

27
2-4-80
24cp to NTIS

ORNL/CSD/TM-84

UCC-ND

NUCLEAR
DIVISION



MASTER

Diffusion from Solid Cylinders

C. W. Nestor, Jr.

UNION CARBIDE CORPORATION
200 NORTH ZEEB ROAD
DAYTON, OHIO 45424

DISCLAIMER

This book was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

ORNL/CSD/TM-84

Contract No. W-7405 eng 26

COMPUTER SCIENCES DIVISION

DIFFUSION FROM SOLID CYLINDERS

C. W. Nestor, Jr

Date Published - January 1980

Sponsor: H. W. Godbee
Originator: C. W. Nestor, Jr.

NOTICE This document contains information of a preliminary nature. It is subject to revision or correction and therefore does not represent a final report.

UNION CARBIDE CORPORATION, NUCLEAR DIVISION
operating the
Oak Ridge Gaseous Diffusion Plant Oak Ridge National Laboratory
Oak Ridge Y-12 Plant Paducah Gaseous Diffusion Plant
for the
DEPARTMENT OF ENERGY

zb

CONTENTS

	Page
List of Figures	v
Acknowledgment	vii
Abstract	1
Analysis	3
Convergence Acceleration.	11
Results.	11
References.	17
Appendix	19

LIST OF FIGURES

	Page
Figure 1. Fraction Leached vs Dt/a^2 (log-log plot)	14
Figure 2. Fraction Leached vs Dt/a^2 (linear plot)	15
Figure 3. Fraction Leached vs Square Root of Dt/a^2	16

ACKNOWLEDGMENT

The author would like to thank H. W. Godbee of the ORNL Chemical Technology Division for bringing this problem to his attention and for providing the necessary financial support.

Thanks also are due the secretarial staff of the Computing Applications Department for their assistance in the preparation of this report.

DIFFUSION FROM SOLID CYLINDERS

C. W. Nestor, Jr.

ABSTRACT

The problem considered in this report is the diffusion of material from a solid cylinder initially containing a uniform concentration and immersed in a well-stirred bath which maintains the external concentration at zero. The Fourier-Bessel series form of the fraction of the original material removed from the cylinder as a function of time converges very slowly for small time. We have obtained an alternate form which converges reasonably rapidly for small time and have also used the convergence acceleration method of P. Wynn to provide an efficient method for computation. Numerical examples and program listings are included.

ANALYSIS

The diffusion equation in cylindrical geometry is

$$D \left[\frac{\partial^2 C}{\partial r^2} + \frac{1}{r} \frac{\partial C}{\partial r} + \frac{\partial^2 C}{\partial z^2} \right] = \frac{\partial C}{\partial t}, \quad 0 < r < a, \quad -l < z < l \quad (1)$$

where

C = the concentration of material inside the cylinder,

D = the diffusion coefficient,

a = the radius of the cylinder, and

l = its half-height.

For the problem to be considered in this report, the initial condition is

$$C(r, z, 0) = C_0$$

(a uniform initial concentration) and the boundary conditions are

$$\left. \begin{array}{l} C(a, z, t) = 0 \\ C(r, \pm l, t) = 0 \end{array} \right\} t > 0$$

The amount of material leaving the cylinder per unit time is

$$\int_{-l}^l \left[-D \frac{\partial C}{\partial r} \right]_{a, z, t} 2\pi a dz + 2 \int_0^a \left[-D \frac{\partial C}{\partial z} \right]_{r, l, t} 2\pi r dr,$$

and the fraction of the initial material leaving the cylinder in time t is

$$f(t) = \frac{\int_0^t \left\{ \int_{-l}^l \left[-D \frac{\partial C}{\partial r} \right]_{a, z, \tau} 2\pi a dz + 2 \int_0^a \left[-D \frac{\partial C}{\partial z} \right]_{r, l, \tau} 2\pi r dr \right\} d\tau}{2\pi a^2 l C_0}$$

Taking Laplace transforms¹ $\left[F(s) = \int_0^{\infty} e^{-st} f(t) dt \right]$, we obtain

$$D \left[\frac{\partial^2 \bar{C}}{\partial r^2} + \frac{1}{r} \frac{\partial^2 \bar{C}}{\partial z^2} \right] = s\bar{C} - C_0$$

and²

$$F(s) = \frac{\int_{-l}^l \left[-D \frac{\partial \bar{C}}{\partial r} \right]_{a,z} 2\pi a dz + 2 \int_0^a \left[-D \frac{\partial \bar{C}}{\partial z} \right]_{r,l} 2\pi r dr}{2\pi a^2 l C_0 s}$$

We assume a separable form for \bar{C} :

$$\bar{C}(r,z) = \bar{G}(r) \bar{H}(z)$$

and we can satisfy the boundary conditions by taking

$$\bar{G}(a) = 0,$$

$$\bar{H}(\pm l) = 0.$$

If we substitute

$$\bar{H}(z) = \sum_{n=1}^{\infty} A_n \cos \beta_n z$$

with $\beta_n = \frac{(2n-1)\pi}{2l}$, to satisfy the boundary conditions on the ends, into the partial differential equation for \bar{C} and use the orthogonality property

$$\int_{-l}^l \cos \beta_k z \cos \beta_n z dz = l, \quad k=n, \\ 0, \quad k \neq n$$

we obtain, for the coefficients A_n ,

$$A_n \left[-D \left(\frac{d^2}{dr^2} + \frac{1}{r} \frac{d}{dr} \right) \bar{G}(r) + (s + \beta_n^2 D) \bar{G}(r) \right] = \frac{4C_0}{\pi} \frac{(-1)^{n-1}}{2n-1}$$

The term in brackets must be independent of r . Let

$$\bar{C}(r) = \frac{1}{s + D\beta_n^2} + \bar{Q}(r)$$

with

$$\bar{Q}(a) = \frac{-1}{s + D\beta_n^2}$$

to satisfy the boundary condition at $r = a$; we have

$$\frac{d^2}{dr^2} + \frac{1}{r} \frac{d}{dr} \bar{Q}(r) - \mu^2 \bar{Q}(r) = 0$$

with

$$\mu^2 = \frac{s + D\beta_n^2}{D}$$

A solution of the differential equation for $\bar{Q}(r)$, satisfying the boundary condition at $r = a$, is

$$\bar{Q}(r) = -\frac{1}{s + D\beta_n^2} \frac{I_0(\mu r)}{I_0(\mu a)}$$

where $I_0(z)$ is the modified Bessel function of the first kind.³

The Laplace transform of the concentration profile is

$$\bar{C}(r, z) = \frac{4C_0}{\pi} \sum_{n=1}^{\infty} \frac{(-1)^{n-1}}{2n-1} \frac{1}{s + D\beta_n^2} \left[1 - \frac{I_0(\mu r)}{I_0(\mu a)} \right] \cos \beta_n z$$

and, after inserting this into our expression for $F(s)$, performing all the differentiations and integrations and collecting terms, we have

$$F(s) = \frac{2D}{R^2 s} \sum_{n=1}^{\infty} \frac{1}{s + D\beta_n^2} + \frac{16}{\pi^2} \sum_{n=1}^{\infty} \frac{1}{s + D\beta_n^2} \frac{I_1(\mu a)}{\mu a I_0(\mu a)} \frac{1}{(2n-1)^2}$$

Since³

$$I_0(z) = J_0(iz)$$

the denominator of the Bessel function term will vanish for

$$\mu a = i j_{0m}$$

where j_{0m} is the m -th zero of $J_0(x)$, the Bessel function of the first kind. The singularities of $F(s)$ are then all on the negative real axis:

$$s + D\beta_n^2 = -Dj_{0m}^2/a^2$$

$$s = -D(\beta_n^2 + j_{0m}^2/a^2)$$

and

$$s = -D\beta_n^2$$

Inversion of $F(s)$ by the method of residues¹ leads to the double series form for $f(t)$:

$$f(t) = 1 - \frac{32}{\pi^2} \sum_{m=1}^{\infty} \frac{e^{-Dtj_{0m}^2/a^2}}{j_{0m}^2} \sum_{n=1}^{\infty} \frac{e^{-D\beta_n^2 t}}{(2n-1)^2}$$

For small time, this expression suffers from two serious computational difficulties. Both series converge very slowly for small time, so that a large number of terms must be included to give even modest accuracy; but also the result is very close to 1 and most of the significant figures are lost in the subtraction. An alternative expression can be obtained using the asymptotic expansions of the modified Bessel function^{1,3}

$$I_0(z) \sim \frac{e^z}{\sqrt{2\pi z}} \left[1 + \frac{1}{8z} + \frac{9}{2(8z)^2} + \frac{75}{2(8z)^3} + \dots \right]$$

$$I_1(z) \sim \frac{e^z}{\sqrt{2\pi z}} \left[1 - \frac{3}{8z} - \frac{15}{2(8z)^2} - \frac{105}{2(8z)^3} - \dots \right]$$

$$\frac{I_1(z)}{I_0(z)} \sim 1 - \frac{1}{2z} - \frac{1}{8z^2} - \frac{1}{8z^3} - \dots$$

$$\begin{aligned} \mu a &= \frac{a}{\sqrt{D}} \sqrt{s + \beta^2 D} \\ F(s) &= \sum_{n=1}^{\infty} \frac{1}{s + \beta^2 D} \left\{ \frac{2D}{\ell^2 s} \right. \\ &+ \left. \frac{16}{\pi^2} \left[\frac{\sqrt{D}}{a} \frac{1}{\sqrt{s + \beta^2 D}} - \frac{D}{2a^2} \frac{1}{s + \beta^2 D} - \frac{D^{3/2}}{8a^3} \frac{1}{(s + \beta^2 D)^{3/2}} - \frac{D^2}{8a^4} \frac{1}{(s + \beta^2 D)^2} - \dots \right] \right\} \end{aligned}$$

Using the translation property

$$F(s+a) = L \left\{ e^{-at} f(t) \right\} ,$$

we can invert the series for $F(s)$ term by term to give

$$f(t) = \frac{8}{\pi^2} \sum_{n=1}^{\infty} \frac{1 - e^{-\beta^2 D t}}{(2n-1)^2} +$$

$$\frac{16}{\pi^2} \left[\frac{D}{a} 2 \sqrt{\frac{t}{\pi}} - \frac{D}{2a^2} t - \frac{D^{3/2}}{8a^3} \frac{2t^{3/2}}{3\sqrt{\pi}} - \frac{D^2}{8a^4} \frac{t^2}{2} - \dots \right] \sum_{n=1}^{\infty} \frac{e^{-\beta^2 D t}}{(2n-1)^2}$$

$$f(t) = \frac{8}{\pi^2} \sum_{n=1}^{\infty} \frac{1 - e^{-\beta^2 D t}}{(2n-1)^2} + \frac{8}{\pi^2} \left[\frac{4}{\sqrt{\pi}} \left(\frac{Dt}{a^2} \right)^{1/2} - \left(\frac{Dt}{a^2} \right) - \frac{1}{6\sqrt{\pi}} \left(\frac{Dt}{a^2} \right)^2 \right] \sum_{n=1}^{\infty} \frac{e^{-\beta^2 D t}}{(2n-1)^2}$$

By a similar technique¹ we can obtain two mathematically equivalent forms for the finite slab problem and show that

$$\frac{8}{\pi^2} \sum_{n=1}^{\infty} \frac{1 - e^{-\beta^2 D t}}{(2n-1)^2} = \frac{2}{\sqrt{\pi}} \sqrt{\frac{Dt}{\ell^2}} \left[1 + 2\sqrt{\pi} \sum_{m=1}^{\infty} (-1)^m \operatorname{ierfc} \frac{m\ell}{\sqrt{Dt}} \right]$$

where³

$$\text{ierfc}(x) = \int_x^{\infty} \text{erfc}(t) dt$$

$$\text{erfc}(x) = \frac{2}{\sqrt{\pi}} \int_x^{\infty} e^{-t^2} dt$$

The asymptotic expansion for the integrated complementary error function has a factor of e^{-z^2} , so that the sum of terms is negligible with respect to 1 for small time; we put

$$\frac{8}{\pi^2} \sum_{n=1}^{\infty} \frac{1 - e^{-\beta^2 \frac{Dt}{n}}}{(2n-1)^2} = \frac{2}{\sqrt{\pi}} \sqrt{\frac{Dt}{\ell^2}}$$

and

$$\frac{8}{\pi^2} \sum_{n=1}^{\infty} \frac{e^{-\beta^2 \frac{Dt}{n}}}{(2n-1)^2} = 1 - \frac{2}{\sqrt{\pi}} \sqrt{\frac{Dt}{\ell^2}}$$

so that

$$\begin{aligned} f(t) &= \frac{2}{\sqrt{\pi}} \sqrt{\frac{Dt}{\ell^2}} + \left[1 - \frac{2}{\sqrt{\pi}} \frac{Dt}{\ell^2} \right] \left[\frac{4}{\sqrt{\pi}} \left(\frac{Dt}{a^2} \right)^{1/2} - \frac{Dt}{a^2} - \frac{1}{6\sqrt{\pi}} \left(\frac{Dt}{a^2} \right)^{3/2} - \right. \\ &\quad \left. \frac{1}{8} \left(\frac{Dt}{a^2} \right)^2 - \dots \right] = \left(\frac{Dt}{a^2} \right)^{1/2} \left(\frac{4}{\sqrt{\pi}} + \frac{2}{\sqrt{\pi}} \frac{1}{\ell/a} \right) - \frac{Dt}{a^2} \left(1 + \frac{8}{\pi} \frac{1}{\ell/a} \right) - \left(\frac{Dt}{a^2} \right)^{3/2} \\ &\quad \left(\frac{1}{6\sqrt{\pi}} - \frac{2}{\sqrt{\pi}} \frac{1}{\ell/a} \right) - \left(\frac{Dt}{a^2} \right)^2 \left(\frac{1}{8} - \frac{1}{3\pi} \frac{1}{\ell/a} \right) - \dots \end{aligned}$$

For small values of ℓ/a , a more useful dimensionless parameter is Dt/ℓ^2 ; our expression for $f(t)$ becomes

$$\begin{aligned} f(t) &= \left(\frac{Dt}{\ell^2} \right)^{1/2} \left[\frac{2}{\sqrt{\pi}} + \frac{4}{\sqrt{\pi}} \left(\frac{\ell}{a} \right) \right] - \frac{Dt}{\ell^2} \left[\frac{8}{\pi} \left(\frac{\ell}{a} \right) + \left(\frac{\ell}{a} \right)^2 \right] + \\ &\quad \left(\frac{Dt}{\ell^2} \right)^{3/2} \left[\frac{2}{\sqrt{\pi}} \left(\frac{\ell}{a} \right)^2 - \frac{1}{6\sqrt{\pi}} \left(\frac{\ell}{a} \right)^3 \right] + \left(\frac{Dt}{\ell^2} \right)^2 \left[\frac{1}{3\pi} \left(\frac{\ell}{a} \right)^3 - \frac{1}{8} \left(\frac{\ell}{a} \right)^4 \right] + \dots \end{aligned}$$

which reduces to the "infinite sheet" result for $\ell/a = 0$.

The surface of the cylinder is

$$S = 2\pi a^2 + 2\pi a(2l) ;$$

its volume is

$$V = 2\pi a^2 l$$

so that the surface-to-volume ratio is

$$\frac{S}{V} = \frac{a^2 + 2al}{a^2 l} = \frac{1}{a} \left(2 + \frac{l}{a} \right)$$

The first term in the expansion for $f(t)$ is

$$\left(\frac{Dt}{a^2} \right)^{1/2} \frac{2}{\sqrt{\pi}} \left(2 + \frac{l}{a} \right) = 2 \frac{S}{V} \sqrt{\frac{Dt}{\pi}}$$

the semi-infinite medium result.*

Example

The first four coefficients in the series expansion in $(Dt/a^2)^{1/2}$ are

$$C_1 = \frac{1}{\sqrt{\pi}} \left(4 + \frac{2}{l/a} \right)$$

$$C_2 = - \left(1 + \frac{4}{\pi} \frac{2}{l/a} \right)$$

$$C_3 = \frac{1}{\sqrt{\pi}} \left(\frac{2}{l/a} - \frac{1}{6} \right)$$

$$C_4 = \frac{1}{6\pi} \frac{2}{l/a} - \frac{1}{8}$$

For a cylinder of radius and half-height both 1 cm, the coefficients are

$$C_1 = \frac{6}{\sqrt{\pi}} = 3.38514$$

$$C_2 = - \left(1 + \frac{8}{\pi} \right) = -3.54648$$

$$C_3 = \frac{11}{6\sqrt{\pi}} = 1.03435$$

$$C_4 = \frac{1}{3\pi} - \frac{1}{8} = -0.018897$$

The fraction leached as a function of the dimensionless parameter $\frac{Dt}{a^2}$ is shown in Table I.

Table I. Sample Calculation of $f(t)$

$\frac{Dt}{a^2}$	10^{-6}	10^{-4}	10^{-2}
$f(t)$	$3.382(10^{-3})$	$3.3498(10^{-2})$	0.30408

For $Dt/a^2 = 10^{-2}$, the eleventh term in the j_{om}^2 series is $9.73 (10^{-9})$; the sum of the first eleven terms is 0.196132; the eleventh term in the $(2n-1)^2$ series is $4.05 (10^{-9})$ and the sum is 1.094492; the series result for $f(t)$ is then

$$f(t) = 0.303998$$

Our approximate value obtained from four terms agrees reasonably well. For smaller values of Dt/a^2 , many more terms would be required in evaluating the series. If we require

$$e^{-\beta^2 n^2 Dt} < 10^{-6}$$

or

$$\beta^2 n^2 Dt > 16.1,$$

then, for $\frac{Dt}{a^2} = 10^{-4}$ and $l/a = 1$,

$$(2n-1)^2 \frac{\pi^2}{4} > 16.1(10^4)$$

$$n > 128$$

so of the order of 120 to 130 terms would be needed to attain reasonable accuracy in the series form.

CONVERGENCE ACCELERATION

For moderate values of time where the error after the first few terms of the expansion in $(Dt/a^2)^{1/2}$ would be unacceptably large, the convergence of the Fourier-Bessel series form can be considerably accelerated by the use of a scheme studied by (among others) P. Wynn.⁵ The method is to determine a rational function in $1/n$ to match the partial sums of the series, and to extrapolate the rational function to $1/n = 0$. A portion of the calculation for the $(2n-1)^2$ series is shown in Table II, using a value of $Dt/l^2 = 10^{-4}$. We have

$$\frac{l}{\sqrt{Dt}} = 100$$

so the additional terms involving integrated complementary error functions are negligible, and the value of the sum, correct to six significant figures, is 1.21978. Extrapolating as far as possible after nine terms in the sum gives 1.21822. The successive columns of the table are generated by the "rhombus rule"

$$t_j^k = t_{j+1}^{k-2} + 1 / \left(t_{j+1}^{k-1} - t_j^{k-1} \right) ,$$

and a convenient FORTRAN subroutine for generating successive upward-sloping diagonals of the table is given in the Appendix. (Subroutine EXTRAP.)

RESULTS

Sample calculations for cylinders of various sizes with a wide range of diffusion coefficients have been done with the computer program and subroutines listed in the Appendix. The results are shown in Figs. 1, 2, and 3 and tabulated in Table III.

Table III. Fraction Leached from Finite Cylinders

Dt/a^2	$l/a = 0.3$	$l/a = 0.5$	$l/a = 1.0$	$l/a = 3.0$	$l/a = 5.0$
.0003	.101408	.076360	.057574	.045045	.042545
.001	.180772	.136705	.103534	.081419	.076790
.003	.301748	.229279	.174942	.138664	.131416
.01	.510551	.392523	.303998	.244982	.233120
.02	.670959	.522430	.410497	.335875	.320950
.03	.771965	.610018	.484897	.401478	.384795
.04	.840159	.676009	.542837	.454011	.436245
.05	.887240	.728300	.590358	.498200	.479768
.06	.920116	.770865	.630548	.536468	.517652
.07	.943235	.806055	.665235	.570251	.551254
.08	.959574	.835428	.695608	.600484	.581459
.09	.971162	.860099	.722490	.627813	.608878
.10	.979401	.880912	.746475	.652708	.633954
.12	.989462	.913467	.787452	.696527	.678341
.15	.996127	.946170	.835666	.750653	.733647
.20	.999266	.975470	.891964	.818792	.804134
.25	.999861	.988796	.928648	.867662	.855401
.30	.999973	.994879	.952804	.903111	.893055
.40	.999999	.998930	.979326	.947847	.941336
.50	1.000000	.999776	.990941	.971829	.967746

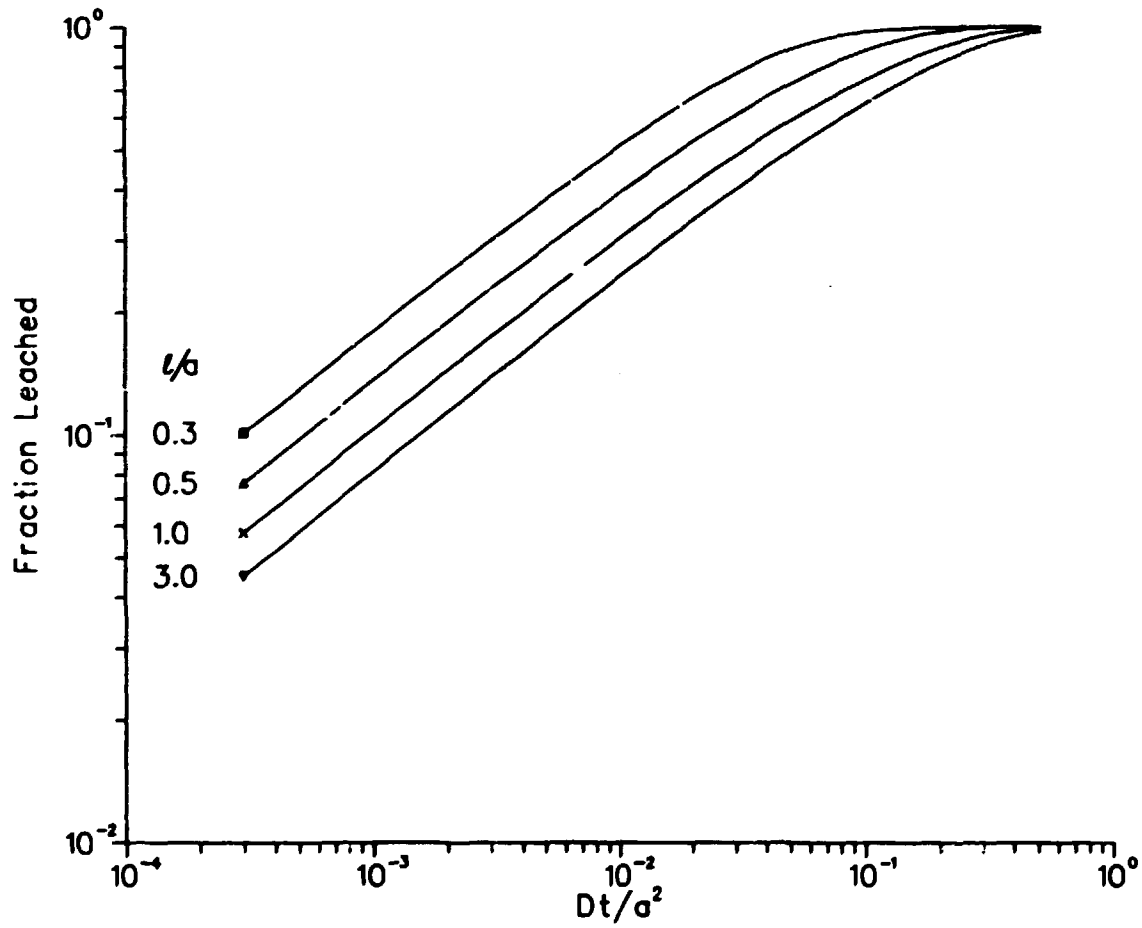


Figure 1. Fraction Leached vs Dt/a^2 (log-log plot)

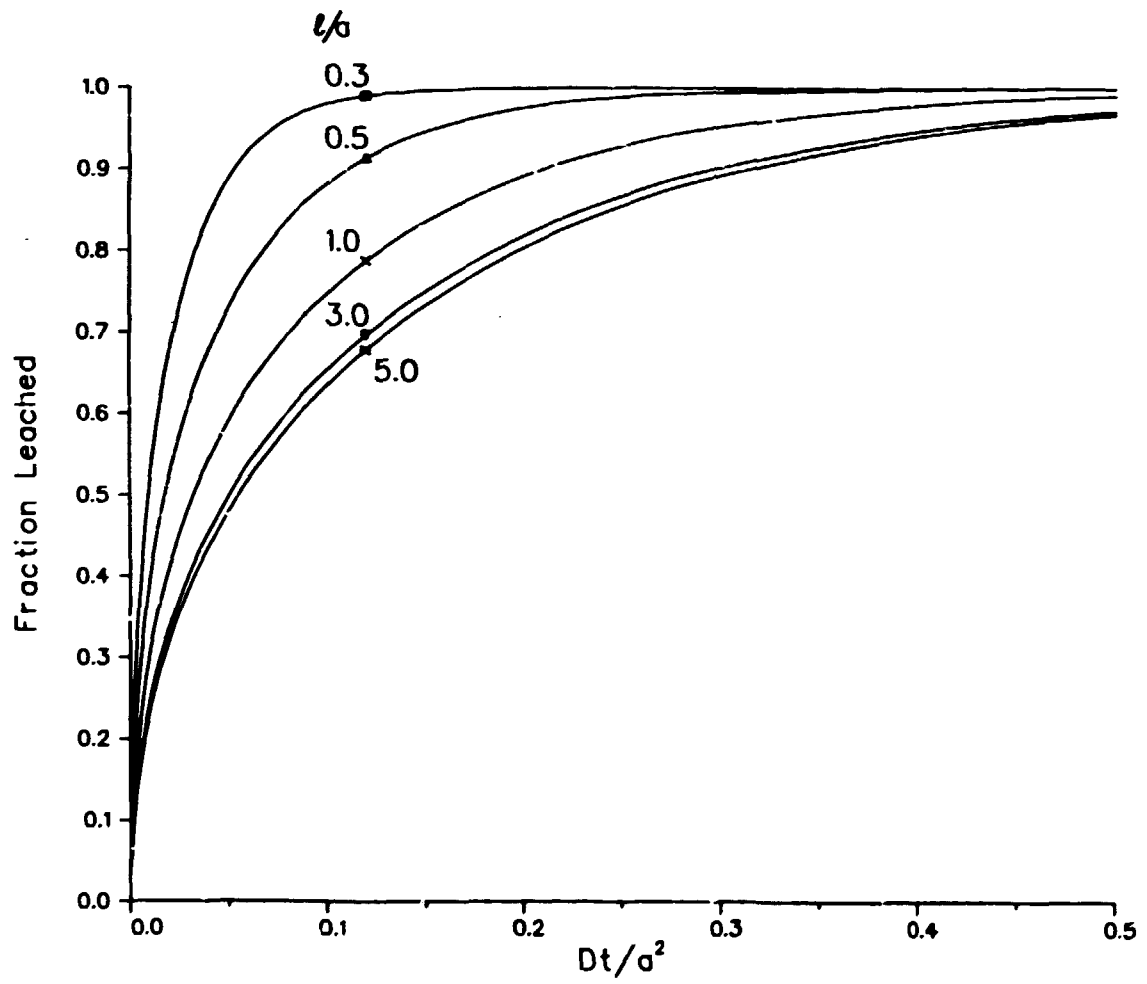


Figure 2. Fraction Leached vs Dt/a^2 (linear plot)

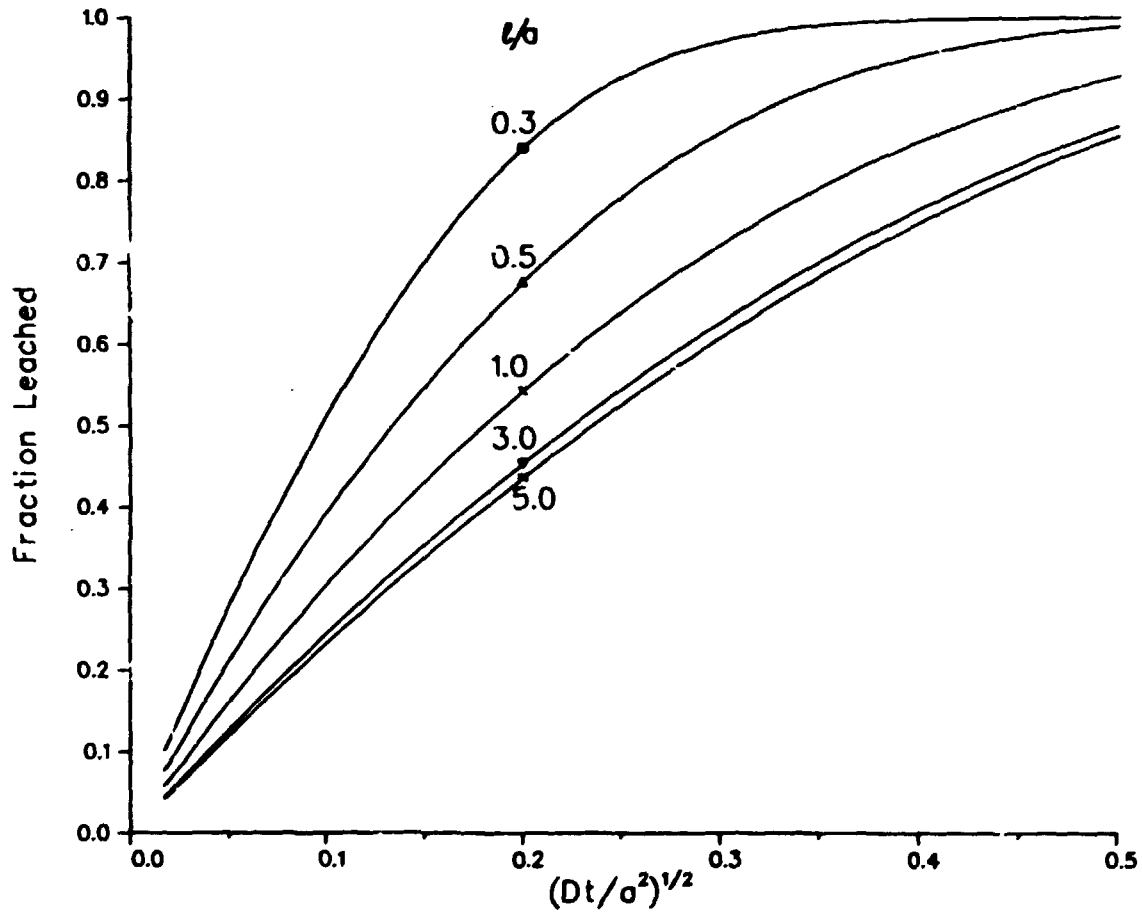


Figure 3. Fraction Leached vs Square Root of Dt/a^2

REFERENCES

1. H. S. Carslaw and J. C. Jaeger, *Operational Methods in Applied Mathematics*, Second Edition, Oxford, 1948.
2. G. E. Lee-Whiting, *One-Dimensional Diffusion with Time-Dependent Boundary Conditions and Diffusion Coefficient*, AECL-4374, January 1973.
3. M. Abramowitz and I. A. Stegun, eds., *Handbook of Mathematical Functions*, National Bureau of Standards, Applied Mathematics Series 55, June 1964, Chapt. 9.
4. H. W. Godbee and D. S. Joy, *Assessment of the Loss of Radioactive Isotopes from Waste Solids to the Environment. Part I: Background and Theory*, ORNL/TM-4333, February 1974.
5. See, for example, J. F. Hart et al., *Computer Approximations*, John Wiley and Sons, New York, 1968, p. 38.

APPENDIX**Computer Program and Subroutines**

The computer program listed was used to generate the results shown in Table III and to produce the graphs shown in Figs. 1, 2, and 3. The subroutines called by the main program, except for FCALC and INOMP, are contained in the computer graphics package DISSPLA*. The total time required to compile, load, and execute the program was 1.2 minutes on the IBM 360/75; 7 seconds on the 360/91.

* A proprietary software product of Integrated Software Systems Corporation, San Diego, California.

C
C
C

F PLOT.FOR (29 JAN. 1979)

```

REAL*8 DTOASQ(20), XLOA(5), FL(20,5)
REAL*4 XP(20), YP(20)
DATA DTOASQ /3.D-4, 1.D-3, 3.D-3, 1.D-2, 2.D-2, 3.D-2, 4.D-2,
1 5.D-2, 6.D-2, 7.D-2, 8.D-2, .1D0, .12D0, .15D0, .2D0, .25D0,
2 .3D0, .4D0, .5D0, 0.D0/
DATA XLOA / 3D0, 5D0, 1.D0, 3.D0, 5.D0/
DATA NDT /19/
DO 95 N=1,NDT
  XP(N) = DTOASQ(N)
95 CONTINUE
  CALL FCALC (DTOASQ, NDT, XLOA, 5, FL, 20)
  WRITE (6, 1) (XLOA(K), K=1,5)
1  FORMAT (1H1, 20X, 'FRACTION LEACHED FROM FINITE CYLINDERS'/
2 1H0, 18X, 5(3X, 'L/A =', F4.1, 2X)/
2 1H0, 10X, 'DT/A**2'/1X)
  DO 97 N=1,NDT
    WRITE (6, 2) DTOASQ(N), (FL(N,K), K=1,5)
2  FORMAT (10X, 1PE8.1, 5E14.5)
    IF (MOD (N, 5) .EQ. 0) WRITE (6, 3)
3  FORMAT (1X)
97 CONTINUE
  WRITE (6, 4)
4  FORMAT (1H1)
  CALL INCMP
  CALL PSPLIN
  CALL SIMPLX
  CALL YAXANG (0.)
  CALL TITLE (0, 0, 'D&T/A/EH.6&2$', 100, 'F&RACTION *L&EACHED$',
1 100, 10., 8.)
  CALL LOGLOG (1.E-4, 2.5, .01, 4.)
  CALL MSHIFT (0.1, -0.1)
  CALL RLMESS ('1A.5M5&L/1MXA-.5&A$', 100, 1.2E-4, .15)
  DO 105 K=1,4
    DO 100 N=1,NDT
      YP(N) = FL(N,K)
100 CONTINUE
      CALL CURVE (XP, YP, 1, 1)
      CALL RLREAL (XLOA(K), 1, 1.E-4, YP(1))
      CALL CURVE (XP, YP, NDT, 0)
105 CONTINUE
  CALL ENDPL (1)

```

```

CALL RETITL
CALL XTICKS (2)
CALL GRAF (0., .1, .5, 0., .1, 1.)
CALL MSHIFT (-0.6, 0.1)
CALL RLMESS ('!A.5M5&L/!MXA-.5&A$', 100, .12, 1.05)
DO 115 K=1,5
  IF (K .EQ. 5) CALL MSHIFT (-0.1, -0.3)
  MKNO = K + K - 2
  CALL MARKER (MKNO)
  DO 110 N=1,NDT
    YP(N) = FL(N,K)
110  CONTINUE
    CALL CURVE (XP(13), YP(13), 1, 1)
    CALL RLREAL (XLOA(K), 1, XP(13), YP(13))
    CALL CURVE (XP, YP, NDT, 0)
115  CONTINUE
    CALL RESET ('MSHIFT')
    CALL ENDPL (2)
    CALL TITLE (0, 0, '(*D&T/A!E!L.6&2!EXHX&)!EH.6&1/2$', 100,
      ' *F&REACTION *L&EACHED$', 100, 10., 8.)
    CALL XTICKS (2)
    CALL GRAF (0., .1, .5, 0., .1, 1.)
    NKP = 0
    DO 130 N=1,NDT
      TEST = DSQRT (DIOASQ(N))
      IF (TEST .GT. 0.5) GO TO 130
      NKP = NKP + 1
      XP(NKP) = TEST
C
130  CONTINUE
    CALL MSHIFT (-0.5, 0.15)
    CALL RLMESS ('!A.5M5&L/!MXA-.5&A$', 100, XP(7) + .01, .95)
    DO 140 K=1,5
      MKNO = K + K - 2
      CALL MARKER (MKNO)
      DO 135 N=1,NDT
        YP(N) = FL(N,K)
135  CONTINUE
        CALL CURVE (XP(7), YP(7), 1, 1)
        IF (K .EQ. 5) CALL MSHIFT (-0.3, -0.3)
        CALL RLREAL (XLOA(K), 1, XP(7), YP(7))
        CALL CURVE (XP, YP, NKP, 0)
140  CONTINUE
    CALL ENDPL (3)
    CALL DONEPL
    STOP
    END

```



```

SUBROUTINE FCALC (DTOASQ, NDT, XLOA, NXL, FRAC, IPD)
IMPLICIT REAL*8 (A-H, O-Z)
DIMENSION DTOASQ(1), XLOA(1), FRAC(IPD, 1)
DATA RSRP /1.564189583548DO/
DATA FOROP /1.2732395447DO/, SMAX /1.E-4/
DATA R6PI /5.3051647697D-2/
DO 105 K=1,NXL
  TQ = 2.DO/XLOA(K)
  C1 = RSRP*(4.DC + TQ)
  C2 = -.DO - FOROP*TQ
  C3 = RSRP*(TQ - .166666665667DO)
  C4 = R6PI*TQ - .125DO
  DO 100 N=1,NDT
    PSQ = DTOASQ(N)
    P = DSQRT (PSQ)
    SMT = DABS(C4*PSQ)
    IF (SMT .LE. SMAX) FRAC(N,K) = (((C4*P + C3)*P + C2)*P + C1)*P
    IF (SMT .GT. SMAX) CALL SERSUM (PSQ, XLOA(K), FRAC(N,K))
100  CONTINUE
105  CONTINUE
RETURN
END
SUBROUTINE SERSUM (A, B, ANS)
IMPLICIT REAL*8 (A-H, O-Z)
DIMENSION U(31), V(30)
DATA CONST /3.242277876DG/, PIO2 /1.5707963268DO/
EXTERNAL ATERM, BTERM
CALL EXTRAP (A, ATERM, 15, 1.D-8, U, V, ASUM, INDA)
IF (INDA .NE. 0) WRITE (6, 1)
1  FORMAT ('0A SERIES NOT CONVERGED')
BT1 = A*(PIO2/B)**2
CALL EXTRAP (BT1, BTERM, 15, 1.D-8, U, V, BSUM, INDB)
IF (INDB .NE. 0) WRITE (6, 2)
2  FORMAT ('0B SERIES NOT CONVERGED')
ANS = 1.DO - CONST*ASUM*BSUM
RETURN
END

```

C
C
C

ATERM.FOR (30 AUGUST 1978)

```

FUNCTION ATERM (N, A)
IMPLICIT REAL*8 (A-H, O-Z)
DIMENSION XJZT(20)
DATA XJZT /
1 2.4048255577D0, 5.5202781103D0, 8.6537279129D0,
2 11.7915344391D0, 14.9309177086D0, 18.0710639679D0,
3 21.2116366299D0, 24.3524715308D0, 27.4934791320D0,
4 30.6346064684D0, 33.7758202135D0, 36.9170983537D0,
5 40.0584257646D0, 43.1997917132D0, 46.3411883717D0,
6 49.4826090974D0, 52.6240518411D0, 55.7655107550D0,
7 58.9069839261D0, 62.0484691902D0/
IF (N .LE. 20) XJZ = XJZT(N)
IF (N .GT. 20) XJZ = XJZM(N)
ANS = 0.D0
ARG = A*(XJZ**2)
IF (ARG .LT. 170.D0) ANS = DEXP(-ARG)/(XJZ**2)
ATERM = ANS
RETURN
END
FUNCTION XJZM(N)
IMPLICIT REAL*8 (A-H, O-Z)
DATA PI /3.14159265359D0/
ATEB = PI*DFLOAT(8*N - 2)
R8BT = 1.D0/ATEB
T = R8BT**2
XJZM = .125D0*ATEB + ((6046.4D0*T - 31.D0)*T**4.D0/3.D0 + 1.D0)
1 *R8BT
RETURN
END

```

C
C
C

BTERM.FOR (30 AUGUST 1978)

```

FUNCTION BTERM (N, B)
IMPLICIT REAL*8 (A-H, O-Z)
ODDSQ = DFLOAT ((N + N - 1)**2)
ANS = 0.D0
ARG = ODDSQ*B
IF (ARG .LE. 170.D0) ANS = DEXP(-ARG)/ODDSQ
BTERM = ANS
RETURN
END

```

```

C
C      EXTRAP.FOR (30 NOV. 1978)
C
C      SUBROUTINE EXTRAP (T, TRAT, NMAX, EPS, U, V, ANS, IND)
C
C      P. WYNN'S EPSILON ALGORITHM (SEE HART ET AL.,
C      "COMPUTER APPROXIMATIONS", WILEY, NEW YORK, 1968, PG. 38.)
C
C      IMPLICIT REAL*8 (A-H, O-Z)
C      EXTERNAL TRAT
C
C      THE FUNCTION TRAT (N, T) COMPUTES THE N-TH TERM OF THE
C      SERIES TO BE SUMMED:
C
C      INF
C
C      SUM F (T)
C          N
C      N=1
C
C      DIMENSION U(2), V(2)
C
C      THE ARRAYS U AND V MUST BE DIMENSIONED IN THE CALLING
C      PROGRAM WITH AT LEAST 2*NMAX AND 2*NMAX + 1
C      ELEMENTS, RESPECTIVELY. THEY WILL CONTAIN SUCCESSIVE
C      UPWARD-SLOPING DIAGONALS OF THE 'ADE' TABLE.
C
C      NMAX IS HALF THE MAXIMUM NUMBER OF TERMS,
C      ANS IS THE ESTIMATE OF THE SUM, AND
C      IND IS RETURNED AS ZERO IF THE EXTRAPOLATION CONVERGED,
C      WITH A RELATIVE ERROR OF EPS, BUT IS RETURNED AS -1
C      OTHERWISE.
C
C      IND = 0
C      TEMP = TRAT (1, T)
C      U(1) = TEMP
C      IF (DABS(TEMP) .LE. EPS) GO TO 120
C      NV = 0
C      NU = 1
C      NN = 2

```

```

DO 115 N=1,NMAX
  TNEW = TRAT (NN, T)
  V(1) = U(1) + TNEW
  TEMP = V(1)
  IF (DABS(TNEW/TEMP) .LT. EPS) GO TO 120
  V(2) = 1.DO/TNEW
  NN = NV + 1
  IF (NV .LT. 1) GO TO 105
  IQ = 1
  DO 100 KV=1,NV
    V(KV+2) = U(KV) + 1.DO/(V(KV+1) - U(KV+1))
    IF (IQ .EQ. 0) GO TO 100
    TEMP = V(KV+2)
    IF (DABS (V(KV)/TEMP - 1.DO) .LT. EPS) GO TO 120
C
100   IQ = 1 - IQ
C
105   TNEW = TRAT(NN, T)
      U(1) = V(1) + TNEW
      TEMP = U(1)
      IF (DABS(TNEW/TEMP) .LT. EPS) GO TO 120
      U(2) = 1.DO/TNEW
      NN = NN + 1
      IQ = 1
      DO 110 KU=1,NU
        U(KU+2) = V(KU) + 1.DO/(U(KU+1) - V(KU+1))
        IF (IQ .EQ. 0) GO TO 110
        TEMP = U(KU+2)
        IF (DABS (U(KU)/TEMP - 1.DO) .LT. EPS) GO TO 120
C
110   IQ = 1 - IQ
      NV = NU + 1
      NU = NV + 1
C
115   CONTINUE
      IND = -1
C
120   ANS = TEMP
      RETURN
      END

```

```
C
C      INCMP.FOR (15 DEC. 1978)
C
C      SUBROUTINE INCMP
C
C      INITIALIZES DISSPLA FOR 14 BY 11 INCH PLOTS IN
C      A COMPRESSED DATA SET
C
C      CALL COMPRS
C      CALL BGMPL (1)
C      CALL PAGE (14., 11.)
C      CALL HEIGHT (0.2)
C      CALL MX1ALF ('L/CSTD', '&')
C      CALL MX2ALF ('STANDA', '*')
C      CALL MX3ALF ('INSTRU', '!')
C      RETURN
C      END
```