0	158	16886.0	159	16779.0	160	16765.0
161	16902.0	162	16940.0	163	16698.0	164	16781.0	165	15906.0	166	16695.0	167	16670.0	168	16957.0

SHUTTER FUNCTION TRAPEZOID .214.572.214

INTERMEDIATE VALUES

STANDARD DEVIATION = .410E+01 DBETA = .2942E+00 OVZRO = .1556E+03

FINAL PARAMETER VALUES

BETA = .1424E+01 VZRO = .0924E+01 SPEED RATIO = .1065E+02 ALPHA = .9301E+00 ITERATIONS = 1 AVERAGE DEVIATION = 2.3
ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA AND VZRO = .1084E-01 .6190E-02

CALCULATED DISTRIBUTION

74	16802.7	75	16802.7	76	16802.7	77	16802.7	78	16832.7	79	16832.7	80	16832.7	81	16802.7
82	16802.7	83	16802.7	84	16802.7	85	16802.7	86	16803.2	87	16804.2	88	16806.9	89	16819.4
90	16827.6	91	16856.2	92	16909.7	93	17002.2	94	17156.1	95	17304.1	96	17712.6	97	18154.4
98	18715.1	99	19347.1	100	20148.0	101	20951.0	102	21774.5	103	22547.0	104	23214.0	105	23744.4
106	24075.6	107	24220.9	108	24170.1	109	23938.0	110	23551.4	111	23044.6	112	22455.6	113	21821.4
114	21175.4	115	20562.5	116	19955.1	117	19415.9	118	18917.3	119	18522.4	120	18173.2	121	17877.1
122	17637.0	123	17443.6	124	17290.2	125	17169.9	126	17076.9	127	17005.8	128	16952.0	129	16911.6
130	16881.6	131	16859.5	132	16834.4	133	16811.7	134	16823.2	135	16817.2	136	16812.0	137	16809.8
138	16807.7	139	16806.2	140	16805.1	141	16804.4	142	16833.8	143	16833.5	144	16833.2	145	16803.1
146	16833.0	147	16802.9	148	16802.9	149	16802.8	150	16802.9	151	16802.8	152	16832.7	153	16802.7
154	16802.7	155	16802.7	156	16802.7	157	16802.7	158	16802.7	159	16802.7	160	16802.7	161	16802.7
162	16802.7	163	16802.7	164	16802.7	165	16802.7	166	16802.7	167	16802.7	168	16802.7	169	16802.7

The image shows a document page with a grid of horizontal and vertical lines. The page is oriented vertically. In the upper right quadrant, there are several black marks, including dots and dashes, arranged in a pattern that suggests a sequence or a list. The marks are scattered across the page, with a higher concentration in the upper right. The overall appearance is that of a high-contrast, black and white scan of a document, possibly a ledger or a form, with a grid of lines and scattered black marks.

COOLED AN IN TEST CHAMBER

MASS = 40.000

CHANNEL WIDTH = 10.3 MICROSECONDS BEGINNING CHANNEL = 101, ENDING CHANNEL = 2501, SLIT LENGTH = 0.77 CM, IONIZER LENGTH = .53 CM.

DPFSET = 7.6 CHANNELS

WHEEL FREQ. = 72. HZ; WHEEL DIAMETER = 11.8 CM; SLOT WIDTH = .78 MM; DEFLECTOR APERTURE = .91 MM

INPUT DISTRIBUTION

101	47939.0	102	48745.0	103	48208.0	104	47793.0	105	48189.0	106	47536.0	107	47917.0	108	48219.0
109	47842.0	110	48451.0	111	48136.0	112	48313.0	113	47947.0	114	48313.0	115	48391.0	116	47878.0
117	47886.0	118	47842.0	119	47987.0	120	47771.0	121	48135.0	122	48497.0	123	48191.0	124	48227.0
125	47889.0	126	48044.0	127	48287.0	128	48519.0	129	47941.0	130	48436.0	131	48417.0	132	48072.0
133	47928.0	134	48651.0	135	48547.0	136	48543.0	137	48811.0	138	48751.0	139	48694.0	140	48258.0
141	48976.0	142	50011.0	143	50132.0	144	50205.0	145	51153.0	146	51684.0	147	52139.0	148	52992.0
149	53798.0	150	54116.0	151	54697.0	152	55823.0	153	55745.0	154	58281.0	155	58422.0	156	59973.0
157	60675.0	158	62808.0	159	62721.0	160	64551.0	161	65076.0	162	66138.0	163	67070.0	164	67643.0
165	68031.0	166	68894.0	167	69485.0	168	68715.0	169	68535.0	170	69123.0	171	68497.0	172	67986.0
173	67511.0	174	66624.0	175	65905.0	176	65014.0	177	64337.0	178	63267.0	179	62592.0	180	62118.0
181	60167.0	182	58444.0	183	58735.0	184	58048.0	185	57362.0	186	56588.0	187	55535.0	188	54977.0
189	54577.0	190	53935.0	191	53359.0	192	52755.0	193	52454.0	194	51672.0	195	51749.0	196	51183.0
197	50646.0	198	50556.0	199	50027.0	200	50312.0	201	49564.0	202	49514.0	203	49650.0	204	49667.0
205	48781.0	206	49087.0	207	48705.0	208	49022.0	209	49774.0	210	48541.0	211	48654.0	212	48449.0
213	48729.0	214	48674.0	215	48505.0	216	48824.0	217	48446.0	218	48802.0	219	48369.0	220	48727.0
221	48292.0	222	47929.0	223	48525.0	224	48321.0	225	48031.0	226	48222.0	227	48234.0	228	48524.0
229	48197.0	230	47813.0	231	48366.0	232	47986.0	233	47943.0	234	47902.0	235	47845.0	236	48349.0
237	47853.0	238	48025.0	239	47776.0	240	48113.0	241	48743.0	242	48050.0	243	48327.0	244	48187.0
245	48112.0	246	48227.0	247	48287.0	248	47845.0	249	48142.0	250	47711.0				

SHUTTER FUNCTION TRAPEZOID .022, .117, .216, .217, .117, .022

INTERMEDIATE VALUES

STANDARD DEVIATION = .471E+01 DBETA = .3910E+00 DV2H3 = -.8470E-02
STANDARD DEVIATION = .257E+01 DBETA = .3083E+00 DV2H3 = .346E-02

FINAL PARAMETER VALUES

BETA = .4992E+01 V2H0 = .4076E+01 SPEED RATIO = .8697E+01 ALPHA = .4687E+00 ITERATIONS = 2 AVERAGE DEVIATION = .17
ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA AND V2H0 = .1424E-01 .1353E-02

CALCULATED DISTRIBUTION

104	48049.6	105	48049.6	106	48049.6	107	48049.6	108	48049.6	109	48049.6	110	48049.6	111	48049.6
112	48049.6	113	48049.6	114	48049.6	115	48049.6	116	48049.6	117	48049.6	118	48049.6	119	48049.6
120	48049.6	121	48049.6	122	48049.6	123	48049.6	124	48049.6	125	48049.6	126	48049.6	127	48049.6
128	48057.1	129	48052.1	130	48059.8	131	48281.5	132	48090.3	133	48124.5	134	48160.8	135	48211.4
136	48280.7	137	48373.5	138	48445.6	139	48653.6	140	48851.8	141	49103.7	142	49410.3	143	49780.3
144	50219.9	145	50733.7	146	51325.6	147	51947.1	148	52747.9	149	53574.7	150	54473.9	151	55456.3
152	56452.4	153	57510.0	154	58594.9	155	59641.6	156	60711.5	157	61853.3	158	62844.0	159	63948.9

160	48172.9	169	48000.7	172	48301.2	183	48413.9	194	48411.0	195	48787.4	196	48040.1	187	48108.8
168	48172.9	169	48000.7	172	48301.2	183	48413.9	194	48411.0	195	48787.4	196	48040.1	187	48108.8
170	48455.4	177	48022.9	178	48119.9	179	48244.0	180	48370.2	181	48370.2	182	48001.7	173	48354.4
184	48455.4	185	48022.9	186	48119.9	187	48244.0	188	48370.2	189	48370.2	190	48001.7	181	48354.4
200	48018.0	193	48022.9	194	48119.9	195	48244.0	196	48370.2	197	48370.2	198	48001.7	189	48354.4
208	48018.0	209	48022.9	210	48119.9	211	48244.0	212	48370.2	213	48370.2	214	48001.7	207	48354.4
216	48444.8	217	48022.9	218	48119.9	219	48244.0	220	48370.2	221	48370.2	222	48001.7	215	48354.4
224	48444.8	225	48022.9	226	48119.9	227	48244.0	228	48370.2	229	48370.2	230	48001.7	217	48354.4
232	48000.7	233	48022.9	234	48119.9	235	48244.0	236	48370.2	237	48370.2	238	48001.7	219	48354.4
240	48000.7	241	48022.9	242	48119.9	243	48244.0	244	48370.2	245	48370.2	246	48001.7	219	48354.4

HE 640 PSI SHORT FLIGHT PATH

MASS = 4.000

CHANNEL WIDTH = 2.0 MICROSECONDS BEGINNING CHANNEL = 101, ENDING CHANNEL = 234; FLIGHT LENGTH = 29.40 CM; IONIZER LENGTH = 1.00 CM,

OFFSET = -3.0 CHANNELS

HMF FREQ. = 350, HZ1 WHEEL DIAMETER = 17.3 CM; SLOT WIDTH = .86 MM; DETECTOR APERTURE = .13 MM

INPUT DISTRIBUTION

101	1043.0	102	1120.0	103	1075.0	104	1088.0	105	1105.0	106	1033.0	107	1057.0	108	1094.0
109	1044.0	110	1038.0	111	1067.0	112	1085.0	113	1231.0	114	1355.0	115	1308.0	116	1094.0
117	1108.0	118	1091.0	119	1069.0	120	1055.0	121	1124.0	122	1074.0	123	1029.0	124	1084.0
125	1134.0	126	1149.0	127	1066.0	128	1134.0	129	1047.0	130	1126.0	131	1075.0	132	1064.0
135	1101.0	136	1121.0	137	1072.0	138	1137.0	139	1183.0	140	1106.0	141	1238.0	142	1246.0
141	1336.0	142	1441.0	143	1391.0	144	1424.0	145	1452.0	146	1410.0	147	1460.0	148	1432.0
149	1501.0	150	1443.0	151	1408.0	152	1453.0	153	1767.0	154	2083.0	155	2923.0	156	5446.0
157	1152.0	158	1121.0	159	1048.0	160	1407.0	161	16751.0	162	25649.0	163	14207.0	164	7875.0
165	4450.0	166	2787.0	167	2084.0	168	1654.0	169	1576.0	170	1411.0	171	1370.0	172	1316.0
173	1356.0	174	1292.0	175	1369.0	176	1347.0	177	1316.0	178	1354.0	179	1311.0	180	1256.0
181	1328.0	182	1350.0	183	1253.0	184	1274.0	185	1259.0	186	1192.0	187	1211.0	188	1137.0
189	1096.0	190	1137.0	191	1275.0	192	1172.0	193	1091.0	194	1397.0	195	1186.0	196	1127.0
197	1021.0	198	1086.0	199	1073.0	200	1115.0	201	1143.0	202	1022.0	203	1054.0	204	1090.0

SHUTTER FUNCTION TRAPEZOID .280,440,280

INTERMEDIATE VALUES

STANDARD DEVIATION=	.185E+03	DBETA=	.6467E+01	OVZRO=	.1986E-01
STANDARD DEVIATION=	.161E+03	DBETA=	.7542E+01	OVZRO=	-.1718E-02
STANDARD DEVIATION=	.145E+03	DBETA=	.7115E+01	OVZRO=	-.2640E-03
STANDARD DEVIATION=	.135E+03	DBETA=	.6566E+01	OVZRO=	.3225E-03
STANDARD DEVIATION=	.128E+03	DBETA=	.6001E+01	OVZRO=	.2742E-03
STANDARD DEVIATION=	.121E+03	DBETA=	.5450E+01	OVZRO=	.2207E-03
STANDARD DEVIATION=	.123E+03	DBETA=	.4952E+01	OVZRO=	.1611E-03
STANDARD DEVIATION=	.117E+03	DBETA=	.4448E+01	OVZRO=	.1504E-03
STANDARD DEVIATION=	.115E+03	DBETA=	.4067E+01	OVZRO=	.1262E-03
STANDARD DEVIATION=	.114E+03	DBETA=	.3686E+01	OVZRO=	.1370E-03

FINAL PARAMETER VALUES

RETA=	.1001E+03	VZRO=	.9508E+01	SPEED RATIO=	.9514E+02	ALPHA=	.9796E-01	ITERATIONS=	10	AVERAGE DEVIATION=	10.5
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C A U T I O N----- THE FULL NUMBER OF ITERATIONS HAS OCCURRED WITHOUT CONVERGENCE

ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA AND VZRO= .9844E-01 .2974E-03

CALCULATED DISTRIBUTION

102	1194.6	103	1194.6	104	1194.6	105	1194.6	106	1194.6	107	1194.6	108	1194.6	109	1194.6
110	1194.6	111	1194.6	112	1194.6	113	1194.6	114	1194.6	115	1194.6	116	1194.6	117	1194.6
118	1194.6	119	1194.6	120	1194.6	121	1194.6	122	1194.6	123	1194.6	124	1194.6	125	1194.6

124	1194.6	127	1194.6	128	1194.6	129	1194.6	130	1194.6	131	1194.6	132	1194.6	133	1194.6
142	1194.6	135	1194.6	144	1194.6	145	1194.6	146	1194.6	147	1194.6	148	1194.6	149	1194.6
152	1194.6	143	1194.6	152	1194.6	153	1194.6	154	1194.6	155	1194.6	156	1194.6	157	1194.6
164	1194.6	151	1194.6	160	1194.6	161	1194.6	162	1194.6	163	1194.6	164	1194.6	165	1194.6
174	1194.6	167	1194.6	176	1194.6	177	1194.6	178	1194.6	179	1194.6	180	1194.6	181	1194.6
182	1194.6	175	1194.6	184	1194.6	185	1194.6	186	1194.6	187	1194.6	188	1194.6	189	1194.6
190	1194.6	183	1194.6	192	1194.6	193	1194.6	194	1194.6	195	1194.6	196	1194.6	197	1194.6
198	1194.6	191	1194.6	200	1194.6	201	1194.6	202	1194.6	203	1194.6	204	1194.6	205	1194.6

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XEO002.TOF

MASS = 44.000

CHANNEL WIDTH = 6.0 MICROSECONDS; BEGINNING CHANNEL = 121; ENDING CHANNEL = 210; FLIGHT LENGTH = 29.30 CM; IONIZER LENGTH = 1.95 CM;

OFFSETH = 3.0 CHANNELS

WHEEL FREQ. = 150. HZ; WHEEL DIAMETER = 17.3 CM; SLOT WIDTH = .06 MM; DETECTOR APERTURE = .13 MM

INPUT DISTRIBUTION

121	1665.0	122	1668.0	123	1674.0	124	1582.0	125	1570.0	126	1533.0	127	1616.0	128	1625.3
129	1521.0	130	1602.0	131	1607.0	132	1507.3	133	1617.3	134	1618.0	135	1616.0	136	1649.0
137	1551.0	138	1715.0	139	1847.0	140	1820.0	141	1323.3	142	2267.0	143	2105.0	144	2158.0
145	2478.0	146	2717.0	147	3099.0	148	3454.0	149	4037.0	150	4527.0	151	5254.0	152	6011.0
153	7186.0	154	8246.0	155	9404.0	156	10810.0	157	12357.0	158	13722.0	159	15348.0	160	16848.0
161	18218.0	162	19232.0	163	20259.0	164	20985.0	165	21007.0	166	21312.0	167	21999.0	168	22588.0
169	19922.0	170	18875.0	171	17648.0	172	16322.0	173	15171.0	174	13511.0	175	12327.0	176	11033.0
177	9936.0	178	8762.0	179	7615.0	180	6544.0	181	5171.0	182	3549.0	183	2014.0	184	932.0
186	3784.0	187	2577.0	188	1621.0	189	922.0	190	2799.0	191	2526.0	192	2332.0	193	2302.0
195	2126.0	196	2098.0	197	2026.0	198	1993.0	199	2011.0	200	1813.0	201	1851.0	202	1844.0
201	1742.0	202	1850.0	203	1723.0	204	1722.0	205	1654.0	206	1737.0	207	1612.0	208	1650.0
209	1675.0	210	1665.0	211	1644.0	212	1732.0	213	1574.0	214	1623.0	215	1657.0	216	1618.0

SHUTTER FUNCTION TRAPEZOID .217.565.217

INTERMEDIATE VALUES

STANDARD DEVIATION	+.101E+02	DBETA	+.3315E+00	DVZRO	+.6750E-02
STANDARD DEVIATION	+.927E+01	DBETA	+.3408E+00	DVZRO	+.2134E-03
STANDARD DEVIATION	+.903E+01	DBETA	+.1922E+00	DVZRO	+.9846E-04
STANDARD DEVIATION	+.895E+01	DBETA	+.1045E+00	DVZRO	+.5128E-04
STANDARD DEVIATION	+.894E+01	DBETA	+.5841E-01	DVZRO	+.2081E-04

FINAL PARAMETER VALUES

BETA = .2016E+02 VZPO = .3035E+01 SPEED RATIO = .1363E+02 ALPHA = .2227E+00 IEPAT115 = 7 AVERAGE DEVIATION = 2.9
 ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA (MM) VZRO = .2662E-01 .3131E-01

CALCULATED DISTRIBUTION

122	1705.8	123	1705.8	124	1705.8	125	1705.8	126	1705.8	127	1705.8	128	1705.8	129	1705.8
130	1705.8	131	1705.8	132	1705.8	133	1706.1	134	1736.4	135	1707.7	136	1736.7	137	1711.7
138	1717.3	139	1727.4	140	1744.8	141	1773.8	142	1820.6	143	1893.5	144	2001.1	145	2163.1
146	2389.2	147	2590.1	148	3111.5	149	3644.5	150	4313.4	151	5131.4	152	6131.3	153	7273.4
154	8447.8	155	9860.6	156	11321.6	157	12827.4	158	14330.7	159	15781.0	160	17124.9	161	18410.7
162	19316.4	163	20082.4	164	20593.6	165	20837.1	166	20812.1	167	20578.6	168	20206.7	169	19774.4
170	18365.6	171	17317.5	172	16168.9	173	14957.4	174	13718.5	175	12483.7	176	11272.2	177	10129.7
178	9049.2	179	8053.2	180	7143.3	181	6321.7	182	5573.3	183	4957.9	184	4436.7	185	3929.4
186	3525.2	187	3184.5	188	2899.9	189	2664.0	190	2473.1	191	2312.0	192	2183.4	193	2083.8
194	1908.5	195	1831.1	196	1801.4	197	1843.9	198	1833.3	199	1784.7	200	1765.7	201	1751.1
202	1739.9	203	1731.4	204	1725.0	205	1720.1	206	1716.4	207	1713.7	208	1711.6	209	1710.1

210 1708.9 211 1708.1 212 1707.5 213 1707.0 214 1706.7 215 1706.4

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KR0002.TOF

MASS = 42.000

CHANNEL WIDTH = 5.0 MICROSECONDS BEGINNING CH

113; ENDING CHANNEL = 224; FLIGHT LENGTH = 20.50 CM; IONIZER LENGTH = 1.02 CM

OFFSET = -3.6 CHANNELS

WHEEL FREQ. = 200. HZ; WHEEL DIAMETER = 17.3 CM; SLIT WIDTH = .86 MM; DETECTOR APERTURE = .13 MM

INPUT DISTRIBUTION

113	380.0	114	352.0	115	354.0	116	337.0	117	343.0	118	361.0	119	387.0	120	353.0
121	389.0	122	381.0	123	411.0	124	395.0	125	426.0	126	426.0	127	449.0	128	472.0
129	490.0	130	532.0	131	601.0	132	611.0	133	732.0	134	843.0	135	1000.0	136	1190.0
137	141.0	138	165.0	139	215.0	140	261.0	141	337.0	142	411.0	143	497.0	144	678.0
145	776.0	146	959.0	147	1160.0	148	1355.0	149	1634.0	150	1923.0	151	2221.0	152	2562.0
153	2807.0	154	3106.0	155	3381.0	156	3615.0	157	3806.0	158	3973.0	159	3974.0	160	3941.0
161	3914.0	162	3786.0	163	3559.0	164	3352.0	165	3142.0	166	2806.0	167	2577.0	168	2319.0
169	2062.0	170	1804.0	171	1589.0	172	1357.0	173	1186.0	174	991.0	175	851.0	176	716.0
177	607.0	178	516.0	179	429.0	180	376.0	181	312.0	182	265.0	183	225.0	184	195.0
185	180.0	186	157.0	187	131.0	188	119.0	189	106.0	190	95.0	191	80.0	192	87.0
193	82.0	194	70.0	195	64.0	196	65.0	197	59.0	198	55.0	199	53.0	200	49.0
201	53.0	202	49.0	203	44.0	204	50.0	205	43.0	206	46.0	207	45.0	208	45.0
209	45.0	210	43.0	211	45.0	212	40.0	213	40.0	214	39.0	215	41.0	216	37.0
217	36.0	218	37.0	219	37.0	220	37.0	221	34.0	222	37.0	223	35.0	224	34.0

SHUTTER FUNCTION TRAPEZOID .186,628,186

INTERMEDIATE VALUES

STANDARD DEVIATION=	.356E+02	BETA=	-.1306E+01	DV1R3=	-.2933E-01
STANDARD DEVIATION=	.347E+02	BETA=	-.1416E+00	DV1R2=	-.5992E-07
STANDARD DEVIATION=	.345E+02	BETA=	-.6896E-01	DV1R3=	-.1272E-04
STANDARD DEVIATION=	.345E+02	BETA=	-.3407E-01	DV1R2=	-.6768E-05

FINAL PARAMETER VALUES

BETA=	.1175E+02	VZRO=	.3803E+01	SPEED HATU=	.1304E+02	ALPHA=	.2917E+00	ITERATIONS=	4	AVERAGE DEVIATION=	5.8
ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA		AND VZRO=	.8731E-02							.2406E-03	

CALCULATED DISTRIBUTION

114	462.8	115	462.8	116	462.8	117	462.8	118	462.8	119	462.8	120	462.8	121	462.8
122	462.8	123	462.8	124	462.9	125	462.9	126	461.1	127	461.4	128	464.1	129	465.7
130	468.9	131	475.3	132	487.3	133	509.0	134	546.7	135	609.7	136	711.4	137	869.8
138	1100.2	139	1455.4	140	1944.7	141	2613.3	142	3609.3	143	4638.9	144	6362.3	145	7780.7
146	9827.0	147	12162.6	148	14745.2	149	17582.7	150	20544.2	151	23562.4	152	26538.8	153	29560.7
154	31972.5	155	34193.0	156	36010.7	157	37344.4	158	38155.0	159	38277.0	160	38158.4	161	37498.7
162	36105.4	163	34505.8	164	32265.8	165	30406.7	166	28163.4	167	25713.3	168	23271.8	169	20960.8
170	18507.5	171	16285.6	172	14212.9	173	12308.5	174	10589.9	175	9039.4	176	7615.2	177	6482.8
178	5451.6	179	4568.6	180	3819.4	181	3189.5	182	2666.1	183	2229.5	184	1872.6	185	1581.7
186	1346.1	187	1154.6	188	1005.2	189	884.8	190	789.5	191	714.9	192	654.4	193	615.9

194	575.7	195	568.5	196	527.7	197	511.7	198	493.6	199	470.4	200	453.4	201	438.2
202	424.2	203	411.3	204	400.1	205	387.4	206	366.2	207	345.3	208	324.4	209	303.5
210	282.6	211	261.7	212	240.8	213	219.9	214	199.0	215	178.1	216	157.2	217	136.3
218	115.4	219	94.5	220	73.6	221	52.7	222	31.8	223	10.9	224	-10.0	225	-30.9

HE 14 30 PER C. 12

MASS = 4.000

CHANNEL WIDTH = 15.0 MICROSECONDS; BEGINNING CHANNEL = 51; ENDING CHANNEL = 167; FLIGHT LENGTH = 07.70 CM; TWTIZER LENGTH = 1.00 CM.

OFFSET = -2.0 CHANNELS

WHEEL PAFO = 140. HZ; WHEEL DIAMETER = 11.8 CM; SLOT WIDTH = .78 MM; DETECTOR APERTURE = .13 MM

INPUT DISTRIBUTION

51	22587.0	52	22438.0	53	22674.0	54	22848.0	55	22582.0	56	22731.0	57	22715.0	58	22420.0
59	22572.0	60	22644.0	61	22698.0	62	22746.0	63	22851.0	64	22977.0	65	22971.0	66	23076.0
67	23115.0	68	23120.0	69	23478.0	70	23745.0	71	23578.0	72	24143.0	73	24540.0	74	24910.0
75	25492.0	76	26211.0	77	27050.0	78	28851.0	79	29861.0	80	32407.0	81	35398.0	82	39255.0
83	44418.0	84	51788.0	85	60152.0	86	71590.0	87	86114.0	88	103485.0	89	124611.0	90	148447.0
91	17576.0	92	204685.0	93	233852.0	94	266209.0	95	299429.0	96	329633.0	97	361952.0	98	390139.0
99	419296.0	100	463173.0	101	464408.0	102	482133.0	103	493522.0	104	498572.0	105	501311.0	106	496337.0
107	486475.0	108	471641.0	109	452810.0	110	429786.0	111	433311.0	112	376397.0	113	347324.0	114	319460.0
115	240919.0	116	264926.0	117	242086.0	118	220418.0	119	230052.0	120	191126.0	121	163631.0	122	135501.0
123	139683.0	124	119469.0	125	106486.0	126	95366.0	127	87958.0	128	76558.0	129	68371.0	130	62910.0
131	46006.0	132	51471.0	133	47115.0	134	43543.0	135	40242.0	136	37221.0	137	34986.0	138	32419.0
139	31178.0	140	30035.0	141	28626.0	142	27540.0	143	26729.0	144	26267.0	145	25564.0	146	25095.0
147	24578.0	148	24412.0	149	24219.0	150	24083.0	151	23781.0	152	23675.0	153	23333.0	154	22973.0
155	23279.0	156	23150.0	157	23172.0	158	22837.0	159	22883.0	160	22664.0	161	22953.0	162	22445.0
163	22810.0	164	22644.0	165	22548.0	166	22712.0	167	22567.0						

SHUTTER FUNCTION TRAPEZOID .020.960.020

INTERMEDIATE VALUES

STANDARD DEVIATION	.437E+03	DBETA	.318E-01	DVZRO	-.453E-31
STANDARD DEVIATION	.329E+03	DBETA	-.523E-01	DVZRO	-.249E-02
STANDARD DEVIATION	.299E+03	DBETA	.285E-01	DVZRO	.904E-03
STANDARD DEVIATION	.291E+03	DBETA	.148E-01	DVZRO	.426E-03
STANDARD DEVIATION	.289E+03	DBETA	.756E-02	DVZRO	.2091E-03
STANDARD DEVIATION	.289E+03	DBETA	.379E-02	DVZRO	.9498E-04

FINAL PARAMETER VALUES

BETA = .1465E+01 VZRO = .9852E+01 SPEED RATIO = .7084E+01 ALPHA = .0261E+00 ITERATIONS = 6 AVERAGE DEVIATION = .36.7
ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA AND VZRO = .4395E-03 .2179E-03

CALCULATED DISTRIBUTION

52	23176.4	53	23176.4	54	23176.4	55	23176.4	56	23176.4	57	23176.4	58	23176.4	59	23176.4
60	23176.4	61	23176.4	62	23176.4	63	23176.4	64	23176.4	65	23176.4	66	23176.4	67	23176.4
68	23176.4	69	23176.4	70	23176.4	71	23176.4	72	23111.2	73	23189.7	74	23210.4	75	23257.8
76	23353.2	77	23563.2	78	23550.6	79	24647.1	80	25117.1	81	27774.4	82	32788.1	83	35799.2
84	4705.1	85	50552.1	86	62294.6	87	77346.1	88	96004.8	89	118414.7	90	144505.6	91	173900.5
92	206152.0	93	240861.7	94	276617.1	95	312495.2	96	347711.6	97	380898.0	98	411165.3	99	437578.9
100	459491.5	101	476373.2	102	487924.4	103	494055.0	104	498808.3	105	496368.8	106	481781.4	107	468816.5

108	432316.1	100	432970.3	110	411357.1	121	368117.6	112	363895.0	113	330042.4	114	314237.2	115	260981.5
116	26597.8	117	243120.4	118	271550.3	119	231085.1	120	182131.2	121	164565.1	122	144546.4	123	133750.5
134	56810.9	135	100550.3	136	97892.8	137	88271.0	138	79780.8	139	72298.8	140	65684.2	141	59868.5
142	52782.5	143	39071.3	144	29762.3	145	28777.2	146	29157.2	147	27851.2	148	25737.3	149	33865.5
148	25634.7	149	25258.5	150	24939.3	151	24688.6	152	24435.3	153	24242.0	154	23980.2	155	26077.4
156	23823.4	157	23721.0	158	23639.5	159	23568.2	160	23504.3	161	23457.0	162	23413.9	163	23377.5
166	23346.7	165	23320.7	166	23298.7										

HE 660 PSI LONG FLIGHT PATH

MASS = 4.000

CHANNEL WIDTH = 5.0 MICROSECONDS BEGINNING CHANNEL = 151, ENDING CHANNEL = 230, FLIGHT LENGTH = 92.20 CM, IONIZER LENGTH = 1.00 CM.

OFFSET = -2.0 CHANNELS

WHEEL FREQ. = 209.471 MMEL DIAMETER = 11.8 CM, SLOT WIDTH = .78 MM, DETECTOR APERTURE = .13 MM

INPUT DISTRIBUTION

151	58708.0	152	58727.0	153	59037.0	154	58649.3	155	58978.3	156	58772.0	157	59230.0	158	59188.0
159	58934.0	160	59297.0	161	59042.0	162	58827.0	163	58865.0	164	59099.0	165	59075.0	166	58956.0
167	59556.0	168	58809.0	169	58979.0	170	59080.0	171	59244.0	172	59202.0	173	59007.0	174	59374.3
175	58928.0	176	58765.0	177	59314.0	178	59211.0	179	59143.0	180	59766.0	181	59224.0	182	59266.0
183	58902.0	184	58843.0	185	59013.0	186	59162.0	187	59543.0	188	57691.0	189	60016.0	190	60701.0
191	62463.0	192	67548.0	193	77070.0	194	88348.0	195	96037.0	196	94168.0	197	82147.0	198	79425.0
199	64478.0	200	61168.0	201	60447.0	202	59634.0	203	59356.0	204	59034.0	205	59190.0	206	59371.0
207	59186.0	208	59335.0	209	58930.0	210	59462.0	211	59259.0	212	59011.0	213	59244.0	214	58996.0
215	58876.0	216	59295.0	217	59054.0	218	58404.0	219	59031.0	220	59023.0	221	59232.0	222	59181.0
223	58950.0	224	58985.0	225	59365.0	226	58944.0	227	58969.0	228	59105.0	229	58824.0	230	58971.0

SHUTTER FUNCTION TRAPEZOID .262.476.262

INTERMEDIATE VALUES

STANDARD DEVIATION = .283E+01 DBETA = .264E+01 DVZRO = .1367E-01

FINAL PARAMETER VALUES

BETA = .7548E+02 VZRO = .9567E+01 SPEED RATIO = .8311E+02 ALPHA = .1151E+00 ITERATIONS = 1 AVERAGE DEVIATION = 1.6

ESTIMATED ERROR IN LOCATION OF MINIMUM ON SURFACE IN BETA AND VZRO = .1230E+03 .5614E-01

CALCULATED DISTRIBUTION

152	59103.7	153	59103.7	154	59103.7	155	59103.7	156	59133.7	157	59103.7	158	59103.7	159	59123.7
160	59103.7	161	59103.7	162	59103.7	163	59133.7	164	59133.7	165	59103.7	166	59103.7	167	59103.7
168	59103.7	169	59103.7	170	59103.7	171	59103.7	172	59133.7	173	59103.7	174	59103.7	175	59133.7
176	59103.7	177	59103.7	178	59133.7	179	59133.7	180	59133.7	181	59103.7	182	59133.7	183	59103.7
184	59103.7	185	59133.7	186	59103.7	187	59133.7	188	59170.1	189	59238.7	190	59069.5	191	62146.5
192	67967.6	193	77087.6	194	88234.3	195	95543.7	196	92765.8	197	82966.5	198	72360.9	199	64407.3
200	60918.6	201	59516.9	202	59186.1	203	59114.3	204	59136.8	205	59133.8	206	59133.7	207	59103.7
208	59103.7	209	59103.7	210	59103.7	211	59103.7	212	59133.7	213	59103.7	214	59133.7	215	59103.7
216	59103.7	217	59133.7	218	59103.7	219	59133.7	220	59133.7	221	59133.7	222	59133.7	223	59103.7
224	59103.7	225	59103.7	226	59103.7	227	59103.7	228	59103.7	229	59103.7	230	59103.7		