LBL--25610

DE89 013359

LBL-25610
ESG-47

A GENERAL FORMALISM FOR QUASI-LOCAL CORRECTION OF MULTIPOLE
DISTORTIONS IN PERIODIC TRANSPORT SYSTEMS*

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June 1988

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*This work was supported by the Office of Energy Research, Office of Basic Energy Sciences, Department of Energy under Contract No. DE-AC03-76SF00098.

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A General Formalism for Quasi-Local Correction of Multipole Distortions in Periodic Transport Systems

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Abstract

We generalize a new concept of local correction of nonlinearities due to multipole content by giving it a mathematical description. We present a general method which allows for a general reduction of all the distortions produced by a given set of multipole errors. The method can be applied to correct an arbitrary distribution of the errors in any transport system, such as transport lines, linacs, synchrotrons and storage rings.

For reasons of stability and reliability, predominantly linear motion is required in a long beam transport system. In this linear motion, particle trajectories lie on ellipses in position-momentum phase space. Nonlinear motion due to multipole fields changes these trajectories in both amplitude and phase, distorting the phase space and causing instability on short or long time scales[1,2]. Therefore, one must correct the nonlinear effects of the multipole content present in the various elements of the system. A common correction technique for short optical systems (mass spectrometers or electron microscopes) is to identify a few key distortions and insert lumped correctors specifically designed to eliminate those. However, in long periodic transport systems, nonlinear effects can accumulate either coherently or noncoherently over repeated cells and a large number of distortions can affect the beam. Hence the nonlinear effects cannot be cancelled by a lumped correction scheme without either a prohibitively large number of correctors or undesirable high order effects due to large corrector strengths. In this paper, we present a new method of locally correcting nonlinearities in each transport cell in a way which reduces all nonlinear effects due to a given multipole content.

Figure 1 shows schematically a cell of a periodic transport system. Regions 1 and 3 are linear focussing or defocussing elements. Region 2 between those elements contains an arbitrary transport element with significant multipole content. The linear motion is represented by a Hamiltonian $H(s)$ which has two parts: a s -independent part H_0 which controls the motion in region 2 and an additional s -dependent part $U(s)$ which differs from H_0 in the focussing regions 1 and 3.

$$H(s) = H_0 + U(s), \quad (1)$$

Let us assume that the Hamiltonian is modified by a multipole represented by a term $e(s)W$, where $e(s)$ is the known multipole distribution throughout region 2,

and W is the Hamiltonian perturbation due to that multipole. We counteract its effect with a corrector distribution $c(s)$ of the same multipole. The trivial correction solution is given by

$$c(s) = -e(s). \quad (2)$$

We refer to this solution as "local" correction; it is not practical in general. Instead, we derive conditions on $c(s)$ which achieves a close approximation to Eq.(2).

In region 2, the motion is governed by the Hamiltonian $K(s)$:

$$K(s) = H_0 + (e(s) + c(s))W. \quad (3)$$

Following Dragt's notation for the Lie operators [3] parametrizing a beam transport, we can write a map $\mathcal{M}$ which transforms any function of phase space from the beginning of region 2 at $s = 0$ to its end at $s = L$. To second order order in W , $\mathcal{M}$ is given by [4]:

$$\mathcal{M} = \exp(: w_2 :) \exp(: w_1 :) \exp(: -LH_0 :) \dots, \quad (4a)$$

$$w_1 = \int_0^L \exp(: -sH_0 :) (e(s) + c(s)) W ds. \quad (4b)$$

$$w_2 = \frac{1}{2} \int_0^L \int_0^b [\exp(: -aH_0 :) (e(a) + c(a))W, \exp(: -bH_0 :) (e(b) + c(b))W] db da. \quad (4c)$$

We expand the function w_1 in powers of the Lie operator H_0 :

$$w_1 = \sum_{n=0}^{\infty} F_n \frac{(-H_0 :)^n W}{n!}, \quad (5a)$$

$$F_n = \int_0^L (e(s) + c(s)) s^n ds. \quad (5b)$$

The F_n are the n^{th} moments of the total multipole distribution in region 2. We call a

system that sets all F_n to zero for $n \leq m - 1$ a m -parameter quasi-local correction system. We re-emphasize the underlying assumptions behind this approach and contrast it with "lumped" correction. The region 2 in which errors are cancelled is a constant unperturbed Hamiltonian (H_0) region; this is essential if the expansion of equation (5a) is to be valid. We have also implicitly assumed that the form factors $:-H_0 :^n W$ are well-behaved as n increases; this is generally valid where H_0 is either a drift or a bend.

An important advantage of quasi-local correction is that its ability to reduce the multipole distortions is not affected by deviations in the focussing potential $U(s)$. By contrast, lumped correction uses correctors which are far from the corrected multipole content (i.e. separated by one focussing regions) to eliminate a few distortions. Their strengths are dependent on $U(s)$; changes in $U(s)$ can greatly deteriorate the correction. This sensitivity is greatly increased as the length of the beam transport and the number of nontrivial nonlinear effects increases.

In practice $c(s)$ will consist of short elements and in the examples presented below they are represented by zero length correctors of integrated strength C_i at locations s_i :

$$c(s) = \sum_{i=1}^m C_i \delta(s - s_i). \quad (6)$$

All the examples use a simple FODO cell with six sector bends per half cell. We display results for three types of errors in the bends: normal sextupole, normal octupole and normal decapole (b_2 , b_3 , and b_4 respectively). The results are indicative of the type of correction achievable by quasi-local correction.

In the first example, we consider a constant $e(s) = E_0$ in region 2. For m correctors equally spaced from $s = 0$ to $s = L$, the weights C_i are given by the Newton-Cotes [5](NC) integration strengths. For $m = 3$ we obtain the Simpson's

Rule values ($C_1 = C_3 = \frac{-LE_0}{6}$; $C_2 = \frac{-4LE_0}{6}$), as shown in Figure 2. To compare the various configurations, we use a norm for the Lie polynomials w_1 and w_2 of the full cell [6]. The uncorrected configuration has norm one. In table 1, a dramatic improvement is obtained in going from $m = 2$ to $m = 3$. In general, one obtains one extra order of accuracy from symmetry when m is odd and $c(s)$ is constant (or symmetric about $s = L/2$) in a NC geometry. Also, to show the dependence on proper selection of the corrector strengths, we display the results of a three-point equal-weight scheme. Improvement is also obtained in the second order nonlinearities w_2 , which occurs because the methods are quasi-local.

The case $m = 2$ corresponds to placing the correctors near the focussing elements, which has previously been the usual practice. The case $m = 3$ adds a corrector at the center of the transport cell and provide great improvements over previous methods [7, 8, 9].

If the focussing potential $U(s)$ nearly commutes with the potential W , it is possible to use $m - 1$ actual correctors and obtain an m -parameter NC correction by combining the last corrector of one constant H_0 region with the first one of the following region. This can be extended to any distribution of errors and correctors provided that a corrector is very near the focussing region. In practice, W nearly commutes if $U(s)$ represents a sufficiently thin quadrupole.

In the second example [table 2], we consider again a constant $c(s)$ but optimize the locations as well as the strengths of the correctors. In this case the weights C_i and the positions s_i are given by Gaussian Quadrature (GQ) values [5]. Choosing the positions s_i to zero extra moments is not always feasible; however the possibility of optimizing these positions should be considered. For the same m , the GQ method is better in our example than the corresponding NC configuration. This is not a general result; it depends on the nature of the cell and its errors.

In the previous examples, the case $e(s) = E_0$ was used. The method is easily extended to include $e(s)$ varying throughout region 2 with similar improvements in linearity. For example [see figure 3], we consider a region with six independent errors which are corrected by an equally spaced arrangement. The optimal strengths for the correction are:

$$C_1 = \frac{L}{648}(-83e_1 - 41e_2 - 11e_3 + 7e_4 + 13e_5 + 7e_6), \quad (7a)$$

$$C_2 = -\frac{L}{81}(4e_1 + 10e_2 + 13e_3 + 13e_4 + 10e_5 + 4e_6), \quad (7b)$$

$$C_3 = \frac{L}{648}(7e_1 + 13e_2 + 7e_3 - 11e_4 - 41e_5 - 83e_6). \quad (7c)$$

If all e_i are equal, we regain the NC formula. Statistical computation and tracking results confirm the validity of this correction [10].

If $e(s)$ varies from cell to cell, the strengths C_i should also vary from cell-to-cell. However if a GQ-like algorithm is employed, the corrector locations must also vary from cell-to-cell. That may be impractical in a repeating cell structure.

We have outlined an extremely powerful method of quasi-local correction of multipole content in a long transport system. The method uses discrete correctors powered so as to locally cancel the lowest-order moments of that multipole content. In the simplest case of constant multipole fields, the solutions can be expressed in terms of finite-point integration formulae. The full method can provide enormous reduction in all nonlinear effects, and in all orders.

We acknowledge stimulating discussions with J. M. Peterson, P. Channell, R. Talman and A. Chao.

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2. M. Michelotti, in Ref. 1, p.260 .
3. A.J. Dragt and E. Forest, J. Math. Phys. **24**,2734 (1983).
4. The derivation of this result uses a differential equation for the symplectic map $\mathcal{M}$ and the concept of the Dirac representation (ref. 3). See A. Messiah, **Mecanique Quantique**, p.270 (Dunod, 1965) for a familiar quantum mechanical version.
5. Handbook of Mathematical Functions, National Bureau of Standards, Washington, DC, (1972).
6. The norm $\sigma(w_i)$ of w_i , the i^{th} order Lie polynomial in $e(s)$, is computed by transforming w_i into normalized variables and adding the radii of the resonance driving terms:

$$w_i = \sum_{abcd} (A_{abcd}^i \cos(c\phi_x + d\phi_y) + B_{abcd}^i \sin(c\phi_x + d\phi_y)) J_x^{\frac{a}{2}} J_y^{\frac{b}{2}}$$

$$\sigma(w_i) = \sum_{abcd} (A_{abcd}^2 + B_{abcd}^2)^{\frac{1}{2}}$$

This norm is a good figure of merit whenever the system is periodic and equal J_x and J_y are expected.

7. D. Neuffer, Particle Accelerators, Vol. **23**, p. 21, (1988)
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9. In these initial applications (Refs. 4 and 5), correction by more than two orders of magnitude are obtained in the critical non-linearities of trajectory dependent phase shifts, which add coherently from cell to cell.
10. E. Forest and J. M. Peterson, "Correction of Random Multipole Errors with Lumped Correctors", to be published in the European Accelerator Conference proceedings, Rome, (1988).
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Figure Captions

Figure 1: A transport cell with short focussing elements (1 and 3) and long transport regions (2).

Figure 2: Three-point Newton-Cotes-like correction of a constant error E_0 , and two-point Gaussian-Quadrature-like correction.

Figure 3: A transport segment with six independent error elements and three correctors.

Table 1: Newton-Cotes-like correction
of sextupole, octupole and decapole.

corrector strengths	$\sigma(w_1)$			$\sigma(w_2)$			
	m	b_2	b_3	b_4	b_2	b_3	b_4
(1/2,1/2)	2	.54	.68	.83	.62	1.0	***
(1/6,4/6,1/6)	3	.17	.14	.20	.074	.09	***
(1/8,3/8,3/8,1/8)	4	.13	.11	.15	.039	.045	***
Equal weights 3-corrector scheme							
(1/3,1/3,1/3)	2	.35	.40	.50	.26	.38	***

***not available (see ref. 11)

Table 2: Gaussian Quadrature-like correction of sextupole, octupole and decapole.

corrector strenghts	$\sigma(w_1)$			$\sigma(w_2)$			
	m	b_2	b_3	b_4	b_2	b_3	b_4
(1/2,1/2)	4	.0016	.0088	.01	.036	.038	...
(5/18,8/18,5/18)	6	.0088	.008	.0087	.018	.018	...

***not available (see ref. 11)

Figure 1

Figure 2

XBL 886-9662

Figure 3

XBL 886-9679