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Physics Division

ATOMIC DATA FOR FUSION - VOLUME VI  
SPECTROSCOPIC DATA FOR TITANIUM, CHROMIUM, AND NICKEL  
Volume 2. Chromium

W. L. Wiese and A. Musgrove  
National Institute for Standards and Technology

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### Series Preface

The primary objective of the Controlled Fusion Atomic Data Center at Oak Ridge National Laboratory is to publish handbooks containing numerical and graphical cross sections and other physical data relevant to fusion energy research. In 1977, a two-volume compilation was published as ORNL reports ORNL-5206 and ORNL-5207. Since that time, a large volume of pertinent data has become available, necessitating an update of the previous compilation. Plans are to include both cross sections and rate coefficients for collisional processes, and to publish the revised series in handbook form. The specific volumes which are in preparation are listed below, with their expected completion dates.

- Vol. 1, "Collisions of H, H<sub>2</sub>, He, and Li Atoms and Ions with Atoms and Molecules," C. F. Barnett, ORNL (December 1989).
- Vol. 2, "Collisions of Electrons with Atoms and Molecules," J. W. Gallagher, National Institute of Standards and Technology; and D. C. Gregory, ORNL (December 1990).
- Vol. 3, "Particle Interactions with Surfaces," E. W. Thomas, Georgia Institute of Technology (January 1985).
- Vol. 4, "Spectroscopic Data for Iron," W. L. Wiese, National Bureau of Standards (March 1985).
- Vol. 5, "Collisions of Carbon and Oxygen Ions with Electrons, H, H<sub>2</sub>, and He," R. A. Phaneuf, ORNL; R. K. Janev, Institute of Physics, Yugoslavia; and M. S. Pindzola, Auburn University (January 1987).
- Vol. 6, "Spectroscopic Data for Titanium, Chromium, and Nickel," W. L. Wiese and A. Musgrove, National Institute for Standards and Technology (September 1989).

C. F. Barnett  
D. C. Gregory  
H. T. Hunter  
M. I. Kirkpatrick  
R. A. Phaneuf

### **Abstract**

Comprehensive spectroscopic data tables are presented for all ionization stages of titanium, chromium, and nickel. Tables of ionization potentials, spectral lines, energy levels, and transition probabilities are presented. These tables contain data which have been excerpted from general critical compilations prepared under the sponsorship of the National Standard Reference Data System (NSRDS).

# Spectroscopic Data for Titanium, Chromium, and Nickel – Volume 2. Chromium

W. L. Wiese and A. Musgrove, Editors

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## General Introduction

This compendium contains a collection of recent spectroscopic data tables for titanium, chromium, and nickel. The tables are issued in three separate volumes, each containing one element. The individual volumes are identified as Oak Ridge National Laboratory ORNL 6551/V1 (titanium); ORNL 6551/V2 (chromium); and ORNL 6551/V3 (nickel). These chemical elements, together with the earlier tabulated<sup>1</sup> element iron, are the principal heavy metals which are widely used as first-wall materials (including limiters, armor plates, etc.) of magnetic fusion research machines, particularly tokamaks. Spectral radiation data for both high and low stages of ionization for Ti, Cr and Ni have thus become important for the assessment and modeling of the effects of impurities on plasma properties and power balance, for the study of plasma-wall interactions as well as for the application of plasma diagnostic techniques.

Numerical data are tabulated for those spectroscopic quantities which are of principal importance for such plasma studies and for plasma diagnostics. The specific spectroscopic quantities are ionization energies, wavelengths of allowed and forbidden lines, atomic energy levels, and atomic transition probabilities. Most of the critical evaluation and compilation work for these data has been done at the National Institute of Standards and Technology, formerly the National Bureau of Standards. The tables are usually parts of larger tabulations<sup>2-7</sup> containing many other chemical elements besides Ti, Cr, and Ni. Excerpting the data from these larger compilations required some modifications in the reprinted material, especially the modification of the introductory remarks with comments and explanations that specifically refer to the Ti, Cr, and Ni spectra. All of the material is quite recent, and is under the sponsorship of the National Standard Reference Data System (NSRDS). Since the various data tables have been completed at different times, there may be occasional slight inconsistencies between overlapping material when the data are based on different sources. Also, sometimes there may be different judgments of independent evaluators on the quality of the source material. For example, wavelengths which are derived from atomic energy levels may be sometimes slightly different from the observed data in the wave-

length tables. There also may be slight inconsistencies between the energy level data contained in the wavelength and transition probability tables when compared to the data in the energy level table itself. But any such differences are so small that they do not matter for any plasma applications, and therefore the use of any of the recent tabulations is appropriate. But we generally recommend to use the *primary* tables to obtain data on a specific atomic quantity.

Each of the three volumes of this compendium is divided into six sections which cover:

Ionization energies,  
General spectral line lists,  
Vacuum ultraviolet lines,  
Magnetic dipole lines,  
Atomic energy levels, and  
Atomic transition probabilities.

The editors gratefully acknowledge the cooperation of the data compilers. We also thank NSRDS, the American Institute of Physics, and American Chemical Society for permission to reprint excerpts of these tables.

## References

1. W. L. Wiese, Editor, *Spectroscopic Data for Iron*, ORNL-6089 [1985], Fourth Volume of Oak Ridge Natl. Lab. Series 6086.
2. J. Reader, C. H. Corliss, W. L. Wiese, and G. A. Martin, *Wavelengths and Transition Probabilities for Atoms and Atomic Ions*, Natl. Stand. Ref. Data Ser., Natl. Bur. Stand. (U.S.), 68, 415 pgs. [1980].
3. R. L. Kelly, *Atomic and Ionic Spectral Lines Below 2000 Å (H through Kr)*, *J. Phys. Chem. Ref. Data* 16, Suppl. 1 (1987).
4. J. Sugar and C. Corliss, *Atomic Energy Levels of the Iron-Period Elements: Potassium through Nickel*, *J. Phys. Chem. Ref. Data* 14, Suppl. 2 [1985].
5. V. Kaufman and J. Sugar, *Forbidden Lines in  $ns^2np^3$  Ground Configurations and  $nsnp$  Excitation Configurations of Be through Mo Atoms and Ions*, *J. Phys. Chem. Ref. Data* 15, 321-350 [1986].
6. G. A. Martin, J. R. Fuhr, and W. L. Wiese, *Atomic Transition Probabilities—Scandium through Manganese*, *J. Phys. Chem. Ref. Data* 17, Suppl. 3 [1988].
7. J. R. Fuhr, G. A. Martin, and W. L. Wiese, *Atomic Transition Probabilities—Iron through Nickel*, *J. Phys. Chem. Ref. Data* 17, Suppl. 4 [1988].

**A. Ionization Energies of Chromium Ions**



## A. Ionization Energies of Chromium Ions

[Excerpted from: J. Sugar and C. Corliss, J. Phys. Chem. Ref. Data 14, Suppl. 2 (1985)]

Spectrum	Ground State Configuration	Ground Level	Ionization Energy (eV)
Cr I	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^5 4s$	$^7S_3$	6.76669
Cr II	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^5$	$^6S_{5/2}$	16.4858
Cr III	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^4$	$^5D_0$	30.96
Cr IV	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^3$	$^4F_{3/2}$	49.16
Cr V	$1s^2 2s^2 2p^6 3s^2 3p^6 3d^2$	$^3F_2$	69.46
Cr VI	$1s^2 2s^2 2p^6 3s^2 3p^6 3d$	$^3D_{3/2}$	90.6356
Cr VII	$1s^2 2s^2 2p^6 3s^2 3p^6$	$^1S_0$	160.18
Cr VIII	$1s^2 2s^2 2p^6 3s^2 3p^5$	$^3P_{3/2}$	184.7
Cr IX	$1s^2 2s^2 2p^6 3s^2 3p^4$	$^3P_2$	209.3
Cr X	$1s^2 2s^2 2p^6 3s^2 3p^3$	$^4S_{3/2}$	244.4
Cr XI	$1s^2 2s^2 2p^6 3s^2 3p^2$	$^3P_0$	270.8
Cr XII	$1s^2 2s^2 2p^6 3s^2 3p$	$^3P_{1,2}$	298.0
Cr XIII	$1s^2 2s^2 2p^6 3s^2$	$^1S_0$	354.8
Cr XIV	$1s^2 2s^2 2p^6 3s$	$^2S_{1/2}$	384.171
Cr XV	$1s^2 2s^2 2p^6$	$^1S_0$	1010.6
Cr XVI	$1s^2 2s^2 2p^5$	$^3P_{3/2}^o$	1097
Cr XVII	$1s^2 2s^2 2p^4$	$^3P_2$	1185
Cr XVIII	$1s^2 2s^2 2p^3$	$^4S_{3/2}^o$	1299
Cr XIX	$1s^2 2s^2 2p^2$	$^3P_0$	1396
Cr XX	$1s^2 2s^2 2p$	$^3P_{1/2}^o$	1496
Cr XXI	$1s^2 2s^2$	$^1S_0$	1634
Cr XXII	$1s^2 2s$	$^2S_{1/2}$	1721.4
Cr XXIII	$1s^2$	$^1S_0$	7481.8
Cr XXIV	$1s$	$^2S_{1/2}$	7894.87

**B. Prominent Spectral Lines for Cr I to Cr V  
(Wavelengths for Vacuum Ultraviolet to Near Infrared Regions)**

## B. Prominent Spectral Lines for Cr I to Cr V (Vacuum Ultraviolet to Near Infrared Regions)

[Excerpted from: J. Reader, C. H. Corliss, W. L. Wiese, and G. A. Martin, Natl. Stand. Ref. Data Ser., Natl. Bur. Stand. (U.S.) 68, 415 pgs. (1980); and J. Reader and C. H. Corliss, in *Handbook of Chemistry and Physics*, 70th Edition (1989)]

These lists were recently prepared under the auspices of the Committee of Line Spectra of the Elements of the National Academy of Sciences—National Research Council as part of a general wavelength table<sup>1,2</sup>. The tables contain the outstanding spectral lines,—from the far ultraviolet to the far infrared,—of neutral (I), singly ionized (II), doubly ionized (III), triply ionized (IV), and quadruply ionized (V) chromium atoms. The lines are selected from larger lists (see references) in such a way as to include the stronger observed lines in each spectral region.

The data were compiled by Charles H. Corliss, NBS (Cr I—Cr V). For Cr I and II, the following literature references were used as the principal sources of data:

W. F. Meggers, C. H. Corliss, and B. F. Scribner, Nat. Bur. Stand. (U.S.), Monogr. 145, Washington, D.C. (1975).

For Cr III, IV and V, the following references were used:

F. L. Moore, Thesis, Princeton University (1949).  
J. O. Ekberg, Phys. Scr. 7, 55 (1973).  
J. O. Ekberg, Phys. Scr. 7, 59 (1973).

All wavelengths are given in Angstrom units (Å). Below 2000 Å, the wavelengths are in vacuum; above 2000 Å,

the wavelengths are in air. Wavelengths given to three decimal places have an uncertainty of less than 0.001 Å and are, therefore, suitable for the calibration of most spectrometers. The line intensities are normally estimates of the relative strengths of lines which are not greatly separated in wavelength. However, because different sources are involved, based on different scales for the intensity estimates, these intensities are only useful as a rough indication of the appearances of the spectra. Furthermore, in the tables of first and second spectra the intensities of the lines of the singly ionized atoms relative to those of the neutral atom should be used with caution, inasmuch as the concentration of the ions in the light source depends greatly on the excitation conditions.

The descriptive symbols used in the tables have the following meaning:

H — hazy  
D — line consists of two unresolved lines

### References

1. J. Reader, C. H. Corliss, W. L. Wiese, and G. A. Martin, *Wavelengths and Transition Probabilities for Atoms and Atomic Ions*, Natl. Stand. Ref. Data Ser., Natl. Bur. Stand. (U.S.), 68, 415 pgs. (1980).
2. J. Reader and C. H. Corliss, in *Handbook of Chemistry and Physics*, 70th Edition (R. C. Weast, Ed.), CRC Press, Inc., Boca Raton, FL (1989).

## Chromium (Cr)

Z = 24

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
	Cr I and II		440	2666.02	II
	Air		280	2668.71	II
			350	2671.81	II
			280	2672.83	II
19000	2055.52	II	1800	2677.16	II
14000	2061.49	II	35	2678.16	I
8900	2065.42	II	320	2678.79	II
80	H 2364.71	I	18	2680.34	II
130	2383.33	I	230	2687.09	II
140	2408.62	I	60	2688.04	I
170	2496.31	I	55	2688.29	II
110	2502.53	I	26	2690.26	I
190	2504.31	I	280	2691.04	II
50	2508.11	I	35	2693.52	II
60	2508.98	I	35	2697.91	II
40	2513.62	I	180	2698.41	II
110	2516.92	I	180	2698.69	II
80	2518.71	I	18	2700.60	I
390	2519.52	I	110	2701.99	I
190	2527.12	I	18	2702.53	I
40	2530.45	I	70	2703.48	I
70	2534.34	II		2703.55	II
50	2545.64	I	35	2703.86	II
160	2549.54	I	18	2705.43	I
40	2553.06	I	60	2708.79	II
80	2557.15	I	35	2709.31	II
130	2560.69	I	140	2712.31	II
150	2571.74	I	45	2716.18	I
100	2577.65	I	55	2717.51	II
50	2588.20	I	45	2718.43	II
380	2591.85	I	170	2722.75	II
35	2603.57	I	18	2724.04	II
35	2622.86	I	420	H 2726.51	I
22	2625.32	I	45	2727.26	II
18	2626.60	I	280	H 2731.91	I
18	2629.82	I	170	H 2736.47	I
35	2642.12	I	70	2739.38	I
250	2653.59	II	70	2740.10	II
250	2658.59	II	95	2741.07	I
70	2661.73	II	95	2742.03	II
320	2663.42	II	95	2742.17	I
70	2663.68	II	250	2743.64	II

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
35	2746.21	H	45	2849.29	I
110	2748.29	H	1200	2849.84	H
330	2748.98	H	120	2851.36	H
390	2750.73	H	55	2853.22	H
45	2751.60	H	55	2855.07	H
280	2751.87	H	880	2855.68	H
110	2752.88	H	90	2856.77	H
35	2754.28	H	70	2857.40	H
22	2754.90	H	610	2858.91	H
22	2755.27	H	440	2860.93	H
22	2756.75	H	790	2862.57	H
150	2757.10	H	750	2865.11	H
350	2757.72	H	55	2865.33	H
60	2758.98	H	610	2866.74	H
80	2759.39	H	90	2867.10	H
45	2759.73	H	480	2867.65	H
90	2761.70	H	210	2877.44	H
750	2762.59	H	110	2871.63	H
22	2763.06	H	160	2873.48	H
80	2764.35	H	90	2873.82	H
750	2766.54	H	320	2875.99	H
22	2767.54	H	230	2876.24	H
250	2769.92	H	180	2877.98	H
18	2771.45	H	70	2878.45	H
45	2778.06	H	120	2879.27	H
22	2779.14	H	95	2880.87	H
80	2780.30	H	30	2881.14	H
610	2780.70	H	170	2887.00	H
70	2785.70	H	55	2888.74	H
35	2787.63	H	700	2889.29	H
35	2787.84	H	55	2889.82	H
90	2792.16	H	55	2891.42	H
55	2798.67	H	370	2893.25	H
70	2800.77	H	190	2894.17	H
80	2812.01	H	55	2896.46	H
60	2818.36	H	210	2896.75	H
45	2822.01	H	55	2897.67	H
180	2822.37	H	55	2897.73	H
22	2826.75	H	90	2898.54	H
180	2830.47	H	80	2899.21	H
70	2834.26	H	55	2899.48	H
2500	2835.63	H	26	2903.97	H
45	2836.48	H	55	2904.68	H
55	2838.79	H	180	2905.49	H
110	2840.02	H	260	2909.05	H
1700	2843.25	H	260	2910.90	H
22	2846.02	H	250	2911.14	H

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
45	2911.68	II	240	3018.82	I
60	2913.73	I	430	3020.67	I
22	2915.23	II	2800	3021.56	I
22	2915.46	II	1100	3024.35	I
90	2921.24	II	85	3026.65	II
60	2921.82	II	170	3029.16	I
60	2927.08	II	710	3030.24	I
80	2928.15	II	140	3031.35	I
95	2928.30	II	28	3032.93	II
26	2929.44	II	390	3034.19	I
35	2930.85	II	555	3037.04	I
26	2932.70	II	80	3039.78	I
55	2933.97	II	550	3040.85	I
90	2935.14	II		3040.91	II
45	2940.22	II	55	3041.74	II
60	2946.84	II	110	3050.14	II
55	2953.36	II	710	3053.88	I
45	2953.71	II	24	3059.52	II
55	2961.73	II	85	3065.07	I
45	2966.05	II	28	3067.16	II
480	2967.64	I	85	3073.68	I
480	2971.11	I	55	3077.83	I
210	2971.91	II	28	3095.86	I
480	2975.48	I	28	3109.34	I
30	2976.72	II	28	3110.86	I
190	2979.74	II	240	3118.65	II
350	2980.79	I	45	3119.25	I
110	2985.32	II	40	3119.71	I
480	2985.85	I	430	3120.37	II
1500	2986.00	I	28	3122.60	II
2100	2986.47	I	470	3124.94	II
660	2988.65	I		3125.02	II
160	2989.19	II	120	3128.70	II
480	2991.89	I	590	3132.06	II
230	2994.07	I	140	3136.68	II
300	2995.10	I	140	3147.23	II
700	2996.58	I	85	3148.44	I
210	2998.79	I	100	3155.15	I
1100	3000.89	I	100	3163.76	I
750	3005.06	I	240	3180.70	II
140	3013.03	I	30	3181.43	II
710	3013.71	I	65	H 3188.01	I
710	3014.76	I	220	3197.08	II
1400	3014.92	I	24	3198.11	I
710	3015.19	I	30	3208.59	II
2800	3017.57	I	170	3209.18	II
430	3018.50	I	140	3217.40	II

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength(Å)	Spectrum
30	3229.20	I	270	3433.60	I
28	3234.06	II	55	3434.11	I
65	3237.73	I	160	3436.19	I
120	3245.54	I	70	3441.12	I
130	3251.84	I	140	3441.44	I
130	3257.82	I	30	3443.79	I
95	3259.98	I	170	3445.62	I
20	3295.43	II	30	3447.02	I
24	3307.02	II	170	3447.43	I
55	3324.06	II	70	3447.76	I
28	3326.59	I	190	3453.33	I
30	3328.35	II	40	3453.74	I
30	3329.05	I	130	3455.60	I
95	3336.33	II	100	3460.43	I
130	3339.80	II	65	3465.25	I
110	3342.59	II	40	3467.02	I
30	3343.34	I	70	3467.72	I
95	3346.02	I	45	3469.59	I
95	3346.74	I	16	3472.76	I
95	3347.84	II	24	3472.91	I
65	3349.07	I	40	3473.61	I
55	3349.32	I	70	3481.30	I
30	3351.60	I	55	3481.54	I
55	3351.97	I	55	3494.97	I
55	H 3353.03	I	40	3495.38	II
	3353.13	II	80	3510.54	I
170	3358.50	II	40	3511.84	II
160	3360.30	II	120	3550.64	I
65	3361.77	II	80	3558.52	I
55	3362.21	I	130	3566.16	I
430	3368.05	II	130	3573.64	I
30	3376.40	I	80	3574.04	I
55	3378.34	II	330	H 3574.80	I
30	3379.17	I		3574.94	I
30	3379.37	II	19000	3578.69	I
95	3379.83	II	160	H 3584.33	I
140	3382.68	II	130	3585.30	II
95	3391.43	II	17000	3593.49	I
55	3392.99	II	350	3601.67	I
70	3393.84	II	40	3602.57	I
55	3394.30	II	85	3603.74	I
30	3402.40	II		3603.78	II
170	3403.32	II	13000	3605.33	I
360	3408.76	II	40	3608.40	I
210	3421.21	II	40	3609.48	I
270	3422.74	II	40	3610.05	I
140	3433.31	II	70	3612.61	I

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
85	3615.64	I	120	3793.29	I
130	3632.64	I	130	3793.88	I
350	3636.59	I	85	3794.61	I
630	3639.80	I	140	3797.13	I
85	3640.39	I	200	3797.72	I
70	3641.47	I	530	3804.80	I
220	3641.83	I	110	3806.83	I
45	3646.16	I	110	3807.93	I
85	3648.53	I	180	3815.43	I
220	3649.00	I	70	3818.48	I
170	3653.91	I	180	3819.56	I
220	3656.26	I	70	3823.52	I
45	3662.84	I	130	3826.42	I
130	3663.21	I	130	3830.03	I
45	3665.98	I	380	3841.28	I
95	3666.64	I	190	3848.98	I
55	3668.03	I	140	3849.36	I
65	3676.32	I	290	3850.04	I
40	3677.68	II	140	3852.22	I
55	3677.89	II	190	3854.22	I
40	3679.82	I	110	3855.29	I
19	3681.69	I	140	3855.57	I
120	3685.55	I	260	3857.63	I
130	3686.80	I	70	3874.53	I
130	3687.25	I	660	3883.29	I
75	3687.54	I	50	3883.66	I
19	3688.46	I	570	3885.22	I
75	3712.95	II	380	3886.79	I
40	3716.53	I	60	3891.93	I
130	3730.81	I	260	3894.04	I
150	3732.03	I	40	3897.65	I
95	3742.97	I	35	3902.11	I
480	3743.58	I	360	3902.92	I
570	3743.88	I	60	3903.16	I
85	3744.49	I	960	3908.76	I
55	3748.61	I	120	HD 3911.82	I
340	3749.00	I		3912.00	I
50	3757.17	I	120	3915.84	I
230	3757.66	I	40	3916.24	I
60	3758.04	I	35	3917.60	I
24	3767.43	I	1900	3919.16	I
260	3768.24	I	600	3921.02	I
95	3768.73	I	30	3926.65	I
95	3788.86	I	600	3928.64	I
95	3790.45	I	410	3941.49	I
130	3791.38	I	30	3951.10	I
130	3792.14	I	40	3952.40	I



Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
35	3953.16	I	70	4165.52	I
1900	3963.69	I	40	4169.84	I
120	3969.06	I	35	4170.20	I
1600	3969.75	I	40	4172.77	I
85	3971.26	I	170	4174.80	I
1600	3976.66	I	30	4175.94	I
85	3978.68	I	170	4179.26	I
40	3979.80	I	35	4184.90	I
85	3981.23	I	30	4186.36	I
960	3983.91	I	35	4190.13	I
190	3984.34	I	85	4191.27	I
160	3989.99	I	35	4192.10	I
960	3991.12	I	85	4193.66	I
160	3991.67	I	70	4194.95	I
190	3992.84	I	40	4197.23	I
40	3993.97	I	85	4198.52	I
160	4001.44	I	60	4203.59	I
120	4012.47	II	40	4204.47	I
30	4014.67	I	35	4208.36	I
85	4022.26	I	110	4209.37	I
70	4025.01	I	40	4209.76	I
120	4026.17	I	40	4211.35	I
85	4027.10	I	40	4216.36	I
85	4030.68	I	85	4217.63	I
190	4039.10	I	40	4221.57	I
160	4048.78	I	40	4222.73	I
120	4058.77	I	40	4238.96	I
40	4065.72	I	60	4240.70	I
85	4066.94	I	20000	4254.35	I
35	4074.86	I	70	4255.50	I
40	4076.06	I	60	4261.35	I
40	4077.09	I	110	4263.14	I
40	4077.68	I	30	4271.06	I
40	4104.87	I	40	4272.91	I
40	4109.58	I	16000	4274.80	I
40	4120.61	I	85	4280.40	I
40	4121.82	I	10000	4289.72	I
35	4122.16	I	40	4291.96	I
40	4123.39	I	85	4295.76	I
140	4126.52	I	70	4297.74	I
35	4127.30	I	35	4300.51	I
40	4127.64	I	50	4301.18	I
40	4131.36	I	30	4305.45	I
30	4152.78	I	35	4319.64	I
120	4153.82	I	60	4325.08	I
85	4161.42	I	780	4337.57	I
140	4163.62	I	1100	4339.45	I

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength(Å)	Spectrum
380	4339.72	I	380	4530.74	I
60	4340.13	I	50	4535.15	I
1900	4344.51	I	240	4535.72	I
70	4346.83	I	40	4539.79	I
380	4351.05	I	240	4540.50	I
2300	4351.77	I	240	4540.72	I
570	4359.63	I	35	4541.07	I
70	4363.13	I	19	4541.51	I
530	4371.28	I	24	4542.62	I
70	4373.25	I	140	4544.62	I
110	4374.16	I	24	4545.34	I
70	4375.33	I	600	4545.96	I
50	4381.11	I	50	4556.17	I
530	4384.98	I	22	4558.66	II
60	4387.50	I	19	4564.17	I
70	4391.75	I	120	4565.51	I
60	4403.50	I	95	4569.64	I
24	4410.30	I	120	4571.68	I
60	4411.09	I	22	4575.12	I
35	4412.25	I	360	4580.06	I
50	4413.87	I	24	4586.14	I
60	4424.28	I	360	4591.39	I
24	4428.50	I	70	4595.59	I
50	4430.49	I	50	4600.10	I
50	4432.18	I	480	4600.75	I
110	4458.54	I	50	4601.02	I
30	4459.74	I	240	4613.37	I
30	4465.36	I	600	4616.14	I
30	4482.88	I	70	4619.55	I
40	4488.05	I	85	4621.96	I
50	4489.47	I	70	4622.49	I
60	4492.31	I	24	4622.76	I
660	4496.86	I	550	4626.19	I
50	4498.73	I	24	4632.18	I
70	4500.30	I	40	4637.18	I
50	4501.11	I	50	4637.77	I
22	4501.79	I	50	D 4639.52	I
24	4506.85	I		4639.70	I
95	4511.90	I	1600	4646.17	I
12	4514.37	I	24	4646.81	I
35	4514.53	I	24	4648.13	I
24	4521.14	I	24	4648.87	I
24	4526.11	I	35	4649.46	I
380	4526.47	I	570	4651.28	I
70	D 4527.34	I	840	4652.16	I
	4527.47	I	35	4654.74	I
24	4529.85	I	19	4656.19	I

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
40	4663.33	I	35	4964.93	I
70	4663.83	I	60	5013.32	I
95	4664.80	I	17	5051.90	I
35	4665.90	I	17	5065.91	I
22	4666.22	I	40	5067.71	I
70	4666.51	I	40	5072.92	I
50	4669.34	I	30	5110.75	I
40	4680.54	I	17	5113.13	I
19	4680.87	I	17	5123.46	I
70	4689.37	I	50	5139.65	I
60	4693.95	I	14	5144.67	I
24	4695.15	I	70	5166.73	I
60	4697.06	I	35	5177.43	I
240	D 4698.46	I	70	5184.59	I
	4698.62	I	70	5192.00	I
35	4700.61	I	12	5193.49	I
190	4706.04	I	85	5196.44	I
240	4718.43	I	35	5200.19	I
50	4723.10	I	5300	5204.52	I
50	4724.42	I	8400	5206.04	I
50	4727.15	I	11000	5208.44	I
24	4729.72	I	19	5214.13	I
120	4730.71	I	30	5221.75	I
140	4737.35	I	85	5224.94	I
19	4745.31	I	12	5226.89	I
70	4752.08	I	19	5238.97	I
340	4756.11	I	30	5243.40	I
50	4764.29	I	290	5247.56	I
22	4766.63	I	60	5254.92	I
30	4767.86	I	60	5255.13	I
190	4789.32	I	19	5261.75	I
95	4792.51	I	530	5264.15	I
120	4801.03	I	30	5265.16	I
110	4829.38	I	180	5265.72	I
14	4836.86	I	35	5272.01	I
17	4861.20	I	30	5273.44	I
70	4861.84	I	95	H 5275.17	I
140	4870.80	I	35	H 5275.69	I
35	4885.78	I	70	H 5276.03	I
19	4885.96	I	19	5280.29	I
130	4887.01	I	10	5287.19	I
19	4888.53	I	340	5296.69	I
35	4903.24	I	70	H 5297.36	I
260	4922.27	I	660	5298.27	I
110	4936.33	I	85	5300.75	I
70	4942.50	I	17	5304.21	I
110	4954.81	I	24	5312.88	I

Intensity	Wavelength (Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
24	5318.78	I	17	H 6925.20	I
340	H 5328.34	I	30	H 6978.48	I
70	H 5329.17	I	11	H 6979.82	I
17	H 5329.72	I	7	7185.52	I
14	5340.44	I	6	H 7236.20	I
10	5344.76	I	85	7355.90	I
780	5345.81	I	130	7400.21	I
380	5348.32	I	150	7462.31	I
30	5386.98	I	11	H 7942.04	I
22	5387.57	I	5	H 8163.18	I
10	5390.39	I	9	8348.28	I
40	5400.61	I	6	8450.26	I
22	5405.00	I	3	8455.24	I
1400	5409.79	I	6	8548.86	I
12	5442.41	I	40	8947.15	I
19	5463.97	I	19	8976.83	I
19	5480.50	I			
24	5628.64	I		Cr III	
7	5642.36	I		Vacuum	
12	H 5649.37	I			
24	5664.04	I			
7	H 5681.20	I	20	969.26	III
7	H 5682.48	I	40	1000.86	III
24	5694.73	I	40	1001.04	III
40	5698.33	I	30	1002.96	III
24	5702.31	I	50	1017.14	III
12	5712.64	I	50	1017.31	III
24	5712.78	I	50	1017.57	III
7	5719.82	I	30	1028.33	III
7	5746.43	I	60	1030.47	III
7	5753.69	I	30	1030.89	III
12	H 5781.20	I	50	1033.23	III
6	H 5781.81	I	50	1033.45	III
24	H 5783.11	I	100	1033.69	III
30	H 5783.93	I	50	1035.93	III
24	H 5785.00	I	100	1036.03	III
19	H 5785.82	I	30	1040.17	III
60	H 5787.99	I	40	1040.53	III
180	H 5791.00	I	40	1045.06	III
35	6330.10	I	40	1045.14	III
22	6362.87	I	40	1045.14	III
19	6661.08	I	60	1059.13	III
11	6669.26	I	60	1060.15	III
5	H 6881.62	I	60	1061.04	III
10	H 6882.38	I	50	1062.68	III
21	H 6883.03	I	30	1064.32	III
27	H 6924.13	I	30	1064.43	III

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
50	1066.23	III	80	2047.23	III
80	1068.41	III	100	2113.73	III
30	1100.61	III	100	2113.83	III
30	1101.43	III	50	2114.26	III
30	1102.88	III	50	2114.53	III
30	1117.19	III	100	2114.87	III
30	1132.75	III	100	2117.53	III
50	1136.67	III	80	2123.53	III
50	1161.43	III	80	2139.11	III
30	1187.65	III	100	2141.15	III
60	1206.38	III	80	2144.15	III
80	1209.13	III	50	2147.16	III
80	1211.12	III	50	2147.56	III
40	1221.07	III	50	2148.65	III
40	1221.90	III	50	2149.48	III
30	1225.65	III	50	2152.76	III
30	1228.65	III	100	2157.17	III
30	1231.88	III	50	2163.86	III
50	1232.96	III	60	2166.25	III
40	1236.20	III	100	2170.70	III
40	1238.51	III	50	2183.71	III
50	1252.61	III	100	2185.01	III
40	1259.02	III	50	2190.09	III
40	1261.86	III	100	2190.76	III
30	1262.34	III	100	2191.58	III
35	1263.61	III	100	2197.59	III
35	1264.21	III	100	2198.62	III
40	1287.05	III	100	2203.22	III
30	1455.27	III	60	2208.70	III
40	1584.60	III	200	2226.72	III
30	1603.19	III	100	2231.81	III
30	1679.25	III	100	2233.81	III
30	1690.28	III	200	2235.91	III
60	1692.89	III	150	2237.59	III
60	1696.64	III	150	2244.10	III
60	1701.48	III	80	2251.45	III
80	1707.43	III	50	2257.92	III
40	1707.78	III	100	2273.30	III
45	1762.81	III	80	2275.43	III
30	1766.92	III	100	2276.38	III
30	1769.17	III	80	2277.47	III
30	1827.26	III	150	2284.44	III
	Air		50	2289.23	III
			80	2290.66	III
60	2036.39	III	60	2295.55	III
50	2039.63	III	50	2309.99	III
			80	2314.63	III

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
100	2319.07	III	80	630.30	IV
150	2324.88	III	30	632.62	IV
60	2340.51	III	30	637.34	IV
50	2456.83	III	50	637.55	IV
100	2472.88	III	50	638.13	IV
100	2479.77	III	30	638.54	IV
100	2483.06	III	100	666.55	IV
60	2488.26	III	75	667.30	IV
80	2506.41	III	40	677.55	IV
80	2530.99	III	40	687.12	IV
80	2537.73	III	50	688.46	IV
80	2544.57	III	100	693.92	IV
50	2545.17	III	50	695.21	IV
80	2564.76	III	50	705.98	IV
80	2616.50	III	30	712.90	IV
100	2626.08	III	80	1055.89	IV
100	2640.73	III	60	1057.85	IV
50	2647.50	III	30	1367.39	IV
40	2655.28	III	40	1375.05	IV
40	2916.57	III	70	1401.82	IV
			100	1417.42	IV
	Cr IV		30	1485.05	IV
	Vacuum		80	1595.04	IV
			90	1595.59	IV
			100	1658.08	IV
			120	1672.66	IV
50	575.05	IV	90	1686.07	IV
30	576.24	IV	100	1690.88	IV
30	576.62	IV	80	1725.26	IV
30	595.09	IV	90	1727.07	IV
50	612.64	IV	100	1732.04	IV
40	613.75	IV	40	1733.98	IV
40	614.03	IV	80	1734.16	IV
40	614.90	IV	50	1739.19	IV
30	615.34	IV	70	1746.88	IV
30	615.60	IV	80	1747.13	IV
50	616.82	IV	110	1755.64	IV
40	618.23	IV	120	1758.51	IV
40	619.13	IV	100	1769.64	IV
100	620.65	IV	100	1777.82	IV
60	621.36	IV	40	1791.09	IV
40	622.09	IV	140	1802.72	IV
30	623.54	IV	130	1812.41	IV
40	625.04	IV	60	1819.23	IV
40	625.99	IV	30	1826.21	IV
100	629.26	IV	30	1826.86	IV
50	629.74	IV	100	1840.14	IV

Intensity	Wavelength(Å)	Spectrum	Intensity	Wavelength (Å)	Spectrum
50	1851.89	v	50	825.60	v
100	1863.11	v	50	968.70	v
140	1873.89	v	50	1045.04	v
35	1883.16	v	60	1060.65	v
40	1937.63	v	50	1112.45	v
30	1946.59	v	60	1114.35	v
140	1967.18	v	100	1116.48	v
120	1972.07	v	80	1117.56	v
40	1990.25	v	50	1118.16	v
			150	1121.07	v
	Air		150	1127.63	v
			100	1193.95	v
50	2042.91	v	80	1196.04	v
40	2055.73	v	50	1210.50	v
70	2299.21	v	50	1259.99	v
90	2299.59	v	100	1263.50	v
100	2316.85	v	150	1465.86	v
40	2324.06	v	50	1481.65	v
50	2360.40	v	50	1482.76	v
70	2405.15	v	50	1484.67	v
60	2423.32	v	100	1489.71	v
			150	1497.97	v
	Cr v		170	1519.03	v
			220	1579.70	v
	Vacuum		170	1591.72	v
100	438.62	v	150	1603.19	v
100	464.02	v	60	1638.50	v
50	469.64	v	50	1639.40	v
			200	1837.44	v

**C. Vacuum Ultraviolet Lines for Cr I through Cr XXIV  
(Wavelengths and Classifications)**



## C. Vacuum Ultraviolet Lines for Cr I through Cr XXIV

[Excerpted from: R. L. Kelly, *J. Phys. Chem. Ref. Data* 16, Supplement 1 (1987)]

The following tables, including the introductory comments, are excerpted from a new tabulation by R. L. Kelly,<sup>1</sup> which supersedes and revises his previous tables published with Palumbo in 1973.<sup>2</sup>

The listed wavelength data are generally from observations, with lines of the helium-like and hydrogen-like ions (Cr XXIII and Cr XXIV) as notable exceptions. But also in some cases where lines have been observed, wavelengths given here are those resulting from a comprehensive analysis of the spectrum rather than the measured values. A few lines have been predicted from unpublished extrapolations along isoelectronic sequences, and some unobserved weak lines in multiplets have been included for completeness. Such predicted values of wavelength are marked by the symbol P in the column labeled "Notes".

The lines are arranged in order of increasing wavelength within each spectrum, and the vacuum wavelengths are given as they are reported in the reference listed first for each line. A complete listing of these references is given at the end of these introductory comments. Where more than one publication reports the wavelength of the line, the decision as to which to retain was based primarily on the present author's judgement of the best value. This judgement was based on consideration of the dates of publication, on probable accuracy from the type of instrumentation used and the wavelength standards employed, on the spectroscopic source used, and on the comparison of the observations with the wavelengths predicted from the best known values of energy levels as described above.

With respect to the accuracy of the wavelength data, it is conservatively estimated that all wavelengths reported should have uncertainties of ten to twenty in the last digit given.

The listed intensities have been normalized to a maximum of 1000 for convenience in comparing the different references. The normalization procedure used was generally a linear or logarithmic transformation of the intensities reported by the original authors, depending on the particular case. Intensities given by different observers have seldom been found compatible, however, and the tabulated intensities should be used only as a rough estimate.

The transitions are shown in standard spectroscopic notation with the lower level given first, and the energy levels, i.e., energies above the ground state, are presented in units of  $1000 \text{ cm}^{-1}$ , each value being rounded off to conserve space. Additive uncertainties are indicated by B, C, K, etc. which may be thousands of  $\text{cm}^{-1}$ . The energy level data are taken from the files of the Naval Postgraduate School Spectroscopic Data Center (and thus do not necessarily agree with those tabulated in Section E of this book).

The multiplet numbers assigned by C. E. Moore<sup>3</sup> are given in a separate column. The classifications of the transitions are given in the accepted form, the primary references being the NBS spectroscopy tables.<sup>3,4</sup> For convenience, separate columns are used for showing the configurations, terms, and  $J$ -values. In the term column, the symbol  $g$  is used to denote the ground term. Otherwise, the term designation follows that of Cowan and Andrew.<sup>5</sup>

The parent terms are given where they are known and where they are not immediately obvious. The older practice of using primes, double primes, etc. to indicate that the parent term of a configuration is an excited state of the next higher ion has been abandoned. But the notation of a, b, c, ... (for even terms) and z, y, x, ... (for odd terms) to indicate the order of appearance of terms of the same multiplicity and same type has been continued.

A few descriptive symbols are used in the "Notes" column which have the following meanings:

- F - line is forbidden by electric dipole selection rules
- A - line observed in absorption
- Q - uncertain classification
- P - predicted value of wavelength

There are three classes of predicted lines:

- (a) lines that have been observed but for which calculations of wavelengths from energy levels are superior to the observations as in hydrogenic spectra and in other specific transitions.
- (b) lines which have not been observed but for which Ritz calculations between known levels can be made, as in many of the forbidden lines.
- (c) lines for which one or both of the energy levels have been found by Hartree-Fock type calculations, by interpolation, or by extrapolation.

These three classes are not separately distinguished in the "Notes" column.

### References for Introductory Comments

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**CHROMIUM, Z = 24**  
**Unclassified Lines**

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	0	12.201						716
	0	12.329						716
	0	12.435						716
	0	12.589						716
	0	12.778						716
	10	13.217						716
	2	12.394						1089
		14.53						716
	10	14.775						716
	20	15.21						716
	10	15.680						716
	80	17.107						716
	100	205.82						256
	100	206.53						256
	300	210.16						256
	300	215.38						256
	300	217.19						256
	200	217.55						256
	200	217.61						256
	100	218.06						256
	100	218.15						256
	400	219.29						256
	200	219.94						256
	200	222.16						256
	300	226.89						256
		334.95						251
		380.7						251
		419.2						251

**CHROMIUM I ( $\text{Cr}^0$ ), Z = 24**  
**Ground State  $1s^2 2s^2 2p^6 3s^2 3p^4 3d^5 4s^1 ({}^7S_3)$  (24 electrons)**  
**Ionization Potential 54 575.6  $\text{cm}^{-1}$ ; 6.7666 eV**

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	10	1653.06	0.0 - 60 49342	$3d^1(a^1S)4s - 3d^44s(a^1D)6p$	$g^1S - q^1D^o$	3 - 3		490
	300	1747.14	0.0 - 57 23750	$3d^1(a^1S)4s - 3d^44s(a^1D)6p$	$g^1S - p^1F^o$	3 - 4		490
		1798.2					A	882
		1798.6					A	882
		1799.7					A	882
		1800.7					A	882
		1800.9					A	882
		1801.1					A	882
		1801.7					A	882
		1802.4					A	882
		1803.0					A	882
		1803.7					A	882

## CR I - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
		1805.2					A	882
		1805.4					r.	882
		1806.5					A	882
		1807.7					A	882
		1808.4					A	882
		1809.7					A	882
		1810.4					A	882
		1812.2					A	882
		1813.7					A	882
		1815.9					A	882
		1818.4	0.0 - 54.99293	$3d^1(a^4S)4s - 3d^1(a^4D)4p$	$g^2S - v^1P^o$	3 - 2	A	882
	1	1835.2	0.0 - 54.4900	$3d^1(a^4S)4s - 3d^1(a^4S)38p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1835.4	0.0 - 54.4840	$3d^1(a^4S)4s - 3d^1(a^4S)37p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1835.5	0.0 - 54.4806	$3d^1(a^4S)4s - 3d^1(a^4S)36p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1835.7	0.0 - 54.4748	$3d^1(a^4S)4s - 3d^1(a^4S)35p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1835.9	0.0 - 54.4685	$3d^1(a^4S)4s - 3d^1(a^4S)34p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1836.2	0.0 - 54.4603	$3d^1(a^4S)4s - 3d^1(a^4S)33p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1836.4	0.0 - 54.4534	$3d^1(a^4S)4s - 3d^1(a^4S)32p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1836.7	0.0 - 54.4456	$3d^1(a^4S)4s - 3d^1(a^4S)31p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1837.0	0.0 - 54.4361	$3d^1(a^4S)4s - 3d^1(a^4S)30p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1837.4	0.0 - 54.4254	$3d^1(a^4S)4s - 3d^1(a^4S)29p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1837.8	0.0 - 54.4135	$3d^1(a^4S)4s - 3d^1(a^4S)28p$	$g^2S - ^7P^o$	3 - 4	A	882
	5	1838.2	0.0 - 54.4005	$3d^1(a^4S)4s - 3d^1(a^4S)27p$	$g^2S - ^7P^o$	3 - 4	A	882
	5	1838.7	0.0 - 54.3855	$3d^1(a^4S)4s - 3d^1(a^4S)26p$	$g^2S - ^7P^o$	3 - 4	A	882
	0	1839.1					A	882
	5	1839.3	0.0 - 54.3686	$3d^1(a^4S)4s - 3d^1(a^4S)25p$	$g^2S - ^7P^o$	3 - 4	A	882
	5	1839.9	0.0 - 54.3508	$3d^1(a^4S)4s - 3d^1(a^4S)24p$	$g^2S - ^7P^o$	3 - 4	A	882
	10	1840.69	0.0 - 54.3272	$3d^1(a^4S)4s - 3d^1(a^4S)23p$	$g^2S - ^7P^o$	3 - 4	A	490
	10	1841.5	0.0 - 54.3036	$3d^1(a^4S)4s - 3d^1(a^4S)22p$	$g^2S - ^7P^o$	3 - 4	A	882
	00	1842.4					A	882
	10	1842.6	0.0 - 54.2711	$3d^1(a^4S)4s - 3d^1(a^4S)21p$	$g^2S - ^7P^o$	3 - 4	A	882
	00	1843.1					A	882
	5	1843	0.0 - 54.2388	$3d^1(a^4S)4s - 3d^1(a^4S)20p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1844.6					A	882
	10	1845.1	0.0 - 54.1966	$3d^1(a^4S)4s - 3d^1(a^4S)19p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1846.4					A	882
	10	1846.8	0.0 - 54.1477	$3d^1(a^4S)4s - 3d^1(a^4S)18p$	$g^2S - ^7P^o$	3 - 4	A	882
	5	1847.2					A	882
	00	1847.3	0.0 - 54.13288	$3d^1(a^4S)4s - 3d^1(a^4D)5p$	$g^2S - v^1P^o$	3 - 3	A	882
	10	1848.8	0.0 - 54.0890	$3d^1(a^4S)4s - 3d^1(a^4S)17p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1849.5					A	882
	10	1851.3	0.0 - 54.0171	$3d^1(a^4S)4s - 3d^1(a^4S)16p$	$g^2S - ^7P^o$	3 - 4	A	882
	10	1854.3	0.0 - 53.9280	$3d^1(a^4S)4s - 3d^1(a^4S)15p$	$g^2S - ^7P^o$	3 - 4	A	882
	15	1858.2	0.0 - 53.8158	$3d^1(a^4S)4s - 3d^1(a^4S)14p$	$g^2S - ^7P^o$	3 - 4	A	882
	5	1859.3	0.0 - 53.78277	$3d^1(a^4S)4s - 3d^1(a^4D)5p$	$g^2S - v^1D^o$	3 - 4	A	882
	25	1863.2	0.0 - 53.6714	$3d^1(a^4S)4s - 3d^1(a^4S)13p$	$g^2S - ^7P^o$	3 - 4	A	882
	1	1864.3	0.0 - 53.64074	$3d^1(a^4S)4s - 3d^1(a^4D)5p$	$g^2S - v^1D^o$	3 - 3	A	882
	25	1869.7					A	882
	25	1869.8	0.0 - 53.4826	$3d^1(a^4S)4s - 3d^1(a^4S)12p$	$g^2S - ^7P^o$	3 - 4	A	882
	50	1873.7					A	882
	1	1874.4					A	882
	1	1878.0					A	882
	50	1878.4					A	882
	1	1878.8	0.0 - 53.2268	$3d^1(a^4S)4s - 3d^1(a^4S)11p$	$g^2S - ^7P^o$	3 - 4	A	882

Multiplet	Rel. Int.	$\lambda_{air}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J-J	Notes	References
	5	1879.1					A	882
	5	1879.2					A	882
	50	1880.39	7.92747 - 61.10795	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - r^1P^o$	2-2		341
	250	1881.87	7.92747 - 61.06596	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - r^1P^o$	2-1		341
	1	1882.6	0.0 - 53.11754	$3d^1(a^1S)4s - 3d^1(a^1D)4s4p(^1P^o)$	$ga^1S - r^1F^o$	3-4	A	882
	50	1883.11	8.09521 - 61.19868	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - r^1P^o$	3-3		341
	1	1884.2	0.0 - 53.07390	$3d^1(a^1S)4s - 3d^1(a^1D)4s4p(^1P^o)$	$ga^1S - r^1F^o$	3-3	A	882
	00	1885.3					A	882
	50	1885.50	7.59316 - 60.62967	$3d^1(a^1S)4s - 3d^1(a^1D)4p$	$a^1S - s^1D^o$	2-2		490
	500	1886.34	8.09521 - 61.10795	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - r^1P^o$	3-2		341
	150	1887.60	7.92747 - 60.90484	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - o^1F^o$	2-3		341
	50	1887.85	7.81082 - 60.78125	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - o^1F^o$	1-2		341
	150	1888.17	8.09521 - 61.05641	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - o^1F^o$	3-4		341
	50	1889.20	7.75078 - 60.68353	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - o^1F^o$	0-1		341
	1	1890.0					A	882
	50	1890.4					A	882
	300	1890.78	8.30757 - 61.19577	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - o^1F^o$	4-5		341
		1891.4	0.0 - 52.8695	$3d^1(a^1S)4s - 3d^1(a^1S)10p$	$ga^1S - ^1P^o$	3-4	P	375
	50	1892.01	7.92747 - 60.78125	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - o^1F^o$	2-2		341
	50	1892.8					A	882
	50	1893.59	8.09521 - 60.90484	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - o^1F^o$	3-3		341
	5	1894.2					A	882
	50	1895.78	8.30757 - 61.05641	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - o^1F^o$	4-4		341
	1	1896.9					A	882
	150	1902.43	7.81082 - 60.37494	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	1-2		341
	50	1903.30	7.75078 - 60.29104	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	0-1		341
	50	1903.57	8.09521 - 60.62796	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	3-4		341
	100	1906.67	7.92747 - 60.37494	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	2-2		341
	100	1907.28	7.81082 - 60.2415	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	1-0		341
	200	1908.46	8.09521 - 60.49342	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	3-3		341
	100	1909.72	7.92747 - 60.29104	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	2-1		341
		1910.3	0.0 - 52.3488	$3d^1(a^1S)4s - 3d^1(a^1S)9p$	$ga^1S - ^1P^o$	3-4	P	375
	350	1911.30	8.30757 - 60.62796	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	4-4		341
	200	1912.79	8.09521 - 60.37494	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	3-2		341
	100	1916.23	8.30757 - 60.49342	$3d^4 4s^2 - 3d^4 4s(a^1D)6p$	$a^1D - q^1D^o$	4-3		341
	10	1924.8					A	882
	15	1927.1					A	882
	10	1928.7					A	882
	10	1929.60	7.59316 - 59.41701	$3d^1(a^1S)4s - 3d^1(a^1F)4s4p(^1P^o)$	$a^1S - r^1F^o$	2-3		490
	50	1940.45	0.0 - 51.5344	$3d^1(a^1S)4s - 3d^1(a^1S)8p$	$ga^1S - v^1P^o$	3-4	A	882
	50	1940.56	0.0 - 51.5315	$3d^1(a^1S)4s - 3d^1(a^1S)8p$	$ga^1S - v^1P^o$	3-3	A	882
		1940.64	0.0 - 51.5294	$3d^1(a^1S)4s - 3d^1(a^1S)8p$	$ga^1S - v^1P^o$	3-2	A	882
49	40	1948.51	8.09521 - 59.41701	$3d^4 4s^2 - 3d^4(a^1F)4s4p(^1P^o)$	$a^1D - r^1F^o$	3-3		490
	10	1961.93						490
49	200	1989.05	7.92747 - 58.20265	$3d^4 4s^2 - 3d^4(a^1F)4p$	$a^1D - s^1F^o$	2-3	P	341
48	750	1989.92	7.81082 - 58.06380	$3d^4 4s^2 - 3d^4 4s(a^1D)5p$	$a^1D - r^1D^o$	1-2		341
48	400	1990.27	7.75078 - 57.99504	$3d^4 4s^2 - 3d^4 4s(a^1D)5p$	$a^1D - r^1D^o$	0-1		341
	750	1991.22	0.0 - 50.2210	$3d^1(a^1S)4s - 3d^1(a^1S)7p$	$ga^1S - ^1P^o$	3-4		341, 375
48	300	1992.12	8.09521 - 58.29262	$3d^4 4s^2 - 3d^4 4s(a^1D)5p$	$a^1D - r^1D^o$	3-4		341
48	250	1992.65	7.81082 - 57.99504	$3d^4 4s^2 - 3d^4 4s(a^1D)5p$	$a^1D - r^1D^o$	1-1		341
48	400	1994.10	7.81082 - 57.95842	$3d^4 4s^2 - 3d^4 4s(a^1D)5p$	$a^1D - r^1D^o$	1-0		341
48	750	1994.55	7.92747 - 58.06380	$3d^4 4s^2 - 3d^4 4s(a^1D)5p$	$a^1D - r^1D^o$	2-2		341
49	250	1995.69	8.09521 - 58.20265	$3d^4 4s^2 - 3d^4(a^1F)4p$	$a^1D - s^1P^o$	3-3		341
49	250	1997.09	8.09521 - 58.16789	$3d^4 4s^2 - 3d^4(a^1F)4p$	$a^1D - s^1P^o$	3-4		341

CR I - Continued

Multiplet	Rel. Int.	$\lambda_{av}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
48	500	1997.30	7.92747 - 57.99504	$3s^2 4s^2 - 3d^4 4s(a^4D)^2$	$a^4D - r^4D$	2 - 1		341
48	600	1997.90	8.09521 - 58.14776	$3s^2 4s^2 - 3d^4 4s^2 (D)5p$	$a^4D - r^4D$	3 - 3		341

**CHROMIUM II ( $\text{Cr}^{2+}$ ), Z = 24**  
**Ground State  $1s^2 2s^2 2p^6 3s^2 3p^4 3d^4 ({}^5S_{4/2})$  (23 electrons)**  
**Ionization Potential  $133\,060 \text{ cm}^{-1}$ ; 16.4975 eV**

Multiplet	Rel. Int.	$\lambda_{av}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	10	1392.83	19.63128 - 91.42631	$3d^4(a^4D)4s - 3d^4(b^4P)4p$	$a^4D - u^4D$			490
	100	1406.90	20.02418 - 91.10336	$3d^4(a^4D)4s - 3d^4(b^4F)4p$	$a^4D - w^4G$			490
	40	1492.23	0.0 - 67.01228	$3d^4 - 3d^4(a^4P)4p$	$g^4S - y^4F$			490
	20	1504.16	20.02418 - 86.50738	$3d^4(a^4D)4s - 3d^4(a^4F)4p$	$a^4D - v^4D$			490
	20	1604.82	11.96200 - 74.27348	$3d^4(a^4D)4s - 3d^4(a^4D)4p$	$a^4D - w^4F$			490
	20	1606.67	12.05272 - 74.27348	$3d^4(a^4D)4s - 3d^4(a^4D)4p$	$a^4D - w^4F$			490
	50	1626.85	25.04310 - 86.51108	$3d^4 - 3d^4(a^4F)4p$	$b^4D - v^4D$			490
	10	1657.18	31.08311 - 91.42631	$3d^4(a^4F)4s - 3d^4(b^4P)4p$	$a^4F - u^4D$			490
	10	1661.02	31.35115 - 91.55654	$3d^4 - 3d^4(b^4P)4p$	$a^4D - u^4D$			490
	20	1665.98	31.53162 - 91.55654	$3d^4 - 3d^4(b^4P)4p$	$a^4D - u^4D$			490
	70	1696.27	32.60373 - 91.55654	$3d^4 - 3d^4(b^4P)4p$	$a^4F - u^4D$			490
	10	1712.85	32.60373 - 90.98631	$3d^4 - 3d^4(b^4F)4p$	$a^4F - w^4G$			490
	70	1727.11	47.46494 - 105.3652	$3d^4(a^4D)4p - 3d^4(a^4G)5s$	$r^4F - r^4G$			490
	10	1727.78	25.04310 - 82.92003	$3d^4 - 3d^4(a^4D)4p$	$b^4D - w^4P$			490
	40	1729.79	25.04310 - 82.85400	$3d^4 - 3d^4(a^4D)4p$	$b^4D - w^4P$			490
	200	1736.63	33.52123 - 91.10336	$3d^4(a^4G)4s - 3d^4(b^4F)4p$	$b^4G - w^4G$			490
	20	1754.36	12.49679 - 69.49827	$3d^4(a^4D)4s - 3d^4(a^4G)4p$	$a^4D - r^4F$			490
224	40	1786.11	35.56902 - 91.55654	$3d^4(a^4F)4s - 3d^4(b^4P)4p$	$b^4F - u^4D$		P	340
	30	1789.24	21.82482 - 77.71366	$3d^4 - 3d^4(a^4S)4p$	$a^4P - r^4P$			490
224	40	1791.51	35.60760 - 91.42631	$3d^4(a^4F)4s - 3d^4(b^4P)4p$	$b^4F - u^4D$			340
	10	1794.47	12.14800 - 67.87568	$3d^4(a^4D)4s - 3d^4(a^4F)4p$	$a^4D - r^4D$			490
18	60	1808.66	19.63128 - 74.92080	$3d^4(a^4D)4s - 3d^4(a^4D)4p$	$a^4D - r^4P$			340
	100	1810.08	12.14800 - 67.39380	$3d^4(a^4D)4s - 3d^4(a^4P)4p$	$a^4D - y^4F$			340
	20	1812.91	31.35115 - 86.51108	$3d^4 - 3d^4(a^4F)4p$	$a^4D - v^4D$		P	340
	20	1813.41	12.30398 - 67.44882	$3d^4(a^4D)4s - 3d^4(a^4P)4p$	$a^4D - y^4F$		P	340
	60	1815.32	19.63128 - 74.71805	$3d^4(a^4D)4s - 3d^4(a^4D)4p$	$a^4D - r^4P$			340
	20	1818.89	31.53162 - 86.51108	$3d^4 - 3d^4(a^4F)4p$	$a^4D - v^4D$			340
	100	1819.77	12.49679 - 67.44882	$3d^4(a^4D)4s - 3d^4(a^4P)4p$	$a^4D - y^4F$		P	340
	20	1820.77	12.14800 - 67.07048	$3d^4(a^4D)4s - 3d^4(a^4P)4p$	$a^4D - y^4F$			490
18	80	1820.84	19.79801 - 74.71805	$3d^4(a^4D)4s - 3d^4(a^4D)4p$	$a^4D - r^4P$			340
	160	1821.58	12.49679 - 67.39380	$3d^4(a^4D)4s - 3d^4(a^4P)4p$	$a^4D - y^4F$			340
	20	1823.07	19.63128 - 74.48425	$3d^4(a^4D)4s - 3d^4(a^4D)4p$	$a^4D - r^4P$			340
4	60	1825.34	0.0 - 54.78467	$3d^4 - 3d^4(a^4D)4p$	$g^4S - r^4D$			340
	20	1828.56	19.63128 - 74.31886	$3d^4(a^4D)4s - 3d^4(a^4D)4p$	$a^4D - w^4P$			490
	60	1828.62	19.79801 - 74.48425	$3d^4(a^4D)4s - 3d^4(a^4D)4p$	$a^4D - r^4P$			340
4	100	1830.61	0.0 - 54.62576	$3d^4 - 3d^4(a^4D)4p$	$g^4S - r^4D$			340
18	240	1836.23	20.02418 - 74.48425	$3d^4(a^4D)4s - 3d^4(a^4D)4p$	$a^4D - r^4P$			340
33	500	1852.13	20.51275 - 74.50451	$3d^4 - 3d^4(a^4D)4p$	$a^4G - w^4P$			340
	30	1852.31	20.51833 - 74.50451	$3d^4 - 3d^4(a^4D)4p$	$a^4G - w^4P$			490
33	60	1852.37	20.51985 - 74.50451	$3d^4 - 3d^4(a^4D)4p$	$a^4G - w^4P$			340
	20	1854.46	20.51262 - 74.43614	$3d^4 - 3d^4(a^4G)4p$	$a^4G - r^4P$			340
	60	1854.68	20.51833 - 74.43614	$3d^4 - 3d^4(a^4G)4p$	$a^4G - r^4P$			340

CR II - Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $\text{M}^{\circ} \text{cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
33	400	1835.14	20.51985 - 74.42394	$3d^2 - 3d^2(D)4p$	$a^{\circ}G - w^{\circ}F$	-		340
33	400	1838.54	20.51262 - 74.31886	$3d^2 - 3d^2(D)4p$	$a^{\circ}G - w^{\circ}F$	-		340
33	300	1838.72	20.51833 - 74.31886	$3d^2 - 3d^2(D)4p$	$a^{\circ}G - w^{\circ}F$	-		340
33	240	1860.89	20.51262 - 74.27348	$3d^2 - 3d^2(D)4p$	$a^{\circ}G - w^{\circ}F$	-		340
	20	1865.80	20.51833 - 74.11448	$3d^2 - 3d^2(G)4p$	$a^{\circ}G - x^{\circ}F$	-	F	340
156	300	1866.22	32.35594 - 85.93950	$3d^2 - 3d^2(F)4p$	$a^{\circ}F - v^{\circ}G$	-		340
	20	1870.51	20.82418 - 73.48360	$3d^2(D)4s - 3d^2(D)4p$	$a^{\circ}D - w^{\circ}D$	-	F	340
	60	1875.22	31.35115 - 84.67739	$3d^2 - 3d^2(F)4p$	$a^{\circ}D - u^{\circ}F$	-		340
156	200	1879.08	32.35594 - 85.57343	$3d^2 - 3d^2(F)4p$	$a^{\circ}F - v^{\circ}G$	-	F	340
	120	1881.06	21.82286 - 74.98493	$3d^2 - 3d^2(D)4p$	$a^{\circ}F - y^{\circ}F$	-		340
40	200	1883.35	21.82425 - 74.92880	$3d^2 - 3d^2(D)4p$	$a^{\circ}F - x^{\circ}F$	-		340
	20	1884.18	31.53162 - 84.68499	$3d^2 - 3d^2(F)4p$	$a^{\circ}D - u^{\circ}F$	-	F	340
	120	1887.96	20.51833 - 73.48360	$3d^2 - 3d^2(D)4p$	$a^{\circ}G - w^{\circ}D$	-		340
40	600	1890.55	21.82286 - 74.71805	$3d^2 - 3d^2(D)4p$	$a^{\circ}F - x^{\circ}F$	-		340
40	700	1898.92	21.82286 - 74.88425	$3d^2 - 3d^2(D)4p$	$a^{\circ}F - x^{\circ}F$	-		340
	30	1900.86	21.82286 - 74.83684	$3d^2 - 3d^2(G)4s$	$a^{\circ}F - x^{\circ}F$	-		490
	60	1907.60	12.49679 - 64.52430	$3d^2(D)4s - 3d^2(F)4p$	$a^{\circ}D - y^{\circ}D$	-	F	340
155	140	1911.26	32.35594 - 84.67739	$3d^2 - 3d^2(F)4p$	$a^{\circ}F - u^{\circ}F$	-	F	340
	30	1918.30	20.51985 - 72.64679	$3d^2(8H)4p$	$a^{\circ}G - x^{\circ}G$	-		340
155	160	1923.02	32.60373 - 84.68499	$3d^2 - 3d^2(F)4p$	$a^{\circ}F - u^{\circ}F$	-		340
	70	1928.61	34.65948 - 86.51108	$3d^2(F)4s - 3d^2(F)4p$	$a^{\circ}F - v^{\circ}D$	-		490
285	240	1929.96	39.74236 - 91.55664	$3d^2 - 3d^2(F)4p$	$c^{\circ}F - a^{\circ}D$	-		340
273	100	1932.64	39.68400 - 91.42631	$3d^2(G)4s - 3d^2(F)4p$	$c^{\circ}G - a^{\circ}D$	-		340
39	500	1935.63	21.82286 - 73.48360	$3d^2 - 3d^2(F)4p$	$a^{\circ}F - w^{\circ}D$	-	F	340
	35	1937.56	21.82482 - 73.43627	$3d^2 - 3d^2(D)4p$	$a^{\circ}F - w^{\circ}D$	-		340
39	60	1938.42	21.82286 - 73.41194	$3d^2 - 3d^2(D)4p$	$a^{\circ}F - w^{\circ}D$	-		340
136	120	1939.15	31.35115 - 82.92003	$3d^2 - 3d^2(F)4p$	$a^{\circ}D - w^{\circ}F$	-		340
285	100	1939.40	39.87728 - 91.42631	$3d^2 - 3d^2(F)4p$	$c^{\circ}F - a^{\circ}D$	-		340
136	200	1945.48	31.53162 - 82.92003	$3d^2 - 3d^2(D)4p$	$a^{\circ}D - w^{\circ}F$	-		340
136	200	1948.67	31.53162 - 82.85400	$3d^2 - 3d^2(D)4p$	$a^{\circ}D - w^{\circ}F$	-	F	340
205	800	1949.10	34.63114 - 85.93950	$3d^2(H)4s - 3d^2(F)4p$	$a^{\circ}H - v^{\circ}G$	-		340
272	700	1949.22	39.68400 - 90.98631	$3d^2(G)4s - 3d^2(F)4p$	$c^{\circ}G - w^{\circ}G$	-		340
272	1000	1950.12	39.82452 - 91.10336	$3d^2(G)4s - 3d^2(F)4p$	$c^{\circ}G - w^{\circ}G$	-	F	340
205	300	1955.43	34.81306 - 85.93950	$3d^2(H)4s - 3d^2(F)4p$	$a^{\circ}H - v^{\circ}G$	-		340
205	300	1963.67	34.63114 - 85.57343	$3d^2(H)4s - 3d^2(F)4p$	$a^{\circ}H - v^{\circ}G$	-		340
31	440	1985.42	20.51275 - 70.67995	$3d^2 - 3d^2(G)4p$	$a^{\circ}G - x^{\circ}G$	-	F	340
	31	1985.67	20.51985 - 70.67995	$3d^2 - 3d^2(G)4p$	$a^{\circ}G - x^{\circ}G$	-		340
	10	1987.19	19.63128 - 69.95420	$3d^2(D)4s - 3d^2(F)4p$	$a^{\circ}D - y^{\circ}D$	-		490
154	100	1987.41	32.60373 - 82.92003	$3d^2 - 3d^2(D)4p$	$a^{\circ}F - w^{\circ}F$	-		340
234	200	1990.79	35.70766 - 85.93950	$3d^2 - 3d^2(F)4p$	$b^{\circ}H - v^{\circ}G$	-		340
31	300	1993.37	20.51275 - 70.67922	$3d^2 - 3d^2(G)4p$	$a^{\circ}G - x^{\circ}G$	-		340
31	500	1993.63	20.51985 - 70.67922	$3d^2 - 3d^2(G)4p$	$a^{\circ}G - x^{\circ}G$	-		340
	60	1996.62	20.02418 - 70.10783	$3d^2(D)4s - 3d^2(F)4p$	$a^{\circ}D - y^{\circ}D$	-		340
204	40	1998.14	34.63114 - 84.67739	$3d^2(H)4s - 3d^2(F)4p$	$a^{\circ}H - u^{\circ}F$	-		340

CHROMIUM III (Cr<sup>3+</sup>), Z = 24  
 Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>6</sup>3d<sup>3</sup>(<sup>4</sup>F<sub>3</sub>) (22 electrons)  
 Ionization Potential 249 780 cm<sup>-1</sup>; 30.96 eV

Multiplicity	Rel. Int.	$\lambda_{max}$ (in Å)	Levels (in 10 <sup>3</sup> cm <sup>-1</sup> )	Configurations	Terms	J-J	Notes	References
	200	735.89						490
	80	748.35						490
	10	755.69						490
	1	756.567	17.14856 - 149.34483	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> F	1-2		893
	1	763.187	18.58339 - 149.62630	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> F	4-4		893
	10	767.30						490
	10	767.61						490
	20	767.83						490
	20	768.21	16.77136 - 146.93618	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> D	0-1		490
	30	768.51	18.45184 - 148.57381	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> D	2-2		490
	40	769.20						490
	30	769.66						490
	1	777.362	20.78364 - 149.34483	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> G - <sup>3</sup> F	3-2		893
	25	777.425	20.99604 - 149.62630	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> G - <sup>3</sup> F	5-4		893
	10	777.86						490
	10	778.826	20.85295 - 149.38364	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> G - <sup>3</sup> F	4-3		893
	40	778.165	18.58339 - 147.80073	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> D	4-3		893
	4	778.306	18.45184 - 146.93618	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> D	2-1		893
	25	778.438	18.51118 - 146.97333	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> D	3-2		893
	10	779.43						490
	50	780.87						490
	40	781.42						490
	30	781.88						490
	20	782.26						490
	10	782.45						490
	10	788.032	25.13887 - 152.03721	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> G - <sup>3</sup> F	4-3		893
	30	788.90						490
	10	789.59						490
	10	789.81						490
	10	790.65						490
	4	794.246	25.78094 - 151.68744	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> D - <sup>3</sup> F	2-1		893
	10	796.025	25.72644 - 151.35127	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> D - <sup>3</sup> F	3-2		893
	10	798.31						490
	30	801.04						490
	10	814.71						490
	10	814.90						490
	10	815.40						490
	10	815.99						490
	10	816.57						490
	10	817.87						490
	20	821.74						490
	4	823.971	25.72644 - 147.09073	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> D - <sup>3</sup> D	3-3		893
	1	825.141	25.78094 - 146.97333	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> D - <sup>3</sup> D	2-2		893
	10	825.593	25.84831 - 146.97333	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> D - <sup>3</sup> D	1-2		893
	4	834.131	32.15199 - 152.03721	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> D - <sup>3</sup> F	2-3		893
	10	843.37						490
	10	845.90						490
	4	846.977	.35655 - 118.42299	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> F) <sup>1</sup> 4p	a <sup>3</sup> D - <sup>3</sup> D	3-2		893
	10	866.19						490
	40	869.327	37.00516 - 152.03721	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> D) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> F	3-3		893
	20	875.05	18.45184 - 132.73422	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> F) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> D	2-1		490
	4	875.147	17.85118 - 132.11750	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> F) <sup>1</sup> 4p	a <sup>3</sup> F - <sup>3</sup> D	2-3		893
	10	876.785	17.39692 - 131.45016	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> F) <sup>1</sup> 4p	a <sup>3</sup> H - <sup>3</sup> D	5-5		893
	200	877.255	17.27370 - 131.26546	3d <sup>3</sup> - 3d <sup>2</sup> ( <sup>3</sup> F) <sup>1</sup> 4p	a <sup>3</sup> H - <sup>3</sup> D	4-4		893



Number	Ref. No.	$\lambda_c$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J-J	Notes	References
90	90	677.807	17.53065 - 131.65016	$3d^2 - 3d^1e^27p^4$	$^3H - ^3G$	6-5		893
60	60	678.407	17.59602 - 131.26566	$3d^2 - 3d^1e^27p^4$	$^3H - ^3G$	5-4		893
50	50	823.00	17.27370 - 131.11636	$3d^2 - 3d^1e^27p^4$	$^3H - ^3G$	4-3		893
20	20	824.18						490
25	25	826.007	18.58339 - 131.65016	$3d^2 - 3d^1e^27p^4$	$^3F - ^3G$	4-5		893
4	4	826.879	18.51118 - 131.26566	$3d^2 - 3d^1e^27p^4$	$^3F - ^3G$	3-4		893
4	4	827.528	18.45184 - 131.11636	$3d^2 - 3d^1e^27p^4$	$^3F - ^3G$	2-3		893
40	40	828.25						490
40	40	828.54						490
40	40	829.33						490
40	40	829.09						490
40	40	829.86						490
40	40	829.19						490
4	4	826.310	37.80516 - 148.57281	$3d^2 - 3d^1e^27p^4$	$^3F - ^3D$	3-2		893
4	4	826.82	17.27370 - 128.78413	$3d^2 - 3d^1e^27p^4$	$^3H - ^3P$	4-3		893
50	50	827.229	17.29627 - 128.85049	$3d^2 - 3d^1e^27p^4$	$^3H - ^3P$	5-4		893
4	4	828.454	17.85118 - 128.78413	$3d^2 - 3d^1e^27p^4$	$^3F - ^3P$	2-3		893
4	4	828.454						893
220	220	828.479	20.70364 - 131.26566	$3d^2 - 3d^1e^27p^4$	$^3G - ^3G$	3-4		893
60	60	828.354	20.59604 - 131.65016	$3d^2 - 3d^1e^27p^4$	$^3G - ^3G$	5-5		893
40	40	828.488	20.85395 - 131.26566	$3d^2 - 3d^1e^27p^4$	$^3G - ^3G$	4-4		893
40	40	828.92						490
4	4	826.290	18.51118 - 128.85049	$3d^2 - 3d^1e^27p^4$	$^3F - ^3P$	3-4		893
4	4	826.358	18.45184 - 128.78413	$3d^2 - 3d^1e^27p^4$	$^3F - ^3P$	2-3		893
10	10	826.596	18.45184 - 128.78413	$3d^2 - 3d^1e^27p^4$	$^3F - ^3P$	2-2		893
40	40	826.844	18.51118 - 128.78413	$3d^2 - 3d^1e^27p^4$	$^3F - ^3P$	3-3		893
60	60	826.896	18.58339 - 128.85049	$3d^2 - 3d^1e^27p^4$	$^3F - ^3P$	4-4		893
40	40	826.763	25.13827 - 134.88754	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	3-4		893
60	60	826.166			$^3G - ^3P$	4-3		490
10	10	826.26						490
120	120	826.587	57.608 - 180.15489	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	4-4		893
60	60	826.911	1.8316 - 108.72279	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	2-3		893
10	10	826.172	0.822 - 109.57089	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	1-2		893
30	30	826.75						490
4	4	824.115	0.822 - 109.45811	$3d^2 - 3d^1e^27p^4$	$^3D - ^3P$	1-0		893
60	60	824.178	1.8316 - 109.57089	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	2-2		893
25	25	824.340	3.5655 - 108.72279	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	3-3		893
10	10	824.67						490
20	20	825.02	3.5655 - 109.57089	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	3-2		893
60	60	826.200	57.608 - 108.72279	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	4-3		490
10	10	827.40						490
20	20	827.75	57.608 - 109.53625	$3d^2 - 3d^1e^27p^4$	$^3D - ^3P$	4-4		490
40	40	828.183	0.822 - 108.97290	$3d^2 - 3d^1e^27p^4$	$^3D - ^3P$	1-2		893
25	25	828.571	0 - 108.86498	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	0-1		893
25	25	828.859	25.13827 - 133.96957	$3d^2 - 3d^1e^27p^4$	$^3G - ^3G$	4-4		893
10	10	828.095	0.822 - 108.86498	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	1-1		893
120	120	829.200	1.8316 - 108.97290	$3d^2 - 3d^1e^27p^4$	$^3D - ^3P$	2-2		893
25	25	829.119	1.8316 - 108.86498	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	2-1		893
25	25	829.511	0.822 - 108.69765	$3d^2 - 3d^1e^27p^4$	$^3D - ^3D$	1-0		893
40	40	829.699	1.8316 - 108.79584	$3d^2 - 3d^1e^27p^4$	$^3D - ^3P$	2-3		893
4	4	829.171	3.5655 - 108.79484	$3d^2 - 3d^1e^27p^4$	$^3D - ^3P$	1-3		893
120	120	829.517	0.822 - 108.46140	$3d^2 - 3d^1e^27p^4$	$^3D - ^3P$	1-2		893
4	4	829.543	1.8316 - 108.46140	$3d^2 - 3d^1e^27p^4$	$^3D - ^3P$	2-2		893

## CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J-J	Notes	References
4	150	923.704	0 - 108.25009	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	0-1		893
4	330	924.045	.57008 - 108.79304	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	4-3		893
4	380	924.310	.8622 - 108.25009	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	1-1		893
4	330	925.026	.39655 - 108.46340	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	3-2		893
27	25	925.257	20.70064 - 128.70413	$3d^2 - 3d^2(7^2)4p$	$^3G - ^3F$	3-3		893
4	230	925.343	.18316 - 108.25009	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	2-1		893
27	230	925.087	20.70064 - 128.75462	$3d^2 - 3d^2(7^2)4p$	$^3G - ^3F$	3-2		893
27	25	925.945	20.85295 - 128.83049	$3d^2 - 3d^2(7^2)4p$	$^3G - ^3F$	4-4		893
27	300	926.510	20.85295 - 128.70413	$3d^2 - 3d^2(7^2)4p$	$^3G - ^3F$	4-3		893
	90	926.703	43.44199 - 151.35127	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3F$	2-2		893
27	300	927.173	20.99804 - 128.83049	$3d^2 - 3d^2(7^2)4p$	$^3G - ^3F$	5-4		893
	10	927.097	43.94609 - 151.65704	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3F$	1-1		893
	10	929.831	44.14136 - 151.65704	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3F$	0-1		893
	25	930.794	43.94609 - 151.35127	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3F$	1-2		893
	4	934.971	25.70004 - 132.73022	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3D$	2-1		893
	40	935.575	25.04031 - 132.73022	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3D$	1-1		893
	4	936.900	25.72644 - 132.49976	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3D$	3-2		893
	90	937.000	25.70004 - 132.49976	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3D$	2-2		893
	120	939.926	25.72644 - 132.11730	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3D$	3-3		893
	200	940.304	43.20671 - 149.62630	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3F$	4-4		893
	10	940.704	43.32217 - 149.62630	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3F$	3-4		893
	40	942.534	43.20671 - 149.36364	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3F$	4-3		893
	10	942.694	43.30453 - 149.36364	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3F$	2-3		893
	150	942.849	43.32217 - 149.36364	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3F$	3-3		893
	150	943.045	43.30453 - 149.34403	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3F$	2-2		893
	40	943.304	43.32217 - 149.34403	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3F$	3-2		893
	100	953.94						490
	100	954.07						490
	150	963.352	43.20671 - 147.09073	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3D$	4-3		893
	25	963.603	43.32217 - 147.09073	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3D$	3-3		893
	25	964.615	43.30453 - 146.97333	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3D$	2-2		893
	120	964.770	43.32217 - 146.97333	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3D$	3-2		893
	90	964.956	43.30453 - 146.93618	$3d^2 - 3d^2(7^2)4p$	$^3F - ^3D$	2-1		893
	4	965.295	17.85118 - 121.44677	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3D$	2-1		893
11	200	966.238	17.27370 - 120.76726	$3d^2 - 3d^2(7^2)4p$	$^3H - ^3G$	4-3		893
11	25	966.430	17.27370 - 120.74935	$3d^2 - 3d^2(7^2)4p$	$^3H - ^3G$	4-4		893
11	230	967.355	17.39692 - 120.74935	$3d^2 - 3d^2(7^2)4p$	$^3H - ^3G$	5-4		893
11	25	968.021	17.39692 - 120.70027	$3d^2 - 3d^2(7^2)4p$	$^3H - ^3G$	5-5		893
11	200	969.272	17.53065 - 120.70027	$3d^2 - 3d^2(7^2)4p$	$^3H - ^3G$	6-5		893
	120	969.703	25.72644 - 128.83049	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	3-4		893
	90	970.040	25.70004 - 128.70413	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	2-3		893
	60	971.758	25.04031 - 128.75462	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	1-2		893
	10	973.374	32.15199 - 134.00754	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	2-3		893
	0	974.915	17.27370 - 119.04667	$3d^2 - 3d^2(7^2)4p$	$^3H - ^3F$	4-3		893
	90	977.009	49.76065 - 152.09721	$3d^2 - 3d^2(7^2)4p$	$^3G - ^3F$	4-3		893
	10	984.54	17.85118 - 119.42142	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3F$	2-2		490
	10	984.95	.57008 - 102.10076	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	4-4		490
	4	985.109	17.39692 - 118.90053	$3d^2 - 3d^2(7^2)4p$	$^3H - ^3G$	5-4		393
	10	986.250	16.77136 - 118.14515	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3D$	0-1		893
	60	987.530	.18316 - 101.44497	$3d^2 - 3d^2(7^2)4p$	$^3D - ^3F$	2-2		893
	10	987.611	17.14656 - 118.42209	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3D$	1-2		893
	120	992.972	17.85118 - 118.99911	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3D$	2-3		893
	20	994.08						490
	40	994.313	17.85118 - 118.42209	$3d^2 - 3d^2(7^2)4p$	$^3P - ^3D$	2-2		893

Subjected to	L <sub>c</sub> (in A)	Length (in m <sup>2</sup> cm <sup>-1</sup> )	Configurations	Terms	J-J	Notes	References
130	906.804	17.53065 - 117.60299	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> g	d <sup>+</sup> H - <sup>+</sup> H	6-7		805
10	906.50	32.15199 - 132.69976	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> D - <sup>+</sup> D	2-2		490
130	999.882	17.59692 - 117.68895	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	5-6		805
150	999.363	20.78064 - 120.79226	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> G - <sup>+</sup> G	3-3		805
26	999.541	20.78064 - 120.79955	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> G - <sup>+</sup> G	3-4		805
130	999.837	18.58239 - 118.59911	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	4-3		805
19	1000.291	18.65184 - 118.63299	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	2-2		805
40	1000.421	17.53065 - 117.60895	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	6-6		805
120	1000.813	32.15199 - 132.69871	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> D - <sup>+</sup> D	2-2		805
130	1000.882	18.51118 - 118.62299	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	3-2		805
130	1001.893	20.83295 - 120.79955	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> G - <sup>+</sup> G	4-4		805
120	1001.277	17.27370 - 117.64985	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	4-5		805
26	1001.531	20.83295 - 120.79827	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> G - <sup>+</sup> G	4-5		805
40	1002.489	20.96604 - 120.79955	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> G - <sup>+</sup> G	5-4		805
25	1002.518	17.29692 - 117.64985	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	5-5		805
200	1002.872	18.65184 - 118.64815	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	2-1		805
200	1002.964	20.59604 - 120.79827	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> G - <sup>+</sup> G	5-5		805
19	1003.213	16.57736 - 116.65119	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> F	0-1		805
90	1003.37						805
90	1003.220	17.14605 - 116.65119	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> F	1-1		805
4	1003.647	20.78064 - 119.84647	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> G - <sup>+</sup> H	3-3		805
4	1003.810	17.85118 - 116.73085	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	2-2		805
1	1003.888	17.85118 - 116.73080	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	2-1		805
4	1004.031	20.59604 - 119.84200	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> G - <sup>+</sup> H	5-5		805
130	1004.193	17.85118 - 116.65119	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> F	2-1		805
40	1005.807	17.85118 - 116.37292	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> F	2-1		805
40	1005.644	18.51118 - 116.56809	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> H	3-3		805
90	1005.770	17.29692 - 115.84458	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	5-6		805
130	1006.295	17.27370 - 115.67074	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	4-5		805
18	1006.405	18.58239 - 116.86809	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> H	4-3		805
25	1006.983	18.65184 - 116.73085	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	2-2		805
40	1007.064	18.65184 - 116.73080	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	2-1		805
900	1007.148	17.53065 - 115.84458	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	6-6		805
300	1007.304	17.27370 - 115.57196	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	4-4		805
400	1007.544	17.29692 - 115.67074	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	5-5		805
9	1008.594	17.29692 - 115.57196	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	5-4		805
9	1008.942	17.53065 - 115.67074	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> H - <sup>+</sup> H	6-5		805
10	1009.60	18.65184 - 116.53295	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	2-3		490
4	1009.914	20.83295 - 118.59053	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> G - <sup>+</sup> G	4-4		805
40	1020.181	18.51118 - 116.53295	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	3-3		805
40	1020.273	17.14605 - 115.18215	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	1-2		805
130	1020.979	18.58239 - 116.53295	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	4-3		805
18	1021.029	18.65184 - 116.39166	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> F	2-3		805
4	1021.230	18.65184 - 116.37292	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> F	2-1		805
130	1021.642	18.51118 - 116.39166	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> H	3-2		805
40	1021.512	17.85118 - 115.55428	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	2-3		805
40	1025.37	17.14605 - 114.71679	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	1-1		805
200	1025.433	18.518 - 97.64399	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> D - <sup>+</sup> D	2-3		805
120	1026.349	17.14605 - 114.59914	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> F	1-2		805
120	1027.434	35455 - 97.48399	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> D - <sup>+</sup> D	3-3		805
3	1028.336	1022 - 97.30659	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> D - <sup>+</sup> D	1-2		805
120	1029.567	16.77336 - 113.89943	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> H	0-1		805
40	1029.785	57608 - 97.64399	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> D - <sup>+</sup> D	4-3		805
120	1029.835	18.65184 - 115.55428	3d <sup>+</sup> -3d <sup>+</sup> (D) <sub>3</sub> p	d <sup>+</sup> F - <sup>+</sup> D	2-3		805

CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J-J	Notes	Reference
3	150	1030.002	0 - 97.07796	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	0-1		893
2	400	1030.461	57008 - 97.82948	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-5		893
3	40	1030.762	.0622 - 97.07796	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	1-1		893
2	150	1030.800	35635 - 97.39901	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-4		893
	120	1031.239	18.58339 - 115.53428	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	4-3		893
3	90	1031.466	35635 - 97.30659	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-2		893
2	10	1031.506	.18316 - 97.12142	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	2-3		893
3	25	1032.053	.18316 - 97.07796	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	2-1		893
1	60	1032.421	.0622 - 96.92202	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	1-2		893
2	350	1033.228	57008 - 97.39901	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-4		893
1	90	1033.339	0 - 96.77438	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	0-1		893
2	350	1033.433	35635 - 97.12142	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-3		893
	150	1033.606	17.85118 - 114.99914	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	2-2		893
1	300	1033.693	35635 - 97.00028	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-4		893
	90	1033.807	18.45184 - 115.10215	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	2-2		893
1	150	1033.996	.0622 - 96.77438	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	1-1		893
	120	1034.199	17.10236 - 113.06447	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	1-0		893
	120	1034.428	18.51118 - 115.10215	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	3-2		893
1	150	1034.853	.0622 - 96.60997	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	1-0		893
	60	1035.031	25.70094 - 122.39649	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	2-1		893
	40	1035.212	17.16836 - 113.76713	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	1-2		893
1	250	1035.281	.18316 - 96.77438	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	2-1		893
1	250	1035.565	35635 - 96.92202	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-2		893
2	200	1035.785	57008 - 97.12142	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-3		893
1	350	1035.938	.18316 - 96.71404	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	2-3		893
1	350	1036.035	57008 - 97.00028	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-4		893
	250	1036.334	20.99604 - 117.10158	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	5-6		893
1	250	1037.007	35635 - 96.71404	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-3		893
2	300	1038.163	.0622 - 96.30631	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	1-2		893
24	90	1038.794	20.70364 - 116.96909	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-3		893
24	60	1038.976	20.85295 - 117.10158	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-4		893
	20	1039.40						897
2	150	1040.046	0 - 96.14925	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	0-1		893
1	150	1040.173	57608 - 96.71404	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-3		893
24	150	1040.410	20.85295 - 116.96909	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-3		893
24	250	1040.521	20.99604 - 117.10158	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	5-4		893
2	40	1040.723	.0622 - 96.14925	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	1-1		893
	120	1040.811	20.70364 - 116.78205	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-2		893
	90	1041.135	17.85118 - 113.09943	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	2-1		893
2	120	1041.345	35635 - 96.30631	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-2		893
2	40	1042.036	.18316 - 95.14925	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	2-1		893
	40	1042.578	17.85118 - 113.76713	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	2-2		893
	60	1042.866	17.53065 - 113.41993	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	6-5		893
	40	1043.309	17.27370 - 113.11521	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-4		893
	25	1043.529	20.70364 - 116.53295	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-3		893
	60	1044.729	17.39692 - 113.11521	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	5-4		893
	400	1045.06	20.70364 - 116.39166	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	3-2		490
	150	1045.150	20.85295 - 116.53295	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-3		893
	1	1045.306	25.70094 - 121.44677	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	2-1		893
	60	1045.719	25.13087 - 120.76726	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-3		893
	25	1047.061	17.85118 - 113.35706	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	2-2		893
	25	1049.192	18.45184 - 113.76713	$3d^2 - 3d^2(7)4p$	$^3P - ^3D$	2-2		893
	60	1050.494	17.27370 - 112.46701	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-3		893
	40	1051.532	17.27370 - 112.37288	$3d^2 - 3d^2(7)4p$	$^3D - ^3P$	4-4		893

CR II - Continued

Multiplet	Rel. Int.	$\lambda_c$ (in Å)	Levels (in $\text{cm}^{-1}$ )	Configurations	Terms	J-J	Notes	References	
	120	1051.905	37.00516 - 132.00071	$3d^2 - 3d^2(7)4p$	$^3F - ^3D$	3-2		093	
	40	1052.365	27.37232 - 122.39669	$3d^2 - 3d^2(7)4p$	$^3S - ^3P$	0-1		093	
	25	1052.901	17.39002 - 112.37208	$3d^2 - 3d^2(7)4p$	$^3H - ^3F$	5-4		093	
	40	1054.000	10.45100 - 112.32000	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	2-3		093	
	60	1054.095	20.70044 - 115.57196	$3d^2 - 3d^2(7)4p$	$^3G - ^3H$	3-4		093	
	120	1054.313	20.99000 - 115.00050	$3d^2 - 3d^2(7)4p$	$^3G - ^3H$	5-6		093	
	4	1054.451	10.58339 - 113.01993	$3d^2 - 3d^2(7)4p$	$^3F - ^3H$	4-5		093	
	150	1054.605	20.85295 - 115.67096	$3d^2 - 3d^2(7)4p$	$^3G - ^3H$	4-5		093	
	25	1055.699	10.58339 - 113.32000	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	4-3		093	
	25	1055.763	20.85295 - 115.57196	$3d^2 - 3d^2(7)4p$	$^3G - ^3H$	4-4		093	
	400	1055.885	25.13007 - 119.00667	$3d^2 - 3d^2(7)4p$	$^3G - ^3H$	4-3		093	
	120	1056.151	26.00409 - 120.70027	$3d^2 - 3d^2(7)4p$	$^3I - ^3G$	6-5		093	
	40	1056.250	20.99000 - 115.67096	$3d^2 - 3d^2(7)4p$	$^3G - ^3H$	5-5		093	
	1	1057.043	10.51110 - 113.11521	$3d^2 - 3d^2(7)4p$	$^3H - ^3G$	3-4		093	
	5	1057.50	17.27370 - 111.00007	$3d^2 - 3d^2(7)4p$	$^3H - ^3G$	4-5		093	
	200	1057.840	10.58339 - 113.11521	$3d^2 - 3d^2(7)4p$	$^3F - ^3G$	4-4		093	
	3	1058.63	17.39002 - 111.00007	$3d^2 - 3d^2(7)4p$	$^3H - ^3G$	5-5		097	
	350	1059.116	26.00409 - 120.63259	$3d^2 - 3d^2(7)4p$	$^3I - ^3F$	6-6		093	
8	400	1060.150	17.53065 - 111.05097	$3d^2 - 3d^2(7)4p$	$^3H - ^3G$	6-5		093	
8	350	1061.005	17.39002 - 111.64676	$3d^2 - 3d^2(7)4p$	$^3H - ^3G$	5-4		093	
	1	1062.475	25.72644 - 119.00667	$3d^2 - 3d^2(7)4p$	$^3D - ^3F$	3-3		093	
8	300	1062.680	17.27370 - 111.37009	$3d^2 - 3d^2(7)4p$	$^3H - ^3G$	4-3		093	
	40	1063.009	25.70094 - 119.00667	$3d^2 - 3d^2(7)4p$	$^3D - ^3F$	2-3		093	
17	40	1063.663	10.45100 - 112.06701	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	2-3		093	
17	300	1064.326	10.51110 - 112.06701	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	3-3		093	
17	300	1064.422	10.45100 - 112.39904	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	2-2		093	
17	90	1065.005	10.51110 - 112.39904	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	3-2		093	
17	90	1065.152	10.58339 - 112.06701	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	4-3		093	
17	40	1065.398	10.51110 - 112.37208	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	3-4		093	
17	350	1066.213	10.58339 - 112.37208	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	4-4		093	
	90	1066.356	25.04031 - 119.62562	$3d^2 - 3d^2(7)4p$	$^3D - ^3F$	1-0		093	
	90	1066.531	25.13007 - 119.00053	$3d^2 - 3d^2(7)4p$	$^3G - ^3G$	4-4		093	
	120	1067.145	25.70094 - 119.00002	$3d^2 - 3d^2(7)4p$	$^3D - ^3F$	2-1		093	
	150	1067.209	25.72644 - 119.42142	$3d^2 - 3d^2(7)4p$	$^3D - ^3F$	3-2		093	
	120	1067.910	25.70094 - 119.42142	$3d^2 - 3d^2(7)4p$	$^3D - ^3F$	2-2		093	
	400	1068.401	26.00409 - 119.61200	$3d^2 - 3d^2(7)4p$	$^3I - ^3H$	6-5		093	
	1	1069.602	25.04031 - 119.42142	$3d^2 - 3d^2(7)4p$	$^3D - ^3F$	1-2		093	
	20	1069.65						490	
	60	1069.979	25.13007 - 118.99911	$3d^2 - 3d^2(7)4p$	$^3G - ^3D$	4-3		093	
	30	1070.55	35655 - 93.70621	$3d^2 - 3d^2(7)4p$	$^3D - ^3G$	3-2		490	
16	200	1072.114	10.58339 - 111.05097	$3d^2 - 3d^2(7)4p$	$^3F - ^3G$	4-5		093	
16	150	1073.727	10.51110 - 111.64676	$3d^2 - 3d^2(7)4p$	$^3F - ^3G$	3-4		093	
	10	1073.993	17.39002 - 110.50710	$3d^2 - 3d^2(7)4p$	$^3H - ^3H$	5-6		093	
16	60	1074.546	10.58339 - 111.64676	$3d^2 - 3d^2(7)4p$	$^3F - ^3G$	4-4		093	
16	150	1076.147	10.45100 - 111.37009	$3d^2 - 3d^2(7)4p$	$^3F - ^3G$	2-3		093	
	25	1076.641	17.27370 - 110.15009	$3d^2 - 3d^2(7)4p$	$^3H - ^3D$	4-4		093	
32	120	1076.746	25.72644 - 118.99911	$3d^2 - 3d^2(7)4p$	$^3D - ^3D$	3-3		093	
16	10	1076.833	10.51110 - 111.37009	$3d^2 - 3d^2(7)4p$	$^3F - ^3G$	3-3		093	
	32	10	1077.370	25.70094 - 118.99911	$3d^2 - 3d^2(7)4p$	$^3D - ^3D$	2-3		093
	10	1077.590	16.77136 - 109.57063	$3d^2 - 3d^2(7)4p$	$^3F - ^3F$	0-1		093	
	40	1078.794	25.72644 - 118.42299	$3d^2 - 3d^2(7)4p$	$^3D - ^3D$	3-2		093	
	32	120	1079.423	25.70094 - 118.42299	$3d^2 - 3d^2(7)4p$	$^3D - ^3D$	2-2		093
	120	1079.97						490	
32	10	1080.211	25.04031 - 118.42299	$3d^2 - 3d^2(7)4p$	$^3D - ^3D$	1-2		093	

CM - Continued

Reference	1 - J	Notes	Terms	Configurations	Levels (in $W^2 \text{ cm}^{-1}$ )	$\lambda$ (in Å)	Wavelength (in Å)	31
093	6-5		"F - F"	$M^+ - M^+(D)_{1/2}$	17.5365 - 109.9498	1082.088	159	
093	1-1		"F - F"	$M^+ - M^+(D)_{1/2}$	17.1656 - 109.5762	1082.231	25	32
093	2-1		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7894 - 116.16515	1082.044	25	32
093	1-1		"D - D"	$M^+ - M^+(D)_{1/2}$	25.8821 - 116.16515	1082.230	50	32
093	1-1		"F - F"	$M^+ - M^+(D)_{1/2}$	17.2750 - 109.5325	1083.22	20	
093	4-4		"F - F"	$M^+ - M^+(D)_{1/2}$	17.2750 - 109.5325	1083.889	10	
093	5-4		"F - F"	$M^+ - M^+(D)_{1/2}$	17.2750 - 109.5325	1084.26	20	
093	5-4		"F - F"	$M^+ - M^+(D)_{1/2}$	17.2750 - 109.5325	1085.34	40	
093	20		"F - F"	$M^+ - M^+(D)_{1/2}$	17.2750 - 109.5325	1084.88	20	
093	20		"F - F"	$M^+ - M^+(D)_{1/2}$	17.2750 - 109.5325	1085.96	20	
093	20		"F - F"	$M^+ - M^+(D)_{1/2}$	17.2750 - 109.5325	1087.30	10	
093	20		"F - F"	$M^+ - M^+(D)_{1/2}$	17.2750 - 109.5325	1088.28	10	
093	20		"F - F"	$M^+ - M^+(D)_{1/2}$	16.7136 - 108.2289	1093.17	50	31
093	0-1		"F - F"	$M^+ - M^+(D)_{1/2}$	25.7664 - 117.1828	1084.387	150	31
093	3-4		"F - F"	$M^+ - M^+(D)_{1/2}$	18.5839 - 109.9498	1084.557	60	31
093	3-3		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7664 - 116.9889	1085.283	40	31
093	2-3		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7664 - 116.9889	1086.64	150	31
093	2-1		"F - F"	$M^+ - M^+(D)_{1/2}$	65.7821 - 156.9293	1096.899	120	31
093	4-3		"F - F"	$M^+ - M^+(D)_{1/2}$	18.5839 - 109.7229	1097.25	100	
093	2-2		"F - F"	$M^+ - M^+(D)_{1/2}$	17.8518 - 108.9729	1097.638	60	
093	3-2		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7664 - 116.7825	1098.231	60	
093	3-4		"F - F"	$M^+ - M^+(D)_{1/2}$	18.5118 - 109.5325	1098.626	40	
093	2-1		"D - D"	$M^+ - M^+(D)_{1/2}$	17.8518 - 108.8628	1098.780	25	
093	2-2		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7894 - 116.7825	1098.888	120	
093	2-1		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7894 - 116.7825	1098.989	60	
093	2-1		"D - D"	$M^+ - M^+(D)_{1/2}$	32.1579 - 123.1828	1099.454	150	
093	1-1		"D - D"	$M^+ - M^+(D)_{1/2}$	25.8821 - 116.7400	1099.882	50	
093	5-5		"D - D"	$M^+ - M^+(D)_{1/2}$	20.9704 - 111.8397	1100.585	200	
093	3-3		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7894 - 116.5295	1101.247	50	
093	4-4		"D - D"	$M^+ - M^+(D)_{1/2}$	20.8529 - 111.6476	1101.622	250	
093	2-3		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7894 - 116.5295	1101.907	120	
093	2-3		"D - D"	$M^+ - M^+(D)_{1/2}$	20.7064 - 111.3769	1102.809	200	
093	2-2		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7894 - 116.3916	1103.630	25	
093	1-1		"D - D"	$M^+ - M^+(D)_{1/2}$	25.8821 - 116.3916	1103.727	4	
093	1-2		"D - D"	$M^+ - M^+(D)_{1/2}$	25.8821 - 116.3916	1104.666	150	
093	4-3		"D - D"	$M^+ - M^+(D)_{1/2}$	20.8529 - 111.3769	1104.672	60	
093	4-4		"D - D"	$M^+ - M^+(D)_{1/2}$	25.1307 - 115.9796	1105.797	50	
093	2-1		"D - D"	$M^+ - M^+(D)_{1/2}$	112.68	1108.888	200	
093	10		"D - D"	$M^+ - M^+(D)_{1/2}$	112.68	1112.265	250	
093	25		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7894 - 115.9528	1113.265	250	
093	25		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7894 - 115.9528	1113.921	25	
093	250		"D - D"	$M^+ - M^+(D)_{1/2}$	20.9704 - 110.90718	1117.174	250	
093	60		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7664 - 115.18215	1117.807	60	
093	250		"D - D"	$M^+ - M^+(D)_{1/2}$	25.7664 - 115.18215	1118.541	250	
093	25		"D - D"	$M^+ - M^+(D)_{1/2}$	25.8821 - 115.18215	1119.400	25	
093	25		"D - D"	$M^+ - M^+(D)_{1/2}$	32.1579 - 121.46077	1119.892	25	
093	90		"D - D"	$M^+ - M^+(D)_{1/2}$	65.3217 - 132.0978	1121.309	90	
093	150		"D - D"	$M^+ - M^+(D)_{1/2}$	20.8529 - 109.9498	1122.43	150	

CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J-J	Notes	References
30	90	1122.870	43.44199 - 132.49978	$3d^2 - 3d^2(a^2F)4p$	$b^2P - ^1D'$	2-2		893
	30	1123.37	28.78964 - 109.72279	$3d^2 - 3d^2(a^2F)4p$	$a^2G - ^1D'$	3-3		490
	150	1123.587	27.37232 - 116.37292	$3d^2 - 3d^2(a^2D)4p$	$a^2S - ^1F'$	0-1		893
	40	1124.405	25.78094 - 114.71679	$3d^2 - 3d^2(a^2F)4p$	$a^2D - ^1D'$	2-1		893
	30	1125.257	25.84831 - 114.71679	$3d^2 - 3d^2(a^2F)4p$	$a^2D - ^1D'$	1-1		893
22	300	1125.736	28.78964 - 109.53425	$3d^2 - 3d^2(a^2G)4p$	$a^2G - ^1F'$	3-4		893
	90	1125.902	25.78094 - 114.99914	$3d^2 - 3d^2(a^2F)4p$	$a^2D - ^1F'$	2-2		893
	10	1126.35						490
	250	1127.706	43.44199 - 132.11750	$3d^2 - 3d^2(a^2F)4p$	$b^2P - ^1D'$	2-3		893
	90	1128.757	44.14136 - 132.73422	$3d^2 - 3d^2(a^2F)4p$	$b^2P - ^1D'$	0-1		893
	120	1128.878	43.91609 - 132.49978	$3d^2 - 3d^2(a^2F)4p$	$b^2P - ^1D'$	1-2		893
	150	1131.90						490
	150	1132.742	25.13087 - 113.41993	$3d^2 - 3d^2(a^2G)4p$	$a^2G - ^1F'$	4-5		893
	90	1133.913	25.13087 - 113.32880	$3d^2 - 3d^2(a^2G)4p$	$a^2G - ^1F'$	4-3		893
	60	1134.256	43.28671 - 131.45065	$3d^2 - 3d^2(a^2F)4p$	$b^2F - ^1G'$	4-5		893
	90	1136.535	25.78094 - 113.76713	$3d^2 - 3d^2(a^2F)4p$	$a^2D - ^1D'$	2-2		893
	400	1136.666	25.13087 - 113.11521	$3d^2 - 3d^2(a^2G)4p$	$a^2G - ^1G'$	4-4		893
	10	1136.91						490
	90	1137.091	43.32217 - 131.26566	$3d^2 - 3d^2(a^2F)4p$	$b^2F - ^1G'$	3-4		893
	10	1137.408	25.84831 - 113.76713	$3d^2 - 3d^2(a^2F)4p$	$a^2D - ^1D'$	1-2		893
	90	1138.797	43.30453 - 131.11636	$3d^2 - 3d^2(a^2F)4p$	$b^2F - ^1G'$	2-3		893
	10	1139.024	43.32217 - 131.11636	$3d^2 - 3d^2(a^2F)4p$	$b^2F - ^1G'$	3-3		893
	10	1141.155	25.72644 - 113.35704	$3d^2 - 3d^2(a^2F)4p$	$a^2D - ^1S'$	3-2		893
	25	1142.226	25.78094 - 113.32880	$3d^2 - 3d^2(a^2G)4p$	$a^2D - ^1F'$	2-3		893
	150	1143.61						490
	250	1144.096	26.01489 - 113.41993	$3d^2 - 3d^2(a^2G)4p$	$a^2I - ^1F'$	6-5		893
	200	1144.308	25.72644 - 113.11521	$3d^2 - 3d^2(a^2G)4p$	$a^2D - ^1G'$	3-4		893
	300	1146.335	25.13087 - 112.37288	$3d^2 - 3d^2(a^2G)4p$	$a^2G - ^1F'$	4-4		893
29	40	1152.859	25.72644 - 112.46701	$3d^2 - 3d^2(a^2G)4p$	$a^2D - ^1F'$	3-3		893
29	200	1153.580	25.78094 - 112.46701	$3d^2 - 3d^2(a^2G)4p$	$a^2D - ^1F'$	2-3		893
29	200	1154.109	25.72644 - 112.37288	$3d^2 - 3d^2(a^2G)4p$	$a^2D - ^1F'$	3-4		893
29	25	1154.679	25.78094 - 112.39984	$3d^2 - 3d^2(a^2G)4p$	$a^2D - ^1F'$	2-2		893
29	50	1155.378	25.84831 - 112.39984	$3d^2 - 3d^2(a^2G)4p$	$a^2D - ^1F'$	1-2		893
	4	1155.710	27.37232 - 113.89943	$3d^2 - 3d^2(a^2F)4p$	$a^2S - ^1F'$	0-1		893
	20	1156.42						490
	25	1159.096	65.76321 - 152.03721	$3d^2 - 3d^2(b^2D)4p$	$b^2D - ^1F'$	2-3		893
	350	1161.428	37.00516 - 123.10584	$3d^2 - 3d^2(a^2D)4p$	$a^2F - ^1D'$	3-2		893
	10	1162.610	32.15199 - 118.16515	$3d^2 - 3d^2(a^2D)4p$	$a^2D - ^1D'$	2-1		893
	10	1166.23						490
	25	1168.292	25.78094 - 111.37609	$3d^2 - 3d^2(a^2G)4p$	$a^2D - ^1G'$	2-3		893
	120	1168.726	43.28671 - 128.85049	$3d^2 - 3d^2(a^2F)4p$	$b^2F - ^1F'$	4-4		893
	25	1169.208	43.32217 - 128.85049	$3d^2 - 3d^2(a^2F)4p$	$b^2F - ^1F'$	3-4		893
	90	1170.111	43.32217 - 128.78413	$3d^2 - 3d^2(a^2F)4p$	$b^2F - ^1F'$	3-3		893
	90	1170.273	43.30453 - 128.75462	$3d^2 - 3d^2(a^2F)4p$	$b^2F - ^1F'$	2-2		893
	30	1170.64						490
	40	1173.19						490
	50	1173.34						490
	100	1173.77						490
	300	1174.825	49.76465 - 134.88754	$3d^2 - 3d^2(a^2F)4p$	$b^2G - ^1F'$	4-3		893
	30	1178.55						490
	20	1178.80						490
	10	1178.99	32.15199 - 116.96909	$3d^2 - 3d^2(a^2D)4p$	$a^2D - ^1F'$	2-3		490
	30	1179.68						490
	4	1180.579	17.39492 - 102.10076	$3d^2 - 3d^2(a^2F)4p$	$a^2H - ^1F'$	5-4		893

CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J-J	Notes	Reference
	60	1180.81						490
	10	1181.03						490
	10	1181.45						490
	30	1181.63	32.15199 - 116.78205	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	2-2		490
	90	1181.723	32.15199 - 116.77480	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	2-1		493
	120	1186.254	32.15199 - 116.45119	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	2-1		493
	130	1187.330	32.15199 - 116.37292	$3d^2 - 3d^2(^1D)4p$	$a^1D - ^1D'$	2-1		493
	230	1187.637	49.76865 - 133.96957	$3d^2 - 3d^2(^1P)4p$	$b^1G - ^1G'$	4-4		493
	150	1192.686	25.72644 - 109.57089	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	3-2		493
	200	1193.466	25.78094 - 109.57062	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	2-1		493
	10	1193.89	63.17430 - 146.93618	$3d^2(^1P)4s - 3d^2(^1D)4p$	$^1P - ^1D'$	2-1		490
	30	1194.44	25.84831 - 109.57062	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	1-1		490
	30	1194.96						490
	10	1195.42						490
	30	1196.84	25.84831 - 109.45811	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	1-0		490
	90	1196.328	18.51118 - 102.10076	$3d^2 - 3d^2(^1P)4p$	$a^1F - ^1F'$	3-4		493
	150	1197.365	18.58339 - 102.10076	$3d^2 - 3d^2(^1P)4p$	$a^1F - ^1F'$	4-4		493
	10	1197.60						490
	70	1198.31	65.89238 - 149.34403	$3d^2(^1G)4s - 3d^2(^1D)4p$	$^1G - ^1D'$	3-2		490
	120	1200.567	18.45184 - 101.74621	$3d^2 - 3d^2(^1P)4p$	$a^1F - ^1F'$	2-3		493
	50	1200.91						490
	50	1201.00						490
	400	1201.247	25.72644 - 108.97290	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	3-2		493
	300	1201.426	18.51118 - 101.74621	$3d^2 - 3d^2(^1P)4p$	$a^1F - ^1F'$	3-3		493
	60	1202.043	25.78094 - 108.97290	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	2-2		493
	120	1202.460	18.58339 - 101.74621	$3d^2 - 3d^2(^1P)4p$	$a^1F - ^1F'$	4-3		493
	150	1203.604	25.78094 - 108.86498	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	2-1		493
	20	1203.95						490
	1	1204.375	32.15199 - 115.18215	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	2-2		493
	90	1204.440	17.39692 - 100.42301	$3d^2 - 3d^2(^1P)4p$	$a^1H - ^1G'$	5-5		493
	60	1204.580	25.84831 - 108.86498	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	1-1		493
	300	1204.929	18.45184 - 101.44457	$3d^2 - 3d^2(^1P)4p$	$a^1F - ^1F'$	2-2		493
	10	1205.15						490
	120	1205.787	18.51118 - 101.44457	$3d^2 - 3d^2(^1P)4p$	$a^1F - ^1F'$	3-2		493
	10	1206.12						490
	570	1206.381	17.53065 - 100.42301	$3d^2 - 3d^2(^1P)4p$	$a^1H - ^1G'$	6-5		493
	30	1206.70	49.62825 - 132.49978	$3d^2(^1F)4s - 3d^2(^1F)4p$	$^1F - ^1D'$	2-2		490
	200	1206.99	25.84831 - 108.69763	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	1-0		490
	200	1207.017	25.84831 - 108.69763	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	1-0		493
	200	1207.124	37.00516 - 119.84647	$3d^2 - 3d^2(^1D)4p$	$a^1F - ^1F'$	3-3		493
	90	1207.340	17.27370 - 100.10066	$3d^2 - 3d^2(^1P)4p$	$a^1H - ^1G'$	4-4		493
	350	1207.580	65.76321 - 148.57381	$3d^2 - 3d^2(^1D)4p$	$b^1D - ^1D'$	2-2		493
	25	1208.684	25.72644 - 108.46140	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	3-2		493
	500	1209.133	17.39692 - 100.10066	$3d^2 - 3d^2(^1P)4p$	$a^1H - ^1G'$	5-4		493
	10	1209.42	65.89238 - 148.57381	$3d^2(^1G)4s - 3d^2(^1D)4p$	$^1G - ^1D'$	3-2		490
	10	1209.66	49.82891 - 132.49978	$3d^2(^1F)4s - 3d^2(^1F)4p$	$^1F - ^1D'$	3-2		490
	400	1211.123	17.27370 - 99.84167	$3d^2 - 3d^2(^1P)4p$	$a^1H - ^1G'$	4-3		493
	10	1211.84						490
	50	1212.98	49.62825 - 132.07071	$3d^2(^1F)4s - 3d^2(^1F)4p$	$^1F - ^1D'$	2-2		490
	50	1213.51	25.84831 - 108.25089	$3d^2 - 3d^2(^1P)4p$	$a^1D - ^1D'$	1-1		490
	10	1213.82						490
	100	1218.40						490
	50	1218.89						490
	50	1219.55						490



## CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J-J	Notes	References
14	200	1220.14	37.00516 - 118.90053	$3d^4 - 3d^3(n^2D)4p$	$a^4F - ^4G^o$	3-4		490
	350	1221.076						
	10	1221.45						
	400	1221.908						
	25	1223.266						
	30	1224.43	18.58339 - 100.42301 32.15199 - 113.89943	$3d^4 - 3d^3(n^2F)4p$	$a^4F - ^4G^o$	4-5	493	
	25	1223.266						
	30	1224.43						
	300	1225.02						
	300	1225.263						
150	1225.32	18.51118 - 100.10066	$3d^4 - 3d^3(n^2F)4p$	$a^4D - ^4D^o$	2-2	490		
300	1225.445							
10	1226.18							
14	1226.735							
14	1226.735							
20	1227.11	27.57232 - 108.86498	$3d^4 - 3d^3(n^2F)4p$	$a^4S - ^4D^o$	0-1	490		
10	1228.03							
10	1228.37							
14	1228.647							
14	1229.552							
10	1230.35	18.45184 - 99.84167 18.51118 - 99.84167	$3d^4 - 3d^3(n^2F)4p$	$a^4F - ^4G^o$	2-3	493		
10	1230.35							
10	1230.49							
21	1230.802							
21	1230.802							
50	1231.878	20.85295 - 102.10076 32.15199 - 113.32880 20.99604 - 102.10076	$3d^4 - 3d^3(n^2G)4p$	$a^4G - ^4F^o$	4-4	493		
50	1231.878							
570	1232.975							
10	1233.28							
21	1233.919							
200	1233.919	20.70364 - 101.74621	$3d^4 - 3d^3(n^2F)4p$	$a^4G - ^4F^o$	3-3	493		
21	1233.919							
500	1236.197							
40	1236.424							
10	1236.51							
10	1236.71	20.70364 - 101.74621 27.37232 - 108.25089 70.98126 - 151.85212	$3d^4 - 3d^3(n^2F)4p$	$a^4G - ^4F^o$	4-3	493		
10	1236.71							
10	1236.71							
400	1238.529							
20	1241.32							
10	1242.08	20.70364 - 101.74621 17.27370 - 97.68399	$3d^4 - 3d^3(n^2F)4p$	$a^4G - ^4F^o$	3-2	493		
20	1243.43							
25	1243.627							
40	1243.97							
10	1244.41							
100	1244.58	17.27370 - 97.61948	$3d^4 - 3d^3(n^2F)4p$	$a^4H - ^4D^o$	4-3	490		
100	1244.58							
90	1245.097							
200	1245.231							
100	1246.83							
6	1246.83	17.16856 - 97.30659 17.53065 - 97.61948	$3d^4 - 3d^3(n^2D)4p$	$a^4D - ^4F^o$	0-1	493		
6	1246.83							
350	1247.846							
90	1248.621							
20	1250.33							
20	1250.57	17.39692 - 97.35981 17.16856 - 97.07796 17.85118 - 97.68399	$3d^4 - 3d^3(n^2D)4p$	$a^4H - ^4F^o$	5-4	490		
20	1250.57							
250	1251.424							
6	1252.616							
5	1253.87							
20	1256.066	17.16856 - 96.92202	$3d^4 - 3d^3(n^2F)4p$	$a^4P - ^4D^o$	1-2	493		
20	1256.066							
20	1256.066							
20	1256.754							
150	1256.754							
6	1258.568	20.85295 - 100.42301	$3d^4 - 3d^3(n^2F)4p$	$a^4G - ^4G^o$	4-5	493		
6	1258.568							
250	1258.568							
20	1259.014							
20	1259.467							
20	1259.467	17.85118 - 97.30659 20.99604 - 100.42301 20.70364 - 100.10066 16.77136 - 96.14925	$3d^4 - 3d^3(n^2D)4p$	$a^4P - ^4D^o$	2-2	493		
20	1259.467							
250	1259.794							
20	1261.53							
20	1261.53							
20	1261.844	17.85118 - 97.12142 20.85295 - 100.10066	$3d^4 - 3d^3(n^2F)4p$	$a^4P - ^4F^o$	2-3	490		
20	1261.844							
570	1259.014							
400	1259.467							
250	1259.794							
20	1261.53	17.85118 - 97.12142 20.85295 - 100.10066	$3d^4 - 3d^3(n^2F)4p$	$a^4G - ^4G^o$	4-4	493		
20	1261.53							
20	1261.844							
570	1259.014							
400	1259.467							

## CR III - Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
6	40	1262.229	17.85118 - 97.07796	$3d^2 - 3d^2(nF)4p$	$a^7P - ^7D$	2 - 1		893
	250	1262.347	17.16856 - 96.38631	$3d^2 - 3d^2(nF)4p$	$a^7P - ^7F$	1 - 2		893
	200	1263.064	18.51118 - 97.68399	$3d^2 - 3d^2(nF)4p$	$a^7P - ^7D$	3 - 3		893
13	300	1263.617	20.70364 - 99.84167	$3d^2 - 3d^2(nF)4p$	$a^6G - ^6G$	3 - 3		893
	350	1264.206	18.58339 - 97.68399	$3d^2 - 3d^2(nF)4p$	$a^6F - ^6D$	4 - 3		893
20	200	1265.239	18.58339 - 97.61948	$3d^2 - 3d^2(nF)4p$	$a^6F - ^6F$	4 - 5		893
	40	1266.000	20.85295 - 99.84167	$3d^2 - 3d^2(nF)4p$	$a^6G - ^6G$	4 - 3		893
13	300	1266.125	17.16856 - 96.14925	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6F$	1 - 1		893
	40	1266.551	43.44199 - 122.39649	$3d^2 - 3d^2(nF)4p$	$b^7P - ^7F$	2 - 1		893
	250	1268.025	17.85118 - 96.71404	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6D$	2 - 3		893
13	60	1268.148	18.45184 - 97.30659	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6D$	2 - 2		893
	400	1269.110	18.51118 - 97.30659	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6D$	3 - 2		893
13	250	1271.839	18.45184 - 97.07796	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6D$	2 - 1		893
	200	1273.312	17.85118 - 96.38631	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6F$	2 - 2		893
	150	1275.34	18.51118 - 96.92202	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6D$	3 - 2		897
	200	1276.76	18.45184 - 96.77438	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6D$	2 - 1		897
	25	1277.174	17.85118 - 96.14925	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6F$	2 - 1		893
12	20	1278.71	18.51118 - 96.71404	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6D$	3 - 3		490
	250	1279.906	18.58339 - 96.71404	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6D$	4 - 3		893
12	1	1281.055	71.32327 - 149.38364	$3d^2(nD)4s - 3d^2(nD)4p$	$^7D - ^7F$	2 - 3		893
	300	1281.977	43.44199 - 121.44677	$3d^2 - 3d^2(nF)4p$	$b^7P - ^7S$	2 - 1		893
	60	1283.132	18.45184 - 96.38631	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6F$	2 - 2		893
	200	1284.103	18.51118 - 96.38631	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6F$	3 - 2		893
	10	1284.46						490
	10	1285.90						490
	400	1287.05	18.45184 - 96.14925	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6F$	2 - 1		490
37	250	1289.824	43.91659 - 121.44677	$3d^2 - 3d^2(nF)4p$	$b^7P - ^7S$	1 - 1		893
	300	1290.940	43.30453 - 120.76726	$3d^2 - 3d^2(nF)4p$	$b^7P - ^6G$	2 - 3		893
37	60	1291.240	43.32217 - 120.76726	$3d^2 - 3d^2(nF)4p$	$b^7P - ^6G$	3 - 3		893
	350	1291.531	43.32217 - 120.74955	$3d^2 - 3d^2(nF)4p$	$b^7P - ^6G$	3 - 4		893
37	400	1291.763	43.28671 - 120.70027	$3d^2 - 3d^2(nF)4p$	$b^7P - ^6G$	4 - 5		893
	200	1293.569	44.14136 - 121.44677	$3d^2 - 3d^2(nF)4p$	$b^7P - ^7S$	0 - 1		893
	40	1296.01						490
	40	1299.56						490
	20	1302.45						490
	4	1302.739	37.00516 - 113.76713	$3d^2 - 3d^2(nF)4p$	$a^6P - ^6D$	3 - 2		893
	5	1302.85	17.27370 - 94.02999	$3d^2 - 3d^2(nF)4p$	$a^6H - ^6G$	4 - 3		490
	40	1303.67						490
	25	1305.088	20.99604 - 97.61948	$3d^2 - 3d^2(nF)4p$	$a^6G - ^6F$	5 - 5		893
	10	1306.168	43.28671 - 119.84647	$3d^2 - 3d^2(nD)4p$	$b^7P - ^7F$	4 - 3		893
	25	1306.679	43.30453 - 119.84647	$3d^2 - 3d^2(nD)4p$	$b^7P - ^7F$	2 - 3		893
	100	1307.24						490
28	10	1307.67						490
	60	1307.64						490
	150	1308.27						490
	350	1309.348	25.72644 - 102.10076	$3d^2 - 3d^2(nF)4p$	$a^6D - ^6F$	3 - 4		893
28	60	1310.179	43.28671 - 119.61200	$3d^2 - 3d^2(nF)4p$	$b^7P - ^7H$	4 - 5		893
	150	1314.968	43.44199 - 119.48902	$3d^2 - 3d^2(nD)4p$	$b^7P - ^7F$	2 - 1		893
28	60	1315.450	25.72644 - 101.74621	$3d^2 - 3d^2(nF)4p$	$a^6D - ^6F$	3 - 3		893
	350	1316.151	43.44199 - 119.62142	$3d^2 - 3d^2(nD)4p$	$b^7P - ^7F$	2 - 2		893
28	300	1316.386	25.78094 - 101.74621	$3d^2 - 3d^2(nF)4p$	$a^6D - ^6F$	2 - 3		893
	60	1320.844	43.91659 - 119.62362	$3d^2 - 3d^2(nD)4p$	$b^7P - ^7F$	1 - 0		893
28	40	1321.639	25.78094 - 101.44457	$3d^2 - 3d^2(nF)4p$	$a^6D - ^6F$	2 - 2		893
	250	1322.819	25.84831 - 101.44457	$3d^2 - 3d^2(nF)4p$	$a^6D - ^6F$	1 - 2		893

## CR III - Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	10	1323.240	43.91699 - 119.48902	$3d^2 - 3d^1(n^2D)4p$	$b^2P - ^2P$	1-1		893
	250	1324.415	43.91699 - 119.42142	$3d^2 - 3d^1(n^2D)4p$	$b^2P - ^2P$	1-2		893
	40	1327.180	44.14136 - 119.48902	$3d^2 - 3d^1(n^2D)4p$	$b^2P - ^2P$	0-1		893
	120	1327.806	43.28671 - 118.59911	$3d^2 - 3d^1(n^2D)4p$	$b^2F - ^2D$	4-3		893
	25	1328.421	43.32217 - 118.59911	$3d^2 - 3d^1(n^2D)4p$	$b^2F - ^2D$	3-3		893
	10	1328.78	18.51118 - 93.76621	$3d^2 - 3d^1(n^2F)4p$	$a^2F - ^2G$	3-2		490
	20	1329.11						490
	20	1329.29						490
	25	1331.224	43.30453 - 118.42299	$3d^2 - 3d^1(n^2D)4p$	$b^2F - ^2D$	2-2		893
	150	1331.543	43.32217 - 118.42299	$3d^2 - 3d^1(n^2D)4p$	$b^2F - ^2D$	3-2		893
	10	1341.17						490
	40	1342.24						490
	100	1345.12						490
	70	1345.46						490
	10	1351.94						490
	10	1354.16						490
36	25	1354.735	43.28671 - 117.10158	$3d^2 - 3d^1(n^2D)4p$	$b^2F - ^2F$	4-4		893
	10	1356.25						490
	20	1356.86						490
36	200	1357.180	43.28671 - 116.96909	$3d^2 - 3d^1(n^2D)4p$	$b^2F - ^2F$	4-3		893
	20	1357.69						490
36	5	1357.85	43.32217 - 116.96909	$3d^2 - 3d^1(n^2D)4p$	$b^2F - ^2F$	3-3		490
	30	1358.65						490
	20	1358.75						490
	60	1360.40						490
	20	1360.56						490
	40	1360.960	43.30453 - 116.78205	$3d^2 - 3d^1(n^2F)4p$	$b^2F - ^2D$	2-2		893
	250	1361.106	43.30453 - 116.77400	$3d^2 - 3d^1(n^2F)4p$	$b^2F - ^2D$	2-1		893
	300	1361.276	43.32217 - 116.78205	$3d^2 - 3d^1(n^2F)4p$	$b^2F - ^2D$	3-2		893
	50	1362.85						490
	20	1363.73	20.70364 - 94.02999	$3d^2 - 3d^1(n^2F)4p$	$a^2G - ^2G$	3-3		490
	50	1364.26						490
	40	1365.06						490
	300	1365.257	43.28671 - 116.53295	$3d^2 - 3d^1(n^2F)4p$	$b^2F - ^2D$	4-3		893
	60	1365.921	43.32217 - 116.53295	$3d^2 - 3d^1(n^2F)4p$	$b^2F - ^2D$	3-3		893
	70	1366.06						490
	120	1366.63						490
	20	1366.88						490
	40	1367.13	43.30453 - 116.45119	$3d^2 - 3d^1(n^2F)4p$	$b^2F - ^2S$	2-1		491
36	20	1368.23	43.30453 - 116.39166	$3d^2 - 3d^1(n^2D)4p$	$b^2F - ^2F$	2-2		490
36	200	1368.563	43.32217 - 116.39166	$3d^2 - 3d^1(n^2D)4p$	$b^2F - ^2F$	3-2		893
	20	1370.20						490
	20	1370.74						490
	60	1372.27						490
	10	1374.91						490
	60	1376.800	44.14136 - 116.77400	$3d^2 - 3d^1(n^2F)4p$	$b^2P - ^2D$	0-1		893
	30	1381.67						490
	100	1382.19						490
35	350	1383.749	43.28671 - 115.55428	$3d^2 - 3d^1(n^2F)4p$	$b^2F - ^2D$	4-3		893
35	60	1384.420	43.32217 - 115.55428	$3d^2 - 3d^1(n^2F)4p$	$b^2F - ^2D$	3-3		893
	10	1385.07						490
	40	1388.13						490
	20	1388.24						490
	70	1389.55	37.00516 - 108.97290	$3d^2 - 3d^1(n^2F)4p$	$a^2F - ^2P$	3-2		400

## CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References	
35	230	1389.699	25.72644 - 97.68399	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	3-3		893	
	120	1390.760	25.78094 - 97.68399	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	2-3		893	
	40	1391.267	43.30453 - 115.18215	$3d^2 - 3d^2(n^2F)4p$	$b^1F - ^1D'$	2-2		893	
	35	230	1391.580	43.32217 - 115.18215	$3d^2 - 3d^2(n^2F)4p$	$b^1F - ^1D'$	3-2		893
		10	1391.78						490
	100	1392.40	49.62825 - 121.44677	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^7F - ^5F$	2-1		490	
	10	1393.00						490	
	10	1393.22						490	
	10	1393.98						490	
	100	1394.33						490	
70	1394.58						490		
10	1396.26						490		
35	100	1396.42						490	
	30	1396.63						490	
	60	1397.033	25.72644 - 97.30659	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	3-2		893	
	30	1397.40						490	
	10	1397.69						490	
	30	1397.90						490	
	130	1398.090	25.78094 - 97.30659	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	2-2		893	
	100	1399.05						490	
	60	1399.415	25.84831 - 97.30659	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	1-2		893	
	25	1400.036	57.42340 - 128.85049	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^7F - ^7F'$	4-4		893	
35	230	1400.316	43.30453 - 114.71679	$3d^2 - 3d^2(n^2F)4p$	$b^1F - ^1D'$	2-1		893	
	10	1400.62	25.72644 - 97.12142	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1F'$	3-3		490	
	10	1400.72						490	
	100	1401.55						490	
	30	1402.07						490	
	10	1402.589	25.78094 - 97.07796	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	2-1		893	
	40	1402.985	43.32217 - 114.59914	$3d^2 - 3d^2(n^2F)4p$	$b^1F - ^1F'$	3-2		893	
	10	1403.200	43.91659 - 115.18215	$3d^2 - 3d^2(n^2F)4p$	$b^1F - ^1D'$	1-2		893	
	70	1403.42						490	
	120	1403.906	25.84831 - 97.07796	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	1-1		893	
10	1404.50						490		
30	1405.37	43.44199 - 114.59914	$3d^2 - 3d^2(n^2F)4p$	$b^1F - ^1F'$	2-2		490		
40	1405.657	25.78094 - 96.92202	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	2-2		893		
20	1405.72	49.62825 - 120.76726	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^7F - ^1G'$	2-3		490		
40	1406.31						490		
10	1407.22						490		
40	1407.89						490		
10	1408.477	49.76065 - 120.76726	$3d^2 - 3d^2(n^2H)4p$	$b^1G - ^1G'$	4-3		893		
120	1408.608	25.72644 - 96.71404	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	3-3		893		
10	1409.10						490		
90	1409.796	25.78094 - 96.71404	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	2-3		893		
20	1410.03	49.82091 - 120.74955	$3d^2(n^2F)4s - 3d^2(n^2H)4p$	$^7F - ^1G'$	3-4		490		
20	1410.82						490		
10	1411.53	25.84831 - 96.69397	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1D'$	1-0		490		
30	1412.67						490		
10	1413.32						490		
40	1413.77						490		
50	1414.62						490		
10	1414.780	43.91659 - 114.59914	$3d^2 - 3d^2(n^2F)4p$	$b^1F - ^1F'$	1-2		893		
60	1415.235	25.72644 - 96.38631	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1F'$	3-2		893		
10	1415.81						490		
90	1416.315	25.78094 - 96.38631	$3d^2 - 3d^2(n^2F)4p$	$a^1D - ^1F'$	2-2		893		

CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J-J	Notes	References
	70	1417.13						490
	25	1417.667	25.84831 - 96.30631	$3d^2 - 3d^1(n^2F)4p$	$a^1D - ^1F$	1-2		493
	10	1419.794	43.44199 - 113.89943	$3d^2 - 3d^1(n^2F)4p$	$b^1P - ^1F$	2-1		493
	100	1420.81						490
	40	1421.091	25.78094 - 96.14925	$3d^2 - 3d^1(n^2F)4p$	$a^1D - ^1F$	2-1		493
	50	1421.20						490
	10	1421.80						490
	40	1422.47	25.84831 - 96.14925	$3d^2 - 3d^1(n^2F)4p$	$a^1D - ^1F$	1-1		490
	10	1422.55						490
	10	1425.30						490
	200	1426.988	49.76865 - 119.84647	$3d^2 - 3d^1(n^2D)4p$	$b^1G - ^1F$	4-3		493
	10	1427.20						490
	10	1427.71	43.28671 - 113.32880	$3d^2 - 3d^1(n^2G)4p$	$b^1F - ^1F$	4-3		490
	10	1428.46	43.32217 - 113.32880	$3d^2 - 3d^1(n^2G)4p$	$b^1F - ^1F$	3-3		490
	50	1429.84						490
	50	1429.17						490
	10	1429.783	43.91659 - 113.86147	$3d^2 - 3d^1(n^2F)4p$	$b^1P - ^1F$	1-0		493
	4	1430.023	49.49246 - 119.42142	$3d^1(n^2F)4s - 3d^1(n^2D)4p$	$^1F - ^1F$	1-2		493
	30	1430.15						490
	50	1430.42						490
	1	1431.620	43.91659 - 113.76713	$3d^2 - 3d^1(n^2F)4p$	$b^1P - ^1D$	1-2		493
	250	1431.758	49.76865 - 119.61280	$3d^2 - 3d^1(n^2F)4p$	$b^1G - ^1F$	4-5		493
	50	1433.26						490
	10	1434.19						490
	20	1436.65						490
	70	1437.17						490
	20	1437.76						490
	10	1438.03						490
	5	1438.90						490
	60	1441.06						490
	50	1441.90						490
	10	1442.78						490
	20	1443.08						490
	60	1443.82						490
	1	1444.305	25.13887 - 94.37629	$3d^2 - 3d^1(n^2F)4p$	$a^1G - ^1G$	4-4		493
	20	1444.84						490
	10	1445.876	43.30453 - 112.46701	$3d^2 - 3d^1(n^2G)4p$	$b^1F - ^1F$	2-3		493
	90	1446.247	43.32217 - 112.46701	$3d^2 - 3d^1(n^2G)4p$	$b^1F - ^1F$	3-3		493
	300	1446.511	49.76865 - 118.90053	$3d^2 - 3d^1(n^2H)4p$	$b^1G - ^1G$	4-4		493
	250	1446.673	65.76321 - 134.88754	$3d^2 - 3d^1(n^2F)4p$	$b^1D - ^1F$	2-3		493
	40	1447.284	43.30453 - 112.39984	$3d^2 - 3d^1(n^2G)4p$	$b^1F - ^1F$	2-2		493
	20	1447.50	43.28671 - 112.37288	$3d^2 - 3d^1(n^2G)4p$	$b^1F - ^1F$	4-4		490
	4	1448.221	43.32217 - 112.37288	$3d^2 - 3d^1(n^2G)4p$	$b^1F - ^1F$	3-4		493
	20	1449.89	49.67825 - 118.59911	$3d^1(n^2F)4s - 3d^1(n^2D)4p$	$^1F - ^1D$	2-3		490
	5	1450.22						490
	10	1450.52						490
	80	1451.95						490
	50	1454.00	27.37232 - 96.14925	$3d^2 - 3d^1(n^2F)4p$	$a^1S - ^1F$	0-1		490
	30	1457.22						490
	10	1458.17						490
	80	1458.41						490
	30	1462.12						490
	10	1463.87						490
	20	1467.04						490

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	50	1467.68						490
	50	1468.05						490
	50	1469.55						490
	10	1470.60						490
	60	1471.842	63.17430 - 131.11636	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^3F - ^3G$	2-3		493
	20	1472.45						490
	30	1473.32						490
	10	1473.82						490
	50	1476.06						490
	10	1477.49						490
	20	1478.08						490
	20	1478.64						490
	100	1480.16						490
	20	1483.11						490
	10	1483.45						490
	50	1483.75						490
	10	1484.39						490
	10	1486.02						490
	10	1486.54						490
	40	1487.03						490
	10	1487.86						490
	20	1488.72						490
	20	1489.10	69.62825 - 116.78205	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^3F - ^3D$	2-2		490
	20	1489.35						490
	40	1489.93						490
	20	1491.50						490
	40	1492.05						490
	50	1492.98						490
	10	1493.462	69.69246 - 116.45119	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^3F - ^3S$	1-1		493
	10	1493.68						490
	50	1494.45						490
	20	1495.01						490
	20	1495.21	69.69246 - 116.37292	$3d^2(n^2F)4s - 3d^2(n^2D)4p$	$^3F - ^3F$	1-1		490
	20	1495.36						490
	10	1496.47	69.62825 - 116.45119	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^3F - ^3S$	2-1		490
	30	1501.38	65.89238 - 132.69978	$3d^2(n^2G)4s - 3d^2(n^2F)4p$	$^3G - ^3D$	3-2		490
	30	1502.87						490
	30	1503.65						490
	100	1505.76						490
	10	1506.82						490
	10	1506.95						490
	30	1507.93						490
	200	1508.122	65.76321 - 132.07071	$3d^2 - 3d^2(n^2F)4p$	$^3D - ^3D$	2-2		493
	4	1508.740	43.44199 - 109.72279	$3d^2 - 3d^2(n^2F)4p$	$^3F - ^3D$	2-3		493
	30	1509.31						490
	10	1510.05	65.89238 - 132.11730	$3d^2(n^2G)4s - 3d^2(n^2F)4p$	$^3G - ^3D$	3-3		490
	10	1510.62						490
	80	1511.78						490
	300	1512.205	43.44199 - 109.57062	$3d^2 - 3d^2(n^2F)4p$	$^3F - ^3F$	2-1		493
	10	1513.18	66.03001 - 132.11730	$3d^2(n^2G)4s - 3d^2(n^2F)4p$	$^3G - ^3D$	4-3		490
	10	1513.39						490
	20	1515.01						490
	80	1515.44						490
	20	1517.43	69.76867 - 115.67074	$3d^2 - 3d^2(n^2H)4p$	$^3G - ^3H$	4-5		490

CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	20	1517.85						490
	40	1518.48						490
	10	1519.66	49.76865 - 115.57196	$3d^2 - 3d^1(a^1D)4p$	$b^1G - ^1H$	4-4		490
	70	1520.01						490
	40	1520.79						490
	10	1521.29						490
	30	1521.59						490
	5	1522.29	49.49246 - 115.18215	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$^1F - ^1D$	1-2		490
	200	1523.133	43.91659 - 109.57062	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1P$	1-1		493
	80	1523.21	43.32217 - 108.97290	$3d^2 - 3d^1(a^1F)4p$	$b^1F - ^1P$	3-2		490
	20	1524.65						490
	10	1525.27	43.30453 - 108.86498	$3d^2 - 3d^1(a^1F)4p$	$b^1F - ^1D$	2-1		490
	5	1525.42	49.62825 - 115.18215	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$^1F - ^1D$	2-2		490
	150	1525.751	43.91659 - 109.45811	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1P$	1-0		493
	230	1525.993	43.44199 - 108.97290	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1P$	2-2		493
	90	1528.362	44.14136 - 109.57062	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1P$	0-1		493
	120	1528.517	43.44199 - 108.86498	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1D$	2-1		493
	20	1528.91						490
	20	1529.16						490
	5	1530.59	63.42192 - 128.75462	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$^1P - ^1P$	3-2		490
	20	1532.09						490
	40	1532.517	84.37412 - 149.62630	$3d^1(a^1F)4s - 3d^1(b^1D)4p$	$^1F - ^1F$	4-4		493
	4	1532.906	66.03001 - 131.26566	$3d^1(a^1G)4s - 3d^1(a^1F)4p$	$^1G - ^1G$	4-4		493
	90	1533.094	69.65974 - 134.88754	$3d^1(a^1G)4s - 3d^1(a^1F)4p$	$^1G - ^1F$	4-3		493
	4	1533.176	66.22509 - 131.45016	$3d^1(a^1G)4s - 3d^1(a^1F)4p$	$^1G - ^1G$	5-5		493
	80	1534.09						490
	10	1534.40						490
	10	1535.66						490
	1	1536.201	37.00516 - 102.10076	$3d^2 - 3d^1(a^1F)4p$	$a^1F - ^1P$	3-4		493
	150	1537.133	43.91659 - 108.97290	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1P$	1-2		493
	40	1537.997	43.44199 - 108.46140	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1P$	2-2		493
	10	1538.43	94.80170 - 159.8033	$3d^1(a^1F)4p - 3d^1(a^1F)4s$	$^1G - ^1F$	5-4		490
	30	1539.70	43.91659 - 108.86498	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1D$	1-1		490
	90	1540.865	84.48476 - 149.38364	$3d^1(a^1F)4s - 3d^1(b^1D)4p$	$^1F - ^1P$	3-3		493
	10	1541.57						490
	10	1542.52						490
	150	1543.665	43.91659 - 108.69763	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1D$	1-0		493
	4	1543.884	84.57253 - 149.34403	$3d^1(a^1F)4s - 3d^1(b^1D)4p$	$^1F - ^1F$	2-2		493
	120	1545.031	44.14136 - 108.86498	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1D$	0-1		493
	30	1546.34						490
	30	1546.55						490
	30	1547.05						490
	20	1548.86	32.15199 - 96.71404	$3d^2 - 3d^1(a^1F)4p$	$a^1D - ^1D$	2-3		490
	10	1549.306	43.91659 - 108.46140	$3d^2 - 3d^1(a^1F)4p$	$b^1P - ^1P$	1-2		493
	20	1550.09						490
	10	1550.94						490
	50	1551.43						490
	40	1552.31						490
	10	1552.95						490
	40	1553.30						490
	50	1553.38						490
	30	1554.71						490
	30	1555.94	49.62825 - 113.89943	$3d^1(a^1F)4s - 3d^1(a^1P)4p$	$^1F - ^1P$	2-1		490
	30	1557.01						490

## CR III - Continued

Multiplet	Ref. No.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	30	1558.14						490
	10	1559.67	96.65137 - 120.76726	$3d^2(n^2F)4s - 3d^2(n^2D)4p$	$^7F - ^3G$	2-3		490
	10	1561.72	109.53425 - 173.5699	$3d^2(n^2G)4p - 3d^2(n^2D)4d$	$^3H - ^3H$	4-5		490
	10	1564.07						490
	10	1564.32						490
	20	1565.40						490
	20	1565.54						490
	10	1567.41						490
	10	1567.80						490
	60	1568.471	56.99308 - 120.74955	$3d^2(n^2F)4s - 3d^2(n^2D)4p$	$^7F - ^3G$	3-4		493
	30	1568.87						490
	20	1569.36						490
	30	1569.51						490
	40	1570.67	109.53425 - 173.2005	$3d^2(n^2G)4p - 3d^2(n^2D)4d$	$^3H - ^3H$	4-5		490
	230	1571.055	49.76865 - 113.41993	$3d^2 - 3d^2(n^2G)4p$	$^3G - ^3H$	4-5		493
	20	1571.38						490
	30	1571.98						490
	20	1572.13	94.02999 - 157.6373	$3d^2(n^2F)4p - 3d^2(n^2F)4s$	$^3G - ^3F$	3-3		490
	10	1572.54						490
	20	1572.89						490
	10	1573.34	49.76865 - 113.32000	$3d^2 - 3d^2(n^2G)4p$	$^3G - ^3F$	4-3		490
	70	1573.87	93.76621 - 157.3032	$3d^2(n^2F)4p - 3d^2(n^2F)4s$	$^3G - ^3F$	2-1		490
	40	1574.00	94.37629 - 157.9080	$3d^2(n^2F)4p - 3d^2(n^2F)4s$	$^3G - ^3F$	4-4		490
	20	1574.63						490
73	20	1576.24						490
	100	1577.14	94.02999 - 157.4351	$3d^2(n^2F)4p - 3d^2(n^2F)4s$	$^3G - ^3F$	3-2		490,488
	30	1577.36						490
	10	1578.01	110.90718 - 173.8763	$3d^2(n^2G)4p - 3d^2(n^2D)4d$	$^3H - ^3H$	6-7		490
	10	1578.39						490
	120	1578.624	49.76865 - 113.11521	$3d^2 - 3d^2(n^2G)4p$	$^3G - ^3G$	4-4		493
	90	1580.116	49.82091 - 113.11521	$3d^2(n^2F)4s - 3d^2(n^2G)4p$	$^7F - ^3G$	3-4		493
	10	1580.34	57.42340 - 120.70027	$3d^2(n^2F)4s - 3d^2(n^2D)4p$	$^7F - ^3G$	4-5		490
73	200	1580.73	94.37629 - 157.6373	$3d^2(n^2F)4p - 3d^2(n^2F)4s$	$^3G - ^3F$	4-3		490,488
	100	1581.15						490
	20	1581.57						490
	230	1582.62						490
	200	1582.93						490
	20	1583.70						490
	25	1583.965	69.60150 - 132.73422	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^7F - ^3D$	0-1		493
	10	1584.09						490
73	400	1584.60	94.80170 - 157.9080	$3d^2(n^2F)4p - 3d^2(n^2F)4s$	$^3G - ^3F$	5-4		490,488
	30	1584.84						490
	30	1585.01	96.71404 - 159.8033	$3d^2(n^2F)4p - 3d^2(n^2F)4s$	$^3D - ^3F$	3-4		490
	130	1586.35						490
	60	1586.779	65.76321 - 128.70413	$3d^2 - 3d^2(n^2F)4p$	$^3D - ^3F$	2-3		493
	10	1587.35						490
	20	1587.54	65.76321 - 128.75462	$3d^2 - 3d^2(n^2F)4p$	$^3D - ^3F$	2-2		490
	20	1588.00						490
	130	1588.42						490
	200	1588.87						490
	20	1589.91						490
	20	1590.49						490
	40	1590.789	65.89238 - 128.75462	$3d^2(n^2G)4s - 3d^2(n^2F)4p$	$^3G - ^3F$	3-2		493
	50	1591.09						490



## CR III - Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	100	1592.39						490
	40	1593.16	56.65137 - 119.42142	$3d^2(^3F)4s - 3d^2(^3D)4p$	$^3F - ^3P$	2-2		490
	40	1593.38						490
	25	1593.523	66.03001 - 128.70413	$3d^2(^3G)4s - 3d^2(^3F)4p$	$^3G - ^3F$	4-3		893
	10	1593.71						490
	80	1594.03						490
	40	1594.674	84.37412 - 147.88873	$3d^2(^3F)4s - 3d^2(^3D)4p$	$^3F - ^3D$	4-3		893
	20	1595.86	96.71404 - 159.3736	$3d^2(^3F)4p - 3d^2(^3F)4s$	$^3D - ^3F$	3-3		490
	10	1596.86						490
	150	1596.52	49.82891 - 112.46701	$3d^2(^3F)4s - 3d^2(^3G)4p$	$^3F - ^3F$	3-3		490
	10	1596.76	66.22589 - 128.85049	$3d^2(^3G)4s - 3d^2(^3F)4p$	$^3G - ^3F$	5-4		490
	120	1597.06						490
	10	1597.86						490
	50	1598.05						490
	30	1598.48						490
	30	1599.81						490
	70	1600.82						490
	50	1600.21						490
	40	1601.57						490
	100	1602.17						490
	100	1602.79						490
	300	1603.19	58.89117 - 112.46701	$3d^2(^3F)4s - 3d^2(^3G)4p$	$^3F - ^3F$	4-3		490
	10	1603.93						490
	10	1604.34						490
	20	1605.18						490
	10	1606.19	96.77438 - 159.0318	$3d^2(^3F)4p - 3d^2(^3F)4s$	$^3D - ^3F$	1-2		490
	60	1606.490	70.48701 - 132.73422	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3P - ^3D$	0-1		893
	10	1607.57	70.29286 - 132.49978	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3P - ^3D$	2-2		490
	20	1607.78						490
	30	1607.92						490
	10	1608.19						490
	30	1609.01						490
	200	1609.35						490
	150	1609.79	97.68399 - 159.8033	$3d^2(^3F)4p - 3d^2(^3F)4s$	$^3D - ^3F$	3-4		490
	200	1609.91						490
	10	1610.10	96.92202 - 159.0318	$3d^2(^3F)4p - 3d^2(^3F)4s$	$^3D - ^3F$	2-2		490
	40	1610.56	49.76865 - 111.85497	$3d^2 - 3^1(^3G)4p$	$^3G - ^3G$	4-5		490
	10	1610.88	96.38631 - 158.4636	$3d^2(^3F)4p - 3d^2(^3F)4d$	$^3P - ^3F$	2-3		490
	100	1611.08	111.85497 - 173.9266	$3d^2(^3G)4p - 3d^2(^3G)4d$	$^3G - ^3H$	5-6		490
	10	1611.57						490
	30	1612.07						490
	10	1612.57						490
	10	1613.02						490
	100	1614.04						490
	80	1614.17						490
	10	1615.21	97.12142 - 159.0318	$3d^2(^3F)4p - 3d^2(^3F)4s$	$^3P - ^3F$	3-2		490
	90	1616.040	70.19101 - 132.07071	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3P - ^3D$	2-2		893
	10	1616.461	87.77048 - 149.62630	$3d^2(^3F)4s - 3d^2(^3D)4p$	$^3P - ^3P$	3-4		893
	20	1617.23						490
	90	1617.475	70.29286 - 132.11750	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3P - ^3D$	2-3		893
	5	1617.72	49.82891 - 111.44476	$3d^2(^3F)4s - 3d^2(^3G)4p$	$^3P - ^3G$	3-4		490
	10	1617.90						490
	25	1619.359	70.98126 - 132.73422	$3d^2(^3D)4s - 3d^2(^3F)4p$	$^3D - ^3D$	1-1		893
	100	1619.94	96.71404 - 158.4429	$3d^2(^3F)4p - 3d^2(^3F)4d$	$^3D - ^3G$	3-4		490

Multiplet	Rel. Int.	$\lambda_{air}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J-J	Notes	References
	25	1620.004	70.36536 - 132.07071	$3d^4(^7F)_{4g} - 3d^4(^7F)_{4p}$	$^7P - ^7D'$	1-2		893
	10	1620.46						490
	10	1620.76						490
	30	1621.10						490
	10	1621.60						490
	30	1621.87						490
	10	1623.01	87.77068 - 149.38366	$3d^4(^7F)_{4g} - 3d^4(^7D)_{4p}$	$^7F - ^7F'$	3-3		490
	30	1625.32	97.09828 - 158.6237	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4d}$	$^7D' - ^7F'$	4-4		490
	10	1625.78						490
	100	1626.33						490
	30	1627.25						490
	20	1627.80						490
	150	1628.301	71.32327 - 132.73422	$3d^4(^7D)_{4g} - 3d^4(^7F)_{4p}$	$^7D - ^7D'$	2-1		893
	10	1628.58						490
	100	1628.98						490
	100	1629.56	97.09828 - 158.6636	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4d}$	$^7D' - ^7F'$	4-3		490
	100	1630.94						490
	20	1631.49						490
	20	1631.68	96.14925 - 157.4351	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4g}$	$^7F - ^7F'$	1-2		490
	20	1631.89						490
	100	1632.62	96.30631 - 157.6373	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4g}$	$^7F - ^7F'$	2-3		490
	20	1632.85						490
	20	1633.17						490
	20	1633.60						490
	120	1634.12	96.71404 - 157.9080	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4g}$	$^7D' - ^7F'$	3-4		490
	10	1634.61	57.42340 - 118.99911	$3d^4(^7F)_{4g} - 3d^4(^7D)_{4p}$	$^7F - ^7D'$	4-3		490
	100	1635.10	97.30659 - 158.6636	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4d}$	$^7D' - ^7F'$	2-3		490
	100	1635.48	97.09828 - 158.2418	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4g}$	$^7D' - ^7F'$	4-5		490
	200	1636.35						490
	10	1636.69						490
	100	1637.53						490
	100	1637.90						490
	10	1638.10						490
	10	1638.78	97.30659 - 158.3283	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4d}$	$^7D' - ^7F'$	2-2		490
	10	1639.46						490
	20	1639.90						490
	100	1640.94	97.68399 - 158.6237	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4d}$	$^7D' - ^7F'$	3-4		490
	30	1641.09						490
	100	1641.56	96.30631 - 157.3032	$3d^4(^7F)_{4p} - 3d^4(^7F)_{4g}$	$^7F - ^7F'$	2-1		490
	10	1641.83						490
	100	1642.16						490
	70	1643.07						490
	100	1643.20						490
	80	1643.34						490
	30	1643.86						490
	150	1644.652	87.77068 - 148.57301	$3d^4(^7F)_{4g} - 3d^4(^7D)_{4p}$	$^7F - ^7D'$	3-2		893
	90	1644.882	71.32306 - 132.11750	$3d^4(^7D)_{4g} - 3d^4(^7F)_{4p}$	$^7D - ^7D'$	3-3		893
	50	1645.16						490
	70	1646.15	71.32306 - 132.07071	$3d^4(^7D)_{4g} - 3d^4(^7F)_{4p}$	$^7D - ^7D'$	3-2		490
	20	1646.56						490
	5	1647.71						790
	30	1648.36						490
	10	1648.58						490
	30	1649.13						490

CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	150	1609.51	97.68948 - 158.2618	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3F - ^3F$	5-5		490
	40	1609.95	96.69397 - 157.3852	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3D - ^3F$	0-1		490
	10	1651.32						490
	100	1651.56	97.35981 - 157.9880	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3F - ^3F$	4-4		490
	20	1651.92						490
	50	1652.08	96.77033 - 157.3852	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3D - ^3F$	1-1		490
	150	1652.46	97.12342 - 157.6373	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3F - ^3F$	3-3		490
	10	1654.23	113.11521 - 173.5669	$3d^2(^3G)4p - 3d^2(^3G)3d$	$^3G - ^3G$	4-5		490
	10	1654.79						490
	70	1655.08						490
	20	1657.65						490
	20	1658.30	37.88516 - 97.38659	$3d - 3d^2(^3F)4p$	$^3F - ^3D$	3-2		490
	20	1658.63						490
	100	1659.26						490
	30	1659.82						490
	10	1660.24						490
	10	1660.64	97.68399 - 157.9880	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3D - ^3F$	3-4		490
	150	1660.70						490
	20	1661.58						490
	40	1661.93						490
	25	1663.051	56.65137 - 116.76285	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3D$	2-2		493
	40	1663.75						490
	90	1663.926	74.70808 - 134.88754	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3D - ^3F$	2-3		493
	1	1664.049	49.62825 - 109.72279	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3D$	2-3		493
	150	1664.35	113.11521 - 173.2885	$3d^2(^3G)4p - 3d^2(^3G)3d$	$^3G - ^3F$	4-5		490
	4	1664.491	49.49246 - 109.57889	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3D$	1-2		493
	10	1664.90	50.89117 - 110.15489	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3D$	4-4		490
	20	1665.18	94.80170 - 154.8546	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3G - ^3G$	5-6		490
	70	1665.53						490
	50	1665.62						490
	40	1667.337	56.99308 - 116.96909	$3d^2(^3F)4s - 3d^2(^3D)4p$	$^3F - ^3F$	3-3		493
	30	1667.44						490
	250	1667.621	49.49246 - 109.45811	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3F$	1-0		493
	20	1667.92	97.68399 - 157.6373	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3D - ^3F$	3-3		490
	100	1668.24	49.62825 - 109.57889	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3D$	2-2		490
	80	1668.33						490
	70	1668.96	37.88516 - 96.92202	$3d - 3d^2(^3F)4p$	$^3F - ^3D$	3-2		490
	40	1669.619	49.82891 - 109.72279	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3D$	3-3		493
	150	1669.97	56.65137 - 116.53295	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3D$	2-3		490
	50	1670.27						490
	150	1670.45	94.02999 - 153.8935	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3G - ^3F$	3-2		490
	20	1670.80						490
	10	1671.40						490
	30	1671.85						490
	10	1672.03						490
	20	1673.00	71.67719 - 131.45016	$3d^2(^3H)4s - 3d^2(^3F)4p$	$^3H - ^3G$	4-5		490
	50	1673.58	97.68399 - 157.6351	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3D - ^3F$	3-2		490
	150	1673.784	50.41006 - 110.15489	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3D$	5-4		493
	90	1673.867	49.82891 - 109.57889	$3d^2(^3F)4s - 3d^2(^3F)4p$	$^3F - ^3D$	3-2		493
	1	1674.439	56.65137 - 116.37292	$3d^2(^3F)4s - 3d^2(^3D)4p$	$^3F - ^3F$	2-1		493
	150	1674.73	94.37629 - 154.0857	$3d^2(^3F)4p - 3d^2(^3F)3d$	$^3G - ^3F$	4-3		490
	4	1674.896	49.82891 - 109.53425	$3d^2(^3F)4s - 3d^2(^3G)4p$	$^3F - ^3H$	3-4		493
	200	1675.72						490
	150	1676.20						490

CR III - Continued

Multiplet	Rel. Int.	$\lambda_{air}$ (m Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References							
71	150	1676.955	50.89117 - 109.72279	$3d^2(nF)4s - 3d^2(nF)4p$	$^3F - ^3D$	4-3		893							
	10	1677.54							890						
	10	1677.68							890						
	150	1678.414	71.87017 - 131.43016	$3d^2(nH)4s - 3d^2(nF)4p$	$^3H - ^3G$	6-5		893							
	300	1679.25							890						
	150	1679.375	57.42340 - 116.96909	$3d^2(nF)4s - 3d^2(nD)4p$	$^3F - ^3F$	4-3		893							
	200	1679.537	49.09246 - 108.86498	$3d^2(nF)4s - 3d^2(nF)4p$	$^3F - ^3D$	3-3		893							
	1	1679.691							30.41806 - 109.94498	$3d^2(nF)4s - 3d^2(nG)4p$	$^3F - ^3H$	5-5		893	
	100	1679.83							71.73756 - 131.26566	$3d^2(nH)4s - 3d^2(nF)4p$	$^3H - ^3G$	5-4		890	
	150	1682.303							71.67719 - 131.11636	$3d^2(nH)4s - 3d^2(nF)4p$	$^3H - ^3G$	4-3		893	
	90	1683.540							56.99308 - 116.39166	$3d^2(nF)4s - 3d^2(nD)4p$	$^3F - ^3F$	3-2		893	
	150	1684.02							100.62301 - 159.8033	$3d^2(nF)4p - 3d^2(nF)4s$	$^3G - ^3F$	5-4		890	
	100	1684.14												890	
	4	1684.277										$^3F - ^3D$	1-1		893
	4	1685.072							49.62825 - 108.97250	$3d^2(nF)4s - 3d^2(nF)4p$	$^3F - ^3F$	2-2		893	
	10	1685.38												890	
	150	1685.85						890							
	40	1686.44						890							
	150	1687.05	100.10066 - 159.3756	$3d^2(nF)4p - 3d^2(nF)4s$	$^3G - ^3F$	4-3		890							
	70	1687.56							890						
40	1688.134	49.62825 - 108.86498	$3d^2(nF)4s - 3d^2(nF)4p$	$^3F - ^3D$	2-1		893								
40	1688.39							890							
1	1689.038							49.09246 - 108.69763	$3d^2(nF)4s - 3d^2(nF)4p$	$^3F - ^3D$	1-0		893		
10	1689.14							87.77068 - 146.97333	$3d^2(nF)4s - 3d^2(nD)4p$	$^3F - ^3D$	3-2		890		
200	1689.457	99.84167 - 159.0318	$3d^2(nF)4p - 3d^2(nF)4s$	$^3G - ^3F$	3-2		893								
80	1689.77							890							
30	1690.00							890							
300	1690.28							93.76621 - 152.9273	$3d^2(nF)4p - 3d^2(nF)4d$	$^3G - ^3H$	2-3		890		
20	1690.52													890	
10	1690.72	890													
50	1691.09						890								
50	1691.64						890								
120	1691.774	57.42340 - 116.53295	$3d^2(nF)4s - 3d^2(nF)4p$	$^3F - ^3D$	4-3		893								
30	1692.31							890							
20	1692.63							890							
600	1692.89							94.02999 - 153.0991	$3d^2(nF)4p - 3d^2(nF)4d$	$^3G - ^3H$	3-4		890		
30	1693.43							890							
20	1693.72	890													
70	1694.53						890								
70	1694.92						890								
70	1695.77	49.09246 - 108.46140	$3d^2(nF)4s - 3d^2(nF)4p$	$^3F - ^3F$	1-2		890								
600	1696.64							94.37629 - 153.3146	$3d^2(nF)4p - 3d^2(nF)4d$	$^3G - ^3H$	6-5		890		
20	1696.95						890								
60	1697.43						890								
40	1697.84	94.02999 - 152.9273	$3d^2(nF)4p - 3d^2(nF)4d$	$^3G - ^3H$	3-3		890								
40	1698.03							890							
200	1698.75							890							
10	1699.35							890							
20	1699.84						890								
20	1700.12						890								
34	250	1700.269	43.20671 - 102.10076	$3d^2 - 3d^2(nF)4p$	$b^3P - ^3F$	6-4		893							
30	1701.05	890													
34	60	1701.297	43.32217 - 102.10076	$3d^2 - 3d^2(nF)4p$	$b^3P - ^3F$	3-4		893							
600	1701.48	890													

## CR III - Continued

Multiplet	Ref. Int.	$\lambda_{air}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References	
71	80	1702.89	94.37629 - 153.8991	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$^3G^o - e^3H$	4-4		490	
	40	1703.73							
	10	1704.79							
	71	10	1705.36	109.94498 - 168.5823	$3d^2(n^2G)4p - 3d^2(n^2G)4d$	$^3H^o - f^3H$	5-6		490
		10	1705.76						
		250	1705.961						
		30	1706.15						
		30	1706.65						
	71	30	1707.27	56.99308 - 115.55428	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^3F - ^3D^o$	3-3		490
		800	1707.43						
		40	1707.608						
		400	1707.78						
		25	1708.498						
60		1708.98							
30		1710.10							
34	60	1710.36	43.28671 - 101.74621	$3d^o - 3d^2(n^2F)4p$	$^3P^o - ^3F^o$	4-3		490	
	200	1711.02							
34	5	1711.25	43.32217 - 101.74621	$3d^o - 3d^2(n^2F)4p$	$^3P^o - ^3F^o$	3-3		490	
	200	1711.63							
	20	1712.24							
	10	1712.52							
	50	1713.43							
	150	1714.01							
	10	1714.26							
	40	1714.63							
	30	1715.17							
	20	1715.65							
	40	1716.21							
	40	1716.33							
	40	1716.50							
34	200	1717.43	99.84167 - 158.0667	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$^3G^o - e^3G$	3-3		490	
	40	1717.65							
	40	1717.92							
	40	1718.16							
	120	1718.530							
	40	1719.735							
	80	1720.00							
34	80	1720.00	100.10066 - 158.2418	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$^3G^o - e^3F$	5-4		490	
	200	1720.249							
34	40	1720.512	43.32217 - 101.44457	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$^3F - ^3D^o$	4-3		490	
	150	1721.18							
	10	1721.43							
	200	1721.67							
	70	1721.84							
	150	1722.191							
	100	1723.16							
	100	1723.50							
	10	1723.83							
	120	1724.32							
	100	1725.12							
	150	1725.29							
	40	1725.60							
20	1726.61								
10	1727.51								
34	200	1721.67	115.84458 - 173.9266	$3d^2(n^2H)4p - 3d^2(n^2H)4d$	$^3H^o - g^3H$	6-6		490	
	70	1721.84							
	150	1722.191							
	100	1723.16							
	100	1723.50							
	10	1723.83							
	120	1724.32							
	100	1725.12							
	150	1725.29							
	40	1725.60							
	20	1726.61							
	10	1727.51							

## CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (m Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	10	1727.97						490
	20	1728.24						490
	80	1728.34						490
	10	1730.34						490
	5	1730.92	70.98126 - 128.75462	$3d^2(n^2D)4s - 3d^2(n^2F)4p$	$D - F$	1-2		490
	20	1731.53	97.09828 - 154.8496	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$D - cF$	4-5		490
	90	1731.76	96.14925 - 153.8935	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$F - cF$	1-2		490
	30	1732.85						490
	200	1733.00	97.35981 - 155.0640	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$F - cD$	4-4		490
	150	1733.13	96.38631 - 154.0857	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$F - cF$	2-3		490
	70	1734.83						490
	70	1735.20	101.74621 - 159.3756	$3d^2(n^2F)4p - 3d^2(n^2F)4s$	$F - FF$	3-3		490
	10	1735.61						490
	10	1735.76						490
	30	1736.49	101.44457 - 159.0318	$3d^2(n^2F)4p - 3d^2(n^2F)4s$	$F - FF$	2-2		490
	30	1737.67						490
	120	1738.23	115.67074 - 173.2005	$3d^2(n^2H)4p - 3d^2(n^2H)4d$	$H - F$	5-5		490
	4	1738.300	71.32305 - 128.85049	$3d^2(n^2D)4s - 3d^2(n^2F)4p$	$D - F$	3-4		493
	10	1738.90	96.38631 - 153.8935	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$F - cF$	2-2		490
	10	1740.06						490
	20	1740.31	71.32327 - 128.78413	$3d^2(n^2D)4s - 3d^2(n^2F)4p$	$D - F$	2-3		490
	60	1740.78	97.61948 - 155.0640	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$F - cD$	5-4		490
	150	1742.19						490
	20	1742.52						490
	70	1742.96						490
	100	1743.44	97.09828 - 154.4571	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$D - cF$	4-4		490
	30	1743.65						490
	30	1743.87	65.76321 - 123.10584	$3d^2 - 3d^2(n^2D)4p$	$b^1D - D$	2-2		490
	20	1744.07	97.12142 - 154.4571	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$F - cF$	3-4		490
	30	1744.81						490
	40	1745.04						490
	80	1745.55						490
	120	1745.751	74.78888 - 132.07071	$3d^2(n^2D)4s - 3d^2(n^2F)4p$	$D - D$	2-2		493
	10	1746.48						490
	200	1746.77	56.65137 - 113.89943	$3d^2(n^2F)4s - 3d^2(n^2F)4p$	$F - F$	2-1		490
	70	1747.30	97.61948 - 154.8496	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$F - cF$	5-5		490
	80	1748.74						490
	40	1748.87	96.71404 - 153.8935	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$D - cF$	3-2		490
	70	1749.67						490
	10	1749.88						490
	20	1750.27						490
	10	1750.98						490
	100	1751.34						490
	80	1752.47						490
	30	1753.23						490
	30	1753.60	37.00516 - 94.02999	$3d^2 - 3d^2(n^2F)4p$	$a^1F - G$	3-3		490
	300	1754.76	97.09828 - 154.0857	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$D - cF$	4-3		490
	20	1754.94						490
	150	1755.24	96.92202 - 153.8935	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$D - cF$	2-2		490
	200	1755.46	97.12142 - 154.0857	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$F - cF$	3-3		490
	100	1755.78	96.77438 - 153.7298	$3d^2(n^2F)4p - 3d^2(n^2F)4d$	$D - cF$	1-1		490
	30	1756.29						490
	10	1756.58						490
	10	1756.97						490

Multiplet	Rel. Int.	$\lambda_{air}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	10	1757.45						490
	10	1757.95	101.44457 - 158.3283	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3F - e^3F$	2-2		490
	30	1758.20	101.74621 - 158.6237	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3F - e^3F$	3-4		490
	30	1759.19						490
	20	1759.34						490
	50	1759.50						490
	10	1760.31	96.92202 - 153.7298	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3D - e^3F$	2-1		490
	40	1761.38	97.12142 - 153.8935	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3F - e^3F$	3-2		490
	20	1761.73	37.00516 - 93.76621	$3d^3 - 3d^3(n^2F)4p$	$a^3F - ^3G^o$	3-2		490
	30	1762.52						490
	70	1763.13	101.74621 - 158.4636	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3F - e^3F$	3-3		490
	150	1763.77	101.74621 - 158.4429	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3F - e^3G$	3-4		490
	10	1764.16						490
	120	1765.06						490
	10	1765.53						490
	60	1765.739	65.76321 - 122.39649	$3d^3 - 3d^3(n^2F)4p$	$b^3D - ^3F$	2-1		893
	10	1765.93						490
	10	1766.08	101.44457 - 158.0667	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3F - e^3G$	2-3		490
	60	1766.58						490
	300	1766.92						490
	10	1767.18	97.30659 - 153.8935	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3D - e^3F$	2-2		490
	40	1768.32						490
	40	1768.50						490
	50	1768.78	43.30453 - 95.84167	$3d^3 - 3d^3(n^2F)4p$	$b^3F - ^3G^o$	2-3		490
	100	1769.03						490
	300	1769.17	102.10076 - 158.6237	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3F - e^3F$	4-4		490
	30	1770.10						490
	20	1770.35						490
	20	1770.66						490
	30	1770.96						490
	40	1772.46	117.14585 - 173.5659	$3d^3(n^2H)4p - 3d^3(n^2H)4d$	$^3F - g^3H$	5-5		490
	50	1772.60						490
	20	1773.32						490
	10	1773.70						490
	20	1774.51						490
	10	1774.89	102.10076 - 158.4429	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3F - e^3G$	4-4		490
	30	1775.06	56.99308 - 113.32880	$3d^3(n^2F)4s - 3d^3(n^2G)4p$	$^3F - ^3F$	3-3		490
	40	1777.27						490
	10	1777.49						490
	200	1778.93	96.71404 - 152.9273	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3G^o - e^3H$	3-3		490
	40	1779.91						490
	40	1779.99						490
	50	1780.14	117.48895 - 173.6628	$3d^3(n^2H)4p - 3d^3(n^2H)4d$	$^3F - ^3F$	6-6		490
	20	1781.45						490
	10	1781.73						490
	100	1782.07						490
	250	1782.99						490
	200	1783.95	117.14585 - 173.2005	$3d^3(n^2H)4p - 3d^3(n^2H)4d$	$^3F - ^3F$	5-5		490
	150	1784.43						490
	50	1784.72						490
	10	1785.53	96.92202 - 152.9273	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3D - e^3H$	2-3		490
	30	1786.16						490
	120	1787.18	97.35981 - 153.3146	$3d^3(n^2F)4p - 3d^3(n^2F)4d$	$^3F - e^3H$	4-5		490
	1	1788.464	75.35163 - 131.26566	$3d^3(n^2H)4s - 3d^3(n^2F)4p$	$^3H - ^3G^o$	5-4		893

## CN III - Continued

Multiplet	Rel. Int.	$\lambda_{air}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	40	1789.77						490
	40	1790.48						490
	10	1790.71						490
	30	1791.48						490
	80	1792.73						490
	10	1793.60						490
	50	1793.75	56.65137 - 112.39984	$3d^2(a^1F)4s - 3d^2(a^1G)4p$	$^1F - ^1F'$	2-2		490
	80	1793.95						490
	30	1795.58	57.42340 - 113.11521	$3d^2(a^1F)4s - 3d^2(a^1G)4p$	$^1F - ^1G'$	4-4		490
	10	1796.57						490
	10	1796.89						490
	20	1797.92	97.30659 - 152.9273	$3d^2(a^1F)4p - 3d^2(a^1F)4d$	$^1D' - e^1H$	2-3		490
	50	1798.33						490
	20	1798.97						490
	10	1799.40						490
	10	1800.84						490
	10	1801.46						490
	120	1802.60	56.99308 - 112.46701	$3d^2(a^1F)4s - 3d^2(a^1G)4p$	$^1F - ^1F'$	3-3		490
	10	1803.47						490
	10	1804.85	56.99308 - 112.39984	$3d^2(a^1F)4s - 3d^2(a^1G)4p$	$^1F - ^1F'$	3-2		490
	10	1807.45						490
	10	1809.58						490
	30	1810.14	97.46399 - 152.9273	$3d^2(a^1F)4p - 3d^2(a^1F)4d$	$^1D' - e^1H$	3-3		490
	30	1810.77						490
	40	1810.92						490
	40	1812.24						490
	10	1812.98						490
	20	1813.60						490
	80	1815.49						490
	10	1816.09						490
	100	1817.16						490
	20	1817.79						490
	40	1818.28						490
	60	1819.853	57.42340 - 112.37288	$3d^2(a^1F)4s - 3d^2(a^1G)4p$	$^1F - ^1F'$	4-4		493
	20	1821.08						490
	60	1822.333	65.89238 - 120.76726	$3d^2(a^1G)4s - 3d^2(a^1H)4p$	$^1G - ^1G'$	3-3		493
	10	1825.28						490
	10	1825.66						490
	300	1827.26						490
	20	1829.39						490
46	200	1829.761	56.99308 - 111.64476	$3d^2(a^1F)4s - 3d^2(a^1G)4p$	$^1F - ^1G'$	3-4		493
	40	1830.54						490
	100	1831.15						490
	10	1831.60	102.33349 - 156.92993	$3d^2(b^1D)4s - 3d^2(b^1D)4p$	$^1D - ^1F'$	2-1		490
	10	1832.34						490
	40	1832.87						490
	10	1833.00						490
	1	1833.915	102.40180 - 156.92993	$3d^2(b^1D)4s - 3d^2(b^1D)4p$	$^1D - ^1F'$	1-1		493
	10	1834.68						490
	90	1835.693	66.22509 - 120.70027	$3d^2(a^1G)4s - 3d^2(a^1H)4p$	$^1G - ^1G'$	5-5		493
46	250	1837.099	57.42340 - 111.85697	$3d^2(a^1F)4s - 3d^2(a^1G)4p$	$^1F - ^1G'$	4-5		493
	30	1838.34	43.28671 - 97.68399	$3d^2 - 3d^2(a^1F)4p$	$b^1F - ^1D'$	4-3		490
	25	1838.933	43.30453 - 97.68399	$3d^2 - 3d^2(a^1F)4p$	$b^1F - ^1D'$	2-3		493
	10	1839.72	100.10066 - 154.4571	$3d^2(a^1F)4p - 3d^2(a^1F)4d$	$^1G' - e^1F$	4-4		490



Cr III - Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	10	1840.48	43.28671 - 97.61948	$3d^2 - 3d^2(s^2F)4p$	$b^2F - ^2F^{\circ}$	4-5		490
	10	1842.09						490
	100	1843.40						490
	100	1844.99						490
	80	1846.45						490
	10	1846.71						490
	100	1848.56	65.76321 - 119.84647	$3d^2 - 3d^2(s^2D)4p$	$b^2D - ^2F^{\circ}$	2-3	490	
	120	1848.995					893	
	10	1849.76					490	
	30	1849.99					490	
	10	1850.45					490	
	25	1853.021					893	
	10	1853.36	74.78888 - 128.75462	$3d^2(s^2D)4s - 3d^2(s^2F)4p$	$^1D - ^2F^{\circ}$	2-2	490	
	20	1854.63					490	
	10	1856.20					490	
	20	1857.59					490	
	10	1858.03					490	
	10	1866.12					490	
	20	1866.63	119.64280 - 173.2805	$3d^2(s^2H)4p - 3d^2(s^2H)4d$	$^3H - ^1H$	5-5	490	
	10	1867.52					490	
	20	1871.00					490	
	10	1875.18					490	
	10	1875.52					490	
	10	1877.93					490	
	20	1878.77	120.70027 - 173.9266	$3d^2(s^2H)4p - 3d^2(s^2H)4d$	$^1G^{\circ} - g^2H$	5-6	490	
	20	1878.99					490	
	20	1881.02					490	
	20	1881.33					490	
	20	1881.73					490	
	45	1883.32					490	
	5	1884.30	56.65137 - 109.72279	$3d^2(s^2F)4s - 3d^2(s^2F)4p$	$^3F - ^3D^{\circ}$	2-3	490	
	5	1884.49					490	
	10	1888.83					490	
	10	1893.30					490	
	20	1894.05					490	
	30	1896.09					490	
	90	1896.406	57.42340 - 110.15489	$3d^2(s^2F)4s - 3d^2(s^2F)4p$	$^3F - ^3D^{\circ}$	4-4	893	
	10	1899.15					490	
	20	1899.56					490	
	20	1900.02					490	
	20	1902.19					490	
	20	1902.99					490	
	5	1903.29	56.99308 - 109.53425	$3d^2(s^2F)4s - 3d^2(s^2G)4p$	$^3F - ^3H^{\circ}$	3-4	490	
	10	1903.979					893	
	30	1904.84					490	
	40	1906.12					490	
	50	1910.33					490	
	10	1911.263					893	
	80	1911.66	56.65137 - 108.97290	$3d^2(s^2F)4s - 3d^2(s^2F)4p$	$^3F - ^3F^{\circ}$	2-2	490	
	40	1912.90					490	
	20	1913.85					490	
	30	1914.87					490	
	10	1917.52					490	
	1	1918.489					893	
			63.42192 - 115.57196	$3d^2(s^2F)4s - 3d^2(s^2H)4p$	$^3F - ^3H^{\circ}$	3-4	490	
							70.98126 - 123.10584	$3d^2(s^2D)4s - 3d^2(s^2D)4p$

## CR III - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
	40	1918.61						490
	30	1919.05						490
	20	1922.72	50.09117 - 102.10076	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - F'$	: 4		490
	4	1922.790	63.17430 - 115.18215	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - D'$	2 - 2		493
	10	1923.41						490
	10	1925.26						490
	40	1926.64						490
	250	1928.814	69.60150 - 121.44677	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - S'$	0 - 1		493
	20	1930.39	56.99308 - 108.79584	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - T'$	3 - 3		490
	10	1934.581	50.41006 - 102.10076	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - F'$	5 - 4		493
	200	1935.530	69.78189 - 121.44677	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - S'$	1 - 1		493
	4	1935.918	50.09117 - 101.74621	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - F'$	4 - 3		493
	30	1937.84						490
	20	1939.44						490
	50	1942.30						490
	10	1942.73						490
	5	1944.94	70.98126 - 122.39649	$3d^1(n^1D)4s - 3d^1(n^1F)4p$	$D - F'$	1 - 1		490
	10	1945.47						490
	150	1949.198	105.62689 - 156.92993	$3d^1(n^1D)4s - 3d^1(n^1D)4p$	$D - F'$	2 - 1		493
	60	1950.997	70.19101 - 121.44677	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - S'$	2 - 1		493
	50	1953.26						490
	250	1954.874	70.29286 - 121.44677	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - S'$	2 - 1		493
	40	1956.36	66.03001 - 117.14585	$3d^1(n^1G)4s - 3d^1(n^1H)4p$	$G - T'$	4 - 5		490
	120	1956.899	70.34556 - 121.44677	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - S'$	1 - 1		493
	4	1957.839	65.89238 - 116.96909	$3d^1(n^1G)4s - 3d^1(n^1D)4p$	$G - F'$	3 - 3		493
	1	1958.038	66.03001 - 117.10158	$3d^1(n^1G)4s - 3d^1(n^1D)4p$	$G - F'$	4 - 4		493
	10	1959.224	69.65974 - 120.70027	$3d^1(n^1G)4s - 3d^1(n^1H)4p$	$G - G'$	4 - 5		493
	10	1960.18						490
	10	1960.69						490
	5	1962.16						490
	10	1962.334	70.48701 - 121.44677	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - S'$	0 - 1		493
	120	1963.119	66.03001 - 116.96909	$3d^1(n^1G)4s - 3d^1(n^1D)4p$	$G - F'$	4 - 3		493
	90	1965.031	65.89238 - 116.78205	$3d^1(n^1G)4s - 3d^1(n^1F)4p$	$G - D'$	3 - 2		493
	200	1965.541	66.22509 - 117.10158	$3d^1(n^1G)4s - 3d^1(n^1D)4p$	$G - F'$	5 - 4		493
	10	1966.57						490
	20	1971.11						490
	100	1972.45						490
	70	1973.20						490
	50	1974.03	117.92389 - 168.5823	$3d^1(n^1H)4p - 3d^1(n^1G)4d$	$T - FH$	7 - 6		490
	60	1974.43						490
	10	1974.70	65.89238 - 116.53295	$3d^1(n^1G)4s - 3d^1(n^1F)4p$	$G - D'$	3 - 3		490
	100	1975.56						490
	4	1975.902	65.76321 - 116.37292	$3d^1 - 3d^1(n^1D)4p$	$D - F'$	2 - 1		493
	30	1976.07						490
	40	1978.91						490
	120	1980.083	66.03001 - 116.53295	$3d^1(n^1G)4s - 3d^1(n^1F)4p$	$G - D'$	4 - 3		493
	90	1980.225	65.89238 - 116.39166	$3d^1(n^1G)4s - 3d^1(n^1D)4p$	$G - F'$	3 - 2		493
	!	1981.558	70.98126 - 121.44677	$3d^1(n^1D)4s - 3d^1(n^1F)4p$	$D - S'$	1 - 1		493
	20	1981.82						490
	50	1983.72						490
	50	1986.54						490
	10	1986.82	50.09117 - 100.42301	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - G'$	4 - 5		490
	10	1987.00						490
49	200	1987.620	63.04574 - 113.35704	$3d^1(n^1F)4s - 3d^1(n^1F)4p$	$F - S'$	1 - 2		493

CR III - Continued

Multiplet	Rel. Int.	$\lambda_{air}$ (m Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
49	10	1989.64	69.65974 - 119.84647 63.17430 - 113.35784 71.32327 - 121.44677	$3d^4(a^2G)4s - 3d^4(a^2D)4p$ $3d^4(a^2F)4s - 3d^4(a^2F)4p$ $3d^4(a^2D)4s - 3d^4(a^2F)4p$	'G - F' 'F - G' 'D - G'	4 - 3 2 - 2 2 - 1		490
	40	1991.17						490
	90	1992.556						893
	25*	1992.716						893
	10	1995.866						893
	10	1996.85	490					
	20	1996.70	490					
	20	1999.12	490					
	90	1999.484	50.41006 - 100.42301	$3d^4(a^2F)4s - 3d^4(a^2F)4p$	'F - G'	5 - 5	893	

**CHROMIUM IV ( $\text{Cr}^{2+}$ ),  $Z = 24$**   
**Ground State  $1s^2 2s^2 2p^6 3s^2 3p^3 3d^4(F_{3/2})$  (21 electrons)**  
**Ionization Potential [305 688]  $\text{cm}^{-1}$ ; [40.1] eV**

Multiplet	Rel. Int.	$\lambda_{air}$ (m Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	1	523.808	20.6643 - 211.5740	$3d^4 - 3d^4(a^2S)4p$	$a^2D - a^2P$			219
	5	573.356	0.5556 - 174.9674	$3d^4 - 3d^4(a^2D)4p$	$g^4F - a^2D'$			219
	20	573.758	0.5556 - 174.8449	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
	160	575.048	0.9456 - 174.8449	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
	20	575.175	0.2358 - 174.0948	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
	20	575.850	0.0 - 173.6579	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
	110	576.241	0.5556 - 174.0948	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
	110	576.623	0.2358 - 173.6579	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
	40	579.831	15.0518 - 187.5167	$3d^4 - 3d^4(a^2G)4p$	$a^2G - a^2F'$			219
	40	582.824	15.4016 - 186.9788	$3d^4 - 3d^4(a^2G)4p$	$a^2G - a^2F'$			219
	70	595.093	15.4016 - 183.4426	$3d^4 - 3d^4(a^2G)4p$	$a^2G - a^2H'$			219
	40	596.569	15.0518 - 182.6777	$3d^4 - 3d^4(a^2G)4p$	$a^2G - a^2H'$			219
	1	601.273	20.6643 - 186.9788	$3d^4 - 3d^4(a^2G)4p$	$a^2D - a^2F'$			219
	5	608.138	19.4386 - 183.8739	$3d^4 - 3d^4(a^2F)4p$	$a^2F - a^2F'$			219
	20	608.713	19.4386 - 183.7187	$3d^4 - 3d^4(a^2F)4p$	$a^2F - a^2F'$			219
5	609.013	19.5192 - 183.7187	$3d^4 - 3d^4(a^2F)4p$	$a^2F - a^2F'$			219	
110	612.643	20.6499 - 183.8739	$3d^4 - 3d^4(a^2F)4p$	$a^2D - a^2F'$			219	
110	612.643	14.1771 - 177.4050	$3d^4 - 3d^4(a^2F)4p$	$a^2F - a^2F'$			219	
70	613.746	14.4713 - 177.4050	$3d^4 - 3d^4(a^2F)4p$	$a^2F - a^2F'$			219	
70	614.028	14.0590 - 176.9153	$3d^4 - 3d^4(a^2F)4p$	$a^2F - a^2F'$			219	
5	614.480	14.1771 - 176.9153	$3d^4 - 3d^4(a^2F)4p$	$a^2F - a^2F'$			219	
70	614.903	15.4016 - 178.0281	$3d^4 - 3d^4(a^2G)4p$	$a^2G - a^2G'$			219	
40	615.335	14.1771 - 176.6091	$3d^4 - 3d^4(a^2F)4p$	$a^2F - a^2F'$			219	
40	615.598	14.4713 - 176.9153	$3d^4 - 3d^4(a^2F)4p$	$a^2F - a^2F'$			219	
285	616.819	21.3207 - 183.4426	$3d^4 - 3d^4(a^2G)4p$	$a^2H - a^2H'$			219	
4	40	617.047	0.2358 - 162.2996	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
3	20	617.94	0.2358 - 162.0633	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			791
3	70	618.230	0.0 - 161.7548	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
4	70	618.262	0.5556 - 162.2996	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
160	618.766	21.0659 - 182.6777	$3d^4 - 3d^4(a^2G)4p$	$a^2H - a^2H'$			219	
3	110	619.133	0.2558 - 161.7548	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
3	110	619.758	0.0 - 161.3534	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
3	5	620.125	0.2358 - 161.4939	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
3	360	620.665	0.9456 - 162.0633	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
3	285	621.358	0.5556 - 161.4939	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219
4	220	622.089	0.2358 - 160.9850	$3d^4 - 3d^4(a^2F)4p$	$g^4F - a^2D'$			219

Multiplet	Ref. Int. $\lambda_{\text{c}}$ (in Å)	Levels (in $\text{M}^{\circ} \text{cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	70	623.541	14.6713 - 174.8449	$3d^1 - 3d^0 7p^6$	$^2P - ^4D$	1 1	219
	140	625.037	0.9858 - 160.5336	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	20	625.323	14.1771 - 174.0948	$3d^1 - 3d^0 7p^6$	$^2P - ^4D$	1 1	219
	20	625.596	0.5556 - 160.2029	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	1	626.564	14.0790 - 173.6579	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	1	627.037	14.1771 - 173.6579	$3d^1 - 3d^0 7p^6$	$^2P - ^4D$	1 1	219
	40	627.185	15.4016 - 174.8449	$3d^1 - 3d^0 7p^6$	$^2G - ^4D$	1 1	219
	1	627.471	14.0790 - 173.6306	$3d^1 - 3d^0 7p^6$	$^2P - ^4D$	1 1	219
	40	627.719	0.5556 - 159.2621	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	110	628.482	0.2358 - 159.3305	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	450	629.264	0.9858 - 159.2621	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	110	629.355	0.0 - 158.8912	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	360	629.743	0.5556 - 159.3305	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	285	630.301	0.2358 - 158.8912	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	40	630.522	52.9753 - 211.5740	$3d^1 - 3d^0 5p^6$	$^1D - ^3P$	1 1	219
	220	630.812	0.0 - 158.5259	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	285	630.902	0.9858 - 159.4400	$3d^1 - 3d^0 7p^6$	$^2P - ^4G$	1 1	219
	40	631.289	0.9858 - 159.3305	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	70	631.567	0.5556 - 158.8912	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	70	631.666	15.0518 - 173.2644	$3d^1 - 3d^0 7p^6$	$^2G - ^3P$	1 1	219
	70	631.748	0.2358 - 158.5259	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	220	632.623	0.5556 - 158.6275	$3d^1 - 3d^0 7p^6$	$^2P - ^4G$	1 1	219
	285	633.079	15.4016 - 173.2644	$3d^1 - 3d^0 7p^6$	$^2G - ^3P$	1 1	219
	220	634.133	0.2358 - 157.9311	$3d^1 - 3d^0 7p^6$	$^2P - ^4G$	1 1	219
	285	634.582	15.0518 - 172.6347	$3d^1 - 3d^0 7p^6$	$^2G - ^3P$	1 1	219
	5	635.265	53.1420 - 160.5367	$3d^1 - 3d^0 5p^6$	$^1D - ^3P$	1 1	219
	220	635.485	0.0 - 157.3595	$3d^1 - 3d^0 7p^6$	$^2P - ^4G$	1 1	219
	1	636.44	0.2358 - 157.3595	$3d^1 - 3d^0 7p^6$	$^2P - ^4G$	1 1	219
	110	636.859	14.0590 - 171.0797	$3d^1 - 3d^0 7p^6$	$^2P - ^4G$	1 1	219
	1	637.096	21.0659 - 174.0281	$3d^1 - 3d^0 7p^6$	$^2H - ^4G$	1 1	219
	160	637.338	14.1771 - 171.0797	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	220	637.553	21.0659 - 177.5144	$3d^1 - 3d^0 7p^6$	$^2H - ^4G$	1 1	219
	285	638.127	21.5707 - 174.0281	$3d^1 - 3d^0 7p^6$	$^2H - ^4G$	1 1	219
	285	638.535	14.6713 - 171.0797	$3d^1 - 3d^0 7p^6$	$^2P - ^4G$	1 1	219
	40	642.970	19.4306 - 174.9674	$3d^1 - 3d^0 7p^6$	$^2P - ^4D$	1 1	219
	5	644.756	19.4306 - 174.5304	$3d^1 - 3d^0 7p^6$	$^2P - ^4D$	1 1	219
	220	648.077	20.6643 - 174.9674	$3d^1 - 3d^0 7p^6$	$^2D - ^4D$	1 1	219
	160	649.821	20.6699 - 174.5304	$3d^1 - 3d^0 7p^6$	$^2D - ^4D$	1 1	219
	20	649.876	20.6643 - 174.5304	$3d^1 - 3d^0 7p^6$	$^2D - ^4D$	1 1	219
	1	651.766	20.6643 - 174.0743	$3d^1 - 3d^0 7p^6$	$^2D - ^4D$	1 1	219
	40	652.305	19.5192 - 172.8216	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	160	653.782	24.5557 - 187.5167	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	160	654.688	19.4306 - 172.1821	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	5	655.039	19.5192 - 172.1821	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	160	655.237	24.2628 - 186.9782	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	1	656.065	24.5557 - 186.9782	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219
	110	657.152	20.6699 - 172.8216	$3d^1 - 3d^0 7p^6$	$^2D - ^4P$	1 1	219
	110	659.986	20.6643 - 172.1821	$3d^1 - 3d^0 7p^6$	$^2D - ^4P$	1 1	219
	1	664.828	20.6643 - 171.0797	$3d^1 - 3d^0 7p^6$	$^2D - ^4P$	1 1	219
	30	665.00	15.0518 - 166.4289	$3d^1 - 3d^0 7p^6$	$^2G - ^4G$	1 1	219
	220	666.546	15.4016 - 166.6729	$3d^1 - 3d^0 7p^6$	$^2G - ^4G$	1 1	219
	160	667.297	15.0518 - 164.9006	$3d^1 - 3d^0 7p^6$	$^2G - ^4G$	1 1	219
	20	668.867	15.4016 - 164.9006	$3d^1 - 3d^0 7p^6$	$^2G - ^4G$	1 1	219
	40	673.596	19.4306 - 167.9951	$3d^1 - 3d^0 7p^6$	$^2P - ^4P$	1 1	219

CR IV - Continued

Multiplet	Rel. Int.	$\lambda_{air}$ (m $\text{\AA}$ )	Levels (in $10^3$ $\text{cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
5	20	673.964	19.5192 - 167.8951	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1S$	1 - 1		219
	5	675.180	14.1771 - 162.2996	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	1	676.457	14.4713 - 162.2996	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	20	677.070	14.0590 - 161.7548	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	160	677.552	14.4713 - 162.0633	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
5	190	678.808	14.1771 - 161.4939	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
5	40	678.904	14.0590 - 161.3534	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	5	679.141	20.6499 - 167.8951	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1S$	1 - 1		219
	1	679.455	14.1771 - 161.3534	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	40	680.170	14.4713 - 161.4939	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	5	680.619	14.0590 - 160.9850	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
6	160	680.833	34.3628 - 181.2415	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	20	681.166	14.1771 - 160.9850	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	190	681.568	34.5557 - 181.2763	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	20	681.841	15.4016 - 162.0633	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219
	40	682.760	14.4713 - 160.9358	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1P$	1 - 1		219
	20	684.338	14.1771 - 160.3039	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1P$	1 - 1		219
	285	687.125	15.4016 - 160.9358	$3d^1 - 3d^2(4F)4p$	$2^1G - 2^1P$	1 - 1		219
	220	688.463	15.0518 - 160.3039	$3d^1 - 3d^2(4F)4p$	$2^1G - 2^1P$	1 - 1		219
	5	692.705	21.0659 - 165.4289	$3d^1 - 3d^2(4F)4p$	$2^1H - 2^1G$	1 - 1		219
	360	693.934	21.3207 - 165.4289	$3d^1 - 3d^2(4F)4p$	$2^1H - 2^1G$	1 - 1		219
	285	695.208	21.0659 - 164.9086	$3d^1 - 3d^2(4F)4p$	$2^1H - 2^1G$	1 - 1		219
8	190	696.063	34.3628 - 178.0281	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1G$	1 - 1		219
	190	697.554	34.5557 - 177.9144	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1G$	1 - 1		219
	110	699.981	19.4386 - 162.2996	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	40	702.667	19.4386 - 161.7548	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	40	703.060	19.5192 - 161.7548	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	160	705.975	20.6499 - 162.2996	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219
	20	706.062	20.6443 - 162.2996	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219
	70	706.481	19.4386 - 160.9850	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	70	706.885	19.5192 - 160.9850	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1D$	1 - 1		219
	40	709.900	19.4386 - 160.3039	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1P$	1 - 1		219
	5	709.992	20.6499 - 161.4939	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219
	5	710.077	20.6443 - 161.4939	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219
	5	712.576	20.6499 - 160.9850	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219
	220	712.901	20.6443 - 160.9358	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1P$	1 - 1		219
	40	716.128	20.6443 - 160.3039	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1P$	1 - 1		219
	1	719.420	34.3628 - 173.3644	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1P$	1 - 1		219
	1	724.218	34.5557 - 172.6347	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1P$	1 - 1		219
	0	743.271	52.9753 - 187.5167	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1P$	1 - 1		219
	70	744.190	53.1420 - 187.5167	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1P$	1 - 1		219
	110	745.248	52.9753 - 186.9788	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1P$	1 - 1		219
	8	110	763.947	52.9753 - 183.8739	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1P$	1 - 1	
1		764.923	53.1420 - 183.8739	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1P$	1 - 1		219
70		765.833	53.1420 - 183.7187	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1P$	1 - 1		219
40		779.627	52.9753 - 181.2415	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219
5		780.428	53.1420 - 181.2763	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219
20		780.058	34.3628 - 160.9358	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1P$	1 - 1		219
40		795.241	34.5557 - 160.3039	$3d^1 - 3d^2(4F)4p$	$2^1P - 2^1P$	1 - 1		219
10		816.92						490
1		819.732	52.9753 - 174.9674	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219
10		820.88	53.1420 - 174.9674	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		490
1	914.714	52.9753 - 162.2996	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1D$	1 - 1		219	
1	926.261	52.9753 - 160.9358	$3d^1 - 3d^2(4F)4p$	$2^1D - 2^1P$	1 - 1		219	

CR IV - Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	0	933.172	53.1420 - 140.3039	$3d^2 - 3d^2(^7F)4p$	$6D - 2F'$	$\frac{3}{2} - \frac{1}{2}$		219
	30	1002.39						490
	30	1090.97						490
	10	1092.23						490
	10	1098.06						490
	10	1111.17						490
	10	1227.43						490
	100	1315.00						490
	125	1315.69	157.3595 - 233.365	$3d^2(^7F)4p - 3d^2(^7F)4d$	$2G' - eH$	$\frac{3}{2} - \frac{1}{2}$	P	791
	150	1319.49	157.9311 - 233.718	$3d^2(^7F)4p - 3d^2(^7F)4d$	$2G' - eH$	$\frac{3}{2} - \frac{1}{2}$	P	791
	200	1324.85	158.6275 - 234.178	$3d^2(^7F)4p - 3d^2(^7F)4d$	$2G' - eH$	$\frac{3}{2} - \frac{1}{2}$	P	791
	50	1325.66	157.9311 - 233.365	$3d^2(^7F)4p - 3d^2(^7F)4d$	$2G' - eH$	$\frac{3}{2} - \frac{1}{2}$	P	791
	50	1331.73	158.6275 - 233.718	$3d^2(^7F)4p - 3d^2(^7F)4d$	$2G' - eH$	$\frac{3}{2} - \frac{1}{2}$	P	791
	250	1332.27	159.4480 - 234.508	$3d^2(^7F)4p - 3d^2(^7F)4d$	$2G' - eH$	$\frac{3}{2} - \frac{1}{2}$	P	791
	10	1338.02	158.6275 - 233.365	$3d^2(^7F)4p - 3d^2(^7F)4d$	$2G' - eH$	$\frac{3}{2} - \frac{1}{2}$	P	791
	50	1339.41	159.4480 - 234.108	$3d^2(^7F)4p - 3d^2(^7F)4d$	$2G' - eH$	$\frac{3}{2} - \frac{1}{2}$	P	791
	10	1346.44	159.4480 - 233.718	$3d^2(^7F)4p - 3d^2(^7F)4d$	$2G' - eH$	$\frac{3}{2} - \frac{1}{2}$	P	791
	20	1348.44						490
	40	1351.63						490
	10	1359.93						490
	10	1364.49	104.6286 - 177.9144	$3d^2(^7F)4s - 3d^2(^7G)4p$	$6F - 2G'$	$\frac{3}{2} - \frac{1}{2}$		490
	150	1367.39						490
	20	1369.58						490
	20	1373.46	105.1041 - 177.9144	$3d^2(^7F)4s - 3d^2(^7G)4p$	$6F - 2G'$	$\frac{3}{2} - \frac{1}{2}$		490
	200	1375.56						490
	10	1383.24						490
	20	1388.49						490
	30	1395.33						490
	10	1399.50						490
	220	1401.822	109.9402 - 181.2763	$3d^2(^7F)4s - 3d^2(^7F)4p$	$6F - 2D'$	$\frac{3}{2} - \frac{1}{2}$		219
	20	1410.37						490
	30	1412.24						490
	450	1417.418	110.6904 - 181.2415	$3d^2(^7F)4s - 3d^2(^7F)4p$	$6F - 2D'$	$\frac{3}{2} - \frac{1}{2}$		219
	100	1423.16						490
	100	1424.62						490
	10	1426.58						490
	10	1429.41						490
	10	1447.03	104.2571 - 173.3644	$3d^2(^7F)4s - 3d^2(^7D)4p$	$6F - 2F'$	$\frac{3}{2} - \frac{1}{2}$		490
	20	1461.04						490
	30	1465.00	105.1041 - 173.3644	$3d^2(^7F)4s - 3d^2(^7D)4p$	$6F - 2F'$	$\frac{3}{2} - \frac{1}{2}$	Q	490
	20	1466.14						490
	70	1471.151	109.9402 - 177.9144	$3d^2(^7F)4s - 3d^2(^7G)4p$	$6F - 2G'$	$\frac{3}{2} - \frac{1}{2}$		219
	10	1475.10						490
	20	1482.07						490
	20	1482.36						490
	220	1485.052	110.6904 - 178.0281	$3d^2(^7F)4s - 3d^2(^7G)4p$	$6F - 2G'$	$\frac{3}{2} - \frac{1}{2}$		219
	10	1500.46						490
	120	1508.89						490
	10	1509.85						490
	20	1533.42						490
	10	1551.20						490
	10	1553.09						490
	5	1558.745	110.6904 - 174.8449	$3d^2(^7F)4s - 3d^2(^7F)4p$	$6F - 2D'$	$\frac{3}{2} - \frac{1}{2}$		219
	5	1576.691	109.9402 - 173.3644	$3d^2(^7F)4s - 3d^2(^7D)4p$	$6F - 2F'$	$\frac{3}{2} - \frac{1}{2}$		219

## CRW - Continued

Multiplet	Rel. Int.	$\lambda_c$ (in Å)	Levels (in 10 <sup>3</sup> cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
	5	1594.739	118.5780 - 181.2763	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	cD - rD'			219
	285	1595.039	109.5462 - 172.6347	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub>	bF - yF			219
	380	1595.558	110.8904 - 175.3644	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub>	bF - yF		P	219
	60	1595.622	118.5780 - 181.2415	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	cD - rD'		P	219
	40	1598.723	118.7265 - 181.2763	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	cD - rD'			219
	5	1599.619	118.7265 - 181.2415	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	cD - rD'			219
	20	1613.14	119.2506 - 181.2415	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	bF - rD'			490
	40	1657.71	105.1041 - 165.4289	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	bF - rG'			490
	450	1658.083	127.2063 - 187.5167	3d <sup>2</sup> ( <sup>3</sup> G) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> G) <sub>4</sub>	bG - rF			219
	120	1658.93	104.6286 - 164.9086	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rG'			490
	100	1666.66	173.3644 - 233.365	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	yF - cH			490
	550	1672.660	127.1939 - 186.9788	3d <sup>2</sup> ( <sup>3</sup> G) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> G) <sub>4</sub>	bG - rF			219
	160	1673.021	127.2063 - 186.9788	3d <sup>2</sup> ( <sup>3</sup> G) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> G) <sub>4</sub>	bG - rF			219
	110	1681.673	124.4092 - 183.8739	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
	40	1685.82						490
	360	1686.072	124.4092 - 183.7187	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
	450	1690.881	124.7329 - 183.8739	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
	160	1695.328	124.7329 - 183.7187	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
	30	1698.55	174.8449 - 233.718	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	yD' - cH			490
	110	1699.677	118.5780 - 177.4050	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	cD - yF			219
	20	1704.203	118.7265 - 177.4050	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	cD - yF			219
	10	1706.48						490
	50	1709.89						490
	50	1713.69						490
	30	1715.04						490
	110	1718.533	118.7265 - 176.9153	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	cD - yF			219
	450	1719.560	119.2506 - 177.4050	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF		P	219
	70	1722.38	174.8449 - 232.905	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	yD' - cG			490
14	160	1722.857	104.2571 - 162.2996	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219
	285	1725.257	118.7265 - 176.6091	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> P) <sub>2</sub>	cD - yF			219
	20	1726.00	174.9674 - 232.905	3d <sup>2</sup> ( <sup>1</sup> D) <sub>3</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	yD' - cG			490
	360	1727.067	119.0133 - 176.9153	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
13	70	1729.919	104.2571 - 162.0633	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219
13	220	1731.280	103.9947 - 161.7544	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219
	450	1732.043	119.6700 - 177.4050	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
	220	1733.832	119.0133 - 176.6091	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
14	450	1733.979	104.6286 - 162.2996	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219
	285	1734.156	119.2506 - 176.9153	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
	60	1734.68						490
13	450	1739.193	104.2571 - 161.7548	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219
	160	1740.968	119.2506 - 176.6091	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
13	160	1741.100	104.6286 - 162.0633	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219
	30	1741.93						490
13	220	1743.421	103.9947 - 161.3534	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219
	220	1746.875	119.6700 - 176.9153	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - yF			219
13	285	1747.132	104.2571 - 161.4939	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219
	20	1754.52						490
14	110	1754.685	103.9947 - 160.9850	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'		P	219
13	550	1755.643	105.1041 - 162.0633	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219
	50	1758.37						490
	250	1758.486	124.4092 - 181.2763	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'		P	219
13	400	1758.542	104.6286 - 161.4939	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'		P	219
	30	1762.52						490
14	285	1762.804	104.2571 - 160.9850	3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub> - 3d <sup>2</sup> ( <sup>3</sup> F) <sub>4</sub>	bF - rD'			219

CR IV - Continued

Multiplet	Rel. Int.	$\lambda_{\text{air}}$ (m Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	360	1764.324	104.2571 - 160.9358	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	110	1768.549	124.7329 - 181.2763	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - x^1D$			219
	450	1769.635	124.7329 - 181.2415	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - x^1D$			219
	360	1773.131	118.5700 - 174.9674	$3d^1(a^1D)4s - 3d^1(a^1D)4p$	$c^1D - y^1D$			219
	30	1775.909	103.9947 - 160.3039	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$		P	219
	10	1775.972	104.6286 - 160.9358	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$		P	219
	20	1776.992	118.5700 - 174.8449	$3d^1(a^1D)4s - 3d^1(a^1P)4p$	$c^1D - y^1D$			219
	450	1777.821	127.1939 - 183.4426	$3d^1(a^1G)4s - 3d^1(a^1G)4p$	$b^1G - z^1H$			219
	110	1778.053	118.7265 - 174.9674	$3d^1(a^1D)4s - 3d^1(a^1D)4p$	$c^1D - y^1D$			219
	40	1784.223	104.2571 - 160.3039	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$		P	219
	220	1791.094	105.1041 - 160.9358	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	285	1791.729	118.7265 - 174.5384	$3d^1(a^1D)4s - 3d^1(a^1D)4p$	$c^1D - y^1D$			219
	40	1794.796	119.2506 - 174.9674	$3d^1(a^1P)4s - 3d^1(a^1D)4p$	$b^1P - y^1D$			219
	70	1796.129	104.6286 - 160.3039	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	220	1800.991	119.0133 - 174.5384	$3d^1(a^1P)4s - 3d^1(a^1D)4p$	$b^1P - y^1D$			219
	20	1802.340	127.1939 - 182.6777	$3d^1(a^1G)4s - 3d^1(a^1G)4p$	$b^1G - z^1H$			219
	870	1802.723	127.2063 - 182.6777	$3d^1(a^1G)4s - 3d^1(a^1G)4p$	$b^1G - z^1H$			219
	110	1808.410	119.6700 - 174.9674	$3d^1(a^1P)4s - 3d^1(a^1D)4p$	$b^1P - y^1D$			219
12	110	1808.723	119.2506 - 174.5384	$3d^1(a^1P)4s - 3d^1(a^1D)4p$	$b^1P - y^1D$			219
	360	1810.499	104.6286 - 159.8621	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	750	1812.413	119.6700 - 174.8449	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - y^1D$			219
12	360	1815.100	104.2571 - 159.3505	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	10	1818.90						490
16	870	1819.231	109.9402 - 164.9086	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1G$			219
	70	1820.454	118.7265 - 173.6579	$3d^1(a^1D)4s - 3d^1(a^1P)4p$	$c^1D - y^1D$			219
12	220	1821.621	103.9947 - 158.8912	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	20	1822.49						490
	450	1823.341	119.2506 - 174.0948	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - y^1D$			219
	450	1824.995	118.5700 - 173.3644	$3d^1(a^1D)4s - 3d^1(a^1D)4p$	$c^1D - y^1F$			219
12	750	1826.211	105.1041 - 159.8621	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
16	650	1826.863	110.6904 - 165.4289	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1G$			219
12	650	1827.408	104.6286 - 159.3505	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	220	1830.010	119.0133 - 173.6579	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - y^1D$			219
12	450	1830.350	104.2571 - 158.8912	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	10	1833.66						490
12	450	1833.812	103.9947 - 158.5259	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	1000	1837.400	119.6700 - 174.0948	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - y^1D$		P	219
	450	1837.642	119.0133 - 173.4306	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - y^1D$			219
	220	1837.991	119.2506 - 173.6579	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - y^1D$			219
11	1000	1840.139	105.1041 - 159.4480	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1G$			219
12	220	1842.686	104.2571 - 158.5259	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
12	220	1842.897	104.6286 - 158.8912	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
12	220	1843.448	105.1041 - 159.3505	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1F$			219
	40	1844.407	110.6904 - 164.9086	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1G$			219
	70	1845.705	119.2506 - 173.4306	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - y^1D$			219
	285	1848.593	118.7265 - 172.8216	$3d^1(a^1D)4s - 3d^1(a^1D)4p$	$c^1D - z^1P$			219
	160	1849.632	118.5700 - 172.6347	$3d^1(a^1D)4s - 3d^1(a^1D)4p$	$c^1D - y^1F$			219
11	1000	1851.890	104.6286 - 158.6275	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1G$			219
	220	1852.277	119.6700 - 173.6579	$3d^1(a^1P)4s - 3d^1(a^1P)4p$	$b^1P - y^1D$			219
	285	1855.012	118.7265 - 172.6347	$3d^1(a^1D)4s - 3d^1(a^1D)4p$	$c^1D - y^1F$			219
	20	1858.449	119.0133 - 172.8216	$3d^1(a^1P)4s - 3d^1(a^1D)4p$	$b^1P - z^1P$			219
11	870	1863.108	104.2571 - 157.9311	$3d^1(a^1F)4s - 3d^1(a^1F)4p$	$b^1F - z^1G$			219
	360	1865.255	118.5700 - 172.1821	$3d^1(a^1D)4s - 3d^1(a^1D)4p$	$c^1D - z^1P$			219
	20	1866.685	119.2506 - 172.8216	$3d^1(a^1P)4s - 3d^1(a^1D)4p$	$b^1P - z^1P$			219



CR IV - Continued

Multiplet	Rel Int	$\lambda_{ul}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
11	750	1868 344	105 1041 - 158 6275	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> G <sup>+</sup>	1 - 4		219
11	870	1873 892	103 9947 - 157 3595	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> G <sup>+</sup>	1 - 4		219
11	750	1876 083	104 6286 - 157 9311	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> G <sup>+</sup>	1 - 4		219
	1	1880 811	119 0133 - 172 1821	3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> D <sub>4</sub> p	b <sup>1</sup> P - z <sup>1</sup> P <sup>+</sup>	1 - 4		219
11	650	1883 156	104 2571 - 157 3595	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> G <sup>+</sup>	1 - 4		219
1 <sup>1</sup>	40	1892 960	105 1041 - 157 9311	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> G <sup>+</sup>	1 - 4		219
11	20	1896 419	104 6286 - 157 3595	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> G <sup>+</sup>	1 - 4		219
	400	1904 323	119 6700 - 172 1821	3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> D <sub>4</sub> p	b <sup>1</sup> P - z <sup>1</sup> P <sup>+</sup>	1 - 4	P	219
	350	1904 410	118 5700 - 171 0797	3d <sup>4</sup> (a <sup>1</sup> D <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> p	c <sup>1</sup> D - z <sup>1</sup> S <sup>+</sup>	1 - 4	P	219
	50	1909 88	109 9402 - 162 2996	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> D <sup>+</sup>	1 - 4	P	47
	70	1910 107	118 7265 - 171 0797	3d <sup>4</sup> (a <sup>1</sup> D <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> p	c <sup>1</sup> D - z <sup>1</sup> S <sup>+</sup>	1 - 4		219
	5	1918 542	109 9402 - 162 0633	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> D <sup>+</sup>	1 - 4		219
	160	1920 620	119 0133 - 171 0797	3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> p	b <sup>1</sup> P - z <sup>1</sup> S <sup>+</sup>	1 - 4		219
	220	1929 422	119 2506 - 171 0797	3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> p	b <sup>1</sup> P - z <sup>1</sup> S <sup>+</sup>	1 - 4		219
	285	1929 953	109 9402 - 161 7548	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> D <sup>+</sup>	1 - 4		219
	20	1934 13						490
	750	1937 630	110 6904 - 162 2996	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> D <sup>+</sup>	1 - 4		219
	110	1939 723	109 9402 - 161 4939	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> D <sup>+</sup>	1 - 4		219
	220	1945 160	119 6700 - 171 0797	3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> p	b <sup>1</sup> P - z <sup>1</sup> S <sup>+</sup>	1 - 4		219
	360	1946 549	110 6904 - 162 0633	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> D <sup>+</sup>	1 - 4		219
	20	1948 28						490
	550	1959 060	109 9402 - 160 9850	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> D <sup>+</sup>	1 - 4		219
15	650	1960 950	109 9402 - 160 9358	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> F <sup>+</sup>	1 - 4		219
	870	1967 181	127 1939 - 178 0281	3d <sup>4</sup> (a <sup>1</sup> G <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> G <sub>4</sub> p	b <sup>1</sup> G - y <sup>1</sup> G <sup>+</sup>	1 - 4		219
	360	1968 364	110 6904 - 161 4939	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> D <sup>+</sup>	1 - 4		219
	70	1971 583	127 1939 - 177 9144	3d <sup>4</sup> (a <sup>1</sup> G <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> G <sub>4</sub> p	b <sup>1</sup> G - y <sup>1</sup> G <sup>+</sup>	1 - 4		219
	650	1972 075	127 2063 - 177 9144	3d <sup>4</sup> (a <sup>1</sup> G <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> G <sub>4</sub> p	b <sup>1</sup> G - y <sup>1</sup> G <sup>+</sup>	1 - 4		219
15	450	1985 552	109 9402 - 160 3039	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> F <sup>+</sup>	1 - 4		219
15	650	1990 247	110 6904 - 160 9358	3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> F <sub>4</sub> p	b <sup>1</sup> F - z <sup>1</sup> F <sup>+</sup>	1 - 4		219
	450	1990 664	124 7329 - 174 9674	3d <sup>4</sup> (a <sup>1</sup> P <sub>4</sub> s - 3d <sup>4</sup> (a <sup>1</sup> D <sub>4</sub> p	b <sup>1</sup> P - y <sup>1</sup> D <sup>+</sup>	1 - 4	P	219
	20	1997 35						490

CHROMIUM V (Cr<sup>4+</sup>), Z = 24  
 Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>4</sup>3d<sup>2</sup>(<sup>3</sup>F<sub>2</sub>) (20 electrons)  
 Ionization Potential 560 200 cm<sup>-1</sup>; 69.46 eV

Multiplet	Rel Int	$\lambda_{ul}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	20	433 119	5082 - 231 3929	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - F <sup>+</sup>	3 - 4		218
	5	434 180	0 - 230 3163	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - F <sup>+</sup>	2 - 3		218
	220	434 306	1 1417 - 231 3929	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - F <sup>+</sup>	4 - 4		218
	110	435 143	5082 - 230 3163	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - F <sup>+</sup>	3 - 3		218
	110	435 636	0 - 229 5517	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - F <sup>+</sup>	2 - 2		218
	70	436 351	1 1417 - 230 3163	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - F <sup>+</sup>	4 - 3		218
	70	437 420	5082 - 229 1208	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - D <sup>+</sup>	3 - 3		218
	40	437 655	0 - 228 4891	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - D <sup>+</sup>	2 - 2		218
	100	438 593	0 - 228 0018	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - D <sup>+</sup>	2 - 1	P	218
	130	438 633	5082 - 228 4891	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - D <sup>+</sup>	3 - 2	P	218
	220	438 637	1 1417 - 229 1208	3d <sup>2</sup> - 3d4p	g <sup>3</sup> F - D <sup>+</sup>	4 - 3	P	218
	110	441 056	13 1880 - 239 9175	3d <sup>2</sup> - 3d4p	D <sup>+</sup> - P <sup>+</sup>	2 - 1		218

## CR V - Continued

Multiplet	Rel Int.	$\lambda_{\text{vac}}$ (m Å)	Levels (m $10^3$ cm $^{-1}$ )	Configurations	Terms	J-J	Notes	References
20	442 243		0 - 226 1198	3d <sup>2</sup> - 3d4p	g <sup>4</sup> F <sup>-</sup> D <sup>+</sup>	2-2		218
20	445 751		13 1880 - 237 5295	3d <sup>2</sup> - 3d4p	D <sup>-</sup> F <sup>+</sup>	2-3		218
5	446 672		16 0410 - 239 9175	3d <sup>2</sup> - 3d4p	P <sup>-</sup> P <sup>+</sup>	2-1		218
5	451 141		13 1880 - 234 8464	3d <sup>2</sup> - 3d4p	D <sup>-</sup> P <sup>+</sup>	2-2		218
5	451 607		13 1880 - 234 6184	3d <sup>2</sup> - 3d4p	D <sup>-</sup> P <sup>+</sup>	2-1		218
110	456 272		15 6766 - 234 8464	3d <sup>2</sup> - 3d4p	P <sup>-</sup> P <sup>+</sup>	1-2		218
70	456 357		15 4918 - 234 6184	3d <sup>2</sup> - 3d4p	P <sup>-</sup> P <sup>+</sup>	0-1		218
70	456 637		15 6766 - 234 6685	3d <sup>2</sup> - 3d4p	P <sup>-</sup> P <sup>+</sup>	1-0		218
40	456 743		15 6766 - 234 6184	3d <sup>2</sup> - 3d4p	P <sup>-</sup> P <sup>+</sup>	1-1		218
160	457 028		16 0410 - 234 8464	3d <sup>2</sup> - 3d4p	P <sup>-</sup> P <sup>+</sup>	2-2		218
70	457 504		16 0410 - 234 6184	3d <sup>2</sup> - 3d4p	P <sup>-</sup> P <sup>+</sup>	2-1		218
450	464 015		22 0192 - 237 5295	3d <sup>2</sup> - 3d4p	G <sup>-</sup> F <sup>+</sup>	4-3		218
110	469 311		16 0410 - 229 1208	3d <sup>2</sup> - 3d4p	P <sup>-</sup> D <sup>+</sup>	2-3		218
220	469 634		13 1880 - 226 1198	3d <sup>2</sup> - 3d4p	D <sup>-</sup> D <sup>+</sup>	2-2		218
70	469 893		15 6766 - 228 4891	3d <sup>2</sup> - 3d4p	P <sup>-</sup> D <sup>+</sup>	1-2		218
40	470 567		15 4918 - 228 0018	3d <sup>2</sup> - 3d4p	P <sup>-</sup> D <sup>+</sup>	0-1		218
20	470 697		16 0410 - 228 4891	3d <sup>2</sup> - 3d4p	P <sup>-</sup> D <sup>+</sup>	2-2		218
5	470 976		15 6766 - 228 0018	3d <sup>2</sup> - 3d4p	P <sup>-</sup> D <sup>+</sup>	1-1		218
160	529 742		51 1464 - 239 9175	3d <sup>2</sup> - 3d4p	S <sup>-</sup> P <sup>+</sup>	0-1		218
110	754 521		226 1198 - 358 6538	3d4p - 3d5s	D <sup>-</sup> D <sup>+</sup>	2-2		218
1	764 151		226 1198 - 356 9813	3d4p - 3d5s	D <sup>-</sup> D <sup>+</sup>	2-2		218
1	768 251		228 4891 - 358 6538	3d4p - 3d5s	D <sup>-</sup> D <sup>+</sup>	2-2		218
1	774 079		228 4891 - 357 6759	3d4p - 3d5s	D <sup>-</sup> D <sup>+</sup>	2-3		218
1	775 308		228 0018 - 356 9813	3d4p - 3d5s	D <sup>-</sup> D <sup>+</sup>	1-2		218
5	776 743		228 0018 - 356 7448	3d4p - 3d5s	D <sup>-</sup> D <sup>+</sup>	1-1		218
160	777 873		229 1208 - 357 6759	3d4p - 3d5s	D <sup>-</sup> D <sup>+</sup>	3-3		218
40	778 253		228 4891 - 356 9813	3d4p - 3d5s	D <sup>-</sup> D <sup>+</sup>	2-2		218
1	779 209		230 3163 - 358 6538	3d4p - 3d5s	F <sup>-</sup> D <sup>+</sup>	3-2		218
40	786 210		229 5517 - 356 7448	3d4p - 3d5s	F <sup>-</sup> D <sup>+</sup>	2-1		218
110	789 492		230 3163 - 356 9813	3d4p - 3d5s	F <sup>-</sup> D <sup>+</sup>	3-2		218
160	791 872		231 3929 - 357 6759	3d4p - 3d5s	F <sup>-</sup> D <sup>+</sup>	4-3		218
40	814 148		234 8464 - 357 6759	3d4p - 3d5s	P <sup>-</sup> D <sup>+</sup>	2-3		218
5	817 246		234 6184 - 356 9813	3d4p - 3d5s	P <sup>-</sup> D <sup>+</sup>	1-2		218
1	818 803		234 6184 - 356 7448	3d4p - 3d5s	P <sup>-</sup> D <sup>+</sup>	1-1		218
1	819 153		234 6685 - 356 7448	3d4p - 3d5s	P <sup>-</sup> D <sup>+</sup>	0-1		218
220	825 600		237 5295 - 358 6538	3d4p - 3d5s	F <sup>-</sup> D <sup>+</sup>	3-2		218
1	832 309		237 5295 - 357 6759	3d4p - 3d5s	F <sup>-</sup> D <sup>+</sup>	3-3		218
1	837 157		237 5295 - 356 9813	3d4p - 3d5s	F <sup>-</sup> D <sup>+</sup>	3-2		218
20	842 195		239 9175 - 358 6538	3d4p - 3d5s	P <sup>-</sup> D <sup>+</sup>	1-2		218
220	968 703		226 1198 - 329 3503	3d4p - 3d4d	D <sup>-</sup> D <sup>+</sup>	2-2		218
1	978 064		228 0018 - 330 2451	3d4p - 3d4d	D <sup>-</sup> P <sup>+</sup>	1-1		218
1	979 590		228 0018 - 330 0848	3d4p - 3d4d	D <sup>-</sup> P <sup>+</sup>	1-0		218
1	979 934		228 4891 - 330 5368	3d4p - 3d4d	D <sup>-</sup> P <sup>+</sup>	2-2		218
70	982 736		228 4891 - 330 2451	3d4p - 3d4d	D <sup>-</sup> P <sup>+</sup>	2-1		218
110	986 035		229 1208 - 330 5368	3d4p - 3d4d	D <sup>-</sup> P <sup>+</sup>	3-2		218
1	997 709		229 1208 - 329 3503	3d4p - 3d4d	D <sup>-</sup> D <sup>+</sup>	3-2		218
1	1002 024		229 5517 - 329 3503	3d4p - 3d4d	F <sup>-</sup> D <sup>+</sup>	2-2		218
70	1029 842		228 0018 - 325 1041	3d4p - 3d4d	D <sup>-</sup> F <sup>+</sup>	1-2		218
110	1031 105		228 4891 - 325 4725	3d4p - 3d4d	D <sup>-</sup> F <sup>+</sup>	2-3		218
110	1033 452		229 1208 - 325 8842	3d4p - 3d4d	D <sup>-</sup> F <sup>+</sup>	3-4		218
5	1035 037		228 4891 - 325 1041	3d4p - 3d4d	D <sup>-</sup> F <sup>+</sup>	2-2		218
40	1042 544		234 6184 - 330 5368	3d4p - 3d4d	P <sup>-</sup> P <sup>+</sup>	1-2		218
220	1045 044		234 8464 - 330 5368	3d4p - 3d4d	P <sup>-</sup> P <sup>+</sup>	2-2		218
5	1045 733		234 6184 - 330 2451	3d4p - 3d4d	P <sup>-</sup> P <sup>+</sup>	1-1		218

## CR V — Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
20	1046.294		234.6685 - 330.2451	3d4p - 3d4d	'P' - 'P'	0 - 1		218
40	1046.364		230.3163 - 325.8842	3d4p - 3d4d	'F' - 'F'	3 - 4		218
20	1046.542		229.5517 - 325.1041	3d4p - 3d4d	'F' - 'F'	2 - 2		218
5	1047.494		234.6184 - 330.0848	3d4p - 3d4d	'P' - 'P'	1 - 0		218
20	1048.236		234.8464 - 330.2451	3d4p - 3d4d	'P' - 'P'	2 - 1		218
70	1050.901		230.3163 - 325.4725	3d4p - 3d4d	'F' - 'F'	3 - 3		218
1	1054.991		230.3163 - 325.1041	3d4p - 3d4d	'F' - 'F'	3 - 2		218
110	1058.298		231.3929 - 325.8842	3d4p - 3d4d	'F' - 'F'	4 - 4		218
285	1060.651		237.5295 - 331.8112	3d4p - 3d4d	'F' - 'G'	3 - 4		218
1	1062.933		231.3929 - 325.4725	3d4p - 3d4d	'F' - 'F'	4 - 3		218
20	1073.367		226.1198 - 319.2840	3d4p - 3d4d	'D' - 'P'	2 - 1		218
5	1089.079		237.5295 - 329.3503	3d4p - 3d4d	'F' - 'D'	3 - 2		218
40	1103.390		228.4891 - 319.1191	3d4p - 3d4d	'D' - 'G'	2 - 3		218
160	1104.296		226.1198 - 316.6749	3d4p - 3d4d	'D' - 'F'	2 - 3		218
20	1105.250		229.1208 - 319.5168	3d4p - 3d4d	'D' - 'G'	3 - 4		218
5	1108.322		228.0018 - 318.2276	3d4p - 3d4d	'D' - 'D'	1 - 2		218
5	1109.731		228.4891 - 318.6017	3d4p - 3d4d	'D' - 'D'	2 - 3		218
220	1112.452		228.0018 - 317.8938	3d4p - 3d4d	'D' - 'D'	1 - 1		218
285	1114.350		228.4891 - 318.2276	3d4p - 3d4d	'D' - 'D'	2 - 2		218
450	1116.478		229.5517 - 319.1191	3d4p - 3d4d	'F' - 'G'	2 - 3		218
360	1117.559		229.1208 - 318.6017	3d4p - 3d4d	'D' - 'G'	3 - 3		218
220	1118.157		239.9175 - 329.3503	3d4p - 3d4d	'P' - 'D'	1 - 2		218
5	1118.518		228.4891 - 317.8938	3d4p - 3d4d	'D' - 'D'	2 - 1		218
650	1121.066		230.3163 - 319.5168	3d4p - 3d4d	'F' - 'G'	3 - 4		218
5	1122.255		229.1208 - 318.2276	3d4p - 3d4d	'D' - 'D'	3 - 2		218
20	1126.090		230.3163 - 319.1191	3d4p - 3d4d	'F' - 'G'	3 - 3		218
650	1127.631		231.3929 - 320.0744	3d4p - 3d4d	'F' - 'G'	4 - 5		218
40	1134.768		231.3929 - 319.5168	3d4p - 3d4d	'F' - 'G'	4 - 4		218
160	1137.529		234.6184 - 322.5281	3d4p - 3d4d	'P' - 'S'	1 - 1		218
20	1138.177		234.6685 - 322.5281	3d4p - 3d4d	'P' - 'S'	0 - 1		218
160	1140.489		234.8464 - 322.5281	3d4p - 3d4d	'P' - 'S'	2 - 1		218
40	1146.668		231.3929 - 318.6017	3d4p - 3d4d	'F' - 'D'	4 - 3		218
450	1193.950		234.8464 - 318.6017	3d4p - 3d4d	'P' - 'D'	2 - 3		218
360	1196.042		234.6184 - 318.2276	3d4p - 3d4d	'P' - 'D'	1 - 2		218
70	1200.834		234.6184 - 317.8938	3d4p - 3d4d	'P' - 'D'	1 - 1		218
110	1201.556		234.6685 - 317.8938	3d4p - 3d4d	'P' - 'D'	0 - 1		218
70	1204.126		234.8464 - 317.8938	3d4p - 3d4d	'P' - 'D'	2 - 1		218
220	1210.499		239.9175 - 322.5281	3d4p - 3d4d	'P' - 'S'	1 - 1		218
220	1259.986		239.9175 - 319.2840	3d4p - 3d4d	'P' - 'P'	1 - 1		218
450	1263.501		237.5295 - 316.6749	3d4p - 3d4d	'F' - 'F'	3 - 3		218
650	1465.861		171.6981 - 239.9175	3d4s - 3d4p	'D' - 'P'	2 - 1		218
5	1477.769		167.1764 - 234.8464	3d4s - 3d4p	'D' - 'P'	1 - 2		218
220	1481.651		167.1764 - 234.6685	3d4s - 3d4p	'D' - 'P'	1 - 0		218
220	1482.757		167.1764 - 234.6184	3d4s - 3d4p	'D' - 'P'	1 - 1		218
220	1484.666		167.4910 - 234.8464	3d4s - 3d4p	'D' - 'P'	2 - 2		218
450	1489.711		167.4910 - 234.6184	3d4s - 3d4p	'D' - 'P'	2 - 1		218
650	1497.966		168.0895 - 234.8464	3d4s - 3d4p	'D' - 'P'	3 - 2		218
750	1519.030		171.6981 - 237.5295	3d4s - 3d4p	'D' - 'F'	2 - 3		218
1000	1579.696		168.0895 - 231.3929	3d4s - 3d4p	'D' - 'F'	3 - 4		218
750	1591.721		167.4910 - 230.3163	3d4s - 3d4p	'D' - 'F'	2 - 3		218
650	1603.191		167.1764 - 229.5517	3d4s - 3d4p	'D' - 'F'	1 - 2		218
40	1607.035		168.0895 - 230.3163	3d4s - 3d4p	'D' - 'F'	3 - 3		218
40	1611.330		167.4910 - 229.5517	3d4s - 3d4p	'D' - 'F'	2 - 2		218
40	1622.607		167.4910 - 229.1208	3d4s - 3d4p	'D' - 'D'	2 - 3		218

## CR V - Continued

Multiplet	Rel. Int.	$\lambda_{\text{av}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
110	1630.989		167.1764 - 228.4891	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> D*	1 - 2		218
285	1638.495		168.0895 - 229.1208	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> D*	3 - 3		218
220	1639.403		167.4910 - 228.4891	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> D*	2 - 2		218
160	1644.053		167.1764 - 228.0018	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> D*	1 - 1		218
70	1652.595		167.4910 - 228.0018	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> D*	2 - 1		218
70	1655.639		168.0895 - 228.4891	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> D*	3 - 2		218
70	1705.629		167.4910 - 226.1198	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> D*	2 - 2		218
20	1705.968		171.6981 - 230.3163	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> F*	2 - 3		218
110	1728.497		171.6981 - 229.5517	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> F*	2 - 2		218
1000	1837.502		171.6981 - 226.1198	3d4s - 3d4p	<sup>1</sup> D - <sup>1</sup> D*	2 - 2	P	218

**CHROMIUM VI (Cr<sup>5+</sup>), Z = 24**  
**Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>3</sup>3d(<sup>4</sup>D<sub>3/2</sub>) (19 electrons)**  
**Ionization Potential 731 020 cm<sup>-1</sup>; 90.636 eV**

Multiplet	Rel. Int.	$\lambda_{\text{av}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
1	144.76		0 - 690.781	3p <sup>3</sup> 3d - 3p <sup>3</sup> 10f	g <sup>2</sup> D - <sup>2</sup> F*	- -	P	009
1	144.961		940 - 690.781	3p <sup>3</sup> 3d - 3p <sup>3</sup> 10f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
1	146.776		0 - 681.307	3p <sup>3</sup> 3d - 3p <sup>3</sup> 9f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
4	146.980		940 - 681.307	3p <sup>3</sup> 3d - 3p <sup>3</sup> 9f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
4	149.706		0 - 667.973	3p <sup>3</sup> 3d - 3p <sup>3</sup> 8f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
12	149.918		940 - 667.973	3p <sup>3</sup> 3d - 3p <sup>3</sup> 8f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
30	154.197		0 - 648.521	3p <sup>3</sup> 3d - 3p <sup>3</sup> 7f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
50	154.418		940 - 648.521	3p <sup>3</sup> 3d - 3p <sup>3</sup> 7f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
80	161.659		0 - 618.583	3p <sup>3</sup> 3d - 3p <sup>3</sup> 6f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
80	161.687		940 - 619.419	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> F*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> D*	- -		222
80	161.836		940 - 618.849	3p <sup>3</sup> 3d - 3p <sup>3</sup> 6f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
12	161.908		940 - 618.583	3p <sup>3</sup> 3d - 3p <sup>3</sup> 6f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
1	161.930		940 - 618.491	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> D*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> D*	- -		222
110	162.565		940 - 616.079	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> F*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
12	162.764		0 - 614.385	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> F*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
50	163.014		940 - 614.385	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> F*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
12	163.514		0 - 611.568	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> D*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> D*	- -		222
12	163.801		0 - 610.497	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> D*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> D*	- -		222
4	164.159		0 - 609.166	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> D*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> D*	- -		222
1	164.301		0 - 608.631	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> D*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> D*	- -		222
12	164.564		940 - 608.631	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> D*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> D*	- -		222
12	164.833		940 - 607.615	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> D*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> D*	- -		222
11	168.088		0 - 594.926	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> F*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
4	168.355		940 - 594.926	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> F*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
150	169.435		940 - 591.137	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> F*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
12	170.569		0 - 586.273	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> F*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
30	171.400		940 - 584.371	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> F*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
4	172.204		0 - 580.697	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> P*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> P*	- -		222
80	172.487		940 - 580.697	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> P*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> P*	- -		222
50	172.841		0 - 578.566	3p <sup>3</sup> 3d - 3p <sup>3</sup> 3d( <sup>1</sup> P*) <sub>4s</sub>	g <sup>2</sup> D - <sup>2</sup> P*	- -		222
4	173.973		940 - 575.742	3p <sup>3</sup> 3d - 3p <sup>3</sup> 6p	g <sup>2</sup> D - <sup>2</sup> P*	- -		222
12	174.175		0 - 574.135	3p <sup>3</sup> 3d - 3p <sup>3</sup> 6p	g <sup>2</sup> D - <sup>2</sup> P*	- -		222
150	175.756		0 - 568.9574	3p <sup>3</sup> 3d - 3p <sup>3</sup> 5f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
200	176.037		940 - 568.9930	3p <sup>3</sup> 3d - 3p <sup>3</sup> 5f	g <sup>2</sup> D - <sup>2</sup> F*	- -		222
375	201.007		0 - 497.495	3p <sup>3</sup> 3d - 3p <sup>3</sup> ( <sup>1</sup> P*)(3d <sup>1</sup> ( <sup>1</sup> F))	g <sup>2</sup> D - <sup>2</sup> D*	- -		222
250	201.224		0 - 496.958	3p <sup>3</sup> 3d - 3p <sup>3</sup> ( <sup>1</sup> P*)(3d <sup>1</sup> ( <sup>1</sup> F))	g <sup>2</sup> D - <sup>2</sup> D*	- -		222

## CR VI - Continued

Multiplet	Rel. Int.	$\lambda_{\infty}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
200	201.388		940 - 597.495	$3p^3d - 3p^1(1P^o)(3d^2(1F))$	$g^1D - 1D^o$	1 - 1		222
450	201.606		940 - 496.958	$3p^3d - 3p^1(1P^o)(3d^2(1F))$	$g^1D - 1D^o$	1 - 1		222
110	202.057		0 - 494.9112	$3p^3d - 3p^1(1P^o)(3d^2(1P))$	$g^1D - 1P^o$	1 - 1		222
375	202.442		940 - 494.9112	$3p^3d - 3p^1(1P^o)(3d^2(1P))$	$g^1D - 1P^o$	1 - 1		222
300	202.739		0 - 493.2471	$3p^3d - 3p^1(1P^o)(3d^2(1P))$	$g^1D - 1P^o$	1 - 1		222
110	204.682		0 - 488.5619	$3p^3d - 3p^3p$	$g^1D - 1P^o$	1 - 1		222
450	205.084		940 - 488.5619	$3p^3d - 3p^3p$	$g^1D - 1P^o$	1 - 1		222
375	207.489		0 - 481.9560	$3p^3d - 3p^4f$	$g^1D - 1F^o$	1 - 1		222
450	207.651		940 - 482.5171	$3p^3d - 3p^4f$	$g^1D - 1F^o$	1 - 1		222
110	207.892		940 - 481.9560	$3p^3d - 3p^4f$	$g^1D - 1F^o$	1 - 1		222
450	226.241		940 - 442.9454	$3p^3d - 3p^1(1P^o)(3d^2(1F))$	$g^1D - 1F^o$	1 - 1		222
375	227.202		0 - 440.1352	$3p^3d - 3p^1(1P^o)(3d^2(1F))$	$g^1D - 1F^o$	1 - 1		222
80	227.689		940 - 440.1352	$3p^3d - 3p^1(1P^o)(3d^2(1F))$	$g^1D - 1F^o$	1 - 1		222
250	264.078		0 - 378.677	$3p^3d - 3p^1(1P^o)(3d^2(1D))$	$g^1D - 1F^o$	1 - 1		222
12	264.732		940 - 378.677	$3p^3d - 3p^1(1P^o)(3d^2(1D))$	$g^1D - 1F^o$	1 - 1		222
300	269.776		940 - 371.618	$3p^3d - 3p^1(1P^o)(3d^2(1D))$	$g^1D - 1F^o$	1 - 1		222
80	279.154		940 - 359.165	$3p^3d - 3p^1(1P^o)(3d^2(1G))$	$g^1D - 1F^o$	1 - 1		222
50	280.143		0 - 356.962	$3p^3d - 3p^1(1P^o)(3d^2(1G))$	$g^1D - 1F^o$	1 - 1		222
12	280.879		940 - 356.962	$3p^3d - 3p^1(1P^o)(3d^2(1G))$	$g^1D - 1F^o$	1 - 1		222
150	335.123		0 - 298.3967	$3p^3d - 3p^4p$	$g^1D - 1P^o$	1 - 1		222
600	336.184		940 - 298.3967	$3p^3d - 3p^4p$	$g^1D - 1P^o$	1 - 1		222
450	337.185		0 - 296.5732	$3p^3d - 3p^4p$	$g^1D - 1P^o$	1 - 1		222
1	383.575		227.8579 - 488.5619	$3p^4s - 3p^5p$	$1S - 1P^o$	1 - 1		222
1	385.015		227.8579 - 487.5895	$3p^4s - 3p^5p$	$1S - 1P^o$	1 - 1		222
0	420.499		296.5732 - 534.3817	$3p^4p - 3p^5d$	$1P^o - 1D$	1 - 1		222
0	423.559		298.3967 - 534.4897	$3p^4p - 3p^5d$	$1P^o - 1D$	1 - 1		222
1	562.572		442.9454 - 620.7005	$3p^1(1P^o)(3d^2(1F)) - 3p^6g$	$1F^o - 1G$	1 - 1		222
1	602.011		402.8886 - 568.9930	$3p^4d - 3p^5f$	$1D - 1F^o$	1 - 1		222
30	607.239		296.5732 - 461.2530	$3p^4p - 3p^5s$	$1P^o - 1S$	1 - 1		222
50	614.028		298.3967 - 461.2530	$3p^4p - 3p^5s$	$1P^o - 1S$	1 - 1		222
4	720.771		481.9560 - 620.6963	$3p^4f - 3p^6g$	$1F^o - 1G$	1 - 1		222
4	723.675		482.5171 - 620.7005	$3p^4f - 3p^6g$	$1F^o - 1G$	1 - 1		222
12	756.786		440.1352 - 572.2723	$3p^1(1P^o)(3d^2(1F)) - 3p^5g$	$1F^o - 1G$	1 - 1		222
30	773.223		442.9454 - 572.2744	$3p^1(1P^o)(3d^2(1F)) - 3p^5g$	$1F^o - 1G$	1 - 1		222
520	942.610		296.5732 - 402.6617	$3p^4p - 3p^4d$	$1P^o - 1D$	1 - 1		222
600	957.009		298.3967 - 402.8886	$3p^4p - 3p^4d$	$1P^o - 1D$	1 - 1		222
300	959.093		298.3967 - 402.6617	$3p^4p - 3p^4d$	$1P^o - 1D$	1 - 1		222
12	1086.681		402.8886 - 494.9112	$3p^4d - 3p^1(1P^o)(3d^2(1P))$	$1D - 1P^o$	1 - 1		222
12	1103.926		402.6617 - 493.2471	$3p^4d - 3p^1(1P^o)(3d^2(1P))$	$1D - 1P^o$	1 - 1		222
150	1107.225		481.9560 - 572.2723	$3p^4f - 3p^5g$	$1F^o - 1G$	1 - 1		222
200	1114.114		482.5171 - 572.2744	$3p^4f - 3p^5g$	$1F^o - 1G$	1 - 1		222
12	1164.146		402.6617 - 488.5619	$3p^4d - 3p^5p$	$1D - 1P^o$	1 - 1		222
110	1167.222		402.8886 - 488.5619	$3p^4d - 3p^5p$	$1D - 1P^o$	1 - 1		222
80	1177.469		402.6617 - 487.5895	$3p^4d - 3p^5p$	$1D - 1P^o$	1 - 1		222
200	1255.832		402.8886 - 482.5171	$3p^4d - 3p^4f$	$1D - 1F^o$	1 - 1		222
150	1261.128		402.6617 - 481.9560	$3p^4d - 3p^4f$	$1D - 1F^o$	1 - 1		222
50	1264.746		402.8886 - 481.9560	$3p^4d - 3p^4f$	$1D - 1F^o$	1 - 1		222
80	1281.439		572.2744 - 650.3108	$3p^5g - 3p^7h$	$1G - 1H^o$	1 - 1		222
50	1342.741		487.5895 - 562.0641	$3p^5p - 3p^6s$	$1P^o - 1S$	1 - 1		222
80	1360.504		488.5619 - 562.0641	$3p^5p - 3p^6s$	$1P^o - 1S$	1 - 1		222
800	1417.659		227.8579 - 298.3967	$3p^4s - 3p^4p$	$1S - 1P^o$	1 - 1		222
700	1455.282		227.8579 - 296.5732	$3p^4s - 3p^4p$	$1S - 1P^o$	1 - 1		222
50	1907.462		481.9560 - 534.3817	$3p^4f - 3p^5d$	$1F^o - 1D$	1 - 1		222
80	1924.089		482.5171 - 534.4897	$3p^4f - 3p^5d$	$1F^o - 1D$	1 - 1		222

CR VI - Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
12	1932.783		568.9574 - 620.6963	$3p^5f - 3p^5g$	$^3F - ^3G$	0-1		222
30	1933.955		568.9930 - 620.7005	$3p^5f - 3p^5g$	$^3F - ^3G$	0-1		222

**CHROMIUM VII ( $\text{Cr}^{6+}$ ), Z = 24**  
**Ground State  $1s^2 2s^2 2p^6 3s^2 3p^4 (^3S_1)$  (18 electrons)**  
**ionization Potential 1 291 900  $\text{cm}^{-1}$ ; 160.18 eV**

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
		71.744	0 - 1393.84	$3s^2 3p^4 - 3s 3p^5 7p$	$g^1 S - ^1 P$	0-1	A	440
1	74.875		0 - 1335.56	$3s^2 3p^4 - 3s 3p^5 6p$	$g^1 S - ^1 P$	0-1	A	440
4	81.491		0 - 1227.13	$3s^2 3p^4 - 3s 3p^5 5p$	$g^1 S - ^1 P$	0-1	A	440
1	81.980		0 - 1219.81	$3s^2 3p^4 - 3s 3p^5 5p$	$g^1 S - ^1 P$	0-1	A	440
1	92.128		0 - 1085.446	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 6s$	$g^1 S - ^3 D$	0-1		907
5	92.969		0 - 1075.627	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 6s$	$g^1 S - ^3 D$	0-1		907
5	95.917		0 - 1042.568	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 5d$	$g^1 S - ^3 D$	0-1		907
20	96.760		0 - 1033.485	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 5d$	$g^1 S - ^3 D$	0-1		907
20	100.593		0 - 994.105	$3s^2 3p^4 - 3s 3p^5 4p$	$g^1 S - ^1 P$	0-1		907
1	101.565		0 - 984.59	$3s^2 3p^4 - 3s 3p^5 4p$	$g^1 S - ^1 P$	0-1	A	440
40	104.127		0 - 960.366	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 5s$	$g^1 S - ^3 D$	0-1		907
40	105.139		0 - 951.122	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 5s$	$g^1 S - ^3 D$	0-1		907
285	114.235		0 - 875.3805	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 4d$	$g^1 S - ^3 D$	0-1		907
285	115.407		0 - 866.5028	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 4d$	$g^1 S - ^3 D$	0-1		907
5	116.654		0 - 857.2345	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 4d$	$g^1 S - ^3 D$	0-1		907
650	146.497		0 - 682.6102	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 4s$	$g^1 S - ^3 D$	0-1		907
450	148.714		0 - 672.4277	$3s^2 3p^4 - 3s^2 3p^3 (^4P_{1/2}) 4s$	$g^1 S - ^3 D$	0-1		907
20	166.488	341.1793 - 941.811	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 P - ^3 D$	0-1		907	
70	166.560	342.7735 - 943.1491	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 P - ^3 D$	1-2		907	
40	166.936	342.7735 - 941.811	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 P - ^3 D$	1-1		907	
220	167.020	346.1371 - 944.8667	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 P - ^3 D$	2-3		907	
110	167.496	346.1371 - 943.1491	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 P - ^3 D$	2-2		907	
40	168.523	363.0609 - 956.454	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 F - ^3 D$	2-3		907	
5	169.084	357.5437 - 948.9439	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 F - ^3 D$	4-4		907	
5	169.842	360.1719 - 948.9439	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 F - ^3 D$	3-4		907	
5	170.086	357.5437 - 945.4757	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 F - ^3 D$	4-4		907	
20	170.139	360.1719 - 947.9174	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 F - ^3 D$	3-3		907	
450	170.393	357.5437 - 944.4168	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 F - ^3 D$	4-5		907	
285	170.850	360.1719 - 945.4757	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 F - ^3 D$	3-4		907	
160	170.982	363.0609 - 947.9174	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 F - ^3 D$	2-3		907	
5	174.070	382.7374 - 957.2051	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	3-4		907	
160	174.286	382.6823 - 956.454	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	2-3		907	
220	175.315	386.6166 - 957.0046	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	2-3		907	
70	175.812	385.8283 - 954.623	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	1-2		907	
110	176.053	386.6166 - 954.623	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	2-2		907	
5	176.295	389.2262 - 956.454	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 F - ^3 D$	3-3		907	
285	176.613	382.7374 - 948.9439	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	3-4		907	
40	176.916	382.6823 - 947.9174	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	2-3		907	
70	177.694	382.7374 - 945.4757	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	3-4		907	
70	177.895	382.7374 - 944.8667	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	3-3		907	
1	178.851	382.6823 - 941.811	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	2-1		907	
5	179.682	386.6166 - 943.1491	$3s^2 3p^3 3d - 3s^2 3p^3 (^4P_{1/2}) 4f$	$^1 D - ^3 D$	2-2		907	

## CR VII — Continued

Multiplet	Rel. Int.	$\lambda_{air}$ (in Å)	Levels (in $10^4 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	40	179.776	389.2262 - 945.4757	$3s^2 3p^3 3d - 3s^2 3p^3 ({}^2P_{1,2}) 4f$	${}^1F - {}^3D$	3 - 4		907
	870	202.828	0 - 493.0354	$3s^2 3p^4 - 3s^2 3p^3 3d$	$g^1S - {}^1P$	0 - 1		907
	20	241.393	342.7735 - 757.0358	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1P$	1 - 0		907
	5	242.461	346.1371 - 758.5721	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1P$	2 - 1		907
	70	242.579	346.1371 - 758.3744	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1D$	2 - 2		907
	20	242.953	342.7735 - 754.3789	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1P$	1 - 1		907
	5	244.565	342.7735 - 751.6493	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1P$	1 - 2		907
	20	245.431	341.1793 - 748.6293	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1D$	0 - 1		907
	70	246.599	346.1371 - 751.6493	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1P$	2 - 2		907
	40	250.311	346.1371 - 745.6311	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1D$	2 - 3		907
	20	251.124	360.1719 - 758.3744	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1D$	3 - 2		907
	1	252.837	363.0609 - 758.5721	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1P$	2 - 1		907
	20	254.177	341.1793 - 734.6053	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1S$	0 - 1		907
	70	255.210	342.7735 - 734.6053	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1S$	1 - 1		907
	1	255.447	360.1719 - 751.6493	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1P$	3 - 2		907
	40	255.545	363.0609 - 754.3789	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1P$	2 - 1		907
	70	257.422	346.1371 - 734.6053	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1P - {}^1S$	2 - 1		907
	450	257.676	357.5437 - 745.6311	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1D$	4 - 3		907
	285	259.181	0 - 385.8283	$3s^2 3p^4 - 3s^2 3p^3 3d$	$g^1S - {}^1D$	0 - 1		907
	110	259.360	363.0609 - 748.6293	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1D$	2 - 1		907
	40	259.432	360.1719 - 745.6311	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1D$	3 - 3		907
	360	259.636	360.1719 - 745.3289	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1D$	3 - 2		907
	20	261.598	363.0609 - 745.3289	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1D$	2 - 2		907
	1	266.172	382.6823 - 758.3744	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1D$	2 - 2		907
	70	268.852	386.6166 - 758.5721	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1P$	2 - 1		907
	70	269.038	382.6823 - 754.3789	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1P$	2 - 1		907
	20	269.397	385.8283 - 757.0358	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1P$	1 - 0		907
	160	270.897	389.2262 - 758.3744	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1D$	3 - 2		907
	160	271.070	382.7374 - 751.6493	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1P$	3 - 2		907
	5	273.269	382.6823 - 748.6293	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1D$	2 - 1		907
	1	273.952	386.6166 - 751.6493	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1P$	2 - 2		907
	1	275.563	382.7374 - 745.6311	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1D$	3 - 3		907
	5	275.635	385.8283 - 748.6293	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1D$	1 - 1		907
	1	275.756	382.6823 - 745.3289	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1D$	2 - 2		907
	1	275.792	382.7374 - 745.3289	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1D - {}^1D$	3 - 2		907
	5	275.926	389.2262 - 751.6493	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1P$	3 - 2		907
	1	280.571	389.2262 - 745.6311	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1D$	3 - 3		907
	20	280.823	389.2262 - 745.3289	$3s^2 3p^3 3d - 3s^2 3p^3 4p$	${}^1F - {}^1D$	3 - 2		907
	20	291.738	0 - 342.7735	$3s^2 3p^4 - 3s^2 3p^3 3d$	$g^1S - {}^1P$	0 - 1		907
	1	355.012	346.1371 - 627.8267	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1P - {}^1D$	2 - 2		907
	220	375.425	342.7735 - 609.1427	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1P - {}^1D$	1 - 2		907
	70	376.073	342.7735 - 608.6796	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1P - {}^1D$	1 - 1		907
	5	377.687	363.0609 - 627.8267	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1F - {}^1D$	2 - 2		907
	360	379.153	346.1371 - 609.8878	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1P - {}^1D$	2 - 3		907
	110	380.219	346.1371 - 609.1427	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1P - {}^1D$	2 - 2		907
	1	380.897	346.1371 - 608.6796	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1P - {}^1D$	2 - 1		907
	450	396.288	357.5437 - 609.8878	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1F - {}^1D$	4 - 3		907
	40	400.452	360.1719 - 609.8878	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1F - {}^1D$	3 - 3		907
	360	401.658	360.1719 - 609.1427	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1F - {}^1D$	3 - 2		907
	70	406.369	363.0609 - 609.1427	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1F - {}^1D$	2 - 2		907
	285	407.138	363.0609 - 608.6796	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1F - {}^1D$	2 - 1		907
	220	407.918	382.6823 - 627.8267	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1D - {}^1D$	2 - 2		907
	160	408.019	382.7374 - 627.8267	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1D - {}^1D$	3 - 2		907
	160	414.582	386.6166 - 627.8267	$3s^2 3p^3 3d - 3s^2 3p^3 3d$	${}^1D - {}^1D$	2 - 2		907

## CR VII - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
110		419.104	389.2262 - 627.8267	$3s^2 3p^3 d - 3s 3p^4 d$	$^1F - ^1D$	3 - 2		907
1		440.121	382.6823 - 609.8878	$3s^2 3p^3 d - 3s 3p^4 d$	$^1D - ^1D$	2 - 3		907
285		440.244	382.7374 - 609.8878	$3s^2 3p^3 d - 3s 3p^4 d$	$^1D - ^1D$	3 - 3		907
70		441.584	382.6823 - 609.1427	$3s^2 3p^3 d - 3s 3p^4 d$	$^1D - ^1D$	2 - 2		907
20		441.680	382.7374 - 609.1427	$3s^2 3p^3 d - 3s 3p^4 d$	$^1D - ^1D$	3 - 2		907
40		447.792	385.8283 - 609.1427	$3s^2 3p^3 d - 3s 3p^4 d$	$^1D - ^1D$	1 - 2		907
40		447.882	386.6166 - 609.8878	$3s^2 3p^3 d - 3s 3p^4 d$	$^1D - ^1D$	2 - 3		907
110		448.729	385.8283 - 608.6796	$3s^2 3p^3 d - 3s 3p^4 d$	$^1D - ^1D$	1 - 1		907
110		449.386	386.6166 - 609.1427	$3s^2 3p^3 d - 3s 3p^4 d$	$^1D - ^1D$	2 - 2		907
20		450.314	386.6166 - 608.6796	$3s^2 3p^3 d - 3s 3p^4 d$	$^1D - ^1D$	2 - 1		907
110		453.183	389.2262 - 609.8878	$3s^2 3p^3 d - 3s 3p^4 d$	$^1F - ^1D$	3 - 3		907
20		741.889	493.6354 - 627.8267	$3s^2 3p^3 d - 3s 3p^4 d$	$^1P - ^1D$	1 - 2		907
40		801.277	734.6053 - 859.4071	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1S - ^3D$	1 - 2		907
20		815.474	734.6053 - 857.2345	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1S - ^3D$	1 - 1		907
5		820.239	751.6493 - 873.5655	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1P - ^3D$	2 - 2		907
5		821.788	734.6053 - 856.2922	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1S - ^3D$	1 - 0		907
20		836.644	745.6311 - 865.1558	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1D - ^3D$	3 - 3		907
20		841.747	745.3289 - 864.1295	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1D - ^3D$	2 - 2		907
5		844.989	757.0358 - 875.3805	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1P - ^3D$	0 - 1		907
40		848.517	754.3789 - 872.2316	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1P - ^3D$	1 - 2		907
160		862.043	745.3289 - 861.1984	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1D - ^3D$	2 - 3		907
70		865.800	748.6293 - 864.1295	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1D - ^3D$	1 - 2		907
20		869.615	758.5721 - 873.5655	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1P - ^3D$	1 - 2		907
220		870.980	745.6311 - 860.4443	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1D - ^3D$	3 - 4		907
110		871.296	758.3744 - 873.1461	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1D - ^3D$	2 - 3		907
70		881.012	751.6493 - 865.1558	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1P - ^3D$	2 - 3		907
20		926.520	758.5721 - 866.5028	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1P - ^3D$	1 - 1		907
1		936.492	758.3744 - 865.1558	$3s^2 3p^4 p - 3s^2 3p^3 (^1P^o); 4d$	$^1D - ^3D$	2 - 3		907
5		1163.516	672.4277 - 758.3744	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1D$	1 - 2		907
1		1163.947	857.2345 - 943.1491	$3s^2 3p^3 (^1P^o); 4d - 3s^2 3p^3 (^1P^o); 4f$	$^3D - ^3D$	1 - 2		907
5		1170.143	859.4071 - 944.8667	$3s^2 3p^3 (^1P^o); 4d - 3s^2 3p^3 (^1P^o); 4f$	$^3D - ^3D$	2 - 3		907
40		1181.920	672.4277 - 757.0358	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1P$	1 - 0		907
5		1186.561	861.1984 - 945.4757	$3s^2 3p^3 (^1P^o); 4d - 3s^2 3p^3 (^1P^o); 4f$	$^3D - ^3D$	3 - 4		907
5		1189.640	873.1461 - 957.2051	$3s^2 3p^3 (^1P^o); 4d - 3s^2 3p^3 (^1P^o); 4f$	$^3D - ^3D$	3 - 4		907
20		1190.867	860.4443 - 944.4168	$3s^2 3p^3 (^1P^o); 4d - 3s^2 3p^3 (^1P^o); 4f$	$^3D - ^3D$	4 - 5		907
70		1193.492	865.1558 - 948.9439	$3s^2 3p^3 (^1P^o); 4d - 3s^2 3p^3 (^1P^o); 4f$	$^3D - ^3D$	3 - 4		907
20		1198.481	873.5655 - 957.0046	$3s^2 3p^3 (^1P^o); 4d - 3s^2 3p^3 (^1P^o); 4f$	$^3D - ^3D$	2 - 3		907
220		1207.866	668.8586 - 751.6493	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1P$	2 - 2		907
360		1302.551	668.8586 - 745.6311	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1D$	2 - 3		907
160		1307.696	668.8586 - 745.3289	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1D$	2 - 2		907
220		1312.307	672.4277 - 748.6293	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1D$	1 - 1		907
220		1319.885	682.6102 - 758.3744	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1D$	1 - 2		907
110		1393.366	682.6102 - 754.3789	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1P$	1 - 1		907
220		1426.644	678.5347 - 748.6293	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1D$	0 - 1		907
40		1448.457	682.6102 - 751.6493	$3s^2 3p^3 (^1P^o); 4s - 3s^2 3p^4 p$	$^3D - ^1P$	1 - 2		907



**CHROMIUM VIII (Cr<sup>7+</sup>), Z = 24**  
**Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>4</sup>(<sup>3</sup>P<sub>2,2</sub>) (17 electrons)**  
**Ionization Potential [1 490 000] cm<sup>-1</sup>; [184.7] eV**

Multiplet Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in 10 <sup>3</sup> cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
	102.45	0.0 - 976.08	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)4d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> D	1 - 2		854
	103.03	0.0 - 970.59	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)4d	g <sup>1</sup> P <sup>1</sup> - <sup>1</sup> P	1 - 1		854
	103.36	9.8919 - 977.38	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)4d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> D	1 - 2		854
	103.48	0.0 - 966.37	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> S	1 - 2		854
	103.92	9.8919 - 972.17	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)4d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> F	1 - 2		854
	105.69	0.0 - 946.16	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4d	g <sup>1</sup> P <sup>1</sup> - <sup>1</sup> D	1 - 1		854
	106.68	9.8919 - 947.27	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4d	g <sup>1</sup> P <sup>1</sup> - <sup>1</sup> D	1 - 1		854
200	124.184	0.0 - 805.26	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> S)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> S	1 - 2		182
100	125.728	9.8919 - 805.26	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> S)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> S	1 - 2		182
700	129.998	0.0 - 769.24	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> D	1 - 2		182
600	131.638	9.8919 - 769.55	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> D	1 - 2		182
200	132.321	0.0 - 755.74	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		182
600	133.395	0.0 - 749.64	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		182
300	134.076	9.8919 - 755.74	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		182
400	134.942	0.0 - 741.06	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		182
100	135.185	9.8919 - 749.64	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		182
50	135.892	0.0 - 735.88	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4s	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		182
	143.17	135 + D - 833.47 + D	3s <sup>2</sup> 3p <sup>1</sup> ( <sup>1</sup> P)3d - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4f	<sup>4</sup> D - <sup>2</sup> F	1 - 1		854
	146.37	146.335 + S - 829.535 + S	3s <sup>2</sup> 3p <sup>1</sup> ( <sup>1</sup> P)3d - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4f	<sup>2</sup> F - <sup>2</sup> G <sup>+</sup>	1 - 1		854
	146.63	142.359 + S - 824.347 + S	3s <sup>2</sup> 3p <sup>1</sup> ( <sup>1</sup> P)3d - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4f	<sup>2</sup> F - <sup>2</sup> G <sup>+</sup>	1 - 1		854
	147.20	145 + S - 824.347 + S	3s <sup>2</sup> 3p <sup>1</sup> ( <sup>1</sup> P)3d - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4f	<sup>2</sup> F - <sup>2</sup> G <sup>+</sup>	1 - 1		854
	147.30	164 + L - 842.886 + L	3s <sup>2</sup> 3p <sup>1</sup> ( <sup>1</sup> D)3d - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)4f	<sup>2</sup> G - <sup>2</sup> H <sup>+</sup>	1 - 1		854
	147.49	146.335 + S - 824.347 + S	3s <sup>2</sup> 3p <sup>1</sup> ( <sup>1</sup> P)3d - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> P)4f	<sup>2</sup> F - <sup>2</sup> G <sup>+</sup>	1 - 1		854
	201.54	0.0 - 496.17	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> D	1 - 2		260
700	205.01	0.0 - 487.78	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> D	1 - 2		260,256
400	205.65	9.8919 - 496.17	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> D	1 - 2		260,256
300	207.07	0.0 - 482.91	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		260,256
200	208.63	0.0 - 479.31	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		260,256
200	211.42	9.8919 - 482.91	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		260,256
200	213.03	9.8919 - 479.31	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> P	1 - 2		260,256
400	216.67	0.0 - 461.54	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> S	1 - 2		260,256
200	221.41	9.8919 - 461.54	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> S	1 - 2		260,256
650	413.112	0.0 - 242.065	3s <sup>2</sup> 3p <sup>1</sup> - 3s3p <sup>6</sup>	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> S	1 - 1		726
450	430.713	9.8919 - 242.065	3s <sup>2</sup> 3p <sup>1</sup> - 3s3p <sup>6</sup>	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> S	1 - 1		726

**CHROMIUM IX (Cr<sup>6+</sup>), Z = 24**  
**Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>4</sup>(<sup>3</sup>P<sub>2</sub>) (16 electrons)**  
**Ionization Potential [1 688 000] cm<sup>-1</sup>; [209.3] eV**

Multiplet Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in 10 <sup>3</sup> cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
	94.33	7.821 - 1067.9	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D) <sup>+</sup> 4d	g <sup>1</sup> P <sup>1</sup> - <sup>1</sup> D <sup>+</sup>	1 - 2		851
	96.17	30.284 - 1070.112	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D) <sup>+</sup> 4d	<sup>1</sup> D - <sup>1</sup> F <sup>+</sup>	2 - 3		854
	96.48	30.284 - 1066.771	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>1</sup> D) <sup>+</sup> 4d	<sup>1</sup> D - <sup>1</sup> D <sup>+</sup>	2 - 2		854
	96.55	66.855 - 1102.576	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> d	S - <sup>1</sup> P <sup>+</sup>	0 - 1		854
	97.19	0 - 1028.91	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>3</sup> S) <sup>+</sup> 4f	g <sup>1</sup> P <sup>1</sup> - <sup>2</sup> G <sup>+</sup>	2 - 3		854
	97.97	7.821 - 1028.54	3s <sup>2</sup> 3p <sup>1</sup> - 3s <sup>2</sup> 3p <sup>4</sup> ( <sup>3</sup> S) <sup>+</sup> 4d	g <sup>1</sup> P <sup>1</sup> - <sup>1</sup> D <sup>+</sup>	1 - 2		854

CN IX - Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
		98.08	9 549 - 1029.14	$3s^2 3p^4 - 3s^2 3p^3(^4S^o)4d$	$g^4P - ^4D^o$	0 - 1		854
200	117.435		30.284 - 881.72	$3s^2 3p^4 - 3s^2 3p^3(^4P^o)4s$	$^4D - ^4P^o$	2 - 1		181
625	117.942		0 - 847.87	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)4s$	$g^4P - ^4D^o$	2 - 3		181
200	118.165		0 - 846.26	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)4s$	$g^4P - ^4D^o$	2 - 2		181
400	119.269		7.821 - 846.26	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)4s$	$g^4P - ^4D^o$	1 - 2		181
200	119.320		7.821 - 845.90	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)4s$	$g^4P - ^4D^o$	1 - 1		181
100	119.569		9.549 - 845.90	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)4s$	$g^4P - ^4D^o$	0 - 1		181
600	121.293		30.284 - 854.73	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)4s$	$^4D - ^4D^o$	2 - 2		181
400	121.781		0 - 821.07	$3s^2 3p^4 - 3s^2 3p^3(^4S^o)4s$	$g^4P - ^4S^o$	2 - 1		181
200	122.720		66.855 - 881.72	$3s^2 3p^4 - 3s^2 3p^3(^4P^o)4s$	$^4S - ^4P^o$	0 - 1		181
200	122.964		7.821 - 821.07	$3s^2 3p^4 - 3s^2 3p^3(^4S^o)4s$	$g^4P - ^4S^o$	1 - 1		181
50	123.226		9.549 - 821.07	$3s^2 3p^4 - 3s^2 3p^3(^4S^o)4s$	$g^4P - ^4S^o$	0 - 1		181
		127.31	1028.645 + S - 1814.129 - S	$3s^2 3p^3(^4D^o)3d - 3s^2 3p^3(^4D^o)4f$	$^4F - ^4G$	2 - 3		854
		127.42	1029.323 - S - 1814.129 - S	$3s^2 3p^3(^4D^o)3d - 3s^2 3p^3(^4D^o)4f$	$^4F - ^4G$	3 - 4		854
		127.53	1030 - S - 1814.129 - S	$3s^2 3p^3(^4D^o)3d - 3s^2 3p^3(^4D^o)4f$	$^4F - ^4G$	4 - 5		854
		127.88	879.572 - D - 1661.555 - D	$3s^2 3p^3(^4S^o)3d - 3s^2 3p^3(^4S^o)4f$	$^4D - ^4F$	3 - 4		854
		127.95	880 - D - 1661.555 - D	$3s^2 3p^3(^4S^o)3d - 3s^2 3p^3(^4S^o)4f$	$^4D - ^4F$	4 - 5		854
		129.77	1030 + L - 1800.594 - L	$3s^2 3p^3(^4D^o)3d - 3s^2 3p^3(^4D^o)4f$	$^4G - ^4H$	5 - 6		854
		129.99	1170 + R - 1939.289 + R	$3s^2 3p^3(^4P^o)3d - 3s^2 3p^3(^4P^o)4f$	$^4F - ^4G$	4 - 5		854
		131.08	500.00 + K - 1262.89 + K	$3s^2 3p^3(^4D^o)3d - 3s^2 3p^3(^4D^o)4f$	$^4G - ^4H$	4 - 5		851
		176.86	400.00 + X - 965.42 + X	$3s^2 3p^3(^4S^o)3d - 3s^2 3p^3(^4S^o)4p$	$^4D - ^4P$	4 - 3		851
		180.57	460.00 + Y - 1013.80 + Y	$3s^2 3p^3(^4D^o)3d - 3s^2 3p^3(^4D^o)4p$	$^4G - ^4F$	5 - 4		851
		208.53	0 - 479.57	$3s^2 3p^4 - 3s^2 3p^3(^4S^o)3d$	$g^4P - ^4D^o$	2 - 2		239
200	209.44		30.284 - 507.75	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)3d$	$^4D - ^4F^o$	2 - 3		239,256
		210.62	0 - 474.79	$3s^2 3p^4 - 3s^2 3p^3(^4S^o)3d$	$g^4P - ^4D^o$	2 - 3		239
		211.32	9.549 - 482.76	$3s^2 3p^4 - 3s^2 3p^3(^4S^o)3d$	$g^4P - ^4D^o$	0 - 1		239
		211.97	7.821 - 479.57	$3s^2 3p^4 - 3s^2 3p^3(^4S^o)3d$	$g^4P - ^4D^o$	1 - 2		239
		215.04	66.855 - 531.88	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)3d$	$^4S - ^4P^o$	0 - 1		239
		215.97	30.284 - 493.31	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)3d$	$^4D - ^4D^o$	2 - 2		239
		220.02	0 - 454.51	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)3d$	$g^4P - ^4P^o$	2 - 2		239
		223.87	7.821 - 454.51	$3s^2 3p^4 - 3s^2 3p^3(^4D^o)3d$	$g^4P - ^4P^o$	1 - 2		239
1	327.267		0 - 305.561	$3s^2 3p^4 - 3s^2 3p^3$	$g^4P - ^4P^o$	2 - 1		726
110	363.271		30.284 - 305.561	$3s^2 3p^4 - 3s^2 3p^3$	$^4D - ^4P^o$	2 - 1		726
110	407.637		0 - 245.317	$3s^2 3p^4 - 3s^2 3p^3$	$g^4P - ^4P^o$	2 - 1		726
110	414.602		7.821 - 249.016	$3s^2 3p^4 - 3s^2 3p^3$	$g^4P - ^4P^o$	1 - 0		726
160	418.290		0 - 239.068	$3s^2 3p^4 - 3s^2 3p^3$	$g^4P - ^4P^o$	2 - 2		726
70	418.925		66.855 - 305.561	$3s^2 3p^4 - 3s^2 3p^3$	$^4S - ^4P^o$	0 - 1		726
110	421.057		7.821 - 245.317	$3s^2 3p^4 - 3s^2 3p^3$	$g^4P - ^4P^o$	1 - 1		726
70	424.146		9.549 - 245.317	$3s^2 3p^4 - 3s^2 3p^3$	$g^4P - ^4P^o$	0 - 1		726
70	432.440		7.821 - 239.068	$3s^2 3p^4 - 3s^2 3p^3$	$g^4P - ^4P^o$	1 - 2		726
	1496		0 - 66.849	$3s^2 3p^4 - 3s^2 3p^3$	$g^4P - ^4S$	2 - 0	F, P	375, 726
185	1694.11		7.821 - 66.849	$3s^2 3p^4 - 3s^2 3p^3$	$g^4P - ^4S$	1 - 0	F	726

**CHROMIUM X ( $\text{Cr}^{0+}$ ),  $Z = 24$**   
**Ground State  $1s^2 2s^2 2p^6 3s^2 3p^4 (^5S_{2,2})$  (15 electrons)**  
**Ionization Potential [1 971 000]  $\text{cm}^{-1}$ ; [244.4] eV**

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
		106.49	0 - 939.055	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{1/2}$	$g^4 S^1 - ^1P$	-		854
		107.14	0 - 933.358	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$g^4 S^1 - ^1P$	-		854
		107.45	37.106 - 967.84	$3s^2 3p^1 - 3s^2 3p^1 (^1D)_{3/2}$	$^1D^1 - ^1D$	-		854
		107.70	0 - 928.505	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$g^4 S^1 - ^1P$	-		854
		107.80	39.454 - 966.93	$3s^2 3p^1 - 3s^2 3p^1 (^1D)_{3/2}$	$^1D^1 - ^1D$	-		854
		109.84	39.454 - 949.78	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1D^1 - ^1P$	-		854
		110.37	37.106 - 943.30	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1D^1 - ^1P$	-		854
		111.02	67.163 - 967.84	$3s^2 3p^1 - 3s^2 3p^1 (^1D)_{3/2}$	$^1P^1 - ^1D$	-		854
		111.16	67.163 - 966.93	$3s^2 3p^1 - 3s^2 3p^1 (^1D)_{3/2}$	$^1P^1 - ^1D$	-		854
		113.31	67.163 - 949.78	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1P^1 - ^1P$	-		854
		113.70	63.936 - 943.30	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1P^1 - ^1P$	-		854
		115.29	750 + D - 1617.377 + D	$3s^2 3p^1 (^1P)_{3/2} - 3s^2 3p^1 (^1P)_{1/2}$	$^1F^1 - ^1G^1$	-		854
		116.75	950 + S - 1806.531 + S	$3s^2 3p^1 (^1D)_{3/2} - 3s^2 3p^1 (^1D)_{1/2}$	$^1G^1 - ^1H^1$	-		854
		117.09	950 + S - 1804.043 + S	$3s^2 3p^1 (^1D)_{3/2} - 3s^2 3p^1 (^1D)_{1/2}$	$^1G^1 - ^1H^1$	-		854
		216.72	39.454 - 500.88	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1D^1 - ^1F$	-		239
		218.88	63.936 - 520.82	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1P^1 - ^1D$	-		239
		220.42	67.163 - 520.82	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1P^1 - ^1D$	-		239
		221.18	67.163 - 519.28	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1P^1 - ^1D$	-		239
		223.86	0 - 446.71	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$g^4 S^1 - ^1P$	-		239
		224.74	0 - 444.96	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$g^4 S^1 - ^1P$	-		239
		226.24	0 - 442.01	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$g^4 S^1 - ^1P$	-		239
		227.42	37.106 - 476.82	$3s^2 3p^1 - 3s^2 3p^1 (^1D)_{3/2}$	$^1D^1 - ^1D$	-		239
		228.71	39.454 - 476.68	$3s^2 3p^1 - 3s^2 3p^1 (^1D)_{3/2}$	$^1D^1 - ^1D$	-		239
		231.21	63.936 - 496.43	$3s^2 3p^1 - 3s^2 3p^1 (^1D)_{3/2}$	$^1P^1 - ^1P$	-		239
		232.96	67.163 - 496.43	$3s^2 3p^1 - 3s^2 3p^1 (^1D)_{3/2}$	$^1P^1 - ^1P$	-		239
		233.80	63.936 - 491.65	$3s^2 3p^1 - 3s^2 3p^1 (^1D)_{3/2}$	$^1P^1 - ^1P$	-		239
		247.67	37.106 - 440.87	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1D^1 - ^1P$	-		239
		252.64	37.106 - 432.92	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1D^1 - ^1P$	-	P	239
		254.15	39.454 - 432.92	$3s^2 3p^1 - 3s^2 3p^1 (^1P)_{3/2}$	$^1D^1 - ^1P$	-		239
	70	333.035	37.106 - 337.373	$3s^2 3p^1 - 3s^2 3p^1$	$^1D^1 - ^1P$	-		726
	5	337.490	37.106 - 333.414	$3s^2 3p^1 - 3s^2 3p^1$	$^1D^1 - ^1P$	-		726
	220	340.181	39.454 - 333.414	$3s^2 3p^1 - 3s^2 3p^1$	$^1D^1 - ^1P$	-		726
	1	351.092	63.936 - 348.763	$3s^2 3p^1 - 3s^2 3p^1$	$^1P^1 - ^1S$	-		726
	40	355.112	67.163 - 348.763	$3s^2 3p^1 - 3s^2 3p^1$	$^1P^1 - ^1S$	-		726
	20	365.718	63.936 - 337.373	$3s^2 3p^1 - 3s^2 3p^1$	$^1P^1 - ^1P$	-		726
	1	371.086	63.936 - 333.414	$3s^2 3p^1 - 3s^2 3p^1$	$^1P^1 - ^1P$	-		726
	1	375.584	67.163 - 333.414	$3s^2 3p^1 - 3s^2 3p^1$	$^1P^1 - ^1P$	-		726
	360	395.984	37.106 - 289.639	$3s^2 3p^1 - 3s^2 3p^1$	$^1D^1 - ^1D$	-		726
	450	398.150	39.454 - 290.614	$3s^2 3p^1 - 3s^2 3p^1$	$^1D^1 - ^1D$	-		726
	40	399.707	39.454 - 289.639	$3s^2 3p^1 - 3s^2 3p^1$	$^1D^1 - ^1D$	-		726
	70	411.655	0 - 242.922	$3s^2 3p^1 - 3s^2 3p^1$	$g^4 S^1 - ^1P$	-		726
	110	416.690	0 - 239.987	$3s^2 3p^1 - 3s^2 3p^1$	$g^4 S^1 - ^1P$	-		726
	220	427.551	0 - 233.890	$3s^2 3p^1 - 3s^2 3p^1$	$g^4 S^1 - ^1P$	-		726
	1	443.062	63.936 - 289.639	$3s^2 3p^1 - 3s^2 3p^1$	$^1P^1 - ^1D$	-		726
	20	447.529	67.163 - 290.614	$3s^2 3p^1 - 3s^2 3p^1$	$^1P^1 - ^1D$	-		726
	0	1489.04	0 - 67.1574	$3s^2 3p^1 - 3s^2 3p^1$	$g^4 S^1 - ^1P^1$	-	F	940
		1564.10	0 - 63.9345	$3s^2 3p^1 - 3s^2 3p^1$	$g^4 S^1 - ^1P^1$	-	F	940

**CHROMIUM XI ( $\text{Cr}^{10+}$ ),  $Z = 24$**   
**Ground State  $1s^2 2s^2 2p^6 3s^2 3p^2 (^3P_0)$  (14 electrons)**  
**Ionization Potential [2 184 000]  $\text{cm}^{-1}$ ; [270.8] eV**

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (m Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
		81.02	0 - 1234.3	$3s^2 3p^2 - 3s^2 3p4d$	$g^1 P - ^1 D^o$	0 - 1		970
		81.18	11.980 - 1243.8	$3s^2 3p^2 - 3s^2 3p4d$	$g^1 P - ^1 F^o$	2 - 3		970
		81.23	5.536 - 1236.6	$3s^2 3p^2 - 3s^2 3p4d$	$g^1 P - ^1 D^o$	1 - 2		970
		81.39	5.536 - 1234.3	$3s^2 3p^2 - 3s^2 3p4d$	$g^1 P - ^1 D^o$	1 - 1		970
		81.55	11.980 - 1238.2	$3s^2 3p^2 - 3s^2 3p4d$	$g^1 P - ^1 D^o$	2 - 3		970
		82.05	36.994 - 1255.8	$3s^2 3p^2 - 3s^2 3p4d$	$^1 D - ^1 F^o$	2 - 3		970
		83.31	74.9863 - 1275.3	$3s^2 3p^2 - 3s^2 3p4d$	$^1 S - ^1 P^o$	0 - 1		970
		98.47	5.536 - 1021.058	$3s^2 3p^2 - 3s^2 3p4s$	$g^1 P - ^1 P^o$	1 - 2		854
		98.94	0 - 1010.713	$3s^2 3p^2 - 3s^2 3p4s$	$g^1 P - ^1 P^o$	0 - 1		854
		99.10	11.980 - 1021.058	$3s^2 3p^2 - 3s^2 3p4s$	$g^1 P - ^1 P^o$	2 - 2		854
		99.13	306.570 - 1315.4	$3s^2 3p^2 - 3s^2 3p4f$	$^1 D^o - ^1 F^o$	2 - 3		970
		99.48	5.536 - 1010.713	$3s^2 3p^2 - 3s^2 3p4s$	$g^1 P - ^1 P^o$	1 - 1		854
		99.67	5.536 - 1008.796	$3s^2 3p^2 - 3s^2 3p4s$	$g^1 P - ^1 P^o$	1 - 0		854
		100.09	306.570 - 1305.7	$3s^2 3p^2 - 3s^2 3p4f$	$^1 D^o - ^1 G^o$	2 - 3		970
		100.13	11.980 - 1010.713	$3s^2 3p^2 - 3s^2 3p4s$	$g^1 P - ^1 P^o$	2 - 1		854
		100.90	36.994 - 1028.067	$3s^2 3p^2 - 3s^2 3p4s$	$^1 D - ^1 P^o$	2 - 1		854
		105.26	384.0 + D - 1334.03 + D	$3s^2 3p^2 - 3s^2 3p4f$	$^1 F^o - ^1 G^o$	4 - 5		970
		105.65	378.5 + D - 1325.02 + D	$3s^2 3p^2 - 3s^2 3p4f$	$^1 F^o - ^1 G^o$	3 - 4		970
		115.13	478.59 - 1347.2	$3s^2 3p^2 - 3s^2 3p4f$	$^1 F^o - ^1 G^o$	3 - 4		970
		117.13	490.35 - 1344.1	$3s^2 3p^2 - 3s^2 3p4f$	$^1 P^o - ^1 D^o$	1 - 2		970
		226.45	36.994 - 478.59	$3s^2 3p^2 - 3s^2 3p3d$	$^1 D - ^1 F^o$	2 - 3		239
		230.29	0 - 434.24	$3s^2 3p^2 - 3s^2 3p3d$	$g^1 P - ^1 D^o$	0 - 1		239
		232.18	5.536 - 436.21	$3s^2 3p^2 - 3s^2 3p3d$	$g^1 P - ^1 D^o$	1 - 2		239
		233.26	5.536 - 434.24	$3s^2 3p^2 - 3s^2 3p3d$	$g^1 P - ^1 D^o$	1 - 1		239
		235.03	0 - 425.48	$3s^2 3p^2 - 3s^2 3p3d$	$g^1 P - ^1 P^o$	0 - 1		239
		235.53	11.980 - 436.55	$3s^2 3p^2 - 3s^2 3p3d$	$g^1 P - ^1 D^o$	2 - 3		239
		235.74	11.980 - 436.21	$3s^2 3p^2 - 3s^2 3p3d$	$g^1 P - ^1 D^o$	2 - 2		239
		237.24	5.536 - 427.09	$3s^2 3p^2 - 3s^2 3p3d$	$g^1 P - ^1 D^o$	1 - 2		239
		240.76	74.9863 - 490.35	$3s^2 3p^2 - 3s^2 3p3d$	$^1 S - ^1 P^o$	0 - 1		239
		241.87	5.536 - 418.98	$3s^2 3p^2 - 3s^2 3p3d$	$g^1 P - ^1 P^o$	1 - 2		239
		245.70	11.980 - 418.98	$3s^2 3p^2 - 3s^2 3p3d$	$g^1 P - ^1 P^o$	2 - 2		239
		256.32	36.994 - 427.09	$3s^2 3p^2 - 3s^2 3p3d$	$^1 D - ^1 D^o$	2 - 2		239
1		280.572	0 - 356.424	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 S^o$	0 - 1		726
20		284.988	5.536 - 356.424	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 S^o$	1 - 1		726
40		290.323	11.980 - 356.424	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 S^o$	2 - 1		726
40		298.059	36.994 - 372.498	$3s^2 3p^2 - 3s3p^1$	$^1 D - ^1 P^o$	2 - 1		726
		336.121	74.9863 - 372.498	$3s^2 3p^2 - 3s3p^1$	$^1 S - ^1 P^o$	0 - 1		726
5		339.446	11.980 - 306.570	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 D^o$	2 - 2		726
		359.203	0 - 278.394	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 P^o$	0 - 1		726
40		366.085	5.536 - 278.698	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 P^o$	1 - 2		726
5		366.491	5.536 - 278.394	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 P^o$	1 - 1		726
5		366.942	5.536 - 278.059	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 P^o$	1 - 0		726
40		370.959	36.994 - 306.570	$3s^2 3p^2 - 3s3p^1$	$^1 D - ^1 D^o$	2 - 2		726
70		374.927	11.980 - 278.698	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 P^o$	2 - 2		726
		375.362	11.980 - 278.394	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 P^o$	2 - 1		726
5		412.629	0 - 242.346	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 D^o$	0 - 1		726
20		422.083	5.536 - 242.456	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 D^o$	1 - 2		726
5		422.282	5.536 - 242.346	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 D^o$	1 - 1		726
20		431.154	11.980 - 243.916	$3s^2 3p^2 - 3s3p^1$	$g^1 P - ^1 D^o$	2 - 3		726
0		1439.85	5.536 - 74.9863	$3s^2 3p^2 - 3s^2 3p^2$	$g^1 P - ^1 S$	1 - 0	F	726, 442
		1587.1	11.980 - 74.9863	$3s^2 3p^2 - 3s^2 3p^2$	$g^1 P - ^1 S$	2 - 0	F.P	375, 726

**CHROMIUM XII (Cr<sup>11+</sup>), Z = 24**  
**Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>3p<sup>2</sup>(<sup>3</sup>P<sub>1,2</sub>) (13 electrons)**  
**Ionization Potential [2 404 000] cm<sup>-1</sup>; [298.0] eV**

Multiplet	Rel. Int.	$\lambda_{\infty}$ (in Å)	Levels (in 10 <sup>3</sup> cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
200	75.815		0 - 1319.00	3s <sup>2</sup> 3p - 3s <sup>2</sup> 4d	g <sup>2</sup> P - <sup>1</sup> D	1 - 1		180
300	76.488		12.261 - 1319.65	3s <sup>2</sup> 3p - 3s <sup>2</sup> 4d	g <sup>2</sup> P - <sup>1</sup> D	1 - 1		180
	90.86		200.00 + W - 1300.6 + W	3s3p <sup>2</sup> - 3s3p4s	<sup>3</sup> P - <sup>3</sup> P	1 - 1		241
	96.11		1200.0 + X - 2240.5 + X	3s3p3d - 3s3p4f	<sup>3</sup> F - <sup>3</sup> G	1 - 1		241
	96.35		1170.0 + Z - 2207.9 + Z	3s3p3d - 3s3p4f	<sup>3</sup> F - <sup>3</sup> G	1 - 1		241
	96.50		1180.0 + Y - 2216.3 + Y	3s3p3d - 3s3p4f	<sup>3</sup> F - <sup>3</sup> G	1 - 1		241
	101.39		408.66 - 1394.95	3s <sup>2</sup> 3d - 3s <sup>2</sup> 4f	<sup>1</sup> D - <sup>3</sup> F	3 - 4		241
	101.46		408.84 - 1395.45	3s <sup>2</sup> 3d - 3s <sup>2</sup> 4f	<sup>1</sup> D - <sup>3</sup> F	3 - 4		241
	244.70		0 - 408.66	3s <sup>2</sup> 3p - 3s <sup>2</sup> 3d	g <sup>2</sup> P - <sup>1</sup> D	1 - 1		239
	251.52		12.261 - 409.84	3s <sup>2</sup> 3p - 3s <sup>2</sup> 3d	g <sup>2</sup> P - <sup>1</sup> D	1 - 1		239
	252.27		12.261 - 408.66	3s <sup>2</sup> 3p - 3s <sup>2</sup> 3d	g <sup>2</sup> P - <sup>1</sup> D	1 - 1	P	267
	294.77		0 - 339.25	3s <sup>2</sup> 3p - 3s3p <sup>2</sup>	g <sup>2</sup> P - <sup>3</sup> P	1 - 1		239
	300.08		0 - 333.24	3s <sup>2</sup> 3p - 3s3p <sup>2</sup>	g <sup>2</sup> P - <sup>3</sup> P	1 - 1	P	251
	305.81		12.261 - 339.25	3s <sup>2</sup> 3p - 3s3p <sup>2</sup>	g <sup>2</sup> P - <sup>3</sup> P	1 - 1		239
	311.55		12.261 - 333.24	3s <sup>2</sup> 3p - 3s3p <sup>2</sup>	g <sup>2</sup> P - <sup>3</sup> P	1 - 1		239
	318.89		0 - 313.58	3s <sup>2</sup> 3p - 3s3p <sup>2</sup>	g <sup>2</sup> P - <sup>3</sup> S	1 - 1	P	239
	320.20		188.84 + W - 501.15 + W	3s3p <sup>2</sup> - 3p	<sup>3</sup> P - <sup>3</sup> S	1 - 1		239
	325.13		193.58 + W - 501.15 + W	3s3p <sup>2</sup> - 3p	<sup>3</sup> P - <sup>3</sup> S	1 - 1		239
	331.87		12.261 - 313.58	3s <sup>2</sup> 3p - 3s3p <sup>2</sup>	g <sup>2</sup> P - <sup>3</sup> S	1 - 1	P	239
	332.06		200.00 + W - 501.15 + W	3s3p <sup>2</sup> - 3p	<sup>3</sup> P - <sup>3</sup> S	1 - 1		239
	393.00		0 - 254.45	3s <sup>2</sup> 3p - 3s3p <sup>2</sup>	g <sup>2</sup> P - <sup>1</sup> D	1 - 1		239
	410.91		12.261 - 255.62	3s <sup>2</sup> 3p - 3s3p <sup>2</sup>	g <sup>2</sup> P - <sup>1</sup> D	1 - 1		239
	412.90		12.261 - 254.45	3s <sup>2</sup> 3p - 3s3p <sup>2</sup>	g <sup>2</sup> P - <sup>1</sup> D	1 - 1	P	239

**CHROMIUM XIII (Cr<sup>12+</sup>), Z = 24**  
**Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>6</sup>3s<sup>2</sup>(<sup>1</sup>S<sub>0</sub>) (12 electrons)**  
**Ionization Potential [2 862 000] cm<sup>-1</sup>; [354.8] eV**

Multiplet	Rel. Int.	$\lambda_{\infty}$ (in Å)	Levels (in 10 <sup>3</sup> cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
	40.92		0.0 - 2443.80	3s <sup>2</sup> - 3s7p	g <sup>1</sup> S - <sup>1</sup> P	0 - 1		851
	43.75		0.0 - 2285.70	3s <sup>2</sup> - 3s6p	g <sup>1</sup> S - <sup>1</sup> P	0 - 1		851
	47.26		203.45 - 2319.45	3s3p - 3s6d	<sup>1</sup> P - <sup>1</sup> D	0 - 1		851
	47.34		207.38 - 2319.78	3s3p - 3s6d	<sup>1</sup> P - <sup>1</sup> D	1 - 2		851
	47.55		216.57 - 2319.57	3s3p - 3s6d	<sup>1</sup> P - <sup>1</sup> D	2 - 3		851
	49.03		216.57 - 2256.17	3s3p - 3s6s	<sup>1</sup> P - <sup>3</sup> S	2 - 1		851
	49.59		0.0 - 2016.50	3s <sup>2</sup> - 3s5p	g <sup>1</sup> S - <sup>1</sup> P	0 - 1		851
	53.02		590.08 - 2476.18	3s3d - 3s7f	<sup>1</sup> D - <sup>3</sup> F	3 - 4		851
	53.39		203.45 - 2076.45	3s3p - 3s5d	<sup>1</sup> P - <sup>1</sup> D	0 - 1		851
50	53.506		207.38 - 2076.33	3s3p - 3s5d	<sup>1</sup> P - <sup>1</sup> D	1 - 2		180
100	53.765		216.57 - 2076.52	3s3p - 3s5d	<sup>1</sup> P - <sup>1</sup> D	2 - 3		180
	56.37		304.61 - 2078.61	3s3p - 3s5d	<sup>1</sup> P - <sup>1</sup> D	1 - 2		851
	56.96		207.38 - 1963.00	3s3p - 3s5s	<sup>1</sup> P - <sup>3</sup> S	1 - 1		851
	57.24		590.08 - 2337.08	3s3d - 3s6f	<sup>1</sup> D - <sup>3</sup> F	3 - 4		851
	65.04		216.57 - 1754.07	3s3p - 3p4p	<sup>1</sup> P - <sup>3</sup> S	2 - 1		851
	65.13		216.57 - 1751.97	3s3p - 3p4p	<sup>1</sup> P - <sup>3</sup> P	2 - 2		851
	65.39		216.57 - 1745.87	3s3p - 3p4p	<sup>1</sup> P - <sup>1</sup> D	2 - 3		851
50	65.968		590.08 - 2105.97	3s3d - 3s5f	<sup>1</sup> D - <sup>3</sup> F	3 - 4		180

Multiplet Ref. Int. $\lambda_{\text{c}}$ (m Å)	Levels (m 10 <sup>-3</sup> cm <sup>-1</sup> )	Configurations	Terms	J, J	Notes	References
200	66 983	0 0 - 1492 92	<sup>3</sup> S - <sup>3</sup> P	0 - 1		180
100	70 792	203 45 - 1616 04	<sup>3</sup> P - <sup>3</sup> D	0 - 1		180
300	70 973	207 38 - 1616 37	<sup>3</sup> P - <sup>3</sup> D	1 - 2		180
300	71 398	216 57 - 1617 17	<sup>3</sup> P - <sup>3</sup> D	2 - 3		180
50	71 435	216 57 - 1616 37	<sup>3</sup> P - <sup>3</sup> D	2 - 2		180
	71 86	499 21 - 1890 81	<sup>3</sup> P - <sup>3</sup> D	2 - 2		851
	72 13	483 15 - 1869 55	<sup>3</sup> P' - <sup>3</sup> D	2 - 3		851
	72 27	482 14 - 1865 84	<sup>3</sup> P' - <sup>3</sup> D	0 - 1		851
	72 57	488 22 - 1866 22	<sup>3</sup> P' - <sup>3</sup> D	1 - 2		851
	72 88	499 21 - 1871 31	<sup>3</sup> P' - <sup>3</sup> D	2 - 3		851
	73 31	483 15 - 1847 25	<sup>3</sup> P' - <sup>3</sup> D	2 - 3		851
	76 17	304 61 - 1617 46	<sup>3</sup> 3p - <sup>3</sup> 4d	1 - 2		854
50	82 79	483 15 - 1690 71	<sup>3</sup> P' - <sup>3</sup> 4d	2 - 3		854
200	84 616	203 45 - 1385 26	<sup>3</sup> 3p - <sup>3</sup> 4s	0 - 1		180
200	84 898	207 38 - 1385 26	<sup>3</sup> 3p - <sup>3</sup> 4s	1 - 1		180
300	85 566	216 57 - 1385 26	<sup>3</sup> 3p - <sup>3</sup> 4s	2 - 1		180
	86 78	499 21 - 1651 51	<sup>3</sup> P' - <sup>3</sup> 4s	2 - 2		851
	89 99	818 89 - 1930 09	<sup>3</sup> 3d - <sup>3</sup> 4d	4 - 5		241
	90 02	805 20 - 1916 06	<sup>3</sup> 3d - <sup>3</sup> 4d	2 - 3		241
	90 17	811 53 - 1920 53	<sup>3</sup> 3d - <sup>3</sup> 4d	3 - 4		241
	90 85	824 54 + K - 1925 24 + K	<sup>3</sup> 3d - <sup>3</sup> 4d	2 - 3		241
200	91 30	304 61 - 1399 91	<sup>3</sup> 3p - <sup>3</sup> 4s	1 - 0		851
200	91 749	588 56 - 1678 49	<sup>3</sup> 3d - <sup>3</sup> 4d	1 - 2		180
300	91 792	589 19 - 1678 61	<sup>3</sup> 3d - <sup>3</sup> 4d	2 - 3		180
400	91 855	590 08 - 1678 75	<sup>3</sup> 3d - <sup>3</sup> 4d	3 - 4		180
	92 01	852 11 + R - 1938 91 + R	<sup>3</sup> 3d - <sup>3</sup> 4d	0 - 1		241
	92 16	853 81 + R - 1938 91 + R	<sup>3</sup> 3d - <sup>3</sup> 4d	1 - 1		241
	92 37	857 34 + R - 1939 94 + R	<sup>3</sup> 3d - <sup>3</sup> 4d	2 - 2		241
	92 61	860 99 - 1940 79	<sup>3</sup> 3d - <sup>3</sup> 4d	3 - 3		241
	93 42	860 99 - 1931 42	<sup>3</sup> 3d - <sup>3</sup> 4d	3 - 4		241
	96 86	820 00 + L - 1852 40 + L	<sup>3</sup> 3d - <sup>3</sup> 4d	3 - 4		241
	97 25	662 24 - 1690 71	<sup>3</sup> 3d - <sup>3</sup> 4d	2 - 3		854
	248 66	483 15 - 885 30	<sup>3</sup> P' - <sup>3</sup> 4d	2 - 1	P	375
	259 68	203 45 - 588 56	<sup>3</sup> 3p - <sup>3</sup> 3d	0 - 1		854
	261 91	207 38 - 589 19	<sup>3</sup> 3p - <sup>3</sup> 3d	1 - 2		854
	262 33	207 38 - 588 56	<sup>3</sup> 3p - <sup>3</sup> 3d	1 - 1		854
	267 73	216 57 - 590 08	<sup>3</sup> 3p - <sup>3</sup> 3d	2 - 3		854
	276 61	499 21 - 860 99	<sup>3</sup> P' - <sup>3</sup> D	2 - 3	P	251
	279 32	499 21 - 857 21	<sup>3</sup> P' - <sup>3</sup> D	2 - 2		854
	279 62	304 61 - 662 24	<sup>3</sup> 3p - <sup>3</sup> 3d	1 - 2	P	854
	316 60	569 44 - 885 30	<sup>3</sup> P' - <sup>3</sup> D	0 - 1	P	251
150	328 29	0 0 - 304 61	<sup>3</sup> S - <sup>3</sup> P	0 - 1		270, A37
	342 69	207 38 - 499 21	<sup>3</sup> 3p - <sup>3</sup> P'	1 - 2		270
	351 16	203 45 - 448 22	<sup>3</sup> 3p - <sup>3</sup> P'	0 - 1	P	270
	353 81	216 57 - 499 21	<sup>3</sup> 3p - <sup>3</sup> P'	2 - 2		270
	356 07	207 38 - 448 22	<sup>3</sup> 3p - <sup>3</sup> P'	1 - 1	P	270
	363 96	207 38 - 442 14	<sup>3</sup> 3p - <sup>3</sup> P'	1 - 0		270
	368 12	216 57 - 448 22	<sup>3</sup> 3p - <sup>3</sup> P'	2 - 1	P	270
	369 13	590 08 - 860 99	<sup>3</sup> 3d - <sup>3</sup> 3d	3 - 3		251
	377 60	304 61 - 569 44	<sup>3</sup> 3p - <sup>3</sup> P'	1 - 0		242
	437 05	590 08 - 818 89	<sup>3</sup> 3d - <sup>3</sup> 3d	3 - 4	P	251
	448 31	662 24 - 885 30	<sup>3</sup> 3d - <sup>3</sup> 3d	2 - 1		375
	449 76	589 19 - 811 53	<sup>3</sup> 3d - <sup>3</sup> 3d	2 - 3		242
	461 60	588 56 - 805 20	<sup>3</sup> 3d - <sup>3</sup> 3d	1 - 2		251

## CR XIV — Continued

Multiplet	Rel Int	$\lambda$ , (m Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	482.2		0 0 - 207.38	$3s^2 - 3s3p$	$g^2S - ^1P^o$	0 - 1		1131
	560.11		304.61 - 483.15	$3s3p - 3p^2$	$^1P^o - ^3D$	1 - 2	P	854

**CHROMIUM XIV ( $\text{Cr}^{13+}$ ),  $Z = 24$   
 Ground State  $1s^2 2s^2 2p^6 3s^2 (^4S_{1/2})$  (11 electrons)  
 Ionization Potential  $3\ 098\ 500 \text{ cm}^{-1}$ ;  $384.17 \text{ eV}$**

Multiplet	Rel Int	$\lambda$ , (m Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
		21.467	0 - 4658.3	$2p^3 3s - 2p^3 3s^2$	$g^2S - ^1P^o$			265
		21.770	0 - 4593.5	$2p^3 3s - 2p^3 3s^2$	$g^2S - ^1P^o$			265
0	35.450		0 - 2820.87	$2p^3 3s - 2p^3 3p$	$g^2S - ^1P^o$			118
2	36.466		0 - 2742.280	$2p^3 3s - 2p^3 3p$	$g^2S - ^1P^o$			118
8	38.036		0 - 2629.088	$2p^3 3s - 2p^3 7p$	$g^2S - ^1P^o$			118
0	38.679		242.724 - 2828.106	$2p^3 3p - 2p^3 9d$	$^1P^o - ^3D$			118
0	38.899		256.535 - 2827.295	$2p^3 3p - 2p^3 9d$	$^1P^o - ^3D$			118
1	39.796		242.724 - 2755.539	$2p^3 3p - 2p^3 8d$	$^1P^o - ^3D$			118
2	40.018		256.535 - 2755.410	$2p^3 3p - 2p^3 8d$	$^1P^o - ^3D$			118
7	40.782		0 - 2452.062	$2p^3 3s - 2p^3 6p$	$g^2S - ^1P^o$			118
10	40.800		0 - 2450.980	$2p^3 3s - 2p^3 6p$	$g^2S - ^1P^o$			118
2	41.556		242.724 - 2649.115	$2p^3 3p - 2p^3 7d$	$^1P^o - ^3D$			118
2	41.788		256.535 - 2649.566	$2p^3 3p - 2p^3 7d$	$^1P^o - ^3D$			118
	42.453		256.535 - 2612.081	$2p^3 3p - 2p^3 7s$	$^1P^o - ^3S$			118
3	44.597		242.724 - 2485.027	$2p^3 3p - 2p^3 6d$	$^1P^o - ^3D$			118
4	44.869		256.535 - 2485.245	$2p^3 3p - 2p^3 6d$	$^1P^o - ^3D$			118
15	45.835		242.724 - 2424.510	$2p^3 3p - 2p^3 6s$	$^1P^o - ^3S$			118
1	46.039		589.568 - 2761.639	$2p^3 3d - 2p^3 8f$	$^1D - ^3F^o$			118
5	46.125		256.535 - 2424.510	$2p^3 3p - 2p^3 6s$	$^1P^o - ^3S$			118
55	46.468		0 - 2152.018	$2p^3 3s - 2p^3 5p$	$g^2S - ^1P^o$			118
12	46.527		0 - 2146.289	$2p^3 3s - 2p^3 5p$	$g^2S - ^1P^o$			118
2	48.308		587.867 - 2658.260	$2p^3 3d - 2p^3 7f$	$^1D - ^3F^o$			118
3	48.338		589.568 - 2658.333	$2p^3 3d - 2p^3 7f$	$^1D - ^3F^o$			118
3	50.821		242.724 - 2210.414	$2p^3 3p - 2p^3 5d$	$^1P^o - ^3D$			118
4	51.172		256.535 - 2210.728	$2p^3 3p - 2p^3 5d$	$^1P^o - ^3D$			118
2	52.321		587.867 - 2499.145	$2p^3 3d - 2p^3 6f$	$^1D - ^3F^o$			118
3	52.363		589.568 - 2499.313	$2p^3 3d - 2p^3 6f$	$^1D - ^3F^o$			118
25	53.760		242.724 - 2102.811	$2p^3 3p - 2p^3 5s$	$^1P^o - ^3S$			118
20	54.164		256.535 - 2102.811	$2p^3 3p - 2p^3 5s$	$^1P^o - ^3S$			118
8	60.699		587.867 - 2235.25	$2p^3 3d - 2p^3 5f$	$^1D - ^3F^o$			118
10	60.756		589.568 - 2235.28	$2p^3 3d - 2p^3 5f$	$^1D - ^3F^o$			118
70	63.324		0 - 1579.180	$2p^3 3s - 2p^3 4p$	$g^2S - ^1P^o$			118
60	63.539		0 - 1573.836	$2p^3 3s - 2p^3 4p$	$g^2S - ^1P^o$			118
4	64.005		589.568 - 2152.018	$2p^3 3d - 2p^3 5p$	$^1D - ^3P^o$			118
10	68.594		242.724 - 1700.577	$2p^3 3p - 2p^3 4d$	$^1P^o - ^3D$			118
20	69.213		256.535 - 1701.350	$2p^3 3p - 2p^3 4d$	$^1P^o - ^3D$			118
10	69.247		256.535 - 1700.577	$2p^3 3p - 2p^3 4d$	$^1P^o - ^3D$			118
25	80.916		242.724 - 1478.517	$2p^3 3p - 2p^3 4s$	$^1P^o - ^3S$			118
30	81.838		256.535 - 1478.517	$2p^3 3p - 2p^3 4s$	$^1P^o - ^3S$			118
27	86.057		587.867 - 1749.887	$2p^3 3d - 2p^3 4f$	$^1D - ^3F^o$			118
28	86.164		589.568 - 1750.145	$2p^3 3d - 2p^3 4f$	$^1D - ^3F^o$			118
10	101.05		589.568 - 1579.180	$2p^3 3d - 2p^3 4p$	$^1D - ^3P^o$			118

## CR XIV - Continued

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
12	101.42		587.867 - 1573.836	$2p^4 3d - 2p^4 4p$	$^1D - ^1P$	- -	-	118
10	187.02		1700.577 - 2235.25	$2p^4 4d - 2p^4 5f$	$^1D - ^1F$	- -	-	1091
10	187.30		1701.350 - 2235.28	$2p^4 4d - 2p^4 5f$	$^1D - ^1F$	- -	-	1091
30	204.91		1749.887 - 2237.91	$2p^4 4f - 2p^4 5g$	$^1F - ^1G$	- -	-	1091
30	205.01		1750.145 - 2237.92	$2p^4 4f - 2p^4 5g$	$^1F - ^1G$	- -	-	1091
50	289.735		242.724 - 587.867	$2p^3 3p - 2p^3 3d$	$^1P - ^1D$	- -	-	118, 437
	300.271		256.535 - 589.568	$2p^3 3p - 2p^3 3d$	$^1P - ^1D$	- -	-	118
	301.814		256.535 - 587.867	$2p^3 3p - 2p^3 3d$	$^1P - ^1D$	- -	-	118
250	389.81		0 - 256.535	$2p^3 s - 2p^3 3p$	$g^1S - ^1P$	- -	-	270, 437
200	411.99		0 - 242.724	$2p^3 s - 2p^3 3p$	$g^1S - ^1P$	- -	-	270, 437

**CHROMIUM XV ( $\text{Cr}^{14+}$ ), Z = 24**  
**Ground State  $1s^2 2s^2 2p^6 (^1S_0)$  (10 electrons)**  
**Ionization Potential 8 151 000  $\text{cm}^{-1}$ ; 1010.6 eV**

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
10	13.294		0.0 - 7522.2	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3d$	$g^1S - \frac{3}{2} \frac{3}{2} \frac{1}{2}$	0 - 1		716
10	13.416		0.0 - 7453.8	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3d$	$g^1S - \frac{3}{2} \frac{3}{2} \frac{1}{2}$	0 - 1		716
20	13.862		0.0 - 7214.0	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3d$	$g^1S - \frac{3}{2} \frac{3}{2} \frac{1}{2}$	0 - 1		716
20	13.991		0.0 - 7147.4	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3d$	$g^1S - \frac{3}{2} \frac{3}{2} \frac{1}{2}$	0 - 1		716
10	15.509		0.0 - 6447.9	$2s^2 2p^4 - 2s^2 2p^4 (^1F^o) 4s$	$g^1S - ^1P$	0 - 1		716
20	15.788		0.0 - 6333.9	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 4s$	$g^1S - ^1P$	0 - 1		716
100	16.889		0.0 - 5921.0	$2s^2 2p^4 - 2s^2 2p^4 (^1S) 3p$	$g^1S - ^1P$	0 - 1		716
50	16.971		0.0 - 5894.5	$2s^2 2p^4 - 2s^2 2p^4 (^1S) 3p$	$g^1S - ^1P$	0 - 1		716
400	18.497		0.0 - 5406.3	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3d$	$g^1S - \frac{3}{2} \frac{3}{2} \frac{1}{2}$	0 - 1		766
200	18.782		0.0 - 5324.2	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3d$	$g^1S - \frac{3}{2} \frac{3}{2} \frac{1}{2}$	0 - 1		766
50	19.015		0.0 - 5259.0	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3d$	$g^1S - \frac{3}{2} \frac{3}{2} \frac{1}{2}$	0 - 1		766
400	20.863		0.0 - 4793.2	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3s$	$g^1S - (\frac{3}{2}, \frac{3}{2})$	0 - 1		766
300	21.153		0.0 - 4727.5	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3s$	$g^1S - (\frac{3}{2}, \frac{3}{2})$	0 - 1		766
	21.213		0.0 - 4714.1	$2s^2 2p^4 - 2s^2 2p^4 (^1P^o) 3s$	$g^1S - \frac{3}{2} \frac{3}{2} \frac{1}{2}$	0 - 2	F	1112
	52.88	5269.0 + C - 7160.1 + F		$2s^2 2p^4 (^1P^o) 3d - 2s^2 2p^4 (^1P^o) 3f$	$^1F - \frac{3}{2} \frac{3}{2} \frac{1}{2}$	4 - 5	P	1055
	58.02	4714.1 - 6437.6		$2s^2 2p^4 (^1P^o) 3s - 2s^2 2p^4 (^1P^o) 4p$	$\frac{3}{2} \frac{3}{2} \frac{1}{2} - ^1D$	2 - 3		1055
	58.20	4793.2 - 6511.4		$2s^2 2p^4 (^1P^o) 3s - 2s^2 2p^4 (^1P^o) 4p$	$(\frac{3}{2}, \frac{3}{2}) - ^1P$	1 - 1		1055
	62.375	4961.0 + C - 6566.2 + C		$2s^2 2p^4 (^1P^o) 3p - 2s^2 2p^4 (^1P^o) 4d$	$^1P - ^1D$	1 - 2		395
	62.481	4946.1 + C - 6546.6 + C		$2s^2 2p^4 (^1P^o) 3p - 2s^2 2p^4 (^1P^o) 4d$	$^1D - ^1D$	2 - 3		395
	62.837	4954.1 + C - 6545.5 + C		$2s^2 2p^4 (^1P^o) 3p - 2s^2 2p^4 (^1P^o) 4d$	$^1D - ^1F$	3 - 4		395
	62.951	5040.9 + C - 6629.4 + C		$2s^2 2p^4 (^1P^o) 3p - 2s^2 2p^4 (^1P^o) 4d$	$^1P - ^1F$	1 - 2		395
	63.055	5042.9 + C - 6628.8 + C		$2s^2 2p^4 (^1P^o) 3p - 2s^2 2p^4 (^1P^o) 4d$	$^1D - ^1F$	2 - 3		395
	63.31	4974.6 + C - 6554.1 + C		$2s^2 2p^4 (^1P^o) 3p - 2s^2 2p^4 (^1P^o) 4d$	$^1P - ^1F$	2 - 3	P	395
	74.70	5255.0 + C - 6593.7 + C		$2s^2 2p^4 (^1P^o) 3d - 2s^2 2p^4 (^1P^o) 4f$	$^1P - \frac{3}{2} \frac{3}{2}$	2 - 2		1055
	74.97	5269.0 + C - 6602.9 + C		$2s^2 2p^4 (^1P^o) 3d - 2s^2 2p^4 (^1P^o) 4f$	$^1F - \frac{3}{2} \frac{3}{2}$	4 - 5		1055
	75.25	5312.1 + C - 6641.0 + C		$2s^2 2p^4 (^1P^o) 3d - 2s^2 2p^4 (^1P^o) 4f$	$^1F - \frac{3}{2} \frac{3}{2}$	2 - 3		1055
	75.29	5274.3 + C - 6602.5 + C		$2s^2 2p^4 (^1P^o) 3d - 2s^2 2p^4 (^1P^o) 4f$	$^1F - \frac{3}{2} \frac{3}{2}$	3 - 4		1055
	75.44	5360.5 + C - 6686.1 + C		$2s^2 2p^4 (^1P^o) 3d - 2s^2 2p^4 (^1P^o) 4f$	$^1F - \frac{3}{2} \frac{3}{2}$	3 - 3		1055
	75.73	5360.5 + C - 6681.0 + C		$2s^2 2p^4 (^1P^o) 3d - 2s^2 2p^4 (^1P^o) 4f$	$^1F - \frac{3}{2} \frac{3}{2}$	3 - 4		1055
	76.14	5292.4 + C - 6605.8 + C		$2s^2 2p^4 (^1P^o) 3d - 2s^2 2p^4 (^1P^o) 4f$	$^1D - \frac{3}{2} \frac{3}{2}$	3 - 4		1055



**CHROMIUM XVI (Cr<sup>15+</sup>), Z = 24**  
**Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>4</sup>(<sup>3</sup>P<sub>2,2</sub>) ( 9 electrons)**  
**Ionization Potential [8 850 000] cm<sup>-1</sup>; [1097] eV**

Multiplet	Rel. Int.	$\lambda_{\alpha}$ (in Å)	Levels (in 10 <sup>3</sup> cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
3	13.528		0.0 - 7392.1	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> D)4d	g <sup>1</sup> P <sup>o</sup> - <sup>2</sup> S	-		1089
10	13.556		0.0 - 7376.8	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> S)4d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		716
10	13.953		0.0 - 7166.9	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)4d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		716
10	14.039		0.0 - 7123.0	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)4d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-	Q	716
	14.29		0.0 - 6997.9	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)4d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-	P	716
	14.47		0.0 - 6910.8	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> S)4s	g <sup>1</sup> P <sup>o</sup> - <sup>2</sup> S	-		716
30	17.073		0.0 - 5857.2	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> S)3d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		850
50	17.242		70.890 - 5870.7	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> S)3d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		850
80	17.370		0.0 - 5757.1	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		850
60	17.438		0.0 - 5734.6	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> D)3d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> S	-		850
30	17.514		70.890 - 5780.6	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		850
20	17.589		70.890 - 5756.2	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> D)3d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
50	17.603		0.0 - 5680.8	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		850
20	17.633		0.0 - 5671.2	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
40	17.671		0.0 - 5659.0	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> F	-		850
20	17.704		0.0 - 5648.5	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		850
30	17.730		0.0 - 5640.2	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
50	17.785		0.0 - 5622.7	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> F	-		850
20	17.793		0.0 - 5620.3	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
20	17.833		0.0 - 5607.7	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
20	17.856		70.890 - 5671.2	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
20	17.931		70.890 - 5648.5	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		850
30	17.993		70.890 - 5628.6	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
20	18.017		70.890 - 5620.3	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3d	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
300	18.775		0.0 - 5325.3	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> S)3s	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> S	-		850
80	19.038		70.890 - 5325.3	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> S)3s	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> S	-		850
150	19.255		0.0 - 5193.5	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> D)3s	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		850
60	19.442		0.0 - 5143.5	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3s	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
100	19.511		70.890 - 5196.2	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> D)3s	g <sup>1</sup> P <sup>o</sup> - <sup>1</sup> D	-		850
100	19.538		0.0 - 5118.2	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3s	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
200	19.714		70.890 - 5143.5	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3s	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
100	19.807		0.0 - 5048.7	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3s	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
10	19.847		70.890 - 5109.4	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3s	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
60	19.921		937.829 - 5950.3	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3s	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
20	19.995		70.890 - 5072.4	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3s	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> P	-		850
300	106.629		0.0 - 937.829	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup>	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> S	-	P	1104,1091
250	115.348		70.890 - 937.829	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup>	g <sup>1</sup> P <sup>o</sup> - <sup>3</sup> S	-	P	1104,1091
	1410.6		0.0 - 70.890	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup>	g <sup>1</sup> P <sup>o</sup> - g <sup>1</sup> P <sup>o</sup>	-	F.P	1137

**CHROMIUM XVII (Cr<sup>16+</sup>), Z = 24**  
**Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>4</sup>(<sup>3</sup>P<sub>2</sub>) ( 8 electrons)**  
**Ionization Potential [9 560 000] cm<sup>-1</sup>; [1185] eV**

Multiplet	Rel. Int.	$\lambda_{\alpha}$ (in Å)	Levels (in 10 <sup>3</sup> cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
30	16.221		0.0 - 6164.8	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3d	g <sup>1</sup> P - <sup>1</sup> D'	2 - 3		877
30	16.249		60.378 - 6214.6	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3d	g <sup>1</sup> P - <sup>1</sup> D'	1 - 2		877
30	16.31		58.146 - 6189.4	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> P)3d	g <sup>1</sup> P - <sup>1</sup> D'	0 - 1		877
90	16.455		0.0 - 6075.3	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P - <sup>1</sup> D'	2 - 3		716
10	16.64		60.378 - 6070.0	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>1</sup> D)3d	g <sup>1</sup> P - <sup>1</sup> D'	1 - 2		877
40	16.675		263.00 - 6260.3	2s <sup>2</sup> 2p <sup>4</sup> - 2s <sup>2</sup> 2p <sup>4</sup> ( <sup>3</sup> P)3d	g <sup>1</sup> P - <sup>3</sup> P'	0 - 1	P	947

## CR XVII - Continued

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
	10	16.696	135.10 - 6124.6	$2s^2 2p^4 - 2s^2 2p^3(^1D^o)3d$	$^1D - ^1F^o$	2-3		877
		16.773	135.10 - 6096.0	$2s^2 2p^4 - 2s^2 2p^3(^1D^o)3d$	$^1D - ^1D^o$	2-2	P	877
	10	16.811	0.0 - 5948.5	$2s^2 2p^4 - 2s^2 2p^3(^1S^o)3d$	$g^1P - ^1D^o$	2-3		877
	150	17.957	0.0 - 5568.9	$2s^2 2p^4 - 2s^2 2p^3(^1D^o)3s$	$g^1P - ^1D^o$	2-3		865
	50	17.968	135.10 - 5701.0	$2s^2 2p^4 - 2s^2 2p^3(^1P^o)3s$	$^1D - ^1P^o$	2-1		865
	150	18.020	0.0 - 5549.3	$2s^2 2p^4 - 2s^2 2p^3(^1D^o)3s$	$g^1P - ^1D^o$	2-2		865
	50	18.219	60.378 - 5549.3	$2s^2 2p^4 - 2s^2 2p^3(^1D^o)3s$	$g^1P - ^1D^o$	1-2		865
	200	18.336	0.0 - 5453.9	$2s^2 2p^4 - 2s^2 2p^3(^1S^o)3s$	$g^1P - ^1S^o$	2-1		865
	50	18.389	263.00 - 5731.0	$2s^2 2p^4 - 2s^2 2p^3(^1P^o)3s$	$^1S - ^1P^o$	0-1		865
		18.52	0.0 - 5399.4 + K	$2s^2 2p^4 - 2s^2 2p^3(^1S^o)3s$	$g^1P - ^1S^o$	2-2	P	680
	150	18.531	60.378 - 5453.9	$2s^2 2p^4 - 2s^2 2p^3(^1S^o)3s$	$g^1P - ^1S^o$	1-1		865
		18.73	60.378 - 5399.4 + K	$2s^2 2p^4 - 2s^2 2p^3(^1S^o)3s$	$g^1P - ^1S^o$	1-2	P	680
	150	89.57	0.0 - 1116.42	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1P^o$	2-1		1091
	10	94.49	58.146 - 1116.42	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1P^o$	0-1		1091
	4	94.69	60.378 - 1116.42	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1P^o$	1-1		1091
	30	97.20	858.15 - 1886.95	$2s^2 2p^4 - 2p^6$	$^1P^o - ^1S$	1-0		1091
	250	101.91	135.10 - 1116.42	$2s^2 2p^4 - 2s^2 2p^3$	$^1D - ^1P^o$	2-1		1091
	250	116.53	0.0 - 858.15	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1P^o$	2-1		1091
	110	117.20	263.00 - 1116.42	$2s^2 2p^4 - 2s^2 2p^3$	$^1S - ^1P^o$	0-1		1091
	200	120.84	60.378 - 887.92	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1P^o$	1-0		1091
	375	122.91	0.0 - 813.60	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1P^o$	2-2		1091
	150	125.00	58.146 - 858.15	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1P^o$	0-1		1091
	200	125.35	60.378 - 858.15	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1P^o$	1-1		1091
	200	129.78	1116.42 - 1886.95	$2s^2 2p^4 - 2p^6$	$^1P^o - ^1S$	1-0		1091
	250	132.76	60.378 - 813.60	$2s^2 2p^4 - 7s^2 2p^4$	$g^1P - ^1P^o$	1-2		1091
	10	147.40	135.10 - 813.60	$2s^2 2p^4 - 2s^2 2p^3$	$^1D - ^1P^o$	2-2		1091
		380.2	0.0 - 263.00	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1S$	2-0	F,P	375,1091
		493.8	60.378 - 263.00	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1S$	1-0	F	1120
		740.8	0.0 - 135.10	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1D$	2-2	F	1120
		781.9	135.10 - 263.00	$2s^2 2p^4 - 2s^2 2p^3$	$^1D - ^1S$	2-0	F,P	375,1091
	1299.		58.146 - 135.10	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1D$	0-2	F,P	375,1091
	1338		60.378 - 135.10	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - ^1D$	1-2	F,P	375,1091
	1656.3		0.0 - 60.378	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - g^1P$	2-1	F	1120
	1720.		0.0 - 58.146	$2s^2 2p^4 - 2s^2 2p^3$	$g^1P - g^1P$	2-0	F,P	375,1091

CHROMIUM XVIII (Cr<sup>17+</sup>), Z = 24Ground State  $1s^2 2s^2 2p^3(^4S_{3/2})$  (7 electrons)Ionization Potential [10 480 000] cm<sup>-1</sup>; [1299] eV

Multiplet	Rel. Int.	$\lambda_{vac}$ (in Å)	Levels (in $10^3$ cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
		15.501	126.040 - 6577.2 + F	$2s^2 2p^3 - 2s^2 2p^2(^1D)3d$	$^1D^o - ^1F$	-	P	877
		15.512	0.0 - 6446.6 + F	$2s^2 2p^3 - 2s^2 2p^2(^1P)3d$	$g^4S^o - ^4P$	-	P	877
	10	15.52	0.0 - 6443.3	$2s^2 2p^3 - 2s^2 2p^2(^1P)3d$	$g^4S^o - ^4P$	-		877
		15.550	150.776 - 6581.7 + F	$2s^2 2p^3 - 2s^2 2p^2(^1D)3d$	$^1D^o - ^1P$	-	P	877
	20	15.587	150.776 - 6564.7	$2s^2 2p^3 - 2s^2 2p^2(^1D)3d$	$^1D^o - ^1F$	-	Q	716,877
		15.835	150.776 - 6466.0 + F	$2s^2 2p^3 - 2s^2 2p^2(^1P)3d$	$^1D^o - ^1F$	-	I	877
		16.292	264.482 - 6402.5 + F	$2s^2 2p^3 - 2s^2 2p^2(^1P)3d$	$^1P^o - ^1P$	-	P	877
	50	90.63	0.0 - 1103.35	$2s^2 2p^3 - 2s^2 2p^2$	$g^4S^o - ^4P$	-		1091
	10	93.36	667.56 - 1738.69	$2s^2 2p^3 - 2p^6$	$^1P^o - ^1P^o$	-		1091
	4	94.16	0.0 - 1062.04	$2s^2 2p^3 - 2s^2 2p^2$	$g^4S^o - ^4S$	-		1091
	150	95.77	126.040 - 1170.20	$2s^2 2p^3 - 2s^2 2p^2$	$^1D^o - ^1P$	-		1091
	150	102.32	126.040 - 1103.35	$2s^2 2p^3 - 2s^2 2p^2$	$^1D^o - ^1P$	-		1091

CR XVIII — Continued

Multiplet	Rel Int	$\lambda$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
300	104 98		150 776 - 1103 35	$2s^2 2p^1 - 2s 2p^4$	$^1D^{\circ} - ^1P$	- -		1091
10	105 92		226 068 - 1170 20	$2s^2 2p^1 - 2s 2p^4$	$^1P^{\circ} - ^1P$	- -		1091
150	106 84		126 040 - 1062 04	$2s^2 2p^1 - 2s 2p^4$	$^1D^{\circ} - ^1S$	- -		1091
10	108 37		0 0 - 922 77	$2s^2 2p^1 - 2s 2p^4$	$g^4 S^{\circ} - ^1D$	- -		1091
375	110 41		264 482 - 1170 20	$2s^2 2p^1 - 2s 2p^4$	$^1P^{\circ} - ^1P$	- -		1091
110	112 27		922 77 - 1813 47	$2s 2p^4 - 2p^1$	$^1D - ^1P^{\circ}$	- -		1091
300	113 99		226 068 - 1103 35	$2s^2 2p^1 - 2s 2p^4$	$^1P^{\circ} - ^1P$	- -		1091
110	119 21		264 482 - 1103 35	$2s^2 2p^1 - 2s 2p^4$	$^1P^{\circ} - ^1P$	- -		1091
200	119 62		226 068 - 1062 04	$2s^2 2p^1 - 2s 2p^4$	$^1P^{\circ} - ^1S$	- -		1091
80	122 56		922 77 - 1738 69	$2s 2p^4 - 2p^1$	$^1D - ^1P^{\circ}$	- -		1091
250	123 87		931 41 - 1738 69	$2s 2p^4 - 2p^1$	$^1D - ^1P^{\circ}$	- -		1091
200	125 38		264 482 - 1062 04	$2s^2 2p^1 - 2s 2p^4$	$^1P^{\circ} - ^1S$	- -		1091
300	125 51		126 040 - 922 77	$2s^2 2p^1 - 2s 2p^4$	$^1D^{\circ} - ^1D$	- -		1091
375	128 10		150 776 - 931 41	$2s^2 2p^1 - 2s 2p^4$	$^1D^{\circ} - ^1D$	- -		1091
150	136 52		0 0 - 732 49	$2s^2 2p^1 - 2s 2p^4$	$g^4 S^{\circ} - ^4P$	- -		1091
375	139 87		0 0 - 714 95	$2s^2 2p^1 - 2s 2p^4$	$g^4 S^{\circ} - ^4P$	- -		1091
110	140 82		1103 35 - 1813 47	$2s 2p^4 - 2p^1$	$^1P - ^1P^{\circ}$	- -		1091
50	143 53		226 068 - 922 77	$2s^2 2p^1 - 2s 2p^4$	$^1P^{\circ} - ^1D$	- -		1091
30	147 79		1062 04 - 1738 69	$2s 2p^4 - 2p^1$	$^1S - ^1P^{\circ}$	- -		1091
300	149 80		0 0 - 667 56	$2s^2 2p^1 - 2s 2p^4$	$g^4 S^{\circ} - ^4P$	- -		1091
200	149 94		264 482 - 931 41	$2s^2 2p^1 - 2s 2p^4$	$^1P^{\circ} - ^1D$	- -		1091
80	155 46		1170 20 - 1813 47	$2s 2p^4 - 2p^1$	$^1P - ^1P^{\circ}$	- -		1091
200	157 40		1103 35 - 1738 69	$2s 2p^4 - 2p^1$	$^1P - ^1P^{\circ}$	- -		1091
	378 10		0 0 - 264 482	$2s^2 2p^1 - 2s^2 2p^1$	$g^4 S^{\circ} - ^1P^{\circ}$	- -	F,P	375,1091
	442 34		0 0 - 226 068	$2s^2 2p^1 - 2s^2 2p^1$	$g^4 S^{\circ} - ^1P^{\circ}$	- -	F,P	375,1091
	663 24		0 0 - 150 776	$2s^2 2p^1 - 2s^2 2p^1$	$g^4 S^{\circ} - ^1D^{\circ}$	- -	F,P	375,1091
	722 32		126 040 - 264 482	$2s^2 2p^1 - 2s^2 2p^1$	$^1D^{\circ} - ^1P^{\circ}$	- -	F,P	375,1091
	793 3		0 0 - 126 040	$2s^2 2p^1 - 2s^2 2p^1$	$g^4 S^{\circ} - ^1D^{\circ}$	- -	F	1120
	879 46		150 776 - 264 482	$2s^2 2p^1 - 2s^2 2p^1$	$^1D^{\circ} - ^1P^{\circ}$	- -	F,P	375,1091
	999 72		126 040 - 226 068	$2s^2 2p^1 - 2s^2 2p^1$	$^1D^{\circ} - ^1P^{\circ}$	- -	F,P	375,1091
	1328		150 776 - 226 068	$2s^2 2p^1 - 2s^2 2p^1$	$^1D^{\circ} - ^1P^{\circ}$	- -	F,P	375,1091

CHROMIUM XIX ( $\text{Cr}^{18+}$ ),  $Z = 24$   
 Ground State  $1s^2 2s^2 2p^2 (^3P_0)$  (6 electrons)  
 Ionization Potential [11 260 000]  $\text{cm}^{-1}$ ; [1396] eV

Multiplet	Rel Int	$\lambda$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
	14 802		47 806 - 6803 5 + B	$2s^2 2p^1 - 2s^2 2p^3 d$	$g^1 P - ^1D^{\circ}$	1 - 2	P	949
	14 809		82 453 - 6835 0 + B	$2s^2 2p^1 - 2s^2 2p^3 d$	$g^1 P - ^1P^{\circ}$	2 - 2	P	949
10	14 836		82 453 - 6822 5 + B	$2s^2 2p^1 - 2s^2 2p^3 d$	$g^1 P - ^1D^{\circ}$	2 - 3	P	949,716
0	14 925		184 596 - 6885 7 + B	$2s^2 2p^1 - 2s^2 2p^3 d$	$^1D - ^1P^{\circ}$	2 - 1	Q	716,949
	15 027		82 453 - 6737 1 + B	$2s^2 2p^1 - 2s^2 2p^3 d$	$g^1 P - ^1P^{\circ}$	2 - 3	P	949
	15 180		298 87 - 6885 7 + B	$2s^2 2p^1 - 2s^2 2p^3 d$	$^1S - ^1P^{\circ}$	0 - 1	P	949
	15 251		184 596 - 6742 2 + B	$2s^2 2p^1 - 2s^2 2p^3 d$	$^1D - ^1D^{\circ}$	2 - 2	P	949
	15 301		686 83 - 7222 3 + F	$2s 2p^1 - 2s 2p^1 (^4P) 3d$	$^1D^{\circ} - ^1F$	3 - 4	P	877
	15 91		82 453 - 6367 6	$2s^2 2p^1 - 2s^2 2p^3 s$	$g^1 P - ^1P^{\circ}$	2 - 2	P	375
10	95 62		404 41 - 1450 73	$2s 2p^1 - 2p^1$	$^1S - ^1P$	2 - 2		1091
30	95 88		47 806 - 1090 68	$2s^2 2p^1 - 2s 2p^1$	$g^1 P - ^1P^{\circ}$	1 - 1		1091
110	104 18		0 0 - 959 88	$2s^2 2p^1 - 2s 2p^1$	$g^1 P - ^1S$	0 - 1		1091

## CR XIX - Continued

Multiplet	Rel. Int.	$\lambda_{\lambda}$ (in Å)	Levels (in $10^3$ cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
200	109.64		47.806 - 959.88	$2s^2p^2 - 2s2p^3$	$g^1P - ^1S^*$	1 - 1		1091
250	110.37		184.596 - 1090.68	$2s^2p^2 - 2s2p^3$	$^1D - ^1P^*$	2 - 1		1091
50	111.18		686.83 - 1586.24	$2s2p^2 - 2p^4$	$^1D - ^1D$	3 - 2		1091
80	111.88		82.453 - 976.22	$2s^2p^2 - 2s2p^3$	$g^1P - ^1D^*$	2 - 2		1091
300	113.97		82.453 - 959.88	$2s^2p^2 - 2s2p^3$	$g^1P - ^1S^*$	2 - 1		1091
110	118.31		672.77 - 1517.98	$2s2p^2 - 2p^4$	$^1D^* - ^1P$	1 - 0		1091
150	118.67		671.63 - 1514.32	$2s2p^2 - 2p^4$	$^1D^* - ^1P$	2 - 1		1091
110	118.83		672.77 - 1514.32	$2s2p^2 - 2p^4$	$^1D^* - ^1P$	1 - 1		1091
50	125.93		0.0 - 794.12	$2s^22p^2 - 2s2p^3$	$g^1P - ^1P^*$	0 - 1		1091
175	126.30		298.87 - 1090.68	$2s^22p^2 - 2s2p^3$	$^1S - ^1P^*$	0 - 1		1091
200	125.33		184.596 - 976.22	$2s^22p^2 - 2s2p^3$	$^1D - ^1D^*$	2 - 2		1091
4	127.95		804.74 - 1586.24	$2s2p^2 - 2p^4$	$^1P^* - ^1D$	2 - 2		1091
375	128.43		671.63 - 1450.23	$2s2p^2 - 2p^4$	$^1D^* - ^1P$	2 - 2		1091
30	128.63		672.77 - 1450.23	$2s2p^2 - 2p^4$	$^1D^* - ^1P$	1 - 2		1091
250	130.99		686.83 - 1450.23	$2s2p^2 - 2p^4$	$^1D^* - ^1P$	3 - 2		1091
10	132.11		47.806 - 804.74	$2s^22p^2 - 2s2p^3$	$g^1P - ^1P^*$	1 - 2		1091
250	133.99		47.806 - 794.12	$2s^22p^2 - 2s2p^3$	$g^1P - ^1P^*$	1 - 1		1091
80	134.89		47.806 - 789.15	$2s^22p^2 - 2s2p^3$	$g^1P - ^1P^*$	1 - 0		1091
10	137.89		789.15 - 1514.32	$2s2p^2 - 2p^4$	$^1P^* - ^1P$	0 - 1		1091
50	138.15		794.12 - 1517.98	$2s2p^2 - 2p^4$	$^1P^* - ^1P$	1 - 0		1091
300	138.45		82.453 - 804.74	$2s^22p^2 - 2s2p^3$	$g^1P - ^1P^*$	2 - 2		1091
4	138.86		794.12 - 1514.32	$2s2p^2 - 2p^4$	$^1P^* - ^1P$	1 - 1		1091
30	140.51		82.453 - 794.12	$2s^22p^2 - 2s2p^3$	$g^1P - ^1P^*$	2 - 1		1091
110	140.92		804.74 - 1514.32	$2s2p^2 - 2p^4$	$^1P^* - ^1P$	2 - 1		1091
110	143.57		1090.68 - 1787.21	$2s2p^2 - 2p^4$	$^1P^* - ^1S$	1 - 0		1091
110	148.64		0.0 - 672.77	$2s^22p^2 - 2s2p^3$	$g^1P - ^1D^*$	0 - 1		1091
30	152.42		794.12 - 1450.23	$2s2p^2 - 2p^4$	$^1P^* - ^1P$	1 - 2		1091
30	154.92		804.74 - 1450.23	$2s2p^2 - 2p^4$	$^1P^* - ^1P$	2 - 2		1091
10	160.01		47.806 - 672.77	$2s^22p^2 - 2s2p^3$	$g^1P - ^1D^*$	1 - 1		1091
150	160.30		47.806 - 671.63	$2s^22p^2 - 2s2p^3$	$g^1P - ^1D^*$	1 - 2		1091
250	163.94		976.22 - 1586.24	$2s2p^2 - 2p^4$	$^1D^* - ^1D$	2 - 2		1091
150	165.46		82.453 - 686.83	$2s^22p^2 - 2s2p^3$	$g^1P - ^1D^*$	2 - 3		1091
4	169.73		82.453 - 671.63	$2s^22p^2 - 2s2p^3$	$g^1P - ^1D^*$	2 - 2		1091
50	179.18		959.88 - 1517.98	$2s2p^2 - 2p^4$	$^1S^* - ^1P$	1 - 0		1091
30	180.37		959.88 - 1514.32	$2s2p^2 - 2p^4$	$^1S^* - ^1P$	1 - 1		1091
10	201.82		1090.68 - 1586.24	$2s2p^2 - 2p^4$	$^1P^* - ^1D$	1 - 2		1091
300	203.94		959.88 - 1450.23	$2s2p^2 - 2p^4$	$^1S^* - ^1P$	1 - 2		1091
	310.6		82.453 - 404.41	$2s^22p^2 - 2s2p^3$	$g^1P - ^1S^*$	2 - 2	P	375,1091
	398.4		47.806 - 298.87	$2s^22p^2 - 2s^22p^2$	$g^1P - ^1S$	1 - 0	F	1120
	462.07		82.453 - 298.87	$2s^22p^2 - 2s^22p^2$	$g^1P - ^1S$	2 - 0	F,P	375,1120
	541.72		0.0 - 184.596	$2s^22p^2 - 2s^22p^2$	$g^1P - ^1D$	0 - 2	F,P	375,1120
	731.1		47.806 - 184.596	$2s^22p^2 - 2s^22p^2$	$g^1P - ^1D$	1 - 2	F	1120
	875.09		184.596 - 298.87	$2s^22p^2 - 2s^22p^2$	$^1D - ^1S$	2 - 0	F,P	375,1120
	979.0		82.453 - 184.596	$2s^22p^2 - 2s^22p^2$	$g^1P - ^1D$	2 - 2	F	1120
	1213		0.0 - 82.453	$2s^22p^2 - 2s^22p^2$	$g^1P - g^1P$	0 - 2	F,P	375,1120

CHROMIUM XX (Cr<sup>10+</sup>), Z = 24  
 Ground State 1s<sup>2</sup>2s<sup>2</sup>2p<sup>3</sup>(<sup>4</sup>P<sub>1/2</sub>) (5 electrons)  
 Ionization Potential [12 070 000] cm<sup>-1</sup>; [1496] eV

Multiplet	Rel. Int.	$\lambda_{\lambda}$ (m Å)	Levels (in 10 <sup>4</sup> cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
3	10.712		0.0 - 9335.3	2s <sup>2</sup> 2p - 2s <sup>2</sup> 4d	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> D	1 - 1		1089
2	10.840		82.950 - 9308.1	2s <sup>2</sup> 2p - 2s <sup>2</sup> 4d	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> D	1 - 1		1089
3	10.940		0.0 - 9145.0	2s <sup>2</sup> 2p - 2s <sup>2</sup> 4s	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>3</sup> S	1 - 1		1089
5	11.030		82.950 - 9145.0	2s <sup>2</sup> 2p - 2s <sup>2</sup> 4s	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>3</sup> S	1 - 1		1089
	13.631		0.0 - 7336.2 + F	2s <sup>2</sup> 2p - 2s2p( <sup>1</sup> P)3p	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> D	1 - 1	P	877
	13.683		82.950 - 7391.2 + F	2s <sup>2</sup> 2p - 2s2p( <sup>1</sup> P)3p	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> D	1 - 1	P	877
	13.910		0.0 - 7189.1 - F	2s <sup>2</sup> 2p - 2s2p( <sup>1</sup> P)3p	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> P	1 - 1	P	877
	13.946		82.950 - 7253.4 + F <sup>2</sup>	2s <sup>2</sup> 2p - 2s2p( <sup>1</sup> P)3p	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> P	1 - 1	P	877
2	14.065		861.671 - 7971.6	2s2p <sup>2</sup> - 2s2p( <sup>1</sup> P <sup>o</sup> )3d	<sup>2</sup> P - <sup>2</sup> D <sup>o</sup>	1 - 1		1089
1	14.093		653.010 - 7748.8	2s2p <sup>2</sup> - 2s2p( <sup>1</sup> P <sup>o</sup> )3d	<sup>2</sup> D - <sup>2</sup> F <sup>o</sup>	1 - 1		1089
	14.129		0.0 - 7077.6 + F	2s <sup>2</sup> 2p - 2s <sup>2</sup> 3d	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> D	1 - 1	P	877
10	14.205		428.13 - 7466.4 + F	2s2p <sup>2</sup> - 2s2p( <sup>1</sup> P <sup>o</sup> )3d	<sup>2</sup> P - <sup>2</sup> P <sup>o</sup>	1 - 1	Q	716,877
	14.214		428.13 - 7463.4 + F	2s2p <sup>2</sup> - 2s2p( <sup>1</sup> P <sup>o</sup> )3d	<sup>2</sup> P - <sup>2</sup> D <sup>o</sup>	1 - 1	P	877
2	14.261		428.13 - 7440.3	2s2p <sup>2</sup> - 2s2p( <sup>1</sup> P <sup>o</sup> )3d	<sup>2</sup> P - <sup>2</sup> F <sup>o</sup>	1 - 1		1089
	14.447		653.010 - 7574.9 + F	2s2p <sup>2</sup> - 2s2p( <sup>1</sup> P <sup>o</sup> )3d	<sup>2</sup> D - <sup>2</sup> F <sup>o</sup>	1 - 1	P	877
	14.524		640.990 - 7526.2 + F	2s2p <sup>2</sup> - 2s2p( <sup>1</sup> P <sup>o</sup> )3d	<sup>2</sup> D - <sup>2</sup> F <sup>o</sup>	1 - 1	P	877
0	14.641		640.990 - 7470.1 + F	2s2p <sup>2</sup> - 2s2p( <sup>1</sup> P <sup>o</sup> )3d	<sup>2</sup> D - <sup>2</sup> D <sup>o</sup>	1 - 1	Q	716,877
	14.669		653.010 - 7470.1 + F	2s2p <sup>2</sup> - 2s2p( <sup>1</sup> P <sup>o</sup> )3d	<sup>2</sup> D - <sup>2</sup> D <sup>o</sup>	1 - 1	P	877
30	15.061		82.950 - 6724.5	2s <sup>2</sup> 2p - 2s <sup>2</sup> 3s	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>3</sup> S	1 - 1	Q	716,375
80	116.05		0.0 - 861.671	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>2</sup> P	1 - 1		1091
30	117.95		0.0 - 847.763	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>2</sup> P	1 - 1		1091
10	122.29					1 - 1		1091
375	128.42		82.950 - 861.671	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>2</sup> P	1 - 1		1091
50	129.26		640.990 - 1414.60	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> D - <sup>2</sup> P <sup>o</sup>	1 - 1		1091
250	130.76		82.950 - 847.763	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>2</sup> P	1 - 1		1091
150	131.31		653.010 - 1414.60	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> D - <sup>2</sup> P <sup>o</sup>	1 - 1		1091
250	131.50		0.0 - 760.410	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>3</sup> S	1 - 1		1091
150	133.82		352.33 - 1099.51	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> P - <sup>4</sup> S <sup>o</sup>	1 - 1		1091
110	135.26		640.990 - 1380.28	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> D - <sup>2</sup> P <sup>o</sup>	1 - 1		1091
250	140.75		389.12 - 1099.51	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> P - <sup>4</sup> S <sup>o</sup>	1 - 1		1091
4	147.62		82.950 - 760.410	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>3</sup> S	1 - 1		1091
250	148.99		428.13 - 1099.51	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> P - <sup>4</sup> S <sup>o</sup>	1 - 1		1091
30	152.86		760.410 - 1414.60	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> S - <sup>2</sup> P <sup>o</sup>	1 - 1		1091
200	156.00		0.0 - 640.990	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> D	1 - 1		1091
10	161.33		760.410 - 1380.28	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> S - <sup>2</sup> P <sup>o</sup>	1 - 1		1091
50	164.63		640.990 - 1248.39	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> D - <sup>2</sup> D <sup>o</sup>	1 - 1		1091
200	167.97		653.010 - 1248.39	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> D - <sup>2</sup> D <sup>o</sup>	1 - 1		1091
80	169.87		640.990 - 1229.67	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> D - <sup>2</sup> D <sup>o</sup>	1 - 1		1091
50	173.42		653.010 - 1229.67	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> D - <sup>2</sup> D <sup>o</sup>	1 - 1		1091
150	175.42		82.950 - 653.010	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> D	1 - 1		1091
4	176.42		847.763 - 1414.60	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> P - <sup>2</sup> P <sup>o</sup>	1 - 1		1091
50	179.21		82.950 - 640.990	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>1</sup> D	1 - 1		1091
80	180.85		861.671 - 1414.60	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> P - <sup>2</sup> P <sup>o</sup>	1 - 1		1091
30	187.79		847.763 - 1380.28	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> P - <sup>2</sup> P <sup>o</sup>	1 - 1		1091
4	192.82		861.671 - 1380.28	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> P - <sup>2</sup> P <sup>o</sup>	1 - 1		1091
50	213.10		760.410 - 1229.67	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> S - <sup>2</sup> D <sup>o</sup>	1 - 1		1091
	257.0		0.0 - 389.12	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>4</sup> P	1 - 1		1058
50	258.57		861.671 - 1248.39	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> P - <sup>2</sup> D <sup>o</sup>	1 - 1		1091
10	271.72		861.671 - 1229.67	2s2p <sup>2</sup> - 2p <sup>3</sup>	<sup>2</sup> P - <sup>2</sup> D <sup>o</sup>	1 - 1		1091
	283.8		0.0 - 352.33	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>4</sup> P	1 - 1	P	1058
	289.7		82.950 - 428.13	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>4</sup> P	1 - 1		1058
	326.6		82.950 - 389.12	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>4</sup> P	1 - 1		1058
	371.2		82.950 - 352.33	2s <sup>2</sup> 2p - 2s2p <sup>2</sup>	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>4</sup> P	1 - 1	P	1058
	1208.9		0.0 - 82.950	2s <sup>2</sup> 2p - 2s <sup>2</sup> 2p	<sup>2</sup> G <sup>o</sup> P <sup>o</sup> - <sup>2</sup> G <sup>o</sup> P <sup>o</sup>	1 - 1	F	1120

**CHROMIUM XXI ( $\text{Cr}^{20}$ ), Z = 24**  
**Ground State  $1s^22s^2(^1S_0)$  (4 electrons)**  
**Ionization Potential [13 180 000]  $\text{cm}^{-1}$ ; [1634] eV**

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
10	12.909		341.12 - 8087.1 + B	$1s^22s2p - 1s^22p3p$	$^1P - ^1P$	1 - 1	Q	716,619
10	12.981		405.03 - 8108.7	$1s^22s2p - 1s^22p3p$	$^1P - ^1S$	2 - 1		643
0	13.018		405.03 - 8086.8	$1s^22s2p - 1s^22p3p$	$^1P - ^1D$	2 - 1		643
0	13.060		318.04 - 7975.1	$1s^22s2p - 1s^22p3p$	$^1P - ^1D$	0 - 1		643
	13.081		0.0 - 7644.7 + B	$1s^22s^2 - 1s^22s3p$	$g^1S - ^1P$	0 - 1	P	619
0	13.123		0.0 - 7620.2	$1s^22s^2 - 1s^22s3p$	$g^1S - ^1P$	0 - 1		643
0	13.205		667.23 - 8241.3	$1s^22s2p - 1s^22s3s$	$^1P - ^1S$	1 - 0		643
	13.316		667.23 - 8177.0 + B	$1s^22s2p - 1s^22p3p$	$^1P - ^1D$	1 - 2	P	619
	13.514		318.04 - 7718.0 + B	$1s^22s2p - 1s^22s3d$	$^1P - ^1D$	0 - 1	P	619
10	13.55		341.12 - 7721.2	$1s^22s2p - 1s^22s3d$	$^1P - ^1D$	1 - 2		877
0	13.647		405.03 - 7732.7	$1s^22s2p - 1s^22s3d$	$^1P - ^1D$	2 - 3		643
0	13.684		911.09 - 8218.8	$1s^22p^2 - 1s^22p3d$	$^1P - ^1P$	1 - 1		643
0	13.752		947.08 - 8218.8	$1s^22p^2 - 1s^22p3d$	$^1P - ^1P$	2 - 1		643
10	13.760		864.74 - 8134.4	$1s^22p^2 - 1s^22s2p$	$^1P - ^1D$	0 - 1	Q	877
10	13.779		947.08 - 8204.5	$1s^22p^2 - 1s^22p3d$	$^1P - ^1D$	2 - 3		643
10	13.844		1051.89 - 8275.4	$1s^22p^2 - 1s^22p3d$	$^1D - ^1P$	2 - 1		643
0	13.870		911.09 - 8121.0	$1s^22p^2 - 1s^22p3d$	$^1P - ^1D$	1 - 2		643
0	13.950		1051.89 - 8220.4	$1s^22p^2 - 1s^22p3d$	$^1D - ^1P$	2 - 2		643
10	14.029		667.23 - 7795.3	$1s^22s2p - 1s^22s3d$	$^1P - ^1D$	1 - 2	P	619,716
0	14.041		341.12 - 7463.2	$1s^22s2p - 1s^22s3s$	$^1P - ^1S$	1 - 1		643
2	14.172		405.03 - 7463.2	$1s^22s2p - 1s^22s3s$	$^1P - ^1S$	2 - 1	Q	1089
2	14.217		911.09 - 7946.8	$1s^22p^2 - 1s^22p3s$	$^1P - ^1P$	1 - 2	Q	1089
	14.244		1254.91 - 8275.4	$1s^22p^2 - 1s^22p3d$	$^1S - ^1P$	0 - 1	P	619
	14.457		1051.89 - 7969.0	$1s^22p^2 - 1s^22p3s$	$^1D - ^1P$	2 - 1	P	619
	14.896		1254.91 - 7969.0	$1s^22p^2 - 1s^22p3s$	$^1S - ^1P$	0 - 1	P	619
300	149.87		0.0 - 667.23	$1s^22s^2 - 1s^22s2p$	$g^1S - ^1P$	0 - 1		1091
50	154.61		405.03 - 1051.89	$1s^22s2p - 1s^22p^2$	$^1P - ^1D$	2 - 2		1091
80	165.03		341.12 - 947.08	$1s^22s2p - 1s^22p^2$	$^1P - ^1P$	1 - 2		1091
50	168.62		318.04 - 911.09	$1s^22s2p - 1s^22p^2$	$^1P - ^1P$	0 - 1		1091
50	170.16		667.23 - 1254.91	$1s^22s2p - 1s^22p^2$	$^1P - ^1S$	1 - 0		1091
150	175.45		341.12 - 911.09	$1s^22s2p - 1s^22p^2$	$^1P - ^1P$	1 - 1		1091
110	184.48		405.03 - 947.08	$1s^22s2p - 1s^22p^2$	$^1P - ^1P$	2 - 2		1091
50	190.98		341.12 - 864.74	$1s^22s2p - 1s^22p^2$	$^1P - ^1P$	1 - 0		1091
10	197.61		405.03 - 911.09	$1s^22s2p - 1s^22p^2$	$^1P - ^1P$	2 - 1		1091
10	259.97		667.23 - 1051.89	$1s^22s2p - 1s^22p^2$	$^1P - ^1D$	1 - 2		1091
50	293.15		0.0 - 341.12	$1s^22s^2 - 1s^22s2p$	$g^1S - ^1P$	0 - 1		437,730

**CHROMIUM XXII ( $\text{Cr}^{21}$ ), Z = 24**  
**Ground State  $1s^22s(^8S_{1/2})$  (3 electrons)**  
**Ionization Potential 13 882 000  $\text{cm}^{-1}$ ; 1721.6 eV**

Multiplet	Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in $10^3 \text{ cm}^{-1}$ )	Configurations	Terms	J - J	Notes	References
		2.190	0.0 - 4566.2	$1s^22s - 1s2s2p$	$g^1S - ^1P$	- - -	P	631
		7.562	0.0 - 13224.1	$1s^22s - 1s^2p$	$g^1S - ^1P$	- - -	P	643
		7.664	0.0 - 13048.4	$1s^22s - 1s^2p$	$g^1S - ^1P$	- - -	P	643
		7.774	357.49 - 13220.9	$1s^2p - 1s^2d$	$^1P - ^1D$	- - -	P	643
		7.817	0.0 - 12793.6	$1s^2s - 1s^2p$	$g^1S - ^1P$	- - -	P	643
		7.828	448.40 - 13223.0	$1s^2p - 1s^2d$	$^1P - ^1D$	- - -	P	643

## CN XXII — Continued

Multiplet	Rel. Int.	$\lambda$ (in Å)	Levels (in $10^3$ cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
		7 881	357 49 - 13046 2	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	643
		7 936	448 40 - 13049 2	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	643
		8 042	357 49 - 12792 2	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	643
		8 066	0 0 - 12398 0	1s <sup>2</sup> s - 1s <sup>2</sup> p	g <sup>o</sup> S - P <sup>o</sup>	- - -	P	643
		8 100	448 40 - 12794 1	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	643
		8 304	357 49 - 12400 0	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	643
		8 365	448 40 - 12403 0	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	643
		8 516	0 0 - 11743 0	1s <sup>2</sup> s - 1s <sup>2</sup> p	g <sup>o</sup> S - P <sup>o</sup>	- - -	P	643
		8 778	357 49 - 11749 6	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	643
		8 847	448 40 - 11751 7	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	643
		9 498	0 0 - 10529 7	1s <sup>2</sup> s - 1s <sup>2</sup> p	g <sup>o</sup> S - P <sup>o</sup>	- - -	P	977
		9 498	0 0 - 10528 3	1s <sup>2</sup> s - 1s <sup>2</sup> p	g <sup>o</sup> S - P <sup>o</sup>	- - -	P	977
		9 806	357 49 - 10555 3	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	977
		9 870	357 49 - 10489 0	1s <sup>2</sup> p - 1s <sup>2</sup> s	P <sup>o</sup> - S	- - -	P	977
		9 891	448 40 - 10558 6	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	977
		9 966	448 40 - 10489 0	1s <sup>2</sup> p - 1s <sup>2</sup> s	P <sup>o</sup> - S	- - -	P	977
100		12 613	0 0 - 7928 32	1s <sup>2</sup> s - 1s <sup>2</sup> p	g <sup>o</sup> S - P <sup>o</sup>	- - -	P	977,273
200		12 656	0 0 - 7901 26	1s <sup>2</sup> s - 1s <sup>2</sup> p	g <sup>o</sup> S - P <sup>o</sup>	- - -	P	977,273
200		13 142	357 49 - 7966 68	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	977,273
200		13 286	448 40 - 7975 12	1s <sup>2</sup> p - 1s <sup>2</sup> d	P <sup>o</sup> - D	- - -	P	977,273
20		13 428	357 49 - 7804 86	1s <sup>2</sup> p - 1s <sup>2</sup> s	P <sup>o</sup> - S	- - -	P	977,273
200		13 594	448 40 - 7804 86	1s <sup>2</sup> p - 1s <sup>2</sup> s	P <sup>o</sup> - S	- - -	P	977,273
150		223 015	0 0 - 448 40	1s <sup>2</sup> s - 1s <sup>2</sup> p	g <sup>o</sup> S - P <sup>o</sup>	- - -	P	977,730
120		279 731	0 0 - 357 49	1s <sup>2</sup> s - 1s <sup>2</sup> p	g <sup>o</sup> S - P <sup>o</sup>	- - -	P	977,730

**CHROMIUM XXIII (Cr<sup>2+</sup>), Z = 24**  
**Ground State 1s<sup>2</sup>(<sup>1</sup>S<sub>0</sub>) ( 2 electrons)**  
**Ionization Potential 60 349 000 cm<sup>-1</sup>; 7482.4 eV**

Multiplet	Rel. Int.	$\lambda$ (in Å)	Levels (in $10^3$ cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
		1 724	0 0 - 58023 1	1s - 1s5p	g <sup>o</sup> S - P <sup>o</sup>	0 - 1	P	728
		1 763	0 0 - 56714 4	1s - 1s4p	g <sup>o</sup> S - P <sup>o</sup>	0 - 1	P	728
		1 856	0 0 - 53888 2	1s - 1s3p	g <sup>o</sup> S - P <sup>o</sup>	0 - 1	P	728
		2 182	0 0 - 45832 0	1s - 1s2p	g <sup>o</sup> S - P <sup>o</sup>	0 - 1	P	956
1		2 192	0 0 - 45614 9	1s - 1s2p	g <sup>o</sup> S - P <sup>o</sup>	0 - 1	P	856
		2 203	0 0 - 45389 1	1s - 1s2s	g <sup>o</sup> S - S	0 - 1	F.P.	375,918
		11 82	45389 1 - 53850 9	1s2s - 1s3p	S - P <sup>o</sup>	1 - 2	P	375
		12 09	45619 0 - 53888 2	1s2s - 1s3p	S - P <sup>o</sup>	0 - 1	P	375
		126 26	45389 1 - 45695 6	1s2s - 1s2p	S - P <sup>o</sup>	1 - 2	P	375
		469 48	45619 0 - 45832 0	1s2s - 1s2p	S - P <sup>o</sup>	0 - 1	P	375
		1154 71	53764 3 - 53850 9	1s3s - 1s3p	S - P <sup>o</sup>	1 - 2	P	375
		1582 28	53825 0 - 53888 2	1s3s - 1s3p	S - P <sup>o</sup>	0 - 1	P	375

**CHROMIUM XXIV (Cr<sup>2+</sup>), Z = 24**  
**Ground State 1s(<sup>2</sup>S<sub>1/2</sub>) (1 electron)**  
**Ionization Potential 63 675 300 cm<sup>-1</sup>; 7894.79 eV**

Multiplet Rel. Int.	$\lambda_{\text{vac}}$ (in Å)	Levels (in 10 <sup>4</sup> cm <sup>-1</sup> )	Configurations	Terms	J - J	Notes	References
1 603		0 0 - 62385 1385	1s - 7p	g <sup>2</sup> S - P <sup>2</sup>	- - -	P	1042
1 615		0 0 - 61919 1477	1s - 6p	g <sup>2</sup> S - P <sup>2</sup>	- - -	P	1042
1 636		0 0 - 61141 5413	1s - 5p	g <sup>2</sup> S - P <sup>2</sup>	- - -	P	1042
1 675		0 0 - 59715 3160	1s - 4p	g <sup>2</sup> S - P <sup>2</sup>	- - -	P	1042
1 766		0 0 - 56634 2120	1s - 3p	g <sup>2</sup> S - P <sup>2</sup>	- - -	P	1042
1 767		0 0 - 56597 5100	1s - 3p	g <sup>2</sup> S - P <sup>2</sup>	- - -	P	1042
2 090		0 0 - 47843 0420	1s - 2p	g <sup>2</sup> S - P <sup>2</sup>	- - -	P	1042
2 096		0 0 - 47719 2500	1s - 2p	g <sup>2</sup> S - P <sup>2</sup>	- - -	P	1042
6 820		47722 8200 - 62385 1385	2s - 7p	S - P <sup>2</sup>	- - -	P	1042
6 877		47843 0420 - 62385 1385	2p - 7d	P <sup>2</sup> - D	- - -	P	1042
7 044		47722 8200 - 61919 1477	2s - 6p	S - P <sup>2</sup>	- - -	P	1042
7 104		47843 0420 - 61919 1477	2p - 6d	P <sup>2</sup> - D	- - -	P	1042
7 452		47722 8200 - 61141 5413	2s - 5p	S - P <sup>2</sup>	- - -	P	1042
7 518		47843 0420 - 61144 1334	2p - 5d	P <sup>2</sup> - D	- - -	P	1042
8 339		47722 8200 - 59715 3160	2s - 4p	S - P <sup>2</sup>	- - -	P	1042
8 419		47843 0420 - 59720 3786	2p - 4d	P <sup>2</sup> - D	- - -	P	1042
11 222		47722 8200 - 56634 2120	2s - 3p	S - P <sup>2</sup>	- - -	P	1042
11 360		47843 0420 - 56646 2052	2p - 3d	P <sup>2</sup> - D	- - -	P	1042
17 281		56598 5810 - 62385 1385	3s - 7p	S - P <sup>2</sup>	- - -	P	1042
17 388		56634 2120 - 62385 1385	3p - 7d	P <sup>2</sup> - D	- - -	P	1042
17 425		56646 2052 - 62385 1385	3d - 7f	D - F <sup>2</sup>	- - -	P	1042
18 795		56598 5810 - 61919 1477	3s - 6p	S - P <sup>2</sup>	- - -	P	1042
18 922		56634 2120 - 61919 1477	3p - 6d	P <sup>2</sup> - D	- - -	P	1042
18 965		56646 2052 - 61919 1477	3d - 6f	D - F <sup>2</sup>	- - -	P	1042
22 012		56598 5810 - 61141 5413	3s - 5p	S - P <sup>2</sup>	- - -	P	1042
22 173		56634 2120 - 61144 1334	3p - 5d	P <sup>2</sup> - D	- - -	P	1042
22 226		56646 2052 - 61145 4279	3d - 5f	D - F <sup>2</sup>	- - -	P	1042
32 085		56598 5810 - 59715 3160	3s - 4p	S - P <sup>2</sup>	- - -	P	1042
32 403		56634 2120 - 59720 3786	3p - 4d	P <sup>2</sup> - D	- - -	P	1042
32 502		56646 2052 - 59722 9060	3d - 4f	D - F <sup>2</sup>	- - -	P	1042
831 794		47722 8200 - 47843 0420	2s - 2p	S - P <sup>2</sup>	- - -	P	1042



**D. Magnetic Dipole Lines for Chromium Ions  
(Wavelengths, Classifications, and Transition Probabilities)**

## D. Magnetic Dipole Lines for Chromium Ions

[Excerpted from: V. Kaufman and J. Sugar, *J. Phys. Chem. Ref. Data* 15, 321 (1986)]

### 1. Introduction

The following tables, including the introductory comments, are excerpted from the above cited compilation of observed and predicted wavelengths of magnetic dipole lines arising within ground configurations of the type  $ns^2np^k$  ( $n=2$  and  $3$ ,  $k=1$  to  $5$ ). The compilation work was done by V. Kaufman and J. Sugar of the National Institute of Standards and Technology (formerly the National Bureau of Standards).

All measured lines that are correctly identified are included. Some are only tentatively classified by the authors, but appear to be reasonable on the basis of predictions along isoelectronic sequences.

Also included is a selected group of electric quadrupole lines (E2) that are frequently observed in  $ns^2np^2$  and  $ns^2np^4$  configurations; these are the  $^1D_2 - ^1S_0$  transitions.

It will probably be difficult to observe the  $nsnp$  ( $^3P_{0,1,2} - ^1P_1$ ) transitions in the Be and Mg isoelectronic sequences because the very large electric-dipole transition probability of the  $ns^2^1S_0 - nsnp^1P_1$  resonant transition will tend to rapidly deplete the  $nsnp^1P_1$  level. Similarly, but to a lesser extent, the  $^3P_0 - ^3P_1$  transition can be expected to be weak because of the  $ns^2^1S_0 - nsnp^3P_1$  transition. However, these magnetic-dipole transitions have been included for the sake of completeness.

Calculations of line strengths and transition probabilities have been made for all of these lines by both relativistic and non-relativistic methods. Preference has been given to the relativistic results. Calculations by both methods for the  $n=3$  shell differ on the average by only 5%.<sup>1</sup>

### 2. Predicted Wavelengths

For the chromium ions, predicted values for the wavelengths of the M1 and E2 lines were obtained from the known energy levels by the Ritz principle of deriving wavelengths from energy differences. Their uncertainties are derived from the reported level uncertainties. The source of data is given in Sec. 7 below.

### 3. Observed Wavelengths

The most common laboratory source generating copious forbidden lines is the tokamak, which contains a magnetically-confined, high-temperature plasma with an ion density similar to that of the solar corona. By injecting any impurity element, magnetic dipole lines of that

element may be seen in stages of ionization determined by the plasma temperature. Most of the chromium data are from tokamak observations. The other wavelength data are from astronomical sources, including gaseous nebulae, stars and the solar corona.

The sources of observed data that have been credited are those providing the best measurements.

### 4. Predicted Transition Probabilities

In most cases multiconfiguration Dirac-Fock calculations of line strengths are available. These calculations do not generally converge for neutral and singly ionized atoms, but non-relativistic calculations have been made in every such case. Line strengths for the magnetic dipole lines of the isoelectronic sequences of B I, C I, N I, and F I were taken from Cheng *et al.*<sup>2</sup> Those for the Al I, Si I, P I, and Cl I sequences were taken from Huang<sup>3,5</sup> and Huang *et al.*<sup>6</sup> The relativistic calculations are not available for the Be, Mg, and S isoelectronic sequences. The transition probabilities for all magnetic-dipole lines of the Be-like, Mg-like, and S-like ions were therefore calculated in the manner described by Sugar and Kaufman.<sup>1</sup> These are non-relativistic calculations in intermediate coupling. They agree within a few percent with relativistic calculations in the  $n=3$  sequences for which both are available.

Line strengths for the electric-quadrupole lines of  $2s^2p^k$  ( $^1D_2 - ^1S_0$ ) [ $k=2$ ] and [ $k=4$ ] are for the carbon and oxygen sequences from Cheng *et al.*<sup>2</sup> The transition probabilities for these lines in the sulfur sequence,  $3s^23p^4$ , are from Mendoza and Zeippen.<sup>7</sup>

Relations between transition probabilities  $A$  ( $s^{-1}$ ) and line strengths  $S$  are given explicitly as

$$A = \frac{2.697 \times 10^{13}}{\lambda^3 g} S(M1),$$

$$A = \frac{1.680 \times 10^{10}}{\lambda^3 g} S(E2),$$

where  $\lambda$  is the transition wavelength in Å and  $g$  is the  $2J+1$  degeneracy of the upper level.  $S(M1)$  in Bohr magneton units ( $\mu_B$ ) and  $S(E2)$  in atomic units ( $ea_0^2$ ) are the magnetic-dipole and electric-quadrupole line strengths, respectively.

The magnetic-dipole transition rate in almost all cases is a few orders of magnitude greater than the electric-quadrupole transition rate. The E2 rate has been added to the M1 rate in those cases for which the former is

greater than 1% of the latter. This is true only for some of the N I ( $2p^2$ ) and P I ( $3p^2$ ) sequence transitions. An asterisk following the transition rate in the tables shows where this occurs.

### 5. Data Table Information

The tables contain the predicted and observed wavelengths and predicted transition probabilities for magnetic-dipole transitions within  $ns^2np^k$  ( $k = 1-5$ ) and  $nsnp$  configurations for  $n = 2, 3$ . The electric quadrupole transition  $^1D_2-^1S_0$  for  $k = 2, 4$  is included because it is frequently observed. The data are presented in order of increasing wavelength. The columns from left to right in order of appearance contain the following information:

Column No.	Description
1	Wavelengths (observed and predicted) in Å below 20 000 Å, and in micrometers (μm) between 2 and 1000 μm. Wavelengths given without units are in Å. Wavelengths in vacuum are given below 2000 Å, in air between 2000 Å and 5 μm, and in vacuum above 5 μm. Each wavelength is followed by its uncertainty in parentheses. Tentative identifications are preceded by "T". E2 transitions are denoted by "Q".
2	Transition probabilities ( <i>A</i> ) are written as a factor times 10 to a power. The power of ten follows the decimal factor. For example, $2.20 + 4$ means $2.20 \times 10^4$ . An asterisk following the transition probability indicates that the E2 rate for the transition is greater than 1% of the M1 rate and has been added to that value.
3	Spectrum.
4	Electronic configuration.
5	Line classification. Lower level is given first.
6	Ionization energy in thousands of electron volts (keV). <sup>8-10</sup>

Column No.	Description
7	References for observed wavelengths. Definitions of symbols are given in Sec. 8, "References for Observed Wavelengths".

### 6. References to Text

- <sup>1</sup>J. Sugar and V. Kaufman, *J. Opt. Soc. Am. B* 1, 218 (1984).  
<sup>2</sup>K. T. Cheng, Y. -K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* 24, 111 (1979).  
<sup>3</sup>K. -N. Huang, private communication (1985).  
<sup>4</sup>K. -N. Huang, *At. Data Nucl. Data Tables* 32, 503 (1985).  
<sup>5</sup>K. -N. Huang, *At. Data Nucl. Data Tables* 30, 313 (1984).  
<sup>6</sup>K. -N. Huang, Y. -K. Kim, K. T. Cheng, and J. P. Desclaux, *At. Data Nucl. Data Tables* 28, 355 (1983).  
<sup>7</sup>C. Mendoza and C. J. Zeppen, *Mon. Not. R. Astron. Soc.* 202, 981 (1983).  
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## Magnetic Dipole Lines for Chromium

Observed	Wavelength		$\lambda$ ( $\text{\AA}$ )	Spectrum	Config.	Classification	I.E. (keV)	Ref. (obs. H)
	Observed	Calculated						
		286.51(17)	1.24 +4	Cr XXI	2s 2p	$3P_0 - 1P_1$	1.63	
		306.80(5)	7.42 +3	Cr XXI	2s 2p	$3P_1 - 1P_1$	1.63	
378.0(3)		378.1(3)	1.61 +4	Cr XVIII	$2s^2 2p^3$	$4S_{3/2} - 2P_{3/2}$	1.30	DH
		381.6(3)	6.56 +3	Cr XXI	2s 2p	$3P_2 - 1P_1$	1.63	
398.4(3)		398.42(16)	6.38 +4	Cr XIX	$2s^2 2p^2$	$3P_1 - 1S_0$	1.40	HSCS
442.1(3)		442.3(4)	1.31 +4	Cr XVIII	$2s^2 2p^3$	$4S_{3/2} - 2P_{1/2}$	1.30	DH
493.8(3)		493.79(24)	6.42 +4	Cr XVII	$2s^2 2p^4$	$3P_1 - 1S_0$	1.19	HSCS
663.1(3)		663.1(9)	3.22 +2	Cr XVIII	$2s^2 2p^3$	$4S_{3/2} - 2D_{5/2}$	1.30	DH
722.1(3)		722.56(16)	1.56 +4	Cr XVIII	$2s^2 2p^3$	$2D_{3/2} - 2P_{3/2}$	1.30	DH
731.1(3)		731.07(8)	5.62 +3	Cr XIX	$2s^2 2p^2$	$3P_1 - 1D_2$	1.40	HSCS
740.75(3)		740.75(3)	6.67 +3	Cr XVII	$2s^2 2p^4$	$3P_2 - 1D_2$	1.19	PSS
	Q	781.9(6)	4.19 +1	Cr XVII	$2s^2 2p^4$	$1D_2 - 1S_0$	1.19	
793.3(3)		793.3(1.3)	6.12 +3	Cr XVIII	$2s^2 2p^3$	$4S_{3/2} - 2D_{3/2}$	1.30	HSCS
	Q	875.6(8)	2.03 +1	Cr XIX	$2s^2 2p^2$	$1D_2 - 1S_0$	1.40	
		879.96(23)	5.14 +3	Cr XVIII	$2s^2 2p^3$	$2D_{5/2} - 2P_{3/2}$	1.30	
979.0(3)		979.06(14)	5.93 +3	Cr XIX	$2s^2 2p^2$	$3P_2 - 1D_2$	1.40	HSCS
		988.5(1.0)	7.59 +1	Cr XIII	3s 3p	$3P_0 - 1P_1$	0.35	
		999.6(3)	3.33 +3	Cr XVIII	$2s^2 2p^3$	$2D_{3/2} - 2P_{1/2}$	1.30	
		1028.49(10)	5.03 +1	Cr XIII	3s 3p	$3P_1 - 1P_1$	0.35	
		1135.8(1.3)	6.25 +1	Cr XIII	3s 3p	$3P_2 - 1P_1$	0.35	
1205.9(3)		1205.9(3)	5.11 +3	Cr XX	$2s^2 2p$	$2P_{1/2} - 2P_{3/2}$	1.50	HSCS
1340.7(4)		1340.09(20)	4.09 +2	Cr XVII	$2s^2 2p^4$	$3P_1 - 1D_2$	1.19	FBM
1410.60(2)		1410.62(4)	6.39 +3	Cr XVI	$2s^2 2p^5$	$2P_{3/2} - 2P_{1/2}$	1.10	PSS
1440.01(2)		1440.8(2.1)	3.68 +2	Cr XI	$3s^2 3p^2$	$3P_1 - 1S_0$	0.27	SBT
1489.04(3)		1489.05(16)	1.21 +2	Cr X	$3s^2 3p^3$	$4S_{3/2} - 2P_{3/2}$	0.24	SBT
1564.30(2)		1564.09(17)	5.89 +1	Cr X	$3s^2 3p^3$	$4S_{3/2} - 2P_{1/2}$	0.24	SBT
1566.4(1)		1565.5(5)	3.38 +3	Cr XXI	2s 2p	$3P_1 - 3F_2$	1.63	Su
1656.3(3)		1656.29(27)	4.58 +3	Cr XVII	$2s^2 2p^4$	$3P_2 - 3P_1$	1.19	HSCS
		1693.9(6)	3.40 +2	Cr IX	$3s^2 3p^4$	$3P_1 - 1S_0$	0.21	
2090.9(3)		2090.9(4)	1.81 +3	Cr XIX	$2s^2 2p^2$	$3P_0 - 3P_1$	1.40	HSCS
		2534.1(5)	3.67 +1*	Cr X	$3s^2 3p^3$	$4S_{3/2} - 2D_{5/2}$	0.24	
2606.4(3)		2606.4(3)	3.80 +2	Cr XVIII	$2s^2 2p^3$	$2P_{1/2} - 2P_{3/2}$	1.30	DH
	Q	2634.7(7)	1.03 +1	Cr XI	$3s^2 3p^2$	$1D_2 - 1S_0$	0.27	
		2694.4(5)	1.14 +1	Cr X	$3s^2 3p^3$	$4S_{3/2} - 2D_{3/2}$	0.24	
	Q	2733.8(1.5)	6.41 +0	Cr IX	$3s^2 3p^4$	$1D_2 - 1S_0$	0.21	
2885.4(3)		2885.4(1.2)	4.69 +2	Cr XIX	$2s^2 2p^2$	$3P_1 - 3P_2$	1.40	HSCS
3178		3177.9(7)	1.77 +1	Cr XI	$3s^2 3p^2$	$3P_1 - 1D_2$	0.27	M
		3301.1(5)	2.99 +1	Cr IX	$3s^2 3p^4$	$3P_2 - 1D_2$	0.21	
		3328.4(8)	6.22 +1	Cr X	$3s^2 3p^3$	$2D_{3/2} - 2P_{3/2}$	0.24	
		3608.2(9)	2.86 +1*	Cr X	$3s^2 3p^3$	$2P_{3/2} - 2P_{3/2}$	0.24	
		3725.8(1.0)	2.82 +1*	Cr X	$3s^2 3p^3$	$2D_{3/2} - 2P_{1/2}$	0.24	

## Magnetic Dipole Lines for Chromium - Continued

Observed	Wavelength		$\lambda$ ( $s^{-1}$ )	Spectrum	Config.	Classification	$\lambda$ E (keV)	Ref	
	Observed	Calculated						Obs	H
3996.6(4)	3996.6(1.1)		2.60 +1	Cr XI	3s <sup>2</sup> 3p <sup>2</sup>	<sup>3</sup> P <sub>2</sub> - <sup>1</sup> D <sub>2</sub>	0.27		J
4038.6(3)	4039.(7)		1.27 +2	Cr XVIII	2s <sup>2</sup> 2p <sup>3</sup>	<sup>2</sup> D <sub>3/2</sub> - <sup>2</sup> D <sub>5/2</sub>	1.30		DH
	4330.(40)		2.38 +2	Cr XXI	2s 2p	<sup>3</sup> P <sub>0</sub> - <sup>3</sup> P <sub>1</sub>	1.63		
	4450.5(1.4)		4.19 +0	Cr IX	3s <sup>2</sup> 3p <sup>4</sup>	<sup>3</sup> P <sub>1</sub> - <sup>1</sup> D <sub>2</sub>	0.21		
8153.8(4)	8153.7(7)		1.66 +1	Cr XII	3s <sup>2</sup> 3p	<sup>2</sup> P <sub>1/2</sub> - <sup>2</sup> P <sub>3/2</sub>	0.30		J
	10106.4(2.0)		1.74 +1	Cr VIII	3s <sup>2</sup> 3p <sup>5</sup>	<sup>2</sup> P <sub>3/2</sub> - <sup>2</sup> P <sub>1/2</sub>	0.18		
	10878.(120)		1.03 +1	Cr XIII	3s 3p	<sup>3</sup> P <sub>1</sub> - <sup>3</sup> F <sub>2</sub>	0.35		
	12783.(8)		1.04 +1	Cr IX	3s <sup>2</sup> 3p <sup>4</sup>	<sup>3</sup> P <sub>2</sub> - <sup>3</sup> P <sub>1</sub>	0.21		
	15514.(17)		3.46 +0	Cr XI	3s <sup>2</sup> 3p <sup>2</sup>	<sup>3</sup> P <sub>1</sub> - <sup>3</sup> P <sub>2</sub>	0.27		
	18059.(16)		2.98 +0	Cr XI	3s <sup>2</sup> 3p <sup>2</sup>	<sup>3</sup> P <sub>0</sub> - <sup>3</sup> P <sub>1</sub>	0.27		
	2.54(6) $\mu$ m		1.13 +0	Cr XIII	3s 3p	<sup>3</sup> P <sub>0</sub> - <sup>3</sup> P <sub>1</sub>	0.35		
	3.103(7) $\mu$ m		2.74 -1	Cr X	3s <sup>2</sup> 3p <sup>3</sup>	<sup>2</sup> P <sub>1/2</sub> - <sup>2</sup> P <sub>3/2</sub>	0.24		
	4.260(13) $\mu$ m		1.28 -1	Cr X	3s <sup>2</sup> 3p <sup>3</sup>	<sup>2</sup> D <sub>3/2</sub> - <sup>2</sup> D <sub>5/2</sub>	0.24		
	4.3(4) $\mu$ m		1.93 -1	Cr XVII	2s <sup>2</sup> 2p <sup>4</sup>	<sup>3</sup> P <sub>0</sub> - <sup>3</sup> P <sub>1</sub>	1.19		
	5.787(24) $\mu$ m		2.73 -1	Cr IX	3s <sup>2</sup> 3p <sup>4</sup>	<sup>3</sup> P <sub>1</sub> - <sup>3</sup> P <sub>0</sub>	0.21		

**E. Atomic Energy Levels of Chromium, Cr I through Cr XXIV**

## E. Atomic Energy Levels of Chromium, Cr I through Cr XXIV

[Excerpted from: J. Sugar and C. Corliss, *J. Phys. Chem. Ref. Data* 14, Suppl. 2 (1985)].

### 1. Introduction

The following tables, including the introductory comments, are excerpted from the iron-period compilation of atomic energy levels by J. Sugar and C. Corliss (1985) of the Atomic Energy Levels Data Center at the National Institute of Standards and Technology (formerly the National Bureau of Standards).

Generally, only published papers have been used as sources of data. Unpublished data are included when they constitute a substantial improvement over material in the literature. For many of the higher ions the original papers do not give energy level values, but only classifications of observed lines. In these cases the level values have been derived from the given data.

All energy levels are given in units of  $\text{cm}^{-1}$ , beginning with a value of zero for the ground level. Ionization energies found in the literature are usually given in eV or  $\text{cm}^{-1}$ . The conversion factor,  $8065.479(21) \text{ cm}^{-1}/\text{eV}$ , given by Cohen and Taylor (1973), is used here. In a few cases where adequate data were available but the ionization energy had not been derived, this calculation was carried out. For a number of the ions, no suitable series are known. In these cases values obtained by Lotz (1967), by a method of successive differences along isoelectronic sequences, have been quoted. Although uncertainties are not provided with these extrapolated values, it is estimated that they are accurate to 0.2% by comparing them with recently determined values.

Nearly all of the data are based on observations of various types of laboratory light sources. However, the laboratory data are sometimes supplemented by data obtained from solar observations. This is particularly true where spin-forbidden lines are needed to establish the absolute energy of a system of excited levels and where parity-forbidden transitions between levels of a ground configuration are used to obtain accurate relative energies for the low levels. Whenever both solar data and equivalent laboratory data are available preference is generally given to the laboratory measurements.

When no observations are available to connect independent systems of levels, an estimate of the connecting energy is adopted. Those level values affected by the estimate are denoted by  $+x$  following the value. The value of  $x$  is the systematic error of the estimate.

Included under the heading "Leading Percentages" are the results of calculations that express the eigenvector percentage composition of levels (rounded to the nearest %) in terms of the basis states of a single configuration, or more than one configuration where configura-

tion interaction has been included. First the percentage of the basis state corresponding to the level's name is given; next the second largest percentage together with the related basis state. Sometimes the leading percentage in an alternative coupling scheme is given. Generally, when the leading percentage is less than 40%, no name is given. When the first and second resultant terms are the same and sum to  $>40\%$  the first name is given. When the first and second resultant terms are the same but have different percentages, and their share of the eigenvector composition sums to 40% or more, the level will be named as the higher percentage term. In cases where these percentages differ by one or two units (an insignificant difference), either term may be selected for the level name, and the lower percentage may appear first. For the unnamed level, the term symbol follows the percentage. The user should of course bear in mind that the percentages are model dependent, so that the results of different calculations can yield notably different percentages. In the case of Cr, the 1969 results by Roth are adopted. It was intended to use his new 1980 calculations as well, but it was found that the sum of percentages for a number of states exceeded 100 by significant amounts.

For configurations of equivalent  $d$ -electrons, several terms of the same  $LS$  type may occur. These are theoretically distinguished by their seniority number. In the present compilations they are designated in the notation of Nielson and Koster (1963). For example, in the  $3d^3$  configuration there are three  $^3D$  terms with seniorities of 1, 3, and 5. These terms are denoted as  $^3D_1$ ,  $^3D_2$ , and  $^3D_3$ , respectively, by Nielson and Koster. Martin, Zalubas, and Hagan (1978) give a complete summary of the coupling notations used here, tables of the allowed terms for equivalent electrons, etc.

The text for each ion does not include a complete review of the literature but is intended to credit the major contributions. In assembling the data for each spectrum the following bibliographies were used:

- i. Papers cited by Moore (1949, 1952)
- ii. C. E. Moore (1968, 1969)
- iii. L. Hagan and W. C. Martin (1972)
- iv. L. Hagan (1977)
- v. R. Zalubas and A. Albright (1980)
- vi. Card file of publications since June 1979 maintained by the NBS Atomic Energy Levels Data Center

## He I Isoelectronic Sequence

Spectra of K, Ca, Ti, and V were obtained by Aglitskii *et al.* (1974) with a laser-heated plasma in third and fifth orders of a crystal spectrograph. Reference lines of Mg XI and Al XII published by Flemberg (1942) were used, and an uncertainty of  $\pm 0.0005 \text{ \AA}$  was reported for the lines of the He I isoelectronic sequence, which fall in the range of 2.3–3.6  $\text{\AA}$ . Flemberg's reference wavelengths were in  $x$ -units. The equivalence to  $\text{\AA}$  that he used must be increased by 8 parts in  $10^5$ , according to the more recent conversion determined by Deslattes and Henins (1973). With this correction, the data of Aglitskii *et al.* deviate randomly from the calculated wavelengths of Safronova (1981) by  $\pm 0.0008 \text{ \AA}$ .

In a beam-foil experiment the He-like argon spectrum was observed by Briand *et al.* (1983a). Their wavelengths for the  $1s^2 \ ^1S_0 - 1s2p \ ^3P_1^o$  and  $^1P_1^o$  transitions were 3.9693(3)  $\text{\AA}$  and 3.9491(3)  $\text{\AA}$ , in agreement with the calculated values by Safronova.

The  $1s2s \ ^3S_1 - 1s2p \ ^3P_1^o$  transition has been measured in Ca XIX by Livingston (1983) and in Fe XXV by Buchet *et al.* (1982). The measured wavelengths are 466.78(8)  $\text{\AA}$  for Ca and 271.04(10)  $\text{\AA}$  for Fe. The corresponding energy differences are greater than those predicted by Safronova by 1.2(37) and 123(136)  $\text{cm}^{-1}$ , respectively, or 0.07% and 0.03% of the energy difference. A new calculation of these energies by Hata and Grant (1983) predicted values that were 60  $\text{cm}^{-1}$  lower in Ca and 154  $\text{cm}^{-1}$  lower in Fe than the observed values.

Because of the excellent agreement of Safronova's calculations with the best experimental data available and the paucity of these data, the compilation of this sequence was based on her results. Her calculated energies were quoted for the  $1s2s$  and  $1s2p$  levels of the He I isoelectronic sequence and for the principal ionization energies (with correction to the Rydberg for finite atomic mass). The observed  $1s2s \ ^3S_1 - 1s2p \ ^3P_1^o$  intervals in Ca XIX mentioned above are incorporated in the respective level lists. For  $n = 3-5$  the calculated binding energies reported by Ermolaev and Jones (1974) are subtracted from the binding energy of the ground state by Safronova to arrive at energy level values. The uncertainty in the calculated energy levels and the ionization energies is assumed conservatively to be 2 parts in  $10^4$ , corresponding to the deviations from the Aglitskii *et al.* (corrected) observations. (The deviation from the measurements in Ar is 1 part in  $10^4$ .) The uncertainties in energy differences for levels of the same  $n$ -value are estimated to be 2 parts in  $10^3$ . The deviation of the  $1s2p \ ^3P_1^o - ^1P_1^o$  intervals measured by Aglitskii *et al.* with resonance lines differ randomly from the calculated values of Safronova by 3%.

The singlet-triplet mixing coefficients for the  $1snp \ ^3P^o$  states are quoted from Ermolaev and Jones.

## H I Isoelectronic Sequence

No observations of  $1s - np$  transitions have been sufficiently accurate to test the theoretical values. The best measurement available is for the  $1s - 2p$  energies for Fe XXVI with an uncertainty of  $\pm 5000 \text{ cm}^{-1}$ , or 1 part in  $10^6$ , by Briand, Tavernier, and Indelicato (1983b). Erickson (1977) has calculated the absolute binding energies for each of the levels through  $n = 5$  and for the  $ns$  and  $np$  states through  $n = 13$ . An improved calculation of the Lamb-shift effects was reported by Mohr (1983), who gave the energy separations among the  $n = 1$  and 2 levels. Gould and Marrus (1983) have measured the Lamb-shift of the  $2s \ ^2S_{1/2}$  state of Ar XVIII, obtaining the value 1264(13)  $\text{cm}^{-1}$ . Their results agrees with the value 1275.8(0.8)  $\text{cm}^{-1}$  calculated by Mohr and is three standard deviations lower than Erickson's value of 1301(2)  $\text{cm}^{-1}$ .

Mohr's results for the energy separations of  $n = 1$  and 2 levels have been compiled, and Erickson's for  $n = 3-5$  relative to the  $2p \ ^3P_{3/2}$  level. This increases Erickson's values for the levels, or, equivalently, increases the binding energy of the ground state (the ionization energy). Assuming that the uncertainty in these compiled values is mainly due to the error in the Lamb shift, the fractional error is taken as equal to the experimental fractional error in the Ar measurement. This contribution to the level values relative to the ground state is about 4 parts in  $10^6$  for the iron period. This is about 10 times the error estimated by Mohr for his calculated  $1s - 2p$  intervals. The corresponding intervals calculated by Erickson are lower than those of Mohr by about the same fractional amount.

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## Cr I

Z = 24

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^4 4s^1 \ ^3S_1$ Ionization energy =  $54575.6 \pm 0.3 \text{ cm}^{-1}$  ( $6.76669 \pm 0.00004 \text{ eV}$ )

The early contributions to the analysis of this spectrum are summarized by Catalán and Sancho (1931), who give a list of over 700 classified lines. Kiess (1953) remeasured the spectrum in the range of 11 610–189° Å with a wavelength accuracy varying from  $\pm 0.005 \text{ Å}$  to  $\pm 0.05 \text{ Å}$ . About 4400 lines are given, 80% of which are classified, including Zeeman patterns for 10% of them. This constituted a significant extension of the analysis and provided improved values for all the known levels with an estimated uncertainty of  $\pm 0.05 \text{ cm}^{-1}$ . Kiess obtained a value for the ionization energy of  $54\,570 \text{ cm}^{-1}$ .

An absorption spectrum below 2000 Å was observed by Huber, Sandeman, and Tubbs (1975) with an accuracy of  $\pm 0.004 \text{ Å}$ . They identified the  $3d^3(^3S)np \ ^3P^\circ$  Rydberg series for  $n=8$  and for  $n=12-38$  with an uncertainty of  $\pm 0.1 \text{ cm}^{-1}$ , from which they derived a value for the ionization energy of  $54\,575.6 \pm 0.3 \text{ cm}^{-1}$ . Improved wavelengths are given for the multiplets  $a \ ^3D-q \ ^3D'$ ,  $a \ ^3D-o \ ^3F'$ , and  $a \ ^3D-r \ ^3P'$  reported by Kiess.

Further observations of the absorption spectrum at lower wavelengths were reported by Connerade, Baig, and Newsom (1981) with an accuracy of  $\pm 0.05 \text{ Å}$ . They identified five  $3d^3(^3S)4s \ ^3S - 3d^4(^3D)4s \ (^3D)np$  series for  $n=6$  to  $n=28$ . For  $n=6$  the term structure is identified by means of a diagonalization of the energy matrices of the  $3d^4 4s 6p$  configuration, as well as by quantum defects. Their results contradict the assignment by Kiess of terms to  $3d^4 4s 6p$ , which we have therefore dropped. The levels identified by Connerade, Baig, and Newsom with this configuration and their percentage compositions are given. They have also observed the principal series  $3d^3(^3S)np \ ^3P^\circ$  reported by Huber et al. and have identified the missing  $7p$ ,  $9p$ ,  $10p$ , and  $11p$  terms.

Mansfield (1977) reported the observation in absorption of the  $3p^3(^3P)3d^3(^3S)4s^2 \ ^3P^\circ$  term.

Most of the  $g$ -factors for the levels are obtained from Catalán and Sancho, supplemented by Kiess' three-decimal-place values. The more accurate values for the  $3d^3(^3S)4p \ ^3P^\circ$  and  $^3P^\circ$  levels were measured in an atomic beam by Budick, Goshen, and Marcus (1964), and those

for  $3d^3(^3S)4s \ ^3S$  and  $3d^4 4s^2 \ ^3D$  were obtained by Childs and Goodman (1965).

The alphabetic prefixing of terms with lower case letters for distinguishing repeating terms of the same type has been retained from Kiess except where the levels were reinterpreted by Roth (1970) on the basis of his theoretical treatment.

Roth has calculated the odd-parity configurations  $3d^3 4p$ ,  $3d^4 4s 4p$ , and  $3d^4 4s^2 4p$  with configuration interaction. His percentage compositions and designation changes for the experimental levels are adopted here. Roth distinguished repeating terms of the  $3d^3$  core by the letters, a, b, ... rather than by seniority. The percentages include the sum of seniority states contributing to the term.

Fischer, Hansen, and Barwell (1976) pointed out that an error in Roth's calculation arising from insufficient precision in his diagonalization routine resulted in an incorrect mixture of the  $z \ ^3D'$  and  $y \ ^3P'$  terms. Revised percentages were provided for these terms and for  $z \ ^3P'$  by Hansen.

Percentages for the configuration  $3d^4 4s$  were taken from an ab initio calculation by Vizbaraitė, Kupliauskis, and Tutlys (1968).

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## E-5

Cr I

Configuration	Term	J	Level (cm <sup>-1</sup> )	g	Leading percentages		
3d <sup>5</sup> ( <sup>6</sup> S)4s	a <sup>7</sup> S	3	0.00	2.00183	100		
3d <sup>5</sup> ( <sup>6</sup> S)4s	a <sup>5</sup> S	2	7 593.16	2.005	100		
3d <sup>4</sup> 4s <sup>2</sup>	a <sup>3</sup> D	0	7 750.78				
		1	7 810.82	1.50060			
		2	7 927.47	1.50060			
		3	8 095.21	1.50060			
		4	8 307.57	1.50060			
3d <sup>5</sup> ( <sup>4</sup> G)4s	a <sup>3</sup> G	2	20 517.40	0.37	100		
		6	20 519.60	1.33	100		
		3	20 520.92	0.93	100		
		4	20 523.69	1.13	100		
		5	20 523.94	1.25	100		
3d <sup>5</sup> ( <sup>4</sup> P)4s	a <sup>3</sup> P	3	21 840.84	1.6	98		
		2	21 847.88	1.847	98		
		1	21 856.94	2.500	100		
3d <sup>4</sup> 4s <sup>2</sup>	a <sup>3</sup> P	0	23 163.27				
		1	23 512.00				
		2	24 093.16				
3d <sup>5</sup> ( <sup>4</sup> S)4p	z <sup>3</sup> P <sup>o</sup>	2	23 305.01	2.334	67	33	3d <sup>4</sup> ( <sup>5</sup> D)4s4p( <sup>3</sup> P <sup>o</sup> ) <sup>3</sup> P <sup>o</sup>
		3	23 386.35	1.9176	67	33	
		4	23 498.84	1.7510	67	31	
3d <sup>4</sup> 4s <sup>2</sup>	a <sup>3</sup> H	4	23 933.90				
		5	24 056.11				
		6	24 200.23				
3d <sup>5</sup> ( <sup>4</sup> D)4s	b <sup>3</sup> D	0	24 277.06		100		
		4	24 282.24	1.51	100		
		1	24 286.54	1.48	100		
		2	24 299.89	1.51	98		
		3	24 303.94	1.55	98		
3d <sup>5</sup> ( <sup>4</sup> G)4s	a <sup>3</sup> G	3	24 833.86		100		
		4	24 897.55		100		
		5	25 038.61		100		
3d <sup>4</sup> 4s <sup>2</sup>	a <sup>3</sup> F	2	24 940.61				
		3	25 106.34				
		4	25 177.39				
3d <sup>4</sup> ( <sup>5</sup> D)4s4p( <sup>3</sup> P <sup>o</sup> )	z <sup>3</sup> P <sup>o</sup>	0	24 971.21		100		
		1	25 010.84	1.52	100		
		2	25 089.20	1.50	100		
		3	25 206.02	1.49	100		
		4	25 359.82	1.51	100		
		5	25 548.64	1.51	100		
3d <sup>4</sup> ( <sup>4</sup> S)4p	z <sup>3</sup> P <sup>o</sup>	3	26 787.50	1.670	92		
		2	26 796.28	1.830	91		
		1	26 801.93	2.512	92		

## Cr I—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	<i>g</i>	Leading percentages	
$3d^5(^6P)4s$	$b^3P$	0	27 163.20		100	
		1	27 176.22		100	
		2	27 223.05		98	
$3d^4(^1D)4s4p(^3P^o)$	$z^1D^o$	1	27 300.19	3.01	99	
		2	27 382.18	1.99	99	
		3	27 500.37	1.76	99	
		4	27 649.71	1.66	99	
		5	27 825.45	1.61	100	
$3d^4 4s^2$	$b^1G$	3	27 597.22			
		4	27 703.54			
		5	27 816.88			
$3d^4(^1D)4s4p(^3P^o)$	$y^1P^o$	2	27 728.87	2.341	66	33 $3d^5(^6S)4p^1P^o$
		3	27 820.23	1.929	66	33
		4	27 935.26	1.761	67	32
$3d^5(^1D)4s$	$a^3D$	3	28 637.00		100	
		1	28 679.43		100	
		2	28 682.18		98	
$3d^4(^1D)4s4p(^3P^o)$	$y^3P^o$	1	29 420.90	2.513	95	
		2	29 584.62	1.836	95	
		3	29 824.75	1.669	96	
$3d^4(^1D)4s4p(^3P^o)$	$z^3P^o$	1	30 787.30	0.002	96	
		2	30 858.82	0.997	96	
		3	30 965.46	1.245	96	
		4	31 106.37	1.345	95	
		5	31 280.25	1.396	96	
$3d^5(^3D3)4s$	$b^3D$	3	31 009.00		56	18 $(^1D1)^3D$
		2	31 028.33		56	24 $(^1P^o)^3P$
		1	31 048.85		45	41 $(^1P^o)^3P$
$3d^5(^1I)4s$	$a^3I$	7	31 048.00		100	
		6	31 049.33		100	
		5	31 055.35		100	
$3d^5(^1F)4s$	$a^3F$	1	31 352.42		59	31 $(^1D3)^3D$
		2	31 355.21		74	12
		3	31 364.33		88	6
		4	31 377.96		100	
		5	31 393.40		100	
$3d^4 4s^2$	$a^1G$	4	31 987.06			
$3d^4 4s^2$	$a^1I$	6	32 097.36			
$3d^5(^3P1)4s$	$b^3P$	2	33 040.10		79	14 $(^1D3)^3D$
		3	33 060.74		83	13
		4	33 113.27		100	
$3d^4(^1D)4s4p(^3P^o)$	$z^3D^o$	0	33 338.20		89	8 $^3P^o$
		1	33 423.79	1.499	93	
		2	33 542.11	1.497	96	
		3	33 671.55	1.497	97	
		4	33 816.06	1.499	97	

## Cr I—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages		
3d <sup>5</sup> ( <sup>1</sup> D)4s4p( <sup>1</sup> P°)	z <sup>3</sup> P°	0	33 762.56		88	s	<sup>3</sup> D°
		1	33 897.26	1.49	92		
		2	34 190.49	1.55	95		
3d <sup>5</sup> ( <sup>1</sup> F)4s	b <sup>1</sup> I	6	33 762.74		100		
3d <sup>5</sup> 4s <sup>2</sup>	c <sup>3</sup> D	1	33 906.65				
		3	33 934.88				
		2	33 935.65				
3d <sup>6</sup>	c <sup>3</sup> D	4	35 398.02				
		3	35 501.26				
		2	35 572.94				
		1	35 618.51				
		0	35 640.69				
3d <sup>5</sup> ( <sup>1</sup> F)4s	c <sup>3</sup> F	2	35 807.90		100		
		3	35 813.73		100		
		4	35 862.82		98		
3d <sup>5</sup> ( <sup>1</sup> H)4s	b <sup>3</sup> H	4	35 870.53		98		
		5	35 884.40		98		
		6	35 934.02		100		
3d <sup>5</sup> ( <sup>1</sup> D)4s4p( <sup>1</sup> P°)	z <sup>3</sup> F°	2	35 897.87		95		
		3	36 024.22		95		
		4	36 212.15		95		
3d <sup>5</sup> ( <sup>1</sup> F)2)4s	d <sup>3</sup> F	3	36 552.13		100		
		2	36 558.55		100		
		4	36 577.73		100		
3d <sup>5</sup> ( <sup>1</sup> S)5s	e <sup>1</sup> S	3	36 895.73				
3d <sup>5</sup> ( <sup>1</sup> G)2)4s	c <sup>3</sup> G	3	37 205.88		98		
		5	37 233.50		96		
		4	37 244.17		98		
3d <sup>5</sup> ( <sup>1</sup> S)5s	e <sup>1</sup> S	2	37 883.34				
3d <sup>5</sup> ( <sup>1</sup> H)4s	a <sup>1</sup> H	5	38 537.68		98		
3d <sup>5</sup> ( <sup>1</sup> D)4s4p( <sup>3</sup> P°)	z <sup>3</sup> D°	1	38 597.06		95		
		2	38 730.67		95		
		3	38 911.33		95		
3d <sup>5</sup> ( <sup>1</sup> G)2)4s	b <sup>1</sup> G	4	39 158.63		98		
3d <sup>5</sup> ( <sup>1</sup> D)4s4p( <sup>1</sup> P°)	y <sup>1</sup> P°	1	40 906.46	0.004	84	12	3d <sup>5</sup> ( <sup>1</sup> G)4p <sup>1</sup> P°
		2	40 971.29	1.28	83	12	
		3	41 086.26	1.246	83	12	
		4	41 224.78	1.360	82	13	
		5	41 393.47		82	14	
3d <sup>5</sup> ( <sup>1</sup> D)4s4p( <sup>1</sup> P°)	x <sup>1</sup> P°	1	40 930.31	2.455	68	7	3d <sup>5</sup> ( <sup>1</sup> P)4p <sup>1</sup> P°
		2	40 982.97	1.76	56	7	
		3	41 043.35	1.640	55	8	

## Cr I—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	g	Leading percentages			
3d <sup>4</sup> ( <sup>3</sup> D)4s4p( <sup>1</sup> P°)	y <sup>3</sup> D°	0	41 224.80		52	14	3d <sup>4</sup> ( <sup>1</sup> P)4p <sup>3</sup> D°	
		1	41 289.17	1.503	54	14		
		2	41 409.03	1.504	56	13		
		3	41 575.10	1.503	58	13		
		4	41 782.19	1.500	62	14		
3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°)	z <sup>3</sup> H°	3	42 025.60		61	29	3d <sup>4</sup> ( <sup>4</sup> G)4p <sup>3</sup> H°	
		4	42 079.81		55	19	3d <sup>4</sup> ( <sup>4</sup> G)4p <sup>3</sup> H°	
		5	42 152.74		48	17	3d <sup>4</sup> ( <sup>4</sup> G)4p <sup>3</sup> H°	
		7	42 387.32		65	24	3d <sup>4</sup> ( <sup>4</sup> G)4p <sup>3</sup> H°	
3d <sup>4</sup> (a <sup>3</sup> P)4s4p( <sup>3</sup> P°)	x <sup>3</sup> D°	0	42 218.37		49	26	3d <sup>4</sup> ( <sup>3</sup> D)4s4p( <sup>1</sup> P°) <sup>3</sup> D°	
		1	42 292.96	1.501	47	26		
		2	42 433.82	1.494	43	21		
		3	42 643.26	1.498	46	22		
		4	42 908.57	1.497	45	20		
3d <sup>4</sup> ( <sup>4</sup> S)5p	x <sup>3</sup> P°	2	42 233.04					
3		42 254.11						
4		42 275.20						
3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°)		6	42 252.17		30	<sup>3</sup> H°	25	3d <sup>4</sup> ( <sup>4</sup> G)4p <sup>3</sup> G°
3d <sup>4</sup> ( <sup>4</sup> S)4d	e <sup>3</sup> D	1	42 253.42					
		2	42 254.52					
		3	42 256.26					
		4	42 258.37					
		5	42 261.06	1.55				
3d <sup>4</sup> ( <sup>4</sup> G)4p	z <sup>4</sup> G°	2	42 515.25	0.35	61	30	3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°) <sup>4</sup> G°	
		3	42 532.81		57	19	3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°) <sup>4</sup> G°	
		4	42 564.85		53	18	3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°) <sup>4</sup> G°	
		5	42 589.25	1.23	47	16	3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°) <sup>4</sup> G°	
		6	42 605.81	1.32	57	27	3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°) <sup>4</sup> H°	
3d <sup>4</sup> ( <sup>4</sup> P)4p	z <sup>4</sup> S°	2	43 124.88	1.93	46	46	3d <sup>4</sup> (a <sup>3</sup> P)4s4p( <sup>3</sup> P°) <sup>4</sup> S°	
3d <sup>4</sup> ( <sup>4</sup> S)4d	e <sup>4</sup> D	4	44 060.87					
		3	44 068.72					
		2	44 080.90					
		1	44 088.92					
		0	44 082.80					
3d <sup>4</sup> ( <sup>4</sup> S)5p	w <sup>3</sup> P°	1	44 125.90	2.74				
		2	44 136.92	1.79				
		3	44 259.90	1.68				
3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°)	z <sup>3</sup> T°	4	44 246.70		90			
		5	44 307.96		90			
		6	44 332.10		90			
		7	44 514.44		90			
		8	44 666.55		100			
3d <sup>4</sup> (a <sup>3</sup> P)4s4p( <sup>3</sup> P°)	y <sup>4</sup> G°	2	44 299.90	0.35	66			
		3	44 379.24	0.98	69			
		4	44 524.46		68	18	<sup>4</sup> P°	
		5	44 591.46	1.25	66	29	<sup>4</sup> P°	
		6	44 748.98	1.34	66	5	3d <sup>4</sup> ( <sup>4</sup> G)4s4p( <sup>3</sup> P°) <sup>4</sup> G°	

## Cr I—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	g	Leading percentages			
3d <sup>4</sup> (a <sup>3</sup> P)4s4p( <sup>3</sup> P)	c <sup>3</sup> P	1	44 668.74	2.47	78	8	3d <sup>4</sup> ( <sup>3</sup> D)4p <sup>3</sup> P	
		2	44 875.19		76	9		
		3	45 113.22	1.65	70	13		
3d <sup>4</sup> (a <sup>3</sup> F)4s4p( <sup>3</sup> P)	x <sup>3</sup> P	1	45 201.84		66	28	3d <sup>4</sup> ( <sup>3</sup> G)4p <sup>3</sup> P	
		2	45 225.20		62	27	3d <sup>4</sup> ( <sup>3</sup> G)4p <sup>3</sup> P	
		3	45 255.51		58	26	3d <sup>4</sup> ( <sup>3</sup> G)4p <sup>3</sup> P	
		4	45 286.08		59	23	3d <sup>4</sup> ( <sup>3</sup> G)4p <sup>3</sup> P	
3d <sup>4</sup> (a <sup>3</sup> F)4s4p( <sup>3</sup> P)		5	45 306.45	1.41	37	<sup>3</sup> G	34	<sup>3</sup> P
3d <sup>4</sup> ( <sup>3</sup> G)4p	z <sup>3</sup> H	6	45 348.73		68	16	<sup>3</sup> H	
		5	45 354.18		69	32		
		4	45 358.63		59	25		
3d <sup>4</sup> ( <sup>3</sup> G)4p	y <sup>3</sup> H	3	45 568.02	0.52	76	22	3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P) <sup>3</sup> H	
		4	45 614.88		51	29	3d <sup>4</sup> ( <sup>3</sup> G)4p <sup>3</sup> H	
		5	45 662.28		43	28	3d <sup>4</sup> ( <sup>3</sup> G)4p <sup>3</sup> H	
		6	45 707.96		58	29	3d <sup>4</sup> ( <sup>3</sup> G)4p <sup>3</sup> H	
		7	45 741.49		1.29	74	25	3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P) <sup>3</sup> H
3d <sup>4</sup> ( <sup>4</sup> S)6s	f <sup>4</sup> S	3	45 643.38	2.05				
3d <sup>4</sup> ( <sup>4</sup> P)4p	y <sup>4</sup> P	1	45 719.20		45	24	3d <sup>4</sup> (a <sup>3</sup> P)4s4p( <sup>3</sup> P) <sup>4</sup> P	
		0	45 722.59		39	31		
		2	45 734.32		69	29		
3d <sup>4</sup> ( <sup>4</sup> G)4p	y <sup>4</sup> P	2	45 966.45		75	8	3d <sup>4</sup> (a <sup>3</sup> F)4s4p( <sup>3</sup> P) <sup>4</sup> P	
		3	46 000.36		69	8		
		4	46 058.20		63	7		
3d <sup>4</sup> ( <sup>4</sup> S)6s	f <sup>4</sup> S	2	45 967.81					
3d <sup>4</sup> ( <sup>4</sup> P)4p		1	46 077.09		22	<sup>4</sup> D	19	3d <sup>4</sup> ( <sup>4</sup> D)4p <sup>4</sup> P
3d <sup>4</sup> (a <sup>3</sup> F)4s4p( <sup>3</sup> P)	u <sup>4</sup> D	0	46 081.27		69	25	3d <sup>4</sup> (a <sup>3</sup> P)4s4p( <sup>3</sup> P) <sup>4</sup> D	
		1	46 298.32		62	29		
		2	46 349.50		69	22		
		3	46 368.35		36	27		
4	46 422.16	39	34					
3d <sup>4</sup> ( <sup>4</sup> P)4p		2	46 109.26	1.24	23	<sup>4</sup> D	14	3d <sup>4</sup> ( <sup>4</sup> D)4p <sup>4</sup> P
3d <sup>4</sup> ( <sup>4</sup> P)4p		3	46 174.40	1.33	37	<sup>4</sup> D	15	3d <sup>4</sup> (a <sup>3</sup> P)4s4p( <sup>3</sup> P) <sup>4</sup> D
3d <sup>4</sup> 4s6s	f <sup>4</sup> D	1	46 448.60	2.99				
		2	46 524.84	1.99				
		3	46 637.21	1.77				
		4	46 783.06	1.63				
		5	46 958.98	1.61				
3d <sup>4</sup> ( <sup>3</sup> G)4s4p( <sup>3</sup> P)	u <sup>4</sup> P	2	46 677.06		20	18	3d <sup>4</sup> ( <sup>4</sup> D)4p <sup>4</sup> P	
		1	46 678.35		21	18		
		3	46 688.24		1.25	23		22
		5	46 704.98		1.37	23		20
		4	46 720.54			23		24

## Cr I—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	<i>g</i>	Leading percentages		
$3d^4(^3H)4s4p(^3P)$	$z^3G^o$	3	46 846.77		42	20	$3d^4(a^3P)4s4p(^3P)^3G^o$
		4	46 905.03		40	21	$3d^4(a^3P)4s4p(^3P)^3G^o$
		5	46 985.87		34	20	$3d^4(^4G)4p^3G^o$
$3d^4(^3P)4p$	$u^3P^o$	3	46 878.61	1.68	47	20	$3d^4(^4D)4p^3P^o$
		2	46 967.70	1.84	51	20	
		1	47 021.75	2.42	55	20	
$3d^4(^3H)4s4p(^3P)$	$x^3G^o$	2	47 067.47	0.45	67	15	$3d^4(^4G)4p^3G^o$
		3	47 125.70	0.96	62	14	
		4	47 189.87		60	15	
		6	47 222.27	1.44	70	19	
		5	47 228.80	1.27	63	16	
$3d^4(^4G)4p$	$y^3G^o$	3	47 048.48		73	12	$3d^4(^3H)4s4p(^3P)^3G^o$
		4	47 054.91		60	16	
		5	47 055.31		62	24	
$3d^4(a^3P)4s4p(^3P)$	$z^3S^o$	1	47 088.40		72	8	$3d^4(^4P)4p^3S^o$
$3d^4(^3H)4s4p(^3P)$	$z^3T^o$	5	47 586.06		61	28	$3d^4(^4G)4s4p(^3P)^3H^o$
		6	47 630.63		57	34	
		7	47 692.63		52	40	
$3d^4(^3G)4s4p(^3P)$	$x^3H^o$	3	47 621.31		79	12	$3d^4(^3H)4s4p(^3P)^3H^o$
		4	47 638.51		82	11	$3d^4(^3H)4s4p(^3P)^3H^o$
		5	47 722.82		56	30	$3d^4(^3H)4s4p(^3P)^3T^o$
		6	47 942.29		53	35	$3d^4(^3H)4s4p(^3P)^3T^o$
		7	48 140.18		40	42	$3d^4(^3H)4s4p(^3P)^3T^o$
$3d^4(^4D)4s5p(^3P)$	$v^3P^o$	1	47 629.66				
		2	47 631.51				
		3	47 636.25				
		4	47 639.84	1.34			
		5	47 644.76				
$3d^4(^4S)6p$	$w^3P^o$	2	47 697.44				
		3	47 708.59				
		4	47 719.08				
$3d^4(^4S)5d$	$g^3D$	1	47 700.18				
		2	47 700.95				
		3	47 702.30				
		4	47 704.66				
		5	47 709.80				
$3d^4(^4P)4p$	$v^3D^o$	1	47 772.30	1.37	40	26	$3d^4(a^3P)4s4p(^3P)^3D^o$
		2	47 786.10	1.20	40	26	
		0	47 788.08		46	27	
		3	47 814.40	1.53	40	25	
		4	47 866.48	1.50	52	23	
$3d^4(^4G)4p$		1	47 877.55	0.00	15	$^3P^o$ 15	$3d^4(a^3P)4s4p(^3P)^3P^o$
$3d^4(^4G)4p$	$u^3P^o$	2	47 917.93	1.04	35	19	$3d^4(a^3P)4s4p(^3P)^3P^o$
		3	47 974.53	1.26	35	20	
		5	47 985.76	1.38	30	25	
		4	48 014.40		30	23	
		4	48 042.30				



## Cr I—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	g	Leading percentages			
3d <sup>4</sup> (a <sup>1</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	<sup>3</sup> D <sup>o</sup>	1	48 210.04		59	7	3d <sup>4</sup> ( <sup>4</sup> G)4p <sup>3</sup> F <sup>o</sup>	
		2	48 217.83		61	6		
		3	48 251.91		64	5		
3d <sup>4</sup> (a <sup>1</sup> P)4s4p( <sup>3</sup> P <sup>o</sup> )	x <sup>3</sup> P <sup>o</sup>	0	48 226.36		29	24	3d <sup>4</sup> ( <sup>3</sup> P)4p <sup>3</sup> P <sup>o</sup>	
		1	48 331.90		28	15		
		2	48 458.67		42	19		
3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P <sup>o</sup> )	y <sup>3</sup> H <sup>o</sup>	4	48 288.37		76			
		5	48 310.39		80			
		6	48 445.35		83			
3d <sup>4</sup> 4s5s	f <sup>3</sup> D	0	48 488.23					
		1	48 507.56					
		2	48 558.57					
		3	48 661.59	1.46				
	4	48 824.50	1.46					
	x <sup>4</sup> G <sup>o</sup>	3	48 515.08					
		4	48 562.16					
		5	48 786.39					
	3d <sup>4</sup> (a <sup>1</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	<sup>3</sup> F <sup>o</sup>	3	48 636.14		69	15	3d <sup>4</sup> ( <sup>2</sup> G)4s4p( <sup>3</sup> P <sup>o</sup> ) <sup>3</sup> F <sup>o</sup>
	3d <sup>4</sup> (a <sup>1</sup> P)4s4p( <sup>3</sup> P <sup>o</sup> )	x <sup>3</sup> D <sup>o</sup>	1	48 839.90		38	29	3d <sup>4</sup> ( <sup>3</sup> P)4p <sup>3</sup> D <sup>o</sup>
2			49 027.58		46	14		
3			49 310.86		61	7		
3d <sup>4</sup> ( <sup>4</sup> S)7s	g <sup>4</sup> S	3	49 177.83					
3d <sup>4</sup> ( <sup>4</sup> S)7s	g <sup>4</sup> S	2	49 321.51					
3d <sup>4</sup> (a <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	w <sup>4</sup> G <sup>o</sup>	3	49 370.70		49	9	3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P <sup>o</sup> ) <sup>4</sup> G <sup>o</sup>	
		4	49 452.94		49	13		
		5	49 538.06		51	17		
3d <sup>4</sup> ( <sup>4</sup> G)4s4p( <sup>3</sup> P <sup>o</sup> )	w <sup>4</sup> G <sup>o</sup>	2	49 466.77		66	18	3d <sup>4</sup> ( <sup>4</sup> G)4p <sup>4</sup> G <sup>o</sup>	
		3	49 519.72	1.04	68	14		
		4	49 572.03		68	19		
		5	49 617.61		70	17		
		6	49 635.16	1.25	73	17		
		3d <sup>4</sup> ( <sup>4</sup> P)4p	y <sup>4</sup> S <sup>o</sup>	1	49 477.04		73	17
2	49 586.28							
3	49 717.88							
4	49 862.50							
3d <sup>4</sup> ( <sup>4</sup> D)4p	t <sup>4</sup> P <sup>o</sup>	1	49 588.97	2.48	46	29	3d <sup>4</sup> ( <sup>4</sup> P)4p <sup>4</sup> P <sup>o</sup>	
		3	49 812.16	1.77	51	26		
3d <sup>4</sup> (a <sup>3</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )		2	49 598.08	1.88	29	<sup>1</sup> D <sup>o</sup>	14	3d <sup>4</sup> ( <sup>4</sup> D)4p <sup>4</sup> P <sup>o</sup>
3d <sup>4</sup> ( <sup>4</sup> D)4p	x <sup>4</sup> P <sup>o</sup>	4	49 620.69		66	15	3d <sup>4</sup> ( <sup>2</sup> G)4s4p( <sup>3</sup> P <sup>o</sup> ) <sup>4</sup> P <sup>o</sup>	
		3	49 650.22		69	18		
		2	49 652.76		37	18		
3d <sup>4</sup> (a <sup>1</sup> P)4s4p( <sup>3</sup> P <sup>o</sup> )	y <sup>4</sup> S <sup>o</sup>	2	49 822.59	2.00	31	29	3d <sup>4</sup> ( <sup>4</sup> P)4p <sup>4</sup> S <sup>o</sup>	

## Cr I—Continued

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	g	Leading percentages		
$3d^4(^4D)4p$	$^4F^o$	1	50 018.80		44	29	$3d^4(^4G)4s4p(^4P^o)^4F^o$
		2	50 057.61		43	29	
		3	50 102.04	1.27	44	29	
		4	50 210.87	1.25	30	21	
		5	50 252.27	1.39	46	30	
$3d^4(^4D)4p$	$^4D^o$	1	50 105.54		66	11	$3d^4(^4P)4p^4D^o$
		2	50 184.10		57	14	
		3	50 264.48		51	18	
$3d^4(^4S)7p$	$^4P^o$	3	50 185				
		4	50 197				
$3d^4(^4D)4p$	$^4D^o$	4	50 557.56	1.54	44	15	$3d^4(^4D)4p^4F^o$ $3d^4(^4P)4p^4D^o$ $3d^4(^4P)4p^4D^o$ $3d^4(^4P)4p^4D^o$ $3d^4(^4P)4p^4D^o$
		3	50 622.11	1.54	60	7	
		2	50 654.76	1.51	68	8	
		0	50 661.20		60	10	
		1	50 662.77	1.46	71	9	
$3d^4(^4G)4s4p(^4P^o)$	$^4F^o$	2	50 890.15		41	27	$3d^4(^4D)4p^4F^o$
		3	50 950.42		42	26	
		4	51 059.79		46	23	
$3d^4(^4S)8s$	$^4S$	2	51 035.68				
$3d^4(^4D)4p$	$^4P^o$	0	51 176.88		71	11	$3d^4(^4P)4s4p(^4P^o)^4P^o$ $3d^4(^4P)4s4p(^4P^o)^4P^o$ $3d^4(^4P)4s4p(^4P^o)^4D^o$
		1	51 246.87		68	8	
		2	51 286.52		45	22	
$3d^4(^4H)4s4p(^4P^o)$	$^4H^o$	5	51 401.24		60	11	$3d^4(^4I)4p^4H^o$
$3d^4(^4S)8p$	$^4P^o$	2	51 529.4				
		3	51 531.5				
		4	51 534.4				
$3d^4(^4D)4s4p(^4P^o)$	$^4D^o$	0	51 999.62		94		
		1	52 002.06		94		
		2	52 012.44		98		
		3	52 031.72		92		
		4	52 064.27		92		
$3d^4(^4S)9p$	$^4P^o$		52 241				
$3d^4(^4I)4s4p(^4P^o)$	$^4I^o$	5	52 591.94		48	28	$3d^4(^4I)4p^4I^o$
		6	52 600.61		48	28	
		7	52 677.88		49	28	
$3d^4(^4G)4s4p(^4P^o)$	$^4G^o$	4	52 790.07		72	14	$3d^4(^4H)4s4p(^4P^o)^4G^o$
$3d^4(^4S)10p$	$^4P^o$		52 857.2				
$3d^4(^4G)4s4p(^4P^o)$	$^4H^o$	5	52 885.29		67	27	$3d^4(^4I)4p^4H^o$
		6	52 914.94		68	26	
		4	52 962.44		47	26	
$3d^4(^4D)4s4p(^4P^o)$	$^4F^o$	1	53 011.65		66	6	$3d^4(^4D)4p^4F^o$
		2	53 037.52		64	6	
		3	53 072.90		60	6	
		4	53 117.54		61	6	
		5	53 172.22	1.42	66	7	

## Cr I—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages	
3d <sup>4</sup> 4s4d	e <sup>3</sup> G	1	53 148.35			
		2	53 177.87			
		3	53 226.49			
		4	53 298.90			
		5	53 393.50			
		6	53 517.85			
		7	53 662.64			
3d <sup>4</sup> 4s4d	h <sup>3</sup> D	2	53 195.03			
		3	53 284.34			
		4	53 375.46			
		5	53 627.75			
3d <sup>4</sup> 4s4d	e <sup>3</sup> F	1	53 215.40			
		2	53 279.80			
		3	53 384.72			
		4	53 526.22			
		5	53 706.06			
		6	53 927.47			
3d <sup>4</sup> (4S)11p	<sup>3</sup> P°		53 217.0			
3d <sup>4</sup> (4S)12p	<sup>3</sup> P°		53 484.5			
3d <sup>4</sup> 4s5p	s <sup>3</sup> D°	2	53 541.25			
		3	53 640.74			
		4	53 782.77			
3d <sup>4</sup> (4S)13p	<sup>3</sup> P°		53 671.4			
3d <sup>4</sup> (4F)4s <sup>2</sup> 4p	o <sup>3</sup> G°	3	53 804.84		28	22
		4	53 927.59		26	22
		5	54 078.13		25	22
3d <sup>4</sup> (4S)14p	<sup>3</sup> P°		53 815.8			
3d <sup>4</sup> (4S)15p	<sup>3</sup> P°		53 928.0			
3d <sup>4</sup> 4s5p	s <sup>3</sup> P°	1	53 963.05			
		2	54 032.63			
		3	54 132.88			
3d <sup>4</sup> (4S)16p	<sup>3</sup> P°		54 017.1			
3d <sup>4</sup> (4S)17p	<sup>3</sup> P°		54 089.0			
3d <sup>4</sup> (4S)18p	<sup>3</sup> P°		54 147.7			
3d <sup>4</sup> (4S)19p	<sup>3</sup> P°		54 196.6			
3d <sup>4</sup> 4s5p	g <sup>3</sup> P°	1	54 198.23			
		2	54 252.19			
		3	54 328.95			
		4	54 425.29			
		5	54 536.53			
3d <sup>4</sup> (4S)20p	<sup>3</sup> P°		54 237.7			
3d <sup>4</sup> (4S)21p	<sup>3</sup> P°		54 272.4			

3d<sup>4</sup> (4F)4p<sup>3</sup>G°

## Cr I—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages		
	<i>e</i> <sup>3</sup> F	1	54 296.76				
		2	54 383.36				
		3	54 476.29				
		4	54 572.84				
		5	54 660.31				
3d <sup>2</sup> ( <sup>4</sup> S)22p	<sup>1</sup> F		54 902.4				
3d <sup>2</sup> ( <sup>2</sup> I)4p	<sup>3</sup> K	6	54 916.83		54	42	3d <sup>2</sup> ( <sup>1</sup> I)4s4p( <sup>3</sup> P) <sup>3</sup> K
		7	54 404.94		54	46	
		8	54 498.27		50	41	
3d <sup>2</sup> ( <sup>4</sup> S)23p	<sup>1</sup> F		54 337.2				
3d <sup>2</sup> ( <sup>4</sup> S)24p	<sup>1</sup> F		54 349.5				
3d <sup>2</sup> ( <sup>4</sup> S)25p	<sup>1</sup> F		54 368.6				
3d <sup>2</sup> ( <sup>4</sup> S)26p	<sup>1</sup> F		54 385.5				
3d <sup>2</sup> ( <sup>4</sup> S)27p	<sup>1</sup> F		54 400.5				
3d <sup>2</sup> ( <sup>4</sup> S)28p	<sup>1</sup> F		54 413.5				
3d <sup>2</sup> ( <sup>4</sup> S)29p	<sup>1</sup> F		54 425.4				
3d <sup>2</sup> ( <sup>4</sup> S)30p	<sup>1</sup> F		54 436.1				
3d <sup>2</sup> ( <sup>4</sup> S)31p	<sup>1</sup> F		54 445.0				
3d <sup>2</sup> ( <sup>4</sup> S)32p	<sup>1</sup> F		54 453.4				
3d <sup>2</sup> ( <sup>4</sup> S)33p	<sup>1</sup> F		54 461.7				
3d <sup>2</sup> ( <sup>4</sup> S)34p	<sup>1</sup> F		54 468.5				
3d <sup>2</sup> ( <sup>4</sup> S)35p	<sup>1</sup> F		54 474.8				
3d <sup>2</sup> ( <sup>4</sup> S)36p	<sup>1</sup> F		54 480.6				
3d <sup>2</sup> ( <sup>4</sup> S)37p	<sup>1</sup> F		54 485.4				
3d <sup>2</sup> ( <sup>4</sup> S)38p	<sup>1</sup> F		54 491.2				
Cr II ( <sup>6</sup> S <sub>1/2</sub> )	<i>Limit</i>		54 576.6				
3d <sup>2</sup> 4s <sup>2</sup>	<i>g</i> <sup>3</sup> D	0	54 646.20				
		1	54 671.90				
		2	54 818.55				
		3	54 906.82				
		4	55 209.01				
3d <sup>2</sup> ( <sup>3</sup> H)4s4p( <sup>1</sup> P)	<i>w</i> <sup>3</sup> H	4	54 736.55		42	20	3d <sup>2</sup> ( <sup>2</sup> I)4p <sup>3</sup> H
		5	54 799.18		41	21	
		6	54 886.82		42	24	
3d <sup>2</sup> ( <sup>1</sup> I)4s4p( <sup>3</sup> P)	<sup>3</sup> K	6	54 800.26		55	40	3d <sup>2</sup> ( <sup>2</sup> I)4p <sup>3</sup> K
3d <sup>2</sup> 4s <sup>2</sup>	<i>e</i> <sup>3</sup> D	1	54 804.69				
		2	54 974.64				
		3	55 204.79				
3d <sup>2</sup> ( <sup>4</sup> G)5p	<i>v</i> <sup>3</sup> H	4	54 810.94				
		6	54 866.57				
		5	54 929.72				
3d <sup>2</sup> ( <sup>2</sup> D)4s4p( <sup>3</sup> P)	<i>v</i> <sup>3</sup> D	1	54 958.59		33	28	3d <sup>2</sup> ( <sup>1</sup> D)4p <sup>3</sup> D
		2	55 152.69		30	26	
		3	55 451.64		30	19	
3d <sup>2</sup> ( <sup>2</sup> I)4p	<i>z</i> <sup>3</sup> K	7	54 970.22		79	10	<sup>3</sup> K

## Cr I—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages		
3d <sup>5</sup> (a <sup>3</sup> D)4p	v <sup>3</sup> F°	2	54 992.93		30	20	3d <sup>5</sup> (a <sup>3</sup> F)4p <sup>3</sup> F°
		3	55 102.87		22	15	
		4	55 207.40		30	18	
3d <sup>5</sup> ( <sup>4</sup> G)5p	u <sup>3</sup> F°	4	55 120.77				
		3	55 252.72				
		2	55 473.67				
3d <sup>5</sup> ( <sup>3</sup> I)4p		6	55 516.69		35	28	3d <sup>5</sup> ( <sup>1</sup> I)4s4p( <sup>3</sup> P°) <sup>3</sup> H°
3d <sup>5</sup> ( <sup>3</sup> I)4p	x <sup>3</sup> I°	5	55 636.46		29	30	3d <sup>5</sup> ( <sup>1</sup> I)4s4p( <sup>3</sup> P°) <sup>3</sup> I°
		6	55 741.11		34	30	
		7	55 799.10		30	32	
3d <sup>5</sup> ( <sup>1</sup> I)4s4p( <sup>3</sup> P°)	u <sup>3</sup> H°	5	55 874.98		61	12	3d <sup>5</sup> ( <sup>3</sup> H)4p <sup>3</sup> H°
		4	55 915.50		67	—	3d <sup>5</sup> ( <sup>3</sup> H)4p <sup>3</sup> H°
3d <sup>5</sup> ( <sup>1</sup> I)4s4p( <sup>3</sup> P°)		6	55 908.12		37	37	3d <sup>5</sup> ( <sup>3</sup> I)4p <sup>1</sup> I°
3d <sup>5</sup> ( <sup>3</sup> I)4p	y <sup>1</sup> H°	5	55 945.08		43	12	3d <sup>5</sup> ( <sup>3</sup> G)4s4p( <sup>3</sup> P°) <sup>1</sup> H°
3d <sup>5</sup> ( <sup>4</sup> F)4p	v <sup>3</sup> G°	2	56 155.12		46	44	3d <sup>5</sup> ( <sup>4</sup> F)4s <sup>2</sup> 4p <sup>5</sup> G°
		3	56 209.81		47	38	
		4	56 279.56		51	40	
		5	56 361.86		55	28	
		6	56 449.10		50	34	
3d <sup>5</sup> ( <sup>3</sup> D)4s4p( <sup>3</sup> P°)	v <sup>3</sup> P°	2	56 591.88		42	18	3d <sup>5</sup> (a <sup>3</sup> D)4p <sup>3</sup> P°
		1	56 722.60		40	10	3d <sup>5</sup> ( <sup>3</sup> D)4s4p( <sup>3</sup> P°) <sup>1</sup> P°
		0	56 802.50		56	19	3d <sup>5</sup> (a <sup>3</sup> D)4p <sup>3</sup> P°
3d <sup>5</sup> (a <sup>3</sup> F)4s4p( <sup>1</sup> P°)		3	56 985.67		21	16	3d <sup>5</sup> ( <sup>3</sup> D)4s4p( <sup>3</sup> P°) <sup>3</sup> F°
3d <sup>5</sup> (a <sup>3</sup> F)4s4p( <sup>1</sup> P°)	u <sup>3</sup> G°	4	57 033.60		24	15	3d <sup>5</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°) <sup>3</sup> G°
		5	57 088.25		25	23	3d <sup>5</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P°) <sup>3</sup> G°
3d <sup>5</sup> (a <sup>1</sup> S)4s4p( <sup>3</sup> P°)	u <sup>3</sup> P°	2	57 087.70		43	22	3d <sup>5</sup> (a <sup>3</sup> D)4p <sup>3</sup> P°
		1	57 132.59		40	21	
		0	57 154.59		40	22	
	p <sup>3</sup> F°	1	57 096.62				
		2	57 100.66				
		3	57 186.60				
		4	57 237.50				
		5	57 327.66				
		3	57 141.85				
3d <sup>5</sup> ( <sup>3</sup> D)4s4p( <sup>3</sup> P°)		2	57 220.67		24	14	3d <sup>5</sup> ( <sup>4</sup> F)4s <sup>2</sup> 4p <sup>3</sup> P°
3d <sup>5</sup> ( <sup>4</sup> F)4p		3	57 276.42		10	10	3d <sup>5</sup> ( <sup>4</sup> F)4s <sup>2</sup> 4p <sup>3</sup> P°
3d <sup>5</sup> ( <sup>4</sup> F)4p		4	57 335.47		16	12	3d <sup>5</sup> ( <sup>4</sup> F)4s <sup>2</sup> 4p <sup>3</sup> P°
3d <sup>5</sup> ( <sup>4</sup> G)5s	e <sup>4</sup> G	2	57 350.65				
		3	57 261.24				
		4	57 372.78				
		5	57 382.93				
		6	57 389.32				

## Cr I—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages			
3d <sup>5</sup> (a <sup>2</sup> F)4p	t <sup>3</sup> G°	3	57 557.65		40	14	3d <sup>5</sup> ( <sup>4</sup> F)4p <sup>3</sup> F°	
		5	57 702.96		58	20	3d <sup>5</sup> (a <sup>2</sup> F)4s4p( <sup>3</sup> P°) <sup>3</sup> G°	
3d <sup>5</sup> (a <sup>2</sup> F)4p		4	57 587.96		21	<sup>3</sup> G°	18	3d <sup>5</sup> ( <sup>4</sup> F)4p <sup>3</sup> F°
3d <sup>4</sup> 4s5p	r <sup>3</sup> D°	0	57 958.42					
		1	57 995.04					
		2	58 063.80					
		3	58 147.76					
		4	58 292.62					
	e <sup>3</sup> G	3	57 984.94					
		5	57 990.23					
		4	57 992.15					
3d <sup>5</sup> (a <sup>2</sup> F)4p	s <sup>3</sup> F°	2	58 162.84		26	15	3d <sup>5</sup> (a <sup>2</sup> D)4p <sup>3</sup> F°	
		4	58 167.89		25	20		
		3	58 202.65		25	23		
3d <sup>5</sup> ( <sup>4</sup> F)4p		1	58 725.28		33	<sup>3</sup> D°	18	3d <sup>5</sup> ( <sup>4</sup> F)4p <sup>3</sup> D°
3d <sup>5</sup> ( <sup>2</sup> H)4p	t <sup>3</sup> H°	4	58 728.29		23	16	3d <sup>5</sup> ( <sup>2</sup> H)4p <sup>3</sup> H°	
		5	58 754.58		24	17		
		6	58 775.96		26	17		
3d <sup>5</sup> ( <sup>4</sup> P)5p	t <sup>3</sup> D°	2	58 772.03					
		1	58 870.90					
		3	58 924.12					
3d <sup>5</sup> ( <sup>4</sup> F)4p	u <sup>3</sup> D°	2	58 800.23		29	28	3d <sup>5</sup> ( <sup>3</sup> D)4s4p( <sup>3</sup> P°) <sup>3</sup> D°	
		3	59 122.15		22	25	3d <sup>5</sup> ( <sup>3</sup> D)4s4p( <sup>3</sup> P°) <sup>3</sup> D°	
3d <sup>4</sup> 4s( <sup>4</sup> D)6p	<sup>1</sup> F°	2	59 290					
		3	59 310					
		4	59 443					
3d <sup>4</sup> 4s( <sup>4</sup> D)6p	<sup>1</sup> P°	2	59 290					
		3	59 442					
		4	59 659					
3d <sup>5</sup> (a <sup>2</sup> F)4s4p( <sup>1</sup> P°)	r <sup>3</sup> F°	2	59 357.90		51	11	3d <sup>5</sup> ( <sup>4</sup> F)4p <sup>3</sup> F°	
		3	59 417.01		46	9		
		4	59 487.71		60	9		
3d <sup>4</sup> 4s( <sup>4</sup> D)6p	<sup>1</sup> D°	2	59 487					
		3	59 662					
		4	59 877					
3d <sup>5</sup> ( <sup>2</sup> H)4s4p( <sup>1</sup> P°)	u <sup>3</sup> T°	5	59 808.27		64	16	3d <sup>5</sup> ( <sup>2</sup> H)4p <sup>3</sup> T°	
		6	59 884.27		74	13		
		7	59 957.46		77	13		
3d <sup>4</sup> 4s( <sup>4</sup> D)6p	<sup>3</sup> P°	2	59 946					
		3	60 197					
3d <sup>5</sup> (a <sup>2</sup> G)4p		5	60 006.00		20	<sup>3</sup> G°	13	3d <sup>5</sup> ( <sup>2</sup> H)4p <sup>1</sup> H°
3d <sup>5</sup> (a <sup>2</sup> P)4s4p( <sup>1</sup> P°)	x <sup>3</sup> S°	1	60 084.00		48	19	<sup>3</sup> P°	

## Cr I—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	<i>g</i>	Leading percentages						
	$q^3D^{\circ}$	0	60 238.04								
		1	60 286.59								
		2	60 372.86								
		3	60 491.22								
		4	60 625.65								
	$q^3F^{\circ}$	2	60 253.00								
		3	60 326.04								
		4	60 367.38								
	$3d^6(^2H)4p$	$r^3T^{\circ}$	5					60 427.63	50	16	$3d^6(a^2G)4p^1H^{\circ}$
			6					60 527.55	74	11	$3d^6(a^2G)4p^2H^{\circ}$
7			60 656.97	85	6	$3d^6(^2I)4p^2T^{\circ}$					
$3d^6(^2H)4p$	$x^1T^{\circ}$	6	60 441.42	49	17	$3d^6(a^2G)4p^2H^{\circ}$					
$3d^6(a^2G)4p$		5	60 467.85	30	$^3G^{\circ}$ 21	$3d^6(^2H)4p^2T^{\circ}$					
$3d^6(a^2G)4p$	$s^2G^{\circ}$	4	60 502.94	40	9	$3d^6(^2H)4p^2G^{\circ}$					
$3d^6(a^2G)4p$		3	60 518.16	32	$^3G^{\circ}$ 16	$3d^6(a^2F)4p^1F^{\circ}$					
$3d^6(^2F)4p$		3	60 615.84	24	$^3D^{\circ}$ 17	$3d^6(a^2D)4p^2D^{\circ}$					
$3d^6(a^2D)4p$	$s^2D^{\circ}$	2	60 629.87	25	24	$3d^6(a^1D)4s4p(^2P^{\circ})^2D^{\circ}$					
		1	60 678.12	29	2	$3d^6(a^1D)4s4p(^2P^{\circ})^2D^{\circ}$					
	$o^3F^{\circ}$	1	60 678.53								
		2	60 777.85								
		3	60 902.33								
		4	61 052.53								
		5	61 192.98								
$3d^6(b^2F)4p$	$p^2F^{\circ}$	3	60 819.50	40	21	$3d^6(^1F)4s4p(^2P^{\circ})^2F^{\circ}$					
		4	60 960.58	39	24						
$3d^6(a^2G)4p$	$s^2H^{\circ}$	4	60 870.63	52	13	$3d^6(^2H)4s4p(^1P^{\circ})^2H^{\circ}$					
		5	61 008.07	41	11	$3d^6(^2H)4s4p(^1P^{\circ})^2H^{\circ}$					
	$r^2P^{\circ}$	1	61 065.96								
		2	61 107.95								
		3	61 198.68								
$3d^6(^2H)4p$	$r^2G^{\circ}$	3	61 078.28	24	19	$3d^6(b^2F)4p^2G^{\circ}$					
		4	61 122.20	19	15	$3d^6(b^2F)4p^2G^{\circ}$					
$3d^6(^2H)4p$		5	61 161.35	15	$^3G^{\circ}$ 15	$3d^6(a^2G)4p^2H^{\circ}$					
$3d^6(a^2G)4p$		6	61 191.64	25	$^2H^{\circ}$ 27	$3d^6(^2H)4p^1T^{\circ}$					
$3d^6(a^1D)4s4p(^2P^{\circ})$	$t^2P^{\circ}$	0	61 387.86	77	7	$3d^6(a^2D)4p^2P^{\circ}$					
		1	61 527.34	66	8	$3d^6(a^2D)4p^2P^{\circ}$					
		2	61 675.72	58	8	$3d^6(^2F)4s^24p^2P^{\circ}$					
$3d^4 4s5s$	$e^2P$	1	61 558.17								
		2	61 687.56								
		3	61 850.17								

## Cr I—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	<i>g</i>	Leading percentages		
$3d^5(^6F)4p$	$q^3G^o$	3	61 390.05		48	15	$3d^5(^4G)4s4p(^1P^o)^3G^o$
$3d^5(^6F)4p$		4	61 976.50		22	20	$3d^5(^6F)4s^24p^3F^o$
$3d^5 4p^2$	$f^3F$	3	62 034.44				
		4	62 188.83				
		5	62 472.80				
		6	62 658.38				
$3d^5(^6F)4p$		5	62 037.60		21	15	$3d^5(^3G)4s4p(^1P^o)^3H^o$
$3d^5(^4G)4d$	$f^4G$	2	62 646.60				
		3	62 661.96				
		4	62 671.00				
		6	62 673.92				
		5	62 690.96				
$3d^5 4s4p$	$r^3H^o$	4	62 762.06				
		5	62 830.26				
		6	62 903.03				
	$q^3H^o$	4	63 116.80				
		5	63 144.26				
		6	63 182.24				
$3d^5 4p$	$p^3H^o$	4	63 241.81				
		5	63 227.27				
		6	63 227.26				
$3d^5 4s5s$	$e^3H$	3	64 712.04				
		4	64 751.42				
		5	64 802.08				
		6	64 826.20				
		7	64 940.28				
$3d^5 4p$	$p^3G^o$	3	66 008.25				
		4	66 024.06				
		5	66 180.24				
$3p^3 3d^5 4s^2$	$^3P^o$	4	311 290				
		3	314 290				
		2	316 890				



## Cr II

Z = 24

VI isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^4 {}^5S_{3/2}$ Ionization energy =  $132\,966 \pm 10 \text{ cm}^{-1}$  ( $16.4858 \pm 0.0010 \text{ eV}$ )

Kiess (1951) carried out the principal analysis of this spectrum using his extensive measurements of wavelengths and Zeeman-effect data. Changes in several of his term designations for the  $3d^4p$  configuration suggested by Roth (1969) on the basis of theoretical calculations have been adopted here.

Johansson (1983) has reobserved the spectrum, extending the observations into the infrared. All the previously known level values were redetermined, and the new configurations  $3d^4s4p$ ,  $3d^4f$ ,  $5p$ ,  $5d$ ,  $5f$ ,  $5g$ ,  $6s$ ,  $6p$ ,  $6d$ ,  $6g$ , and  $7s$  as well as a few levels of  $3d^4s$  and  $9s$  were found. In addition, new levels of  $3d^4s$ ,  $4p$ , and  $5s$  were added. Altogether 450 new levels were reported. The level value determinations are still in a preliminary stage. The results are given here with an uncertainty of  $\pm 0.05 \text{ cm}^{-1}$ .

From the 6-member  $3d^4({}^4D)ns$   ${}^4D_{n,2}$  series, Johansson (1983) determined a new value for the ionization energy.

The percentage compositions for  $3d^4p$  are by Roth. Repeating terms of the  $3d^4$  core are labeled in alphabetical order rather than by seniority. Shadmi, Oreg. and Stein (1968) have calculated the  $3d^3$ ,  $3d^4s$ , and  $3d^4s^2$  configurations but give percentages only for  $a^2H$  and  $b^2H$ , apparently the only highly mixed terms. No changes of designations were made except for the  $e^2G$  and  $e^2D$  terms. The percentages represent the sum of seniority states contributing the same core term.

## References

- Johansson, S. (1983), private communication.  
 Kiess, C. C. (1951), *J. Res. Natl. Bur. Stand. (U.S.)* 47, 385.  
 Roth, C. (1969), *J. Res. Natl. Bur. Stand. (U.S.)* 73A, 125.  
 Russell, H. N. (1950), *J. Opt. Soc. Am.* 40, 615.  
 Shadmi, Y., Oreg., J., and Stein, J. (1968), *J. Opt. Soc. Am.* 58, 909.

## Cr II

Configuration	Term	J	Level (cm <sup>-1</sup> )	g	Leading percentages
$3d^4$	$a {}^4S$	$\frac{5}{2}$	0.00		
$3d^4({}^4D)4s$	$a {}^4D$	$\frac{1}{2}$	11 961.81	3.323	
		$\frac{3}{2}$	12 082.58	1.867	
		$\frac{5}{2}$	12 147.82	1.669	
		$\frac{7}{2}$	12 308.86	1.578	
		$\frac{9}{2}$	12 496.44	1.554	
$3d^4({}^4D)4s$	$a {}^4D$	$\frac{1}{2}$	19 528.25	0.000	
		$\frac{3}{2}$	19 631.17	1.192	
		$\frac{5}{2}$	19 797.88	1.370	
		$\frac{7}{2}$	20 024.01	1.427	
$3d^4$	$a {}^4G$	$\frac{5}{2}$	20 512.06	0.599	
		$1\frac{1}{2}$	20 512.10	1.278	
		$\frac{7}{2}$	20 517.83	0.994	
		$\frac{9}{2}$	20 519.33	1.161	
$3d^4$	$a {}^4P$	$\frac{5}{2}$	21 822.52	1.590	
		$\frac{1}{2}$	21 823.84	2.693	
		$\frac{3}{2}$	21 824.11	1.717	
$3d^4$	$b {}^4D$	$\frac{7}{2}$	25 033.70	1.432	
		$\frac{1}{2}$	25 036.40	-0.045	
		$\frac{3}{2}$	25 042.81	1.207	
		$\frac{5}{2}$	25 046.76	1.381	
$3d^4({}^3P)4s$	$b {}^4P$	$\frac{1}{2}$	29 961.88	2.685	
		$\frac{3}{2}$	30 307.44	1.756	
		$\frac{5}{2}$	30 864.46	1.572	

## Cr II—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	f	Transition percentages
3d <sup>5</sup>	d <sup>3</sup> F	1 <sup>1</sup> / <sub>2</sub>	30 142.30		
		1 <sup>3</sup> / <sub>2</sub>	30 149.83		
3d <sup>4</sup> 1 <sup>3</sup> H1 <sub>4s</sub>	d <sup>4</sup> H	1/2	30 156.79	0.667	
		3/2	30 218.81	0.978	
		1 <sup>1</sup> / <sub>2</sub>	30 298.51	1.162	
		1 <sup>3</sup> / <sub>2</sub>	30 391.83	1.234	
		1 <sup>3</sup> / <sub>2</sub>	31 082.94	0.418	
3d <sup>4</sup> 1 <sup>3</sup> F1 <sub>4s</sub>	d <sup>4</sup> F	1/2	31 117.39	1.082	
		3/2	31 168.58	1.246	
		1 <sup>3</sup> / <sub>2</sub>	31 219.35	1.340	
3d <sup>5</sup>	d <sup>3</sup> D	1/2	31 350.90		
		3/2	31 531.24		
3d <sup>5</sup>	d <sup>3</sup> F	1/2	32 355.68		
		3/2	32 603.40		
3d <sup>5</sup>	b <sup>3</sup> F	1/2	32 836.63		
		3/2	32 944.76		
		1 <sup>1</sup> / <sub>2</sub>	32 954.31		
		1 <sup>3</sup> / <sub>2</sub>	32 954.95		
		3/2	33 417.99		
3d <sup>4</sup> 1 <sup>3</sup> G1 <sub>4s</sub>	b <sup>3</sup> G	1/2	33 521.11	0.588	
		1 <sup>1</sup> / <sub>2</sub>	33 618.94	1.024	
		1 <sup>3</sup> / <sub>2</sub>	33 694.15	1.185	
3d <sup>4</sup> 1 <sup>3</sup> H1 <sub>4s</sub>	d <sup>3</sup> H	1 <sup>1</sup> / <sub>2</sub>	34 630.95		62 35 3d <sup>4</sup> 1 <sup>3</sup> H1 <sub>4s</sub> 1 <sup>3</sup> H
		1 <sup>3</sup> / <sub>2</sub>	34 812.95		
3d <sup>4</sup> 1 <sup>3</sup> P1 <sub>4s</sub>	d <sup>3</sup> P	1/2	34 659.32	0.670	
		3/2	35 355.89	1.331	
3d <sup>4</sup> 1 <sup>3</sup> F1 <sub>4s</sub>	b <sup>3</sup> F	1/2	35 569.20	0.876	
		3/2	35 607.50	1.144	
3d <sup>4</sup>	b <sup>3</sup> H	1 <sup>1</sup> / <sub>2</sub>	35 610.35		61 37 3d <sup>4</sup> 1 <sup>3</sup> H1 <sub>4s</sub> 1 <sup>3</sup> H
		1 <sup>3</sup> / <sub>2</sub>	35 707.49		
3d <sup>4</sup>	d <sup>3</sup> G	1/2	36 101.58		
		3/2	36 272.54		
3d <sup>4</sup> 1 <sup>3</sup> D1 <sub>4s</sub>	c <sup>3</sup> D	1/2	36 289.59		
		3/2	36 314.86		
		1 <sup>1</sup> / <sub>2</sub>	36 362.45		
		1 <sup>3</sup> / <sub>2</sub>	36 396.23		
		1 <sup>3</sup> / <sub>2</sub>	36 508.93		
3d <sup>4</sup> 1 <sup>3</sup> G1 <sub>4s</sub>	b <sup>3</sup> G	1/2	36 563.01	0.910	
		3/2	36 824.36	1.100	
3d <sup>4</sup> 1 <sup>3</sup> G1 <sub>4s</sub>	c <sup>3</sup> G	1/2	36 683.75		
		3/2	36 824.36		
3d <sup>4</sup>	c <sup>3</sup> F	1/2	36 742.09		
		1 <sup>1</sup> / <sub>2</sub>	36 877.07		

## Cr II—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	g	Leading percentages		
3d <sup>4</sup> ( <sup>1</sup> )4s	b <sup>3</sup> I	13/2	40 202.12				
		11/2	40 228.33				
3d <sup>4</sup> ( <sup>1</sup> S)4s	a <sup>3</sup> S	1/2	40 415.09				
3d <sup>4</sup> ( <sup>3</sup> D)4s	b <sup>3</sup> D	5/2	42 897.99				
		3/2	42 906.62				
3d <sup>6</sup>	b <sup>3</sup> S	1/2	44 307.09				
3d <sup>4</sup> ( <sup>1</sup> D)4s	c <sup>3</sup> D	3/2	45 669.37				
		5/2	45 730.58				
3d <sup>4</sup> ( <sup>3</sup> D)4p	z <sup>4</sup> F	1/2	46 823.39	-0.689	100		
		3/2	46 905.17	1.124	100		
		5/2	47 040.35	1.314	100		
		7/2	47 227.24	1.378	100		
		9/2	47 464.55	1.416	100		
		11/2	47 751.62		100		
3d <sup>6</sup>	d <sup>3</sup> D	5/2	47 354.44				
		3/2	47 372.53				
3d <sup>4</sup> ( <sup>1</sup> D)4p	z <sup>4</sup> P	3/2	48 398.95	2.382	83		
		5/2	48 491.10	1.875	98		
		7/2	48 632.12	1.710	100		
3d <sup>4</sup> ( <sup>1</sup> D)4p	z <sup>4</sup> P	1/2	48 749.36	2.844	67	31	( <sup>3</sup> D) <sup>4</sup> D
		3/2	49 005.93	1.802	55	42	
		5/2	49 706.33	1.624	71	27	
3d <sup>4</sup> ( <sup>1</sup> D)4p	z <sup>4</sup> D	5/2	49 351.80	1.628	73	26	( <sup>3</sup> D) <sup>4</sup> P
		1/2	49 492.77	3.155	69	31	
		3/2	49 564.60	1.824	58	41	
		7/2	49 645.77	1.577	99		
		9/2	49 838.38	1.570	98		
3d <sup>4</sup> ( <sup>1</sup> F)4s	d <sup>4</sup> F	7/2	50 667.24				
		5/2	50 687.62				
3d <sup>4</sup> ( <sup>1</sup> D)4p	z <sup>4</sup> F	3/2	51 584.15	0.406	97		
		5/2	51 669.48	1.025	97		
		7/2	51 788.88	1.248	96		
		9/2	51 942.70	1.338	96		
3d <sup>6</sup>	d <sup>3</sup> G	7/2	52 297.81				
		9/2	52 321.01				
3d <sup>4</sup> 4s <sup>2</sup>	c <sup>4</sup> F	3/2	53 051.35				
		5/2	53 271.09				
		7/2	53 566.28				
		9/2	53 923.60				
3d <sup>4</sup> ( <sup>1</sup> D)4p	z <sup>4</sup> D	1/2	54 418.02	0.007	98		
		3/2	54 499.52	1.178	98		
		5/2	54 625.62	1.376	98		
		7/2	54 784.48	1.430	98		

## Cr II—Continued

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	g	Leading percentages		
$3d^4(^3P)4s$	$d^4P$	$\frac{3}{2}$	54 867.61				
		$\frac{5}{2}$	54 868.62				
		$\frac{7}{2}$	54 883.54				
		$\frac{9}{2}$	54 887.97				
$3d^4(^3P)4s$	$c^4P$	$\frac{5}{2}$	55 022.10				
		$\frac{7}{2}$	55 398.74				
		$\frac{9}{2}$	55 626.21				
$3d^4(^3P)4s$	$b^4P$	$\frac{3}{2}$	59 130.36				
		$\frac{5}{2}$	59 526.73				
$3d^4(^3P)4s$	$e^4P$	$\frac{1}{2}$	59 570.10				
		$\frac{3}{2}$	59 577.66				
$3d^4(^3G)4s$	$e^4G$	$\frac{3}{2}$	62 688.95				
		$\frac{5}{2}$	62 701.67				
$3d^4(^3H)4p$	$z^4H$	$\frac{1}{2}$	63 690.91	0.680	82	16	$(^3G) ^4H$
		$\frac{3}{2}$	63 706.30	1.030	89	16	
		$\frac{5}{2}$	63 848.74	1.138	89	15	
		$\frac{7}{2}$	64 090.53	1.234	83	13	
$3d^4(a^3P)4p$	$y^4D$	$\frac{1}{2}$	63 801.88	0.000	87	7	$(a^3P) ^4D$
		$\frac{3}{2}$	64 061.73	1.199	86	8	
		$\frac{5}{2}$	64 448.81	1.380	85	10	
		$\frac{7}{2}$	64 924.52	1.411	89	14	
$3d^4(a^3P)4p$	$z^4S$	$\frac{1}{2}$	65 029.43		73	7	$(a^3P) ^4P$
$3d^4(a^3P)4p$	$z^4G$	$\frac{3}{2}$	65 156.56	0.583	79	14	$(^3G) ^4G$
		$\frac{5}{2}$	65 256.88	0.920	79	12	
		$\frac{7}{2}$	65 383.95	1.120	59	10	
		$\frac{9}{2}$	65 709.50	1.265	73	13	
$3d^4(^3H)4p$	$z^4I$	$\frac{3}{2}$	65 217.55		96		
		$\frac{5}{2}$	65 419.56		96		
		$\frac{7}{2}$	65 617.99		96		
		$\frac{9}{2}$	65 912.56		100		
$3d^4(^3H)4p$	$z^4G$	$\frac{1}{2}$	65 542.93		49	29	$(a^3P) ^4G$
		$\frac{3}{2}$	65 670.08		41	31	
$3d^4 4s^2$	$d^4P$	$\frac{1}{2}$	66 882.58				
		$\frac{3}{2}$	66 010.29				
		$\frac{5}{2}$	66 256.75				
$3d^4(a^3P)4p$	$y^4P$	$\frac{1}{2}$	66 258.47	2.545	76	13	$(a^3P) ^4S$
		$\frac{3}{2}$	66 354.83	1.671	99		
		$\frac{5}{2}$	66 726.81	1.502	92		
$3d^4(a^3P)4p$	$z^4P$	$\frac{3}{2}$	66 649.38		53	15	$(a^3P) ^4D$
		$\frac{5}{2}$	66 871.93		79	14	$(a^3P) ^4S$
$3d^4(a^3P)4p$	$y^4P$	$\frac{3}{2}$	67 012.10		71	13	$(a^3P) ^4D$
		$\frac{5}{2}$	67 070.45		51	21	$(a^3P) ^4P$
		$\frac{7}{2}$	67 393.51		76	10	$(^3H) ^4G$
		$\frac{9}{2}$	67 448.57		63	16	$(^3H) ^4G$

## Cr II—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	g	Leading percentages		
3d <sup>4</sup> 1H14p	y <sup>4</sup> G°	7/2	67 332.83	1.978	69	18	(a <sup>3</sup> F) <sup>4</sup> F°
		5/2	67 344.03		66	13	(a <sup>3</sup> F) <sup>4</sup> G°
		3/2	67 352.29		51	32	(a <sup>3</sup> F) <sup>4</sup> F°
		11/2	67 369.14		65	22	(a <sup>3</sup> F) <sup>4</sup> G°
3d <sup>4</sup> a <sup>3</sup> F14p	z <sup>3</sup> D°	3/2	67 379.17		28	32	(a <sup>3</sup> F) <sup>4</sup> F°
		5/2	67 387.16		59	19	
3d <sup>4</sup> 1H14p	z <sup>3</sup> T°	11/2	67 506.13		98		
		13/2	67 588.90		95		
3d <sup>4</sup> a <sup>3</sup> F14p	z <sup>3</sup> D°	1/2	67 859.61		88	11	(a <sup>3</sup> P) <sup>4</sup> D°
		3/2	67 867.82		77	13	
		5/2	67 870.24		84	12	
		7/2	67 875.42		89	19	
3d <sup>4</sup> a <sup>1</sup> P14p	z <sup>4</sup> S°	3/2	68 305.64	70	17	(a <sup>3</sup> P) <sup>2</sup> P°	
3d <sup>4</sup> 1H14p	z <sup>2</sup> H°	3/2	68 476.92	81	12	(a <sup>1</sup> G) <sup>2</sup> H°	
		11/2	68 737.82	84	10		
3d <sup>4</sup> a <sup>3</sup> F14p	z <sup>2</sup> P°	3/2	68 582.24	58	21	( <sup>3</sup> G) <sup>2</sup> F°	
		5/2	68 759.89	59	18		
3d <sup>4</sup> 1G14p	y <sup>4</sup> H°	1/2	68 842.30	83	16	( <sup>2</sup> H) <sup>4</sup> H°	
		3/2	68 992.10	82	14		
		11/2	69 170.29	82	13		
		13/2	69 388.25	85	13		
3d <sup>4</sup> a <sup>1</sup> P14p	2D°	3/2	69 248.18	65	28	(a <sup>3</sup> P) <sup>2</sup> D°	
		5/2	69 354.09	66	20		
3d <sup>4</sup> 1G14p	1F°	3/2	69 477.95	71	11	( <sup>2</sup> D) <sup>4</sup> F°	
		5/2	69 498.23	69	13	(a <sup>3</sup> F) <sup>2</sup> G°	
		7/2	69 506.08	69	11	(a <sup>3</sup> F) <sup>2</sup> G°	
		9/2	69 628.63	81	13	( <sup>2</sup> D) <sup>4</sup> F°	
3d <sup>4</sup> a <sup>1</sup> F14p	y <sup>2</sup> G°	1/2	69 902.55	42	25	( <sup>2</sup> H) <sup>2</sup> G°	
		3/2	70 107.67	37	25		
3d <sup>4</sup> 1G14p	z <sup>4</sup> G°	3/2	70 316.90	69	17	( <sup>2</sup> H) <sup>4</sup> G°	
		5/2	70 427.05	61	19	( <sup>2</sup> H) <sup>4</sup> G°	
		7/2	70 679.15	44	22	( <sup>2</sup> G) <sup>2</sup> H°	
		11/2	70 879.80	41	28	( <sup>2</sup> G) <sup>2</sup> H°	
3d <sup>4</sup> 1G14p	y <sup>2</sup> H°	3/2	70 394.90	67	19	( <sup>2</sup> G) <sup>4</sup> G°	
		11/2	70 398.87	47	34		
3d <sup>4</sup> 1G14p	y <sup>2</sup> P°	3/2	70 584.47	45	32	(a <sup>3</sup> F) <sup>2</sup> F°	
		5/2	70 852.23	59	20		
3d <sup>4</sup> 1G14p	z <sup>2</sup> G°	1/2	72 648.52	79	11	( <sup>2</sup> H) <sup>2</sup> G°	
		3/2	72 716.72	75	13		
3d <sup>4</sup> 1D14p	w <sup>4</sup> D°	1/2	73 407.00	96			
		3/2	73 411.96	91			
		5/2	73 436.17	87			
		7/2	73 485.66	89			

## Cr II—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	g	Leading percentages		
3d <sup>4</sup> (e <sup>1</sup> G)4p	x <sup>2</sup> F <sup>o</sup>	1/2	74 114.39		64	19	( <sup>3</sup> G) <sup>2</sup> F <sup>o</sup>
		3/2	74 436.15		77	7	( <sup>3</sup> D) <sup>2</sup> F <sup>o</sup>
3d <sup>4</sup> ( <sup>3</sup> D)4p	u <sup>2</sup> F <sup>o</sup>	3/2	74 273.31		82	13	( <sup>3</sup> G) <sup>2</sup> F <sup>o</sup>
		5/2	74 318.83		88	8	( <sup>3</sup> D) <sup>2</sup> F <sup>o</sup>
		7/2	74 423.67		88	6	( <sup>3</sup> D) <sup>2</sup> F <sup>o</sup>
		9/2	74 504.17		86	13	( <sup>3</sup> G) <sup>2</sup> F <sup>o</sup>
3d <sup>4</sup> ( <sup>1</sup> I)4p	T <sup>o</sup>	11/2	74 421.80		85	12	(e <sup>1</sup> G) <sup>2</sup> H <sup>o</sup>
		13/2	74 743.23		64	35	( <sup>1</sup> I) <sup>2</sup> K <sup>o</sup>
3d <sup>4</sup> ( <sup>1</sup> I)4p	<sup>2</sup> K <sup>o</sup>	13/2	74 424.19		65	33	( <sup>1</sup> I) T <sup>o</sup>
		15/2	74 958.80		100		
3d <sup>4</sup> (e <sup>1</sup> G)4p	x <sup>2</sup> H <sup>o</sup>	9/2	74 455.82		82	11	( <sup>3</sup> H) <sup>2</sup> H <sup>o</sup>
		11/2	74 707.48		72	11	( <sup>1</sup> I) T <sup>o</sup>
3d <sup>4</sup> ( <sup>3</sup> D)4p	x <sup>2</sup> P <sup>o</sup>	5/2	74 483.96		53	39	( <sup>3</sup> D) <sup>2</sup> F <sup>o</sup>
		3/2	74 717.59		88		
		1/2	74 920.44		96		
3d <sup>4</sup> ( <sup>3</sup> D)4p	y <sup>2</sup> P <sup>o</sup>	1/2	74 853.85		56	40	(e <sup>1</sup> S) <sup>2</sup> P <sup>o</sup>
		3/2	74 984.78		61	33	
3d <sup>4</sup> (e <sup>1</sup> G)4p	u <sup>2</sup> G <sup>o</sup>	7/2	75 716.55		82	8	( <sup>3</sup> G) <sup>2</sup> G <sup>o</sup>
		9/2	75 810.04		88	12	
3d <sup>4</sup> ( <sup>3</sup> D)4p	u <sup>2</sup> F <sup>o</sup>	7/2	76 879.02		73	12	(e <sup>1</sup> G) <sup>2</sup> F <sup>o</sup>
		9/2	76 987.70		72	13	
3d <sup>4</sup> ( <sup>1</sup> I)4p	u <sup>2</sup> H <sup>o</sup>	11/2	77 078.92		88	8	( <sup>3</sup> G) <sup>2</sup> H <sup>o</sup>
		9/2	77 270.25		91	8	
3d <sup>4</sup> (e <sup>1</sup> S)4p	x <sup>2</sup> P <sup>o</sup>	3/2	77 713.28		31	36	( <sup>3</sup> D) <sup>2</sup> D <sup>o</sup>
		1/2	77 777.23		48	32	( <sup>3</sup> D) <sup>2</sup> F <sup>o</sup>
3d <sup>4</sup> ( <sup>3</sup> D)4p	x <sup>2</sup> D <sup>o</sup>	3/2	77 935.15		65	26	(e <sup>1</sup> D) <sup>2</sup> D <sup>o</sup>
		5/2	78 100.56		68	22	(e <sup>1</sup> S) <sup>2</sup> F <sup>o</sup>
3d <sup>4</sup> (e <sup>1</sup> D)4p	u <sup>2</sup> D <sup>o</sup>	3/2	80 223.05		74	13	( <sup>3</sup> D) <sup>2</sup> D <sup>o</sup>
		5/2	80 430.20		68	21	
3d <sup>4</sup> (e <sup>1</sup> D)4p	v <sup>2</sup> F <sup>o</sup>	3/2	81 232.92		88		
		1/2	81 432.29		88		
3d <sup>4</sup> ( <sup>7</sup> F)4e4p( <sup>3</sup> P <sup>o</sup> )	y <sup>2</sup> D <sup>o</sup>	1/2	81 849.19				
		3/2	81 737.87				
		5/2	81 816.29				
		7/2	81 973.08				
		9/2	82 192.59				
3d <sup>4</sup> ( <sup>7</sup> F)4e4p( <sup>3</sup> P <sup>o</sup> )	y <sup>2</sup> F <sup>o</sup>	1/2	81 735.08				
		3/2	81 824.40				
		5/2	81 902.29				
		7/2	82 143.15				
		9/2	82 202.19				
		11/2	82 612.69				

## Cr II—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages		
3d <sup>4</sup> ( <sup>3</sup> D)5s	e <sup>4</sup> D	1/2	82 632.86				
		3/2	82 763.75				
		5/2	82 881.17				
		7/2	83 041.38				
		9/2	83 240.41				
3d <sup>4</sup> (a <sup>1</sup> D)4p	u <sup>3</sup> P <sup>o</sup>	1/2	82 852.85		89 78	9 11	( <sup>3</sup> D) <sup>3</sup> P <sup>o</sup>
		3/2	82 919.90				
3d <sup>4</sup> ( <sup>3</sup> D)5s	e <sup>4</sup> D	1/2	84 209.88				
		3/2	84 320.21				
		5/2	84 435.70				
		7/2	84 726.71				
3d <sup>4</sup> ( <sup>1</sup> F)4p	u <sup>3</sup> P <sup>o</sup>	1/2	84 606.84		89 87		
		3/2	84 677.13				
3d <sup>4</sup> ( <sup>4</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	u <sup>4</sup> D <sup>o</sup>	1/2	85 486.24				
		3/2	85 586.69				
		5/2	85 778.69				
		7/2	86 072.90				
3d <sup>4</sup> ( <sup>1</sup> F)4p	o <sup>3</sup> G <sup>o</sup>	1/2	85 572.17		86 97		
		3/2	85 938.96				
3d <sup>4</sup> ( <sup>3</sup> D)4d	e <sup>4</sup> S	3/2	86 165.30				
3d <sup>4</sup> ( <sup>1</sup> F)4p	o <sup>3</sup> D <sup>o</sup>	1/2	86 507.31		75 79	13 12	(b <sup>3</sup> P) <sup>3</sup> D <sup>o</sup>
		3/2	86 919.01				
3d <sup>4</sup> ( <sup>4</sup> F)4s4p( <sup>3</sup> P <sup>o</sup> )	u <sup>4</sup> G <sup>o</sup>	1/2	86 586.55				
		3/2	86 797.35				
		5/2	87 092.65				
		11/2	87 450.17				
3d <sup>4</sup> ( <sup>3</sup> D)4d	e <sup>4</sup> G	3/2	86 594.23				
		5/2	86 654.18				
		7/2	86 738.27				
		9/2	86 847.03				
		11/2	86 980.10				
		13/2	87 137.08				
3d <sup>4</sup> ( <sup>3</sup> D)4d	e <sup>4</sup> P	3/2	86 667.73				
		5/2	86 691.55				
		7/2	86 782.04				
3d <sup>4</sup> ( <sup>3</sup> D)4d	f <sup>4</sup> D	1/2	87 453.50				
		3/2	87 470.58				
		5/2	87 514.82				
		7/2	87 588.00				
		9/2	87 687.52				
3d <sup>4</sup> ( <sup>3</sup> D)4d	e <sup>4</sup> P	1/2	87 594.58				
		3/2	87 666.26				
		5/2	87 759.02				
		7/2	87 858.56				
		9/2	87 948.55				
		11/2	88 001.36				

## Cr II—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	<i>f</i>	Leading percentages	
3d <sup>3</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P)	a <sup>3</sup> F	$\frac{3}{2}$	87 622.74			
		$\frac{5}{2}$	87 766.61			
		$\frac{1}{2}$	87 916.67			
		$\frac{3}{2}$	88 073.49			
3d <sup>3</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P)	a <sup>3</sup> D	$\frac{3}{2}$	88 604.24			
		$\frac{5}{2}$	89 164.64			
3d <sup>3</sup> ( <sup>3</sup> D)4d	c <sup>3</sup> P	$\frac{1}{2}$	89 254.56			
		$\frac{3}{2}$	89 277.95			
		$\frac{5}{2}$	89 336.89			
3d <sup>3</sup> ( <sup>3</sup> D)4d	c <sup>3</sup> G	$\frac{3}{2}$	89 656.02			
		$\frac{1}{2}$	89 174.08			
		$\frac{5}{2}$	89 325.32			
		$1\frac{1}{2}$	89 508.55			
3d <sup>3</sup> ( <sup>3</sup> P)4p	y <sup>3</sup> P	$\frac{3}{2}$	89 422.95		88	6 (b <sup>3</sup> P) <sup>3</sup> D
		$\frac{5}{2}$	89 453.21		82	7
		$\frac{1}{2}$	89 507.94		96	
3d <sup>3</sup> ( <sup>3</sup> D)4d	f <sup>3</sup> D	$\frac{1}{2}$	89 651.66			
		$\frac{3}{2}$	89 724.27			
		$\frac{5}{2}$	89 812.42			
		$\frac{7}{2}$	89 885.08			
3d <sup>3</sup> ( <sup>3</sup> P)4p	v <sup>3</sup> D	$\frac{1}{2}$	90 218.49		89	25 (b <sup>3</sup> P) <sup>3</sup> D
		$\frac{3}{2}$	90 258.90		51	20
		$\frac{5}{2}$	90 450.63		61	24
		$\frac{7}{2}$	90 475.48		70	25
3d <sup>3</sup> ( <sup>3</sup> P)4p	v <sup>3</sup> F	$\frac{3}{2}$	90 262.13		97	
		$\frac{5}{2}$	90 441.78		98	
		$\frac{1}{2}$	90 489.86		95	
		$\frac{7}{2}$	90 588.59		98	
3d <sup>3</sup> ( <sup>3</sup> D)4d	c <sup>3</sup> F	$\frac{3}{2}$	90 512.56			
		$\frac{5}{2}$	90 608.99			
		$\frac{1}{2}$	90 725.87			
		$\frac{7}{2}$	90 850.96			
3d <sup>3</sup> ( <sup>3</sup> P)4p	i <sup>3</sup> F	$\frac{3}{2}$	90 706.82		95	5 (b <sup>3</sup> P) <sup>3</sup> G
		$\frac{5}{2}$	90 830.79		97	5 (b <sup>3</sup> G) <sup>3</sup> F
3d <sup>3</sup> ( <sup>3</sup> P)4p	w <sup>3</sup> G	$\frac{3}{2}$	91 073.72			
		$\frac{1}{2}$	91 122.82		95	
		$\frac{5}{2}$	91 189.51		98	
		$1\frac{1}{2}$	91 292.16			
3d <sup>3</sup> ( <sup>3</sup> P)4p	i <sup>3</sup> D	$\frac{3}{2}$	91 428.06		89	18 (f <sup>3</sup> P) <sup>3</sup> D
		$\frac{5}{2}$	91 556.40		88	21 (b <sup>3</sup> P) <sup>3</sup> D
3d <sup>3</sup> ( <sup>3</sup> F)4s4p( <sup>3</sup> P)	i <sup>3</sup> G	$\frac{1}{2}$	91 752.27			
		$\frac{3}{2}$	92 144.24			
3d <sup>3</sup> ( <sup>3</sup> D)4d	c <sup>3</sup> S	$\frac{3}{2}$	91 955.30			
3d <sup>3</sup> ( <sup>3</sup> P)4s4p( <sup>3</sup> P)	z <sup>3</sup> P	$\frac{3}{2}$	92 225.25			
		$\frac{5}{2}$	92 417.93			
		$\frac{7}{2}$	92 653.28			



## Cr II—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	Leading percentages		
3d <sup>4</sup> (b <sup>1</sup> P)4p	y <sup>4</sup> S	3/2	92 612.28	97		
3d <sup>4</sup> (D)5p	F	1/2	92 988.83			
		3/2	93 047.31			
		5/2	93 143.88			
		7/2	93 276.86			
		9/2	93 444.17			
		11/2	93 642.40			
3d <sup>4</sup> (b <sup>3</sup> F)4p	i <sup>4</sup> D	1/2	93 531.69	73	27	(b <sup>3</sup> P) <sup>4</sup> D
		3/2	93 671.00	72	72	
		5/2	93 770.10	72	27	
		7/2	93 800.29	72	27	
3d <sup>4</sup> (D)5p	D	3/2	93 574.44			
		5/2	93 776.15			
		7/2	93 966.45			
		9/2	94 177.18			
3d <sup>4</sup> (b <sup>3</sup> F)4p	u <sup>4</sup> G	3/2	93 541.50	98		
		5/2	93 801.46	98		
3d <sup>4</sup> (D)5p	P	3/2	93 740.60			
		5/2	93 974.05			
3d <sup>4</sup> (F)4s4p(1P)	s <sup>4</sup> F	3/2	93 890.64			
		5/2	94 218.66			
3d <sup>4</sup> (P)4s4p(1P)	x <sup>4</sup> D	1/2	93 968.70			
		3/2	94 098.13			
		5/2	94 265.99			
		7/2	94 452.57			
		9/2	94 656.24			
3d <sup>4</sup> (D)5p	P	3/2	94 002.56			
		5/2	94 144.63			
		7/2	94 363.51			
3d <sup>4</sup> (D)5p	P	3/2	94 256.07			
		5/2	94 365.19			
		7/2	94 522.31			
		9/2	94 749.20			
3d <sup>4</sup> (b <sup>3</sup> P)4p	u <sup>4</sup> P	3/2	94 323.20	94		
		5/2	94 624.72	92		
3d <sup>4</sup> (D)5p	D	1/2	94 439.87			
		3/2	94 592.95			
		5/2	95 076.72			
		7/2	95 250.69			
3d <sup>4</sup> (b <sup>3</sup> P)4p	y <sup>4</sup> S	1/2	96 245.92	98		
3d <sup>4</sup> (G)4s4p(3P)	i <sup>4</sup> G	3/2	97 071.15			
		5/2	97 187.28			
		7/2	97 333.28			
		9/2	97 493.70			

## Cr II—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	g	Leading percentages		
3d <sup>4</sup> ( <sup>4</sup> P)4s4p( <sup>4</sup> P°)	w <sup>4</sup> P°	1/2	97 168.48				
		3/2	97 182.54				
		5/2	97 294.06				
3d <sup>4</sup> (b <sup>1</sup> G)4p	v <sup>2</sup> H°	3/2	97 480.08		86	12	(b <sup>1</sup> G) <sup>2</sup> G°
		11/2	97 839.41				
3d <sup>4</sup> (b <sup>1</sup> G)4p	s <sup>2</sup> G°	1/2	97 728.25		97		
		3/2	97 906.44				
3d <sup>4</sup> ( <sup>4</sup> P)4s4p( <sup>2</sup> P°)	z <sup>4</sup> S°	3/2	97 875.00				
3d <sup>4</sup> (b <sup>3</sup> F)4p	s <sup>2</sup> D°	3/2	98 207.96		71	29	(b <sup>3</sup> F) <sup>2</sup> D°
		5/2	98 314.99				
3d <sup>4</sup> ( <sup>2</sup> G)4s4p( <sup>2</sup> P°)	t <sup>4</sup> F°	3/2	98 578.50				
		5/2	98 641.83				
		7/2	98 719.40				
		9/2	98 812.67				
3d <sup>4</sup> (b <sup>1</sup> G)4p	r <sup>2</sup> F°	1/2	99 069.99		87	8	(b <sup>2</sup> F) <sup>2</sup> F°
		3/2	99 243.99				
3d <sup>4</sup> (a <sup>3</sup> P)5s	f <sup>4</sup> P	1/2	99 677.93				
		3/2	100 040.22				
		5/2	100 650.52				
3d <sup>4</sup> ( <sup>2</sup> H)5s	e <sup>4</sup> H	1/2	100 068.86				
		3/2	100 135.82				
		11/2	100 221.64				
		13/2	100 322.13				
3d <sup>4</sup> ( <sup>2</sup> P)4s4p( <sup>2</sup> P°)	r <sup>4</sup> D°	3/2	100 691.80				
		5/2	101 074.56				
		7/2	101 514.29				
3d <sup>4</sup> (a <sup>3</sup> P)5s	e <sup>2</sup> P	1/2	100 792.80				
		3/2	101 492.84				
3d <sup>4</sup> ( <sup>2</sup> H)5s	e <sup>2</sup> H	3/2	101 021.84				
		11/2	101 194.83				
3d <sup>4</sup> ( <sup>4</sup> P)4s4p( <sup>2</sup> P°)	u <sup>2</sup> P°	3/2	101 157.49				
3d <sup>4</sup> ( <sup>2</sup> H)4s4p( <sup>2</sup> P°)	w <sup>4</sup> H°	1/2	101 170.33				
		3/2	101 296.80				
		11/2	101 783.20				
		13/2	101 900.82				
3d <sup>4</sup> (a <sup>3</sup> F)5s	f <sup>4</sup> F	3/2	101 245.00				
		5/2	101 276.80				
		7/2	101 321.83				
		9/2	101 382.97				
3d <sup>4</sup> ( <sup>2</sup> G)4s4p( <sup>2</sup> P°)	u <sup>2</sup> H°	3/2	101 696.20				
		11/2	101 892.97				
3d <sup>4</sup> ( <sup>2</sup> G)4s4p( <sup>2</sup> P°)	p <sup>2</sup> F°	1/2	101 864.17				
		3/2	102 145.85				

## Cr II—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentage:
3d <sup>3</sup> ( <sup>2</sup> G)4s4p( <sup>3</sup> P°)	<i>r</i> <sup>2</sup> G°	3/2	101 938.04		
		7/2	102 121.92		
3d <sup>3</sup> ( <sup>2</sup> D)4s4p( <sup>3</sup> P°)	<i>s</i> <sup>4</sup> F°	3/2	101 987.19		
		5/2	102 297.15		
		7/2	102 492.60		
		9/2	102 725.66		
3d <sup>3</sup> ( <sup>2</sup> F)5s	<i>f</i> <sup>2</sup> F	5/2	102 148.81		
		7/2	102 243.22		
3d <sup>3</sup> ( <sup>4</sup> P)4s4p( <sup>3</sup> P°)	<i>q</i> <sup>4</sup> D°	3/2	102 602.40		
		5/2	102 619.58		
		7/2	102 655.95		
		7/2	102 831.62		
3d <sup>3</sup> ( <sup>4</sup> F)4s4p( <sup>1</sup> P°)	<i>s</i> <sup>4</sup> G°	5/2	102 679.00		
		7/2	102 915.01		
		9/2	103 199.80		
		11/2	103 513.67		
3d <sup>3</sup> ( <sup>2</sup> P)4s4p( <sup>3</sup> P°)	<i>x</i> <sup>4</sup> S°	3/2	102 684.02		
3d <sup>3</sup> ( <sup>2</sup> G)5s	<i>f</i> <sup>4</sup> G	9/2	103 627.02		
		11/2	103 736.99		
3d <sup>4</sup> 4d	<i>f</i> <sup>4</sup> I	9/2	103 755.48		
		11/2	103 843.33		
		13/2	103 948.26		
		15/2	104 069.62		
3d <sup>4</sup> 4d	<i>f</i> <sup>4</sup> H	7/2	103 949.27		
		9/2	104 023.95		
		11/2	104 106.35		
		13/2	104 190.63		
3d <sup>3</sup> ( <sup>2</sup> D)4s4p( <sup>3</sup> P°)	<i>o</i> <sup>4</sup> D°	3/2	104 274.62		
		5/2	104 467.83		
		7/2	104 680.78		
3d <sup>3</sup> ( <sup>4</sup> F)4s4p( <sup>1</sup> P°)	<i>p</i> <sup>4</sup> D°	1/2	104 439.77		
		3/2	104 616.27		
		5/2	104 869.13		
		7/2	105 206.69		
3d <sup>3</sup> ( <sup>4</sup> F)4s4p( <sup>1</sup> P°)	<i>r</i> <sup>4</sup> F°	3/2	104 446.50		
		5/2	104 630.01		
		7/2	104 875.34		
		9/2	105 203.46		
3d <sup>4</sup> 4d	<i>a</i> <sup>4</sup> K	11/2	104 480.28		
		13/2	104 539.92		
		15/2	104 633.04		
		17/2	104 734.37		
3d <sup>4</sup> 5s	<i>g</i> <sup>2</sup> G	7/2	104 543.17		
		9/2	104 666.42		

## Cr II—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Loading percentages
3d <sup>4</sup> ( <sup>4</sup> D)6s	<sup>4</sup> D	1/2	105 098.94		
		3/2	105 168.82		
		5/2	105 285.87		
		7/2	105 447.05		
		9/2	105 650.58		
3d <sup>4</sup> ( <sup>4</sup> D)4f	<sup>4</sup> F	5/2	105 122.26		
		7/2	105 282.47		
		9/2	105 392.48		
3d <sup>4</sup> 4d	a <sup>2</sup> K	13/2	105 124.90		
		15/2	105 285.23		
3d <sup>4</sup> 4f	<sup>4</sup> F	7/2	105 172.47		
		9/2	105 408.72		
3d <sup>4</sup> ( <sup>4</sup> D)4f	<sup>4</sup> H	7/2	105 197.22		
		9/2	105 262.52		
		11/2	105 367.22		
		13/2	105 508.05		
		15/2	105 681.22		
3d <sup>4</sup> 4d	g <sup>4</sup> H	7/2	105 196.98		
		9/2	105 256.24		
		11/2	105 337.97		
		13/2	105 434.42		
3d <sup>4</sup> ( <sup>4</sup> D)4f	<sup>4</sup> H	7/2	105 222.52		
		9/2	105 406.99		
		11/2	105 559.52		
		13/2	105 742.62		
3d <sup>4</sup> 4d	g <sup>4</sup> G	9/2	105 366.50		
		11/2	105 422.22		
3d <sup>4</sup> ( <sup>4</sup> D)4f	<sup>4</sup> D	9/2	105 392.27		
		7/2	105 420.09		
		5/2	105 525.25		
3d <sup>4</sup> ( <sup>4</sup> D)4f	<sup>4</sup> G	5/2	105 422.22		
		7/2	105 609.67		
		9/2	105 622.64		
		7/2	105 765.04		
		11/2	105 825.59		
		13/2	105 898.12		
3d <sup>4</sup> ( <sup>4</sup> D)4f	<sup>4</sup> D	7/2	105 507.52		
		5/2	105 522.18		
3d <sup>4</sup> ( <sup>4</sup> D)4f	<sup>4</sup> F	7/2	105 577.19		
3d <sup>4</sup> ( <sup>4</sup> D)4f	<sup>4</sup> F	11/2	105 622.24		
		7/2	105 822.86		
		9/2	105 870.42		
3d <sup>4</sup> ( <sup>4</sup> D)4f	<sup>4</sup> G	5/2	105 677.42		
		7/2	105 724.77		
		11/2	106 022.24		
		9/2	106 045.22		

## Cr II—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages
3d <sup>4</sup> ( <sup>1</sup> D)4f	<sup>4</sup> F	$\frac{3}{2}$	105 790.06		
		$\frac{5}{2}$	105 901.05		
		$\frac{7}{2}$	105 985.63		
3d <sup>4</sup> ( <sup>3</sup> D)6s	<sup>4</sup> D	$\frac{1}{2}$	105 923.4		
		$\frac{3}{2}$	106 030.93		
		$\frac{5}{2}$	106 095.64		
		$\frac{7}{2}$	106 275.24		
3d <sup>4</sup> 4d	<i>f</i> <sup>4</sup> I	$\frac{11}{2}$	106 145.26		
		$\frac{13}{2}$	106 342.95		
3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P <sup>o</sup> )	<i>i</i> <sup>3</sup> H	$\frac{11}{2}$	106 163.16		
		$\frac{9}{2}$	106 165.3		
3d <sup>4</sup> ( <sup>3</sup> H)4s4p( <sup>3</sup> P <sup>o</sup> )	<i>r</i> <sup>4</sup> G	$\frac{3}{2}$	106 719.38		
		$\frac{5}{2}$	106 779.14		
		$\frac{7}{2}$	106 791.84		
		$\frac{11}{2}$	106 827.42		
3d <sup>4</sup> ( <sup>1</sup> P)4s4p( <sup>3</sup> P <sup>o</sup> )	<i>w</i> <sup>4</sup> S	$\frac{3}{2}$	106 726.06		
3d <sup>4</sup> ( <sup>1</sup> D)5d	<sup>4</sup> G	$\frac{3}{2}$	106 877.20		
		$\frac{5}{2}$	106 929.42		
		$\frac{7}{2}$	107 006.29		
		$\frac{9}{2}$	107 111.84		
		$\frac{11}{2}$	107 246.87		
		$\frac{13}{2}$	107 412.09		
3d <sup>4</sup> 4d	<i>i</i> <sup>2</sup> G	$\frac{9}{2}$	106 923.98		
3d <sup>4</sup> ( <sup>1</sup> D)5d	<sup>4</sup> S	$\frac{3}{2}$	106 924.84		
3d <sup>4</sup> ( <sup>1</sup> D)4s4p( <sup>3</sup> P <sup>o</sup> )	<i>o</i> <sup>3</sup> P	$\frac{3}{2}$	107 022.83		
		$\frac{1}{2}$	107 153.15		
3d <sup>4</sup> ( <sup>1</sup> D)5d	<sup>6</sup> P	$\frac{3}{2}$	107 025.34		
		$\frac{5}{2}$	107 056.53		
		$\frac{7}{2}$	107 114.75		
3d <sup>4</sup> ( <sup>1</sup> P)4s4p( <sup>3</sup> P <sup>o</sup> )	<i>q</i> <sup>2</sup> D	$\frac{3}{2}$	107 212.29		
		$\frac{5}{2}$	107 355.53		
3d <sup>4</sup> ( <sup>1</sup> D)5d	<sup>6</sup> F	$\frac{3}{2}$	107 259.87		
		$\frac{5}{2}$	107 309.28		
		$\frac{7}{2}$	107 386.22		
		$\frac{9}{2}$	107 455.55		
		$\frac{11}{2}$	107 701.34		
3d <sup>4</sup> ( <sup>1</sup> D)5d	<sup>4</sup> G	$\frac{3}{2}$	107 400.84		
		$\frac{5}{2}$	107 500.37		
		$\frac{7}{2}$	107 632.26		
		$\frac{11}{2}$	107 794.15		
3d <sup>4</sup> ( <sup>1</sup> D)5d	<sup>4</sup> D	$\frac{3}{2}$	107 414.68		
		$\frac{5}{2}$	107 519.44		
		$\frac{7}{2}$	107 627.40		
		$\frac{9}{2}$	107 696.31		

## Cr II—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages
3d <sup>4</sup> ( <sup>3</sup> D)5d	<sup>4</sup> F	3/2	107 516.77		
		5/2	107 726.82		
		7/2	107 850.60		
		9/2	107 948.05		
3d <sup>4</sup> ( <sup>3</sup> D)5d	<sup>4</sup> D	5/2	107 597.65		
		7/2	107 716.30		
3d <sup>4</sup> 4d	<i>g</i> <sup>4</sup> I	9/2	107 706.84		
		11/2	107 760.85		
		13/2	107 846.75		
		15/2	107 981.81		
3d <sup>4</sup> ( <sup>2</sup> H)4s4p( <sup>3</sup> P <sup>o</sup> )	<i>q</i> <sup>2</sup> G <sup>o</sup>	9/2	107 739.20		
		7/2	107 918.49		
3d <sup>4</sup> 4d	<i>h</i> <sup>4</sup> H	7/2	107 829.54		
		9/2	107 922.41		
		11/2	108 017.98		
		13/2	108 104.01		
3d <sup>4</sup> ( <sup>2</sup> H)4s4p( <sup>3</sup> P <sup>o</sup> )	<i>x</i> <sup>2</sup> I <sup>o</sup>	11/2	107 850.50		
		13/2	108 031.16		
3d <sup>4</sup> ( <sup>3</sup> D)5d	<sup>6</sup> S	5/2	109 394.47		
3d <sup>4</sup> ( <sup>3</sup> D)6p	<sup>4</sup> F <sup>o</sup>	1/2	109 564.97		
		3/2	109 611.24		
		5/2	109 694.38		
		7/2	109 812.06		
		9/2	109 965.71		
		11/2	110 154.04		
3d <sup>4</sup> ( <sup>3</sup> D)6p	<sup>4</sup> P <sup>o</sup>	3/2	109 661.41		
		5/2	109 974.05		
3d <sup>4</sup> ( <sup>3</sup> D)6p	<sup>6</sup> P <sup>o</sup>	3/2	109 772.35		
		5/2	109 864.95		
		7/2	110 097.11		
3d <sup>4</sup> ( <sup>2</sup> D)4s4p( <sup>3</sup> P <sup>o</sup> )	<i>p</i> <sup>2</sup> D <sup>o</sup>	3/2	109 914.68		
		5/2	109 943.57		
3d <sup>4</sup> ( <sup>4</sup> D)6p	<sup>4</sup> D <sup>o</sup>	1/2	109 923.45		
		3/2	110 007.57		
		5/2	110 133.26		
		7/2	110 272.15		
		9/2	110 335.80		
3d <sup>4</sup> ( <sup>4</sup> D)6p	<sup>6</sup> P <sup>o</sup>	5/2	110 315.08		
		7/2	110 471.38		
		9/2	110 665.54		
3d <sup>4</sup> ( <sup>4</sup> D)6p	<sup>4</sup> D <sup>o</sup>	3/2	110 331.72		
		5/2	111 082.38		
		7/2	111 289.22		

## Cr II—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> H	5/2	115 208.57		
		9/2	115 288.81		
		7/2	115 309.16		
		11/2	115 396.86		
		13/2	115 546.61		
		15/2	115 734.85		
3d <sup>4</sup> ( <sup>3</sup> D)7s	<sup>4</sup> D	1/2	115 234.53		
		3/2	115 301.92		
		5/2	115 417.88		
		7/2	115 581.62		
		9/2	115 788.38		
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> P	7/2	115 249.31		
		5/2	115 747.63		
		3/2	115 767.13		
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> P	3/2	115 298.53		
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> D	5/2	115 309.64		
		9/2	115 393.47		
		7/2	115 430.93		
		11/2	115 591.20		
3d <sup>4</sup> ( <sup>3</sup> D <sub>0</sub> )5g	<sup>4</sup> [4]	9/2	115 371.26		
		7/2	115 371.39		
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> H	7/2	115 398.46		
		9/2	115 430.45		
		11/2	115 598.97		
		13/2	115 782.87		
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> G	5/2	115 408.13		
		7/2	115 627.76		
		11/2	115 916.22		
		9/2	115 927.40		
3d <sup>4</sup> ( <sup>3</sup> D <sub>1</sub> )5g	<sup>4</sup> [4]	9/2	115 411.98		
		7/2	115 412.17		
3d <sup>4</sup> ( <sup>3</sup> D <sub>1</sub> )5g	<sup>4</sup> [5]	11/2	115 444.00		
		9/2	115 444.02		
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> G	7/2	115 447.64		
		5/2	115 461.80		
		11/2	115 585.21		
		9/2	115 592.43		
		13/2	115 836.61		
3d <sup>4</sup> ( <sup>3</sup> D <sub>2</sub> )5g	<sup>4</sup> [5]	11/2	115 554.95		
		9/2	115 555.05		
3d <sup>4</sup> ( <sup>3</sup> D <sub>2</sub> )5g	<sup>4</sup> [4]	9/2	115 556.30		
		7/2	115 556.44		
3d <sup>4</sup> ( <sup>3</sup> D <sub>2</sub> )5g	<sup>4</sup> [6]	13/2	115 560.97		
		11/2	115 561.07		

## Cr II—Continued

Configuration	Term	J	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> F	<sup>5</sup> / <sub>2</sub>	115 570.91		
		<sup>3</sup> / <sub>2</sub>	115 605.95		
		<sup>1</sup> / <sub>2</sub>	115 797.28		
		<sup>9</sup> / <sub>2</sub>	115 824.49		
		<sup>13</sup> / <sub>2</sub>	115 840.45		
3d <sup>4</sup> ( <sup>3</sup> D)7s	<sup>4</sup> D	<sup>3</sup> / <sub>2</sub>	115 640.42		
		<sup>5</sup> / <sub>2</sub>	115 818.49		
		<sup>7</sup> / <sub>2</sub>	116 047.90		
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> F	<sup>9</sup> / <sub>2</sub>	115 672.84		
		<sup>7</sup> / <sub>2</sub>	115 882.21		
3d <sup>4</sup> ( <sup>3</sup> D <sub>3</sub> )5g	<sup>2</sup> (7)	<sup>13</sup> / <sub>2</sub>	115 723.70		
		<sup>15</sup> / <sub>2</sub>	115 723.89		
3d <sup>4</sup> ( <sup>3</sup> D <sub>3</sub> )5g	<sup>2</sup> (3)	<sup>7</sup> / <sub>2</sub>	115 732.06		
		<sup>5</sup> / <sub>2</sub>	115 732.23		
3d <sup>4</sup> ( <sup>3</sup> D <sub>3</sub> )5g	<sup>2</sup> (4)	<sup>7</sup> / <sub>2</sub>	115 738.43		
3d <sup>4</sup> ( <sup>3</sup> D <sub>3</sub> )5g	<sup>2</sup> (6)	<sup>13</sup> / <sub>2</sub>	115 741.12		
		<sup>11</sup> / <sub>2</sub>	115 741.30		
3d <sup>4</sup> ( <sup>3</sup> D <sub>3</sub> )5g	<sup>2</sup> (5)	<sup>11</sup> / <sub>2</sub>	115 742.39		
		<sup>9</sup> / <sub>2</sub>	115 742.55		
3d <sup>4</sup> ( <sup>3</sup> D)5f	<sup>4</sup> D	<sup>5</sup> / <sub>2</sub>	115 810.34		
3d <sup>4</sup> ( <sup>3</sup> D <sub>1</sub> )5g	<sup>2</sup> (8)	<sup>17</sup> / <sub>2</sub>	115 927.17		
		<sup>15</sup> / <sub>2</sub>	115 927.30		
3d <sup>4</sup> ( <sup>3</sup> D <sub>1</sub> )5g	<sup>2</sup> (2)	<sup>5</sup> / <sub>2</sub>	115 926.73		
3d <sup>4</sup> ( <sup>4</sup> P)4s4p( <sup>1</sup> P)	<sup>4</sup> P	<sup>1</sup> / <sub>2</sub>	115 943.7		
		<sup>3</sup> / <sub>2</sub>	115 946.7		
		<sup>5</sup> / <sub>2</sub>	116 041.7		
3d <sup>4</sup> ( <sup>3</sup> D <sub>1</sub> )5g	<sup>2</sup> (3)	<sup>7</sup> / <sub>2</sub>	115 945.47		
3d <sup>4</sup> ( <sup>3</sup> D <sub>1</sub> )5g	<sup>2</sup> (4)	<sup>9</sup> / <sub>2</sub>	115 962.72		
		<sup>7</sup> / <sub>2</sub>	115 962.84		
3d <sup>4</sup> ( <sup>3</sup> D <sub>1</sub> )5g	<sup>2</sup> (7)	<sup>15</sup> / <sub>2</sub>	115 968.86		
		<sup>13</sup> / <sub>2</sub>	115 969.19		
3d <sup>4</sup> ( <sup>3</sup> D <sub>1</sub> )5g	<sup>2</sup> (5)	<sup>11</sup> / <sub>2</sub>	115 975.22		
		<sup>9</sup> / <sub>2</sub>	115 975.44		
3d <sup>4</sup> ( <sup>3</sup> D <sub>1</sub> )5g	<sup>2</sup> (6)	<sup>13</sup> / <sub>2</sub>	115 979.31		
		<sup>11</sup> / <sub>2</sub>	115 979.59		
3d <sup>4</sup> ( <sup>3</sup> D)6d	<sup>4</sup> G	<sup>3</sup> / <sub>2</sub>	116 171.71		
		<sup>5</sup> / <sub>2</sub>	116 213.38		
		<sup>7</sup> / <sub>2</sub>	116 281.95		
		<sup>9</sup> / <sub>2</sub>	116 388.95		
		<sup>11</sup> / <sub>2</sub>	116 531.26		
		<sup>13</sup> / <sub>2</sub>	116 708.67		



## Cr II—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	<i>g</i>	Leading percentages
3d <sup>4</sup> 1D16d	4P	3/2	116 253.35		
		5/2	116 295.06		
		7/2	116 385.67		
3d <sup>4</sup> 1D16d	4S	3/2	116 355.55		
3d <sup>4</sup> 1D16d	4F	1/2	116 360.98		
		3/2	116 429.23		
		5/2	116 477.51		
		7/2	116 572.42		
		9/2	116 601.65		
		11/2	116 829.01		
3d <sup>4</sup> 1D16d	4D	3/2	116 581.74		
		5/2	116 687.20		
		7/2	116 790.31		
		9/2	116 831.84		
3d <sup>4</sup> 1D16d	4G	5/2	116 877.15		
		7/2	116 985.30		
		9/2	117 141.58		
		11/2	117 342.41		
3d <sup>4</sup> 1D16d	4D	5/2	117 072.83		
		7/2	117 263.48		
3d <sup>4</sup> 1D16d	4F	5/2	117 228.51		
		7/2	117 488.50		
		9/2	117 520.75		
3d <sup>4</sup> 1D16d	4P	3/2	117 381.64		
		5/2	117 481.24		
3d <sup>4</sup> 1D16d	4S	5/2	117 672.56		
3d <sup>4</sup> (1P14s4p1 1P1)	4D	3/2	118 622.6		
		5/2	118 640.08		
		7/2	118 661.4		
		9/2	118 752.64		
3d <sup>4</sup> 1D18s	4D	1/2	120 702.6		
		3/2	120 757.1		
		5/2	120 870.78		
		7/2	121 096.43		
		9/2	121 246.83		
3d <sup>4</sup> (1D1)6g	2[5]	11/2	120 820.04		
		9/2	120 820.09		
3d <sup>4</sup> (1D2)6g	2[6]	13/2	120 938.67		
3d <sup>4</sup> (1D3)6g	2[7]	15/2	121 106.81		
		13/2	121 106.04		
3d <sup>4</sup> (1D3)6g	4[6]	13/2	121 114.06		
		11/2	121 114.25		
3d <sup>4</sup> (1L3)6g	2[5]	11/2	121 115.31		
		9/2	121 115.45		

## Cr II—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	<i>g</i>	Leading percentages
$3d^4(^5D_2)6g$	$^2[8]$	$^{17/2}$	121 315.57		
		$^{15/2}$	121 315.83		
$3d^4(^5D_1)6g$	$^2[4]$	$^{9/2}$	121 325.13		
		$^{7/2}$	121 335.25		
$3d^4(^5D_0)6g$	$^2[7]$	$^{15/2}$	121 338.96		
		$^{13/2}$	121 338.68		
$3d^4(^5D_1)6g$	$^2[6]$	$^{13/2}$	121 344.81		
		$^{11/2}$	121 345.09		
$3d^4(^5D)9s$	$^6D$	$^{7/2}$	124 310.74		
		$^{5/2}$	124 523.96		
Cr III ( $^4D_1$ )	<i>Limit</i>		132 966		

## Cr III

Z=24

Ti I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^4 3d^4 {}^5D_0$ Ionization energy =  $249\,700 \pm 200 \text{ cm}^{-1}$  ( $30.96 \pm 0.02 \text{ eV}$ )

The analysis was begun by White (1929) who found systems of triplet and quintet terms, which were later unified by Bowen (1937). F. L. Moore considerably augmented this work and provided his unpublished results to C. E. Moore (1952) for inclusion in her compilation. Ekberg (1976) has remeasured the spectrum in the region of 750–2700 Å with an uncertainty of  $\pm 0.005 \text{ Å}$  and established 76 new levels while rejecting 26 of those found by Moore.

We give the results of Ekberg for the  $3d^4$ ,  $3d^3 4s$ , and  $3d^3 4p$  configurations, including his calculated percentage compositions for the levels. The level uncertainty is  $\pm 0.1 \text{ cm}^{-1}$ . The  $3d^3({}^4F)4d {}^3H$  term is from White. The other terms of  $3d^3 4d$  and those of  $3d^3 5s$  are from the analysis by Moore. The uncertainty of these levels is  $\pm 0.5 \text{ cm}^{-1}$ .

Johansson and Ekberg (1982) discovered three terms of the  $3d^2 4s 4p$  configuration and gave their results in a preliminary report.

The ionization energy was derived by Catalán and Velasco (1952) from the 2-member  $3d^3 ns$  series.

## References

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 White, H. E. (1929), *Phys. Rev.* **33**, 914.

## Cr III

Configuration	Term	J	Level (cm <sup>-1</sup> )	Leading percentages		
$3d^4$	${}^5D$	0	0.00	100		
		1	62.22	100		
		2	183.16	100		
		3	356.55	100		
		4	576.08	100		
$3d^4$	${}^3P2$	0	16 771.36	58	41	${}^3P1$
		1	17 168.56	58	41	
		2	17 851.18	58	41	
$3d^4$	${}^3H$	4	17 273.70	99		
		5	17 396.92	99		
		6	17 530.65	100		
$3d^4$	${}^3P2$	2	18 451.84	77	22	${}^3P1$
		3	18 511.18	77	22	
		4	18 583.39	77	21	
$3d^4$	${}^1G$	3	20 703.64	98		
		4	20 852.95	98		
		5	20 996.04	98		
$3d^4$	${}^1G2$	4	25 138.87	64	36	${}^1G1$
$3d^4$	${}^3D$	3	25 726.44	100		
		2	25 790.94	100		
		1	25 848.31	100		
$3d^4$	${}^1I$	6	26 014.89	100		
$3d^4$	${}^1S2$	0	27 372.32	77	22	${}^1S1$

## Cr III—Continued

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$3d^4$	$^1D_2$	2	32 151.99	77	22	$^1D_1$
$3d^4$	$^1F$	3	37 005.16	100		
$3d^4$	$^3P_1$	4	43 286.71	79	21	$^3P_2$
		2	43 304.53	77	22	
		3	43 322.17	78	22	
$3d^4$	$^3P_1$	2	43 441.99	59	41	$^3P_2$
		1	43 916.59	59	41	
		0	44 141.36	59	41	
$3d^4(^3P)4s$	$^3P$	1	49 432.46	100		
		2	49 628.25	100		
		3	49 828.91	100		
		4	50 091.17	100		
		5	50 410.06	100		
$3d^4$	$^1G_1$	4	49 768.65	65	35	$^1G_2$
$3d^4(^3P)4s$	$^3P$	2	56 651.37	100		
		3	56 993.08	100		
		4	57 423.40	100		
$3d^4(^3P)4s$	$^3P$	1	63 045.74	100		
		2	63 174.30	99		
		3	63 421.92	100		
$3d^4$	$^1D_1$	2	65 763.21	78	22	$^1D_2$
$3d^4(^3G)4s$	$^3G$	3	65 892.38	100		
		4	66 090.01	100		
		5	66 225.09	99		
$3d^4(^3P)4s$	$^3P$	0	69 601.50	59	41	$(^3P) ^3P$
		1	69 781.89	56	34	
		2	70 292.86	71	15	
$3d^4(^3G)4s$	$^3G$	4	69 659.74	97		
$3d^4(^3P)4s$	$^3P$	2	70 191.01	63	26	$(^3P) ^3P$
		1	70 345.56	53	41	
		0	70 487.01	59	41	
$3d^4(^3D_2)4s$	$^3D$	1	70 981.26	65	19	$(^3D_1) ^3D$ $(^3D_1) ^3D$ $(^3P) ^3P$
		3	71 323.06	79	21	
		2	71 323.27	80	21	
$3d^4(^3H)4s$	$^3H$	4	71 677.19	97		
		5	71 737.56	99		
		6	71 870.17	100		
$3d^4(^3P)4s$	$^3P$	1	73 881.54	96		
$3d^4(^3D_2)4s$	$^3D$	2	74 788.88	77	22	$(^3D_1) ^3D$
$3d^4(^3H)4s$	$^3H$	5	75 351.63	100		

## Cr III—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$3d^4 \text{ } ^4\text{F} 4s$	$^4\text{F}$	4	84 374.12	100		
		3	84 484.76	100		
		2	84 572.53	100		
$3d^4 \text{ } ^4\text{F} 4s$	$^4\text{F}$	3	87 770.68	100		
$3d^4 \text{ } ^4\text{F} 4p$	$^4\text{G}^{\circ}$	2	93 766.21	100		
		3	94 029.99	100		
		4	94 376.29	100		
		5	94 801.70	100		
		6	95 306.09	100		
$3d^4 \text{ } ^4\text{F} 4p$	$^4\text{F}$	1	96 149.25	52	35	$(^4\text{F}) \text{ } ^4\text{D}$
		2	96 386.31	44	29	$(^4\text{F}) \text{ } ^4\text{D}$
		3	97 121.42	61	37	$(^4\text{F}) \text{ } ^4\text{D}$
		4	97 359.81	73	25	$(^4\text{F}) \text{ } ^4\text{D}$
		5	97 619.48	90		
$3d^4 \text{ } ^4\text{F} 4p$	$^4\text{D}^{\circ}$	0	96 693.97	97		
		3	96 714.04	51	25	$(^4\text{F}) \text{ } ^4\text{F}$
		1	96 774.38	79	18	
		2	96 922.02	56	42	
		4	97 088.28	72	26	
$3d^4 \text{ } ^4\text{F} 4p$	$^4\text{D}^{\circ}$	1	97 077.96	57	30	$(^4\text{F}) \text{ } ^4\text{F}$
		2	97 306.59	67	13	$(^4\text{F}) \text{ } ^4\text{F}$
		3	97 683.99	79	9	$(^4\text{F}) \text{ } ^4\text{D}$
$3d^4 \text{ } ^4\text{F} 4p$	$^4\text{G}^{\circ}$	3	99 841.67	93	5	$(^4\text{G}) \text{ } ^4\text{G}^{\circ}$
		4	100 100.66	93		
		5	100 423.01	92		
$3d^4 \text{ } ^4\text{F} 4p$	$^4\text{F}$	2	101 444.57	96		
		3	101 746.21	95		
		4	102 100.76	96		
$3d^4 \text{ } ^4\text{D} 4s$	$^4\text{D}$	3	102 236.46	79	21	$(^4\text{D}2) \text{ } ^4\text{D}$
		2	102 333.49	79	22	
		1	102 401.80	77	23	
$3d^4 \text{ } ^4\text{D} 4s$	$^4\text{D}$	2	105 626.89	78	22	$(^4\text{D}2) \text{ } ^4\text{D}$
$3d^4 \text{ } ^4\text{P} 4p$	$^4\text{P}^{\circ}$	1	108 250.89	99		
		2	108 461.40	99		
		3	108 795.84	99		
$3d^4 \text{ } ^4\text{P} 4p$	$^4\text{D}^{\circ}$	0	108 697.63	56	27	$(^4\text{P}) \text{ } ^4\text{P}^{\circ}$
		1	108 864.98	60	34	
		2	109 570.89	50	33	
		3	109 722.79	94		
		4	110 154.89	97		
$3d^4 \text{ } ^4\text{P} 4p$	$^4\text{P}^{\circ}$	2	108 972.90	52	20	$(^4\text{P}) \text{ } ^4\text{D}^{\circ}$
		0	109 458 11	47	41	
		1	109 570.62	54	27	
$3d^4 \text{ } ^4\text{G} 4p$	$^4\text{H}^{\circ}$	4	109 534.25	85	13	$(^4\text{H}) \text{ } ^4\text{H}^{\circ}$
		5	109 944.98	83	14	
		6	110 507 18	85	15	

## Cr III—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$3d^3\ ^2G\ 4p$	$^2G^o$	3	111 376.09	86	5	$(^1F)\ ^2G^o$
		4	111 644.76	89	5	
		5	111 856.97	86	5	
$3d^3\ ^2G\ 4p$	$^2F^o$	4	112 372.88	52	37	$(^2G)\ ^2G^o$
		2	112 399.84	73	13	$(^2D2)\ ^2F^o$
		3	112 467.01	70	8	$(^2D2)\ ^2F^o$
$3d^3\ ^2G\ 4p$	$^2G^o$	4	113 115.21	59	30	$(^2G)\ ^2F^o$
$3d^3\ ^2G\ 4p$	$^2F^o$	3	113 328.80	72	12	$(^2D2)\ ^2F^o$
$3d^3\ ^2P\ 4p$	$^2S^o$	2	113 357.04	96		
$3d^3\ ^2G\ 4p$	$^2H^o$	5	113 419.93	77	18	$(^2H)\ ^2H^o$
$3d^3\ ^2P\ 4p$	$^2D^o$	2	113 767.13	43	22	$(^2D2)\ ^2D^o$
$3d^3\ ^2P\ 4p$	$^2P^o$	0	113 861.47	62	22	$(^2D2)\ ^2P^o$
		1	113 899.43	57	23	
		2	114 599.14	47	22	
$3d^3\ ^2P\ 4p$	$^2D^o$	1	114 716.79	70	22	$(^2P)\ ^2D^o$
		2	115 182.15	59	21	
		3	115 554.23	48	31	
$3d^3\ ^2H\ 4p$	$^2H^o$	4	115 571.96	83	13	$(^2G)\ ^2H^o$
		5	115 670.74	85	14	
		6	115 844.58	85	15	
$3d^3\ ^2D2\ 4p$		1	116 372.92	30	$^2P^o$ 28	$(^2P)\ ^2D^o$
$3d^3\ ^2D2\ 4p$	$^2F^o$	2	116 391.66	40	25	$(^2P)\ ^2D^o$
		4	117 101.58	68	17	$(^2D1)\ ^2F^o$
$3d^3\ ^2P\ 4p$	$^2S^o$	1	116 451.19	80	13	$(^2P)\ ^2D^o$
$3d^3\ ^2P\ 4p$	$^2D^o$	3	116 532.95	44	21	$(^2D2)\ ^2F^o$
		2	116 782.05	34	31	$(^2P)\ ^2D^o$
$3d^3\ ^2P\ 4p$		1	116 774.00	32	$^2S^o$ 21	$(^2P)\ ^2D^o$
$3d^3\ ^2D2\ 4p$		3	116 969.09	37	$^2F^o$ 22	$(^2P)\ ^2D^o$
$3d^3\ ^2H\ 4p$	$^2I^o$	5	117 145.85	90		
		6	117 488.95	90		
		7	117 923.89	100		
$3d^3\ ^2D2\ 4p$	$^2D^o$	1	118 165.15	60	17	$(^2D2)\ ^2F^o$
		2	118 422.99	72	16	
		3	118 599.11	71	15	
$3d^3\ ^2H\ 4p$	$^2G^o$	4	118 900.53	81	15	$(^2P)\ ^2G^o$
$3d^3\ ^2D2\ 4p$	$^2P^o$	2	119 421.42	41	30	$(^2P)\ ^2P^o$
		1	119 489.02	42	28	
		0	119 625.62	46	26	
$3d^3\ ^2H\ 4p$	$^2H^o$	5	119 612.80	78	18	$(^2G)\ ^2H^o$

## Cr III—Continued

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$3d^3\ ^2D_{21}4p$	$^1F$	3	119 846.47	61	18	$(^2D_1)\ ^1F$
$3d^3\ ^2H_{14}4p$	$^1I$	6	120 432.99	90		
$3d^3\ ^2H_{14}4p$	$^3G$	5	120 700.27	80		
		4	120 749.55	80		
		3	120 767.26	90		
$3d^3\ ^4P_{14}4p$	$^3S$	1	121 446.77	87		
$3d^3\ ^2P_{14}4p$	$^1P$	1	122 396.49	71	17	$(^2D_2)\ ^1P$
$3d^3\ ^2D_{21}4p$	$^1D$	2	123 105.84	46	41	$(^2P)\ ^1D$
$3d^3\ ^2F_{14}4p$	$^3F$	2	128 754.62	95		
		3	128 784.13	94		
		4	128 850.49	94		
$3d^3\ ^2F_{14}4p$	$^3G$	3	131 116.36	92	5	$(^2H)\ ^3G$
		4	131 265.66	92	5	$(^2H)\ ^3G$
		5	131 450.16	96		
$3d^3\ ^2F_{14}4p$	$^1D$	2	132 070.71	79	18	$(^2D_1)\ ^1D$
$3d^3\ ^2F_{14}4p$	$^3D$	3	132 117.50	92	5	$(^2D_1)\ ^3D$
		2	132 499.78	91	5	
		1	132 734.22	94	5	
$3d^3\ ^2F_{14}4p$	$^1G$	4	133 969.57	83	15	$(^2H)\ ^1G$
$3d^3\ ^2F_{14}4p$	$^1F$	3	134 887.54	94		
$3d^3\ ^2D_{14}4p$	$^3D$	1	146 996.18	77	19	$(^2D_2)\ ^3D$
		2	146 973.33	77	18	
		3	147 090.73	77	17	
$3d^3\ ^2D_{14}4p$	$^1D$	2	148 573.81	53	20	$(^2D_2)\ ^1D$
$3d^3\ ^2D_{14}4p$	$^3F$	2	149 344.03	62	20	$(^2D_2)\ ^3F$
		3	149 383.64	73	23	
		4	149 626.90	75	23	
$3d^3\ ^2D_{14}4p$	$^3P$	2	151 351.27	75	23	$(^2D_2)\ ^3P$
		1	151 687.44	75	24	
		0	151 852.12	75	24	
$3d^3\ ^2D_{14}4p$	$^1F$	3	152 037.21	77	20	$(^2D)\ ^1F$
$3d^3\ ^4F_{14}d$	$^3H$	3	152 927.3			
		4	153 099.1			
		5	153 314.6			
		6	153 571.7			
		7	153 871.7			
$3d^3\ ^2D_{14}4p$	$^1P$	1	156 929.93	75	24	$(^2D_2)\ ^1P$

## Cr III—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Leading percentages
$3d^2(^3F)5s$	$^3F$	1	157 303.2	
		2	157 435.1	
		3	157 637.3	
		4	157 908.0	
		5	158 241.8	
$3d^2(^3F)4d$	$^3G$	3	158 066.7	
		4	158 442.9	
$3d^2(^3F)5s$	$^3P$	2	159 031.8	
		3	159 375.6	
		4	159 803.3	
$3d^2(^3F)4d$	$^3P$	3	158 463.6	
		4	158 623.7	
$3d^2(^3H)4d$	$^3I$	5	173 200.5	
		6	173 662.8	
$3d^2(^3F)4s4p(^3P^o)$	$^3G^o$	2	175 965.9	
		3	176 274.8	
		4	176 684.7	
		5	177 196.0	
		6	177 803.9	
$3d^2(^3F)4s4p(^3P^o)$	$^3F^o$	1	177 292.3	
		2	177 466.1	
		3	177 724.9	
		4	178 063.9	
		5	178 473.5	
$3d^2(^3F)4s4p(^3P^o)$	$^3D^o$	0	179 815.5	
		1	179 863.2	
		2	179 951.6	
		3	180 100.8	
		4	180 334.0	
Cr IV ( $^4F_{2,2}$ )	<i>Limit</i>		249 700	



## Cr IV

Z = 24

Sc I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^1 {}^4F_{3/2}$ Ionization energy =  $396\,500 \pm 400 \text{ cm}^{-1}$  ( $49.16 \pm 0.05 \text{ eV}$ )

The initial analysis was by White (1929) and was later extended by Bowen (1937). Ekberg (1973) reobserved the spectrum and extended the analysis but reported no levels above  $211\,574 \text{ cm}^{-1}$ . With new observations Ekberg and Engström (1982) greatly increased the range of known energy levels by establishing 59 of the 67 possible  $3d^2 4d$  levels and 15 of the 16  $3d^2 5s$  levels, as well as the  $3d^2 ({}^1S) 4s {}^2S_{1/2}$  level. The uncertainty of the energy level values is  $\pm 0.4 \text{ cm}^{-1}$ . Percentage compositions for all the known levels were obtained by these authors.

From the  $3d^2 ({}^3F) ns$  terms for  $n = 4, 5$  and an extrapolated value for the change in effective quantum number between them, Ekberg and Engström determined the value for the ionization energy.

## References

- Bowen, I. S. (1937), *Phys. Rev.* 52, 1153.  
 Ekberg, J. O. (1973), *Phys. Scr.* 7, 55.  
 Ekberg, J. O., and Engström, L. (1982), *Phys. Scr.* 25, 611.  
 White, H. E. (1929), *Phys. Rev.* 33, 672.

## Cr IV

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$3d^2$	${}^4F$	$3/2$	0.0	100		
		$5/2$	237.4	100		
		$7/2$	556.4	100		
		$9/2$	945.5	100		
$3d^2$	${}^4P$	$1/2$	14 059.9	100		
		$3/2$	14 177.5	99		
		$5/2$	14 472.2	100		
$3d^2$	${}^2G$	$7/2$	15 053.6	100		
		$9/2$	15 402.4	100		
$3d^2$	${}^2P$	$3/2$	19 439.4	93		
		$1/2$	19 520.8	100		
$3d^2$	${}^2D_2$	$3/2$	20 651.0	72	22	${}^2D_1$
		$5/2$	20 665.5	78	22	
$3d^2$	${}^2H$	$9/2$	21 066.9	100		
		$11/2$	21 321.1	100		
$3d^2$	${}^2F$	$7/2$	34 364.3	100		
		$5/2$	34 556.9	100		
$3d^2$	${}^2D_1$	$5/2$	52 976.4	78	22	${}^2D_2$
		$3/2$	53 143.8	77	23	
$3d^2 ({}^3F) 4s$	${}^4F$	$5/2$	103 996.5	100		
		$7/2$	104 258.6	100		
		$9/2$	104 630.2	100		
		$11/2$	105 106.7	100		
$3d^2 ({}^3F) 4s$	${}^2F$	$5/2$	109 941.5	100		
		$7/2$	110 691.8	100		
$3d^2 ({}^1D) 4s$	${}^2D$	$5/2$	118 571.5	66	34	$({}^2P) {}^4P^o$
		$3/2$	118 727.8	68	32	

## Cr IV—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	Leading percentages		
3d <sup>2</sup> ( <sup>3</sup> P)4s	<sup>4</sup> P	1/2	119 014.6	100		
		3/2	119 252.0	58	42	( <sup>1</sup> D) <sup>2</sup> D*
		5/2	119 671.3	65	35	( <sup>1</sup> D) <sup>2</sup> D*
3d <sup>2</sup> ( <sup>3</sup> P)4s	<sup>2</sup> P	1/2	124 410.5	100		
		3/2	124 734.4	99		
3d <sup>2</sup> ( <sup>1</sup> G)4s	<sup>2</sup> G	3/2	127 195.7	100		
		5/2	127 208.3	100		
3d <sup>2</sup> ( <sup>1</sup> S)4s	<sup>2</sup> S	1/2	155 354.4	100		
3d <sup>2</sup> ( <sup>3</sup> F)4p	<sup>4</sup> G*	3/2	157 361.4	96		
		5/2	157 933.3	97		
		7/2	158 629.5	98		
		11/2	159 449.2	100		
3d <sup>2</sup> ( <sup>3</sup> F)4p	<sup>4</sup> F	3/2	158 527.7	97		
		5/2	158 892.7	98		
		7/2	159 352.0	98		
		9/2	159 863.6	98		
3d <sup>2</sup> ( <sup>3</sup> F)4p	<sup>2</sup> F	3/2	160 305.4	78	5	( <sup>1</sup> D) <sup>2</sup> F*
		5/2	160 937.4	79	14	( <sup>3</sup> F) <sup>4</sup> D*
3d <sup>2</sup> ( <sup>3</sup> F)4p	<sup>2</sup> D*	3/2	160 986.5	45	42	( <sup>3</sup> F) <sup>4</sup> D*
		5/2	162 301.4	60	22	
3d <sup>2</sup> ( <sup>1</sup> F)4p	<sup>4</sup> D*	1/2	161 354.8	94	6	( <sup>3</sup> P) <sup>4</sup> P*
		3/2	161 495.3	67	15	( <sup>3</sup> F) <sup>2</sup> D*
		5/2	161 756.3	52	36	( <sup>3</sup> F) <sup>2</sup> D*
		7/2	162 064.9	81	13	( <sup>3</sup> F) <sup>2</sup> F*
3d <sup>2</sup> ( <sup>3</sup> F)4p	<sup>2</sup> G*	7/2	164 909.7	96		
		9/2	165 430.0	96		
3d <sup>2</sup> ( <sup>3</sup> P)4p	<sup>2</sup> S*	1/2	167 896.5	99		
3d <sup>2</sup> ( <sup>3</sup> P)4p	<sup>4</sup> S*	3/2	171 081.3	91	9	( <sup>1</sup> D) <sup>2</sup> P*
3d <sup>2</sup> ( <sup>1</sup> D)4p	<sup>2</sup> P*	3/2	172 184.0	84	9	( <sup>3</sup> P) <sup>4</sup> S*
		5/2	172 823.2	96		
3d <sup>2</sup> ( <sup>1</sup> D)4p	<sup>2</sup> F*	3/2	172 636.4	87	7	( <sup>3</sup> F) <sup>2</sup> F*
		5/2	173 366.0	84	7	( <sup>3</sup> P) <sup>4</sup> D*
3d <sup>2</sup> ( <sup>3</sup> P)4p	<sup>4</sup> D*	1/2	173 431.9	98	5	( <sup>3</sup> F) <sup>4</sup> D*
		3/2	173 659.1	92	5	( <sup>3</sup> F) <sup>4</sup> D*
		5/2	174 096.2	89		
		7/2	174 846.2	88	7	( <sup>1</sup> D) <sup>2</sup> F*
3d <sup>2</sup> ( <sup>1</sup> D)4p	<sup>2</sup> D*	3/2	174 539.7	82	6	( <sup>3</sup> F) <sup>2</sup> D*
		5/2	174 968.6	82	6	
3d <sup>2</sup> ( <sup>3</sup> P)4p	<sup>4</sup> P*	1/2	176 690.9	99		
		3/2	176 916.7	99		
		5/2	177 406.5	96		

## Cr IV—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$3d^4\ ^1G_14p$	$^1G^o$	$7/2$	177 916.5	95		
		$9/2$	178 030.0	95		
$3d^4\ ^3P_14p$	$^3D^o$	$5/2$	181 243.1	81	12	$(^3F)\ ^3D^o$
		$3/2$	181 277.9	79	10	
$3d^4\ ^1G_14p$	$^3H^o$	$9/2$	182 679.2	99		
		$11/2$	183 444.2	100		
$3d^4\ ^3P_14p$	$^3P^o$	$1/2$	183 720.3	99		
		$3/2$	183 875.6	97		
$3d^4\ ^1G_14p$	$^3F^o$	$7/2$	186 980.8	96		
		$5/2$	187 519.0	97		
$3d^4\ ^1S_14p$	$^3P^o$	$1/2$	210 559.2	98		
		$3/2$	211 575.9	98		
$3d^4\ ^3F_14d$	$^4G^o$	$5/2$	232 566.1	88	12	$(^3F)\ ^3F$
		$7/2$	232 896.6	87	11	$(^3F)\ ^4H$
		$9/2$	233 236.7	82	18	$(^3F)\ ^4H$
		$11/2$	233 647.0	80	19	$(^3F)\ ^4H$
$3d^4\ ^1F_14d$	$^4F^o$	$5/2$	233 117.3	82	12	$(^3F)\ ^4G$
		$7/2$	233 637.6	89		
$3d^4\ ^3F_14d$	$^4H^o$	$7/2$	233 358.8	89	11	$(^3F)\ ^4G$
		$9/2$	233 708.5	82	18	
		$11/2$	234 100.1	80	20	
		$13/2$	234 500.9	100		
$3d^4\ ^1F_14d$	$^4D^o$	$1/2$	233 618.4	97		
		$3/2$	233 798.9	98		
		$5/2$	234 085.2	98		
		$7/2$	234 502.1	95		
$3d^4\ ^1F_14d$	$^4P^o$	$1/2$	235 743.0	88	7	$(^1D)\ ^3P$
		$3/2$	236 491.4	89	6	
$3d^4\ ^1F_14d$	$^4P^o$	$1/2$	237 798.2	86	13	$(^3P)\ ^4P$
		$3/2$	238 100.4	85	13	
		$5/2$	238 447.1	84	14	
$3d^4\ ^1F_14d$	$^2G^o$	$7/2$	237 999.5	84	12	$(^1D)\ ^2G$
		$9/2$	238 561.3	84	12	
$3d^4\ ^3F_14d$	$^4D^o$	$3/2$	239 541.4	78	18	$(^1D)\ ^3D$
		$5/2$	239 822.2	75	19	
$3d^4\ ^1F_14d$	$^2H^o$	$9/2$	239 582.6	91	9	$(^1G)\ ^4H$
		$11/2$	240 268.8	90	9	
$3d^4\ ^1F_14d$	$^4F^o$	$3/2$	240 967.9	95		
		$5/2$	241 182.5	95		
		$7/2$	241 472.8	95		
		$9/2$	241 832.5	95		

## Cr IV—Continued

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$3d^2(^3P)4d$	$^3P$	$3/2$	247 099.1	69	46	$(^1D) ^3P$
		$1/2$	247 765.0	59	26	
$3d^2(^1D)4d$	$^3F$	$5/2$	247 239.3	84	15	$(^3P) ^3F$
		$1/2$	247 546.7	86	11	
$3d^2(^1D)4d$	$^2G$	$3/2$	249 932.5	75	8	$(^1G) ^2G$
		$1/2$	250 007.7	79	8	
$3d^2(^3P)4d$	$^4F$	$5/2$	250 535.2	91		$(^3P) ^4D$ $(^1G) ^2G$
		$1/2$	250 752.7	86	6	
		$3/2$	251 093.1	86	8	
$3d^2(^3P)4d$	$^4D$	$3/2$	251 017.3	97		$(^3P) ^4F$
		$1/2$	251 095.6	99		
		$3/2$	251 137.8	94		
		$1/2$	251 342.7	93	5	
$3d^2(^3F)5s$	$^4F$	$3/2$	251 563.9	100		
		$5/2$	251 817.0	97		
		$1/2$	252 158.3	98		
		$3/2$	252 694.5	100		
$3d^2(^3P)4d$	$^2F$	$5/2$	252 464.8	54	37	$(^1G) ^2F$
		$1/2$	252 532.8	56	26	
$3d^2(^3F)5s$	$^2F$	$3/2$	253 476.1	97		
		$1/2$	254 212.1	98		
$3d^2(^3P)4d$	$^4P$	$3/2$	254 534.6	81	13	$(^3F) ^4P$
$3d^2(^3P)4d$	$^2D$	$3/2$	255 662.3	35	27	$(^1D) ^2D$
		$5/2$	255 836.9	38	35	
$3d^2(^1D)4d$	$^2P$	$1/2$	255 803.6	51	34	$(^3P) ^2P$ $(^3P) ^2D$
		$3/2$	256 306.2	43	31	
$3d^2(^1G)4d$	$^2I$	$11/2$	256 853.2	100		
		$13/2$	256 885.4	100		
$3d^2(^1G)4d$	$^2G$	$7/2$	257 588.6	88	7	$(^3F) ^2G$
		$9/2$	257 714.4	87	7	
$3d^2(^1G)4d$	$^2H$	$9/2$	259 755.4	91	9	$(^3F) ^2H$
		$11/2$	259 799.6	91	9	
$3d^2(^1G)4d$	$^2F$	$7/2$	263 875.9	62	27	$(^3P) ^2F$
		$9/2$	263 971.0	61	27	
$3d^2(^1D)5s$	$^2D$	$5/2$	265 031.6	96		
		$3/2$	265 048.6	98		
$3d^2(^1G)4d$	$^2D$	$3/2$	266 878.0	64	32	$(^3P) ^2D$
		$5/2$	266 931.7	64	32	
$3d^2(^3P)5s$	$^4P$	$1/2$	266 946.6	100		
		$3/2$	267 130.4	99		
		$5/2$	267 469.0	96		

## Cr IV—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Leading percentages
$3d^4 4p^1 5s$	P	$\frac{1}{2}$	268 458.1	100
		$\frac{3}{2}$	268 813.4	99
$3d^4 4p^1 5s$	G	$\frac{3}{2}$	273 865.3	100
		$\frac{5}{2}$	273 866.6	100
$\text{Cr V } (F_2)$	<i>Limit</i>		396 500	

## Cr v

Z=24

Ca I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^2 {}^3F_2$ Ionization energy =  $560\,200 \pm 300 \text{ cm}^{-1}$  ( $69.46 \pm 0.04 \text{ eV}$ )

The initial analysis is due to White (1929) who reported levels of the  $3d^2$ ,  $3d4s$ ,  $3d4p$ , and  $3d4d$  configurations. Additions and revisions were made by Cady and Edlén and were communicated to Moore for inclusion in her AEL compilation (1952). The spectrum was completely reobserved in the range of 400–1800 Å by Ekberg (1973) whose results are quoted here. The uncertainty in his level values is given as  $\pm 0.5 \text{ cm}^{-1}$ . He added the  ${}^1S_0$  level of  $3d^2$  and all the known levels of  $3d4d$  and  $3d5s$ . The one term of  $3d4d$  due to White was found to be false.

The ionization energy was derived by Ekberg from the series  $3d4s$  and  $3d5s$ .

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## Cr v

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Configuration	Term	J	Level ( $\text{cm}^{-1}$ )				
$3d^2$	${}^3F$	2	0.0	$3d4d$	${}^1P$	3	316 674.9				
		3	508.2			$3d4d$	${}^3D$	1	317 893.8		
		4	1 141.7					2	318 227.6		
$3d^2$	${}^1D$	2	13 188.0	$3d4d$	${}^3G$	3	319 119.1				
		$3d^2$	${}^3P$			0	15 491.8	4	319 516.8		
1	15 676.6					5	320 074.4				
$3d^2$	${}^3P$	2	16 041.0	$3d4d$	${}^1P$	1	319 284.0				
		$3d^2$	${}^1G$			4	22 019.2	$3d4d$	${}^3S$	1	322 528.1
						$3d^2$	${}^1S$			0	51 146.4
2	167 176.4	3	325 472.5								
$3d4s$	${}^3D$	1	167 176.4	$3d4d$	${}^3P$	4	325 884.2				
		2	167 491.0			$3d4d$	${}^1D$	2	329 350.3		
		3	168 089.5					$3d4d$	${}^3P$	0	330 084.8
$3d4s$	${}^1D$	2	171 698.1	1	330 245.1						
		$3d4p$	${}^1D$	2	226 119.8	2	330 596.8				
				$3d4p$	${}^3D$	1	228 001.8	$3d4d$	${}^1G$	4	331 811.2
2	228 489.1					$3d5s$	${}^3D$			1	356 744.8
3	229 120.8	2	356 981.3								
$3d4p$	${}^3P$	2	229 551.7	$3d5s$	${}^3D$	3	357 675.9				
		3	230 316.3			$3d5s$	${}^1D$	2	358 658.8		
		4	231 392.9					Cr VI ( ${}^3D_{1,1}$ )	Limit	560 200	
$3d4p$	${}^3P$	1	234 618.4								
		0	234 668.5								
		2	234 846.4								
$3d4p$	${}^1F$	3	237 529.5								
$3d4p$	${}^1P$	1	239 917.5								

## Cr vi

Z=24

K I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^4 3d^2 D_{3/2}$ Ionization energy =  $731\,020 \pm 6 \text{ cm}^{-1}$  ( $90.6356 \pm 0.0007 \text{ eV}$ )

The first known terms were found by Gibbs and White (1926, 1929) who reported the positions of the  $3p^4 3d^2 D$ ,  $4s^2 S$ , and  $4p^2 P$  terms. The  $n/{}^2F$  series for  $n=5-10$  was identified by Alexander, Feldman, and Fraenkel (1965) and the missing  $4f^2 F$  by Gabriel, Fawcett, and Jordan (1965) who replaced the false levels of this term given earlier by Kruger and Weissberg (1937). The  $4p^2 P - 4d^2 D$  multiplet was found by Fawcett (1970). Observations of open  $3p^6$ -core configurations were first reported by Feldman and Fraenkel (1966) who identified the  $3p^4 3d - 3p^2 3d 4s$  transition array. Some of these lines were classified by Cowan (1967). Gabriel, Fawcett, and Jordan (1966) classified six lines of the  $3p^4 3d - 3p^2 3d^2$  group.

The spectrum was reobserved in the range of 400-2500 Å by Ekberg (1973). He interpreted a considerable number of new lines and verified the earlier work. His revisions of the values for the known levels and his additions to the analysis are quoted here. Levels obtained from transitions to the ground term from 350 000 to

700 000  $\text{cm}^{-1}$  are given to the units place and have an uncertainty varying from  $\pm 5$  to  $\pm 20 \text{ cm}^{-1}$ . The rest have an uncertainty of  $\pm 1 \text{ cm}^{-1}$ . The ionization energy is derived by Ekberg from the  $nA$  series with an estimated uncertainty of  $\pm 6 \text{ cm}^{-1}$ .

## References

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## Cr vi

Configuration	Term	J	Level (cm <sup>-1</sup> )	Configuration	Term	J	Level (cm <sup>-1</sup> )
$3p^4(1S)3d$	${}^3D$	$\frac{3}{2}$	0	$3p^4(2P^o)3d^2(2P)$	${}^2P^o$	$\frac{1}{2}$	488 247.1
		$\frac{5}{2}$	940			$\frac{3}{2}$	494 911.2
$3p^4(1S)4s$	${}^2S$	$\frac{1}{2}$	227 857.9	$3p^4(2P^o)3d^2(2F)$	${}^3D^o$	$\frac{5}{2}$	496 958
$3p^4(1S)4p$	${}^2P^o$	$\frac{1}{2}$	296 573.2			$\frac{3}{2}$	497 495
		$\frac{3}{2}$	298 396.7	$3p^4(1S)5d$	${}^3D$	$\frac{3}{2}$	534 881.7
$3p^4(2P^o)3d^2(1G)$	${}^2P^o$	$\frac{5}{2}$	356 962			$\frac{5}{2}$	534 489.7
		$\frac{7}{2}$	359 165	$3p^4(1S)6s$	${}^2S$	$\frac{1}{2}$	562 064.1
$3p^4(2P^o)3d^2(1D)$	${}^2P^o$	$\frac{7}{2}$	371 618			$3p^4(1S)5f$	${}^2F^o$
		$\frac{5}{2}$	378 677	$\frac{7}{2}$	568 993.0		
$3p^4(1S)4d$	${}^3D$	$\frac{3}{2}$	402 661.7	$3p^4(1S)5g$	${}^2G$	$\frac{7}{2}$	572 272.8
		$\frac{5}{2}$	402 888.6			$\frac{9}{2}$	572 274.4
$3p^4(2P^o)3d^2(2P)$	${}^2P^o$	$\frac{5}{2}$	440 135.2	$3p^4(1S)6p$	${}^2P^o$	$\frac{1}{2}$	574 135
		$\frac{7}{2}$	442 945.4			$\frac{3}{2}$	575 742
$3p^4(1S)5s$	${}^2S$	$\frac{1}{2}$	461 253.0	$3p^4 3d(2P^o)4s$	${}^2P^o$	$\frac{1}{2}$	578 566
$3p^4(1S)4f$	${}^2F^o$	$\frac{5}{2}$	481 956.0			$\frac{3}{2}$	580 697
		$\frac{7}{2}$	482 517.1	$3p^4 3d(2P^o)4s$	${}^4P^o$	$\frac{7}{2}$	584 371
$3p^4(1S)5p$	${}^2P^o$	$\frac{1}{2}$	487 589.5			$\frac{5}{2}$	586 278
		$\frac{3}{2}$	488 561.9				

## Cr VI—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )
3p <sup>5</sup> 3d( <sup>3</sup> F) 4s	<sup>3</sup> F	1/2	591 197	3p <sup>6</sup> ( <sup>1</sup> S)6h	<sup>3</sup> H	3/2 1/2	631 162.9
		3/2	594 926				
3p <sup>5</sup> 3d( <sup>3</sup> D) 4s	<sup>3</sup> D	1/2	607 615	3p <sup>6</sup> ( <sup>1</sup> S)7f	<sup>3</sup> F	1/2	648 531
		3/2	608 631			1/2	
		5/2	609 166	3p <sup>6</sup> ( <sup>1</sup> S)7h	<sup>3</sup> H	3/2 1/2	650 310.8
3p <sup>5</sup> 3d( <sup>1</sup> D) 4s	<sup>3</sup> D	1/2	610 497			3p <sup>6</sup> ( <sup>1</sup> S)8f	
		3/2	611 568				
3p <sup>5</sup> 3d( <sup>1</sup> F) 4s	<sup>3</sup> F	1/2	614 385	3p <sup>6</sup> ( <sup>1</sup> S)9f	<sup>3</sup> F	3/2 1/2	681 907
		3/2	616 079				
3p <sup>5</sup> 3d( <sup>3</sup> D) 4s	<sup>3</sup> D	1/2	618 491	3p <sup>6</sup> ( <sup>1</sup> S)10f	<sup>3</sup> F	3/2 1/2	690 781
		3/2	619 419				
3p <sup>5</sup> ( <sup>1</sup> S)6f	<sup>3</sup> F	1/2	618 583	Cr VII ( <sup>1</sup> S <sub>0</sub> )	Limit		731 020
		3/2	618 849				
3p <sup>5</sup> ( <sup>1</sup> S)6g	<sup>3</sup> G	1/2	620 696.3				
		3/2	620 700.5				



## Cr VII

Z = 24

Ar I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^4 {}^1S_0$ Ionization energy =  $1\,291\,900 \pm 600 \text{ cm}^{-1}$  ( $160.18 \pm 0.07 \text{ eV}$ )

Most of the levels are taken from an extensive analysis by Ekberg (1976) who observed the spectrum in the range of 90–2000 Å with an accuracy of  $\pm 0.01 \text{ Å}$ . The few earlier identifications are noted in his work. Relative to the ground state the level uncertainty is  $\pm 1\%$   $\text{cm}^{-1}$ . Among the excited levels the relative uncertainty is  $\pm 0.5 \text{ cm}^{-1}$ . The designations and percentage compositions for the levels are from Ekberg. A value for the ionization energy of  $1\,291\,900 (600) \text{ cm}^{-1}$  was derived by him by extrapolation. The same value may be derived from the 3-member *ns* series.

The terms  $3s 3p^4 4p {}^3P_1^o$ ,  $5p {}^1P_1^o$  and  ${}^1P_1^o$ ,  $6p {}^1P_1^o$ , and  $7p {}^1P_1^o$  were determined by Kastner, Crooker, Behring, and Cohen (1977) from observations of absorption in a spark between 70 and 100 Å. The level uncertainty obtained from these data is  $\pm 100 \text{ cm}^{-1}$ .

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## Cr VII

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$3s^2 3p^4$	${}^1S$	0	0.0			
$3s^2 3p^3 3d$	${}^3P^o$	0	341 179.3	100		
		1	342 773.5	100		
		2	346 137.1	99		
$3s^2 3p^3 3d$	${}^3F^o$	4	357 543.7	100		
		3	360 771.9	97		
		2	363 060.9	96		
$3s^2 3p^3 3d$	${}^1D^o$	2	382 682.3	77	19	${}^3D^o$
$3s^2 3p^3 3d$	${}^3D^o$	3	382 737.4	74	26	${}^1F^o$
		1	385 828.3	99		
		2	386 616.6	78	20	${}^1D^o$
$3s^2 3p^3 3d$	${}^1F^o$	3	389 226.2	72	25	${}^3D^o$
$3s^2 3p^3 3d$	${}^1P^o$	1	493 035.4	100		
$3s 3p^5 3d$	${}^3D$	1	608 679.6	100		
		2	609 142.7	100		
		3	609 887.8	100		
$3s 3p^5 3d$	${}^1D$	2	627 826.7	100		
$3s^2 3p^3 ({}^4P_{1,2}) 4s$	${}^2[3/2]^o$	2	668 858.6	100		
		1	672 427.7	86	15	$({}^2P_{1/2}^o) {}^2[1/2]^o$
$3s^2 3p^3 ({}^2P_{1/2}) 4s$	${}^2[1/2]^o$	0	678 534.7	100		
		1	682 610.2	86	15	$({}^2P_{3/2}^o) {}^2[3/2]^o$
$3s^2 3p^3 4p$	${}^3S$	1	734 605.3			

## Cr VII—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	Leading percentages		
3s <sup>2</sup> 3p <sup>3</sup> 4p	<sup>3</sup> D	2	745 328.9			
		3	745 631.1			
		1	748 629.3			
3s <sup>2</sup> 3p <sup>3</sup> 4p	<sup>3</sup> P	2	751 649.3			
		0	757 035.8			
		1	758 572.1			
3s <sup>2</sup> 3p <sup>3</sup> 4p	<sup>1</sup> P	1	754 378.9			
3s <sup>2</sup> 3p <sup>3</sup> 4p	<sup>1</sup> D	2	758 374.4			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4d	<sup>2</sup> [1/2] <sup>o</sup>	0	856 292.2	100		
		1	857 234.5	75	20	( <sup>2</sup> P <sub>3/2</sub> ) <sup>2</sup> [3/2] <sup>o</sup>
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4d	<sup>2</sup> [3/2] <sup>o</sup>	2	859 407.1	85	15	( <sup>2</sup> P <sub>3/2</sub> ) <sup>2</sup> [3/2] <sup>o</sup>
		1	866 502.8	79	21	( <sup>2</sup> P <sub>3/2</sub> ) <sup>2</sup> [1/2] <sup>o</sup>
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4d	<sup>2</sup> [7/2] <sup>o</sup>	4	860 444.3	100		
		3	861 198.4	93		
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4d	<sup>2</sup> [5/2] <sup>o</sup>	2	864 129.5	88	11	( <sup>2</sup> P <sub>3/2</sub> ) <sup>2</sup> [5/2] <sup>o</sup>
		3	865 155.8	88	6	( <sup>2</sup> P <sub>3/2</sub> ) <sup>2</sup> [7/2] <sup>o</sup>
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4d	<sup>2</sup> [5/2] <sup>o</sup>	2	872 231.6	88	12	( <sup>2</sup> P <sub>3/2</sub> ) <sup>2</sup> [5/2] <sup>o</sup>
		3	873 146.1	92	7	( <sup>2</sup> P <sub>3/2</sub> ) <sup>2</sup> [5/2] <sup>o</sup>
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4d	<sup>2</sup> [3/2] <sup>o</sup>	2	873 565.5	85	15	( <sup>2</sup> P <sub>3/2</sub> ) <sup>2</sup> [3/2] <sup>o</sup>
		1	875 380.5	95		
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4f	<sup>2</sup> [3/2]	1	941 811			
		2	943 149.1			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4f	<sup>2</sup> [9/2]	5	944 416.8			
		4	945 475.7			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4f	<sup>2</sup> [5/2]	3	944 866.7			
		2	954 623			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4f	<sup>2</sup> [7/2]	3	947 917.4			
		4	948 943.9			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 5s	<sup>2</sup> [3/2] <sup>o</sup>	1	951 122			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4f	<sup>2</sup> [7/2]	3	956 454			
		4	957 205.1			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 4f	<sup>2</sup> [5/2]	3	957 004.6			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 5s	<sup>2</sup> [1/2] <sup>o</sup>	1	960 366			
3s 3p <sup>6</sup> 4p	<sup>3</sup> P <sup>o</sup>	1	984 590			
3s 3p <sup>6</sup> 4p	<sup>1</sup> P <sup>o</sup>	1	994 105			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 5d	<sup>2</sup> [3/2] <sup>o</sup>	1	1 033 485			
3s <sup>2</sup> 3p <sup>3</sup> ( <sup>2</sup> P <sub>3/2</sub> ) 5d	<sup>2</sup> [3/2] <sup>o</sup>	1	1 042 568			

## Cr VII—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Leading percentages
$3s^2 3p^3 \ ^2P_{1/2}^o 16s$	$^2[3/2]^o$	1	1 075 627	
$3s^2 3p^3 \ ^2P_{3/2}^o 16s$	$^2[1/2]^o$	1	1 085 446	
$3s3p^4 \ 5p$	$^3P^o$	1	1 219 810	
$3s3p^4 \ 5p$	$^3P^o$	1	1 227 130	
Cr VIII $\ ^2P_{1/2}^o$	<i>Limit</i>		1 291 900	
$3s3p^4 \ 6p$	$^3P^o$	1	1 335 560	
$3s3p^4 \ 7p$	$^3P^o$	1	1 393 840	

## Cr VII

Z = 24

Cl I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^3 \ ^2P_{1/2}$ Ionization energy =  $1\,490\,000 \pm 3000 \text{ cm}^{-1}$  ( $184.7 \pm 0.4 \text{ eV}$ )

All the known levels are derived from transitions to the  $3s^2 3p^3 \ ^2P$  ground term. Edlén (1937) identified lines originating from all levels of the  $3s^2 3p^4 4s$  configuration except for the  $^2P_{1/2}$ . Earlier, Weissberg and Kruger (1936) had reported lines from the  $^2P$  term of this configuration as well as from the  $^2S$  term of  $3s 3p^6$ . The transitions from  $3s^2 3p^4 3d$  were identified by Gabriel, Fawcett, and Jordan (1966) and by Fawcett and Gabriel (1966). The parent states for the terms  $3s^2 3p^4 3d \ ^2P$  and  $^2D$  are changed to  $3p^4$  ( $^2P$ ) as indicated by the calculated states of Fe X by Bromage, Cowan, and Fawcett (1977). Transitions from  $3s^2 3p^4 4d$  were given by Fawcett, Cowan, and Hayes (1972). Line identifications in the  $3p^4 3d - 3p^4 4d$  transition array were also given in this paper but cannot be used to derive energy levels because they do not combine with known levels.

The recent measurements of the  $3s^2 3p^3 - 3s 3p^4$  doublet by Smitt, Svensson, and Outred (1976) are used to

determine the ground term interval with an uncertainty of  $\pm 2 \text{ cm}^{-1}$  and the  $3s 3p^4 \ ^2S_{1/2}$  level with an uncertainty of  $\pm 10 \text{ cm}^{-1}$ . The uncertainty in the values of the higher-lying levels is estimated to be  $\pm 100 \text{ cm}^{-1}$ .

The ionization energy is an extrapolated value by Lotz (1967).

## References

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## Cr VIII

Configuration	Term	J	Level (cm <sup>-1</sup> )	Configuration	Term	J	Level (cm <sup>-1</sup> )
$2s^2 3p^3$	$^2P$	$\frac{3}{2}$	0	$3s^2 3p^4 ({}^1D) 4s$	$^2D$	$\frac{3}{2}$	769 240
		$\frac{1}{2}$	9 892			$\frac{3}{2}$	769 550
$3s 3p^6$	$^2S$	$\frac{1}{2}$	242 065	$3s^2 3p^4 ({}^1S) 4s$	$^2S$	$\frac{1}{2}$	805 260
$3s^2 3p^4 ({}^1D) 3d$	$^2S$	$\frac{1}{2}$	461 540	$3s^2 3p^4 ({}^2P) 4d$	$^2D$	$\frac{3}{2}$	946 200
$3s^2 3p^4 ({}^2P) 3d$	$^2P$	$\frac{3}{2}$	479 310			$\frac{1}{2}$	947 300
$3s^2 3p^4 ({}^2P) 3d$		$^2D$	$\frac{3}{2}$	487 780	$3s^2 3p^4 ({}^1D) 4d$	$^2S$	$\frac{1}{2}$
	$\frac{3}{2}$		496 170	$\frac{3}{2}$			970 600
$3s^2 3p^4 ({}^2P) 4s$	$^4P$	$\frac{3}{2}$	735 880	$3s^2 3p^4 ({}^1D) 4d$	$^2P$	$\frac{3}{2}$	972 200
		$\frac{1}{2}$	741 060			$\frac{1}{2}$	976 100
$3s^2 3p^4 ({}^2P) 4s$	$^2P$	$\frac{3}{2}$	749 640	Cr IX ( ${}^2P_2$ )	Limit		1 490 000
		$\frac{1}{2}$	755 740				

## Cr IX

Z=24

S 1 isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^4 \ ^3P_2$ Ionization energy =  $1\ 688\ 000 \pm 3000\ \text{cm}^{-1}$  ( $209.3 \pm 0.4\ \text{eV}$ )

Edlén (1937) provided the initial spectral classifications by identifying the  $3p^4 - 3p^3 4s$  transitions. Both singlet and triplet levels were detected but not the connection between them.

Classifications in the  $3p^4 - 3p^3 3d$  transition array were made by Gabriel, Fawcett, and Jordan (1965) and by Fawcett and Gabriel (1966). Some new measurements were later provided by Fawcett (1971) as well as two newly classified lines of this group. The  $3s 3p^3$  configuration was found by Fawcett (1970). Classified lines of the  $3p^4 - 3p^3 4d$  and  $3p^3 3d - 3p^3 4f$  arrays were reported by Fawcett, Cowan, and Hayes (1972). The latter array could not be used to derive  $3p^3 4f$  levels because of the lack of transitions to known levels.

Smitt, Svensson, and Outred (1976) give improved measurements of the  $3s^2 3p^4 - 3s 3p^3$  transitions, obtaining an uncertainty of  $\pm 5\ \text{cm}^{-1}$  for the levels, except for the  $3s^2 3p^4 \ ^1S_0$  determined from a blended line. They also

found the intersystem line  $^3P_2 - ^1P_1$  and identified the  $^1S_0 - ^1P_1$  line. The uncertainty in the levels above the  $3s 3p^3$  configuration is  $\pm 100\ \text{cm}^{-1}$ .

The ionization energy is an extrapolated value by Lotz (1976).

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## Cr IX

Configuration	Term	J	Level (cm <sup>-1</sup> )	Configuration	Term	J	Level (cm <sup>-1</sup> )																																																																																										
$3s^2 3p^4$	$^3P$	2	0	$3s^2 3p^3(^3P^o) 3d$	$^1P^o$	1	531 880																																																																																										
		1	7 821			$3s^2 3p^3(^1S^o) 4s$	$^3S^o$	1	821 100																																																																																								
		0	9 549					$3s^2 3p^4$	$^1D$	2	30 284	$3s^2 3p^3(^3D^o) 4s$	$^3D^o$	1	845 900			2	846 260	$3s^2 3p^4$	$^1S$	0	66 855			3	847 870			$3s 3p^5$	$^3P^o$	2	239 068	$3s^2 3p^3(^3D^o) 4s$	$^1D^o$	2	854 790	1	245 317	$3s^2 3p^3(^3P^o) 4s$	$^1P^o$	1	881 810	0	249 016	$3s 3p^5$	$^1P^o$	1	305 561	$3s^2 3p^3(^1S^o) 4d$	$^3D^o$	2	1 028 500			3	1 028 900	$3s^2 3p^3(^3D^o) 3d$	$^3P^o$	2	454 510			1	1 029 100			$3s^2 3p^3(^3D^o) 3d$	$^1D^o$	2	499 310	$3s^2 3p^3(^3D^o) 4d$	$^1D^o$	2	1 066 800			$3s^2 3p^3(^1S^o) 3d$	$^3D^o$	3	474 790	$3s^2 3p^3(^3D^o) 4d$	$^1P^o$	3	1 070 100	2	479 570	$3s^2 3p^3 4d$	$^1P^o$	1	1 102 600	1	482 760	$3s^2 3p^3(^3D^o) 3d$	$^1P^o$	3	507 750
$3s^2 3p^4$	$^1D$	2	30 284	$3s^2 3p^3(^3D^o) 4s$	$^3D^o$	1	845 900																																																																																										
						2	846 260																																																																																										
$3s^2 3p^4$	$^1S$	0	66 855			3	847 870																																																																																										
						$3s 3p^5$	$^3P^o$	2	239 068	$3s^2 3p^3(^3D^o) 4s$	$^1D^o$	2	854 790	1	245 317	$3s^2 3p^3(^3P^o) 4s$	$^1P^o$	1	881 810	0	249 016	$3s 3p^5$	$^1P^o$	1	305 561	$3s^2 3p^3(^1S^o) 4d$	$^3D^o$	2	1 028 500			3	1 028 900	$3s^2 3p^3(^3D^o) 3d$	$^3P^o$	2	454 510			1	1 029 100			$3s^2 3p^3(^3D^o) 3d$	$^1D^o$	2	499 310	$3s^2 3p^3(^3D^o) 4d$	$^1D^o$	2	1 066 800			$3s^2 3p^3(^1S^o) 3d$	$^3D^o$	3	474 790	$3s^2 3p^3(^3D^o) 4d$	$^1P^o$	3	1 070 100	2	479 570	$3s^2 3p^3 4d$	$^1P^o$	1	1 102 600	1	482 760	$3s^2 3p^3(^3D^o) 3d$	$^1P^o$	3	507 750	Cr X ( $^4S_{3/2}$ )	Limit		1 688 000																				
$3s 3p^5$	$^3P^o$	2	239 068	$3s^2 3p^3(^3D^o) 4s$	$^1D^o$			2	854 790																																																																																								
		1	245 317					$3s^2 3p^3(^3P^o) 4s$	$^1P^o$			1	881 810																																																																																				
		0	249 016			$3s 3p^5$	$^1P^o$			1	305 561	$3s^2 3p^3(^1S^o) 4d$	$^3D^o$	2	1 028 500			3	1 028 900	$3s^2 3p^3(^3D^o) 3d$	$^3P^o$	2	454 510			1	1 029 100			$3s^2 3p^3(^3D^o) 3d$	$^1D^o$	2	499 310	$3s^2 3p^3(^3D^o) 4d$	$^1D^o$	2	1 066 800			$3s^2 3p^3(^1S^o) 3d$	$^3D^o$	3	474 790	$3s^2 3p^3(^3D^o) 4d$	$^1P^o$	3	1 070 100	2	479 570	$3s^2 3p^3 4d$	$^1P^o$	1	1 102 600	1	482 760	$3s^2 3p^3(^3D^o) 3d$	$^1P^o$	3	507 750	Cr X ( $^4S_{3/2}$ )	Limit		1 688 000																																		
$3s 3p^5$	$^1P^o$	1	305 561	$3s^2 3p^3(^1S^o) 4d$	$^3D^o$			2	1 028 500																																																																																								
						3	1 028 900																																																																																										
$3s^2 3p^3(^3D^o) 3d$	$^3P^o$	2	454 510			1	1 029 100																																																																																										
						$3s^2 3p^3(^3D^o) 3d$	$^1D^o$	2	499 310	$3s^2 3p^3(^3D^o) 4d$	$^1D^o$	2	1 066 800			$3s^2 3p^3(^1S^o) 3d$	$^3D^o$	3	474 790	$3s^2 3p^3(^3D^o) 4d$	$^1P^o$	3	1 070 100	2	479 570	$3s^2 3p^3 4d$	$^1P^o$	1	1 102 600	1	482 760	$3s^2 3p^3(^3D^o) 3d$	$^1P^o$	3	507 750	Cr X ( $^4S_{3/2}$ )	Limit		1 688 000																																																										
$3s^2 3p^3(^3D^o) 3d$	$^1D^o$	2	499 310	$3s^2 3p^3(^3D^o) 4d$	$^1D^o$			2	1 066 800																																																																																								
						$3s^2 3p^3(^1S^o) 3d$	$^3D^o$	3	474 790	$3s^2 3p^3(^3D^o) 4d$	$^1P^o$	3	1 070 100	2	479 570			$3s^2 3p^3 4d$	$^1P^o$			1	1 102 600	1	482 760	$3s^2 3p^3(^3D^o) 3d$	$^1P^o$	3	507 750	Cr X ( $^4S_{3/2}$ )	Limit		1 688 000																																																																
$3s^2 3p^3(^1S^o) 3d$	$^3D^o$	3	474 790	$3s^2 3p^3(^3D^o) 4d$	$^1P^o$			3	1 070 100																																																																																								
		2	479 570					$3s^2 3p^3 4d$	$^1P^o$			1	1 102 600																																																																																				
		1	482 760			$3s^2 3p^3(^3D^o) 3d$	$^1P^o$			3	507 750	Cr X ( $^4S_{3/2}$ )	Limit		1 688 000																																																																																		
$3s^2 3p^3(^3D^o) 3d$	$^1P^o$	3	507 750	Cr X ( $^4S_{3/2}$ )	Limit				1 688 000																																																																																								

## Cr x

Z=24

P 1 isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^3 {}^4S_{3/2}$ Ionization energy =  $1\,971\,000 \pm 4000 \text{ cm}^{-1}$  ( $244.4 \pm 0.5 \text{ eV}$ )

The levels of  $3s3p^4$  are due to Smitt, Svensson, and Outred (1976) who gave improved measurements and additional classifications in the  $3s^2 3p^3 - 3s3p^4$  array, previously interpreted by Fawcett and Peacock (1967) and by Fawcett (1970). The important  ${}^4S - {}^2P$  forbidden lines of the  $3s^2 3p^3$  configuration, which unify the term systems, were identified by Feldman and Doschek (1976) in solar coronal spectra. The uncertainty in these level values is  $\pm 5 \text{ cm}^{-1}$ . Transitions from  $3p^2 3d$  to the ground configuration were identified by Gabriel, Fawcett, and Jordan (1966), Fawcett, Gabriel, and Saunders (1967), and most completely by Fawcett (1970). The level value uncertainty is  $\pm 100 \text{ cm}^{-1}$ . Lines of the  $3s^2 3p^3 - 3s^2 3p^2 4s$  array were classified by Fawcett, Cowan, and Hayes (1972), giving a level uncertainty of  $\pm 300 \text{ cm}^{-1}$ . These authors also identified lines arising from the  $3p^2 4f$

configuration but the lower levels have not been determined.

The ionization energy was obtained by Lotz (1967) by extrapolation.

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## Cr x

Configuration	Term	J	Level (cm <sup>-1</sup> )	Configuration	Term	J	Level (cm <sup>-1</sup> )
$3s^2 3p^3$	${}^4S$	$\frac{3}{2}$	0	$3s^2 3p^2 ({}^1D) 3d$	${}^2D$	$\frac{5}{2}$ $\frac{3}{2}$	476 680 476 820
$3s^2 3p^3$	${}^2D$	$\frac{3}{2}$ $\frac{5}{2}$	37 103 39 450	$3s^2 3p^2 ({}^1D) 3d$	${}^2P$	$\frac{1}{2}$ $\frac{3}{2}$	491 650 496 430
$3s^2 3p^3$	${}^2P$	$\frac{1}{2}$ $\frac{3}{2}$	63 935 67 157	$3s^2 3p^2 ({}^3P) 3d$	${}^2P$	$\frac{1}{2}$	500 880
$3s3p^4$	${}^4P$	$\frac{5}{2}$ $\frac{3}{2}$ $\frac{1}{2}$	233 890 239 987 242 922	$3s^2 3p^2 ({}^3P) 3d$	${}^2D$	$\frac{5}{2}$ $\frac{3}{2}$ $\frac{1}{2}$	519 280 520 820
$3s3p^4$	${}^2D$	$\frac{3}{2}$ $\frac{5}{2}$	289 637 290 606	$3s^2 3p^2 ({}^3P) 4s$	${}^4P$	$\frac{1}{2}$ $\frac{3}{2}$ $\frac{5}{2}$	928 500 933 400 939 100
$3s3p^4$	${}^2P$	$\frac{3}{2}$ $\frac{1}{2}$	333 412 337 370	$3s^2 3p^2 ({}^3P) 4s$	${}^2P$	$\frac{1}{2}$ $\frac{3}{2}$	943 300 949 800
$3s3p^4$	${}^2S$	$\frac{1}{2}$	348 760	$3s^2 3p^2 ({}^1D) 4s$	${}^2D$	$\frac{5}{2}$ $\frac{3}{2}$	967 000 967 800
$3s^2 3p^2 ({}^3P) 3d$	${}^2P$	$\frac{3}{2}$ $\frac{1}{2}$	432 830 440 870				
$3s^2 3p^2 ({}^3P) 3d$	${}^4P$	$\frac{5}{2}$ $\frac{3}{2}$ $\frac{1}{2}$	442 010 444 960 446 710	Cr XI ( ${}^2P_0$ )	Limit		1 971 000

## Cr XI

Z = 24

Si I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^3 {}^4P_0$ Ionization energy =  $2\,184\,000 \pm 4000 \text{ cm}^{-1}$  ( $270.8 \pm 0.5 \text{ eV}$ )

Fawcett (1970, 1971) gave the first interpretation of the  $3s^2 3p^2 - 3s 3p^3$  array. The level values were later revised by Smitt, Svensson, and Outred (1976) on the basis of their more accurate measurements with an estimated uncertainty of  $\pm 0.008 \text{ \AA}$  or better. The connection between the singlet and triplet systems results from this later work and from the solar coronal line at  $3996.8 \text{ \AA}$  (air) identified by Jefferies (1969) as arising from the forbidden  ${}^1D_2 - {}^3P_2$  transition in  $3s^2 3p^2$ . The uncertainty in these level values is estimated to be  $\pm 5 \text{ cm}^{-1}$ .

The levels of  $3s^2 3p 3d$  are from Fawcett (1971). Those of  $3s^2 3p 4s$  and the  ${}^1D_1$  and  ${}^1F_3$  of  $3s^2 3p 4d$  are due to Fawcett, Cowan, and Hayes (1972). In table I of this reference the line given as  $98.48 \text{ \AA}$  must be changed to  $99.48 \text{ \AA}$  to fit its classification. Kastner et al. (1978) added

to the known levels of  $3s^2 3p 4d$  and the  ${}^1G$  of  $3s^2 3p 4f$ . The uncertainty in the  $3d$  level values is  $\pm 100 \text{ cm}^{-1}$  and for the others  $300 \text{ cm}^{-1}$ .

The ionization energy was obtained by Lotz (1967) by extrapolation.

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## Cr XI

Configuration	Term	J	Level (cm <sup>-1</sup> )	Configuration	Term	J	Level (cm <sup>-1</sup> )		
$3s^2 3p^2$	${}^3P$	0	0	$3s^2 3p 3d$	${}^3D$	1	434 240		
		1	5 536			2	436 210		
		2	11 980			3	436 550		
$3s^2 3p^2$	${}^1D$	2	36 994	$3s^2 3p 3d$	${}^1F$	3	478 590		
$3s 3p^3$	${}^3D$	1	242 346	$3s^2 3p 4s$	${}^3P$	0	1 008 800		
		2	242 456			1	1 010 700		
		3	243 916			2	1 021 100		
$3s 3p^3$	${}^3P$	0	278 059	$3s^2 3p 4s$	${}^1P$	1	1 028 100		
		1	278 394			$3s^2 3p 4d$	${}^3D$	1	1 234 300
		2	278 698					2	1 236 600
$3s 3p^3$	${}^1D$	2	306 570			3	1 237 900		
$3s 3p^3$	${}^3S$	1	356 424	$3s^2 3p 4d$	${}^3F$	3	1 243 800		
$3s 3p^3$	${}^1P$	1	372 498	$3s^2 3p 4d$	${}^1F$	3	1 255 500		
$3s^2 3p 3d$	${}^3P$	2	418 980	$3s^2 3p 4f$	${}^1G$	4	1 347 200		
		1	425 480						
$3s^2 3p 3d$	${}^1D$	2	427 090	Cr XII ( ${}^3P_{1,2}$ )	Limit		2 184 000		

## Cr XII

Z=24

Al I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 3p^2 P_{1/2}$ Ionization energy =  $2\,404\,000 \pm 5000 \text{ cm}^{-1}$  ( $298.0 \pm 0.6 \text{ eV}$ )

The  $3p-4d$  doublet was identified by Edlén (1936). Thirty years later new observations of this spectrum by Gabriel, Fawcett, and Jordan (1966) resulted in the discovery of the  $3p-3d$  doublet. The non-diagonal line of this multiplet was identified by Fawcett, Gabriel, and Saunders (1967) by means of a laser-produced plasma. The uncertainty in the  $3d$  and  $4d$  level values is  $\pm 100 \text{ cm}^{-1}$ .

The  $^2P$  and  $^2D$  terms of the low-lying  $3s3p^2$  configuration were first reported by Fawcett and Peacock (1967) again utilizing a laser plasma. Fawcett (1970) revised the classification of the  $3s^2 3p^2 P^o - 3s3p^2 D$  multiplet and added the  $^2P^o - ^2S$  lines. He also reported the  $^4P - ^4S^o$  lines of the  $3s3p^2 - 3p^3$  array. The quartet term position relative to the doublet system is not observed or predicted and therefore cannot be included here.

Fawcett (1971) later revised the wavelengths of the  $3s^2 3p - 3s3p^2$  array from new plates taken with the theta pinch source. His value of  $412.46 \text{ \AA}$  for the  $^2P_{1/2}^o - ^2D_{1/2}$  line is inconsistent with the  $^2P_{1/2}^o - ^2D_{1/2}$  principal line and was not used here. He also reported the  $3p-3d$  doublet of the same array. Calculated wavelengths enabled Fawcett, Cowan, Kononov, and Hayes (1972) to identify more

lines from the theta pinch spectrum. They classified the  $3d-4f$  doublet and several quartet transitions unconnected with the doublets. The uncertainty of the level values of  $3s3p^2$  is  $\pm 50 \text{ cm}^{-1}$ .

The ground term  $^2P^o$  splitting is obtained from the solar coronal line  $8153.8 \text{ \AA}$  classified by Jefferies (1969) and has an uncertainty of  $\pm 1 \text{ cm}^{-1}$ .

The value for the ionization energy was obtained by extrapolation by Lotz (1967).

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## Cr XII

Configuration	Term	J	Level (cm <sup>-1</sup> )	Configuration	Term	J	Level (cm <sup>-1</sup> )
$3s^2 3p$	$^2P^o$	$1/2$	0	$3s^2 4d$	$^2D$	$3/2$	1 319 000
		$3/2$	12 261			$5/2$	1 319 660
$3s3p^2$	$^2D$	$3/2$	254 450	$3s^2 4f$	$^2F^o$	$5/2$	1 395 000
		$5/2$	255 620			$7/2$	1 395 400
$3s3p^2$	$^2S$	$1/2$	313 600	Cr XIII ( $^1S_0$ )	Limit		2 404 000
$3s3p^2$	$^2P$	$1/2$	333 240				
		$3/2$	339 250				
$3s^2 3d$	$^2D$	$3/2$	408 700				
		$5/2$	409 840				



## Cr XIII

Z=24

Mg I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 1S_0$ Ionization energy =  $2\,862\,000 \pm 6000\text{ cm}^{-1}$  ( $354.8 \pm 0.7\text{ eV}$ )

The  $3s^2 1S_0 - 3s 4p^1 P_1^o$  resonance line was identified by Edlén (1936). He also reported two unconnected triplet systems, one containing levels of  $3s 3p$ ,  $3s 4s$ ,  $3s 4d$ , and  $3s 5d$ , and the other  $3s 3d$ ,  $3s 4f$ , and  $3s 5f$ . The analysis was resumed 30 years later by Fawcett, Gabriel, and Saunders (1967) who unified the triplets by discovering the  $3s 3p^1 P^o - 3s 3d^1 D$  multiplet. They also identified the resonance line  $3s^2 1S_0 - 3s 3p^1 P_1^o$  at  $328.29 \pm 0.03\text{ \AA}$ . The intersystem transition  $3s^2 1S_0 - 3s 3p^1 P_1^o$  was observed at  $482.2 \pm 0.2\text{ \AA}$  in a tokamak plasma by Finkenthal, Bell, and Moos (1982). These two lines were measured in a tokamak plasma by Peacock, Stamp, and Silver (1984), who obtained the more accurate values of  $328.267 \pm 0.004\text{ \AA}$  and  $482.17 \pm 0.02\text{ \AA}$ , or level uncertainties of  $\pm 4$  and  $\pm 9\text{ cm}^{-1}$ . The uncertainties in the rest of the levels of the above configurations is  $\pm 100\text{ cm}^{-1}$ .

The analysis was extended to  $3p^2$  by Fawcett and Peacock (1967) who identified the  $3s 3p^1 P^o - 3p^2 1P$  multiplet. Fawcett (1970) later found the  $1S_0$  of  $3p^2$ , the  $1D_2$  of  $3s 3d$  and all the levels of  $3p 3d$  presently known. The uncertainty of these level values is  $\pm 100\text{ cm}^{-1}$ .

The analysis was augmented by Fawcett, Cowan, Kononov, and Hayes (1972) with their identification of

transitions from  $3s 4f^1 F_3$ ,  $3s 4d^1 D_2$ , and levels of  $3p 4f$ . Some of the last group are not connected to known levels and are therefore not used here.

Improved measurements of the  $3s 3p^1 P^o - 3s 3d^1 D$  multiplet were made by Fawcett, Cowan, and Hayes (1972). In addition, they reported the  $1D_2$  of  $3s 3d$  and the  $1D_2$  of  $3p^2$ .

The ionization energy is an extrapolated value obtained by Lotz (1967).

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## Cr XIII

Configuration	Term	J	Level (cm <sup>-1</sup> )	Configuration	Term	J	Level (cm <sup>-1</sup> )
$3s^2$	$1S$	0	0	$3p 3d$	$3P^o$	2	805 220
$3s 3p$	$3P^o$	0	203 470			3	811 550
		1	207 400			4	818 910
		2	216 590	$3p 3d$	$3P^o$	2	857 220
$3s 3p$	$1P^o$	1	304 630	$3p 3d$	$3D^o$	3	861 010
$3p^2$	$3P$	0	482 160	$3p 3d$	$1P^o$	1	885 300
		1	488 250	$3s 4s$	$3S$	1	1 385 290
		2	499 220	$3s 4p$	$1P^o$	1	1 492 920
$3p^2$	$1D$	2	483 170	$3s 4d$	$3D$	1	1 616 060
$3p^2$	$1S$	0	569 460			2	1 616 460
$3s 3d$	$3D$	1	588 580			3	1 617 190
		2	589 210	$3s 4d$	$1D$	2	1 617 500
		3	590 100	$3s 4f$	$3F^o$	2	1 678 240
$3s 3d$	$1D$	2	662 240			3	1 678 630
						4	1 678 770

## E-60

## Cr XIII—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )
3s4f	<sup>1</sup> F <sup>o</sup>	3	1 690 800	3s5d	<sup>3</sup> D	2	2 076 350
3p4f	<sup>1</sup> F	3	1 916 140			3	2 076 540
3p4f	<sup>3</sup> G	4	1 920 560	3s5f	<sup>3</sup> F <sup>o</sup>	4	2 105 990
		5	1 930 140	Cr XIV ( <sup>2</sup> S <sub>1,2</sub> )	<i>Limit</i>		2 862 000
3p4f	<sup>3</sup> F	4	1 931 440				
3p4f	<sup>3</sup> D	3	1 940 840				

## Cr XIV

Z=24

Na I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 3s^2 S_{1/2}$ Ionization energy =  $3\,098\,520 \pm 200$  ( $384.171 \pm 0.020$  eV)

Edlén (1936) reported three independent systems of doublets:  $3s-np$ ,  $3p-nd$  (and  $3p-4s$ ), and  $3d-nf$ . These were unified by Fawcett and Peacock (1967) who identified the  $3s-3p$  and  $3p-3d$  doublets. New observations by Peacock, Stamp, and Silver (1984) of the  $3s-3p$  doublet in a tokamak plasma were reported at  $389.804$  and  $412.051$  Å. We use these and the improved values for the  $3p-3d$  doublet by Edlén (1978). The  $4s$ ,  $4p$ ,  $4d$ ,  $4f$ ,  $5d$ ,  $5f$ , and  $6f(^2F_{7/2})$  terms are from the identifications and measurements of Edlén (1936). The uncertainty of the  $n=3$  levels is  $\pm 5$   $\text{cm}^{-1}$ , and the higher ones  $\pm 200$   $\text{cm}^{-1}$ .

The additional series members  $5s-6s$ ,  $6p-9p$ ,  $6d-9d$ , and  $7f-8f$  were identified by Fawcett, Cowan, and Hayes (1972). Improved measurements by Cohen and Behring (1976) in the range of  $35-70$  Å were used. They estimate their measurement uncertainty to be  $\pm 0.005$  Å

although their measurements differ from those of Edlén (1936) by about  $+0.02$  Å. The  $2p^3 3s^2 2^2P^o$  term was found by Feldman and Cohen (1967).

The value for the ionization energy was derived by Edlén (1978) from core polarization theory applied to the  $nf$  series.

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## Cr XIV

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Configuration	Term	J	Level ( $\text{cm}^{-1}$ )
$2p^6 3s$	$^2S$	$1/2$	0	$2p^6 6s$	$^2S$	$1/2$	2 424 470
$2p^6 3p$	$^2P^o$	$1/2$	242 688	$2p^6 6p$	$^2P^o$	$1/2$	2 450 990
		$3/2$	256 500			$3/2$	2 452 060
$2p^6 3d$	$^3D$	$3/2$	587 810	$2p^6 6d$	$^3D$	$3/2$	2 484 990
		$5/2$	589 505			$5/2$	2 485 240
$2p^6 4s$	$^2S$	$1/2$	1 478 580	$2p^6 6f$	$^3F^o$	$5/2$	2 499 090
$2p^6 4p$	$^2P^o$	$1/2$	1 574 180			$7/2$	2 499 260
		$3/2$	1 579 550	$2p^6 7s$	$^2S$	$1/2$	2 612 050
$2p^6 4d$	$^3D$	$3/2$	1 701 150			$3/2$	2 649 530
		$5/2$	1 701 940	$2p^6 7f$	$^3F^o$	$5/2$	2 658 200
$2p^6 4f$	$^3F^o$	$5/2$	1 749 890			$7/2$	2 658 270
		$7/2$	1 750 080	$2p^6 8p$	$^2P^o$	$3/2, 5/2$	2 742 280
$2p^6 5s$	$^2S$	$1/2$	2 102 780	$2p^6 8d$	$^3D$	$3/2$	2 755 510
$2p^6 5p$	$^2P^o$	$1/2$	2 149 290			$5/2$	2 755 380
		$3/2$	2 152 020	$2p^6 8f$	$^3F^o$	$7/2$	2 761 580
$2p^6 5d'$	$^3D$	$3/2$	2 210 730	$2p^6 9p$	$^2P^o$	$3/2, 5/2$	2 820 870
		$5/2$	2 211 080				
$2p^6 5f$	$^2F^o$	$3/2$	2 235 280				
		$7/2$	2 235 440				

## Cr xiv—Continued

Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )	Configuration	Term	<i>J</i>	Level (cm <sup>-1</sup> )
2p <sup>6</sup> 9d	<sup>3</sup> D	$\frac{3}{2}$	2 827 260				
		$\frac{1}{2}$	2 828 070				
Cr xv <sup>1</sup> S <sub>0</sub>	<i>Limit</i>		3 098 520				
2p <sup>6</sup> 3d <sup>2</sup>	<sup>3</sup> P	$\frac{3}{2}$	4 593 500				
		$\frac{1}{2}$	4 658 300				

## Cr xv

Z = 24

Ne I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^6 {}^1S_0$ Ionization energy  $8\,151\,000 \pm 5000 \text{ cm}^{-1}$  ( $1010.6 \pm 0.6 \text{ eV}$ )

Only resonance lines are classified for this ion. Tyrén (1938) identified the lines due to the  $2s^2 2p^3 3s$ ,  $3d$  and  $4d$  as well as the  $2s 2p^4 3p$  levels. Swartz, Kastner, Rothe, and Neupert (1971) identified  $5d$ , and  $6d$ . The magnetic quadrupole transition  $2p^5 {}^1S_0 - 2p^3 3s {}^3P_2^o$  was identified in the spectrum of a tokamak plasma by Klapisch et al. (1978). They confirm the wavelengths of Tyrén for  $2p^3 3s {}^3P_1$  and  ${}^1P_1$  and  $2p^3 3d {}^1D_2$  to within  $\pm 0.003 \text{ \AA}$ , but give the value  $18.488 \text{ \AA}$  for  $2p^3 3d {}^1P_1$ , compared with Tyrén's value of  $18.497 \text{ \AA}$  used here. The uncertainty in the level values is estimated to be  $\pm 2000 \text{ cm}^{-1}$ .

Kastner, Behring, and Cohen (1975) identified transitions between  $2p^3 3p$  and  $2p^3 4d$  but there is no connection with known levels.

The percentage compositions were calculated by Bogdanovich et al. (1980).

We derived the ionization energy from the  $2s^2 2p^3 nd {}^1D_2^o$  series for  $n = 3, 4, 5$ . The  $n = 6$  term does not fit well to a series calculation.

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## Cr xv

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$2s^2 2p^6$	${}^1S$	0	0			
$2s^2 2p^5 3s$	${}^3P$	2	4 714 100	100		
		1	4 727 500	50	50	${}^1P^o$
$2s^2 2p^5 3s$	${}^1P^o$	1	4 793 300	50	50	${}^3P^o$
$2s^2 2p^5 3d$	${}^3P^o$	1	5 259 000	94		
$2s^2 2p^5 3d$	${}^1D^o$	1	5 324 300	93	12	${}^1P^o$
$2s^2 2p^5 3d$	${}^3P^o$	1	5 406 900	96		
$2s 2p^6 3p$	${}^3P^o$	1	5 894 500	92	n	${}^1P^o$
$2s 2p^6 3p$	${}^1P^o$	1	5 921 000	92	n	${}^3P^o$
$2s^2 2p^4 4d$	${}^3D^o$	1	6 576 000	59	41	${}^1P^o$
$2s^2 2p^4 4d$	${}^1P^o$	1	6 641 000	50	34	${}^3D^o$
$2s^2 2p^4 5d$	${}^3D^o$	1	7 148 000			
$2s^2 2p^4 5d$	${}^1P^o$	1	7 215 000			
$2s^2 2p^4 6d$	${}^3D^o$	1	7 452 000			
$2s^2 2p^4 6d$	${}^1P^o$	1	7 524 000			
Cr xvi ( ${}^1P^o_{1/2}$ )	Limit		8 151 000			

## Cr XVI

Z = 24

F I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^4 \ ^3P_1^o$ Ionization energy =  $8\,850\,000 \pm 18\,000\text{ cm}^{-1}$  ( $1097 \pm 2\text{ eV}$ )

The ground term splitting was obtained by Fawcett (1971) from his identification of the  $2s^2 2p^4 - 2s 2p^5$  doublet. It was observed directly from a magnetic dipole transition at  $1410.6 \pm 0.3\text{ \AA}$  in a tokamak discharge by Hinnov et al. (1982). The present value is taken in the more accurate measurement of  $1410.60 \pm 0.02\text{ \AA}$  by Peacock, Stamp, and Silver (1984) in a similar light source, giving an uncertainty of  $2\text{ cm}^{-1}$  for this interval. The  $2s 2p^5 \ ^3S_1^o$  from the measurements of the resonance doublet by Doschek et al. (1974), and has an uncertainty of  $\pm 200\text{ cm}^{-1}$ .

The  $2s^2 2p^2 - 2s^2 2p^4 3s$  and  $3d$  arrays were first analyzed by Cohen, Feldman and Kastner (1968). This work was revised and extended by Feldman et al. (1973) from whose classified lines we derived the energy levels. Their reported wavelength accuracy is  $\pm 0.01\text{ \AA}$ . The consequent level uncertainty is  $\pm 6000\text{ cm}^{-1}$ .

The  $2s 2p^5 \ ^3S_1^o - 2s 2p^5 \ ^3P^o$  multiplet is from Feldman et al. (1973).

Bogdanovich et al. (1980) calculated the percentage compositions of the levels.

The ionization energy was obtained by extrapolation by Lotz (1967).

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## Cr XVI

Configuration	Term	J	Level (cm <sup>-1</sup> )	Leading percentages		
$2s^2 2p^4$	$^3P^o$	$3/2$	0			
		$1/2$	70 892			
$2s 2p^5$	$^3S$	$1/2$	937 940			
$2s^2 2p^4 \ ^1P^o 3s$	$^1P$	$3/2$	5 048 700	94		
		$1/2$	5 072 300	56	42	( $^3P$ ) $^2P$
		$3/2$	5 109 300	94		
$2s^2 2p^4 \ ^1P^o 3s$	$^3P$	$3/2$	5 118 200	49	44	( $^3P$ ) $^4P$
		$1/2$	5 143 400	94		
$2s^2 2p^4 \ ^1D^o 3s$	$^3D$	$3/2$	5 193 500	94		
		$1/2$	5 196 100	90		
$2s^2 2p^4 \ ^1S^o 3s$	$^3S$	$1/2$	5 323 500	90		
$2s^2 2p^4 \ ^3P^o 3d$	$^4P$	$1/2$	5 607 600	72	13	( $^3P$ ) $^2P$
		$3/2$	5 620 600	64	18	( $^3P$ ) $^2D$
		$1/2$	5 640 200	37	34	( $^3P$ ) $^4F$
$2s^2 2p^4 \ ^1P^o 3d$	$^4P$	$3/2$	5 622 700	48	21	( $^3P$ ) $^2P$
$2s^2 2p^4 \ ^1P^o 3d$	$^4P$	$1/2$	5 628 500	42	32	( $^3P$ ) $^4D$
		$3/2$	5 671 200	52	23	( $^1D$ ) $^4P$
$2s^2 2p^4 \ ^3P^o 3d$	$^4D$	$3/2$	5 648 100	28	17	( $^1D$ ) $^2D$
		$1/2$	5 680 800	49	17	

## Cr XVI—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Landig percentages		
$2s^2 2p^4 ({}^3P) 3d$	${}^3P$	$\frac{3}{2}$	5 659 000	65	35	( ${}^3P$ ) ${}^3P$
$2s^2 2p^4 ({}^1D) 3d$	${}^3S$	$\frac{1}{2}$	5 734 600	90		
$2s^2 2p^4 ({}^1D) 3d$	${}^3P$	$\frac{3}{2}$	5 756 200	67	24	( ${}^3P$ ) ${}^3P$
$2s^2 2p^4 ({}^1D) 3d$	${}^3D$	$\frac{3}{2}$	5 757 100	56	25	( ${}^3P$ ) ${}^3D$
		$\frac{3}{2}$	5 780 500	65	28	
$2s^2 2p^4 ({}^1S) 3d$	${}^1D$	$\frac{3}{2}$	5 857 200	90		
		$\frac{3}{2}$	5 870 600	83		
$2s 2p^5 ({}^3P) 3s$	${}^3P$	$\frac{3}{2}$	5 950 200	83		
		$\frac{1}{2}$	5 985 600	90		
Cr XVII ( ${}^3P_2$ )	<i>Limit</i>		8 850 000			

## Cr xvii

Z = 24

O I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^4 \ ^3P_2$ Ionization energy =  $9\,560\,000 \pm 19\,000 \text{ cm}^{-1}$  ( $1185 \pm 2 \text{ eV}$ )

Several magnetic dipole transitions within the  $2s^2 2p^4$  ground configuration were observed by Hinnov et al. (1982) in a tokamak light source with an accuracy of  $\pm 0.3 \text{ \AA}$ . They are  $^3P_2 - ^1P_1$  at  $1656.3 \text{ \AA}$ ,  $^3P_2 - ^1D_2$  at  $740.8 \text{ \AA}$  and  $^3P_1 - ^1S_0$  at  $493.8 \text{ \AA}$ . The  $^3P_1$ ,  $^1D_2$ , and  $^1S_0$  levels are derived from these data. Peacock, Stamp, and Silver (1984) obtained the value  $740.75 \pm 0.03 \text{ \AA}$  for the  $^3P_2 - ^1D_2$  in a similar light source. The  $2s^2 2p^4 - 2s 2p^5$  array was first interpreted by Fawcett (1971). It was reobserved by Lawson and Peacock (1980) who extended the analysis. The  $2s 2p^5 \ ^1P_1 - 2p^6 \ ^1S_0$  transition was identified by Doschek et al. (1975). Both lines of this array were observed by Lawson and Peacock. Their measurements are used here to derive the levels of  $2s 2p^5$ ,  $2p^6$  and the  $^3P_0$  of  $2s^2 2p^4$  with an uncertainty of  $\pm 300 \text{ cm}^{-1}$ . The percentage composition of these levels was provided by Kaufman and Sugar (1982). Their calculation includes configuration interaction between  $2s^2 2p^4$  and  $2p^6$ .

The transition array  $2s^2 2p^4 - 2s^2 2p^3 3s$  and  $18 \text{ \AA}$  was analyzed by Doschek, Feldman, and Cohen (1973), and the  $2s^2 2p^4 - 2s^2 2p^3 3d$  at  $16 \text{ \AA}$  by Fawcett and Hayes (1975). Both report a measurement uncertainty of  $\pm 0.01 \text{ \AA}$ , resulting in level uncertainties of  $\pm 3000 \text{ cm}^{-1}$ . Levels of  $2p^5 3s$  with question marks were derived from doubly

classified lines by Doschek et al. (1973). Some revisions of the  $2p^5 3d$  levels due to Bromage and Fawcett (1977) are included.

The two levels of  $2p^5 4d$  are from Spector et al. (1980) with an uncertainty of  $\pm 3000 \text{ cm}^{-1}$ .

The value for the ionization energy was derived by Lotz (1967) by extrapolation.

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## Cr xvii

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$2s^2 2p^4$	$^3P$	2	0	93	7	$^1D$
		0	58 070	86	13	$^1S$
		1	60 376	100		
$2s^2 2p^4$	$^1D$	2	134 998	93	7	$^3P$
$2s^2 2p^4$	$^1S$	0	262 890	84	14	$^3P$
$2s 2p^5$	$^3P^o$	2	813 540	100		
		1	858 120	98	2	$^1P^o$
		0	887 920	100		
$2s 2p^5$	$^1P^o$	1	1 116 380	98	2	$^3P^o$
$2p^6$	$^1S$	0	1 886 920	98	2	$2s^2 2p^4 \ ^1S$
$2s^2 2p^3 \ ^4S^o \ ^3s$	$^4S^o$	1	5 455 000?			
$2s^2 2p^3 \ ^2D^o \ ^3s$	$^2D^o$	1	5 546 800?			
		2	5 549 400			
		3	5 568 900			



## Cr XVII—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Leading percentages
$2s^2 2p^5 \text{ } ^1\text{D}^o 3s$	$^1\text{D}^o$	2	5 588 700?	
$2s^2 2p^5 \text{ } ^3\text{P}^o 3s$	$^3\text{P}^o$	1	5 700 700	
$2s^2 2p^5 \text{ } ^1\text{S}^o 3d$	$^1\text{D}^o$	3	5 948 500	
$2s^2 2p^5 \text{ } ^1\text{D}^o 3d$	$^1\text{D}^o$	2	6 070 000	
		3	6 074 000	
$2s^2 2p^5 \text{ } ^3\text{D}^o 3d$	$^3\text{F}^o$	3	6 124 400	
$2s^2 2p^5 \text{ } ^3\text{P}^o 3d$	$^3\text{P}^o$	2	6 131 000	
$2s^2 2p^5 \text{ } ^3\text{P}^o 3d$	$^1\text{D}^o$	3	6 164 800	
		1	6 189 000	
		2	6 214 600	
$2s^2 2p^5 \text{ } ^1\text{P}^o 3d$	$^3\text{F}^o$	3	6 338 000	
$2s^2 2p^5 \text{ } ^3\text{P}^o 4d$	$^1\text{D}^o$	2	7 882 000	
$2s^2 2p^5 \text{ } ^3\text{P}^o 4d$	$^3\text{F}^o$	3	7 960 000	
Cr XVIII $^1\text{S}^o_2$	<i>Limit</i>		9 560 000	

## Cr xviii

Z = 27

N 1 isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^4 \text{ } ^4\text{S}^{\circ}_3$ Ionization energy =  $10\,480\,000 \pm 21\,000 \text{ cm}^{-1}$  ( $1299 \pm 3 \text{ eV}$ )

Four lines of the  $2s^2 2p^3 \text{ } ^3\text{D}^{\circ} - 2s 2p^4 \text{ } (^4\text{P}, ^3\text{D})$  multiplets were classified by Fawcett (1971). The analysis of this transition array was extended and partly revised by Doschek, Feldman, Cowan, and Cohen (1974). The  $^4\text{S}^{\circ}_3$  of  $2s 2p^4$  was later reported by Feldman, Doschek, Cowan, and Cohen (1975). Fawcett and Hayes (1975) classified the resonance line arising from  $2s^2 2p^3 \text{ } (^3\text{P}) 3d \text{ } ^4\text{P}^{\circ}_3$  and observed the  $2s^2 2p^3 \text{ } (^3\text{D}) 3d \text{ } ^2\text{F}^{\circ}_3$  level of the doublet system. They also located the  $2p^5$  configuration from transitions to  $2s 2p^4 \text{ } ^3\text{D}$ . The  $^3\text{D}^{\circ}_3 - ^3\text{P}^{\circ}_2$  line of this multiplet was reported by Doschek, Feldman, Davis, and Cowan (1975).

The  $2s^2 2p^3 - 2s 2p^4$  and  $2s 2p^4 - 2p^5$  arrays were re-measured by Lawson and Peacock (1980) who found four intersystem lines. We used their wavelengths, accurate to  $\pm 0.03 \text{ \AA}$ , to determine the energy levels with an uncertainty of  $\pm 200 \text{ cm}^{-1}$ . Magnetic dipole transitions within the ground configuration were observed in a tokamak plasma by Hinnov, Suckewer, Cohen, and Sato (1982). They reported privately the wavelengths  $4038.6 \text{ \AA}$  for  $^3\text{D}^{\circ}_3 - ^3\text{D}^{\circ}_3$  and  $2606.4 \text{ \AA}$  for  $^3\text{P}^{\circ}_2 - ^3\text{P}^{\circ}_2$ , both in air with uncertainties of  $\pm 0.3 \text{ \AA}$ . With these measurements and their published wavelength of  $793.3 \text{ \AA}$  for the

$^4\text{S}^{\circ}_3 - ^3\text{D}^{\circ}_3$  transition, we obtained the position of the  $^3\text{D}$  term with an uncertainty of  $\pm 50 \text{ cm}^{-1}$ , and the fine structure of the  $^3\text{P}$  term with an uncertainty of  $\pm 4 \text{ cm}^{-1}$ .

The percentage compositions for the  $2s^2 2p^3$ ,  $2s 2p^4$ , and  $2p^5$  configurations were provided by Kaufman and Sugar (1982). The calculation included configuration interaction between  $2s^2 2p^3$  and  $2p^5$ .

The ionization energy was obtained by Lotz (1967) by extrapolation.

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## Cr xviii

Configuration	Term	J	Level (cm <sup>-1</sup> )	Leading percentages		
$2s^2 2p^4$	$^4\text{S}^{\circ}$	$3/2$	0	93	6	$2p^5$
$2s^2 2p^4$	$^3\text{D}^{\circ}$	$3/2$	126 060	80	17	$2p^5$
		$5/2$	150 814	100		
$2s^2 2p^4$	$^2\text{P}^{\circ}$	$1/2$	226 100	98	2	$2p^5 \text{ } ^2\text{P}^{\circ}$
		$3/2$	264 456	76	20	$2s^2 2p^3 \text{ } ^3\text{D}^{\circ}$
$2s 2p^5$	$^4\text{P}$	$5/2$	667 560	98	2	$^3\text{D}$
		$3/2$	714 950	99	1	$^3\text{D}$
		$1/2$	732 490	97	3	$^4\text{S}$
$2s 2p^5$	$^3\text{D}$	$3/2$	922 800	96	3	$^4\text{P}$
		$5/2$	931 420	98	2	$^4\text{P}$
$2s 2p^5$	$^2\text{S}$	$1/2$	1 062 040	77	21	$^3\text{P}$
$2s 2p^5$	$^3\text{P}$	$3/2$	1 103 370	96	3	$^3\text{D}$
		$1/2$	1 170 200	79	20	$^2\text{S}$
$2p^5$	$^4\text{P}$	$3/2$	1 738 700	98	2	$2s^2 2p^3 \text{ } ^2\text{P}^{\circ}$
		$1/2$	1 813 490	98	2	

## Cr XVIII—Continued

Configuration	Term	$J$	Level ( $\text{cm}^{-1}$ )	Leading percentages
$2s^2 2p^4 1^1 P 1 3d$	$^1P$	$\frac{3}{2}$	6 443 900	
$2s^2 2p^4 1^1 D 1 3d$	$^3F$	$\frac{7}{2}$	6 555 000	
Cr XIX ( $1^1 P_1$ )	<i>Limit</i>		10 480 000	

## Cr XIX

Z = 24

C I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^2 \ ^1P_0$ Ionization energy =  $11\,260\,000 \pm 22\,000 \text{ cm}^{-1}$  ( $1396 \pm 3 \text{ eV}$ )

Transitions between the  $2s^2 2p^2$  and  $2s 2p^3$  configurations were identified by Feldman et al. (1975). The spectrum was reobserved by Lawson and Peacock (1980) in the range of 95–203 Å with an accuracy of  $\pm 0.03$  Å. They identified many more lines of this array, including several intersystem lines, and classified the  $2s 2p^3 - 2p^4$  array as well.

The levels of the  $2s^2 2p^2$  ground configuration are determined from the magnetic dipole transitions observed in a tokamak plasma by Hinnoy, Suckewer, Cohen, and Saio (1982). Their wavelengths, ranging from 398–2885 Å, have an uncertainty of  $\pm 0.3$  Å. The uncertainty in the  $^3P$  and  $^1D$  levels is  $\pm 10$ , and for the  $^1S \pm 100 \text{ cm}^{-1}$ . With the exception of the  $2s 2p^3 \ ^3S_1$  level, the rest of the levels are due to Lawson and Peacock with an uncertainty of  $\pm 200 \text{ cm}^{-1}$ . Edlén (1984) has compared the known values of the  $^1S_1$  level in the isoelectronic sequence with theoretical predictions. He concluded that the values given by Lawson and Peacock are inconsistent with the trend. We give

Edlén's predicted value in brackets. The percentage compositions were provided by Kaufman and Sugar (1982). The calculation includes configuration interaction between  $2s^2 2p^2$  and  $2p^4$ .

Bromage and Fawcett (1977) have given predicted wavelengths of the  $2s^2 2p^2 - 2s 2p^3$  array.

The value for the ionization energy was obtained by extrapolation by Lotz (1967).

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## Cr XIX

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$2s^2 2p^2$	$^1P$	0	0	92	7	$^1S$
		1	47 811	99	1	$2p^4 \ ^3P$
		2	82 458	83	16	$2s^2 2p^2 \ ^1D$
$2s^2 2p^2$	$^1D$	2	184 597	83	16	$^1P$
$2s^2 2p^2$	$^1S$	0	298 800	89	9	$^3P$
$2s 2p^3$	$^3S$	2	[ 403 270 ]	98	2	$^1P$
$2s 2p^3$	$^1D$	2	671 630	88	12	$^3P$
		1	672 770	90	"	"
		3	686 830	100	"	"
$2s 2p^3$	$^3P$	0	789 160	100	"	"
		1	794 130	89	"	$^1D$
		2	804 750	82	12	"
$2s 2p^3$	$^3S$	1	959 880	86	12	$^1P$
$2s 2p^3$	$^1D$	2	976 220	96	4	$^1P$
$2s 2p^3$	$^1P$	1	1 090 660	87	12	$^1S$
$2p^4$	$^1P$	2	1 450 230	91	"	$2p^4 \ ^1D$
		1	1 514 320	99	"	$2s^2 2p^2 \ ^1P$
		0	1 517 990	90	"	$2p^4 \ ^1S$

## Cr XIX—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$2p^3$	<sup>1</sup> D	2	1 586 230	91	8	<sup>3</sup> P
$2p^3$	<sup>3</sup> S	0	1 787 180	88	9	<sup>3</sup> P
Cr XX ( <sup>2</sup> P <sub>1/2</sub> )	<i>Limit</i>		11 260 000			

## Cr XX

B I isoelectronic sequence

Ground state:  $1s^2 2s^2 2p^3 \text{ } ^4\text{P}^{\circ}_1$ Ionization energy =  $12\,070\,000 \pm 24\,000 \text{ cm}^{-1}$  ( $1496 \pm 3 \text{ eV}$ )

The splitting of the ground  $^4\text{P}^{\circ}$  term was determined with an uncertainty of  $20 \text{ cm}^{-1}$  from a magnetic dipole transition at  $1205.9 \pm 0.3 \text{ \AA}$  observed in a tokamak plasma by Hinnov et al. (1982).

The transition arrays  $2s^2 2p - 2s 2p^2$  and  $2s 2p^2 - 2p^3$  were classified by Lawson and Peacock (1980). They observed the spectrum in the range of  $116\text{--}271 \text{ \AA}$  with an accuracy of  $\pm 0.03 \text{ \AA}$ . The level values have an uncertainty of  $\pm 200 \text{ cm}^{-1}$ . The percentage composition for these levels was provided by Kaufman and Sugar (1982). Their calculation includes configuration interaction between  $2s^2 2p$  and  $2p^3$ .

The higher lying levels are from line identifications by Spector, Zigler, Zmora, and Schwob (1980) from laser-

produced plasmas observed in the  $10\text{--}14 \text{ \AA}$  range. The uncertainty in their values is  $\pm 3000 \text{ cm}^{-1}$ .

The value for the ionization energy was obtained by extrapolation by Lotz (1967).

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## Cr XX

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$2s^2 2p$	$^4\text{P}^{\circ}$	$3/2$	0	96	2	$2p^3 \text{ } ^2\text{P}^{\circ}$
		$5/2$	82 926	97	3	
$2s 2p^2$	$^4\text{P}$	$1/2$	354 570	96	2	$^2\text{S}$
		$3/2$	391 360	100		
		$5/2$	430 650	97	3	$^2\text{D}$
$2s 2p^2$	$^4\text{D}$	$3/2$	640 980	97	3	$^4\text{P}$
		$5/2$	652 990	97	3	$^4\text{P}$
$2s 2p^2$	$^2\text{P}$	$1/2$	760 400	55	43	$^2\text{S}$
		$3/2$	861 660	97	3	$^2\text{D}$
$2s 2p^2$	$^2\text{S}$	$1/2$	847 750	55	45	$^2\text{P}$
$2p^3$	$^4\text{S}^{\circ}$	$3/2$	1 101 840	95	4	$^2\text{P}^{\circ}$
$2p^3$	$^4\text{D}^{\circ}$	$3/2$	1 229 660	88	10	$^2\text{P}^{\circ}$
		$5/2$	1 248 380	100		
$2p^3$	$^2\text{P}^{\circ}$	$1/2$	1 380 270	96	2	$2s^2 2p \text{ } ^2\text{P}^{\circ}$
		$3/2$	1 414 590	84	11	$^2\text{D}^{\circ}$
$2s 2p (^2\text{P}^{\circ}) 3d$	$^4\text{P}^{\circ}$	$1/2$	7 443 000			
$2s^2 4s$	$^2\text{S}$	$1/2$	9 145 000			
$2s^2 4d$	$^2\text{D}$	$3/2$	9 308 000			
		$5/2$	9 335 000			
Cr XXI ( $^1\text{S}_0$ )	Limit		12 070 000			

## Cr XXI

Z=24

Be I isoelectronic sequence

Ground state:  $1s^2 2s^2 1S_0$ Ionization energy =  $13\,180\,000 \pm 26\,000 \text{ cm}^{-1}$  ( $1634 \pm 3 \text{ eV}$ )

Widing (1975) identified the  $2s^2 1S_0 - 2s2p 3P_1^o$  inter-system line in a solar flare spectrum at  $293.11 \pm 0.03 \text{ \AA}$ . The  $1S_0 - 1P_1$  transition was found in a tokamak plasma at  $149.90 \pm 0.03 \text{ \AA}$  by Hinnov (1979). The uncertainty of the  $1P_1$  is  $\pm 50 \text{ cm}^{-1}$ , and of the  $1P_1$   $\pm 150 \text{ cm}^{-1}$ . The transition array  $2s2p - 2p^2$  was observed by Lawson and Peacock (1980) in a laser-generated plasma. They obtained a level uncertainty of  $\pm 200 \text{ cm}^{-1}$ . They identified the inter-system line  $2s2p 3P_1^o - 2p^2 1D_2$ , which confirms the solar identification of Widing.

The higher configurations are from the line classifications of Boiko et al. (1977) at  $13 \text{ \AA}$ . A measurement uncertainty of  $\pm 0.003 \text{ \AA}$  is reported, giving a level uncertainty of  $\pm 2000 \text{ cm}^{-1}$ . The two terms of  $1s2s2p^2$  above

the limit are from the observations of Boiko et al. (1978) at  $2 \text{ \AA}$ , with a level uncertainty of  $\pm 10\,000 \text{ cm}^{-1}$ .

The ionization energy was obtained by extrapolation by Lotz (1967).

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## Cr XXI

Configuration	Term	J	Level (cm <sup>-1</sup> )	Configuration	Term	J	Level (cm <sup>-1</sup> )
$2s^2$	$1S$	0	0	$2p3p$	$3D$	3	8 087 000
$2s2p$	$3P^o$	0	318 080	$2p3p$	$1P$	1	8 022 000
		1	341 170	$2p3p$	$3P$	2	8 109 000
		2	405 070				
$2s2p$	$1P^o$	1	667 110	$2p3d$	$3D^o$	2	8 181 000
$2p^2$	$3P$	0	864 780			1	8 184 000
		1	911 180			3	8 204 000
		2	947 180	$2p3d$	$3P^o$	1,2	8 219 000
$2p^2$	$1D$	2	1 051 810			$2p3d$	$1P^o$
$2p^2$	$1S$	0	1 254 790	$2p3d$	$1F^o$	3	8 275 000
$2s3s$	$3S$	1	7 463 000	Cr XXII ( $2S_{1,2}$ )	Limit		13 180 000
$2s3p$	$1P^o$	1	7 620 000	$1s2s2p^2$	$3D$	2	45 550 000
$2s3d$	$3D$	2	7 721 000	$1s2s2p^2$	$1D$	2	45 800 000
		3	7 733 000				

## Cr XXII

Z = 24

Li I isoelectronic sequence

Ground state:  $1s^2 2s^2 S_{1/2}$ Ionization energy =  $13\,882\,000 \pm 2900\text{ cm}^{-1}$  ( $1721.4 \pm 0.4\text{ eV}$ )

The resonance lines  $2s^2 S - 2p^2 P_{1/2}^o, ^2P_{3/2}^o$  were observed in the solar corona at  $222.99\text{ \AA}$  and  $279.69\text{ \AA}$  by Sandlin, Brueckner, Scherrer, and Tousey (1976). We use the laboratory measurements of Lawson and Peacock (1980) with an uncertainty of  $\pm 0.03\text{ \AA}$ , giving a level uncertainty of  $\pm 50\text{ cm}^{-1}$ . Hinnov (1979) reported observing these lines in a tokamak plasma.

The  $2s - 3p$  and  $2p - 3s, 3d$  transitions were reported by Goldsmith, Feldman, Oren, and Cohen (1972). These series were remeasured and extended by Boiko, Faenov, and Pikuz (1978) to  $4p$  and  $4d$  by measurements in the range of  $9-13\text{ \AA}$  with an uncertainty of  $\pm 0.003\text{ \AA}$ . The uncertainty of these high-lying levels is  $\pm 3000\text{ cm}^{-1}$ .

The ionization energy was determined by Edlén (1979) from the  $2p - nd$  series.

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## Cr XXII

Configuration	Term	J	Level (cm <sup>-1</sup> )	Configuration	Term	J	Level (cm <sup>-1</sup> )
2s	<sup>2</sup> S	1/2	0	3d	<sup>2</sup> D	3/2	7 963 000
						5/2	7 972 000
2p	<sup>2</sup> P <sup>o</sup>	1/2	357 470	4p	<sup>2</sup> P <sup>o</sup>	1/2, 3/2	10 534 000
		3/2	448 470	4d	<sup>2</sup> D	3/2	10 552 000
3s	<sup>2</sup> S	1/2	7 826 000			5/2	10 585 000
3p	<sup>2</sup> P <sup>o</sup>	1/2	7 896 000	Cr XXII ( <sup>1</sup> S <sub>0</sub> )	Limit		13 882 000
		3/2	7 922 000				



## Cr xxii

Z = 24

He I isoelectronic sequence

Ground state:  $1s^2 \ ^1S_0$ Ionization energy =  $60\,344\,000 \pm 12\,000 \text{ cm}^{-1}$  ( $7481.8 \pm 0.6 \text{ eV}$ )

Because of the excellent agreement of the calculated energies of the  $n=2$  shell by Safronova (1981) with the few well-measured spectra in the He I sequence, we have compiled her results for the  $n=2$  levels and for the ionization energy. Detailed comparisons are given in the Introduction. Levels of the  $n=3-5$  shells are from the calculated binding energies by Ermolaev and Jones (1974) subtracted from Safronova's value for the binding energy of the ground state. We have assumed an uncertainty of 2 parts in  $10^4$  for the excited levels relative to the ground state, and for the ionization energy (see Introduction). For differences between excited levels where  $\Delta n = 0$ , we assumed an uncertainty of 2 parts in  $10^3$ .

Observations by Neupert (1971) of a solar flare spectrum place the  $1s2p \ ^1P_1^o$  level at  $45\,540\,000 \text{ cm}^{-1}$  and the  $1s2p \ ^3P_1^o$  at  $45\,890\,000 \text{ cm}^{-1}$  with an estimated uncertainty of  $\pm 60000 \text{ cm}^{-1}$ .

Percentage compositions are from Ermolaev and Jones.

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## Cr xxiii

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$1s^2$	S	0	0			
$1s2s$	S	1	[45 383 500]			
$1s2p$	$^1P^o$	0	[45 595 080]	94	6	$^1P^o$
		1	[45 610 130]			
		2	[45 691 370]			
$1s2s$	S	0	[45 614 430]			
$1s2p$	$^3P^o$	1	[45 827 110]	94	6	$^3P^o$
$1s3s$	S	1	[53 759 820]			
$1s3p$	$^1P^o$	0	[53 818 410]	93	7	$^1P^o$
		1	[53 822 120]			
		2	[53 846 400]			
$1s3s$	S	0	[53 820 510]			
$1s3p$	$^3P^o$	1	[53 883 700]	93	7	$^3P^o$
$1s4s$	S	1	[56 658 460]			
$1s4p$	$^1P^o$	0	[56 682 840]	91	7	$^1P^o$
		1	[56 684 180]			
		2	[56 694 650]			
$1s4s$	S	0	[56 683 050]			
$1s4p$	$^3P^o$	1	[56 709 860]	91	7	$^3P^o$
$1s5s$	S	1	[57 992 520]			

## Cr XXIII—Continued

Configuration	Term	<i>J</i>	Level ( $\text{cm}^{-1}$ )	Leading percentages		
$1s\bar{s}$	$^1S$	0	[58 004 800]			
$1s\bar{s}p$	$^3P$	0	[58 004 840]			
		1	[58 005 640]	92	8	$^1P$
		2	[58 010 900]			
$1s\bar{s}p$	$^1P$	1	[58 018 580]	92	8	$^3P$
Cr XXIV ( $^2S_{1/2}$ )	<i>Limit</i>		60 344 000			

## Cr xxiv

Z = 24

H I isoelectronic sequence

Ground state:  $1s^2 S_{1/2}$ Ionization energy =  $63\,675\,900 \pm 200 \text{ cm}^{-1}$  ( $7894.87 \pm 0.02 \text{ eV}$ )

Swartz, Kastner, Rothe, and Neupert (1971) identified the  $1s-2p$  unresolved pair of lines in a solar flare spectrum at 2.08 Å.

We give calculated values by Mohr (1983) for the  $n=2$  shell and by Erickson (1977) for  $n=3-5$  relative to the  $2p^2 P^{\circ}_{1/2}$  level. Further details are given in the Introduction. Relative to the ground state, the level uncertainty is estimated to be 5 parts in  $10^7$ . The

uncertainty in the excited states relative to  $2p^2 P^{\circ}_{1/2}$  is 1 part in  $10^6$ .

## References

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 Mohr, P. J. (1983), *At. Data Nucl. Data Tables* 29, 452  
 Swartz, M., Kastner, S., Rothe, E., and Neupert, W. (1971), *J. Phys. B* 4, 1747.

## Cr XXIV

Configuration	Term	J	Level ( $\text{cm}^{-1}$ )	Configuration	Term	J	Level ( $\text{cm}^{-1}$ )
1s	$^2S$	$\frac{1}{2}$	0	4f	$^2F^{\circ}$	$\frac{3}{2}$	[59 720 924]
2p	$^2P^{\circ}$	$\frac{1}{2}$	[47 719 790]		$^2F^{\circ}$	$\frac{5}{2}$	[59 723 460]
		$\frac{3}{2}$	[47 843 596]	5p	$^2P^{\circ}$	$\frac{1}{2}$	[61 134 179]
2s	$^2S$	$\frac{1}{2}$	[47 723 241]		$^2P^{\circ}$	$\frac{3}{2}$	[61 142 095]
3p	$^2P^{\circ}$	$\frac{1}{2}$	[56 598 064]	5s	$^2S$	$\frac{1}{2}$	[61 134 411]
		$\frac{3}{2}$	[56 634 766]	5d	$^2D$	$\frac{3}{2}$	[61 142 061]
3s	$^2S$	$\frac{1}{2}$	[56 599 135]		$^2D$	$\frac{5}{2}$	[61 144 687]
3d	$^2D$	$\frac{3}{2}$	[56 634 700]	5f	$^2F^{\circ}$	$\frac{5}{2}$	[61 144 683]
		$\frac{5}{2}$	[56 646 759]		$^2F^{\circ}$	$\frac{7}{2}$	[61 145 982]
4p	$^2P^{\circ}$	$\frac{1}{2}$	[59 700 397]	5g	$^2G$	$\frac{7}{2}$	[61 145 979]
		$\frac{3}{2}$	[59 715 870]		$^2G$	$\frac{9}{2}$	[61 146 758]
4s	$^2S$	$\frac{1}{2}$	[59 700 850]		<i>Limit</i>		63 675 900
4d	$^2D$	$\frac{1}{2}$	[59 715 842]				
		$\frac{3}{2}$	[59 720 933]				

**F. Atomic Transition Probabilities of Chromium, Cr I through Cr XXIV**

## F. Atomic Transition Probabilities of Chromium

[Excerpted from: G. A. Martin, J. R. Fuhr, and W. L. Wiese, *J. Phys. Chem. Ref. Data* 17, Supplement 3 (1968)]

### 1. Introduction

The following tables, including the introductory comments, are excerpted from the above cited compilation of atomic transition probabilities by G. A. Martin, J. R. Fuhr, and W. L. Wiese of the Data Center on Atomic Transition Probabilities at the National Institute of Standards and Technology (formerly the National Bureau of Standards).

This is part of the third major critical compilation by the NBS Data Center on Atomic Transition Probabilities. A first tabulation<sup>1</sup> containing transition probabilities for about 4,000 spectral lines of the elements hydrogen through neon, atomic numbers  $Z = 1$  through 10, including the neutral atoms as well as their various ions, was published in 1966. A second data volume<sup>2</sup> was issued in 1969, containing data for about 5,000 lines of the elements sodium ( $Z = 11$ ) through calcium ( $Z = 20$ ), again for all stages of ionization for which data were available. The data compilation work then continued with a series of smaller tables for the atoms and ions of the elements of the iron group, i.e., Sc and  $Ti^2$ ; V, Cr, and  $Mn^4$ ; Fe, Co, and  $Ni^2$ ; and the forbidden lines of all these elements.<sup>4</sup> From the beginning, it has been the intention to integrate these smaller tabulations into a single volume for the iron-group elements, in updated and expanded form. Unexpectedly, a great deal of new data were generated for these elements during the past few years, often with much improved accuracy, so that the revisions and additions became very extensive. Thus it took a much longer time than anticipated to complete these largely new data tables, and the greatly expanded tabulations had to be split into two separate volumes. Chromium is included in a volume that contains the material on the elements Sc ( $Z = 21$ ) through Mn ( $Z = 25$ ), and a companion volume<sup>7</sup> contains the material on Fe ( $Z = 26$ ) through Ni ( $Z = 28$ ).

In the present compilation, the scope and format of the earlier tabulations is maintained, i.e., critically evaluated atomic transition probabilities of allowed and forbidden discrete transitions of all stages of ionization are presented for which reliable data are available. Data are listed for at least the more prominent lines of each spectrum, even if some of these data are of low accuracy. Furthermore, transition-probability data are also presented for weaker transitions if the accuracy of these data has been estimated to be better than  $\pm 50\%$ .

The original literature is continually monitored by this NBS Data Center, and a master reference list is maintained from which all literature sources for this compilation have been taken.

### 2. Method of Evaluation

For the compilation of data on a critical basis, the central task is the evaluation of the data accuracy and the subsequent choice of the most accurate material. In order to accomplish this task in a consistent manner, general guideposts were established for each experimental and theoretical approach in earlier compilation work, and these criteria were maintained in this work. Specifically, each original literature source was judged by the following principal criteria:

- (1) A general evaluation of the capabilities and reliability of the applied experimental or theoretical method.
- (2) The author's consideration of the major critical factors in his approach that enter into the results.
- (3) The degree of agreement and general consistency between the author's results and other reliable data.
- (4) The degree of fit of the data into established systematic trends and, if deviations exist, the reasons for such disagreements.
- (5) The author's estimate of his uncertainties.

The general evaluations of each experimental and theoretical method have been discussed in considerable detail in the introductions to previous tabulations.<sup>1-4</sup> Thus, these publications are to be consulted for further details. However, it should be pointed out that in this tabulation, particularly interesting situations are illustrated by providing comparison tables or graphs in the introductions to individual spectra.

With respect to error estimates, one should note that the theoretical literature sources, which provide a large part of the data, generally contain no error estimates, since no reliable assessment of the uncertainties introduced by the various approximations is possible. But even for the experimental papers, where error estimates may often readily be made, the statements by some authors are too imprecise and also incomplete, so that they are not particularly useful as presented. Sometimes only statistical measurement errors have been given, without allowance for systematic errors. It therefore became essential to judge each paper by the principal factors 1-4 listed above, in addition to utilizing the author's error estimate (point (5)) whenever appropriate.

### 3. General Arrangement of the Tables

The same general arrangement of the tables is used as in earlier volumes,<sup>12</sup> i.e., data are included which serve to identify the spectral lines, as well as the actual transition probabilities (and related quantities), accuracy estimates, and references to the sources of the compiled material. However, for most of the spectra of neutral and singly-ionized atoms of the iron-group elements, the transition array column was dropped. Instead, in order to identify the lower and upper levels of a transition, the level designation scheme of C. E. Moore<sup>8</sup> was adopted, who affixed lower-case letters (*a, b, c, ..., x, y, z*) to the term designations. This convention is also retained in the very recent tables of "Atomic Energy Levels" by J. Sugar and C. Corliss.<sup>9</sup> In other special cases, the notation was adapted to the special coupling situations encountered in those spectra, as, for example, the  $Jj$  coupling encountered in Ne-like ions and  $Jj$  and  $J_1 \ell$  coupling for Ar-like ions.

Material pertaining to spectral-line identifications has been taken from the comprehensive wavelength tabulations of Reader and Corliss,<sup>10</sup> Kelly,<sup>11,12</sup> and Kelly and Palumbo,<sup>13</sup> the multiplet tables of C. E. Moore,<sup>14,15</sup> and the recent energy-level compilation of Sugar and Corliss<sup>9</sup> (this last reference supersedes earlier compilations by Sugar and others<sup>16,17</sup>). The wavelength and energy-level data from these sources have been supplemented by original literature data when needed in the course of preparing the transition-probability tables.

Wavelengths and energy levels which are the results of theoretical calculations, or which were either calculated from experimentally determined data or interpolated or extrapolated from data on similar (e.g., isoelectronic) species, are placed in square brackets in order to distinguish them from the usually more accurate experimental material.

For each transition-probability table which contains a minimum of twenty distinct wavelength values, a "list of tabulated lines," has been provided, in ascending order of wavelength, of the spectral lines contained therein, along with an index to the multiplet number (or numbers) in which each is to be found. Wavelengths that are printed in italics in the transition-probability tables are not included in these line lists.

The uncertainties in the atomic transition-probability data are denoted by letters as follows:

- A.. for uncertainties within 3 percent,
- B.. for uncertainties within 10 percent,
- C.. for uncertainties within 25 percent,
- D.. for uncertainties within 50 percent,
- E.. for uncertainties greater than 50 percent.

The word *uncertainty* is used here with the connotation "estimated extent of the deviation from the true value." The estimation procedure is based on the evaluation of random errors as well as estimates of the maximum effect of possible systematic errors. Often, further distinctions were made in the uncertainty labels by assigning plus or minus signs to some transitions to indicate that these lines are estimated to be somewhat better or worse than similar lines. These should, therefore, be the first or last choice among similar transitions.

A summary of the abbreviations and special symbols used in the tables is given in Section 4. Included there for convenience are formulas which relate various properties of individual spectral lines to those for entire multiplets. In Table 1, the conversion factors are provided which have been used throughout this compilation to convert from transition probabilities to oscillator strengths and line strengths, and vice versa.

TABLE 1. Conversion factors  
The factor in each box converts by multiplication the quantity above it into the one at its left.

	$A_{ul}$	$f_{ul}$	$S$
$A_{ul}$	1	$\frac{6.670_2 \times 10^{25} g_l}{g_u \lambda^3}$	E1 $\frac{2.026_1 \times 10^{28}}{g_u \lambda^3}$
			E2 $\frac{1.679_2 \times 10^{28}}{g_u \lambda^3}$
			M1 $\frac{2.697_4 \times 10^{23}}{g_u \lambda^3}$
			M2 $\frac{6.626_2 \times 10^{22}}{g_u \lambda^3}$
$f_{ul}$	$\frac{1.499_2 \times 10^{-24} \lambda^3 g_u}{g_l}$	1	E1 $\frac{303.7_6}{g_l \lambda}$
$S$	E1 $4.935_3 \times 10^{-29} g_u \lambda^3$	E1 $3.292_1 \times 10^{-3} g_l \lambda$	1
	E2 $5.952_6 \times 10^{-29} g_u \lambda^3$		
	M1 $3.707_3 \times 10^{-24} g_u \lambda^3$		
	M2 $1.509_1 \times 10^{-23} g_u \lambda^3$		

The line strength ( $S$ ) is given in atomic units; formulas and values for these quantities in SI units are as follows:

For E1 transitions,  $a_0^3 e^2 = 7.188_3 \times 10^{-29} \text{ m}^2 \text{ C}^2$

For E2 transitions,  $a_0^3 e^2 = 2.012_9 \times 10^{-29} \text{ m}^4 \text{ C}^2$

For M1 transitions,  $\mu_B^2 = (eh/4\pi m_e)^2 = 8.600_7 \times 10^{-67} \text{ J}^2 \text{ T}^{-2}$

For M2 transitions,  $\mu_B^2 a_0^2 = 2.408_5 \times 10^{-67} \text{ J}^2 \text{ m}^2 \text{ T}^{-2}$ .

where  $a_0$ ,  $e$ ,  $m_e$ , and  $h$  are the Bohr radius, electron charge, electron mass, and Planck constant, respectively, and  $\mu_B$  is the Bohr magneton.

The transition probability ( $A_{ul}$ ) is in units of  $\text{s}^{-1}$ , and the  $f$ -value is dimensionless. The wavelength ( $\lambda$ ) is given in Angstrom units, and  $g_l$  and  $g_u$  are the statistical weights of the lower and upper level, respectively.

[Note: the definition of the line strength for E2 transitions, which is used by some authors, yields an  $S$ -value that is 50% higher than that employed here and in earlier NBS transition-probability compilations. Such line strengths have been multiplied by  $\frac{1}{2}$  before tabulating them here, and this fact is indicated in the short introductions to the pertinent data tables.]

For the atomic constants entering into the relations given in this table, the recommendations of the CODATA Task Group on Fundamental Constants (E. R. Cohen and B. N. Taylor, Rev. Mod. Phys. 59, 1121 (1987)) have been used. The 1987 values were not available at the time that most of the data was compiled for this publication; however, differences between these and the earlier (CODATA Task Group, 1973) values of the fundamental constants were utilized, which amount to only 0.002% or less for the E1 transitions and 0.05% or less for the M1, E2, and M2 (forbidden) transitions and have therefore not affected the tabulated data.

#### 4. Key to Abbreviations and Symbols Used in the Tables

##### 1. Symbols for indication of accuracy:

- A..... uncertainties within 3 percent,  
 B..... uncertainties within 10 percent,  
 C..... uncertainties within 25 percent,  
 D..... uncertainties within 50 percent,  
 E..... uncertainties greater than 50 percent.

##### 2. Abbreviations appearing in the source column of allowed transitions:

- ls* = LS coupling rules applied  
*n* = normalized to a scale different from that of the author (as explained in the introductory remarks to the pertinent spectrum).  
*interp.* = derived by an interpolation technique, rather than taken directly from the literature.

##### 3. Special symbols used in the wavelength and energy level columns:

The number in parentheses under the multiplet designation refers to the sequence number of Ref. 14 (Revised Multiplet Table). If letters "uv" are added, they refer to the sequence number of Ref. 15 (Ultraviolet Multiplet Table).

Numbers in italics indicate multiplet values, i.e., weighted averages of line values.

Numbers in square brackets indicate approximate calculated or extrapolated values.

##### Useful Relations

##### (A) Statistical weights:

The statistical weights are related to the inner quantum number  $J_L$  (for one-electron spectra:  $j_i$ ) of a level (i.e., initial or final state of a line) by

$$g_L = 2J_L + 1,$$

and to the quantum numbers of a term (initial or final state of a multiplet) by

$$g_M = (2L + 1)(2S + 1).$$

(The "multiplet" values  $g_M$  may also be obtained by summing over all possible "line" values  $g_L$ .  $S$  is the resultant spin.)

##### (B) Relations between the strengths of allowed lines and the total multiplet strength:

##### 1. Line strength $S$ :

$$S(i, k) = \sum_{J_u, J_k} S(J_u, J_k)$$

or

$$S(\text{Multiplet}) = \sum S(\text{line})$$

( $k$  denotes the upper and  $i$  the lower term).

##### 2. Absorption oscillator strength $f_{ik}$ :

$$f_{ik}^{\text{multiplet}} = \frac{1}{\bar{\lambda}_{ik} \sum_{J_i} (2J_i + 1)} \sum_{J_u, J_k} (2J_i + 1) \times \lambda(J_u, J_k) \times f(J_u, J_k).$$

The mean wavelength for the multiplet,  $\bar{\lambda}_{ik}$ , may be obtained from the weighted energy levels. Often the wavelength differences for the lines within a multiplet are small, in which case the wavelength factors may be neglected.

##### 3. Transition probability $A_{ki}$ :

$$A_{ki}^{\text{multiplet}} = \frac{1}{(\bar{\lambda}_{ik})^3 \sum_{J_k} (2J_k + 1)} \sum_{J_i, J_k} (2J_k + 1) \times \lambda(J_i, J_k)^3 \times A(J_i, J_k).$$

Relative strengths  $S(J_i, J_k)$  of the components of a multiplet are listed for the case of LS coupling in C. W. Allen, *Astrophysical Quantities*, 3rd ed. (The Athlone Press, London, 1973); H. E. White and A. Y. Eliason, *Phys. Rev.* **44**, 753 (1933); B. W. Shore and D. H. Menzel, *Principles of Atomic Structure*, p. 447 (John Wiley & Sons, Inc., New York, 1968); L. Goldberg, *Astrophys. J.* **82**, 1 (1935) and **84**, 11 (1936).

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## Chromium

## Cr I

Ground State:  $1s^2 2s^2 2p^6 3s^2 3p^6 3d^4 4s^1 7S_3$ Ionization Energy:  $6.76669 \text{ eV} = 54575.6 \text{ cm}^{-1}$ 

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
1999.95	51	2703.48	32	3163.76	92	4065.71	173
2095.00	7	2716.18	31	3169.58	92	4081.74	68
2095.40	7	2726.50	15	3237.73	91	4097.69	82
2095.83	7	2731.90	15	3238.09	91	4109.58	69
2354.30	50	2736.46	15	3351.97	5	4111.33	82
2364.73	6	2751.58	30	3379.17	5	4126.51	57
2365.91	6	2752.85	30	3578.68	4	4165.52	193
2366.81	6	2757.09	30	3593.48	4	4203.59	57
2375.06	49	2761.74	30	3605.32	4	4204.48	168
2383.30	49	2764.36	30	3615.65	3	4211.48	90
2385.72	49	2769.90	30	3635.28	3	4213.18	115
2389.21	48	2780.70	30	3639.80	61	4222.75	104
2408.60	46	2871.63	29	3730.81	2	4230.49	104
2408.72	47	2879.27	29	3732.03	2	4232.23	188
2479.14	45	2887.00	29	3743.89	60	4234.52	126
2492.57	43	2889.22	29	3744.49	60	4235.99	103
2495.08	42	2893.25	29	3757.17	60	4237.72	103
2496.30	43	2894.17	29	3757.66	60	4238.96	102
2499.84	43	2896.76	29	3758.04	60	4242.84	102
2502.55	44	2899.20	29	3768.24	60	4248.34	102
2504.31	43	2905.48	29	3768.73	60	4252.24	102
2508.11	41	2909.05	29	3804.80	105	4254.33	1
2508.97	41	2910.89	29	3849.54	25	4255.50	89
2513.62	41	2911.15	29	3852.22	25	4257.35	102
2527.11	41	2967.64	28	3883.29	24	4261.35	81
2538.95	17	2971.10	28	3885.24	24	4261.63	127
2544.70	17	2975.48	28	3886.80	24	4262.37	114
2549.55	40	2980.78	28	3894.04	24	4263.15	161
2560.70	40	2988.64	14	3902.91	24	4268.79	167
2571.74	40	2991.88	28	3903.17	24	4269.96	114
2577.66	40	2994.06	14	3908.76	24	4271.07	114
2579.14	38	2995.09	13	3916.25	24	4272.93	81
2584.67	39	2996.57	28	3919.17	24	4274.81	1
2588.19	38	2998.78	14	3921.03	24	4275.98	155
2591.84	40	3000.88	28	3928.65	24	4280.42	161
2603.56	38	3005.06	28	3941.50	24	4280.89	145
2618.27	36	3013.72	27	3963.69	59	4283.00	187
2620.48	34	3015.20	26	3969.75	59	4288.40	124
2622.87	35	3020.67	26	3976.02	59	4289.73	1
2625.32	37	3021.58	26	3981.24	70	4291.97	145
2626.60	35	3024.36	27	3983.90	59	4293.58	81
2629.82	36	3029.17	27	3991.12	59	4296.11	200
2649.36	32	3030.25	26	4001.44	165	4296.30	124
2671.98	32	3031.35	26	4039.10	162	4296.63	161
2673.64	32	3034.19	27	4039.29	162	4297.06	67
2678.15	32	3037.05	26	4042.25	58	4297.75	161
2680.33	32	3040.84	26	4048.78	162	4298.05	200
2690.25	32	3053.87	27	4049.78	162	4299.72	81
2696.53	16	3148.44	92	4050.03	58	4300.52	145
2700.59	31	3155.16	92	4057.83	162	4301.19	145
2701.99	33	3160.62	92	4068.78	162	4302.78	199

## List of tabulated lines — Continued

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
4305.47	81	4442.28	86	4578.33	159	4727.13	83
4307.67	198	4443.72	152	4580.05	12	4729.84	119
4309.73	186	4459.75	99	4582.40	171	4730.69	108
4312.48	125	4460.76	66	4583.90	97	4737.33	108
4317.91	186	4462.79	99	4584.10	122	4741.09	183
4319.66	81	4464.66	99	4584.76	97	4743.12	177
4321.25	74	4465.37	99	4584.94	134	4745.31	64
4321.62	125	4467.57	99	4585.10	144	4752.07	178
4325.08	88	4475.36	80	4586.15	122	4754.73	118
4325.65	124	4477.05	66	4591.41	22	4755.14	95
4330.76	113	4480.27	135	4592.55	190	4756.09	108
4332.57	124	4480.36	151	4595.60	179	4757.31	177
4337.25	185	4482.88	135	4600.11	55	4757.58	149
4337.57	23	4490.55	164	4600.75	22	4764.28	149
4338.80	136	4491.69	80	4601.02	55	4764.65	94
4339.45	23	4491.86	74	4606.36	191	4767.26	149
4339.74	23	4492.31	135	4611.06	84	4767.86	149
4340.14	67	4495.28	174	4611.96	134	4770.68	94
4341.46	67	4496.85	12	4613.36	22	4775.12	148
4343.17	67	4498.73	71	4614.51	158	4789.32	52
4344.51	23	4500.29	112	4616.12	22	4792.49	118
4345.08	136	4501.79	71	4617.37	84	4796.15	176
4346.83	88	4503.04	201	4619.54	71	4797.68	148
4347.49	77	4506.84	182	4622.47	150	4801.02	118
4351.06	23	4510.02	197	4622.76	71	4806.25	64
4351.77	23	4511.90	112	4625.91	157	4810.71	107
4353.94	136	4514.36	181	4626.18	22	4814.25	107
4356.77	101	4515.44	96	4628.48	128	4816.13	196
4357.51	136	4524.84	172	4633.27	128	4819.30	170
4359.65	23	4526.44	56	4639.52	128	4823.90	195
4362.97	73	4527.33	56	4639.70	150	4825.50	107
4363.13	87	4527.45	76	4641.49	184	4831.63	143
4368.25	101	4529.84	56	4641.96	157	4836.85	107
4368.90	136	4530.48	85	4646.15	22	4838.42	194
4370.76	166	4530.68	56	4646.50	109	4870.79	106
4370.87	160	4530.73	56	4646.80	128	4874.65	117
4371.28	23	4530.93	96	4648.12	54	4880.04	117
4373.26	23	4531.24	96	4648.33	84	4885.77	53
4373.65	192	4535.13	56	4651.29	22	4885.97	106
4374.17	88	4535.69	56	4652.16	22	4887.01	106
4375.34	87	4535.75	56	4654.76	128	4903.25	52
4376.80	192	4539.76	56	4656.18	109	4922.28	106
4377.55	74	4540.49	56	4656.82	202	4936.34	116
4379.77	101	4540.72	112	4663.33	128	4942.49	11
4381.11	67	4541.06	56	4665.90	150	4944.57	156
4382.86	67	4541.51	111	4666.20	83	4953.73	116
4384.97	23	4543.73	85	4669.34	128	4954.81	116
4387.38	74	4544.80	56	4680.86	120	4964.92	11
4391.76	23	4545.23	56	4689.38	128	4966.80	156
4393.54	86	4545.95	12	4693.94	83	5013.31	63
4397.24	100	4548.65	180	4695.14	83	5032.54	189
4399.82	100	4552.95	172	4697.04	65	5034.65	189
4410.31	100	4554.82	123	4697.38	133	5045.04	189
4410.97	86	4555.31	144	4698.46	128	5061.90	10
4411.11	100	4556.18	123	4698.94	110	5072.93	10
4412.25	23	4562.24	159	4699.59	183	5112.50	20
4413.00	204	4562.43	72	4700.60	65	5123.47	21
4413.86	152	4562.86	122	4706.09	120	5139.60	142
4422.70	152	4564.17	203	4707.73	133	5177.42	137
4424.10	75	4566.51	22	4708.02	128	5192.01	137
4424.29	100	4569.63	123	4717.67	120	5193.50	141
4428.52	100	4570.99	123	4718.43	128	5196.45	142
4429.93	152	4571.10	96	4722.65	121	5200.20	137
4432.16	71	4571.87	54	4723.06	108	5204.51	9
4432.77	206	4575.11	134	4724.40	108	5206.02	9

List of tabulated lines — Continued

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
5208.42	9	5300.74	19	558.60	139	6630.00	18
5214.14	131	5304.19	147	5588.05	139	6661.10	175
5238.97	62	5312.88	147	5628.64	138	6669.27	175
5241.47	62	5318.79	147	5642.40	154	6882.40	146
5243.38	137	5328.36	79	5648.25	154	6883.05	146
5247.58	19	5329.17	79	5649.38	154	6925.22	146
5261.76	153	5329.76	79	5694.72	154	6978.46	146
5264.16	19	5340.46	147	5702.30	138	6979.81	146
5265.73	19	5344.77	147	5719.82	93	6980.91	146
5272.01	147	5345.77	19	5783.11	129	7170.56	169
5287.19	147	5348.30	19	5783.89	129	7355.93	78
5293.38	132	5400.58	130	5785.02	129	7400.22	78
5296.69	19	5409.78	19	5787.97	129	8916.24	16
5297.37	79	5442.40	140	5838.68	93	8939.21	163
5297.99	79	5548.61	139	5844.60	93	8955.76	163
5298.29	19	5566.55	139	6330.13	8		

For this spectrum, we have utilized seventeen data sources, which are all fairly recent experiments. These include the absorption measurements of Bieniewski<sup>1</sup> and Blackwell and co-workers<sup>15,16</sup>; anomalous dispersion (hook) measurements (plus a few absorption measurements) of Huber and Sandeman<sup>2</sup>; emission experiments performed with a shock tube by Wolnik *et al.*,<sup>9,10</sup> with a hollow cathode by Cocke *et al.*,<sup>11</sup> and by Tozzi *et al.*,<sup>17</sup> and with a wall-stabilized arc by Wujec and Weniger<sup>13</sup>; shock tube absorption studies of Huber and Tobey<sup>12</sup>; and six lifetime determinations<sup>4,18</sup> from which oscillator strengths could be directly derived. Another source that we used in this compilation is that of Kostyk,<sup>14</sup> who derived  $\log gf$ -values from solar spectra. The measurements of Cocke *et al.* were restricted to "branching ratio" determinations, which were then converted to transition probabilities by using available beam-foil lifetimes.

Accurate lifetime measurements are those by Marek,<sup>4</sup> by Measures and co-workers,<sup>18</sup> and by Hannaford and Lowe,<sup>19</sup> who all selectively populated the levels under

study by means of dye laser excitation and then measured the corresponding radiative lifetimes. Other reliable lifetimes were measured by Becker *et al.*,<sup>4</sup> who employed the level-crossing (Hanle) method, and by Marek and Richter,<sup>5</sup> who used the phase-shift technique. It is possible to intercompare oscillator strengths derived from these lifetime sources for lines of the multiplets  $a^3S-z^3P^o$  and  $a^3S-y^3P^o$ . This comparison, also including the absolute scale of Bieniewski, who has performed very careful absorption measurements with an electric furnace, is presented in Table I. In converting the lifetimes to  $f$ -values, we did not include the contributions of non-resonance transitions because of lack of data. However, Huber and Sandeman estimated that these additional decay modes have a practically negligible effect ( $\approx 0.5\%$ ) on the lifetimes involved. We consider the averaged  $f$ -values for these two multiplets to be accurate to within ten percent, as supported by the excellent mutual agreement among the selected data sources.

TABLE I. Comparison of absorption and lifetime data

Multiplet	$\lambda(\text{Å})$	$f_o$ (Bieniewski)	$f_o^*$ (Becker <i>et al.</i> <sup>4</sup> ) <sup>a</sup>	$f_o^*$ (Marek and Richter) <sup>5</sup>	$f_o^*$ (Marek) <sup>4</sup>	$f_o^*$ (Measures <i>et al.</i> <sup>18</sup> )	$f_o^*$ (Kwong and Measures) <sup>19</sup>	$f_o^*$ (Hannaford and Lowe) <sup>19</sup>
$a^3S-z^3P^o$ (1)	4254.33	0.106	0.111	0.111	0.110	0.112		0.110
	4274.81	0.082	0.0849	0.0841		0.0849		
	4289.73	0.059	0.0616	0.0646		0.0627	0.0633	
$a^3S-y^3P^o$ (4)	3578.68	0.34	0.355	0.402				
	3593.48	0.28	0.271	0.319				
	3605.32	0.21	0.220	0.244				

<sup>a</sup>Listed oscillator strengths have been derived from lifetime measurements

<sup>b</sup>Level-crossing technique

<sup>c</sup>Phase shift method

<sup>d</sup>Laser excitation technique

The most reliable general  $f$ -value sources for this spectrum are those of Blackwell *et al.*<sup>15,16</sup> and Tozzi *et al.*<sup>17</sup> Blackwell's group obtained relative oscillator strengths by using their well-known absorption technique with an electric furnace. Their relative values were placed onto an absolute scale either by direct normalization to accurate radiative lifetimes or by comparing their newer measurements (at higher excitation potentials) to their earlier absolute data, via photoelectric pyrometry. Tozzi *et al.* measured branching ratios in emission, using a hollow-cathode discharge as a source and a Fourier transform spectrometer for the spectral recordings. These authors normalized their relative data to lifetimes measured by Kwiatkowski *et al.*<sup>3</sup> We estimate that the data of Refs. 15, 16, and 17 are generally accurate to within ten percent.

Another source providing accurate data is the work of Huber and Sandeman.<sup>2</sup> These authors normalized their relative data to the lifetimes of Ref. 4. Since these lifetimes are very close to our adopted absolute scale, we have tabulated the data of Ref. 2 without change or renormalization. We have also followed their carefully documented error estimates throughout. The data of Wolnik *et al.*,<sup>9,10</sup> which are systematically lower than those of Huber and Sandeman, have been increased by a factor of 1.35 to be consistent with our absolute scale. The data of Cocke *et al.*<sup>11</sup> agree quite well with those of Ref. 2 for overlapping lines, so that we have left their oscillator strength scale unchanged.

Another comprehensive data source that have utilized in this compilation is that of Wujec and Weniger. These authors employed a wall-stabilized arc to measure the oscillator strengths of 275 lines in the wavelength range 4220–4850 Å. They measured the line intensities end-on with a photographic detection system. To determine the plasma conditions, Wujec and Weniger used a variety of spectroscopic techniques. These techniques revealed some significant inconsistencies in the experiment, although the  $f$ -values for overlapping lines agreed quite well with those of an earlier NBS compilation (Ref. 14). For example, a PLTE analysis and Stark broadening study of Ar I lines performed by Wujec and Weniger indicated high electron densities, with corresponding temperatures of about 11000 K. On the other hand, three other methods used by these authors yielded much lower temperatures ( $\approx 8000$  K) for the same experimental runs. These latter methods also produced consistently lower temperature determinations, even for runs performed at 50% higher arc currents. Because of these in-

consistencies, we have assigned "D" accuracies to the data of Ref. 13 and have tabulated them only for unblended lines and only if no other data source was available.

Wujec and Weniger presented two different sets of transition probabilities, corresponding to their different plasma analyses. In this compilation, we have chosen the set of data that was determined by assuming an arc temperature derived from the scale of Younger *et al.*,<sup>14</sup> since this scale is based on reliable oscillator strengths.

Another reference providing reliable  $f$ -values is the work of Kostyk.<sup>18</sup> His oscillator strengths are derived from solar data on line depths of Cr I lines, taken from the Liege solar atlas.<sup>20</sup> For 45 lines, Kostyk's data overlapped with data from either Blackwell *et al.*<sup>15,16</sup> or Tozzi *et al.*<sup>17</sup> For the 45 lines in common, data for 28 lines agreed within 25 percent, and data for 43 lines agreed within 50 percent.

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Cr I: Allowed transitions

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>7</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	$\log gf$	Accu- racy	Source
1.	$a^1S - z^1P$ (1)	4269.6	0	23415	7	21	0.312	0.256	25.2	0.254	B	1,4,5,6,7, 8,19
		4254.33	0	23499	7	9	0.315	0.110	10.8	-0.114	B	1,4,5,6,7, 19
		4274.81	0	23386	7	7	0.307	0.0840	8.27	-0.231	B	1,4,5,7
		4289.73	0	23305	7	5	0.316	0.0622	6.15	-0.361	B	1,4,5,7,8
2.	$a^1S - z^1P$ (2)	3732.03	0	26788	7	7	0.0016	3.3(-4)	0.029	-2.63	C+	17
		3730.81	0	26796	7	5	0.0016	2.4(-4)	0.020	-2.78	C+	17
3.	$a^1S - z^1D$ (3)	3615.65	0	27650	7	9	5.1(-4)	1.3(-4)	0.011	-3.05	C-	2
		3635.26	0	27500	7	7	1.5(-4)	3.5(-5)	0.0026	-3.67	C-	2
4.	$a^1S - y^1P$ (4)	3589.9	0	27848	7	21	1.52	0.881	72.9	0.790	B	1,4,5
		3578.68	0	27935	7	9	1.48	0.366	30.2	0.409	B	1,4,5
		3593.48	0	27820	7	7	1.50	0.290	24.0	0.307	B	1,4,5
		3605.32	0	27729	7	5	1.62	0.225	18.7	0.197	B	1,4,5
5.	$a^1S - y^1P$ (5)	3351.97	0	29825	7	7	0.0012	2.0(-4)	0.015	-2.86	B	17
		3379.17	0	29585	7	5	9.9(-4)	1.2(-4)	0.0095	-3.07	C+	17
6.	$a^1S - x^1P$ (uv 1)	2365.6	0	42259	7	21	0.057	0.014	0.78	-1.00	C	2
		2364.73	0	42275	7	9	0.053	0.0057	0.31	-1.40	C	2
		2365.91	0	42254	7	7	0.055	0.0046	0.25	-1.49	C	2
		2366.81	0	42238	7	5	0.069	0.0041	0.22	-1.54	C	2
7.	$a^1S - u^1P$ (uv 2)	2095.1	0	47710	7	21	0.0114	0.00226	0.109	-1.90	C	2
		2095.00	0	47719	7	9	0.012	9.9(-4)	0.048	-2.16	C	2
		2095.40	0	47709	7	7	0.011	7.3(-4)	0.035	-2.29	C	2
		2095.83	0	47697	7	5	0.011	5.3(-4)	0.026	-2.43	C	2
8.	$a^1S - z^1P$ (6)	6330.13	7593	23386	5	7	2.9(-4)	2.4(-4)	0.025	-2.92	D	18
9.	$a^1S - z^1P$ (7)	5206.9	7593	26793	5	15	0.509	0.621	53.2	0.492	B	15,17
		5204.42	7593	26784	5	7	0.506	0.288	24.7	0.158	B	15,17
		5206.02	7593	26796	5	5	0.514	0.209	17.9	0.019	B	15,17
		5204.51	7593	26802	5	3	0.509	0.124	10.6	-0.208	B	15,17

## Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accu- racy	Source
10.	$a^4S - z^4D^*$ (8)	5051.90	7593	27382	5	5	5.41(-4)	2.07(-4)	0.0172	-2.985	B	15
		5072.93	7593	27300	5	3	0.00159	3.69(-4)	0.0308	-2.734	B	15
11.	$a^4S - y^4P^*$ (9)	4942.49	7593	27820	5	7	0.00198	0.00102	0.0827	-2.294	B	15
		4964.92	7593	27729	5	5	0.00161	5.94(-4)	0.0486	-2.527	B	15
12.	$a^4S - y^4P^*$ (10)	4529.6	7593	29684	5	15	0.029	0.027	2.0	-0.87	B	15,17
		4496.85	7593	29625	5	7	0.033	0.014	1.0	-1.15	B	15,17
		4545.95	7593	29585	5	5	0.027	0.0085	0.64	-1.37	B	15,17
		4580.05	7593	29421	5	3	0.024	0.0045	0.34	-1.65	B	17
13.	$a^4S - y^4P^*$ (uv 3)	2995.09	7593	40971	5	5	0.43	0.058	2.8	-0.54	D	2
14.	$a^4S - x^4P^*$ (uv 4)	2992.5	7593	41000	5	15	0.41	0.16	8.1	-0.09	D	2,15
		2988.64	7593	41043	5	7	0.52	0.098	4.8	-0.31	C	2
		2994.06	7593	40983	5	5	0.25	0.034	1.7	-0.77	E	2
		2998.78	7593	40930	5	3	0.407	0.0329	1.62	-0.784	B	15
15.	$a^4S - w^4P^*$ (uv 7)	2730.3	7593	44308	5	15	0.76	0.256	11.5	0.107	C	2
		2726.50	7593	44259	5	7	0.75	0.12	5.3	-0.23	C	2
		2731.90	7593	44187	5	5	0.78	0.087	3.9	-0.26	C	2
		2736.46	7593	44126	5	3	0.75	0.050	2.3	-0.60	D	2
16.	$a^4S - v^4P^*$ (uv 8)	2696.52	7593	44667	5	3	0.12	0.0076	0.34	-1.42	D	2
17.	$a^4S - u^4P^*$ (uv 9)	2544.70	7593	46879	5	7	0.11	0.014	0.61	-1.14	D-	2
		2538.95	7593	46968	5	5	0.11	0.010	0.44	-1.28	E	2
18.	$a^4D - z^4P^*$ (16)	6630.00	8308	23386	9	7	6.0(-5)	3.1(-5)	0.0060	-3.56	D	18

Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accu- racy	Source
19.	$a^3D - z^3P$ (18)	5445.2	8090	26793	25	15	0.096	0.022	9.7	-0.26	B	15,17
		5409.78	8308	26788	9	7	0.062	0.021	3.4	-0.72	B	15,17
		5345.77	8095	26796	7	5	0.049	0.015	1.8	-0.98	B	15,17
		5296.69	7927	26802	5	3	0.031	0.0079	0.69	-1.40	B	15,17
		5348.30	8095	26788	7	7	0.017	0.0073	0.90	-1.29	B	15,17
		5296.29	7927	26796	5	5	0.033	0.014	1.2	-1.15	B	15,17
		5264.16	7811	26802	3	3	0.041	0.017	0.88	-1.29	B	15,17
		5300.74	7927	26788	5	7	0.0025	0.0015	0.13	-2.12	B	15,17
		5265.73	7811	26796	3	5	0.0085	0.0059	0.31	-1.75	B	15,17
5247.58	7751	26802	1	3	0.019	0.023	0.40	-1.64	B	15,17		
20.	$a^3D - z^3D$ (19)	5112.50	8095	27650	7	9	5.7(-5)	2.9(-5)	0.0034	-3.70	D	18
		5123.47	8308	27820	9	7	4.0(-4)	1.2(-4)	0.018	-2.96	D	18
21.	$a^3D - y^3P$ (20)	4633.9	8090	29664	25	15	0.11	0.022	8.2	-0.27	B	15,17
		4646.15	8308	29825	9	7	0.087	0.022	3.0	-0.70	B	15,17
		4652.16	8095	29585	7	5	0.058	0.013	1.4	-1.03	B	17
		4651.29	7927	29421	5	3	0.036	0.0070	0.54	-1.46	B	15,17
		4600.75	8095	29825	7	7	0.025	0.0079	0.84	-1.26	B	15,17
		4616.12	7927	29585	5	5	0.041	0.013	0.99	-1.19	B	15,17
		4626.18	7811	29421	3	3	0.050	0.016	0.73	-1.32	B	15,17
		4565.51	7927	29825	5	7	0.0041	0.0018	0.14	-2.05	B	15,17
		4591.41	7811	29585	3	5	0.011	0.0060	0.27	-1.74	B	15,17
		4613.36	7751	29421	1	3	0.022	0.021	0.32	-1.68	B	15,17
23.	$a^3D - z^3F$ (22)	4350.4	8090	31070	25	35	0.117	0.0466	16.7	0.067	C	2,15
		4351.77	8308	31290	9	11	0.12	0.040	5.2	-0.44	C	2
		4344.51	8095	31106	7	9	0.11	0.040	4.0	-0.55	C	2
		4339.45	7927	30965	5	7	0.0692	0.0274	1.95	-0.864	B	15
		4337.57	7811	30859	3	5	0.0548	0.0258	1.10	-1.112	B	15
		4339.74	7751	30787	1	3	0.0440	0.0372	0.532	-1.429	B	15
		4384.97	8308	31106	9	9	0.027	0.0079	1.0	-1.15	D	2
		4371.28	8095	30965	7	7	0.041	0.012	1.2	-1.09	C	2
		4359.65	7927	30859	5	5	0.054	0.016	1.1	-1.11	C	2
		4351.06	7811	30787	3	3	0.0418	0.0119	0.509	-1.449	B	15
		4412.25	8308	30965	9	7	9.86(-4)	2.24(-4)	0.0293	-2.696	B	15
		4391.76	8095	30859	7	5	0.00288	5.96(-4)	0.0603	-2.380	B	15
		4373.26	7927	30787	5	3	0.00524	9.02(-4)	0.0649	-2.346	B	15



Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	$\nu g g'$	Accuracy	Source
24.	$a^4D - z^4D$ (23)	3910.5	8090	33655	25	25	0.12	0.028	8.9	-0.16	C-	2
		3919.17	8308	33816	9	9	0.092	0.021	2.5	-0.72	C	2
		3908.76	8095	33672	7	7	0.062	0.014	1.3	-1.00	C-	2
		3902.91	7927	33542	5	5	0.035	0.0080	0.51	-1.40	D	2
		3903.17	7811	33424	3	3	0.018	0.0041	0.16	-1.91	D-	2
		3941.50	8308	33672	9	7	0.028	0.0051	0.59	-1.34	C-	2
		3928.65	8095	33542	7	5	0.052	0.0086	0.78	-1.22	C	2
		3921.03	7927	33424	5	3	0.058	0.0080	0.51	-1.40	C	2
		3916.25	7811	33333	3	1	0.097	0.0075	0.29	-1.65	C	2
		3886.80	8095	33816	7	9	0.022	0.0065	0.58	-1.34	C-	2
		3883.29	7927	33672	5	7	0.039	0.012	0.79	-1.21	C	2
		3885.24	7811	33542	3	5	0.039	0.015	0.56	-1.36	C-	2
		3894.04	7751	33424	1	3	0.039	0.026	0.34	-1.58	C-	2
		25.	$a^4D - z^4P$ (24)	3849.54	7927	33897	5	3	0.023	0.0030	0.19	-1.82
3852.22	7811			33763	3	1	0.070	0.0052	0.20	-1.81	E	2
26.	$a^4D - y^4F$ (27)	3021.58	8308	41393	9	11	2.91	0.487	43.6	0.642	B	15
		3015.20	7751	40906	1	3	1.63	0.668	6.63	-0.175	B	15
		3037.05	8308	41225	9	9	0.54	0.075	6.8	-0.17	C	2
		3030.25	8095	41086	7	7	1.1	0.15	10	0.02	C	2
		3020.67	7811	40906	3	3	1.5	0.21	6.1	-0.21	D-	2
		3040.84	8095	40971	7	5	0.74	0.073	5.1	-0.29	D	2
		3031.35	7927	40906	5	3	0.31	0.026	1.3	-0.89	E	2
		27.	$a^4D - x^4P$ (26)	3053.87	8308	41043	9	7	0.797	0.0666	7.84	-0.106
3029.17	7927			40930	5	3	0.38	0.032	1.6	-0.80	E	2
3034.19	8095			41043	7	7	0.35	0.048	3.4	-0.47	D	2
3024.36	7927			40983	5	5	1.27	0.174	8.65	-0.061	B	15
3013.72	7811			40983	3	5	0.83	0.19	5.6	-0.25	C	2
28.	$a^4D - y^4D$ (uv 11)	3005.06	8308	41575	9	7	0.92	0.097	8.6	-0.06	C-	2
		3000.88	8095	41409	7	5	1.6	0.15	10	0.02	C-	2
		2996.57	7927	41289	5	3	2.0	0.16	7.8	-0.10	C	2
		2991.88	7811	41225	3	1	3.0	0.14	4.0	-0.39	D	2
		2967.64	8095	41782	7	9	0.39	0.067	4.6	-0.33	D	2
		2971.10	7927	41575	5	7	0.71	0.13	6.5	-0.18	C	2
		2975.48	7811	41409	3	5	0.89	0.20	5.8	-0.23	C	2
		2960.78	7751	41289	1	3	0.510	0.204	2.00	-0.691	B	15

Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (int. u.)	$\log gf$	Accuracy	Source
29.	$a^1D - x^1D$ (uv 12)	2892.5	8090	42640	25	25	0.93	0.117	27.9	0.467	C-	2
		2889.22	8308	42909	9	9	0.66	0.082	7.1	-0.13	C	2
		2893.25	8095	42648	7	7	0.52	0.065	4.4	-0.34	C	2
		2896.76	7927	42439	5	5	0.30	0.037	1.8	-0.73	C-	2
		2899.20	7811	42293	3	3	0.15	0.019	0.55	-1.24	D-	2
		2911.15	8308	42648	9	7	0.26	0.025	2.2	-0.64	D	2
		2910.89	8095	42439	7	5	0.34	0.031	2.1	-0.66	D	2
		2909.05	7927	42293	5	3	0.68	0.051	2.5	-0.59	C	2
		2905.48	7811	42218	3	1	1.3	0.053	1.5	-0.80	D	2
		2871.63	8095	42909	7	9	0.12	0.018	1.2	-0.89	D-	2
		2879.27	7927	42648	5	7	0.21	0.036	1.7	-0.74	D	2
		2887.00	7811	42439	3	5	0.27	0.055	1.6	-0.78	D	2
		2894.17	7751	42293	1	3	0.33	0.12	1.2	-0.91	D-	2
		30.	$a^1D - w^1P$ (uv 15)	2780.70	8308	44259	9	7	1.4	0.13	11	0.07
2769.90	8095			44187	7	5	1.1	0.090	5.8	-0.20	C	2
2761.74	7927			44126	5	3	0.68	0.047	2.1	-0.63	D	2
2764.36	8095			44259	7	7	0.37	0.042	2.7	-0.53	D	2
2757.09	7927			44187	5	5	0.68	0.078	3.5	-0.41	C	2
2752.85	7811			44126	3	3	0.87	0.098	2.7	-0.53	D	2
2751.58	7927			44259	5	7	0.069	0.011	0.50	-1.26	D-	2
31.	$a^1D - v^1P$ (uv 17)			2716.18	8308	45113	9	7	0.11	0.0092	0.74	-1.08
		2700.59	8095	45113	7	7	0.075	0.0082	0.51	-1.24	D	2
		32.	$a^1D - r^1F$ (uv 18)	2678.15	7927	45256	5	7	0.12	0.018	0.79	-1.05
2671.98	7811			45225	3	5	0.12	0.022	0.57	-1.19	D-	2
2669.36	7751			45202	1	3	0.12	0.039	0.34	-1.41	E	2
2703.48	8308			45286	9	9	0.063	0.0069	0.55	-1.21	D	2
2690.25	8095			45256	7	7	0.085	0.0092	0.57	-1.19	D	2
2680.33	7927			45225	5	5	0.10	0.011	0.47	-1.27	D	2
2673.64	7811			45202	3	3	0.18	0.019	0.51	-1.24	E	2
33.	$a^1D - t^1F$			2701.99	8308	45306	9	11	0.21	0.028	2.2	-0.60
34.	$a^1D - u^1F$	2620.48	7927	46077	5	3	0.19	0.012	0.50	-1.24	E	2
35.	$a^1D - w^1D$ (uv 21)	2622.87	8308	46422	9	9	0.13	0.013	1.0	0.92	D	2
		2626.60	8308	46368	9	7	0.093	0.0075	0.58	1.17	E	2
36.	$a^1D - v^1F$	2629.82	8095	46109	7	5	0.10	0.0077	0.46	1.27	E	2
		2618.27	7927	46109	5	5	0.095	0.0098	0.42	1.31	E	2

## Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (st. u.)	log $gf$	Accu- racy	Source
37.	$a^3D - ({}^3P)$	2625.32	8095	46174	7	7	0.091	0.0094	0.57	-1.18	E	2
38.	$a^3D - w^3P$ (uv 22)	2603.56	8308	46705	9	11	0.062	0.0077	0.59	-1.16	E	2
		2588.19	8095	46721	7	9	0.088	0.011	0.68	-1.10	E	2
		2579.14	7927	46688	5	7	0.11	0.015	0.64	-1.12	D-	2
39.	$a^3D - z^3G$ (uv 23)	2584.67	8308	46986	9	11	0.061	0.0075	0.58	-1.17	E	2
40.	$a^3D - u^3P$ (uv 24)	2591.84	8308	46879	9	7	0.65	0.051	3.9	-0.34	C	2
		2571.74	8095	46968	7	5	0.64	0.045	2.7	-0.50	E	2
		2577.66	8095	46879	7	7	0.26	0.025	1.5	-0.75	D-	2
		2560.70	7927	46968	5	5	0.43	0.042	1.8	-0.68	D-	2
		2549.55	7811	47022	3	3	0.48	0.047	1.2	-0.85	D-	2
41.	$a^3D - v^3D$ (uv 30)	2527.11	8308	47866	9	9	0.53	0.051	3.6	-0.34	E	2
		2508.11	7927	47786	5	5	0.21	0.020	0.81	-1.01	D-	2
		2508.97	7927	47772	5	3	0.38	0.021	0.89	-0.97	C-	2
		2513.62	8095	47866	7	9	0.11	0.014	0.81	-1.01	C	2
42.	$a^3D - ({}^3P)$	2495.08	7811	47878	3	3	0.27	0.025	0.62	-1.12	C	2
43.	$a^3D - u^3P$ (uv 31)	2504.31	8095	48014	7	9	0.45	0.064	3.1	-0.42	C	2
		2496.30	7927	47975	5	7	0.56	0.073	3.0	-0.44	C	2
		2492.57	7811	47918	3	5	0.45	0.070	1.7	-0.68	C	2
		2499.84	7927	47918	5	5	0.16	0.015	0.61	-1.13	E	2
44.	$a^3D - ({}^3P)$	2502.55	8095	48043	7	9	0.22	0.026	1.5	-0.74	D	2
45.	$a^3D - {}^3D$	2479.14	7924	48252	5	7	0.098	0.013	0.51	-1.20	D	2
46.	$a^3D - t^3P$ (uv 26)	2498.60	8308	49812	9	7	0.67	0.045	3.2	-0.39	D-	2
47.	$a^3D - ({}^3P)$	2498.72	8095	49686	7	5	0.29	0.018	1.0	-0.90	D-	2

Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accu- racy	Source
48.	$a^3D - x^3F$ (uv 37)	2389.21	7811	49653	3	5	0.23	0.033	0.77	-1.01	D-	2
49.	$a^3D - x^3F$ (uv 39)	2383.30	8308	50253	9	11	0.41	0.042	3.0	-0.42	D-	2
		2385.72	8308	50211	9	9	0.17	0.014	1.0	-0.89	D-	2
		2375.06	7927	50019	5	3	0.17	0.0085	0.33	-1.37	E	2
50.	$a^3D - u^3D$ (uv 40)	2354.30	8095	50558	7	9	0.081	0.0086	0.47	-1.22	D-	2
51.	$a^3D - r^3D$ (uv 48)	1999.95	8308	58293	9	9	1.4	0.082	4.9	-0.13	D-	2
52.	$a^3G - y^3F$ (31)	4789.32	20520	41393	13	11	0.114	0.0331	6.79	-0.366	B	16
		4903.25	20517	40906	5	3	0.074	0.016	1.3	-1.10	D	10 <sub>n</sub>
53.	$a^3G - x^3P$ (30)	4885.77	20521	40983	7	5	0.0492	0.0126	1.42	-1.055	B	16
54.	$a^3G - z^3H$ (32)	4571.67	20520	42387	13	15	0.036	0.013	2.5	-0.77	D	13
		4648.12	20517	42026	5	7	0.018	0.0082	0.62	-1.39	D	13
55.	$a^3G - t^3P$	4601.02	20524	42252	11	13	0.015	0.0056	0.94	-1.21	D	13
		4600.11	20520	42252	13	13	0.016	0.0051	1.0	-1.18	D	18
56.	$a^3G - z^3G$ (33)	4533.7	20522	42573	45	45	0.205	0.0633	42.5	0.454	B	16,17
		4526.44	20520	42606	13	13	0.175	0.0538	10.4	-0.156	B	17
		4530.73	20524	42589	11	11	0.158	0.0486	7.98	0.272	B	17
		4535.69	20524	42565	9	9	0.149	0.0460	6.18	-0.383	B	17
		4540.49	20521	42539	7	7	0.150	0.0465	4.87	-0.487	B	16,17
		4544.60	20517	42515	5	5	0.169	0.0523	3.91	0.82	B	17
		4529.84	20520	42589	13	11	0.011	0.0030	0.58	-1.41	C+	17
		4535.75	20524	42565	11	9	0.025	0.0063	1.0	1.16	C+	17
		4541.06	20524	42539	9	7	0.034	0.0081	1.1	1.14	B	16,17
		4545.33	20521	42515	7	5	0.034	0.0075	0.79	1.28	B	17
		4527.33	20524	42606	11	13	0.021	0.0077	1.3	1.07	B	17
		4530.68	20524	42589	9	11	0.036	0.014	1.8	0.91	B	17
		4535.13	20521	42565	7	9	0.038	0.015	1.6	0.98	B	16,17
		4539.76	20517	42539	5	7	0.032	0.014	1.0	1.15	B	16,17

Cr I: Allowed transitions -- Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accuracy	Source
57.	$a^4G - y^4G^*$ (35)	4126.51	20520	44746	13	13	0.0671	0.0171	3.03	-0.652	B	16
		4203.59	20517	44900	5	5	0.057	0.015	1.0	-1.12	D	10a
58.	$a^4G - x^4P^*$ (36)	4042.25	20524	45256	9	7	0.0088	0.0017	0.20	-1.82	D	18
		4060.03	20517	45202	5	3	0.012	0.0017	0.12	-2.06	D	18
59.	$a^4G - y^4H^*$ (38)	3963.69	20520	45741	13	15	1.3	0.36	61	0.67	D-	2
		3969.75	20524	45707	11	13	1.2	0.35	50	0.58	D-	2
		3963.90	20521	45615	7	9	1.05	0.32	29	0.35	C-	11
		3991.12	20517	45566	5	7	1.07	0.367	23.5	0.252	B	16
		3976.02	20520	45663	13	11	0.0023	4.6(-4)	0.078	-2.22	D	11
60.	$a^4G - x^4G^*$ (43)	3743.89	20620	47222	13	13	0.761	0.160	25.6	0.318	B	16
		3757.66	20521	47126	7	7	0.413	0.0875	7.58	-0.213	B	16
		3768.24	20517	47047	5	5	0.510	0.109	6.74	-0.265	B	16
		3758.04	20524	47126	9	7	0.116	0.0192	2.14	-0.763	B	16
		3768.73	20521	47047	7	5	0.119	0.0181	1.57	-0.897	B	16
		3744.49	20524	47222	11	13	0.0501	0.0124	1.69	-0.884	B	16
		3757.17	20517	47126	5	7	0.0616	0.0182	1.13	-1.040	B	16
		61.	$a^4G - u^4P^*$ (47)	3639.80	20620	47986	13	11	1.8	0.30	47	0.59
62.	$a^4P - x^4P^*$ (59)	5241.47	21857	40920	3	3	0.0067	0.0023	0.14	-2.06	D	18
		5238.97	21848	40990	5	3	0.0401	0.00991	0.855	-1.306	B	16
63.	$a^4P - y^4D^*$ (60)	5013.31	21841	41782	7	9	0.035	0.017	2.0	-0.92	D	10a
64.	$a^4P - x^4D^*$ (61)	4745.31	21841	42909	7	9	0.020	0.0087	0.95	-1.22	D	10a
		4806.25	21848	42648	5	7	0.0056	0.0027	0.21	-1.87	D-	13
65.	$a^4P - z^4S^*$ (62)	4697.04	21841	43125	7	5	0.053	0.012	1.2	-1.06	D	18
		4700.60	21857	43125	3	5	0.0236	0.0185	0.860	-1.255	B	16

Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accu- racy	Source
66.	$a^1P - a^1P^o$ (63)	4460.76	21848	44259	5	7	0.015	0.0065	0.48	-1.49	D	18
		4477.05	21857	44187	3	5	0.013	0.0065	0.29	-1.71	D	18
67.	$a^1P - c^1P^o$ (64)	4341.46	21848	44875	5	5	0.0064	0.0018	0.13	-2.04	E	13
		4382.86	21857	44667	3	3	0.030	0.0086	0.37	-1.59	D-	13
		4340.14	21841	44875	7	5	0.12	0.024	2.4	-0.77	D	13
		4381.11	21848	44667	5	3	0.10	0.018	1.3	-1.05	D	10 <sub>n</sub>
		4297.06	21848	45113	5	7	0.048	0.019	1.3	-1.03	D	13
		4343.17	21857	44875	3	5	0.036	0.017	0.73	-1.29	D	13
68.	$a^1P - w^1D^o$ (66)	4081.74	21857	46350	3	5	0.012	0.0050	0.20	-1.82	D	18
69.	$a^1P - (1^1P)$	4109.58	21848	46174	5	7	0.031	0.011	0.74	-1.26	D	18
70.	$a^1P - u^1P^o$ (67)	3981.24	21857	46968	3	5	0.11	0.045	1.8	-0.87	D	10 <sub>n</sub>
71.	$a^1P - y^1P^o$ (81)	4619.54	24093	45734	5	5	0.16	0.051	3.9	-0.59	D	13
		4501.79	23512	45719	3	3	0.10	0.030	1.4	-1.04	D	13
		4622.76	24093	45719	5	3	0.11	0.021	1.6	-0.98	D	18
		4498.73	23512	45734	3	5	0.079	0.040	1.8	-0.92	D	18
		4432.16	23163	45719	1	3	0.18	0.16	2.3	-0.80	D	18
72.	$a^1P - y^1F^o$	4563.43	24093	46000	5	7	0.0055	0.0024	0.18	-1.92	D-	13
73.	$a^1P - (1^1P)$	4362.97	23163	46077	1	3	0.032	0.027	0.39	-1.56	D-	13
74.	$a^1P - w^1D^o$ (83)	4491.86	24093	46350	5	5	0.034	0.010	0.76	-1.29	D	18
		4387.38	23512	46298	3	3	0.054	0.016	0.68	-1.33	D	13
		4377.55	23512	46350	3	5	0.033	0.016	0.69	-1.32	D	18
		4321.25	23163	46298	1	3	0.034	0.029	0.41	-1.54	D	13
75.	$a^1P - (1^1P)$	4424.10	23512	46109	3	5	0.057	0.028	1.2	-1.08	D	13
76.	$a^1P - (1^1P)$	4527.45	24093	46174	5	7	0.062	0.027	2.0	-0.87	D	13

Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	$\log gf$	Accu- racy	Source
77.	$a^3P - z^3S^*$	4347.49	24093	47088	5	3	0.019	0.0032	0.23	-1.79	D-	13
78.	$z^3P - e^3S$ (93)	7400.22 7355.93	23396 23305	36896 36896	7 5	7 7	0.135 0.0914	0.111 0.104	18.9 12.6	-0.111 -0.285	B B	16 16
79.	$z^3P - e^3D$ (94)	5328.36 5297.37 5329.17 5297.99 5329.76	23499 23396 23499 23396 23499	42251 42258 42258 42256 42256	9 7 9 7 9	11 9 9 7 7	0.62 0.388 0.225 0.30 0.0538	0.32 0.210 0.0950 0.12 0.0178	51 25.6 15.1 15 2.81	0.46 0.167 -0.064 -0.06 -0.796	D B B D B	9a 16 16 18 16
80.	$z^3P - f^3S$ (95)	4491.69 4475.36	23396 23305	45643 45643	7 5	7 7	0.044 0.030	0.013 0.013	1.4 0.93	-1.03 -1.20	D D	18 18
81.	$z^3P - f^3D$ (96)	4261.35 4272.93 4293.58 4299.72 4305.47 4319.66	23499 23396 23499 23396 23305 23305	46950 46783 46783 46637 46525 46449	9 7 9 7 5 5	11 9 9 7 5 3	0.066 0.047 0.025 0.061 0.076 0.18	0.022 0.017 0.0070 0.017 0.021 0.030	2.8 1.6 0.80 1.7 1.5 2.1	-0.70 -0.94 -1.20 -0.93 -0.93 -0.82	D D D D D D	13 13 18 13 10a 10a
82.	$z^3P - g^3D$ (97)	4097.69 4111.33	23305 23396	47702 47702	5 7	7 7	0.063 0.12	0.019 0.001	1.3 2.9	-1.03 -0.97	D D	18 18
83.	$a^3H - z^3H^*$ (98)	4727.13 4693.94 4664.29 4695.14	24300 24056 23934 24056	45349 45354 45350 45349	13 11 9 11	13 11 9 13	0.051 0.084 0.036 0.015	0.017 0.011 0.012 0.0000	3.4 1.9 1.6 1.0	-0.66 -0.91 -0.93 -1.18	D D D D	10a 18 13 18
84.	$a^3H - y^3H^*$	4617.37 4648.33 4611.06	24056 24300 23934	45707 45707 45615	11 13 9	13 13 9	5.1(-4) 0.0015 0.0020	1.9(-4) 4.9(-4) 6.4(-4)	0.082 0.087 0.087	-2.97 -2.20 -2.24	D- D- D-	11 11 11
85.	$a^3H - y^3P^*$ (100)	4543.73 4530.46	24056 23934	46058 46000	11 9	9 7	0.010 0.0007	0.0025 0.0016	0.42 0.22	-1.56 -1.84	D- D-	13 18

## Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (st. u.)	log $gf$	Accu- racy	Source
86.	$a^3H - w^3F$ (102)	4442.28	24200	46705	13	11	0.019	0.0048	0.90	-1.21	D	13
		4410.97	24056	46721	11	9	0.023	0.0055	0.88	-1.22	D	13
		4393.54	23934	46688	9	7	0.007	0.002	0.2	-1.8	E	13
87.	$a^3H - z^3G$ (103)	4375.34	24056	46905	11	9	0.072	0.017	2.7	-0.73	D	10a
		4363.13	23934	46847	9	7	0.16	0.036	4.6	-0.50	D	13
88.	$a^3H - y^3G$ (104)	4374.17	24200	47055	13	11	0.103	0.0250	4.68	-0.488	C-	11
		4346.83	24056	47055	11	9	0.090	0.021	3.3	-0.64	D	18
		4325.08	23934	47048	9	7	0.14	0.031	3.9	-0.56	D	13
89.	$a^3H - z^3I$ (105)	4255.50	24200	47693	13	15	0.061	0.019	3.5	-0.60	D	13
90.	$a^3H - x^3H$ (106)	4211.48	24056	47794	11	11	0.0071	0.0019	0.29	-1.68	D	18
91.	$a^3H - v^3H$ (114)	3238.09	24056	54930	11	11	0.20	0.032	3.7	-0.46	D	12
		3237.73	23934	54811	9	9	1.3	0.20	19	0.25	D	12
92.	$a^3H - x^3I$ (115)	3163.76	24200	55799	13	15	0.60	0.10	14	0.13	B	17
		3155.16	24056	55741	11	13	0.57	0.10	11	0.04	B	17
		3148.44	23934	55686	9	11	0.56	0.10	9.5	-0.04	B	17
		3169.58	24200	55741	13	13	0.022	0.0033	0.45	-1.37	E	17
		3160.62	24056	55686	11	11	0.027	0.0041	0.46	-1.35	D-	17
93.	$b^3D - y^3D$ (119)	5844.60	24304	41409	7	5	0.0068	0.0025	0.23	-1.76	D	18
		5719.62	24304	41782	7	9	0.00496	0.00313	0.412	-1.660	B	16
		5638.68	24287	41409	3	5	0.0065	0.0055	0.32	-1.78	D	18
94.	$b^3D - x^3F$ (124)	4764.65	24304	45286	7	9	0.0073	0.0032	0.35	-1.65	D	13
		4770.68	24300	45256	5	7	0.0098	0.0047	0.37	-1.63	D	18



## Cr: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{12}$	S (at. u.)	log $g_f$	Accu- racy	Source
95.	$b^3D - ({}^3P)$	4755.14	24282	45306	9	11	0.0096	0.0040	0.56	-1.45	D	13
96.	$b^3D - u^3D$ (126)	4515.44	24282	46422	9	9	0.022	0.0067	0.90	-1.22	D	13
		4530.93	24304	46368	7	7	0.0065	0.0029	0.21	-1.85	D-	13
		4531.24	24287	46350	3	5	0.010	0.0051	0.23	-1.81	D-	13
97.	$b^3D - ({}^3P)$	4584.76	24304	46100	7	5	0.0075	0.0017	0.18	-1.93	D-	13
		4583.90	24300	46100	5	5	0.016	0.0050	0.38	-1.60	D-	13
98.	$b^3D - ({}^3P)$	4571.10	24304	46174	7	7	0.0095	0.0030	0.31	-1.68	D-	13
99.	$b^3D - u^3P$ (127)	4459.75	24304	46721	7	9	0.084	0.032	3.3	-0.65	D	13
		4465.37	24300	46688	5	7	0.050	0.025	1.8	-0.91	D	13
		4462.79	24277	46678	1	3	0.056	0.050	0.74	-1.30	D	13
		4467.57	24300	46677	5	5	0.037	0.011	0.81	-1.28	D	13
		4464.66	24287	46678	3	3	0.049	0.015	0.65	-1.36	D	13
100.	$b^3D - u^3P$ (129)	4424.29	24282	46879	9	7	0.21	0.048	6.3	-0.37	D	13
		4411.11	24304	46968	7	5	0.13	0.027	2.8	-0.72	D	13
		4390.82	24300	47022	5	3	0.098	0.017	1.2	-1.07	D	10m
		4428.52	24304	46879	7	7	0.055	0.016	1.7	-0.76	D	13
		4410.31	24300	46968	5	5	0.067	0.020	1.4	-1.01	D	13
		4397.24	24287	47022	3	3	0.10	0.029	1.3	-1.06	D	10m
101.	$b^3D - x^3G$ (130)	4356.77	24282	47229	9	11	0.022	0.0077	0.99	-1.16	D	13
		4369.25	24304	47190	7	9	0.021	0.0077	0.78	-1.27	D	13
		4379.77	24300	47126	5	7	0.019	0.0076	0.55	-1.42	D	13
102.	$b^3D - v^3D$ (131)	4238.96	24282	47866	9	9	0.074	0.020	2.5	-0.74	D	10m
		4252.24	24304	47814	7	7	0.051	0.014	1.4	-1.01	D	13
		4249.34	24282	47814	9	7	0.028	0.0059	0.74	-1.28	D	13
		4257.35	24304	47786	7	5	0.029	0.0067	0.56	-1.40	D	13
		4242.84	24304	47756	7	9	0.018	0.0062	0.61	-1.36	D	13
103.	$b^3D - ({}^3P)$	4235.99	24277	47878	1	3	0.066	0.053	0.74	-1.27	D	13
		4237.72	24287	47878	3	3	0.040	0.011	0.45	-1.49	D	13

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Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$f_1$	$g_2$	$A_{21}$ (10 <sup>7</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accu- racy	Source
104.	b 'D - u 'F' (132)	4222.75	24300	47975	5	7	0.056	0.021	1.5	-0.96	D	18
		4230.49	24287	47918	3	5	0.051	0.023	0.95	-1.16	D	13
105.	b 'D - u 'D' (139)	3904.80	24282	50558	9	9	0.69	0.15	17	0.13	D	9a
106.	a 'G - z 'H' (143)	4922.28	25039	45349	11	13	0.40	0.17	30	0.27	D	9a
		4887.01	24898	45354	9	11	0.32	0.14	20	0.10	D	9a
		4870.79	24834	45359	7	9	0.35	0.16	18	0.05	D	9a
		4885.97	24898	45359	9	9	0.0244	0.00874	1.27	-1.104	B	16
107.	a 'G - y 'H' (144)	4836.85	25039	45707	11	13	0.0160	0.00665	1.16	-1.136	B	16
		4814.25	24898	45663	9	11	0.0161	0.0068	0.98	-1.211	C-	11
		4810.71	24834	45615	7	9	0.016	0.0071	0.79	-1.30	D	11
		4825.50	24898	45615	9	9	0.0036	0.0013	0.18	-1.95	D-	11
108.	a 'G - y 'F' (145)	4756.09	25039	46058	11	9	0.40	0.11	19	0.09	D	18
		4737.33	24898	46000	9	7	0.338	0.0885	12.4	-0.099	B	16
		4730.69	24834	45966	7	5	0.393	0.0918	10.0	-0.192	B	16
		4724.40	24898	46058	9	9	0.0614	0.0205	2.88	-0.733	B	16
		4723.06	24834	46000	7	7	0.093	0.031	3.4	-0.66	D	10a
109.	a 'G - u 'D' (147)	4656.18	24898	46368	9	7	0.0327	0.00826	1.14	-1.129	B	16
		4646.50	24834	46350	7	5	0.058	0.013	1.4	-1.03	D	13
110.	a 'G - z 'F'	4698.94	24834	46109	7	5	0.022	0.0052	0.56	-1.44	D	13
111.	a 'G - z 'G' (149)	4541.51	24834	46847	7	7	0.038	0.012	1.2	-1.08	D	13
112.	a 'G - y 'G' (150)	4540.72	25039	47055	11	11	0.314	0.0970	15.9	0.028	B	16
		4511.90	24898	47055	9	9	0.165	0.0504	6.74	0.343	B	16
		4500.29	24834	47048	7	7	0.21	0.064	6.6	0.35	D	13
113.	a 'G - u 'F'	4330.76	24834	47918	7	5	0.014	0.0028	0.28	1.71	D	13

Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{os}$	S (at. u.)	log $g f$	Accuracy	Source
114.	$a^4G - y^4H$ (154)	427.87	25039	48445	11	13	0.053	0.677	2.6	-0.73	D	10a
		4269.96	24898	48310	9	11	0.052	0.911	1.4	-1.02	D	13
		4262.37	24834	48288	7	9	0.024	0.0084	0.83	-1.23	D	13
115.	$a^4G - x^4G$ (155)	4213.18	24834	48562	7	9	0.079	0.927	2.6	-0.72	D	10a
116.	$a^4F - z^4H$ (166)	4954.81	25177	45354	9	11	0.12	0.956	8.2	-0.30	D	10a
		4906.34	25106	45359	7	9	0.14	0.966	7.5	-0.34	D	10a
		4953.73	25177	45359	9	9	0.0085	0.0031	0.46	-1.55	D	18
117.	$a^4F - y^4H$ (167)	4880.04	25177	45663	9	11	0.0081	0.0035	0.51	-1.50	D	18
		4874.65	25106	45615	7	9	0.0069	0.0032	0.36	-1.66	D	11
118.	$a^4F - y^4F$ (168)	4754.73	24941	45966	5	5	0.026	0.0088	0.69	-1.36	D	13
		4901.02	25177	46000	9	7	0.306	0.0822	11.7	-0.131	B	16
		4792.49	25106	45966	7	5	0.26	0.064	7.1	-0.35	D	10a
119.	$a^4F - ({}^4P)$	4729.84	24941	46077	5	3	0.17	0.035	2.7	-0.76	D	10a
120.	$a^4F - w^4D$ (170)	4717.67	25177	46368	9	7	0.0077	0.0020	0.28	-1.75	D-	13
		4706.09	25106	46350	7	5	0.035	0.0084	0.91	-1.23	D	18
		4680.95	24941	46298	5	3	0.16	0.031	2.4	-0.81	D	18
121.	$a^4F - ({}^4P)$	4722.65	24941	46109	5	5	0.0069	0.0023	0.18	-1.94	D-	13
122.	$a^4F - x^4G$ (172)	4584.10	25177	46906	9	11	0.021	0.0081	1.1	-1.14	D	13
		4586.15	25106	46906	7	9	0.027	0.011	1.2	-1.12	D	13
		4563.66	24941	46847	5	7	0.022	0.010	0.76	-1.30	D	13
123.	$a^4F - y^4G$ (172)	4564.82	25106	47066	7	9	0.020	0.0080	0.84	-1.25	D	18
		4569.62	25177	47066	9	9	0.082	0.026	3.5	-0.64	D	13
		4566.16	25106	47048	7	7	0.077	0.024	2.5	-0.78	D	13
		4570.99	25177	47048	9	7	0.0043	0.0010	0.14	-2.08	E	13

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Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	S (at. u.)	log $g f'$	Accu- racy	Source
124.	$a^3F - ^3D'$	4302.57	25177	48252	9	7	0.021	0.0046	0.59	-1.38	D	13
		4325.65	25106	48218	7	5	0.028	0.0056	0.56	-1.41	D	13
		4296.30	24941	48210	5	3	0.032	0.0053	0.38	-1.58	D-	13
		4288.40	24941	48252	5	7	0.028	0.011	0.76	-1.27	D	13
125.	$a^3F - y^3H'$ (177)	4321.62	25177	48310	9	11	0.017	0.0058	0.74	-1.28	D	13
		4312.48	25106	48288	7	9	0.017	0.0061	0.61	-1.37	D	13
126.	$a^3F - x^3G'$ (178)	4234.52	25177	48786	9	11	0.022	0.0072	0.91	-1.19	D	13
127.	$a^3F - ^3F'$	4261.63	25177	48636	9	7	0.064	0.014	1.7	-0.91	D	13
128.	$x^3F' - f^3D$ (186)	4718.43	25771	46959	13	11	0.34	0.095	19	0.09	D	18
		4708.02	25549	46783	11	9	0.431	0.117	20.0	0.110	B	16
		4698.46	25360	46637	9	7	0.22	0.057	7.9	-0.29	D	13
		4689.38	25206	46525	7	5	0.23	0.054	5.8	-0.42	D	10 <sub>n</sub>
		4669.34	25549	46959	11	11	0.0908	0.0297	5.02	-0.486	B	16
		4663.33	25011	46449	3	3	0.20	0.065	3.0	-0.71	D	13
		4628.48	25360	46959	9	11	0.012	0.0045	0.62	-1.39	D	18
		4633.27	25206	46783	7	9	0.020	0.0082	0.88	-1.24	D	18
		4639.52	25089	46637	5	7	0.095	0.043	3.3	-0.67	D	10 <sub>n</sub>
		4646.80	25011	46525	3	5	0.078	0.042	1.9	-0.90	D	13
		4654.76	24971	46449	1	3	0.091	0.089	1.4	-1.05	D	13
129.	$x^3P' - e^3D$ (188)	5787.97	26796	44069	5	7	0.235	0.165	15.7	-0.083	B	16
		5785.02	26788	44069	7	7	0.119	0.0596	7.94	-0.380	B	16
		5783.89	26796	44081	5	5	0.202	0.101	9.65	-0.295	B	16
		5783.11	26902	44089	3	3	0.21	0.11	6.0	-0.50	D	18
130.	$b^3P - y^3P'$ (191)	5400.50	27223	45734	5	5	0.16	0.068	6.0	-0.47	D	10 <sub>n</sub>
131.	$b^3P - u^3D'$ (193)	5214.14	27176	46350	3	5	0.089	0.061	3.1	-0.74	D	18
132.	$b^3P - ^3F'$	5293.38	27223	46109	5	5	0.021	0.0087	0.76	-1.36	D	18

Cr I: Allowed transitions - Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{\lambda}$	S (at. u.)	log gf	Accuracy	Source
133.	$b^3P - x^3P$ (195)	4707.73	27223	48459	5	5	0.031	0.010	0.80	-1.29	D	13
		4697.38	27176	48459	3	5	0.031	0.017	0.79	-1.29	D	13
134.	$b^3P - x^3D$ (196)	4575.11	27176	49028	3	5	0.068	0.036	1.6	-0.97	D	13
		4611.96	27163	49040	1	3	0.060	0.077	1.2	-1.12	D	13
		4584.94	27223	49028	5	5	0.039	0.012	0.93	-1.21	D	13
135.	$b^3P - y^3F$ (197)	4492.31	27223	49477	5	3	0.447	0.0811	6.00	-0.292	B	16
		4482.88	27176	49477	3	3	0.30	0.090	4.0	-0.57	D	10a
		4480.27	27163	49477	1	3	0.10	0.090	1.3	-1.04	D	13
136.	$b^3P - w^3D$ (198)	4338.80	27223	50264	5	7	0.070	0.028	2.0	-0.96	D	13
		4345.08	27176	50184	3	5	0.098	0.046	2.0	-0.96	D	13
		4357.51	27163	50106	1	3	0.068	0.068	0.83	-1.24	D	13
		4353.94	27223	50184	5	5	0.13	0.037	2.7	-0.73	D	13
		4368.90	27223	50106	5	3	0.068	0.010	0.72	-1.30	D	13
137.	$x^3D' - f^3D$ (201)	5243.38	27382	46449	5	3	0.219	0.0542	4.68	-0.567	B	16
		5177.42	27650	46950	9	11	0.061	0.030	4.6	-0.57	D	10a
		5192.01	27382	46937	5	7	0.14	0.081	6.9	-0.30	D	10a
		5200.20	27300	46525	3	5	0.11	0.073	3.7	-0.66	D	13
138.	$b^3G - x^3H$ (203)	5702.30	27817	45349	11	13	0.0340	0.0196	4.34	-0.667	B	16
		5628.64	27597	45350	7	9	0.0306	0.0241	3.13	-0.772	B	16
139.	$b^3G - y^3H$	5686.06	27817	45707	11	13	0.0011	6.1(-4)	0.12	-2.17	Z	11
		5666.56	27704	45663	9	11	0.0015	8.5(-4)	0.14	-2.12	D	11
		5648.61	27597	45615	7	9	0.0019	0.0011	0.14	-2.10	D-	11
		5681.60	27704	45615	9	9	0.0019	8.9(-4)	0.15	-2.10	Z	11
140.	$b^3G - y^3P$ (204)	5442.40	27597	45066	7	5	0.039	0.012	1.6	-1.06	D	13
141.	$b^3G - z^3G$ (206)	5193.50	27597	46847	7	7	0.067	0.027	3.2	-0.72	D	10a

Cr: Allowed transitions - Continued

No.	Multiplet	$\lambda$ (Å)	$E$ (cm <sup>-1</sup> )	$E_1$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>6</sup> s <sup>-1</sup> )	$A_{10}$	$S$ (rel. $\lambda$ )	log $gf$	Accuracy	Source
142	$\delta^4 G - y^4 G$ (297)	5196.45	27817	47055	11	11	0.12	0.045	9.1	-0.27	D	11
		5139.60	27597	47048	7	7	0.13	0.050	8.9	-0.46	D	10a
143	$\delta^4 G - y^4 H$ (208)	4652.52	27597	48288	7	9	0.617	0.0054	0.90	-1.42	D	13
144	$\delta^4 G - x^4 F$ (212)	4587.10	27817	49627	11	9	0.027	0.0055	1.4	-1.03	D	18
		4555.31	27704	49679	7	7	0.079	0.0076	0.95	-1.26	D	18
145	$\delta^4 G - x^4 F$	4301.19	27817	51069	11	5	0.26	0.039	9.2	-0.19	D	13
		4290.52	27704	51056	9	7	0.13	0.041	5.2	-0.43	D	13
		4291.97	27597	50890	7	5	0.24	0.047	4.7	-0.48	D	13
		4280.89	27597	50950	7	7	0.015	0.0052	0.51	-1.44	D	13
146	$y^4 P - e^4 D$ (212)	6978.46	27935	42261	9	11	0.173	0.154	51.9	0.142	B	16
		6979.81	27935	42278	9	9	0.050	0.047	4.9	-0.41	D	18
		6925.22	27820	42254	7	7	0.093	0.067	11	-0.33	D	18
		6882.40	27729	42255	5	5	0.119	0.0843	9.55	-0.275	B	16
		6880.91	27935	42256	9	7	0.015	0.0064	1.7	-1.12	D	18
		6883.05	27729	42253	5	5	0.178	0.0760	8.61	-0.420	B	16
147	$y^4 P - f^4 D$ (225)	5272.01	27820	46763	7	9	0.191	0.0541	6.57	-0.422	B	16
		5267.19	27729	46657	5	7	0.0422	0.0248	2.16	-0.907	B	16
		5264.19	27935	46793	9	9	0.3535	0.0226	3.55	-0.692	B	16
		5312.88	27820	46757	7	7	0.0926	0.0392	4.80	-0.562	B	16
		5316.79	27729	46525	5	5	0.0967	0.0410	3.59	-0.688	B	16
		5344.77	27820	46565	7	5	0.041	0.012	1.5	-1.06	D	18
		5340.46	27729	46449	7	3	0.145	0.0372	3.27	-0.731	B	16
148	$a^4 D - w^4 G$ (210)	4775.12	27837	49573	7	9	0.029	0.013	1.4	-1.05	D	18
		4797.68	27682	49520	5	7	0.013	0.0063	0.50	-1.50	D	13
149	$a^4 D - x^4 F$ (231)	4764.28	27837	49621	7	9	0.17	0.075	8.2	-0.28	D	18
		4767.86	27682	49650	5	7	0.12	0.059	4.6	-0.53	D	18
		4757.58	27837	49650	7	7	0.051	0.017	1.9	-0.92	D	13
		4761.26	27682	49653	5	5	0.056	0.019	1.5	-1.02	D	13

Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accu- racy	Source
150.	$a^3D - w^3D$ (233)	4622.47	29637	50264	7	7	0.41	0.13	14	-0.04	D	18
		4665.90	29679	50106	3	3	0.30	0.098	4.5	-0.53	D	13
		4639.70	29637	50184	7	5	0.077	0.018	1.9	-0.91	D	13
151.	$a^3D - w^3P$	4480.36	29637	50950	7	7	0.035	0.011	1.1	-1.13	D	13
152.	$a^3D - w^3P$ (234)	4413.86	29637	51287	7	5	0.27	0.067	5.8	-0.00	D	18
		4443.72	29679	51177	3	1	0.45	0.044	1.9	-0.88	D	13
		4422.70	29682	51287	5	5	0.27	0.079	5.8	-0.00	D	13
		4429.93	29679	51247	3	3	0.24	0.071	3.1	-0.67	D	13
153.	$y^4P - f^4D$ (237)	5261.76	29825	48825	7	9	0.13	0.460	8.4	-0.32	D	10a
154.	$z^4P - f^4D$ (239)	5604.72	31106	48082	9	7	0.14	0.054	9.2	-0.31	D	18
		5642.00	31106	48825	9	9	0.034	0.016	2.7	-0.83	D	18
		5649.38	30865	48082	7	7	0.051	0.024	3.2	-0.77	D	18
		5648.25	30850	48550	5	5	0.042	0.020	1.9	-1.00	D	18
155.	$z^4P - e^4P$ (240)	4275.98	31280	54600	11	11	0.22	0.060	9.3	-0.18	D	13
156.	$b^3D - w^3P$ (230)	4944.57	31028	51247	5	3	0.13	0.029	2.4	-0.34	D	18
		4946.80	31049	51177	3	1	0.30	0.087	1.5	-0.96	D	18
157.	$a^3I - y^3I$ (244)	4625.91	31049	52061	13	13	0.12	0.008	7.5	-0.31	D	18
		4641.96	31065	52502	11	11	0.000	0.019	3.3	-0.07	D	18
158.	$a^3I - ^3G$	4614.51	31065	52720	11	9	0.087	0.015	2.5	-0.79	D	13
159.	$a^3I - x^3H$ (246)	4578.33	31049	52085	13	11	0.040	0.011	2.1	-0.26	D	18
		4569.24	31065	52968	11	9	0.10	0.026	4.3	-0.54	D	18

Cr I: Allowed transitions -- Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$L_1$	$L_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (int. u.)	$\log gf$	Accuracy	Source
160.	$a^1P - v^1G^o$	4370.87	31055	53926	11	9	0.050	0.012	1.9	-0.89	D	13
161.	$a^1P - z^1K^o$ (247)	4263.15	31048	54498	15	17	0.64	0.20	42	0.47	D	13
		4280.42	31049	54405	13	15	0.47	0.15	27	0.29	D	10 <sub>m</sub>
		4297.75	31055	54317	11	13	0.49	0.16	25	0.25	D	10 <sub>m</sub>
		4296.63	31049	54317	13	13	0.028	0.0077	1.4	-1.00	D	13
162.	$a^1P - z^1P^o$ (251)	4039.10	31048	55799	15	15	0.67	0.16	33	0.39	B	17
		4048.78	31049	55741	13	13	0.64	0.16	27	0.31	B	17
		4058.78	31055	55686	11	11	0.67	0.17	24	0.26	B	17
		4057.83	31049	55686	13	11	0.0072	0.0015	0.26	-1.71	D	11
		4039.29	31049	55799	13	15	0.060	0.017	2.9	-0.66	D	17
		4049.78	31055	55741	11	13	0.056	0.016	2.4	-0.75	D	17
163.	$a^1P - z^1G^o$	8916.24	31393	42606	11	13	0.0025	0.0035	1.1	-1.41	D	17
		8939.21	31355	42539	5	7	9.9(-4)	0.0017	0.24	-2.08	D	17
		8955.76	31352	42515	3	5	0.0020	0.0040	0.35	-1.92	D	17
164.	$a^1P - s^1D^o$ (267)	4490.55	31378	53641	9	7	0.39	0.092	12	-0.08	D	13
165.	$a^1P - v^1G^o$ (268)	4001.44	31378	56262	9	11	0.68	0.20	24	0.26	D	10 <sub>m</sub>
166.	$a^1I - z^1K^o$	4370.76	32097	54970	13	15	0.025	0.0083	1.5	-0.97	D	13
167.	$a^1I - v^1P^o$	4268.79	32097	55517	13	13	0.17	0.046	8.5	-0.22	D	13
168.	$a^1I - u^1H^o$ (272)	4204.48	32097	55875	13	11	0.21	0.070	13	-0.04	D	18
169.	$b^1P - y^1G^o$	7170.56	33113	47055	9	11	0.0025	0.0024	0.50	-1.67	E	11
170.	$b^1P - v^1G^o$	4819.30	33061	52805	7	7	0.13	0.045	5.0	-0.50	D	13
171.	$b^1P - v^1H^o$	4582.40	33113	54930	9	11	0.032	0.012	1.7	-0.46	D	13



## Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{os}$	S (at. u.)	log $g f$	Accu- racy	Source
172.	$b^3P - a^3P$ (275)	4524.84	33113	55207	9	9	0.11	0.094	4.5	-0.52	D	13
		4553.95	33040	54993	5	5	0.12	0.037	2.8	-0.73	D	13
173.	$b^3P - c^3G$ (279)	4065.71	33113	57702	9	11	0.35	0.11	13	-0.02	D	18
174.	$b^3P - a^3P$ (280)	4495.28	33113	55353	9	7	0.20	0.047	6.3	-0.37	D	13
175.	$z^3D - f^3D$ (282)	6661.10	33206	48825	9	9	0.11	0.072	14	-0.19	D	18
		6669.27	33000	48662	7	7	0.050	0.039	6.0	-0.56	D	18
176.	$z^3D - e^3P$ (283)	4796.15	33816	54660	9	11	0.13	0.055	7.8	-0.31	D	13
177.	$z^3P - e^3D$ (290)	4757.31	34190	55205	5	7	0.12	0.057	4.5	-0.55	D	13
		4743.12	33897	54975	3	5	0.080	0.045	2.1	-0.87	D	13
178.	$b^3I - ^3K$	4752.07	33763	54900	13	13	0.62	0.21	43	0.44	D	13
179.	$b^3I - (^3P)$	4505.60	33763	55517	13	13	0.47	0.15	30	0.29	D	10a
180.	$b^3I - z^3I$	4548.65	33763	55741	13	13	0.028	0.0006	1.7	-0.95	E	17
181.	$b^3I - (^3P)$	4514.26	33763	55908	13	13	0.11	0.034	6.5	-0.26	D	13
182.	$b^3I - y^3H$	4506.84	33763	55945	13	11	0.27	0.060	13	-0.05	D	10a
183.	$c^3D - a^3P$	4699.59	33925	55207	7	9	0.13	0.055	6.0	-0.41	D	13
		4741.09	33907	54993	3	5	0.22	0.12	5.8	-0.43	D	13
184.	$c^3D - u^3P$	4641.49	33925	55474	7	5	0.038	0.0088	0.94	-1.21	D	13
185.	$c^3D - (^3P)$	4327.25	33925	56996	5	7	0.20	0.079	5.6	-0.40	D	13

Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>7</sup> s <sup>-1</sup> )	$f_{\lambda}$	$S$ (ml. u.)	log $gf$	Accu- racy	Source
186.	c 'D - u 'P'	4317.91	33935	57088	7	5	0.11	0.022	2.2	-0.81	D	13
		4309.73	33936	57133	5	3	0.17	0.028	2.0	-0.85	D	13
187.	c 'D - i 'P'	4283.00	33935	57276	7	7	0.088	0.024	2.4	-0.77	D	13
188.	c 'D - t 'G' (294)	4232.23	33936	57557	5	7	0.17	0.064	4.5	-0.50	D	13
189.	b 'H - x 'T'	5032.54	35934	55799	13	15	0.020	0.0088	1.9	-0.94	E	17
		5034.65	35984	55741	11	13	0.017	0.0076	1.4	-1.08	E	17
		5045.04	35871	55686	9	11	0.018	0.0064	1.3	-1.12	D	11
190.	b 'H - t 'G' (303)	4592.55	35934	57702	13	11	0.13	0.035	6.8	-0.34	D	13
191.	b 'H - i 'P'	4606.36	35984	57587	11	9	0.12	0.031	5.2	-0.46	D	13
192.	b 'H - t 'H' (304)	4376.80	35934	58775	13	13	0.32	0.092	17	0.08	D	13
		4373.65	35871	58728	9	9	0.28	0.080	10	-0.14	D	13
193.	b 'H - u 'T' (305)	4165.52	35984	59884	11	13	0.75	0.23	35	0.40	D	10 <sub>m</sub>
194.	d 'F - i 'P'	4838.42	36559	57221	5	5	0.11	0.039	3.1	-0.71	D	13
195.	d 'F - i 'P'	4823.90	36552	57276	7	7	0.12	0.042	4.7	-0.53	D	13
196.	d 'F - i 'P'	4816.13	36578	57335	9	9	0.18	0.061	8.7	-0.26	D	18
197.	d 'F - i 'P'	4510.02	36559	58725	5	3	0.0041	7.5 × 10 <sup>-4</sup>	0.056	-2.43	E	13
198.	c 'G <sub>2</sub> - x 'F'	4307.67	37234	60441	11	13	0.082	0.027	4.2	-0.53	D	13
199.	c 'G <sub>2</sub> - i 'P'	4302.78	37234	60468	11	11	0.25	0.069	11	0.12	D	13

## Cr I: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_u$ (cm <sup>-1</sup> )	$E_l$ (cm <sup>-1</sup> )	$g_u$	$g_l$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $gf$	Accuracy	Source
200.	$e^4G - e^4G'$	4296.05	37244	60504	9	9	0.25	0.072	9.2	-0.19	D	13
		4296.11	37234	60504	11	9	0.089	0.020	3.1	-0.65	D	13
201.	$e^4S - x^4S$ (310)	4503.04	37883	60004	5	3	0.083	0.015	1.1	-1.12	D	13
202.	$a^4H - ({}^4P)$	4656.82	38538	60006	11	11	0.11	0.006	6.0	-0.41	D	13
203.	$a^4H - x^4T$	4564.17	38538	60441	21	13	0.51	0.19	31	0.32	D	18
204.	$a^4H - ({}^4P)$	4413.00	38538	61192	11	13	0.097	0.033	5.3	-0.43	D	13
205.	$x^4H' - e^4H$	4432.77	42387	64940	15	15	0.49	0.14	32	0.34	D	13

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

\*The term designation for the level in question was not provided by Sugar and Cortius in their energy level compilation (J. Phys. Chem. Ref. Data 14, Suppl. 2 (1985)), so we have accordingly omitted it from this work.

## Cr II

## V Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 3p^3 3d^1 {}^4S_{3/2}$

Ionization Energy:  $16.4858 \text{ eV} = 132966 \text{ cm}^{-1}$

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
2653.57	3	2867.09	6	3126.68	5	4848.24	16
2658.59	1	2867.65	1	4054.10	8	4856.18	16
2666.02	4	2870.43	6	4087.60	8	4876.41	16
2668.71	4	2873.81	6	4113.24	7	4884.58	16
2671.80	4	2878.45	1	4530.51	19	5097.33	10
2672.83	3	2880.86	6	4555.01	21	5237.35	20
2740.09	2	2898.53	18	4558.66	21	5246.76	9
2744.97	12	2921.81	18	4565.77	19	5249.43	9
2787.61	12	2930.83	11	4567.30	27	5279.88	20
2822.38	14	2935.12	11	4568.22	21	5305.88	10
2835.63	1	2953.34	11	4569.80	21	5308.46	20
2840.01	14	2966.03	17	4592.07	21	5310.73	20
2843.24	1	2971.90	13	4616.64	21	5313.61	20
2849.83	1	2979.73	13	4618.82	21	5346.12	10
2851.35	14	2985.32	13	4634.10	21	5369.36	15
2856.77	6	2989.18	13	4697.61	25	5420.91	9
2857.40	6	3118.64	5	4715.12	25	5502.07	22
2860.92	1	3120.36	5	4812.34	16	5508.63	22
2862.57	1	3122.50	23	4824.12	16	6053.48	24
2866.72	1	3128.09	5	4836.22	16	6129.23	24

For this spectrum, we have chosen the experiments by Musielok and Wujec<sup>1</sup> and by Wujec and Weniger,<sup>2</sup> who measured relative oscillator strengths in emission with similar wall-stabilized arc sources. To obtain an absolute scale, Musielok and Wujec normalized their data to beam-foil lifetimes measured by Engman *et al.*<sup>3</sup> Wujec and Weniger, in turn, normalized their data directly to the  $f$ -value of the 4242.36 Å line tabulated in Ref. 1. In both experiments, a photographic detection system was employed, and a low-current carbon arc served as the absolute radiation standard.

Another data source which we utilized in this compilation is the work of Kostyk and Orlova.<sup>4</sup> These authors derived  $\log gf$ -values from solar spectra by using equivalent widths taken from the Liege solar atlas.<sup>5</sup> In the case of Fe I, Kostyk and co-workers<sup>6</sup> used a similar approach in deriving  $f$ -values, which are of approximately 50 percent accuracy. We feel that the data of Ref. 4 tabulated here are of similar accuracy.

For the evaluation of these data sources, we found very few cases of overlap, so that no significant direct comparisons were possible. Refs. 1 and 2 overlap only for the 4242.36 Å line, where the  $\log gf$ -value of Ref. 2 was made to agree with that of Ref. 1. Thus, to obtain some indication of systematic errors or scatter for these data sources, we compared the experimental data to the comprehensive semiempirical calculations of Kurucz and Peytremann.<sup>7</sup> We had found earlier that for many neutral and singly-ionized members of the iron-group elements,<sup>8</sup> the  $f$ -values of Ref. 5 compare reasonably well with more reliable data sources. While these calculated data show considerable scatter in comparison to experiment, the  $f$ -values of Ref. 5 appear to be generally devoid of gross systematic errors in the absolute scale. If the weaker lines and the intercombination lines are excluded, the majority of the data of Ref. 5 is generally accurate within a factor of two.

By comparing various experimental data to the calculations of Kurucz and Peytremann for Cr II, we found indications of systematic deviations and/or errors in absolute scale in the experimental results. For example, the data of Ref. 1 exhibit a pronounced wavelength dependence. The authors indeed suggest that there may be problems with their standard source in certain spectral regions. The  $f$ -values of Ref. 2 show a similar (though not as pronounced) dependence—the  $\log gf$ -values of near  $uv$  lines are too strong. On the basis of these com-

parisons, we have limited the tabulation of data from Ref. 1 to lines having wavelengths shorter than 3150 Å and upper energy levels less than 67000 cm<sup>-1</sup>.

Wujec and Weniger<sup>2</sup> normalized their data to the 4242.36 Å line of Ref. 1, which appears to be an inappropriate choice, since this wavelength falls in the region strongly affected by calibration problems with the carbon arc, due to molecular-band emission. Additional errors in the work of Wujec and Weniger may have occurred because of inconsistencies in the temperature measurement (discussed by us in the Cr I introduction). On the basis of a comparison with Ref. 5, we have shifted all  $\log gf$ -values of Ref. 2 downward by 0.84 dex and have omitted all lines having wavelengths less than 4500 Å.

A comparison of Refs. 4 and 5 reveals considerable scatter, as well as a shift in scale — the  $\log gf$ -values of Kostyk and Orlova are, on the average, about 50 percent higher than those of Kurucz and Peytremann. This comparison, however, deals only with the weak lines ( $\log gf < -1.00$ ), where the data of Ref. 5 are known to be less accurate. Therefore, we have tabulated the data of Kostyk and Orlova without renormalization.

Another reference which we originally considered for this spectrum is the paper by Goly and Weniger.<sup>7</sup> These authors measured  $f$ -values for over one hundred lines in the 2413-2718 Å region by using a wall-stabilized arc. Our graphical comparisons indicate that these data exhibit pronounced scatter, as well as a substantial deviation in absolute scale. Therefore, they have not been included in this compilation.

## References

- <sup>1</sup>J. Musielok and T. Wujec, *Astron. Astrophys., Suppl. Ser.* **30**, 119 (1979).
- <sup>2</sup>T. Wujec and S. Weniger, *J. Quant. Spectrosc. Radiat. Transfer* **25**, 167 (1981).
- <sup>3</sup>B. Engman, A. Gaupp, L. J. Curtis, and I. Martinson, *Phys. Scr.* **12**, 220 (1975).
- <sup>4</sup>R. I. Kostyk and T. V. Orlova, *Astrometriya Astrofiz.* **49**, 19 (1983).
- <sup>5</sup>R. L. Kurucz and E. Peytremann, *Smithsonian Astrophysical Observatory Special Report* 362 (1975).
- <sup>6</sup>S. M. Younger, J. R. Fuhr, G. A. Martin, and W. L. Wiese, *J. Phys. Chem. Ref. Data* **7**, 495 (1978).
- <sup>7</sup>A. Goly and S. Wenger, *J. Quant. Spectrosc. Radiat. Transfer* **24**, 335 (1980).
- <sup>8</sup>L. Delbouille, I. Neven, and C. Roland, "Photometric Atlas of the Solar Spectrum from 3000 to 10,000 Å," (Institut d'Astrophysique de l'Université de Liege, Observatoire Royal de Belgique, 1973).
- <sup>9</sup>E. A. Gurtovenko and R. I. Kostyk, *Astron. Astrophys., Suppl. Ser.* **47**, 193 (1982).

## Cr II: Allowed transitions

No.	Multiplet	$\lambda$ (Å)	$E_1$ ( $\text{cm}^{-1}$ )	$E_2$ ( $\text{cm}^{-1}$ )	$g_1$	$g_2$	$A_{21}$ ( $10^6 \text{ s}^{-1}$ )	$f_{12}$	$S$ (at. u.)	$\log gf$	Accuracy	Source
1.	$a^4D - z^4P$ (uv 5)	2835.63	12497	47752	10	12	2.9	0.29	27	0.46	C	3
		2843.24	12304	47465	8	10	0.64	0.097	7.3	-0.11	D	1
		2849.83	12148	47228	6	8	0.92	0.15	8.4	-0.05	D	1
		2860.92	11962	46806	2	4	0.69	0.17	3.2	-0.47	D	1
		2862.57	12304	47228	8	8	0.63	0.077	5.8	-0.21	D	1
		2865.72	12033	46806	4	4	1.2	0.15	5.6	-0.23	D	1
		2867.65	11962	46824	2	2	1.1	0.14	2.6	-0.57	D	1
		2878.45	12497	47228	10	8	0.974	0.0974	0.79	-1.13	D-	1
		2.	$a^4D - z^4P$ (uv 6)	2740.09	12148	46632	6	8	0.11	0.017	0.89	-1.80
3.	$a^4D - z^4P$ (uv 7)			2672.83	12304	49706	8	6	0.55	0.044	3.1	-0.45
		2653.57	12033	49706	4	6	0.35	0.055	1.9	-0.65	D	1
4.	$a^4D - z^4D$ (uv 8)	2671.80	12148	46565	6	4	1.0	0.071	3.8	-0.37	D	1
		2668.71	12033	46498	4	2	1.4	0.075	2.6	-0.52	D	1
		2666.02	12148	46546	6	8	0.59	0.084	4.4	-0.30	D	1
		2658.59	11962	46565	2	4	0.58	0.12	2.2	-0.61	D	1
5.	$a^4D - z^4P$ (5)	3120.36	19631	51670	4	6	1.5	0.33	13	0.12	D	1
		3118.64	19523	51584	2	4	1.7	0.50	10	-0.00	D	1
		3136.68	19798	51670	6	6	0.64	0.094	5.8	-0.25	D	1
		3123.69	19631	51584	4	4	0.81	0.12	4.9	-0.32	D	1
6.	$a^4D - z^4D$ (uv 11)	2870.43	19798	54626	6	6	1.3	0.16	9.1	-0.02	D	1
		2867.09	19631	54500	4	4	1.1	0.14	5.1	-0.27	D	1
		2880.86	19798	54500	6	4	0.79	0.066	3.7	-0.41	D	1
		2873.81	19631	54418	4	2	0.98	0.054	2.1	-0.66	D	1
		2867.40	19798	54785	6	8	0.28	0.046	2.6	-0.56	D	1
		2856.77	19631	54626	4	6	0.43	0.079	3.0	-0.50	D	1
7.	$b^4D - z^4P$ (18)	4113.24	25047	49706	6	6	0.0012	3.0(-4)	0.025	-2.74	D	4
8.	$b^4D - z^4D$ (19)	4064.10	25047	49352	6	6	0.0017	4.3(-4)	0.034	-2.59	D	4
		4087.60	25036	49493	2	2	0.0012	3.0(-4)	0.0081	-3.22	D	4

Cr II: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $gf$	Accu- racy	Source
9.	$b^1P - z^1P$ (23)	5420.91	30308	48750	4	2	0.0050	0.0011	0.78	-2.36	D	4
		5249.43	30308	49706	4	6	9.7(-4)	6.0(-4)	0.041	-2.62	D	4
		5246.76	29952	49006	2	4	0.0021	0.0018	0.061	-2.45	D	4
10.	$b^1P - z^1D$ (24)	5097.33	29952	49565	2	4	0.0015	0.0011	0.038	-2.64	D	4
		5305.86	20865	49352	6	6	0.0033	0.0014	0.15	-2.08	D	4
		5346.12	30865	49565	6	4	0.0013	3.7(-4)	0.039	-2.65	D	4
11.	$b^1P - y^1D$ (uv 55)	2225.12	30865	64924	6	8	1.8	0.31	18	0.27	D	1
		2933.83	29952	64062	2	4	1.1	0.28	5.5	-0.25	D	1
		2953.34	29952	63802	2	2	1.8	0.24	4.6	-0.33	D	1
12.	$b^1P - y^1P$ (uv 58)	2717.61	30865	66727	6	6	1.5	0.17	9.6	0.02	D	1
		2744.97	30308	66727	4	6	0.85	0.14	5.2	-0.24	D	1
13.	$a^1H - z^1H$ (uv 80)	2971.90	30392	64031	14	14	2.0	0.26	36	0.57	D	1
		2979.73	30299	63849	12	12	1.8	0.24	28	0.46	D	1
		2985.32	30219	63707	10	10	2.2	0.29	29	0.47	D	1
		2989.18	30157	63601	8	8	2.2	0.29	23	0.37	D	1
14.	$a^1H - z^1I$ (uv 82)	2822.38	30392	65813	14	16	2.3	0.31	41	0.64	C	3
		2840.01	30219	65420	10	12	2.7	0.39	37	0.59	D	1
		2851.35	30157	65218	8	10	2.2	0.34	25	0.43	D	1
15.	$a^1F - z^1D$ (29)	5369.36	31219	49838	10	10	3.2(-4)	1.4(-4)	0.024	-2.86	D	4
16.	$a^1F - z^1F$ (30)	4824.12	31219	51943	10	10	0.017	0.0060	0.96	-1.22	D	2 <sub>n</sub>
		4848.24	31169	51789	8	8	0.026	0.0091	1.2	-1.14	D	4
		4876.41	31169	51670	8	6	0.016	0.0043	0.56	-1.46	D	4
		4884.58	31118	51584	6	4	0.0058	0.0014	0.13	-2.08	D	4
		4812.34	31169	51943	8	10	0.0046	0.0020	0.25	-1.80	D	4
		4836.22	31118	51789	6	8	0.0020	9.4(-4)	0.090	-2.25	D	2 <sub>n</sub>
		4856.18	31083	51670	4	6	0.0026	0.0014	0.088	-2.26	D	4

## Cr II: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (a. u.)	log $g f$	Accuracy	Source
17.	a <sup>7</sup> F - y <sup>7</sup> D (uv 94)	2966.03	31219	64924	10	8	0.54	0.067	5.6	-0.24	D	1
		2898.53	31219	65170	10	12	1.2	0.18	17	0.25	D	1
18.	a <sup>7</sup> F - z <sup>6</sup> G (uv 95)	2921.81	31169	65364	8	10	0.90	0.14	11	0.06	D	1
		4539.61	32804	54626	6	6	0.0016	4.9(-4)	0.044	-2.53	D	2a
19.	a <sup>7</sup> F - z <sup>7</sup> D (39)	4565.77	32804	54500	6	4	0.0062	0.0013	0.12	-2.11	D	2a
		5237.35	32854	51943	10	10	0.017	0.0009	1.2	-1.16	D	4
20.	b <sup>7</sup> F - z <sup>7</sup> F (43)	5313.61	32855	51670	6	6	0.0008	0.0037	0.20	-1.65	D	4
		5279.88	32854	51780	10	8	0.0024	7.9(-4)	0.14	-2.10	D	4
		5305.46	32837	51670	8	6	0.0061	0.0019	0.27	-1.81	D	4
		5310.73	32845	51670	4	6	0.0021	0.0013	0.092	-2.28	D	4
		4558.06	32854	54785	10	8	0.068	0.022	3.3	-0.65	D	2a
		4588.22	32837	54626	8	6	0.12	0.029	3.5	-0.63	D	4
21.	b <sup>7</sup> F - z <sup>7</sup> D (45)	4618.82	32855	54500	6	4	0.061	0.013	1.2	-1.11	D	2a
		4634.10	32845	54418	4	2	0.080	0.014	0.88	-1.24	D	2a
		4555.01	32837	54785	8	8	0.017	0.0062	0.63	-1.36	D	4
		4582.07	32855	54626	6	6	0.032	0.010	0.91	-1.22	D	4
		4616.64	32845	54500	4	4	0.040	0.013	0.78	-1.29	D	4
		4589.89	32845	54626	4	6	0.0012	5.8(-4)	0.033	-2.05	D	2a
		5502.07	33619	51780	10	8	0.0028	0.0010	0.19	-1.90	D	4
		5508.63	33621	51670	8	6	0.0028	9.7(-4)	0.14	-2.11	D	4
22.	b <sup>6</sup> G - z <sup>7</sup> F (50)	3122.50	33694	66710	12	12	0.44	0.064	7.9	-0.11	D	1
23.	b <sup>6</sup> G - z <sup>6</sup> G (54)	0063.48	36270	54785	8	8	0.0016	8.8(-4)	0.14	-2.16	D	4
		6129.23	36315	54626	6	6	0.0011	6.1(-4)	0.073	-2.44	D	4
24.	c <sup>7</sup> D - z <sup>7</sup> D (106)	4715.12	45070	66872	4	2	0.0073	0.0012	0.076	-2.31	D	2a

## Cr II: Allowed transitions — Continued

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accuracy	Source
26.	$c^3D - y^3F$	4697.61	45731	67012	6	6	0.0066	0.0022	0.20	-1.88	D	2a
27.	$d^3G - x^3F$	4587.90	52321	74114	10	8	0.0089	0.0022	0.34	-1.65	D	2a

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr II

## Forbidden Transitions

For this spectrum, we selected the work of Nussbaumer and Swings,<sup>1</sup> who calculated numerous M1 and E2 transition probabilities. They derived their radial wavefunctions by using a central potential which was adjusted to give the optimum fit to observed energy levels. Their calculation included spin-orbit interaction but neglected the effects of configuration interaction. Because of the strong likelihood of configuration interaction, we have tabulated only the E2 transitions of the  $a^4S - a^4D$  multiplet. These lines have been observed in stellar spectra.

Another data source for lines in the  $a^4S - a^4D$  multiplet is that of Garstang.<sup>2</sup> His calculated  $A$ -values are approximately 15 percent less than those of Nussbaumer and Swings, because different radial wavefunctions were used. The data tabulated here are estimated to be accurate to within a factor of two.

## References

- <sup>1</sup>H. Nussbaumer and J. P. Swings, *Astrophys. J.* 162, 589 (1970).  
<sup>2</sup>R. H. Garstang, *J. Res. Nat. Bur. Stand., Sect. A* 68, 61 (1964).

## Cr II: Forbidden transitions

No.	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{21}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$a^4S - a^4D$ (1F)										
		[8000.1]	0	12496	6	16	E2	0.10	20	E	1
		[8125.3]	0	12304	6	8	E2	0.094	16	E	1
		[8229.7]	0	12148	6	6	E2	0.088	12	E	1
		[8308.5]	0	12033	6	4	E2	0.084	7.9	E	1
		[8357.6]	0	11962	6	2	E2	0.082	4.0	E	1



## Cr IV

## Sc Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 3p^4 3d^1 \ ^4F_{3/2}$ Ionization Energy: 49.16 eV = 396500  $\text{cm}^{-1}$ 

## Forbidden Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
1881.7	7	2965.1	16	5294.3	4	7297.9	17
1887.6	7	2973.3	16	5323.5	21	7330.5	2
1890.1	7	2980.9	16	5371.4	21	7360.8	2
1896.1	7	2988.2	16	5378.6	21	7410.9	19
1901.6	7	2991.5	6	5427.5	21	7518.2	19
1907.7	7	3076.7	18	6612.0	15	7664.7	19
1921.9	7	3078.1	18	6648.8	15	16142	9
2507.8	10	3092.6	18	6698.4	15	16180	9
2505.6	10	3094.0	18	6734.0	3	16625	11
2508.8	10	3133.0	20	6747.5	3	16891	11
2576.6	10	4837.6	5	6806.0	3	17649	21
2585.1	10	4841.0	5	6915.2	3	18307	8
2596.3	10	4893.9	5	7023.1	2	18684	8
2624.6	13	4897.3	5	7061.5	2	18900	8
2636.2	13	4971.5	5	7066.2	3	26127	8
2690.6	13	5125.9	12	7110.5	2	81537	14
2802.9	6	5142.8	4	7171.6	2	82513	14
2912.9	6	5177.0	12	7184.1	2	88456	14
2929.4	6	5206.3	4	7189.2	17	250900	1
2940.3	6	5219.3	12	7196.7	17	313400	1
2967.0	6	5272.3	12	7232.6	2		

For this spectrum, we have chosen the work of Pasternack,<sup>1</sup> who calculated M1 and E2 transition probabilities within the  $3d^1$  configuration by using the central-field approximation without consideration of configuration interaction. However, the  $3d^1$  configuration is well-separated from the next configuration— $3d^2 4s$ . For electric quadrupole transitions, we modified the data of Ref. 1 by applying correction factors suggested by Garstang.<sup>2</sup> These factors were introduced because of the availability of better wavefunctions. In the case of Fe VI, which is isoelectronic to Cr IV, we compared the  $A$ -values of Ref. 1 to those of Nussbaumer and Storey,<sup>3</sup> who could

utilize, in their much later work, modern theoretical and computational techniques. The agreement between Refs. 1 and 3 is surprisingly good—generally within 50 percent—even for the E2 transitions (after undergoing Garstang's correction). Weak lines are subject to greater uncertainties, so we have omitted lines having  $A$ -values less than  $0.001 \text{ s}^{-1}$ .

## References

- <sup>1</sup>S. Pasternack, *Astrophys. J.* **92**, 129 (1940).
- <sup>2</sup>R. H. Garstang, *J. Res. Nat. Bur. Stand., Sect. A* **68**, 61 (1964).
- <sup>3</sup>H. Nussbaumer and P. J. Storey, *Astron. Astrophys.* **70**, 37 (1978).

## Cr IV: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	S (st. u.)	Accuracy	Source
1.	3d <sup>3</sup> -3d <sup>1</sup>	F - F	[256900]	556.4	945.5	8	10	M1	0.0017	11	C	1
			[313400]	237.4	556.4	6	8	M1	0.0014	13	C	1
2.	F - P (1F)	[7390.8]	945.5	14472	10	6	E2	0.035	2.8	E	1a	
		[7339.5]	556.4	14178	8	4	E2	0.026	1.3	E	1a	
		[7232.6]	237.4	14060	6	2	E2	0.022	0.52	E	1a	
		[7184.1]	556.4	14472	8	6	E2	0.013	0.89	E	1a	
		[7171.6]	237.4	14178	6	4	E2	0.020	0.90	E	1a	
		[7110.5]	0.0	14060	4	2	E2	0.035	0.76	E	1a	
		[7023.1]	237.4	14472	6	6	E2	0.032	0.20	E	1a	
		[7051.5]	0.0	14178	4	4	E2	0.0073	0.30	E	1a	
3.	F - G (2F)	[6915.2]	945.5	15402	10	10	M1	0.093	0.011	E	1	
		[6896.0]	556.4	15054	8	8	M1	0.035	0.0034	E	1	
		[7086.2]	945.5	15054	10	8	M1	0.0023	2.4 - 4	E	1	
		[6734.0]	556.4	15402	8	10	M1	0.036	0.0041	E	1	
		[6747.5]	237.4	15054	6	8	M1	0.032	0.0029	E	1	
4.	F - P (3F)	[5294.3]	556.4	19439	8	4	E2	0.0011	0.011	E	1a	
		[5206.3]	237.4	19439	6	4	M1	0.055	0.0012	E	1	
		[5142.8]	0.0	19439	4	4	M1	0.034	6.9 - 4	E	1	
5.	F - D2 (4F)	[4971.5]	556.4	20666	8	6	M1	0.16	0.0044	E	1	
		[4897.3]	237.4	20651	6	4	M1	0.13	0.0023	E	1	
		[4893.9]	237.4	20666	6	6	M1	0.020	5.2 - 4	E	1	
		[4841.0]	0.0	20651	4	4	M1	0.071	0.0012	E	1	
		[4837.6]	0.0	20666	4	6	M1	0.0073	1.8 - 4	E	1	
6.	F - F	[2991.5]	945.5	34364	10	8	M1	0.024	2.7 - 4	D	1	
		"	"	"	10	8	E2	0.0011	0.0013	E	1a	
		[2940.3]	556.4	34557	8	6	M1	0.0060	3.4 - 5	D	1	
		[2957.0]	556.4	34364	8	8	M1	0.0034	2.6 - 5	D	1	
		[2912.9]	237.4	34557	6	6	M1	0.0046	2.5 - 5	D	1	
		[2929.4]	237.4	34364	6	8	M1	0.013	9.7 - 5	D	1	
		[2892.9]	0.0	34557	4	6	M1	0.031	1.7 - 4	D	1	
		"	"	"	4	6	E2	0.0011	8.0 - 4	E	1a	
7.	F - D1	[1921.9]	945.5	52976	10	6	E2	0.017	0.0016	E	1a	
		[1901.6]	556.4	53144	8	4	E2	0.0039	2.3 - 4	E	1a	
		[1907.7]	556.4	52976	8	6	M1	0.043	6.6 - 5	E	1	
		"	"	"	8	6	E2	0.0011	9.9 - 5	E	1a	
		[1890.1]	237.4	53144	6	4	M1	0.048	4.8 - 5	E	1	
		[1896.1]	237.4	52976	6	6	M1	0.0046	7.0 - 6	E	1	
		[1881.7]	0.0	53144	4	4	M1	0.025	2.5 - 5	E	1	
		"	"	"	4	4	E2	0.0013	7.3 - 5	E	1a	
		[1887.6]	0.0	52976	4	6	M1	0.0016	2.4 - 6	E	1	

Cr IV: Forbidden transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{if}$ (s <sup>-1</sup> )	S (rat. u.)	Accuracy	Source
8.		$^3P - ^3P$	[20127]	14472	19439	6	4	M1	0.020	0.024	D	1
			[18999]	14178	19439	4	4	M1	0.028	0.028	D	1
			[18307]	14060	19521	2	2	M1	0.052	0.024	D	1
			[18584]	14060	19439	2	4	M1	0.013	0.012	D	1
9.	$^3P - ^3D_2$	[16142]	14472	20666	6	6	M1	0.0077	0.0072	E	1	
		[16180]	14472	20651	6	4	M1	0.018	0.011	E	1	
10.	$^3P - ^3D_1$	[2596.3]	14472	52976	6	6	M1	0.23	9.5(-4)	E	1	
		[2565.6]	14178	53144	4	4	M1	0.069	2.2(-4)	E	1	
		-	-	-	4	4	E2	0.024	0.0064	E	1a	
		[2585.1]	14472	53144	6	4	M1	0.022	5.6(-5)	E	1	
		[2576.6]	14178	52976	4	6	M1	0.041	1.6(-4)	E	1	
		-	-	-	4	6	E2	0.026	0.011	E	1a	
		[2557.8]	14060	53144	2	4	M1	0.023	5.7(-5)	E	1	
		[2568.8]	14060	52976	2	4	E2	0.0092	0.0024	E	1a	
11.	$^4G - ^3H$	[16891]	15402	21321	10	12	M1	0.016	0.034	E	1	
		[16625]	15654	21067	8	10	M1	0.016	0.027	E	1	
		[17649]	15402	21067	10	10	M1	0.030	0.061	E	1	
12.	$^4G - ^3F$	[5219.3]	15402	34557	10	6	E2	0.0012	0.017	E	1a	
		[5272.3]	15402	34364	10	8	M1	0.019	8.7(-5)	E	1	
		-	-	-	10	8	E2	0.088	1.7	E	1a	
		[5125.9]	15054	34557	8	6	M1	0.022	6.6(-4)	E	1	
		-	-	-	8	6	E2	0.098	1.2	E	1a	
		[5177.0]	15054	34364	8	8	M1	0.041	0.0017	E	1	
13.	$^4G - ^3D_1$	[2660.6]	15402	52976	10	6	E2	8.2	3.9	E	1a	
		[2624.6]	15054	53144	8	4	F2	9.4	2.8	E	1a	
		[2636.2]	15054	52976	8	6	E2	0.71	0.32	E	1a	
14.	$^3P - ^3D_2$	[81587]	19439	20656	4	6	M1	0.0062	0.75	E	1	
		[88456]	19521	20651	2	4	M1	0.0041	0.42	E	1	
		[82513]	19439	20651	4	4	M1	0.011	0.92	E	1	
15.	$^3P - ^3F$	[6698.4]	19439	34364	4	8	E2	0.016	1.0	E	1a	
		[6648.8]	19521	34557	2	6	E2	0.0096	0.44	E	1a	
		[6613.0]	19439	34557	4	6	E2	0.0040	0.18	E	1a	

## Cr IV: Forbidden transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$L_1$	$L_2$	Type of transition	$A_{21}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
16.		P - D1	[2988.2]	19521	52976	2	6	E2	0.52	0.44	E	1 <sub>n</sub>
			[2988.9]	19439	52976	4	6	M1	0.000	2.4(-4)	E	1
			-	-	-	4	6	E2	0.79	0.66	E	1 <sub>n</sub>
			[2972.3]	19521	53144	2	4	E2	1.2	0.66	E	1 <sub>n</sub>
			[2968.1]	19439	53144	4	4	E2	1.9	1.0	E	1 <sub>n</sub>
17.		D2 - F	[7297.9]	20666	34364	6	8	M1	0.0015	1.7(-4)	E	1
			-	-	-	6	8	E2	0.027	2.7	E	1 <sub>n</sub>
			[7189.2]	20651	34557	4	6	M1	0.0010	8.3(-5)	E	1
			-	-	-	4	6	E2	0.023	1.6	E	1 <sub>n</sub>
			[7196.7]	20666	34557	6	6	M1	0.0039	3.2(-4)	E	1
			-	-	-	6	6	E2	0.0065	0.45	E	1 <sub>n</sub>
18.		D2 - D1	[3094.0]	20666	52976	6	6	E2	0.69	0.70	E	1 <sub>n</sub>
			[3075.7]	20651	53144	4	4	E2	0.0060	0.0039	E	1 <sub>n</sub>
			[3078.1]	20666	53144	6	4	M1	0.14	6.1(-4)	D	1
			-	-	-	6	4	E2	0.29	0.19	E	1 <sub>n</sub>
			[3092.6]	20651	52976	4	6	M1	0.063	4.1(-4)	D	1
			-	-	-	4	6	E2	1.1	1.1	E	1 <sub>n</sub>
19.		H - F	[7664.7]	21321	34364	12	8	E2	0.039	4.9	E	1 <sub>n</sub>
			[7410.9]	21067	34557	10	6	E2	0.046	3.7	E	1 <sub>n</sub>
			[7518.2]	21067	34364	10	8	E2	0.0012	0.14	E	1 <sub>n</sub>
20.		H - D1	[3133.0]	21067	52976	10	6	E2	0.040	0.043	E	1 <sub>n</sub>
21.		F - D1	[5323.5]	34364	53144	8	4	E2	0.075	0.76	E	1 <sub>n</sub>
			[5371.4]	34364	52976	8	6	M1	0.057	0.0020	E	1
			-	-	-	8	6	E2	0.40	6.4	E	1 <sub>n</sub>
			[5378.6]	34557	53144	6	4	M1	0.060	0.0014	E	1
			-	-	-	6	4	E2	0.40	4.3	E	1 <sub>n</sub>
			[5427.5]	34557	52976	6	6	M1	0.10	0.0036	E	1
-	-	-	6	6	E2	0.069	1.2	E	1 <sub>n</sub>			

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr v

## Ca Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 3p^4 3d^1 \ ^3F_4$ Ionization Energy:  $69.46 \text{ eV} = 560200 \text{ cm}^{-1}$ 

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
434.306	2	456.743	7	1127.63	16	1697.94	10
435.143	2	457.928	7	1134.77	16	1611.33	10
435.636	2	457.504	7	1465.86	14	1622.61	9
436.351	2	464.915	8	1481.65	11	1638.59	9
436.691	2	469.311	6	1482.76	11	1639.40	9
437.420	1	469.634	3	1484.67	11	1644.95	9
437.655	1	469.893	6	1489.71	11	1652.60	9
441.856	5	479.567	6	1497.97	11	1655.64	9
445.751	4	1103.39	15	1519.63	13	1837.44	12
456.272	7	1106.25	15	1579.70	10		
456.357	7	1121.97	16	1591.72	10		
456.637	7	1126.09	16	1603.19	10		

For this spectrum, Kurucz and Peytremann<sup>1</sup> have calculated oscillator strengths for over one hundred transitions using a scaled Thomas-Fermi-Dirac approach with limited configuration interaction. Of these lines, we have chosen only the stronger lines, i.e., with  $\log gf > -1.5$ , and have omitted all intercombination (spin-forbidden) lines. An additional criterion for selecting the data was that all lines had to be experimentally observed, i.e., they appear in the line list of Ekberg.<sup>2</sup>

We estimate that for the stronger lines of this relatively simple spectrum, Kurucz and Peytremann's data

should be fairly reliable. There is indirect support for this estimate from the good consistency between similarly calculated values and lifetime measurements for the isoelectronic ion  $\text{Tl VII}$ .

## References

- <sup>1</sup>R. L. Kurucz and E. Peytremann, *Smithsonian Astrophysical Observatory Special Report 362* (1975).  
<sup>2</sup>J. O. Ekberg, *Phys. Scr.* 7, 59 (1973).

## Cr v: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (st. u.)	$\log gf$	Accuracy	Source
1.	$3d^2-3d4p$	$^3P - ^3D'$	437.420	508.2	229121	7	7	14	0.039	0.40	-0.56	D	1
			437.655	0.0	228489	5	5	13	0.038	0.27	-0.72	D	1
2.	$^3P - ^3P'$		434.306	1141.7	231393	9	9	15	0.042	0.54	-0.42	D	1
			435.143	508.2	230316	7	7	2.9	0.0082	0.082	-1.24	D	1
			435.636	0.0	229562	5	5	2.8	0.0080	0.057	-1.40	D	1
			436.351	1141.7	230316	9	7	24	0.053	0.69	-0.32	D	1
			436.691	508.2	229562	7	5	21	0.043	0.43	-0.52	D	1
3.	$^1D - ^1D'$		469.634	13188	226120	5	5	23	0.076	0.59	-0.42	D	1

Cr V: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $g^2$	Accuracy	Source
4.		'D - 'P	445.751	13188	237530	5	7	1.9	0.0078	0.957	-1.41	D	1
5.		'D - 'P	441.056	13188	239918	5	3	23	0.040	0.29	-0.70	D	1
6.		'P - 'D											
			469.311	16041	229121	5	7	3.9	0.018	0.14	-1.04	D	1
			469.893	15677	228489	3	5	4.9	0.027	0.13	-1.09	D	1
			470.567	15492	228002	1	3	4.9	0.049	0.076	-1.31	D	1
7.		'P - 'P	456.85	15859	234750	9	9	33	0.10	1.4	-0.03	D	1
			457.028	16041	234846	5	5	27	0.083	0.63	-0.38	D	1
			456.743	15677	234618	3	3	9.1	0.028	0.13	-1.07	D	1
			457.504	16041	234618	5	3	12	0.023	0.18	-0.93	D	1
			456.637	15677	234689	3	1	33	0.035	0.16	-0.98	D	1
			456.272	15677	234846	3	5	6.7	0.035	0.16	-0.98	D	1
			456.357	15492	234618	1	3	9.5	0.089	0.13	-1.05	D	1
8.		'G - 'F	464.015	22919	237530	9	7	36	0.090	1.2	0.09	D	1
9.	3d4s-3d4p	'D - 'D											
			1638.50	168090	229121	7	7	6.8	0.27	10	0.28	D	1
			1639.40	167491	228489	5	5	4.9	0.20	5.3	-0.01	D	1
			1644.05	167176	228002	3	3	5.0	0.20	3.3	-0.22	D	1
			1655.64	168090	228489	7	5	1.6	0.048	1.8	-0.47	D	1
			1652.60	167491	228002	5	3	2.5	0.062	1.7	-0.51	D	1
			1622.61	167491	229121	5	7	0.74	0.041	1.1	-0.69	D	1
10.		'D - 'F											
			1579.70	168090	231393	7	9	8.6	0.41	15	0.46	D	1
			1591.72	167491	230316	5	7	7.3	0.29	10	0.29	D	1
			1603.19	167176	229552	3	5	7.0	0.45	7.1	0.13	D	1
			1607.04	168090	230316	7	7	0.83	0.032	1.2	-0.65	D	1
			1611.33	167491	229552	5	5	0.23	0.0089	0.24	-1.35	D	1
11.		'D - 'P											
			1497.97	168090	234846	7	5	7.5	0.18	6.2	0.10	D	1
			1489.71	167491	234618	5	3	6.6	0.13	3.2	-0.18	D	1
			1481.65	167176	234689	3	1	10	0.11	1.7	-0.47	D	1
			1484.67	167491	234846	5	5	2.2	0.073	1.8	-0.44	D	1
			1482.76	167176	234618	3	3	3.5	0.12	1.7	-0.46	D	1
12.		'D - 'D	1837.44	171698	226120	5	5	4.3	0.22	6.6	0.04	D	1
13.		'D - 'F	1519.03	171698	237530	5	7	9.5	0.46	11	0.26	D	1
14.		'D - 'P	1465.86	171698	239918	5	3	11	0.21	5.1	0.02	D	1
15.	3d4p-3d4d	'D - 'G											
			1106.25	229121	319517	7	9	12	0.29	7.4	0.31	D	1
			1103.39	228489	319119	5	7	2.4	0.062	1.1	-0.51	D	1
16.		'P - 'G											
			1127.63	231393	320074	9	11	35	0.80	27	0.86	D	1
			1121.07	220316	319517	7	9	21	0.51	13	0.55	D	1
			1124.77	231393	319517	9	9	2.0	0.038	1.3	-0.47	D	1
			1126.09	220316	319119	7	7	6.1	0.12	3.0	-0.09	D	1

## Cr V

## Forbidden Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
582.42	12	642.44	16	829.52	29	6709.9	3
584.15	12	645.57	13	859.52	19	7500.6	2
586.32	12	648.68	13	1955.2	5	7884.4	2
594.92	11	649.49	13	2633.7	8	8299.0	2
596.73	11	656.11	15	2818.5	10	11320	7
597.95	11	657.68	15	2847.7	10	35041	6
598.17	11	657.90	15	4540.2	4	40172	6
598.96	11	658.70	15	4647.5	4	157000	1
598.99	11	660.07	15	4788.5	4	196700	1
599.99	11	660.28	15	6232.3	3	274300	9
601.14	11	661.66	15	6377.2	3	541000	9
630.87	14	688.10	18	6436.2	3		
640.18	16	684.60	17	6453.2	3		
640.94	16	687.42	17	6590.8	3		

For this ion, we selected the work of Warner and Kirkpatrick,<sup>1</sup> who used a single-configuration approximation and calculated radial integrals with scaled Thomas-Fermi wavefunctions. We have tabulated M1 and E2 transition probabilities for 23 lines within the  $3d^2$  (ground) configuration and E2 data for 30 lines in the  $3d^2-3d4s$  transition array. For long-wavelength lines within the  $3d^2\ ^1F$  and  $3d^2\ ^1P$  terms, we have recalculated

Warner and Kirkpatrick's  $A$ -values by using observed energy-level data instead of theoretically derived values.

## Reference

<sup>1</sup>B. Warner and R. C. Kirkpatrick, Mon. Not. R. Astron. Soc. 104, 397 (1969).

## Cr V: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$3d^2-3d^1$	$^3P - ^3P$	[157800]	508.2	1141.7	7	9	M1	0.0051	6.7	C	1a
			[196700]	0.0	508.2	5	7	M1	0.0037	7.3	C	1a
2.	$^3P - ^1D$ ( $1P$ )	[8299.0]	1141.7	13188	9	5	E2	2.0(-4) <sup>†</sup>	0.040	E	1	
		[7884.4]	508.2	13188	7	5	M1	0.10	0.0001	E	1	
		"	"	"	7	5	E2	8.2(-5)	0.0074	E	1	
		[7500.6]	0.0	13188	5	5	M1	0.067	0.0046	E	1	
		"	"	"	5	5	E2	5.7(-5)	0.0042	E	1	
3.	$^3P - ^3P$ ( $2P$ )	[6709.9]	1141.7	16041	9	5	E2	0.031	1.3	E	1	
		[6600.8]	508.2	15677	7	3	E2	0.031	0.69	E	1	
		[6463.2]	0.0	15402	5	1	E2	0.061	0.24	E	1	
		[6426.2]	508.2	16041	7	5	M1	0.0094	1.7(-4)	E	1	
		"	"	"	7	5	E2	0.010	0.23	E	1	
		[6377.2]	0.0	15677	5	3	M1	1.0(-4)	2.9(-6)	E	1	
		"	"	"	5	3	E2	0.018	0.24	E	1	
		[6232.3]	0.0	16041	5	5	M1	8.7(-4)	3.9(-5)	E	1	
"	"	"	5	5	E2	0.0016	0.045	E	1			

## Cr v: Forbidden transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{if}$ (s <sup>-1</sup> )	S (rel. u.)	Accuracy	Source
4.		P - <sup>1</sup> G (3F)	[4788.5]	1141.7	22919	9	9	M1	0.072	0.0025	E	1
			-	-	-	9	9	E2	4.2(-5)	5.7(-4)	E	1
			[4647.5]	508.2	22919	7	9	M1	0.047	0.0016	E	1
			[4548.2]	0.0	22919	5	9	E2	8.9(-5)	9.2(-4)	E	1
5.		P - <sup>1</sup> S	[1955.2]	0.0	51146	5	1	E2	0.025	4.3(-4)	E	1
6.		D - <sup>3</sup> P	[35041]	13188	16041	5	5	M1	0.024	0.19	E	1
			[40172]	13188	15677	5	3	M1	0.0032	0.066	E	1
7.		D - <sup>1</sup> G	[11320]	13188	22919	5	9	E2	6.3(-4)	0.61	E	1
8.		D - <sup>1</sup> S (4F)	[2633.7]	13188	51146	5	1	E2	9.8	0.74	E	1
9.		P - <sup>3</sup> P	[274300]	15677	16041	3	5	M1	5.2(-4)	2.0	C	1a
			[541000]	15692	15677	1	3	M1	1.27(-4)	2.24	C	1a
10.		P - <sup>1</sup> S (5F)	[2847.7]	16041	51146	5	1	E2	0.21	0.023	E	1
			[2818.5]	15677	51146	3	1	M1	1.1	9.3(-4)	E	1
11.	3d <sup>2</sup> -3d4s	P - <sup>3</sup> D	[601.14]	1141.7	167491	9	5	E2	2700	0.63	E	1
			[599.99]	508.2	167176	7	3	E2	4300	0.60	E	1
			[598.99]	1141.7	168090	9	7	E2	1.0(+4)	3.2	E	1
			[598.86]	508.2	167491	7	5	E2	6500	1.5	E	1
			[598.17]	0.0	167176	5	3	E2	8900	1.2	E	1
			[596.73]	508.2	168090	7	7	E2	2900	0.91	E	1
			[597.06]	0.0	167491	5	5	E2	3900	0.86	E	1
			[594.92]	0.0	168090	5	7	E2	270	0.064	E	1
			12.		P - <sup>1</sup> D	[586.22]	1141.7	171698	9	5	E2	16
[584.15]	508.2	171698				7	5	E2	88	0.018	E	1
[582.42]	0.0	171698				5	5	E2	11	0.0022	E	1
13.		D - <sup>3</sup> D	[645.57]	13188	168090	5	7	E2	77	0.036	E	1
			[648.08]	13188	167491	5	5	E2	200	0.068	E	1
			[649.40]	13188	167176	5	3	E2	61	0.013	E	1
14.		D - <sup>1</sup> D	[620.87]	13188	171698	5	5	E2	6900	2.0	E	1



## Cr v: Forbidden transitions - Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	S (at. u.)	Accuracy	Source
15.		P - D	[656.11]	15677	168990	3	7	E2	1200	0.61	E	1
			[657.90]	15492	167491	1	5	E2	1200	0.44	E	1
			[657.68]	16941	168990	5	7	E2	2300	1.2	E	1
			[658.70]	15677	167491	3	5	E2	290	0.11	E	1
			[660.28]	16941	167491	5	5	E2	1800	0.67	E	1
			[660.07]	15677	167176	3	3	E2	2300	0.58	E	1
			[661.66]	16941	167176	5	3	E2	610	0.18	E	1
16.		P - D	[642.44]	16941	171698	5	5	E2	340	0.11	E	1
			[640.94]	15677	171698	3	5	E2	40	0.0013	E	1
			[640.18]	15492	171698	1	5	E2	10	0.0002	E	1
17.		G - D	[687.42]	22919	167491	9	5	E2	80	0.041	E	1
			[684.60]	22919	168990	9	7	E2	1.2	7.5(-4)	E	1
18.		G - D	[668.10]	22919	171698	9	5	E2	9000	3.8	E	1
19.		S - D	[660.52]	51166	167491	1	5	E2	24	0.0004	E	1
			[629.52]	51166	171698	1	5	E2	390	0.44	E	1

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr vi

## K isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 3p^4 3d^3 D_{3/2}$

Ionization Energy: 90.6356 eV = 731020 cm<sup>-1</sup>

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
161.687	8	172.487	6	202.442	5	269.776	2
161.920	8	172.841	6	202.739	5	279.154	1
162.565	9	201.007	4	226.241	3	280.143	1
168.068	7	201.224	4	227.202	3	280.879	1
168.255	7	201.388	4	227.899	3		
169.435	7	201.606	4	264.078	2		
172.204	6	202.057	5	264.732	2		

For this spectrum, we have chosen the data of Tiwary,<sup>1,2</sup> who calculated absolute multiplet oscillator strengths for the  $3p^3d-3p^3d^2$  and  $3p^3d-3p^3d4s$  arrays by using configuration interaction wavefunctions. For the  $3p^3d-3p^3d4s$  array,  $LS$ -coupling line strengths generally agree quite well with the intermediate coupling calculations of Cowan.<sup>3</sup> For the few cases where the agreement is not good (worse than  $\pm 50\%$ ), we have omitted the lines from this compilation. Within this transition array, we have normalized Cowan's line strengths to the multiplet strengths of Ref. 2.

For lines within the  $3p^3d-3p^3d^2$  transition array, we have obtained line strengths from Tiwary's multiplet strengths by applying  $LS$ -coupling rules. We estimate these data to be accurate within fifty percent for stronger lines.

References

<sup>1</sup>S. N. Tiwary, Chem. Phys. Lett. 93, 47 (1982).  
<sup>2</sup>S. N. Tiwary, Astrophys. J. 269, 803 (1983).  
<sup>3</sup>R. D. Cowan, Astrophys. J. 147, 377 (1967).

Cr VI: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (inf. u.)	log $gf$	Accuracy	Source
1.	$3p^3d-3p^3P^o3d^4G$	'D - 'P'	279.60	564	358221	10	14	5.1	0.010	0.092	-1.00	D-	1
			279.154	940	359165	6	8	6.2	0.0096	0.053	-1.24	D-	ls
			280.143	0	356962	4	6	5.7	0.010	0.037	-1.40	D-	ls
			280.879	940	356962	6	6	0.40	4.7(-4) <sup>o</sup>	0.0026	-2.55	E	ls
2.	$3p^3d-3p^3P^o3d^4D$	'D - 'P'	267.32	564	374643	10	14	27	0.041	0.36	-0.39	D-	1
			269.776	940	371618	6	8	27	0.039	0.21	-0.63	D-	ls
			264.078	0	378677	4	6	26	0.040	0.14	-0.79	D-	ls
			264.732	940	378677	6	6	1.8	0.0019	0.010	-1.94	E	ls
3.	$3p^3d-3p^3P^o3d^4F$	'D - 'P'	226.67	564	441741	10	14	710	0.77	5.7	0.89	D-	1
			226.241	940	442945	6	8	720	0.74	3.3	0.65	D-	ls
			227.202	0	440135	4	6	660	0.77	2.3	0.49	D-	ls
			227.689	940	440135	6	6	46	0.036	0.16	-0.67	E	ls
4.	'D - 'D'	'D - 'D'	201.37	564	497173	10	10	2600	1.6	11	1.20	D-	1
			201.606	940	496958	6	6	2600	1.6	6.2	0.97	D-	ls
			201.007	0	497495	4	4	2500	1.5	4.0	0.78	D-	ls
			201.388	940	497495	6	4	270	0.11	0.44	-0.18	E	ls
			201.224	0	496958	4	6	180	0.17	0.44	-0.18	E	ls
5.	$3p^3d-3p^3P^o3d^4P$	'D - 'P'	202.51	564	494356	10	6	1200	0.44	2.9	0.64	D-	1
			202.442	940	494911	6	4	1000	0.43	1.7	0.41	D-	ls
			202.739	0	493247	4	2	1200	0.36	0.97	0.16	D-	ls
			202.057	0	494911	4	4	120	0.071	0.19	-0.54	E	ls
6.	$3p^3d-3p^3d^1P^o4s$	'D - 'P'	172.59	564	579987	10	6	120	0.032	0.18	-0.49	D	2
			172.487	940	580697	6	4	110	0.032	0.11	-0.71	D	3n
			172.441	0	578566	4	2	120	0.026	0.060	-0.98	D	3n
			172.204	0	580697	4	4	16	0.0071	0.016	-1.55	E	3n

Cr VI: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (st. u.)	log $gf$	Accuracy	Source
7.	$3p^4 3d - 3p^4 3d(^3P^o)4s$	$^3D - ^3P^o$	168.86	564	592751	10	14	180	0.11	0.61	0.04	D	2
			168.435	940	591137	6	8	160	0.093	0.31	-0.26	D	3a
			168.088	0	594926	4	6	200	0.13	0.28	-0.30	D	3a
			168.355	940	594926	6	6	11	0.0045	0.015	-1.57	E	3a
8.	$3p^4 3d - 3p^4 3d(^3D^o)4s$	$^3D - ^3D^o$	161.73	564	618062	10	10	190	0.073	0.39	-0.14	D	2
			161.687	940	618491	6	6	170	0.066	0.21	-0.40	D	3a
			161.687	0	619419	4	4	140	0.056	0.12	-0.65	D	3a
			161.930	940	619419	6	4	30	0.0078	0.025	-1.33	E	3a
9.	$3p^4 3d - 3p^4 3d(^1P^o)4s$	$^3D - ^3P^o$	162.68	564	615353	10	14	79	0.044	0.24	-0.36	D	2
			162.565	940	616079	6	8	83	0.044	0.14	-0.58	D	3a

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr VII

## Ar Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 3p^4 \ ^1S_0$

Ionization Energy: 160.18 eV  $\approx$  1291900 cm<sup>-1</sup>

## Allowed Transitions

Line strengths for the  $3p^4-3p^3 3d$  resonance transitions of this argon-like ion were interpolated from the superposition-of-configurations (SOC) calculations of Weiss,<sup>1</sup> which are expected to be fairly accurate.

Oscillator strengths for transitions of the  $3p^4-3p^3 4s$  array were interpolated from the Dirac-Hartree-Fock data of Lin *et al.*,<sup>2</sup> who included correlation only in the lower state. Their results for lines of the  $3p^4-3p^3 4d$  array in nearby Ar-like species have not been interpolated to provide  $f$ -values for Cr VII, since cancellation effects at

or near V VI—one of the ions treated—introduce considerable uncertainty into the results at the low- $Z$  end of the Ar sequence.

## References

- <sup>1</sup>A. W. Weiss, private communication.  
<sup>2</sup>D. L. Lin, W. Fickler, Jr., and L. Armstrong, Jr., Phys. Rev. A 16, 589 (1977).

## Cr VII: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $gf$	Accuracy	Source
1.	$3p^4-3p^33d$	$^1S-^3D^o$	259.181	0	385828	1	3	0.93	0.0028	0.0024	-2.55	E	interp.
2.		$^1S-^1P^o$	202.828	0	493035	1	3	1670	3.06	2.06	0.489	C	interp.
3.	$3p^4-3p^3(^4P_{1,2})4s$	$^1S-(^1/2,^1/2)^o$	148.714	0	672428	1	3	130	0.13	0.064	-0.89	D	interp.
4.	$3p^4-3p^3(^4P_{1,2})4s$	$^1S-(^1/2,^1/2)^o$	146.497	0	682610	1	3	300	0.29	0.14	-0.54	D	interp.

## Cr VIII

## CI Isoelectronic Sequence

Ground State:  $1s^22s^22p^43s^23p^1\ ^1P^o_{1/2}$ Ionization Energy: 184.7 eV = 1490000 cm<sup>-1</sup>

## Allowed Transitions

Line strengths for transitions of the arrays  $3s^23p^5-3s3p^6$  and  $3p^5-3p^43d$  are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang *et al.*<sup>1</sup> These relativistic calculations include a perturbative treatment of the Breit interaction and the Lamb shift. Configuration mixing was limited to some configurations within the  $n=3$  complex. Those configurations which were assumed to lie far above  $3p^1$  or  $3p^43d$  in energy were excluded, as were all configurations outside the complex.

According to the semi-empirical HX (Hartree-Fock with statistical allowance for exchange) calculations of Bromage *et al.*<sup>2</sup> for Fe x, some levels of the  $3p^43d$  configuration are strongly mixed in the *LS* basis, and in a few cases the *LS* designations given in Ref. 2 differed from those of Huang *et al.* The level designations used in this compilation are in accord with the theoretical results of Refs. 1 and 2 for Fe x. Percentage compositions published by Bromage<sup>1</sup> for the levels of the  $3p^43d$  configuration in V VII and Ni XII indicate that the designations for

the iron ion are appropriate for the neighboring ions of the chlorine isoelectronic sequence. Transitions involving highly mixed levels have been excluded, as have the very weak transitions.

The calculated wavelengths of Huang *et al.* differ appreciably from the observed ones found in the literature. Thus the available experimentally determined wavelengths were used in making the conversion from line strengths to *f*- and *A*-values. (Otherwise, the calculated wavelengths of Huang *et al.* were used, but they provide only a rough idea of the spectral-line positions.) Bromage *et al.* indicate that it was necessary to scale down some configuration-interaction parameters by a greater

amount than usual in order to fit their calculated energy levels for Fe x to the experimental data. This could be an indication that neglecting to take configuration interaction into account on a larger scale yields significant errors in the energy levels and/or *f*-values.

### References

- <sup>1</sup>K.-N. Huang, Y.-K. Kim, K. T. Cheng, and J. P. Desclaux, *At. Data Nucl. Data Tables* 28, 355 (1983).  
<sup>2</sup>G. E. Bromage, R. D. Cowan, and B. C. Fawcett, *Phys. Scr.* 15, 177 (1977).  
<sup>3</sup>G. E. Bromage, *Astron. Astrophys. Suppl. Ser.* 41, 79 (1980).

Cr VIII: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{if}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{if}$	$S$ (at. u.)	log <i>gf</i>	Accuracy	Source
1.	3s <sup>2</sup> 3p <sup>1</sup> -3s3p <sup>4</sup>	<sup>2</sup> P° - <sup>2</sup> S	418.82	3297	242065	6	2	40.3	0.0353	0.292	-0.67	C-	1
			413.112	0	242065	4	2	27.9	0.0357	0.194	-0.85	C-	1
			430.713	9892	242065	2	2	12	0.035	0.096	-1.16	C-	1
2.	3p <sup>5</sup> -3p <sup>4</sup> <sup>2</sup> P3d	<sup>2</sup> P° - <sup>2</sup> F	[265]			4	6	0.063	1.3(-4) <sup>a</sup>	4.6(-4)	-3.28	E	1
			[271]			2	4	0.11	2.4(-4)	4.2(-4)	-3.33	E	1
3.		<sup>2</sup> P° - <sup>2</sup> P	[265]			2	4	0.25	5.2(-4)	9.1(-4)	-2.96	E	1
			[259]			4	4	0.27	2.7(-4)	9.3(-4)	-2.96	E	1
			[267]			2	2	0.27	2.8(-4)	5.0(-4)	-3.25	E	1
			[261]			4	2	0.35	4.4(-4)	0.0015	-2.76	E	1
4.		<sup>2</sup> P° - <sup>2</sup> D	204.99	3297	491140	6	10	1500	1.6	6.5	0.98	C-	1
			205.01	0	487780	4	6	1520	1.44	3.88	0.76	C	1
			205.65	9892	496180	2	4	1440	1.83	2.48	0.56	C	1
			201.54	0	496180	4	4	68	0.041	0.11	-0.78	D	1
5.	3p <sup>5</sup> -3p <sup>4</sup> <sup>1</sup> D3d	<sup>2</sup> P° - <sup>2</sup> F	[223]			4	6	0.56	6.8(-4)	0.0021	-2.56	E	1
6.		<sup>2</sup> P° - <sup>2</sup> S	318.23	3297	461530	6	2	1310	0.311	1.34	0.271	C-	1
			216.67	0	461530	4	2	950	0.33	0.95	0.12	C-	1
			221.41	9892	461530	2	2	368	0.270	0.394	-0.267	C-	1
7.	3p <sup>5</sup> -3p <sup>4</sup> <sup>1</sup> S3d	<sup>2</sup> P° - <sup>2</sup> D	318			6	10	2.5	0.0030	0.013	-1.74	E	1
			[216]			4	6	0.37	3.9(-4)	0.0011	-2.81	E	1
			[222]			2	4	5.1	0.0075	0.011	-1.82	E	1
			[217]			4	4	0.59	4.2(-4)	0.0612	-2.77	E	1

<sup>a</sup>The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr VII

## Forbidden Transitions

Line strengths for the magnetic dipole and electric quadrupole contributions to the transition between the two levels of the  $3p^3$  configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for mixing among odd-parity configurations was limited to the set  $3s^23p^3$ ,  $3s3p^33d$ ,  $3p^33d^2$ , and  $3s^23p^33d^2$ . The strength of the electric

quadrupole transition as defined in Ref. 1 was multiplied by the factor  $2/3$  which is needed to bring this value into conformance with the definition of quadrupole strengths used in the NBS tables.

## Reference

<sup>1</sup>K.-N. Huang, Y.-K. Kim, K. T. Cheng, and J. P. Desclaux, *At. Data Nucl. Data Tables* 28, 355 (1983).

Cr VII: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{if}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$3p^3-3p^3$	$^4P^o - ^4P^o$	[10110]	0	9892	4	2	M1	17.4	1.33	B	1
						4	2	E2	0.0028	0.35	D-	1

## Cr IX

## S Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 3p^4 \ ^3P_2$ Ionization Energy:  $205.3 \text{ eV} = 1688000 \text{ cm}^{-1}$ 

## Allowed Transitions

Oscillator strengths for a few transitions of the arrays  $3s^2 3p^4 - 3s 3p^5$  and  $3p^4 - 3p^3 3d$  were interpolated from the results of Bromage<sup>1</sup> for V VIII and those of Mason<sup>2</sup> and Bromage *et al.*<sup>3</sup> for Fe XI. The term designations used here are in accord with the results of Refs. 1 and 3.

## References

- <sup>1</sup>G. E. Bromage, *Astron. Astrophys. Suppl. Ser.* **41**, 79 (1980).  
<sup>2</sup>H. E. Mason, *Mon. Not. R. Astron. Soc.* **170**, 651 (1975).  
<sup>3</sup>G. E. Bromage, R. D. Cowan, and B. C. Fawcett, *Phys. Scr.* **15**, 177 (1977).

Cr IX: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ ( $\text{cm}^{-1}$ )	$E_2$ ( $\text{cm}^{-1}$ )	$g_1$	$g_2$	$A_{ul}$ ( $10^8 \text{ s}^{-1}$ )	$f_{ul}$	$S$ (at. u.)	$\log gf$	Accuracy	Source
1.	$3s^2 3p^4 - 3s 3p^5$	$^3P - ^3P$	418.290	0	230069	5	5	14	0.937	0.25	-0.73	E	<i>interp.</i>
2.		$^1D - ^1P$	363.271	30284	306561	5	3	57	0.968	0.41	-0.47	D	<i>interp.</i>
3.	$3p^4 - 3p^3 3d$	$^3P - ^3P$	220.02	0	454500	5	5	920	0.97	2.4	0.53	E	<i>interp.</i>
						3	1		0.29		-0.96	E	<i>interp.</i>
4.		$^1D - ^1D$	215.97	30284	493310	5	5	1100	0.75	2.7	0.57	D	<i>interp.</i>
5.		$^1D - ^1P$	208.44	30284	507740	5	7	1400	1.3	4.5	0.81	D	<i>interp.</i>
6.	$3p^4 - 3p^3 3d$	$^3P - ^3P$				5	5		0.021		-0.96	D	<i>interp.</i>
7.		$^1S - ^1P$	215.04	66865	531800	1	3	1300	2.6	1.8	0.41	D	<i>interp.</i>

## Cr IX

## Forbidden Transitions

Transition probabilities for magnetic dipole and electric quadrupole lines within the  $3p^4$  configuration are the results of the scaled Thomas-Fermi calculations of Mendoza and Zeppen.<sup>1</sup> They included a number of correlation configurations in their basis set and introduced Breit-Pauli relativistic corrections as a perturbation to the nonrelativistic Hamiltonian.

## Reference

<sup>1</sup>C. Mendoza and C. J. Zeppen, Mon. Not. R. Astron. Soc. 202, 981 (1983).

Cr IX: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	S (at. u.)	Accuracy	Source
1.	$3p^4-3p^4$	$^3P - ^3P$	[12790]	0	7818	5	3	M1	10.5	2.44	C+	1
			.	.	.	5	3	E2	5.4(-4) <sup>a</sup>	0.33	D-	1
			[57790]	7818	9548	3	1	M1	0.270	1.98	C+	1
			[10470]	0	9548	5	1	E2	0.0021	0.16	D-	1
2.	$^3P - ^1D$	$^3P - ^1D$	[3301.1]	0	30284	5	5	M1	30	0.20	D-	1
			.	.	.	5	5	E2	0.053	0.062	E	1
			[4449.9]	7818	30284	3	5	M1	4.2	0.069	E	1
			.	.	.	3	5	E2	0.0018	0.0003	E	1
			[4821.2]	9548	30284	1	5	E2	6.1(-4)	0.0047	E	1
3.	$^3P - ^1S$	$^3P - ^1S$	[1495.8]	0	66855	5	1	E2	0.88	0.0039	E	1
			[1693.9]	7818	66855	3	1	M1	330	0.059	E	1
			.	.	.	.	.	.	.	.	.	.
4.	$^1D - ^1S$	$^1D - ^1S$	[2733.6]	30284	66855	5	1	E2	6.4	0.58	D-	1

<sup>a</sup>The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.



## Cr x

## P Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 3p^3 \ ^4S_{3/2}$ Ionization Energy: 244.4 eV = 1971000 cm<sup>-1</sup>

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
209.79	9	228.63	11	248.40	7	399.707	2
216.72	8	228.71	11	253	10	411.655	1
217.71	12	231.21	14	254	4	416.690	1
218.83	12	232.96	14	256	4	427.551	1
223.86	5	242.20	13	286	6	443.062	3
224.74	5	244.10	13	287	6	447.529	3
226.24	5	244.13	7	394.47	2	449.48	3
227.42	11	244.19	13	395.984	2		
227.50	11	246.97	7	398.150	2		

Line strengths for transitions of the arrays  $3s^2 3p^3$ – $3s 3p^4$  and  $3p^3$ – $3p^2 3d$  are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang.<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to configurations within the  $n=3$  complex having no more than two electrons in the  $3d$  subshell.

Huang published neither an energy-level diagram nor percentage compositions for levels of the  $3s^2 3p^3$ ,  $3s 3p^4$ , and  $3s^2 3p^2 3d$  configurations in Cr x. We have used the percentages given by Bromage *et al.*<sup>2</sup> for Fe XII, and by Bromage<sup>3</sup> for V IX and Ni XIV, as a guide to naming the levels; their values resulted from Hartree-Fock calculations with relativistic effects and statistical allowance for exchange (HXER), and incorporated correlation effects

due to a few configurations within the  $n=3$  complex. Whenever a term designation of a level in Fe XII, as given in Ref. 1, is different from that indicated in Ref. 2, all transitions involving the corresponding level in Cr x are omitted from this compilation.

Transitions involving levels which are indicated to be of low purity in *LS* coupling are omitted here. Lines which are characterized by very small *f*-values are assigned lower accuracy ratings; the weakest lines have been excluded.

## References

- <sup>1</sup>K.-N. Huang, *At. Data Nucl. Data Tables* 30, 313 (1984).  
<sup>2</sup>G. E. Bromage, R. D. Cowan, and B. C. Fawcett, *Mon. Not. R. Astron. Soc.* 183, 19 (1978).  
<sup>3</sup>G. E. Bromage, *Astron. Astrophys., Suppl. Ser.* 41, 79 (1980).

## Cr x: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	<i>S</i> (at. u.)	log <i>gf</i>	Accuracy	Source
1.	$3s^2 3p^3$ – $3s 3p^4$	<sup>8</sup> S– <sup>4</sup> P	431.18	0	237428	4	12	12	0.097	0.54	–0.41	D	1
			427.561	0	223890	4	6	12	0.048	0.27	–0.72	D	1
			416.690	0	239987	4	4	13	0.023	0.18	–0.88	D	1
			411.655	0	242922	4	2	13	0.017	0.090	–1.18	D	1
2.	<sup>3</sup> D– <sup>3</sup> D	<sup>3</sup> D– <sup>3</sup> D	397.28	38507	390218	10	10	23	0.055	0.72	–0.26	E	1
			398.150	39444	290606	6	6	21	0.051	0.40	–0.52	D	1
			395.984	37102	289637	4	4	24	0.058	0.30	–0.64	D	1
			399.707	39444	289637	6	4	0.71	0.0011	0.0090	–2.16	E	1
			[394.47]	37102	290606	4	6	0.34	0.0012	0.0062	–2.32	E	1

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Cr X: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$L_1$	$L_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accuracy	Source
3.		P - D	446.16	66083	290218	6	10	3.4	0.017	0.15	-0.99	D-	1
			447.529	67157	290696	4	6	4.1	0.019	0.11	-1.13	D	1
			443.062	63935	289637	2	4	2.4	0.014	0.041	-1.55	D	1
			[449.68]	67157	289637	4	4	0.033	1.0(-4) <sup>a</sup>	5.9(-4)	-3.40	E	1
4.	3p <sup>1</sup> -3p <sup>4</sup> D3d	S - D	[254]			4	6	1.1	0.0015	0.0051	-2.21	E	1
			[256]			4	4	1.1	0.0011	0.0035	-2.37	E	1
5.		S - P	225.34	0	443789	4	12	750	1.7	5.1	0.84	D	1
			226.24	0	442010	4	6	730	0.84	2.5	0.53	D	1
			224.74	0	444960	4	4	760	0.57	1.7	0.35	D	1
			223.86	0	446710	4	2	770	0.29	0.85	0.06	D	1
6.		D - D	[287]			6	4	1.3	0.0010	0.0059	-2.20	E	1
			[296]			4	2	1.7	0.0011	0.0040	-2.57	E	1
7.		D - P	[248.40]	39444	442010	6	6	5.7	0.0053	0.025	-1.50	E	1
			[244.13]	37102	446710	4	2	3.4	0.0015	0.0049	-2.21	E	1
			[246.97]	37102	442010	4	6	1.6	0.0022	0.0071	-2.06	E	1
8.		D - F	216.72	39444	500960	6	8	900	0.84	3.6	0.70	E	1
9.	3p <sup>1</sup> -3p <sup>4</sup> D3d	S - D	[209.79]	0	476670	4	6	1.1	0.0011	0.0030	-2.26	E	1
10.		D - G	[253]			6	8	1.0	0.0013	0.0066	-2.10	E	1
11.		D - D	228.20	36507	476730	10	10	530	0.41	3.1	0.62	D	1
			228.71	39444	476670	6	6	450	0.35	1.6	0.23	D	1
			227.42	37102	476820	4	4	520	0.46	1.2	0.20	D	1
			[228.63]	39444	476820	6	4	81	0.042	0.19	-0.60	D	1
			[227.50]	37102	476670	4	6	18	0.021	0.064	-1.07	D	1
12.		D - P	[218.83]	39444	496420	6	4	10	0.0049	0.021	-1.54	E	1
			[217.71]	37102	496420	4	4	7.4	0.0052	0.015	-1.68	E	1
13.		P - D	247.52	66083	476730	6	10	55	0.081	0.29	-0.31	E	1
			[244.19]	67157	476670	4	6	58	0.078	0.25	-0.51	D	1
			[242.20]	63935	476820	2	4	50	0.088	0.14	-0.76	D	1
			[244.10]	67157	476820	4	4	1.0	9.9(-4)	0.0030	-2.43	E	1
14.		P - P	232.96	67157	496420	4	4	440	0.36	1.1	0.16	E	1
			231.21	63935	496420	2	4	120	0.20	0.20	-0.40	E	1

<sup>a</sup>The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied

## Cr X

## Forbidden Transitions

Line strengths for magnetic dipole and electric quadrupole transitions within the  $3p^3$  configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang.<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to configurations within the  $n=3$  complex having no more than two electrons in the  $3d$  subshell. Strengths of electric quadrupole transitions as defined in Ref. 1 were multiplied by the factor  $2/3$ , which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables. We have excluded from this compilation the electric quadrupole contributions to the  $^4S_{3/2} - ^2P_{1/2}$  and

$^4S_{3/2} - ^2P_{1/2}$  transitions, since their strengths are very small and thus subject to considerable uncertainty.

Data for these same transitions calculated by Mendoza and Zeippen<sup>2</sup> with the scaled Thomas-Fermi approach with allowance for correlation are generally in very good agreement with the results of Ref. 1. These latter calculations treated relativistic effects by introducing Breit-Pauli corrections as a perturbation to the relativistic Hamiltonian.

## References

- <sup>1</sup>K.-N. Huang, *At. Data Nucl. Data Tables* 30, 313 (1984).  
<sup>2</sup>C. Mendoza and C. J. Zeippen, *Mon. Not. R. Astron. Soc.* 198, 127 (1982).

Cr X: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E$ (cm <sup>-1</sup> )	$E_1$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$3p^3-3p^3$	$S - ^3D$	[2534.5]	0	39444	4	6	M1	0.30	0.0011	E	1
			-	-	-	4	6	E2	0.040	0.015	E	1
			[2694.5]	0	37102	4	4	M1	11	0.933	D	1
			-	-	-	4	4	E2	0.020	0.0066	E	1
2.	$S - ^3P$		1489.04	0	67157	4	4	M1	120	0.050	D	1
			1564.10	0	63935	4	2	M1	60	0.017	D	1
3.	$^3D - ^3D$		[42690]	37102	39444	4	6	M1	0.127	2.20	C+	1
						4	6	E2	1.8(-7) <sup>a</sup>	0.092	E	1
4.	$^3D - ^3P$		[4082.0]	39444	63935	6	2	E2	0.25	0.34	D-	1
			[3607.4]	39444	67157	6	4	M1	27	0.19	C	1
			-	-	-	6	4	E2	0.76	1.1	D-	1
			[3725.7]	37102	63935	4	2	M1	26	0.10	C	1
			-	-	-	4	2	E2	0.55	0.47	D-	1
			[3226.3]	37102	67157	4	4	M1	62	0.34	C	1
5.	$^3P - ^3P$		[31030]	63935	67157	2	4	M1	0.273	1.21	C+	1
						2	4	E2	5.1(-7)	0.035	E	1

<sup>a</sup>The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.



Cr XI: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (int. u.)	log $g f$	Accuracy	Source
3.		<sup>1</sup> D - <sup>1</sup> D'	(483.27)	36994	263917	5	7	0.51	0.0015	0.012	-2.12	E	1
4.		<sup>3</sup> S - <sup>3</sup> P'	(496)			1	3	0.004	0.0010	0.0017	-2.98	E	1
5.	<sup>3</sup> p' - <sup>3</sup> p3d	<sup>3</sup> P - <sup>3</sup> P'	(273)			5	7	1.3	0.0020	0.0001	-1.90	E	1
6.		<sup>3</sup> P - <sup>3</sup> P'	(232)			3	1	410	0.11	0.25	-0.40	D	1
7.		<sup>3</sup> P - <sup>1</sup> D'	226.53	11981	436550	5	7	550	0.64	2.5	0.51	D	1
8.		<sup>3</sup> P - <sup>3</sup> P'	(214.31)	11981	476500	5	7	14	0.013	0.045	-1.19	E	1
9.		<sup>3</sup> P - <sup>3</sup> P'	(198)			1	3	2.9	0.0051	0.0003	-2.30	E	1
10.		<sup>1</sup> D - <sup>1</sup> D'	(209)			5	5	1.5	0.0020	0.010	-1.90	E	1
11.		<sup>1</sup> D - <sup>1</sup> D'	(250.28)	36994	436550	5	7	10	0.013	0.054	-1.18	E	1
12.		<sup>1</sup> D - <sup>1</sup> P'	226.45	36994	476500	5	7	600	0.65	2.41	0.51	C	1
13.		<sup>3</sup> S - <sup>3</sup> P'	240.76			1	3	430	1.2	0.30	0.10	D	1

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Cr XI

Forbidden Transitions

List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
519.13	11	1500	5	2799.2	8	15520	1
520	10	1500	3	2807.9	8	18050	1
710	9	2630	4	2874.1	8	63720	7
740	9	2750.1	8	2899.4	8	68570	7
840	6	2758.5	8	3178.2	2	901000	7
1400	5	2773.2	8	3995.8	2		
1440	3	2781.7	8	8244.3	1		

Line strengths for magnetic dipole and electric quadrupole transitions are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang.<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration interaction encompassed all configurations within the  $n=3$  complex. Huang calculated line strengths for transitions within the  $3p^2$  configuration, as well as for transitions between pairs of odd-parity levels whose lower level is one of the four lowest-lying odd-parity levels in the  $n=3$  complex. Transitions involving odd-parity levels which are indicated by Bromage *et al.*<sup>2</sup> (for Fe XIII) or Bromage<sup>3</sup> (for V X and Ni XV) to be of low purity in  $LS$  coupling in

Fe-group species are omitted here, as are lines whose strengths are very small. Strengths of electric quadrupole transitions as reported in Ref. 1 were multiplied by the factor  $2/3$  which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables.

## References

- <sup>1</sup>K.-N. Huang, *At. Data Nucl. Data Tables* 32, 503 (1985) and private communication.  
<sup>2</sup>G. E. Bromage, R. D. Cowan, and B. C. Fawcett, *Mon. Not. R. Astron. Soc.* 193, 19 (1978).  
<sup>3</sup>G. E. Bromage, *Astron. Astrophys. Suppl. Ser.* 41, 79 (1980).

Cr II: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$3p^1-3p^1$	P - P	[15520]	5539	11981	3	5	M1	3.45	2.39	C+	1
			-	-	-	3	5	E2	$1.0-4^a$	0.27	D-	1
			[18950]	0	5539	1	3	M1	2.98	1.95	C+	1
			[8344.3]	0	11981	1	5	E2	0.0011	0.13	D-	1
2.	P - D	3996.8	11981	36994	5	5	M1	26	0.31	E	1	
		-	-	-	5	5	E2	0.027	0.001	E	1	
		[3178.2]	5539	36994	3	5	M1	18	0.11	E	1	
		-	-	-	3	5	E2	0.012	0.012	E	1	
3.	P - S	[1590]	-	-	5	1	E2	1.5	0.0092	E	1	
		[1440]	-	-	3	1	M1	370	0.041	E	1	
4.	D - S	[2630]	-	-	5	1	E2	6.9	0.52	D-	1	
5.	$2s2p^1-2s2p^1$	S - D	[1480]	-	-	5	7	E2	0.25	0.0056	E	1
			[1500]	-	-	5	5	M1	7.5	0.0047	E	1
			-	-	-	5	5	E2	0.16	0.0037	E	1
6.	S - P	[940]	-	-	5	5	M1	240	0.037	E	1	
		[940]	-	-	5	3	M1	120	0.012	E	1	
7.	D - D	[68570]	24248	243917	5	7	M1	0.054	4.52	C-	1	
		-	-	-	5	7	E2	$7.7-9)$	0.046	E	1	
		[901000]	24248	242459	2	5	M1	$3.2-5)$	4.4	E	1	
		[63720]	24248	243917	3	7	E2	$2.5-9)$	0.011	E	1	

## Cr II: Forbidden transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (a. u.)	Accuracy	Source
8.		<sup>3</sup> D - <sup>3</sup> F	[2899.4]	263917	278397	7	3	E2	1.4	0.53	D-	1
			[2897.9]	262459	278062	5	1	E2	3.5	0.36	D-	1
			[2874.1]	263917	278709	7	5	M1	32	0.14	E	1
			-	-	-	7	5	E2	1.7	0.99	D-	1
			[2781.7]	262459	278397	5	3	E2	0.28	0.003	E	1
			[2799.2]	262348	278062	3	1	M1	42	0.034	E	1
			[2758.5]	262459	278709	5	5	M1	25	0.008	E	1
			-	-	-	5	5	E2	1.3	0.69	D-	1
			[2773.2]	262348	278397	3	3	M1	42	0.009	E	1
			-	-	-	3	3	E2	1.6	0.67	D-	1
			[2750.1]	262348	278709	3	5	M1	7.3	0.028	E	1
			-	-	-	3	5	E2	0.38	0.18	D-	1
			9.	3s <sup>2</sup> 3p <sup>2</sup> -3s <sup>2</sup> 3p3d	<sup>3</sup> D - <sup>3</sup> F	[710]			5	9	E2	6.5
[709]						3	7	E2	3.9	0.0028	E	1
[710]						7	9	M1	590	0.064	E	1
10.		<sup>3</sup> D - <sup>3</sup> F	[520]			5	1	E2	250	0.0067	E	1
11.		<sup>3</sup> D - <sup>3</sup> D	[519.13]	263917	436559	7	7	M1	41	0.0015	E	1

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XII

## Al Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 3p^1 P_{1/2}$

Ionization Energy: 298.0 eV = 2404000 cm<sup>-1</sup>

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
196	29	247	19,20	289	28	308	15
198	22	248	25	273	28	309	15,16
209	31	250	20	274	28	311.66	3
216	30	251	35	275	6	318.82	2
217	30	251.62	17	278	6,28	320.20	5
218	30	252	19	280	18	324	14
221	21	252.11	17	282	18	325	4,14
222	26	254	25,24,25	286	24	325.13	5
239	32	256	25	294	23	327	14
244	19	256	19,27	294.77	3	330	8
244.70	17	259	27	300.32	3	331	8
246	20	266	23	306.81	3	331.96	2

List of tabulated lines — Continued

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
332	8	401	7	410.91	1	449	11
332.86	5	402	12	412.46	1	458	11
338	4	403	7	413	9	461	11
344	13	405	7	417	12	589	10
346	13	407	7	419	12		
393.00	1	410	9	446	11		

Line strengths for transitions of the arrays  $3s^23p-3s3p^2$ ,  $3s3p^2-3p^3$ ,  $3s^23d-3s3p3d$ ,  $3s^23p-3s^23d$ , and  $3s3p^2-3s3p3d$  are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Huang.<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction. Allowance for configuration mixing included all configurations within the  $n=3$  complex.

Huang published neither an energy-level diagram nor percentage compositions for levels of the  $3s^23p$ ,  $3s3p^2$ ,  $3s^23d$ ,  $3p^3$ , and  $3s3p3d$  configurations in Cr XII. We have used the percentages given by Fawcett<sup>2</sup> as a guide to naming the levels; the latter's values resulted from Hartree-Fock calculations with relativistic effects and statistical allowance for exchange (HXE), and incorporated correlation effects due to all configurations within the  $n=3$  complex.

Transitions involving levels which are indicated to be of low purity in *LS* coupling are omitted here. Lines which are characterized by very small  $f$ -values are assigned lower accuracy ratings; the weakest lines have been excluded. A few wavelengths computed by Huang differ significantly from those which resulted from the fitting and scaling procedure applied by Fawcett<sup>2</sup>; lines for which the wavelengths are in serious disagreement have been omitted.

## References

<sup>1</sup>K.-N. Huang, *At. Data Nucl. Data Tables* 34, 1 (1986) and private communication.

<sup>2</sup>B. C. Fawcett, *At. Data Nucl. Data Tables* 28, 557 (1983).

Cr XII: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (int. u.)	log $gf$	Accuracy	Source
1.	$3s^23p-3s3p^2$	$^7P^o - ^7D$	404.86	8000	255000	6	10	16	0.064	0.51	-0.42	E	1
			410.91	12000	255360	4	6	15	0.065	0.30	-0.65	D	1
			393.00	0	254450	2	4	17	0.077	0.20	-0.81	D	1
			412.46	12000	254450	4	4	0.94	0.0024	0.013	-2.02	E	1
2.	$^7P^o - ^7S$	327.16	8000	313660	6	2	130	0.068	0.44	-0.39	D	1	
		331.96	12000	313660	4	2	21	0.017	0.075	-1.16	D	1	
		318.82	0	313660	2	2	110	0.17	0.36	-0.46	D	1	
3.	$^7P^o - ^7P$	303.80	8000	337160	6	6	230	0.45	2.7	0.43	D	1	
		306.81	12000	339250	4	4	276	0.387	1.56	0.190	C-	1	
		[300.22]	0	332980	2	2	140	0.19	0.38	-0.42	D	1	
		311.55	12000	332980	4	2	160	0.12	0.48	-0.33	D	1	
		294.77	0	339250	2	4	60	0.157	0.304	-0.50	C-	1	
4.	$3s3p^2-3p^3$	$^7P - ^7D$	[338]			6	4	1.6	0.0018	0.012	-1.97	E	1
			[325]			2	4	0.56	0.0018	0.0028	-2.45	E	1
5.	$^7P - ^7S$	327.71			12	4	290	0.15	2.0	0.27	D	1	
		332.06			6	4	140	0.15	1.0	-0.04	D	1	
		325.13			4	4	99	0.16	0.67	-0.20	D	1	
		320.20			2	4	52	0.16	0.34	-0.49	D	1	



## Cr II: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ ( $\text{cm}^{-1}$ )	$E_2$ ( $\text{cm}^{-1}$ )	$g_1$	$g_2$	$A_{21}$ ( $10^6 \text{ s}^{-1}$ )	$f_{12}$	$S$ (at. u.)	$\log gf$	Accuracy	Source
6.		$^3P - ^3P$	[278]			4	4	2.2	0.0026	0.0035	-1.98	E	1
			[275]			2	4	0.97	0.0022	0.0040	-2.95	E	1
7.		$^3D - ^3D$	404			10	10	28	0.060	0.92	-0.16	E	1
			[403]			6	6	26	0.064	0.51	-0.42	E	1
			[405]			4	4	21	0.051	0.27	-0.69	E	1
			[407]			6	4	6.5	6.011	0.0088	-1.18	E	1
			[401]			4	6	2.5	0.0039	0.047	-1.45	E	1
8.		$^3D - ^3P$	331			10	6	100	0.10	1.1	0.00	D	1
			[331]			6	4	85	0.003	0.51	-0.25	D	1
			[332]			4	2	110	0.007	0.38	-0.46	D	1
			[330]			4	4	11	0.018	0.077	-1.15	D	1
9.		$^3S - ^3P$	411			2	6	12	0.009	0.24	-0.75	E	1
			[410]			2	4	16	0.061	0.22	-0.79	D	1
			[413]			2	2	3.0	0.0077	0.021	-1.81	E	1
10.		$^3P - ^3S$											
11.		$^3P - ^3P$	[599]			4	4	0.31	0.0016	0.013	-2.18	E	1
			455			6	6	26	0.061	0.73	-0.31	E	1
12.	$3s^2 3d - 3s 3p(^3P) 3d$	$^3D - ^3P$	[458]			4	4	22	0.070	0.42	-0.56	D	1
			[449]			2	2	27	0.061	0.24	-0.79	D	1
			[461]			4	2	6.5	0.010	0.063	-1.38	D	1
			[446]			2	4	0.23	0.0014	0.0041	-2.55	E	1
			408			10	14	17	0.061	0.82	-0.21	E	1
13.		$^3D - ^3P$	[402]			6	8	19	0.60	0.48	-0.44	E	1
			[417]			4	6	14	0.053	0.29	-0.68	E	1
			[419]			6	6	2.4	0.0063	0.052	-1.42	E	1
			[348]			6	4	2.1	0.0025	0.017	-1.83	E	1
14.	$3s^2 3d - 3s 3p(^1P) 3d$	$^3D - ^3P$	[344]			4	4	2.6	0.0046	0.021	-1.73	E	1
			326			10	14	230	0.50	5.4	0.70	E	1
15.		$^3D - ^3D$	[327]			6	8	220	0.48	3.1	0.46	E	1
			[324]			4	6	220	0.52	2.2	0.31	E	1
			[325]			6	6	9.8	0.016	0.10	-1.03	E	1
16.		$^3D - ^3P$	[309]			6	6	160	0.23	1.1	0.14	E	1
			[308]			4	6	5.0	0.011	0.043	-1.37	E	1
16.		$^3D - ^3P$	[309]			4	2	270	0.19	0.79	-0.11	D	1

Cr II: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (st. u.)	log $gf$	Accuracy	Source
17.	3p-3d	<sup>3</sup> P - <sup>3</sup> D	249.25	8000	409210	6	10	350	0.55	2.7	0.52	D	1
			251.52	12000	409580	4	6	340	0.48	1.6	0.29	D	1
			244.70	0	408660	2	4	300	0.55	0.88	0.04	D	1
			[252.11]	12000	408660	4	4	66	0.063	0.21	-0.60	D	1
18.	3s3p <sup>+</sup> - 3s3p( <sup>3</sup> P)3d	<sup>3</sup> P - <sup>3</sup> F	[282]			6	8	1.2	0.0020	0.011	-1.93	E	1
			[280]			4	6	0.72	0.0013	0.0047	-2.29	E	1
19.		<sup>3</sup> P - <sup>3</sup> P	[256]			6	6	54	0.034	0.17	-0.70	D	1
			[244]			2	2	12	0.011	0.017	-1.67	D	1
			[247]			4	2	240	0.11	0.26	-0.35	D	1
			[252]			4	6	200	0.28	0.94	0.05	D	1
20.		<sup>3</sup> P - <sup>3</sup> D	[250]			6	8	350	0.437	2.16	0.419	C-	1
			[246]			4	6	110	0.15	0.48	-0.23	D	1
			[250]			6	6	220	0.20	1.0	0.08	D	1
			[247]			2	2	330	0.30	0.49	-0.22	D	1
21.		<sup>3</sup> P - <sup>3</sup> F	[221]			6	8	1.9	0.0019	0.0082	-1.95	E	1
22.		<sup>3</sup> P - <sup>3</sup> P	[198]			2	4	1.6	0.0018	0.0024	-2.43	E	1
23.		<sup>3</sup> D - <sup>3</sup> P	[294]			6	6	4.9	0.0064	0.037	-1.42	E	1
24.		<sup>3</sup> D - <sup>3</sup> D	[286]			6	8	1.5	0.0025	0.014	-1.83	E	1
25.		<sup>3</sup> D - <sup>3</sup> P	251			10	14	140	0.18	1.5	0.26	E	1
			[248]			6	8	140	0.17	0.84	0.01	E	1
			[254]			4	6	120	0.17	0.57	-0.17	E	1
			[255]			6	6	18	0.017	0.086	-0.99	E	1
26.		<sup>3</sup> D - <sup>3</sup> P	[222]			4	2	0.44	1.6 <sub>u</sub> - 4 <sub>u</sub>	4.8 <sub>u</sub> - 4 <sub>u</sub>	-3.18	E	1
27.		<sup>3</sup> S - <sup>3</sup> P	258			2	6	290	0.82	1.4	0.22	D	1
			[259]			2	4	320	0.65	1.1	0.11	D	1
			[256]			2	2	150	0.15	0.25	0.53	D	1
28.		<sup>3</sup> P - <sup>3</sup> P	275			6	6	150	0.17	0.93	0.01	D	1
			[278]			4	4	97	0.11	0.41	0.35	D	1
			[269]			2	2	210	0.23	0.40	0.35	D	1
			[274]			4	2	42	0.024	0.086	1.02	D	1
			[273]			2	4	7.7	0.017	0.031	-1.46	D	1

## Cr XII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $g^f$	Accuracy	Source
29.	3s3p <sup>2</sup> - 3s3p(1P)3d	1P - 1P	[196]			6	8	1.6	0.0012	0.0048	-2.13	E	1
			30.	1D - 1P	217		10	14	250	0.25	1.8	0.40	E
30.		1D - 1P	[218]			6	8	240	0.23	1.0	0.14	E	1
			[216]			4	6	240	0.25	0.72	0.01	E	1
			[217]			6	6	14	0.010	0.043	-1.22	E	1
			31.	1D - 1P	[209]			4	2	1.7	5.5(-4)	0.0015	-2.66
32.		1S - 1P	[239]			2	2	160	0.13	0.21	-0.57	D	1
			33.	1P - 1P	[265]			4	6	1.3	0.0020	0.0070	-2.10
34.		1P - 1D	[254]			4	6	520	0.75	2.5	0.48	E	1
35.		1P - 1P	[251]			2	2	70	0.067	0.11	-0.88	D	1
			[254]			4	2	75	6.0362	0.121	-0.84	C-	1

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XII

## Forbidden Transitions

Line strengths for magnetic dipole and electric quadrupole transitions within the 3s<sup>2</sup>3p<sup>2</sup> 1P and 3s3p<sup>2</sup> 1P terms are the results of the multiconfiguration Dirac-Fock (MCDHF) calculations of Huang.<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing included all configurations within the n = 3 complex. Strengths of electric quadrupole transi-

tions as reported in Ref. 1 were multiplied by the factor 2/3 which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables.

## Reference

<sup>1</sup>K.-N. Huang, At. Data Nucl. Data Tables 34, 1 (1986).

Cr XII: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{if}$ (s <sup>-1</sup> )	S (at. u.)	Accuracy	Source
1.	3p-3p	<sup>3</sup> P - <sup>3</sup> P	[8331]	0	12000	2	4	M1	15.5	1.33	C	1
						2	4	E2	0.0025	0.24	D-	1
2.	3s3p <sup>2</sup> -3s3p <sup>2</sup>	<sup>3</sup> P - <sup>3</sup> P	[15600]			4	6	M1	4.24	3.58	C	1
						4	6	E2	1.1(-4) <sup>a</sup>	0.36	D-	1
						2	4	M1	2.38	3.31	C	1
						2	4	E2	3.0(-6)	0.030	E	1
						2	6	E2	0.0013	0.27	D-	1

<sup>a</sup>The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XIII

## Mg Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 \ ^1S_0$

Ionization Energy: 354.8 eV = 2862000 cm<sup>-1</sup>

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
49.59	14	276.4	18	362.6	4	449.76	7
67.01	13	277	22	363.96	3	451.7	7
224	21	279.32	16	367.9	9	461.60	7
228	20	286	24	368.06	3	463.2	7
259.68	15	298	19	369.13	9	465.1	7
261.91	15	328.29	2	371	8	482.2	1
262.33	15	342.69	3	374	12	560.11	5
267.73	15	345	23	375.1	4	638	10
268.4	15	351.14	3	377.60	6		
268.9	15	353.81	3	385	11		
270	17	356.12	3	437.05	7		

Oscillator strengths for the three transitions  $3s^2 \ ^1S_0 - 3snp \ ^1P_1$  ( $n=3-5$ ) are the results of the relativistic random phase approximation (RRPA) calculations of Shorer *et al.*,<sup>1</sup> who allowed for correlation within the context of a frozen core. Oscillator strength data of Fawcett,<sup>2</sup> quoted for most transitions of the arrays  $3s3p-3p^2$ ,  $3s3d-3p3d$ ,  $3s3p-3s3d$ , and  $3p^2-3p3d$ , were derived by means of Hartree-Fock calculations which included relativistic effects and statistical allowance for exchange (HXR); he incorporated correlation effects due to all configurations in the  $n=3$  complex. Froese Fischer and Godefroid<sup>1</sup> determined  $f$ -values for singlet-singlet transitions within the complex by applying a nonrelativistic

multiconfiguration Hartree-Fock (MCHF) technique with large-scale allowance for configuration interaction; their results are quoted for two transitions of the  $3p3d-3d^2$  array for which we estimate the contribution of singlet-triplet mixing to the  $f$ -value to be insignificant.  $A$ -values for the three intercombination lines tabulated here were calculated by Kastner and Bhatia<sup>4</sup> using a scaled Thomas-Fermi approach that allowed for correlation due to all configurations in the  $n=3$  complex.

Transitions involving levels which are indicated in Ref. 2 to be of low purity in  $LS$  coupling are omitted here. Lines which are characterized by very small  $f$ -values are assigned lower accuracy ratings.

## References

- <sup>a</sup>B. C. Fawcett, At. Data Nucl. Data Tables 28, 579 (1983).  
<sup>b</sup>C. Froese Fischer and M. Godfrey, Nucl. Instrum. Methods 202, 307 (1982).  
<sup>c</sup>P. Shorer, C. D. Lin, and W. R. Johnson, Phys. Rev. A 16, 1109 (1977).  
<sup>d</sup>S. O. Kastner and A. K. Bhatia, J. Opt. Soc. Am. 69, 1391 (1979).

## Cr XIII: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (int. u.)	log $g f^o$	Accuracy	Source
1.	3s <sup>2</sup> -3s3p	<sup>3</sup> S - <sup>3</sup> P	482.2	0	297400	1	3	0.18	0.0019	0.0000	-2.73	E	4
2.		<sup>3</sup> S - <sup>1</sup> P	328.29	0	304610	1	3	186	0.302	0.975	-0.045	B	1
3.	3s3p-3p <sup>2</sup>	<sup>3</sup> P - <sup>3</sup> P	355.2	212100	490000	9	9	150	0.28	2.9	0.30	D	2
			353.81	216000	490200	5	5	100	0.19	1.1	-0.02	D	2
			356.12	207400	488200	3	3	40	0.977	0.27	-0.64	C	2
			368.06	216000	490200	5	3	61	0.974	0.45	-0.43	C	2
			363.96	207400	482200	3	1	150	0.10	0.36	-0.52	C	2
			342.69	207400	490200	3	5	34	0.10	0.34	-0.52	D	2
			351.14	203400	488200	1	3	56	0.31	0.36	-0.51	C	2
4.		<sup>3</sup> P - <sup>1</sup> D											
			[375.1]	216000	483150	5	5	13	0.027	0.17	-0.96	E	4
			[362.6]	207400	483150	3	5	6.4	0.021	0.975	-1.20	E	4
5.		<sup>1</sup> P - <sup>1</sup> D	560.11	304610	483150	3	5	13	0.10	0.55	-0.52	E	2
6.		<sup>1</sup> P - <sup>1</sup> S	377.60	304610	509440	3	1	150	0.11	0.41	-0.48	C	2
7.	3s3d-3p3d	<sup>3</sup> D - <sup>3</sup> P	447.2	589500	813100	15	21	42	0.18	3.9	0.42	D	2
			437.05	590100	818900	7	9	46.4	0.171	1.72	0.078	C	2
			449.76	589200	811500	5	7	35	0.15	1.1	-0.12	C	2
			461.60	588500	805100	3	5	28	0.15	0.68	-0.35	D	2
			[451.7]	590100	811500	7	7	6.9	0.021	0.22	-0.83	C	2
			[463.2]	589200	805100	5	5	6.8	0.022	0.17	-0.96	D	2
			[465.1]	590100	805100	7	5	0.13	2.9(-4) <sup>d</sup>	0.0031	-2.69	E	2
8.		<sup>3</sup> D - <sup>3</sup> P											
			[371]			3	1	87	0.060	0.22	-0.74	C	2
9.		<sup>3</sup> D - <sup>3</sup> D											
			369.13	590100	861000	7	7	64	0.13	1.1	-0.04	C	2
			[367.9]	589200	861000	5	7	13	0.038	0.23	-0.72	C	2
10.		<sup>1</sup> D - <sup>1</sup> D	[638]			5	5	5.9	0.036	0.38	-0.74	D	2
11.		<sup>1</sup> D - <sup>1</sup> P	[385]			5	7	150	0.48	3.0	0.38	D	2
12.		<sup>1</sup> D - <sup>1</sup> P	[374]			5	3	100	0.13	0.80	-0.19	D	2
13.	3s <sup>2</sup> -3s4p	<sup>1</sup> S - <sup>1</sup> P	67.01	0	1492000	1	3	1670	0.238	0.075	-0.471	C	1
14.	3s <sup>2</sup> -3s5p	<sup>1</sup> S - <sup>1</sup> P	49.59	0	2017000	1	3	990	0.109	0.0178	-0.96	C	1

Cr XIII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$K$	$g_1$	$A_{21}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (a.t. u.)	log $gf$	Accuracy	Source
15.	3s3p-3s3d	<sup>3</sup> P - <sup>3</sup> D	265.0	21210 <sup>0</sup>	588500	9	15	197	0.345	2.71	0.492	C	2
			267.73	216600	590100	5	7	190	0.286	1.26	0.155	C	2
			261.91	207400	589200	3	5	150	0.26	0.67	-0.11	C	2
			259.68	203400	588500	1	3	120	0.35	0.30	-0.46	C	2
			[268.4]	216600	589200	5	5	48	0.052	0.23	-0.59	C	2
			262.33	207400	588500	3	3	84	0.087	0.23	-0.58	C	2
			[268.9]	216600	588500	5	3	5.2	0.0034	0.015	-1.77	D	2
16.		<sup>1</sup> P - <sup>1</sup> D	279.32	304610	662620	3	5	350	0.69	1.9	0.32	D	2
17.	3p <sup>2</sup> -3p3d	<sup>3</sup> P - <sup>3</sup> P	[270]			3	1	170	0.063	0.17	-0.72	C	2
18.		<sup>3</sup> P - <sup>3</sup> D	[276.4]	439200	861000	5	7	220	0.35	1.6	0.24	D	2
19.		<sup>1</sup> D - <sup>1</sup> D	[298]			5	5	130	0.17	0.83	-0.07	E	2
20.		<sup>1</sup> D - <sup>1</sup> F	[228]			5	7	180	0.20	0.75	0.00	E	2
21.		<sup>1</sup> D - <sup>1</sup> P	[224]			5	3	2.9	0.0013	0.0048	-2.19	E	2
22.		<sup>1</sup> S - <sup>1</sup> P	[277]			1	3	210	0.73	0.67	-0.14	C	2
23.	3p3d-3d <sup>2</sup>	<sup>1</sup> F - <sup>1</sup> G	[345]			7	9	174	0.399	3.17	0.446	C-	3
24.		<sup>1</sup> P - <sup>1</sup> S	[296]			3	1	460	0.188	0.53	-0.249	C-	3

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XIV

Na Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 3s^2 S_{1/2}$ Ionization Energy:  $384.171 \text{ eV} = 3098520 \text{ cm}^{-1}$ 

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
36.466	6	54.164	10	104.5	48	217.2	51
38.936	5	60.699	21	107.7	47	217.4	62
39.796	17	60.756	21	107.8	47	221.5	43
40.016	17	60.761	21	109.8	37	221.9	43
40.018	17	63.324	2	110.4	37	222.9	43
40.782	4	63.539	2	111.2	53	223.3	70
40.800	4	63.935	20	117.6	36	223.4	70
41.566	15	64.005	20	118.3	36	238.8	69
41.788	15	64.045	20	125.2	46	239.0	69
41.796	15	68.594	9	125.3	46	241.5	74
42.207	14	69.213	9	132.1	45	241.7	74
42.453	14	69.247	9	133.2	45	286.3	56
44.597	13	79.126	32	133.3	45	287.2	56
44.869	13	84.631	41	136.0	52	289.735	7
44.873	13	85.012	41	148.5	29	297.9	61
45.835	12	85.020	41	149.1	29	300.1	61
46.125	12	86.060	19	154.4	58	360.271	7
46.417	26	86.169	19	157.1	35	300.3	61
46.453	26	86.185	19	158.4	35	301.814	7
46.468	3	86.911	31	165.0	65	346.3	68
46.527	3	93.006	39	165.7	65	346.5	68
48.300	25	93.432	39	187.02	44	346.6	68
48.336	25	93.467	39	187.2	44	363.5	60
48.340	25	95.997	49	187.30	44	367.1	60
48.991	24	96.061	49	188.0	71	389.81	1
49.032	24	96.330	38	188.1	71	400.3	73
50.821	11	96.824	38	189.1	34	400.5	73
51.172	11	99.443	54	190.0	37	400.6	73
51.180	11	99.453	54	191.0	34	411.99	1
52.321	23	99.473	54	192.3	75	413.7	67
52.363	23	100.88	18	200.1	63	414.3	67
52.367	23	101.06	18	201.0	63	415.6	67
53.642	22	101.42	18	201.2	63	789.3	33
53.674	22	102.7	30	216.1	62	819.0	33
53.691	22	102.8	30	217.0	51	823.7	33
53.760	10	104.4	48	217.1	51		

Strengths of the lines of the  $3s-3p$  and  $3p-3d$  transitions were taken from Edlén's interpolation formulae.<sup>1</sup> These were based on the results of Weiss' Hartree-Fock calculations,<sup>2</sup> in which ratios of relativistic Dirac to non-relativistic line strengths in hydrogenic ions were applied as scaling factors to the nonrelativistic Hartree-Fock line strengths in the corresponding sodiumlike species. Oscillator strengths for the  $4p-4d$  transitions were derived by Gruzdev and Sherstyuk<sup>3</sup> using the relativistic variant of their effective orbital quantum number method, which utilizes a Coulomb potential in conjunction with a semiempirical orbital quantum num-

ber which is determined from experimental energy levels. Strengths of the lines of the  $3s-4p$  transition were interpolated from the results of the relativistic single-configuration Hartree-Fock calculations of Kim and Deaulx<sup>4</sup> for V XIII and Fe XVI.

Multiplet  $f$ -values calculated by Biemont<sup>5</sup> using a fully variational Hartree-Fock approach are quoted for numerous transitions  $n'l-n'l'$  ( $3 \leq n \leq 5$ ;  $4 \leq n' \leq 8$ ;  $l, l' = s, p, d, f$ ). Data for additional transitions (namely, those for which  $n > 5$ , where  $n$  is the principal quantum number of the lower state) can be found in Ref. 5. Whenever wavelengths of individual lines within a mul-

triplet either were available directly or could be determined from the energy levels, the multiplet strength was distributed among the lines according to  $LS$ -coupling rules, except in cases where the wavelengths of all the lines in the multiplet are identical. The strength of the  $3p\ ^3P - 4s\ ^2S$  multiplet was not distributed between the two lines in the multiplet, however, since the relativistic single-configuration Hartree-Fock calculations of Kim and Cheng<sup>6</sup> indicate that in the corresponding transition in sodiumlike iron the ratio of the two line strengths deviates somewhat from the value that would be obtained in the case of pure  $LS$  coupling.

Transitions with small  $f$ -values were generally assigned lower accuracy ratings.

## References

- <sup>1</sup>B. Edlén, *Phys. Scr.* 17, 565 (1978).  
<sup>2</sup>A. W. Weiss, *J. Quant. Spectrosc. Radiat. Transfer* 18, 481 (1977).  
<sup>3</sup>P. F. Grunzev and A. I. Sherstyuk, *Opt. Spectrosc. (USSR)* 46, 353 (1979).  
<sup>4</sup>Y.-K. Kim and J.-P. Desclaux, Argonne National Laboratory Report ANL-76-88, Part I (1976).  
<sup>5</sup>E. Biemont, *Astron. Astrophys., Suppl. Ser.* 31, 285 (1978).  
<sup>6</sup>Y.-K. Kim and K.-T. Cheng, *J. Opt. Soc. Am.* 68, 836 (1978).

## Cr XIV: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $gf$	Accuracy	Source
1.	3s-3p	$^3S - ^3P$	296.94	0	251930	2	6	60.5	0.429	1.12	-0.067	B	1
			389.81	0	256540	2	4	64.1	0.292	0.750	-0.233	B	1
			411.99	0	242720	2	2	53.7	0.137	0.371	-0.563	B	1
2.	3s-4p	$^3S - ^3P$	62.395	0	1577410	2	6	1090	0.197	0.6823	-0.404	C+	interp.
			63.324	0	1579180	2	4	1070	0.129	0.6537	-0.589	C+	interp.
			63.539	0	1573860	2	2	1130	0.0684	0.0286	-0.864	C+	interp.
3.	3s-5p	$^3S - ^3P$	46.488	0	2151100	2	6	660	0.064	0.020	-0.89	C	5
			46.468	0	2152000	2	4	660	0.042	0.013	-1.07	C	ls
			46.527	0	2149300	2	2	670	0.022	0.0067	-1.36	C	ls
4.	3s-6p	$^3S - ^3P$	40.788	0	2451700	2	6	390	0.0292	0.0078	-1.234	C	5
			40.782	0	2452100	2	4	390	0.019	0.0052	-1.41	C	ls
			40.800	0	2451000	2	2	390	0.0097	0.0026	-1.71	D	ls
5.	3s-7p	$^3S - ^3P$	38.036	0	2629100	2	6	247	0.0161	0.00403	-1.492	C	5
6.	3s-8p	$^3S - ^3P$	36.466	0	2742300	2	6	167	0.0100	0.00240	-1.70	C	5
7.	3p-3d	$^3P - ^3D$	296.77	251930	589890	6	10	146	0.321	1.88	0.284	B	1
			300.271	256540	589570	4	6	141	0.286	1.13	0.058	B	1
			289.735	242720	587860	2	4	131	0.329	0.627	-0.182	B	1
			301.814	256540	587860	4	4	23.0	0.0315	0.125	-0.900	B	1
8.	3p-4s	$^3P - ^3S$	81.526	251930	1478500	6	2	2000	0.066	0.11	-0.40	C	5
9.	3p-4d	$^3P - ^3D$	69.008	251930	1701000	6	10	2340	0.278	0.279	0.222	C	5
			69.213	256540	1701300	4	6	2310	0.249	0.227	-0.002	C	ls
			68.594	242720	1700600	2	4	1980	0.279	0.126	-0.253	C	ls
			69.247	256540	1700600	4	4	280	0.027	0.025	-0.96	D	ls
10.	3p-5s	$^3P - ^3S$	54.028	251930	2102800	6	2	880	0.0129	0.0138	-1.111	C	5
			54.164	256540	2102800	4	2	590	0.013	0.0092	-1.29	C	ls
			53.760	242720	2102800	2	2	300	0.0130	0.00460	-1.59	C	ls
11.	3p-5d	$^3P - ^3D$	51.054	251930	2210600	6	10	1400	0.091	0.092	-0.26	C	5
			51.172	256540	2210700	4	6	1400	0.062	0.055	-0.49	C	ls
			50.821	242720	2210400	2	4	1200	0.093	0.031	-0.73	C	ls
			[51.180]	256540	2210400	4	4	230	0.0091	0.0061	-1.44	D	ls



## Cr IV: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ ( $\text{cm}^{-1}$ )	$E_2$ ( $\text{cm}^{-1}$ )	$g_1$	$g_2$	$A_{ul}$ ( $10^6 \text{ s}^{-1}$ )	$f_{ul}$	$S$ (at. u.)	$\log gf$	Accuracy	Source
12.	3p-6s	$^3P - ^3S$	46.030	251930	2424000	6	2	470	0.0050	0.0045	-1.52	D	5
			46.125	256500	2424000	4	2	310	0.0049	0.0000	-1.70	D	Is
			45.895	242720	2424000	2	2	100	0.0050	0.0015	-2.00	D	Is
13.	3p-6d	$^3P - ^3D$	44.779	251930	2485100	6	10	800	0.0421	0.0072	-0.60	C	5
			44.800	256500	2485200	4	6	330	0.0077	0.0223	-0.82	C	Is
			44.507	242720	2485000	2	4	710	0.0422	0.0124	-1.073	C	Is
			[44.873]	256500	2485000	4	4	140	0.0042	0.0025	-1.77	D	Is
14.	3p-7s	$^3P - ^3S$	42.371	251930	2612000	6	2	290	0.0036	0.0022	-1.81	D	5
			42.453	256500	2612000	4	2	200	0.0027	0.0015	-1.97	D	Is
			[42.207]	242720	2612000	2	2	98	0.0026	7.3(-4)	-2.23	D	Is
15.	3p-7d	$^3P - ^3D$	41.712	251930	2649300	6	10	540	0.0233	0.0192	-0.85	C	5
			41.708	256500	2649500	4	6	530	0.0200	0.0115	-1.078	C	Is
			41.556	242720	2649100	2	4	450	0.023	0.0064	-1.33	C	Is
			[41.795]	256500	2649100	4	4	90	0.0024	0.0013	-2.02	D	Is
16.	3p-8s	$^3P - ^3S$				6	2		0.0015		-2.05	D	5
17.	3p-8d	$^3P - ^3D$	39.844	251930	2755400	6	10	361	0.0144	0.0114	-1.063	C	5
			40.818	256500	2755000	4	6	300	0.013	0.0068	-1.29	C	Is
			39.796	242720	2755500	2	4	305	0.0145	0.0000	-1.54	C	Is
			[40.916]	256500	2755500	4	4	60	0.0014	7.8(-4)	-2.24	D	Is
18.	3d-4p	$^3D - ^3P$	101.16	588890	1577410	1 <sup>o</sup>	6	435	0.0446	0.149	-0.351	C	5
			101.05	589570	1579100	6	4	440	0.045	0.009	-0.57	C	Is
			101.42	587860	1573000	4	2	433	0.0372	0.0497	-0.83	C	Is
			[100.88]	587860	1579100	4	4	49	0.0075	0.0009	-1.53	D	Is
19.	3d-4f	$^3D - ^3F$	86.125	588890	1750000	10	14	5000	0.92	2.6	0.96	C	5
			86.169	589570	1750100	6	8	5000	0.88	1.5	0.72	C	Is
			86.060	587860	1749900	4	6	5300	0.88	1.9	0.55	C	Is
			[86.185]	589570	1749900	6	6	390	0.043	0.074	-0.58	D	Is
20.	3d-5p	$^3D - ^3P$	64.012	588890	2151100	10	6	190	0.0070	0.015	-1.15	D	5
			64.005	589570	2152000	6	4	170	0.0071	0.0090	-1.37	D	Is
			[64.045]	587860	2149200	4	2	190	0.0069	0.0050	-1.62	D	Is
			[63.925]	587860	2152000	4	4	19	0.0012	0.0010	-2.32	E	Is
21.	3d-5f	$^3D - ^3F$	60.731	588890	2235500	10	14	2200	0.170	0.240	0.220	C	5
			60.756	589570	2235600	6	8	2190	0.162	0.194	-0.013	C	Is
			60.609	587860	2235400	4	6	2050	0.170	0.126	-0.167	C	Is
			[60.761]	589570	2235400	6	6	150	0.0081	0.0097	-1.21	D	Is
22.	3d-6p	$^3D - ^3P$	53.633	588890	2451700	10	6	96	0.0025	0.0044	-1.60	D	5
			[53.691]	589570	2452100	6	4	85	0.0025	0.0026	-1.83	D	Is
			[53.674]	587860	2451000	4	2	98	0.0021	0.0015	-2.07	D	Is
			[53.642]	587860	2452100	4	4	9.5	4.1(-4)	2.9(-4)	-2.78	E	Is

CR XIV: Allowed transitions — Continued

No.	Transition	Multiplet	$\lambda$ (Å)	$E_2$ (cm <sup>-1</sup> )	$E_1$ (cm <sup>-1</sup> )	$f_{ul}$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{lu}$	$S$ (a. u.)	$\log g^F$	Accy	Source
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23	3d-6f	D - F	52365	588390	269380	10 14	1100	0.063	0.11	-0.20	C	5
			52363	589570	269380	6 8	1100	0.061	0.063	-0.44	C	4
			52321	587860	269380	4 6	1000	0.064	0.064	-0.50	C	4
			[52367]	589570	269380	6 6	73	0.000	0.000	-1.75	D	4
24	3d-7p	D - F	49015	588390	262910	10 6	56	0.0012	0.0019	-1.92	D	5
			[49022]	589570	262910	6 4	47	0.0011	0.0011	-2.17	D	4
			[48991]	587860	262910	4 2	54	9.8(-4)	6.3(-4)	-2.41	E	4
			[48991]	587860	262910	4 4	5.6	2.0(-4)	1.3(-4)	-3.09	E	4
25	3d-7f	D - F	44321	588390	265440	10 14	640	0.0312	0.0496	-0.51	C	5
			48338	589570	265440	6 8	630	0.0296	0.0283	-0.75	C	4
			48300	587860	265380	4 6	500	0.0311	0.0198	-0.90	C	4
			[48340]	589570	265380	6 6	42	0.0015	0.0014	-2.06	D	4
26	3d-8p	D - F	46430	588390	274230	10 6	36	7.0(-4)	0.0011	-2.15	E	5
			[46453]	589570	274230	6 4	33	7.2(-4)	6.6(-4)	-2.36	E	4
			[46417]	587860	274230	4 2	37	6.1(-4)	3.7(-4)	-2.62	E	4
			[46417]	587860	274230	4 4	3.7	1.2(-4)	7.2(-5)	-3.32	E	4
27	3d-8f	D - F				10 14		0.0180		-0.74	C	5
28	4s-4p	S - F				2 6		0.60		0.08	C	5
29	4s-5p	S - F	1687	1478500	2151100	2 6	217	0.216	0.211	-0.265	C	5
			[1485]	1478500	2152000	2 4	218	0.144	0.141	-0.54	C	4
			[1491]	1478500	2149300	2 2	210	0.071	0.070	-0.85	C	4
30	4s-6p	S - F	1028	1478500	2451700	2 6	150	0.070	0.047	-0.85	C	5
			[1027]	1478500	2452100	2 4	140	0.046	0.031	-1.04	C	4
			[1028]	1478500	2451000	2 2	150	0.024	0.016	-1.33	C	4
31	4s-7p	S - F	[86911]	1478500	2629100	2 6	96	0.0327	0.0187	-1.184	C	5
32	4s-8p	S - F	[79126]	1478500	2742300	2 6	66	0.0185	0.0096	-1.432	C	5
33	4p-4d	P - D	8091	1577410	1701000	6 10	29	0.47	1.5	0.45	C	3
			[8190]	1579180	1701300	4 6	24	0.42	4.5	0.23	C	3
			[7931]	1573860	1700600	2 4	26	0.40	2.5	-0.02	C	3
			[8237]	1579180	1700600	4 4	4.5	0.046	0.50	-0.74	C	3
34	4p-5s	P - S	1903	1577410	2102800	6 2	620	0.113	0.425	-0.169	C	5
			[1910]	1579180	2102800	4 2	411	0.113	0.283	-0.347	C	4
			[1911]	1573860	2102800	2 2	213	0.114	0.142	-0.64	C	4
35	4p-5d	P - D	1529	1577410	2710600	6 10	379	0.276	0.74	0.151	C	5
			[1584]	1579180	2710700	4 6	370	0.21	0.44	-0.07	C	4
			[1571]	1573860	2710400	2 4	330	0.24	0.25	0.32	C	4
			[1584]	1579180	2710400	4 4	62	0.023	0.049	1.03	D	4
36	4p-6s	P - S	1181	1577410	2424400	6 2	316	0.0220	0.051	0.088	C	5
			[1183]	1579180	2424400	4 2	210	0.022	0.034	1.06	C	4
			[1176]	1573860	2424400	2 2	110	0.022	0.017	1.36	C	4

Cr XIV: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{os}$	$S$ (at. u.)	$\log g_{os}^{-1}$	Accuracy	Source
37.	4p-6d	<sup>2</sup> P - <sup>2</sup> D	110.2	1577410	2445100	6	10	270	0.003	0.18	-0.30	C	5
			[110.4]	1579180	2405300	4	6	200	0.076	0.11	-0.52	C	h
			[100.8]	1573000	2405000	2	4	230	0.003	0.000	-0.70	C	h
			[110.4]	1579180	2405000	4	4	45	0.0003	0.012	-1.05	D	h
38.	4p-7s	<sup>2</sup> P - <sup>2</sup> S	96.656	1577410	2612000	6	2	180	0.0006	0.016	-1.29	D	5
			[96.824]	1579180	2612000	4	2	120	0.0006	0.011	-1.05	D	h
			[96.330]	1573000	2612000	2	2	60	0.0004	0.0003	-1.70	D	h
39.	4p-7d	<sup>2</sup> P - <sup>2</sup> D	92.292	1577410	2635300	6	10	185	0.0002	0.074	-0.62	C	5
			[92.432]	1579180	2600500	4	6	180	0.006	0.044	-0.84	C	h
			[92.006]	1573000	2609100	2	4	160	0.041	0.025	-1.00	C	h
			[92.067]	1579180	2609100	4	4	30	0.0040	0.0009	-1.90	D	h
40.	4p-8s	<sup>2</sup> P - <sup>2</sup> S				6	2		0.0044		-1.50	D	5
41.	4p-8d	<sup>2</sup> P - <sup>2</sup> D	84.890	1577410	2755400	6	10	128	0.0230	0.0006	-0.95	C	5
			[85.020]	1579180	2756400	4	6	127	0.0207	0.0232	-1.002	C	h
			[84.631]	1573000	2755600	2	4	100	0.0232	0.0129	-1.334	C	h
			[85.012]	1579180	2756600	4	4	21	0.0023	0.0026	-2.03	D	h
42.	4d-4f	<sup>2</sup> D - <sup>2</sup> F				10	14		0.122		0.006	C	5
43.	4d-5p	<sup>2</sup> D - <sup>2</sup> P	222.2	1701000	2151100	10	6	220	0.009	0.72	-0.00	C	5
			[221.9]	1701300	2152000	6	4	200	0.008	0.43	-0.23	C	h
			[222.9]	1700600	2149300	4	2	220	0.002	0.24	-0.49	C	h
			[221.5]	1700000	2152000	4	4	22	0.016	0.008	-1.18	D	h
44.	4d-5f	<sup>2</sup> D - <sup>2</sup> F	187.1	1701000	2235500	10	14	970	0.71	4.4	0.05	C	5
			187.30	1701300	2235600	6	8	900	0.68	2.5	0.61	C	h
			187.02	1700600	2235400	4	6	930	0.73	1.8	0.47	C	h
			[187.2]	1701300	2236400	6	6	67	0.035	0.13	-0.68	D	h
45.	4d-6p	<sup>2</sup> D - <sup>2</sup> P	132.2	1701000	2451700	10	6	103	0.0165	0.072	-0.78	C	5
			[132.2]	1701300	2452100	6	4	92	0.016	0.043	-1.01	C	h
			[132.3]	1700600	2451000	4	2	100	0.014	0.024	-1.26	C	h
			[132.1]	1700000	2452100	4	4	10	0.0027	0.0008	-1.95	D	h
46.	4d-6f	<sup>2</sup> D - <sup>2</sup> F	125.3	1701000	2499300	10	14	540	0.178	0.73	0.250	C	5
			[125.3]	1701300	2499000	6	8	540	0.17	0.42	0.01	C	h
			[125.2]	1700600	2499200	4	6	500	0.18	0.29	-0.15	C	h
			[125.3]	1701300	2499200	6	6	36	0.0006	0.021	-1.29	D	h
47.	4d-7p	<sup>2</sup> D - <sup>2</sup> P	107.7	1701000	2629100	10	6	58	0.0060	0.021	-1.22	D	5
			[107.8]	1701300	2629100	6	4	58	0.0061	0.013	-1.44	D	h
			[107.7]	1700600	2629100	4	2	57	0.0049	0.0070	-1.70	D	h
			[107.7]	1700600	2629100	4	4	5.7	9.3(-4)	0.0014	-2.40	E	h
48.	4d-7f	<sup>2</sup> D - <sup>2</sup> F	104.4	1701000	2668400	10	14	320	0.074	0.26	-0.13	C	5
			[104.5]	1701300	2668400	6	8	310	0.068	0.14	-0.30	C	h
			[104.4]	1700600	2668300	4	6	300	0.073	0.10	-0.54	C	h
			[104.5]	1701300	2668300	6	6	21	0.0034	0.0071	-1.00	D	h

## Cr XIV: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$K$ ( $\text{cm}^{-1}$ )	$K_2$ ( $\text{cm}^{-1}$ )	$g_1$	$g_2$	$A_{21}$ ( $10^6 \text{ s}^{-1}$ )	$f_{12}$	$S$ (wt. u.)	$\log gf$	Accuracy	Source
49.	4d-3p	D - P	96.025	1701000	2742300	10	6	35	0.0000	0.0005	-1.52	D	5
			[96.061]	1701300	2742300	6	4	33	0.0000	0.0057	-1.74	D	Is
			[96.997]	1700000	2742300	4	2	37	0.0025	0.0032	-1.99	D	Is
			[96.997]	1700000	2742300	4	4	3.6	5.0(-4)	6.3(-4)	-2.70	E	Is
50.	4d-3f	D - F				10	14		0.0000		-0.410	C	5
51.	4f-5d	F - D	217.1	1750000	2210000	14	10	30.8	0.0201	0.201	-0.55	C	5
			[217.1]	1750100	2210700	8	6	38.0	0.0201	0.115	-0.79	C	Is
			[217.2]	1749000	2210000	6	4	40	0.019	0.000	-0.95	C	Is
			[217.0]	1749000	2210700	6	6	1.9	0.0013	0.0057	-2.10	D	Is
52.	4f-6d	F - D	[136.0]	1750000	245100	14	10	17	0.0004	0.021	-1.32	D	5
53.	4f-7d	F - D	[111.2]	1750000	2643000	14	10	9.1	0.0012	0.0062	-1.77	D	5
54.	4f-8d	F - D	99.463	1750000	2755400	14	10	5.4	5.7(-4)	0.0026	-2.10	E	5
			[99.473]	1750100	2755000	8	6	5.1	5.7(-4)	0.0015	-2.34	E	Is
			[99.443]	1749000	2755500	6	4	5.2	5.1(-4)	0.0010	-2.52	E	Is
			[99.453]	1749000	2755000	6	6	0.25	3.0(-5)	7.4(-5)	-3.65	E	Is
55.	5s-5p	S - P				2	6		0.78		0.19	C	5
56.	5s-6p	S - P	206.6	2102000	2451700	2	6	63	0.233	0.440	-0.332	C	5
			[206.3]	2102000	2452100	2	4	63	0.155	0.293	-0.51	C	Is
			[207.2]	2102000	2451000	2	2	63	0.078	0.147	-0.81	C	Is
57.	5s-7p	S - P	[190.0]	2102000	2629100	2	6	47	0.076	0.095	-0.82	C	5
58.	5s-8p	S - P	[156.4]	2102000	2742300	2	6	32.7	0.0360	0.0371	-1.143	C	5
59.	5p-5d	P - D				6	10		0.67		0.60	C	5
60.	5p-6s	P - S	365.9	2151100	2424400	6	2	241	0.161	1.16	-0.015	C	5
			[367.1]	2152000	2424400	4	2	160	0.16	0.77	-0.20	C	Is
			[363.5]	2149200	2424400	2	2	82	0.162	0.387	-0.690	C	Is
61.	5p-6d	P - D	299.4	2151100	2485100	6	10	98	0.219	1.30	0.119	C	5
			[300.1]	2152000	2485200	4	6	97	0.20	0.78	-0.10	C	Is
			[297.9]	2149200	2485000	2	4	83	0.221	0.433	-0.255	C	Is
			[300.3]	2152000	2485000	4	4	16	0.022	0.087	-1.06	D	Is
62.	5p-7s	P - S	217.0	2151100	2612000	6	2	133	0.0313	0.134	-0.73	C	5
			[217.4]	2152000	2612000	4	2	88	0.031	0.089	-0.91	C	Is
			[216.1]	2149200	2612000	2	2	44.9	0.0314	0.0447	-1.202	C	Is
63.	5p-7d	P - D	300.7	2151100	2649300	6	10	78	0.079	0.31	-0.32	C	5
			[201.0]	2152000	2649500	4	6	79	0.072	0.19	-0.54	C	Is
			[200.1]	2149200	2649100	2	4	63	0.076	0.10	-0.82	C	Is
			[201.2]	2152000	2649100	4	4	13	0.0079	0.021	-1.50	D	Is
64.	5p-8s	P - S				6	2		0.0123		-1.132	C	5

Cr XIV: Allowed transitions - Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	S (at. u.)	log $gf$	Accuracy	Source
65.	5p-8d	<sup>7</sup> F - <sup>7</sup> D	165.5	2151700	2755400	6	10	57	0.0002	0.128	-0.63	C	5
			[165.7]	2153000	2755400	4	6	57	0.005	0.077	-0.85	C	h
			[165.6]	2149300	2755500	2	4	48.1	0.0003	0.0427	-1.105	C	h
			[165.7]	2153000	2755500	4	4	9.5	0.0000	0.0005	-1.81	D	h
66.	5d-5f	<sup>7</sup> D - <sup>7</sup> F				10	14		0.214		0.230	C	5
67.	5d-6p	<sup>7</sup> D - <sup>7</sup> F	414.8	2210000	2451700	10	6	101	0.157	2.14	0.196	C	5
			[414.3]	2210700	2452100	6	4	91	0.156	1.28	-0.020	C	h
			[415.6]	2210400	2451000	4	2	100	0.13	0.71	-0.25	C	h
			[413.7]	2210400	2452100	4	4	10	0.025	0.14	-0.90	D	h
68.	5d-6f	<sup>7</sup> D - <sup>7</sup> F	344.4	2210000	2493300	10	14	250	0.63	7.2	0.80	C	5
			[344.5]	2210700	2490000	6	8	250	0.60	4.1	0.65	C	h
			[345.3]	2210400	2493300	4	6	240	0.64	2.9	0.41	C	h
			[345.6]	2210700	2490200	6	6	17	0.051	0.21	-0.74	D	h
69.	5d-7p	<sup>7</sup> D - <sup>7</sup> F	231.9	2210000	2629100	10	6	52	0.0200	0.212	-0.57	C	5
			[230.9]	2210700	2629100	6	4	47.1	0.0200	0.127	-0.79	C	h
			[230.8]	2210400	2629100	4	2	53	0.023	0.071	-1.04	C	h
			[230.8]	2210400	2629100	4	4	5.2	0.0045	0.014	-1.75	D	h
70.	5d-7f	<sup>7</sup> D - <sup>7</sup> F	222.3	2210000	2654400	10	14	165	0.174	1.28	0.241	C	5
			[223.4]	2210700	2650400	6	8	170	0.17	0.73	-0.00	C	h
			[223.3]	2210400	2653300	4	6	150	0.17	0.51	-0.16	C	h
			[223.4]	2210700	2653300	6	6	11	0.0004	0.007	-1.30	D	h
71.	5d-8p	<sup>7</sup> D - <sup>7</sup> F	182.1	2210000	2742300	10	6	31.4	0.0100	0.062	-1.000	C	5
			[183.1]	2210700	2742300	6	4	28	0.010	0.007	-1.22	C	h
			[183.0]	2210400	2742300	4	2	32	0.0005	0.021	-1.47	D	h
			[183.0]	2210400	2742300	4	4	3.1	0.0017	0.0041	-2.18	D	h
72.	5d-8f	<sup>7</sup> D - <sup>7</sup> F				10	14		0.077		-0.11	C	5
73.	5f-6d	<sup>7</sup> F - <sup>7</sup> D	400.6	2235500	2485100	14	10	28.4	0.0488	0.90	-0.165	C	5
			[400.5]	2235500	2485200	8	6	27	0.048	0.51	-0.41	C	h
			[400.6]	2235400	2485000	6	4	28	0.045	0.35	-0.56	C	h
			[400.3]	2235400	2485200	6	6	1.4	0.0033	0.026	-1.70	D	h
74.	5f-7d	<sup>7</sup> F - <sup>7</sup> D	241.7	2235500	2649300	14	10	14	0.0006	0.006	-0.92	D	5
			[241.5]	2235500	2649500	8	6	13	0.0006	0.055	-1.16	D	h
			[241.7]	2235400	2649100	6	4	14	0.0000	0.038	-1.32	D	h
			[241.5]	2235400	2649500	6	6	0.65		5.7(-4)	0.0027	-2.47	E
75.	5f-8d	<sup>7</sup> F - <sup>7</sup> D	[192.3]	2235500	2755470	14	10	7.8	0.0031	0.027	-1.36	D	5

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XIV

## Forbidden Transitions

The electric quadrupole  $gf$ -value for the  $3s-3d$  multiplet in this sodiumlike ion was reported by Godefroid *et al.*;<sup>1</sup> it was calculated earlier by Biemont and Godefroid<sup>2</sup> using a fully variational Hartree-Fock approach. This  $f$ -value was converted to a multiplet strength, which was then distributed between the two lines of the multiplet according to  $LS$ -coupling rules.

## References

- <sup>1</sup>M. Godefroid, C. E. Magnusson, P. O. Zetterberg, and I. Joëlsson, *Phys. Scr.* **32**, 125 (1985).  
<sup>2</sup>E. Biemont and M. Godefroid, *Phys. Scr.* **18**, 323 (1978).

Cr XIV: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{if}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$3s-3d$	$^3S-^3D$	[169.62] [170.11]	0 0	589570 587860	2 2	6 4	E2 E2	$5.5(+5)^*$ $5.5(+5)$	0.277 0.185	C C	1, <sup>a</sup> 1, <sup>a</sup>

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XV

## Ne Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^6 ^1S_0$

Ionization Energy:  $1010.6 \text{ eV} = 8151000 \text{ cm}^{-1}$

## Allowed Transitions

List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
18.497	9	102	3	293	13	327	14
18.782	8	102.18	1	304	13	405.127	11
19.015	7	103	3	309	13	417	16
20.863	6	105	4	321.262	15	469	10
21.153	5	111.27	2	324	17	703	12

For resonance transitions to  $J = 1$  levels of the  $2p^3 3s$  and  $2p^3 3d$  configurations, we quote  $A$ -values which were calculated by Vainshtein and Safronova<sup>1</sup> using a charge-expansion perturbation theory approach with allowance for mixing of the  $2p^3 3s$ ,  $2p^3 3d$ , and  $2s 2p^3 3p$  configurations. Their results for the  $2p^3-2p^3 3d$  transitions in the isoelectronic ions Ar IX and Fe XVII are in rather good agreement with those of Shorer,<sup>2</sup> who used the relativistic random phase approximation (RRPA) with allowance for mixing between configurations of type  $2p^3 ns$  and  $2p^3 nd$ , as well as correlation effects due to configurations having a vacancy in the  $1s$  or  $2s$  subshell.

But the data of Ref. 1 for the two  $2p^3-2p^3 3s$  transitions are approximately a factor of two smaller than those of Shorer for the abovementioned neon-like species, so we have increased the transition probabilities of Ref. 1 for these two lines by a factor of two.

$A$ -values quoted here for a number of transitions involving an electron jump of the type  $2s-2p$ ,  $3s-3p$ , or  $3p-3d$  were taken from the work of Pokleba and Safronova,<sup>1</sup> who used wavefunctions calculated by a charge-expansion perturbation theory approach with allowance for mixing of configurations in which a single  $2s$  or  $2p$  electron is excited to an  $n = 3$  orbital but with no

inclusion of configurations in which an electron occupies the  $n=4$  shell. In cases where better wavelength data were available, these transition probabilities were first converted to line strengths, which were then reconverted to  $f$ - and  $A$ -values by using the more accurate wavelengths. Transitions involving levels of the  $2p^33p$  and  $2p^33d$  configurations which are indicated by Fawcett<sup>4</sup> (in Ti XII) or by Jupen and Litzen<sup>5</sup> (in Ti XII or Fe XVII) to be of low to moderate purity in  $LS$  coupling are excluded here, as are very weak lines. The pattern of levels within the  $2s2p^33d$  configuration in the isoelectronic ions Fe XVII and Ni XIX resulting from the scaled Thomas-Fermi calculations of Loulergue and Nussbaumer<sup>6</sup> with extensive allowance for correlation is entirely different from that determined by Vainshtein and

Safronova, whose energy levels were apparently used by Pokleba and Safronova in their transition probability calculations. We have thus excluded transitions out of these levels from our tabulation.

References

<sup>1</sup>L. A. Vainshtein and U. I. Safronova, *Spektralno-picheskije Konstanty Atomov*, 5-122 (Ed. V. B. Belyasin, Akad. Nauk SSSR, Ot. Ob. Fiz. Astron., Nauch. Sov. Spektrosk., Moscow, 1977).  
<sup>2</sup>P. Shore, *Phys. Rev. A* 20, 642 (1979).  
<sup>3</sup>A. K. Pokleba and U. I. Safronova, Preprint No. 11, Akad. Nauk SSSR, Ot. Ob. Fiz. Astron., Inst. Spektrosk. (Moscow, 1981).  
<sup>4</sup>B. C. Fawcett, private communication, as quoted in E. Träbert, *Z. Phys. A* 319, 25 (1984).  
<sup>5</sup>C. Jupen and U. Litzen, *Phys. Scr.* 30, 112 (1984).  
<sup>6</sup>M. Loulergue and H. Nussbaumer, *Astron. Astrophys.* 65, 125 (1975).

Cr XV: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{os}$	$S$ (at. u.)	log $gf$	Accuracy	Source
1.	$2s^22p^4(^4P_{1,2})3s - 2s2p^43s$	$(^1/2, ^1/2)^o - ^3S$	102.18	4713200	5691900	5	3	700	0.065	0.11	-0.69	D	3
2.	$2s^22p^4(^4P_{1,2})3s - 2s2p^43s$	$(^1/2, ^1/2)^o - ^3S$	111.27	4793200	5691900	3	3	170	0.021	0.034	-1.03	D	3
3.	$2s^22p^43p - 2s2p^43p$	$^3S - ^3P$	[102] [103]			3	3	160	0.025	0.025	-1.13	E	3
						3	1	380	0.020	0.020	-1.22	D	3
4.		$^3D - ^3P$	[105]			7	5	530	0.063	0.15	-0.36	D	3
5.	$2p^4 - 2p^4(^4P_{1,2})3s$	$^1S - (^1/2, ^1/2)^o$	21.153	0	4727500	1	3	5600	0.11	0.0078	-0.95	C-	1a
6.	$2p^4 - 2p^4(^4P_{1,2})3s$	$^1S - (^1/2, ^1/2)^o$	20.863	0	4793200	1	3	6000	0.12	0.0061	-0.93	C-	1a
7.	$2p^4 - 2p^43d$	$^1S - ^3P$	19.015	0	5259000	1	3	630	0.010	6.4(-4)	-1.99	E	1
8.		$^3S - ^3D$	18.782	0	5924200	1	3	2.8(+4)	0.44	0.02;	-0.35	D	1
9.		$^1S - ^1P$	18.497	0	5406300	1	3	1.62(+5)	2.49	0.152	0.397	C-	1
10.	$2p^4(^4P_{1,2})3s - 2p^43p$	$(^1/2, ^1/2)^o - ^3S$	[400]			5	3	25	0.049	0.28	-0.61	D	3

Cr xv: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accuracy	Source
11.		$(^1S_{1/2})^2 - ^3D$	405.127	4713200	4960000	5	7	44	0.15	1.0	-0.13	D	3
12.	$2p^4(^3P_1, ^3S_0) - 2p^33p$	$(^1S_{1/2})^2 - ^3S$	[703]			1	3	0.19	0.0042	0.0098	-2.37	E	3
13.	$2p^33p - 2p^33d$	$^3S - ^3P$	298			3	9	56	0.22	0.66	-0.17	E	3
			[293]			3	5	42	0.090	0.26	-0.57	E	3
			[304]			3	3	67	0.093	0.28	-0.56	D	3
			[309]			3	1	79	0.038	0.12	-0.95	D	3
14.		$^3D - ^3P$	[327]			7	5	3.5	0.0040	0.030	-1.55	E	3
15.		$^3D - ^3P$	321.262	4960000	5271300	7	9	81	0.16	1.2	0.05	D	3
16.		$^3P - ^3P$	[417]			1	3	1.7	0.013	0.018	-1.88	D-	3
17.		$^3P - D^*$	[324]			1	3	39	0.18	0.20	-0.73	D	3

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Cr xv

Forbidden Transitions

The  $A$ -value for the single transition tabulated here is the result of the Hartree-Fock-Relativistic (HFR) calculations of Cowan.<sup>1</sup> The wavelength is the result of these same calculations and may be somewhat uncertain, as the energy of the  $J = 0$  level has not been determined experimentally.

Reference

<sup>1</sup>R. D. Cowan, Los Alamos Scientific Laboratory Informal Report LA-6679-MS (Jan. 1977).

Cr xv: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{21}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$2p^4(^3P_1, ^3S_0) - 2p^3(^3P_1, ^3S_0)$	$(^1S_{1/2})^2 - (^1S_{1/2})^2$	[1710]			3	1	M1	5200	0.96	D+	1



## Cr XVI

## F Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^5 \ ^2P_{1/2}$ Ionization Energy:  $1097 \text{ eV} = 8850000 \text{ cm}^{-1}$ 

## Allowed Transitions

Oscillator strengths for lines of the multiplet  $2s^2 2p^5 \ ^2P - 2s 2p^6 \ ^2S$  are the results of the Dirac-Fock calculations of Cheng *et al.*,<sup>1</sup> which included a perturbative treatment of the Breit interaction and the Lamb shift.

For lines of the arrays  $2p^5 - 2p^4 3s$  and  $2p^5 - 2p^4 3d$ , we quote the  $f$ -values calculated by Fawcett<sup>2</sup> using Cowan's Hartree-Fock-Relativistic (HFR) method and incorporating scaling of energy parameters on the basis of a least-squares fit to observed energies. Fawcett's calculations included fairly extensive allowance for configuration mixing in both odd- and even-parity states. Transitions involving levels which are indicated by Fawcett to be of low to moderate purity in  $LS$  coupling in neighboring fluorinelike ions are excluded from this

compilation, as are lines characterized by very small  $f$ -values.

The ratio of  $A$ -values for the two resonance lines out of the  $2s 2p^6 \ ^2S_{1/2}$  level as given in Ref. 1 is in reasonably good agreement with the result of Stratton *et al.*<sup>3</sup> derived from relative-intensity measurements.

## References

- <sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* 24, 111 (1979).  
<sup>2</sup>B. C. Fawcett, *At. Data Nucl. Data Tables* 31, 493 (1984).  
<sup>3</sup>B. C. Stratton, H. W. Moos, S. Sechewer, U. Feldman, J. F. Seely, and A. K. Bhatia, *Phys. Rev. A* 31, 2534 (1985).

Cr XVI: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{os}$	$S$ (at. u.)	log $gf$	Accuracy	Source
1.	$2s^2 2p^5 - 2s 2p^6$	$^2P - ^2S$	109.38	23631	937910	6	2	1060	0.0625	0.135	-0.425	C+	1
			106.62	0	937910	4	2	758	0.0646	0.0907	-0.588	C+	1
			115.33	70892	937910	2	2	295	0.0589	0.0447	-0.929	C+	1
2.	$2p^5 - 2p^4 3s$	$^2P - ^4P$	19.807	0	5048700	4	6	43C	0.0038	9.9(-4) <sup>a</sup>	-1.82	E	2
			3.	$^2P - ^2P$	19.714	70892	5143500	2	2	1.1(+4)	0.064	0.0083	-0.89
	19.442	0	5143500		4	2	9900	0.028	0.0072	-0.95	D	2	
4.	$2p^5 - 2p^4 3d$	$^2P - ^3D$	19.255	0	5198500	4	6	7700	0.064	0.016	-0.59	D	2
			19.511	70892	5196200	2	4	8800	0.10	0.013	-0.70	D	2
			5.	$2p^5 - 2p^4 3s$	18.868	23631	5323600	6	2	9200	0.016	0.0061	-1.01
18.775	0	5323600	4		2	2600	0.0068	0.0017	-1.57	E	2		
19.028	70892	5323600	2		2	6400	0.035	0.0044	-1.15	D	2		
6.	$2p^5 - 2p^4 3d$	$^2P - ^3S$	17.510	23631	5734600	6	2	1.2(+5)	0.19	0.066	0.06	D	2
			17.428	0	5734600	4	2	1.1(+5)	0.24	0.055	-0.02	D	2
			[17.656]	70892	5734600	2	2	2.0(+4)	0.094	0.011	-0.73	D	2

## Cr XVI: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $gf$	Accu- racy	Source
7.		$^3P^o - ^3P$	[17.372]	0	5756300	4	4	1.4(+5)	0.62	0.14	0.39	E	2
			17.587	70892	5756300	2	4	2.0(+4)	0.19	0.022	-0.42	E	2
8.		$^3P^o - ^3D$	17.514	70892	5780600	2	4	1.1(+5)	0.37	0.11	0.29	E	2
			[17.299]	0	5780600	4	4	2.5(+4)	0.11	0.025	-0.36	E	2
9.	$2p^3-2p^4^1S3d$	$^3P^o - ^3D$	17.126	23631	5862800	6	10	4.0(+4)	0.30	0.10	0.25	E	2
			17.073	0	5857200	4	6	1.2(+4)	0.077	0.017	-0.51	D	2
			17.242	70892	5870700	2	4	8.6(+4)	0.77	0.087	0.19	D	2
			[17.034]	0	5870700	4	4	930	0.0043	9.6(-4)	-1.76	E	2

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XVI

## Forbidden Transitions

Line strengths for the magnetic dipole and electric quadrupole contributions to the transition between the two levels of the  $2p^3$  configuration are the results of the Dirac-Fock calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. The strength of the electric quadrupole transition as defined in Ref. 1 was multiplied by the factor  $1/3$  which is needed to bring this

value into conformance with the definition of quadrupole strengths used in the NBS tables.

## Reference

<sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* 24, 111 (1979).

## Cr XVI: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accu- racy	Source
1.	$2p^3-2p^3$	$^3P^o - ^3P^o$	1410.60	0	70892	4	2	M1	6390	1.33	B	1
						4	2	E2	0.45	0.0020	D	1

## Cr xvii

## O Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^4 \ ^3P_2$ Ionization Energy: 1185 eV = 9560000  $\text{cm}^{-1}$ 

## Allowed Transitions

## List of tabulated lines

Wavelength ( $\text{\AA}$ )	No.	Wavelength ( $\text{\AA}$ )	No.	Wavelength ( $\text{\AA}$ )	No.	Wavelength ( $\text{\AA}$ )	No.
16.11	29	16.80	19	18.088	12	101.91	4
16.27	27	16.81	25	18.12	15	116.53	1
16.31	31	16.97	18,19	18.219	11	117.20	6
16.32	24	17.19	20	18.226	11	120.84	1
16.37	28	17.39	14	18.336	10,13	122.91	1
16.44	22,27	17.77	14	18.389	17	125.00	1
16.59	23	17.87	14	18.52	9	125.35	1
16.62	21	17.892	12	18.531	10	129.78	8
16.64	30	17.90	14	18.73	9	132.76	1
16.65	30	17.957	11	89.572	2	147.40	3
16.66	32	17.968	16	94.69	2	168.08	5
16.68	26	18.01	15	94.69	2		
16.78	21	18.020	11	97.20	7		

The tabulated oscillator strengths for transitions of the arrays  $2s^2 2p^4 - 2s 2p^5$  and  $2s 2p^5 - 2p^6$  are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the  $n=2$  complex. The results should be quite accurate, except in the case of weak lines. (The  $2s^2 2p^4 \ ^1D_2 - 2s 2p^5 \ ^3P_1$  transition has been omitted from this tabulation, because its  $f$ -value as reported in Ref. 1 is extremely small, and thus very uncertain.)

Transition probabilities for lines of the  $2s^2 2p^4 - 2s 2p^5$  array were calculated by Froese Fischer and Saha<sup>2</sup> using the multiconfiguration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their basis set included many configurations outside the  $n=2$  complex, but relativistic effects were not treated to the same degree as in Ref. 1. Line strengths derived from these two sources are in reasonably good agreement, particularly for the stronger transitions.

$A$ -values for lines of the  $2p^4 \ ^3P - 2p^5 \ (^3S) 3s \ ^3S$  multiplet are taken from the scaled Thomas-Fermi approach

of Kastner *et al.*<sup>3</sup> with configuration interaction and relativistic effects. For all other lines of the  $2p^4 - 2p^5 3s$  array, and for lines of the  $2p^4 - 2p^5 3d$  array, we quote the  $f$ -values calculated by Fawcett<sup>4</sup> using Cowan's Hartree-Fock-Relativistic (HFR) method and incorporating scaling of energy parameters on the basis of a least-squares fit to observed energies. Fawcett's calculations included fairly extensive allowance for configuration mixing in both odd- and even-parity states. The weakest lines were not reported, and thus are not tabulated here. Transitions involving levels which are indicated by Fawcett to be of low to moderate purity in  $LS$  coupling in neighboring oxygenlike ions are excluded from this compilation.

## References

- <sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Ducloux, *At. Data Nucl. Data Tables* **24**, 111 (1979).
- <sup>2</sup>C. Froese Fischer and H. P. Saha, *J. Phys. B* **17**, 943 (1984).
- <sup>3</sup>S. O. Kastner, A. K. Bhatia, and L. Cohen, *Phys. Scr.* **18**, 259 (1977).
- <sup>4</sup>B. C. Fawcett, *At. Data Nucl. Data Tables* **34**, 215 (1986).

## Cr xvii: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ ( $\text{cm}^{-1}$ )	$E_2$ ( $\text{cm}^{-1}$ )	$g_1$	$g_2$	$A_{ul}$ ( $10^6 \text{ s}^{-1}$ )	$f_{ul}$	$S$ (at. u.)	$\log gf$	Accuracy	Source
1.	$2s^2 2p^4 - 2s 2p^5$	$^3P - ^3P$	122.44	26590	236770	9	9	450	0.10	0.28	-0.83	C	1
			122.91	0	813680	5	5	330	0.074	0.15	-0.43	C	1
			125.25	60380	858150	3	3	100	0.0257	0.0318	-1.113	C	1
			116.53	0	858150	5	3	244	0.0298	0.057	-0.83	C	1
			129.84	60380	887320	3	1	450	0.0364	0.0434	-0.96	C	1
			132.76	60380	813680	3	5	93	0.0409	0.054	-0.91	C	1
			125.00	58150	858150	1	3	140	0.036	0.040	-1.02	C	1
2.	$^3P - ^1P$	[89.572]	0	1116420	5	3	85	0.0061	0.0090	-1.52	E	1	
		94.69	60380	1116420	3	3	4.5	6.5(-4)	6.1(-4)	-2.71	E	1	
		94.49	58150	1116420	1	3	9.5	0.0038	0.0012	-2.42	E	1	
3.	$^1D - ^3P$	147.40	135160	813680	5	5	14	0.0047	0.011	-1.63	E	1	
4.	$^1D - ^1P$	161.91	135160	1116420	5	3	1320	0.123	0.206	-0.211	C	1	
5.	$^1S - ^3P$	[168.06]	263180	858150	1	3	5.6	0.0064	0.0035	-2.19	E	1	
6.	$^1S - ^1P$	117.20	263180	1116420	1	3	96	0.059	0.023	-1.23	C	1	
7.	$2s 2p^4 - 2p^4$	$^3P - ^1S$	97.20	858150	1886950	3	1	59	0.0028	0.0027	-2.08	E	1
8.	$^1P - ^1S$	129.78	1116420	1886950	3	1	1400	0.118	0.151	-0.451	C	1	
9.	$2p^4 - 2p^4 ^4S^o 3s$	$^3P - ^1S$	[18.52]			5	5	160	8.2(-4)	2.5(-4)	-2.39	E	3
			[18.73]			3	5	12	1.1(-4)	1.9(-5)	-3.50	E	3
			18.426	26590	5453800	9	3	2.7(+4)	0.046	0.025	-0.38	C-	4
10.	$2p^4 - 2p^4 ^4S^o 3s$	$^1P - ^1S$	18.336	0	5453800	5	3	1.7(+4)	0.052	0.016	-0.59	C-	4
			18.531	60380	5453800	3	3	5800	0.030	0.0055	-1.05	C-	4
			18.531	58150	5453800	1	3	3200	0.050	0.0031	-1.30	C-	4
			17.957	0	5569900	5	7	7800	0.053	0.016	-0.58	C	4
11.	$2p^4 - 2p^4 ^4D^o 3s$	$^1P - ^1D$	18.219	60380	5549400	3	5	2000	0.017	0.0031	-1.29	D	4
			18.219	58150	5547000	1	3	1700	0.026	0.0016	-1.59	D	4
			18.020	0	5549400	5	5	6400	0.031	0.0092	-0.81	D	4
			[18.226]	60380	5547000	3	3	7000	0.035	0.0063	-0.98	D	4
			[17.892]	0	5569900	5	5	960	0.0046	0.0014	-1.64	E	4
12.	$^3P - ^1D$	[18.059]	60380	5569900	3	5	1700	0.014	0.0025	-1.38	E	4	
		18.336	135160	5569900	5	5	1.6(+4)	0.081	0.024	-0.39	D	4	

## Cr XVII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $g f$	Accuracy	Source
14.	$2p^4 - 2p^3(^3P)3s$	$^3P - ^3P$	[17.59]			5	5	1300	0.0060	0.0017	-1.52	D-	4
			[17.90]			3	1	7500	0.012	0.0021	-1.44	C	4
			[17.77]			3	5	4000	0.035	0.0061	-0.98	D	4
			[17.87]			1	3	4900	0.071	0.0042	-1.15	D	4
15.	$^1D - ^3P$	[18.01]			5	5	4300	0.021	0.0062	-0.96	E	4	
		[18.12]			5	3	2900	0.0086	0.0026	-1.37	E	4	
16.	$^1D - ^1P$		17.968	135160	5701200	5	3	8600	0.025	0.0074	-0.90	D	4
17.	$^1S - ^1P$		18.389	263180	5701200	1	3	9200	0.14	0.0065	-0.85	D	4
18.	$2p^4 - 2p^3(^3S)3d$	$^3P - ^1D$	[16.97]			5	5	1100	0.0046	0.0013	-1.64	E	4
19.	$2p^4 - 2p^3(^3S)3d$	$^3P - ^1D$	[16.80]			5	7	4.4(+4)	0.26	0.072	0.11	D	4
			[16.97]			1	3	2.6(+4)	0.341	0.0191	-0.467	C-	4
			[16.97]			3	3	1.5(+4)	0.066	0.011	-0.70	C-	4
			[16.80]			5	3	1800	0.0046	0.0013	-1.64	D	4
20.	$^1D - ^1D$	[17.19]			5	7	680	0.0042	0.0012	-1.68	E	4	
21.	$2p^4 - 2p^3(^1D)3d$	$^3P - ^3P$	[16.78]			3	5	2600	0.025	0.0041	-1.12	E	4
			[16.62]			5	5	5600	0.023	0.0063	-0.94	E	4
22.	$2p^4 - 2p^3(^1D)3d$	$^3P - ^1D$	[16.44]			5	7	1.2(+5)	0.74	0.20	0.57	D	4
23.	$^3P - ^3P$	[16.59]			3	1	5.7(+4)	0.078	0.012	-0.63	D	4	
24.	$^3P - ^1P$	[16.32]			5	7	3.2(+4)	0.18	0.048	-0.06	E	4	
25.	$^1D - ^1D$	[16.81]			5	7	2000	0.012	0.0033	-1.22	E	4	
26.	$^1D - ^1P$		[16.68]			5	7	6.8(+4)	0.40	0.11	0.30	D	4
27.	$2p^4 - 2p^3(^1D)3d$	$^3P - ^3P$	[16.27]			5	7	5400	0.020	0.0080	-0.82	E	4
			[16.44]			3	5	5800	0.020	0.0063	-0.92	E	4
28.	$^3P - ^3P$		[16.37]			3	1	9.7(+4)	0.13	0.021	-0.41	D	4

Cr XVII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{os}$	$S$ (at. u.)	log $gf$	Accuracy	Source
29.		'P - 'P'	[16.11]			3	3	3900	0.015	0.0024	-1.35	E	4
30.		'D - 'F'	[16.64] [16.65]			5	7	5200	0.030	0.0062	-0.66	E	4
						5	5	1.1(+4)	0.046	0.013	-0.99	E	4
31.		'D - 'P'	[16.31]			5	3	9600	0.023	0.0062	-0.94	D	4
32.		'S - 'P'	[16.66]			1	3	1.8(+5)	2.3	0.13	0.36	D	4

\*The number in parenthesis following the tabulated value indicates the power of ten by which this value has to be multiplied.

Cr XVII

Forbidden Transitions

Line strengths tabulated for magnetic dipole and electric quadrupole transitions within the  $2p^4$  configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the  $n=2$  complex. Strengths of electric quadrupole transitions as defined in Ref. 1 were multiplied by the factor  $2/3$  which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables.

Transition probabilities for these same lines were calculated by Froese Fischer and Saha<sup>2</sup> using the multiconfiguration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their basis included many configurations outside the  $n=2$  complex, but relativistic effects were not treated to the same degree as in Ref. 1.

Line strengths derived from these data are in quite good agreement with the data of Cheng *et al.* For this ion of the oxygen isoelectronic sequence, correlation effects due to mixing with configurations outside the complex were found by Froese Fischer and Saha to be rather small, as shown by a comparison of the results of their calculations employing an extensive basis to those derived by the same technique but limited to configurations within the  $n=2$  complex.

The weakest lines are excluded from this compilation, as their transition probabilities are considered to be very uncertain.

References

- <sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* 24, 111 (1979).
- <sup>2</sup>C. Froese Fischer and H. P. Saha, *Phys. Rev. A* 28, 3169 (1983).

Cr XVII: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$2p^4-2p^4$	'P - 'P'	1656.3	0	60380	5	3	M1	4590	232	C+	1
			.	.	.	5	3	E2	0.13	0.0029	E	1
			[1720]	0	58150	5	1	E2	0.19	0.0017	E	1
2.	'P - 'D'	740.75	0	125160	5	5	M1	6600	0.50	D	1	
		.	.	.	5	5	E2	2.3	0.0015	E	1	
		1340.7	60380	125160	3	5	M1	400	0.1 <sup>a</sup>	D	1	

## Cr XVII: Forbidden transitions - Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
3.		<sup>3</sup> P - <sup>3</sup> S	493.8	60300	263100	3	1	M1	6.5(+4) <sup>a</sup>	0.29	D	1
4.		<sup>1</sup> D - <sup>3</sup> S	[781.13]	135160	263100	5	1	E2	28	0.0049	E	1

<sup>a</sup>The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XVIII

## N Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^3 \ ^4S_{3/2}$

Ionization Energy: 1299 eV = 10480000 cm<sup>-1</sup>

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
90.63	4	108.37	2	129.53	6	157.00	16
92.508	13	110.41	12	133.06	15	164.80	5
93.36	13	112.27	14	136.52	1	169.81	5
94.16	3	113.99	12	139.87	1	175.90	16
95.77	8	119.21	12	140.82	16	184.67	5
97.610	13	119.62	11	143.53	10	193.51	5
99.383	13	122.56	14	147.79	15	197.48	9
102.32	8	123.87	14	149.80	1	222.00	9
104.98	8	125.38	11	149.94	10	248.10	9
105.92	12	125.51	6	151.90	10		
106.84	7	128.10	6	155.46	16		

The tabulated oscillator strengths for transitions of the  $K\alpha$  rays  $2s^2 2p^1 - 2s 2p^2$  and  $2s 2p^2 - 2p^3$  are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. The results should be quite accurate, except

in the case of weak lines. (A few very weak lines have been omitted from this tabulation.)

## Reference

<sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* 24, 111 (1979).

## Cr XVIII: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_0$	$S$ (at. u.)	log $g f$	Accuracy	Source
1.	$2s^2 2p^3 - 2s 2p^4$	<sup>3</sup> S - <sup>3</sup> P	144.05	0	694100	4	12	140	0.13	0.24	-0.30	C	1
			149.80	0	687600	4	6	120	0.060	0.12	-0.63	C	1
			139.87	0	714060	4	4	140	0.9437	0.000	-0.76	C	1
			136.52	0	732400	4	2	166	0.0232	0.0417	-1.082	C	1

Cr XVII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $gf$	Accuracy	Source
2.		S - D	106.37	0	922800	4	4	6.2	0.0011	0.0016	-2.36	E	1
3.		S - S	94.16	0	1062060	4	2	9.2	6.1(-4)	7.6(-4)	-2.61	E	1
4.		S - P	90.63	0	1103370	4	4	24	0.0030	0.0036	-1.92	E	1
5.		D - P	[193.51] [169.81] [164.89] [184.67]	150000 126040 126040 126040	667560 714950 732490 667560	6 4 4 4	6 4 2 6	1.4 0.42 1.3 2.6	3.0(-4) 1.8(-4) 2.6(-4) 0.0020	0.0031 4.0(-4) 5.0(-4) 0.0049	-2.32 -3.14 -2.98 -2.10	E E E E	1 1 1 1
6.		D - D	123.10 125.51 [129.53]	150000 126040 150000	931420 922800 922800	6 4 6	6 4 4	280 340 2.9	0.068 0.061 4.9(-4)	0.17 0.13 0.0013	-0.30 -0.49 -2.53	C C E	1 1 1
7.		D - S	106.84	126040	1062060	4	2	340	0.029	0.041	-0.94	E	1
8.		D - P	101.55 104.98 95.77 102.32	140000 150000 126040 126040	1125650 1103370 1170210 1103370	10 6 4 4	6 4 2 4	840 870 308 154	0.078 0.096 0.0212 0.0242	0.26 0.20 0.3267 0.0326	-0.11 -0.24 -1.072 -1.014	C C C C	1 1 1 1
9.		P - P	[248.10] [222.00] [197.48]	264490 264490 226100	667560 714950 732490	4 4 2	6 4 2	0.23 1.1 1.0	3.2(-4) 8.4(-4) 5.9(-4)	0.0010 0.0025 7.7(-4)	-2.89 -2.47 -2.93	E E E	1 1 1
10.		P - D	147.87 149.94 143.53 [151.90]	251690 264490 226100 264490	927970 931420 922800 922800	6 4 2 4	10 6 4 4	46 53 28.5 6.1	0.025 0.0270 0.0176 0.0021	0.074 0.063 0.0166 0.0042	-0.82 -0.97 -1.453 -2.08	C- C C D	1 1 1 1
11.		P - S	122.40 125.38 119.62	251690 264490 226100	1062060 1062060 1062060	6 4 2	2 2 2	350 53 320	0.026 0.0063 0.068	0.064 0.010 0.064	-0.80 -1.60 -0.87	C- D C	1 1 1
12.		P - P	114.42 119.21 105.92 110.41 113.99	251690 264490 226100 264490 226100	1125650 1103370 1170210 1170210 1103370	6 4 2 4 2	6 4 2 2 4	360 89 49 790 70	0.071 0.0190 0.0083 0.072 0.0274	0.16 0.0298 0.0058 0.10 0.0206	-0.37 -1.119 -1.78 -0.54 -1.261	C- C D C C	1 1 1 1 1



## Cr XVII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$R$ (cm <sup>-1</sup> )	$E_u$ (cm <sup>-1</sup> )	$g_u$	$g_l$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (int. u.)	log $gf$	Accuracy	Source
13.	2s2p <sup>4</sup> -2p <sup>5</sup>	P - P	93.35	657500	1735700	6	4	17	0.0015	0.0025	-2.85	E	1
			[97.680]	714950	1735700	4	4	7.9	0.0010	0.0013	-2.40	E	1
			[92.500]	732430	1813400	2	2	5.5	7.3(-4)	4.3(-4)	-2.85	E	1
			[90.363]	732430	1735700	2	4	2.5	7.3(-4)	4.3(-4)	-2.84	E	1
14.	D - P	D - P	119.67	927970	1735630	10	6	490	0.063	0.25	-0.20	C	1
			123.87	931420	1735700	6	4	300	0.060	0.15	-0.44	C	1
			112.27	922000	1813400	4	2	424	0.0401	0.050	-0.79	C	1
			122.56	922000	1735700	4	4	124	0.0200	0.0452	-0.95	C	1
15.	S - P	S - P	142.54	1062000	1735630	2	6	56	0.051	0.0476	-0.90	C-	1
			147.79	1062000	1735700	2	4	72	0.0400	0.0456	-1.028	C	1
			[133.08]	1062000	1813400	2	2	8.7	0.0023	0.0020	-2.34	D	1
16.	P - P	P - P	156.74	1155450	1735630	6	6	367	0.135	0.418	-0.001	C	1
			157.49	1108370	1735700	4	4	283	0.105	0.218	-0.377	C	1
			155.46	1170210	1813400	2	2	284	0.108	0.105	-0.60	C	1
			[140.82]	1108370	1813400	4	2	222	0.0096	0.073	-0.80	C	1
			[175.90]	1170210	1735700	2	4	20.5	0.0190	0.0220	-1.420	C	1

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XVII

## Forbidden Transitions

Line strengths tabulated for magnetic dipole and electric quadrupole transitions within the 2p<sup>3</sup> configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the  $n=2$  complex. Strengths of electric quadrupole transitions as defined in Ref. 1 were multiplied by the factor  $2/3$ , which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables. The weakest lines are excluded from this compilation, as their strengths are considered to be very uncertain.

$A$ -values for the M1 and E2 components of the single transition within the 2p<sup>3</sup> configuration were obtained by applying  $Z$ -expansion formulas published by Oboladze and Safronova.<sup>2</sup> Their values for the magnetic dipole

contribution to this line are in very good agreement with the results of the scaled Thomas-Fermi calculations of Bhatia *et al.*<sup>3</sup> and Bhatia<sup>4</sup> for nitrogenlike Ti and Mn, respectively. It is not clear whether Oboladze and Safronova incorporated configuration interaction into their calculations. Thus the  $A$ -value for the E2 contribution should be considered rather uncertain.

## References

1. K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* 24, 111 (1979).
2. N. S. Oboladze and U. I. Safronova, *Opt. Spectrosc. (USSR)* 40, 469 (1980).
3. A. K. Bhatia, U. Feldman, and G. A. Doschek, *J. Appl. Phys.* 51, 1464 (1980).
4. A. K. Bhatia, *J. Appl. Phys.* 53, 59 (1982).

## Cr XVIII: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	S (at. u.)	Accuracy	Source
1.	$2p^1-2p^1$	S - D	663.1	0	150000	4	0	M1	320	0.021	D-	1
			793.3	0	126000	4	4	M1	6100	0.45	D	1
2.		D - F	378.0	0	264000	4	4	M1	1.6(+4) <sup>a</sup>	0.13	D	1
			442.1	0	226100	4	2	M1	1.3(+4)	0.084	D-	1
3.		D - D	4639	126000	150000	4	6	M1	127	1.06	C+	1
			-	-	-	4	6	E2	4.3(-4)	0.0019	E	1
4.		D - F	[1328]	150000	226100	6	2	E2	0.63	0.0031	E	1
			[879.58]	150000	264000	6	4	M1	5200	0.52	D	1
			-	-	-	6	4	E2	6.3	0.0079	E	1
			[999.00]	126000	226100	4	2	M1	3400	0.25	D	1
			-	-	-	4	2	E2	3.0	0.0036	E	1
			722.1	126000	264000	4	4	M1	1.6(+4)	0.87	D	1
			-	-	-	4	4	E2	3.0	0.0014	E	1
5.		F - F	2606.4	226100	264000	2	4	M1	382	1.00	C	1
6.	$2p^1-2p^1$	F - F	[1337]	1738700	1813480	4	2	M1	7600	1.3	C+	2
			-	-	-	4	2	E2	0.53	0.0027	E	2

<sup>a</sup>The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XIX

## C Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^1 {}^1P_0$

Ionization Energy: 1396 eV = 11260000 cm<sup>-1</sup>

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
14.73	30	107.70	5	118.83	17	129.00	9
14.80	29	109.33	18	120.86	23	130.99	17
14.81	30	109.64	4	125.93	3	132.11	3
14.84	29	110.37	11	126.24	20	133.99	3
90.102	16	111.18	18	126.20	15	134.89	3
95.62	16	111.88	5	126.33	10	137.89	19
95.88	6	113.97	4	127.95	20	138.15	19
100.69	21	118.31	17	128.43	17	138.45	3
104.18	4	118.67	17	128.63	17	140.51	3

List of tabulated lines - Continued

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
140.92	19	161.29	8	185.87	24	236.11	26
143.57	28	163.94	25	199.16	7	267.55	12
148.64	2	164.89	8	201.82	27	278.21	26
151.32	14	165.46	2	201.97	13	280.37	1
152.42	19	169.40	2	208.94	22	310.54	1
154.92	19	169.73	2	204.89	7		
160.01	2	179.18	22	205.28	7		
160.30	2	180.37	22	211.00	24		

The tabulated oscillator strengths for transitions of the arrays  $2s^22p^2-2s2p^3$  and  $2s2p^3-2p^4$  are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the  $n=2$  complex. The results should be quite accurate, except in the case of weak lines. (A few very weak lines have been omitted from this tabulation.)

Transition probabilities for lines of the  $2s^22p^2-2s2p^3$  array were calculated by Froese Fischer and Saha<sup>2</sup> using the multiconfiguration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their basis included many configurations outside the  $n=2$  complex, but relativistic effects were not treated to the same degree as in Ref. 1.

Line strengths derived from these two sources are in reasonably good agreement, particularly for the stronger transitions.

Data for a few lines of the  $2p^2-2p3d$  array were interpolated from the HX (Hartree-Fock with statistical allowance for exchange)  $f$ -values of Bromage and Fawcett<sup>3</sup> for the isoelectronic ions Ca XV and Fe XXI.

References

<sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* 24, 111 (1979).  
<sup>2</sup>C. Froese Fischer and H. P. Saha, *Phys. Scr.* 32, 181 (1985).  
<sup>3</sup>G. E. Bromage and B. C. Fawcett, *Mon. Not. R. Astron. Soc.* 178, 605 (1977).

Cr XIX: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{os}$	$S$ (at. u.)	log $gf$	Accuracy	Source
1.	$2s^22p^2-2s2p^3$	$^3P - ^4S$	[310.54]	82420	404440	5	5	0.17	2.5(-4) <sup>a</sup>	0.0013	-2.90	E	1
			[280.37]	47770	404440	3	5	0.15	2.9(-4)	8.0(-4)	-3.06	E	1
2.	$^3P - ^3D$	162.02	61710	678920	9	15	72	0.0473	0.227	-0.371	C-	1	
		165.46	82420	686510	5	7	50	0.0329	0.092	-0.77	C	1	
		160.30	47770	671500	3	5	82	0.063	0.084	-0.80	C	1	
		148.64	0	672750	1	3	90	0.080	0.044	-1.05	C	1	
		169.73	82420	671500	5	5	0.096	4.1(-5)	1.1(-4)	-3.69	E	1	
		160.01	47770	672750	3	3	11	0.0041	0.0065	-1.91	D	1	
		[169.40]	82420	672750	5	3	0.26	6.7(-5)	1.9(-4)	-3.47	E	1	
3.	$^3P - ^3P$	135.55	61710	799490	9	9	190	0.062	0.210	-0.327	C-	1	
		138.45	82420	804090	5	5	171	0.0491	0.112	-0.61	C	1	
		133.99	47770	794120	3	3	121	0.0325	0.0430	-1.011	C	1	
		140.51	82420	794120	5	3	36	0.0063	0.015	-1.50	D	1	
		134.80	47770	780100	3	1	198	0.0180	0.0240	-1.268	C	1	
		132.11	47770	804090	3	5	7.1	0.0031	0.0040	-2.03	D	1	
		125.93	0	794120	1	3	40.5	0.0289	0.0120	-1.54	C	1	
4.	$^3P - ^4S$	111.34	61710	960660	9	3	880	0.065	0.18	-0.31	C	1	
		113.97	82420	960660	5	3	560	0.064	0.12	-0.49	C	1	
		109.64	47770	960660	3	3	246	0.0444	0.0481	-0.88	C	1	
		104.18	0	960660	1	3	90	0.0438	0.0160	-1.360	C	1	

Cr XIX: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{\lambda}$	$S$ (at. u.)	log $gf$	Accuracy	Source
5.		'P - 'D'	111.88	82420	976270	5	5	53	0.016	0.018	-1.80	E	1
			[107.70]	47770	976270	3	5	24	7.1(-4)	7.6(-4)	-2.67	E	1
6.		'P - 'P'	95.88	47770	1090760	3	3	36	0.0049	0.0046	-1.83	E	1
7.		'D - 'D'	[199.16]	184690	686810	5	7	6.2	0.0052	0.017	-1.59	E	1
			[205.38]	184690	671590	5	5	0.33	2.1(-4)	7.1(-4)	-2.96	E	1
			[204.89]	184690	672750	5	3	1.2	4.6(-4)	0.9016	-2.64	E	1
8.		'D - 'P'	[161.29]	184690	904690	5	5	1.9	7.6(-4)	0.0020	-2.42	E	1
			[164.09]	184690	794120	5	3	2.8	6.7(-4)	0.0018	-2.47	E	1
9.		'D - 'S'	[129.00]	184690	959860	5	3	0.73	1.1(-4)	2.3(-4)	-3.26	E	1
10.		'D - 'D'	126.33	184690	976270	5	5	435	0.104	0.216	-0.284	C	1
11.		'D - 'P'	110.37	184690	1090760	5	3	600	0.066	0.12	-0.48	C	1
12.		'S - 'D'	[267.56]	298990	672750	1	3	0.37	0.0012	0.0011	-2.92	E	1
13.		'S - 'P'	[201.97]	298990	794120	1	3	1.1	0.0020	0.0013	-2.70	E	1
14.		'S - 'S'	[151.32]	298990	959860	1	3	4.2	0.0043	0.0021	-2.37	E	1
15.		'S - 'P'	126.30	298990	1090760	1	3	156	0.112	0.0466	-0.95	C	1
16.	2s2p <sup>2</sup> -2p <sup>4</sup>	'S - 'P'	95.62	404440	1450200	5	5	7.2	9.3(-4)	0.0016	-2.31	E	1
			[90.102]	404440	1514290	5	3	1.8	1.3(-4)	1.9(-4)	-3.19	E	1
17.		'D - 'P'	124.97	678920	1479090	15	9	400	0.057	0.35	-0.07	C-	1
			130.59	686810	1450200	7	5	290	0.053	0.16	-0.43	C	1
			118.67	671590	1514290	5	3	210	0.0266	0.052	-0.88	C	1
			118.31	672750	1517960	3	1	329	0.0230	0.0269	-1.161	C	1
			128.43	671590	1450200	5	5	119	0.0295	0.062	-0.83	C	1
			118.83	672750	1514290	3	3	135	0.0236	0.0336	-1.067	C	1
128.63	672750	1450200	3	5	23	0.0097	0.012	-1.54	D	1			
18.		'D - 'D'	111.18	686810	1586250	7	5	37	0.0049	0.012	-1.46	E	1
			[109.23]	671590	1586250	5	5	5.5	9.3(-4)	0.0018	-2.31	E	1

## Cr XII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	log $gf$	Accuracy	Source
19.		<sup>3</sup> P - <sup>3</sup> P	154.92	804690	1450200	5	5	35.3	0.9127	0.0324	-1.197	C	1
			140.92	804690	1514290	5	3	138	0.0247	0.067	-0.91	C	1
			138.15	794120	1517960	3	1	175	0.9167	0.0228	-1.980	C	1
			152.42	794120	1450200	3	5	32.7	0.9190	0.0286	-1.244	C	1
			137.89	789100	1514290	1	3	41.6	0.0356	0.9162	-1.449	C	1
20.		<sup>3</sup> P - <sup>1</sup> D	127.95	804690	1586250	5	5	10	0.0025	0.0063	-1.90	E	1
			[126.24]	794120	1586250	3	5	7.0	0.0028	0.0035	-2.08	E	1
21.		<sup>3</sup> P - <sup>1</sup> S	[100.69]	794120	1787280	3	1	26	0.0013	0.0013	-2.41	E	1
22.		<sup>3</sup> S - <sup>3</sup> P	192.59	959860	1479090	3	9	86	0.14	0.27	-0.37	C	1
			[203.94]	959860	1450200	3	5	63	0.065	0.13	-0.71	C	1
			180.37	959860	1514290	3	3	110	0.064	0.096	-0.79	C	1
			179.18	959860	1517960	3	1	145	0.0232	0.9411	-1.157	C	1
23.		<sup>3</sup> S - <sup>1</sup> S	[120.85]	959860	1787280	3	1	45	0.0033	0.0039	-2.00	E	1
24.		<sup>1</sup> D - <sup>3</sup> P	[211.00]	976270	1450200	5	5	6.3	0.0042	0.015	-1.68	E	1
			[185.87]	976270	1514290	5	3	1.4	4.5(-4)	0.0014	-2.65	E	1
25.		<sup>1</sup> D - <sup>1</sup> D	163.94	976270	1586250	5	5	310	0.125	0.337	-0.204	C	1
26.		<sup>1</sup> P - <sup>3</sup> P	[278.21]	1090760	1450200	3	5	0.88	0.0017	0.0047	-2.29	E	1
			[236.11]	1090760	1514290	3	3	4.7	0.0039	0.0091	-1.93	E	1
			201.82	1090760	1586250	3	5	41.6	0.0423	0.084	-0.90	C	1
28.		<sup>1</sup> P - <sup>1</sup> S	143.57	1090760	1787280	3	1	720	0.074	0.10	-0.65	C	1
29.	<sup>2p</sup> <sup>2</sup> - <sup>2p</sup> <sup>3d</sup>	<sup>3</sup> P - <sup>3</sup> D	[14.84]			5	7	1.3(+5)	0.61	0.15	0.48	E	interp.
			[14.80]			1	3	1.3(+5)	1.3	0.063	0.11	D	interp.
30.		<sup>3</sup> P - <sup>3</sup> P	[14.73]			3	3	7.1(+4)	0.23	0.033	-0.16	E	interp.
			[14.81]			5	3	3.4(+4)	0.068	0.017	-0.47	E	interp.

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XIX

## Forbidden Transitions

Line strengths tabulated for magnetic dipole and electric quadrupole transitions within the  $2p^2$  configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing was limited to the  $n=2$  complex. Strengths of electric quadrupole transitions as defined in Ref. 1 were multiplied by the factor  $2/3$ , which is needed to bring these values into conformance with the definition of quadrupole strengths used in the NBS tables. The weakest lines are excluded from this compilation, as their strengths are considered to be very uncertain.

Transition probabilities for these same lines were calculated by Froese Fischer and Saha<sup>2</sup> using the multiconfiguration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their basis included many configurations outside the  $n=2$  complex, but relativistic effects were not treated to the same degree as in Ref. 1. Line strengths derived from these data are in good agreement with the data of Cheng *et al.*

## References

- <sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* 24, 111 (1979).  
<sup>2</sup>C. Froese Fischer and H. P. Saha, *Phys. Scr.* 32, 181 (1985).

Cr XIX: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{if}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$2p^2-2p^2$	'P - 'P	2885.4	47770	82420	3	5	M1	469	2.09	C+	1
			-	-	-	3	5	E2	0.0035	0.0021	E	1
			2090.9	0	47770	1	3	M1	1810	1.84	C+	1
			[1213]	0	82420	1	5	E2	0.18	0.0014	E	1
2.	'P - 'D	979.0	82420	184690	5	5	M1	5700	1.0	C	1	
		-	-	-	5	5	E2	0.90	0.0024	E	1	
		731.1	47770	184690	3	5	M1	5700	0.41	D	1	
3.	'P - 'S	398.4	47770	298990	3	1	M1	6.4 + 4*	0.15	D	1	
4.	'D - 'S	[874.89]	184690	298990	5	1	E2	13	0.0041	E	1	

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XX

## B Isoelectronic Sequence

Ground State:  $1s^2 2s^2 2p^2 P_{1/2}$ Ionization Energy:  $1496 \text{ eV} = 12070000 \text{ cm}^{-1}$ 

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wav-length (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
14.13	14	128.42	3	164.63	8	216.99	7
14.26	14	129.26	9	167.97	8	258.57	11
97.494	6	131.31	9	169.87	8	271.72	11
97.729	6	133.82	4	173.42	8	281.99	1
101.63	6	135.26	9	175.42	2	287.63	1
116.05	3	140.75	4	179.21	2	368.20	1
119.29	5	148.99	4	180.85	12	416.34	10
122.29	5	156.00	2	192.82	12		

The tabulated oscillator strengths for transitions of the arrays  $2s^2 2p-2s2p^2$  and  $2s2p^2-2p^3$  are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations included a perturbative treatment of the Breit interaction and the Lamb shift. The results should be quite accurate, except in the case of weak lines. (A few very weak lines have been omitted from this tabulation.)

According to several sources (see, e.g., introduction to Fe XXII), the two levels  $2s2p^2 \ ^2P_{1/2}$  and  $\ ^2S_{1/2}$  "cross" at about V XIX or Cr XX. Transitions to these levels in Cr XX have been omitted from this compilation, since the precise location of the level crossing, and thus the correct designations of the levels, are uncertain.

The Hartree-Fock results of Shamey<sup>2</sup> for the isoelectronic ions Ar XIV and Fe XXII, which allowed for limited configuration interaction, were interpolated to provide  $f$ -values for the  $2p-3s$ ,  $2p-3d$ , and  $2p-4d$  transitions.

## References

- <sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* **24**, 111 (1979).  
<sup>2</sup>L. J. Shamey, *J. Opt. Soc. Am.* **61**, 942 (1971).

## Cr XX: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $gf$	Accuracy	Source
1.	$2s^2 2p-2s2p^2$	$\ ^2P^{\circ} - \ ^2P$	[287.63]	89090	490700	4	6	0.23	6.1(-4) <sup>*</sup>	0.0023	-2.61	E	1
			[281.99]	0	254620	2	2	0.42	5.0(-4)	0.2(-4)	-3.00	E	1
			[268.20]	89090	254620	4	2	0.11	1.1(-4)	5.2(-4)	-3.26	E	1
2.	$\ ^2P^{\circ} - \ ^2D$	168.66	55350	649370	6	10	63	0.045	0.15	-0.57	D	1	
		175.42	89090	649090	4	6	53	0.0968	0.065	-0.23	C	1	
		166.00	0	641080	2	4	84	0.061	0.063	-0.91	C	1	
		179.21	89090	641080	4	4	1.1	5.4(-4)	0.0013	-2.87	E	1	
3.	$\ ^2P^{\circ} - \ ^2P$	128.42	89090	861700	4	4	390	0.098	0.16	-0.43	C	1	
		116.05	0	861700	2	4	87	0.0220	0.0176	-1.337	C	1	

## Cr XX: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ ( $\text{cm}^{-1}$ )	$E_2$ ( $\text{cm}^{-1}$ )	$g_1$	$g_2$	$A_{21}$ ( $10^6 \text{ s}^{-1}$ )	$f_{12}$	$S$ (at. u.)	$\log gf$	Accuracy	Source
4.	$2s2p^2-2p^3$	$^3P - ^3S$	143.68	404920	1101890	12	4	389	0.0400	0.227	-0.318	C	1
			148.99	430700	1101890	6	4	175	0.0388	0.114	-0.63	C	1
			140.75	391410	1101890	4	4	135	0.0400	0.074	-0.80	C	1
			133.82	354620	1101890	2	4	83	0.0445	0.0392	-1.051	C	1
5.	$^3P - ^3D$	122.29	430700	1248440	6	6	9.8	0.0022	0.0053	-1.88	E	1	
		[119.29]	391410	1229720	4	4	9.8	0.0021	0.0033	-2.08	E	1	
6.	$^3P - ^3P$	[101.63]	430700	1414650	6	4	1.1	1.1(-4)	2.2(-4)	-3.18	E	1	
		[97.729]	391410	1414650	4	4	2.0	2.0(-4)	3.6(-4)	-2.95	E	1	
		[97.494]	354620	1380320	2	2	1.5	2.1(-4)	1.3(-4)	-3.38	E	1	
7.	$^3D - ^3S$	[216.99]	641030	1101890	4	4	0.42	3.0(-4)	8.6(-4)	-2.92	E	1	
		163.73	648270	1240850	10	10	126	0.054	0.296	-0.270	C	1	
8.	$^3D - ^3D$	167.97	653090	1248440	6	6	112	0.0474	0.157	-0.55	C	1	
		169.87	641030	1229720	4	4	71	0.0306	0.068	-0.91	C	1	
		173.42	653090	1229720	6	4	40.3	0.0121	0.0414	-1.139	C	1	
		164.63	641030	1248440	4	6	24.1	0.0147	0.0319	-1.231	C	1	
		132.46	648270	1403210	10	6	195	0.0307	0.134	-0.51	C	1	
9.	$^3D - ^3P$	131.31	653090	1414650	6	4	127	0.0219	0.057	-0.88	C	1	
		135.26	641030	1380320	4	2	241	0.0331	0.059	-0.88	C	1	
		129.26	641030	1414650	4	4	42.7	0.0107	0.0182	-1.369	C	1	
		[416.34]	861700	1101890	4	4	0.19	5.0(-4)	0.0027	-2.70	E	1	
11.	$^3P - ^3D$	[258.57]	861700	1248440	4	6	29.8	0.0448	0.153	-0.75	C	1	
		271.72	861700	1229720	4	4	0.54	6.0(-4)	0.0021	-2.62	E	1	
12.	$^3P - ^3P$	180.85	861700	1414650	4	4	160	0.077	0.18	-0.51	C	1	
		192.82	861700	1380320	4	2	23	0.0065	0.017	-1.59	D	1	
13.	$2p-3s$	$^3P^o - ^3S$				4	2		0.019		-1.12	E	interp.
						2	2		0.020		-1.40	E	interp.
14.	$2p-3d$	$^3P^o - ^3D$	[14.26]			4	6	1.2(+5)	0.56	0.11	0.37	D	interp.
			[14.13]			2	4	1.1(+5)	0.65	0.060	0.11	D	interp.
						4	4		0.064		-0.59	D	interp.



Cr XX: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $gf$	Accuracy	Source
15.	2p-4d	<sup>3</sup> P - <sup>3</sup> D											
						4	6		0.11		-0.36	D	interp.
						2	4		0.12		-0.62	E	interp.
						4	4		0.012		-1.32	D	interp.

The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XX

## Forbidden Transitions

The line strengths tabulated for the single magnetic dipole and single electric quadrupole transition within the 2s<sup>2</sup>2p ground state configuration are the results of the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations include a perturbative treatment of the Breit interaction and the Lamb shift. Allowance for configuration mixing is limited to the n=2 complex. The strength of the electric quadrupole transition as defined in Ref. 1 was multiplied by the factor 2/3 in order to bring this value into conformance with the definition of the quadrupole strength used in the NBS tables.

Transition probabilities for the same lines were calculated by Froese Fischer and Saha<sup>2</sup> using the multiconfig-

uration Hartree-Fock (MCHF) method with Breit-Pauli corrections. Their orbital basis includes many configurations outside the n=2 complex, but relativistic effects were not treated to the same degree as in Ref. 1. The line strengths for both the M1 and E2 transitions, derived from these data by interpolation between appropriately spaced ions of the  $\beta$  sequence, are in very good agreement with the data of Cheng *et al.*<sup>1</sup>

## References

- <sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* 24, 111 (1979).  
<sup>2</sup>C. Froese Fischer and H. P. Saha, *Phys. Rev. A* 28, 3169 (1983).

Cr XX: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	2p-2p	<sup>3</sup> P - <sup>3</sup> P	1205.9	0	82926	2	4	M1	5110	1.33	B	1
						2	4	E2	0.336	0.00204	C	1

## Cr XII

## Be Isoelectronic Sequence

Ground State:  $1s^2 2s^2 1S_0$ Ionization Energy:  $1634 \text{ eV} = 13180000 \text{ cm}^{-1}$ 

## Allowed Transitions

## List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
12.87	11	13.60	12,29	13.99	28	140.72	4
12.97	11	13.65	24	14.00	19	149.90	2
12.98	10,11	13.66	29	14.04	19,25	154.62	4
13.01	10	13.67	24	14.12	30	165.03	3
13.02	10	13.68	29	14.17	19,21	168.62	3
13.06	9	13.75	29	14.20	31	170.16	7
13.12	8	13.76	27	14.23	21	175.45	3
13.13	10	13.78	27	14.24	35	184.48	3
13.22	16	13.84	27,33,34	14.25	21	190.98	3
13.24	15	13.87	27	14.32	21	197.61	3
13.44	14	13.91	27	14.35	21	250.94	6
13.49	24	13.92	28	14.38	22	293.11	1
13.53	24	13.93	26	14.39	21	357.12	5
13.55	24	13.94	27	14.58	20	409.80	5
13.59	13	13.95	32	14.81	23	505.89	5

Oscillator strengths for transitions of the arrays  $2s^2-2s2p$  and  $2s2p-2p^2$  are taken from the multiconfiguration Dirac-Fock (MCDF) calculations of Cheng *et al.*<sup>1</sup> These relativistic calculations include the configuration interaction most relevant for the states of these configurations, as well as a perturbative treatment of the Breit interaction and the Lamb shift. The results should be quite accurate, except for the weakest intercombination lines. (The  $^3P_1 - ^1S_0$  transition of the  $2s2p-2p^2$  array has been omitted here, since the  $f$ -value is considerably smaller than those of the other lines of this array.)

A number of sources of reliable data, from other relativistic calculations, are available for the  $2s-2p$  transitions. However, with the exception of some of the weaker lines, they all agree well with the results of Cheng *et al.*<sup>1</sup> The latter are quoted exclusively here since they provide data from a single set of comprehensive calculations, all done at a uniform and reasonably accurate level of approximation, for the valence shell  $2s-2p$  transitions for all ions of the isoelectronic sequence.

The  $f$ -values for the  $2s^2-2s3p$ ,  $2s2p-2p3p$ ,  $2s2p-2s3s$ ,  $2p^2-2p3s$ ,  $2s2p-2s3d$ , and  $2p^2-2p3d$  arrays of transitions are taken from the work of Fawcett,<sup>2</sup> who used Cowan's version of the relativistic Hartree-Fock method with intermediate coupling and configuration interaction. This work provides a comprehensive set of data for the entire

isoelectronic sequence, calculated at a uniform level of approximation. Some of these transitions, for some ions of this sequence, have also been calculated by Bhatia *et al.*<sup>3</sup> using the program SUPERSTRUCTURE, which includes configuration interaction and intermediate coupling. Where they overlap, these two sets of calculations agree to within the uncertainties assigned here. Transitions involving the  $J=1$  levels of  $2p3p$   $^3S$  and  $^3P$  have been omitted because of erratic behavior of the  $f$ -values along the sequence.

Oscillator strengths for the transition array  $2s^2-2s4p$  have been interpolated from the relativistic random phase approximation (RRPA) calculations along the isoelectronic sequence by Lin and Johnson.<sup>4</sup>

A few multiplet  $f$ -values for transitions involving the outer electron alone,  $2s3s-2s3p$  and  $2s3p-2s3d$ , have been interpolated along the isoelectronic sequence and assigned a low accuracy.

## References

- <sup>1</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* **24**, 111 (1979).
- <sup>2</sup>B. C. Fawcett, *At. Data Nucl. Data Tables* **30**, 1 (1984); **33**, 479 (1985).
- <sup>3</sup>A. K. Bhatia, U. Feldman, and J. F. Seely, *At. Data Nucl. Data Tables* **35**, 449 (1986).
- <sup>4</sup>C. D. Lin and W. R. Johnson, *Phys. Rev. A* **15**, 1046 (1977).

## Cr III: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{12}$	$S$ (at. u.)	$\log gf$	Accuracy	Source
1.	2s <sup>2</sup> -2s2p	<sup>1</sup> S - <sup>3</sup> P	[293.11]	0	341170	1	3	0.25	0.0010	9.6(-4)	-3.00	D	1
2.		<sup>1</sup> S - <sup>1</sup> P	[149.90]	0	667110	1	3	162	0.164	0.0009	-0.785	B	1
3.	2s2p-2p <sup>2</sup>	<sup>3</sup> P - <sup>3</sup> P	181.90	374100	925900	9	9	117	0.0576	0.300	-0.286	B	1
			[184.48]	405070	947130	5	5	73.7	0.0376	0.114	-0.726	B	1
			[175.45]	341170	911130	3	3	34.2	0.0158	0.0274	-1.324	B	1
			[197.61]	405070	911130	5	3	40.1	0.0141	0.0459	-1.152	B	1
			[190.96]	341170	864780	3	1	109	0.0199	0.0375	-1.224	B	1
			[165.93]	341170	947130	3	5	42.8	0.0291	0.0474	-1.059	B	1
			[168.62]	318080	911130	1	3	52.4	0.0670	0.0372	-1.174	B	1
4.		<sup>3</sup> P - <sup>1</sup> D											
			[154.62]	405070	1051810	5	5	28.2	0.0101	0.0257	-1.297	C	1
			[140.72]	341170	1051810	3	5	2.4	0.0012	0.0017	-2.44	D	1
5.		<sup>1</sup> P - <sup>3</sup> P											
			[357.12]	667110	947130	3	5	2.1	0.0066	0.023	-1.70	D	1
			[409.80]	667110	911130	3	3	0.940	1.0(-4)	4.0(-4)	-2.52	E	1
			[505.89]	667110	864780	3	1	0.19	2.4(-4)	0.0012	-2.14	E	1
6.		<sup>1</sup> P - <sup>1</sup> D	[259.94]	667110	1051810	3	5	36.5	0.0616	0.158	-0.733	B	1
7.		<sup>1</sup> P - <sup>1</sup> S	[170.16]	667110	1254790	3	1	271	0.0392	0.0659	-0.930	B	1
8.	2s <sup>2</sup> -2s3p	<sup>1</sup> S - <sup>3</sup> P											
			[13.12]	0	7620000	1	3	3.7(+4)	0.29	0.013	-0.54	C-	2
9.		<sup>1</sup> S - <sup>1</sup> P	[13.08]	0	[7648000]	1	3	5.2(+4)	0.40	0.017	-0.40	C-	2
10.	2s2p-2p3p	<sup>3</sup> P - <sup>3</sup> D											
			[13.02]	405070	8087000	5	7	3.9(+4)	0.14	0.030	-0.15	C-	2
			[13.02]	341170	[8023000]	2	5	3.8(+4)	0.16	0.021	-0.22	C-	2
			[12.98]	318080	[8025000]	1	3	1.1(+4)	0.062	0.0035	-1.09	D	2
			[13.13]	405070	[8023000]	5	5	1900	0.0050	0.0011	-1.60	D	2
			[13.01]	341170	[8025000]	2	3	1.9(+4)	0.047	0.0060	-0.85	D	2
11.		<sup>3</sup> P - <sup>3</sup> P											
			[12.98]	405070	8109000	5	5	3.9(+4)	0.098	0.021	-0.21	C-	2
			[12.97]	341170	[8049000]	3	1	4.8(+4)	0.040	0.0061	-0.92	D	2
			[12.87]	341170	8109000	3	5	2700	0.011	0.0014	-1.48	D	2
12.		<sup>1</sup> P - <sup>1</sup> P	[13.60]	667110	8022000	3	3	1.6(+4)	0.043	0.0068	-0.89	D	2
13.		<sup>1</sup> P - <sup>3</sup> D											
			[13.59]	667110	[8025000]	3	3	1.2(+4)	0.033	0.0044	-1.00	D	2
14.		<sup>1</sup> P - <sup>3</sup> P											
			[13.44]	667110	8109000	3	5	1.2(+4)	0.065	0.0070	-0.80	D	2
			[13.44]	667110	[8109000]	3	3	2.5(+4)	0.067	0.0089	-0.70	C-	2

Cr XXI: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$L_1$	$L_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (at. u.)	log $g^2$	Accuracy	Source
15.		<sup>1</sup> P - <sup>1</sup> D	[13.34]	667110	[8161000]	3	5	5.2(+4)	0.23	0.930	-0.16	C-	2
16.		<sup>1</sup> P - <sup>1</sup> S	[13.22]	667110	[8231000]	3	1	4.6(+4)	0.040	0.9052	-0.92	D	2
17.	2s <sup>2</sup> -2s4p	<sup>1</sup> S - <sup>3</sup> P											
						1	3		0.020		-1.70	D	<i>interp.</i>
18.		<sup>1</sup> S - <sup>1</sup> P				1	3		0.16		-0.80	D	<i>interp.</i>
19.	2s2p-2s3s	<sup>3</sup> P - <sup>1</sup> S	14.11	374100	7463000	9	3	2.6(+4)	0.025	0.011	-0.63	D	2
			[14.17]	405070	7463000	5	3	1.4(+4)	0.025	0.0061	-0.89	D	2
			[14.04]	341170	7463000	3	3	9100	0.027	0.0037	-1.09	D	2
			[14.00]	318080	7463000	1	3	3200	0.028	0.0013	-1.55	D	2
20.		<sup>1</sup> P - <sup>1</sup> S	[14.58]	667110	[7526000]	3	1	9400	0.010	0.0014	-1.52	D	2
21.	2p <sup>2</sup> -2p3s	<sup>3</sup> P - <sup>3</sup> P	14.27	925980	[7933000]	9	9	1.8(+4)	0.054	0.023	-0.31	D	2
			[14.25]	947130	[7966000]	5	5	1.2(+4)	0.038	0.0089	-0.72	D	2
			[14.32]	911130	[7894000]	3	3	3600	0.011	0.0016	-1.48	D	2
			[14.39]	947130	[7894000]	5	3	8100	0.015	0.0036	-1.12	D	2
			[14.35]	911130	[7881000]	3	1	1.7(+4)	0.017	0.0024	-1.29	D	2
			[14.17]	911130	[7966000]	3	5	6000	0.030	0.0042	-1.05	D	2
			[14.23]	864780	[7894000]	1	3	6100	0.055	0.0025	-1.25	D	2
22.		<sup>1</sup> D - <sup>1</sup> P	[14.38]	1051810	[8008000]	5	3	1.5(+4)	0.028	0.0066	-0.85	D	2
23.		<sup>1</sup> S - <sup>1</sup> P	[14.81]	1254790	[8008000]	1	3	5800	0.057	0.0028	-1.24	D	2
24.	2s2p-2s3d	<sup>3</sup> P - <sup>1</sup> D	13.60	374100	[7728000]	9	15	1.6(+5)	0.72	0.29	0.81	C-	2
			[13.65]	405070	7733000	5	7	1.5(+5)	0.60	0.13	0.48	C-	2
			[13.55]	341170	7721000	3	5	1.2(+5)	0.55	0.074	0.22	C-	2
			[13.49]	318080	[7730000]	1	3	9.0(+4)	0.74	0.033	-0.13	C-	2
			[13.67]	405070	7721000	5	5	3.9(+4)	0.11	0.025	-0.26	C-	2
			[13.53]	341170	[7730000]	3	3	6.6(+4)	0.18	0.024	-0.27	C-	2
			[13.65]	405070	[7730000]	5	3	4300	0.0072	0.0016	-1.44	C-	2
25.		<sup>1</sup> P - <sup>1</sup> D	[14.04]	667110	[7792000]	3	5	1.2(+5)	0.61	0.085	0.26	C-	2
26.	2p <sup>2</sup> -2p3d	<sup>1</sup> P - <sup>3</sup> P											
			[13.93]	947130	[8124000]	5	7	4.2(+4)	0.17	0.039	-0.07	C-	2
27.		<sup>1</sup> P - <sup>1</sup> D	13.82	925980	8162000	9	15	1.5(+5)	0.71	0.29	0.80	C-	2
			[13.78]	947130	8204000	5	7	1.7(+5)	0.68	0.15	0.53	C-	2
			[13.87]	911130	8121000	3	5	8.5(+4)	0.407	0.056	0.067	C-	2
			[13.76]	864780	8134000	1	3	1.51(+5)	1.29	0.058	0.111	C-	2
			[13.94]	947130	8121000	5	5	1.1(+4)	0.032	0.0073	-0.80	D	2
			[13.84]	911130	8134000	3	3	3.5(+4)	0.10	0.014	-0.52	C-	?
			[13.91]	947130	8134000	5	3	1000	0.0018	4.1(-4)	-2.05	D	2
28.		<sup>1</sup> P - <sup>1</sup> D											
			[13.99]	947130	[8093000]	5	5	8200	0.024	0.0055	-0.92	C-	2
			[13.92]	911130	[8093000]	3	5	8.5(+4)	0.41	0.056	0.09	D	2

Cr XII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (ml. u.)	log $g^2$	Accuracy	Source
29.		<sup>3</sup> P - <sup>3</sup> P	13.71	925900	[8290000]	9	9	1.15(+5)	0.325	0.132	0.065	C-	2
			[13.75]	947130	8219000	5	5	9.5(+4)	0.270	0.061	0.130	C-	2
			[13.68]	911130	8219000	3	3	8.2(+4)	0.23	0.081	-0.16	C-	2
			[13.75]	947130	8219000	5	3	3.5(+4)	0.076	0.017	-0.42	C-	2
			[13.66]	911130	[8231000]	3	1	1.2(+5)	0.11	0.015	-0.68	C-	2
			[13.68]	911130	8219000	3	5	1.2(+4)	0.067	0.0077	-0.77	D	2
			[13.60]	864780	8219000	1	3	610	0.0051	2.2(-4)	-2.29	D	2
30.		<sup>1</sup> D - <sup>3</sup> P	[14.12]	1051810	[8132000]	5	5	7400	0.022	0.0051	-0.96	D	2
31.		<sup>1</sup> D - <sup>1</sup> D	[14.20]	1051810	[8093000]	5	5	1.7(+4)	0.050	0.012	-0.60	C-	2
32.		<sup>1</sup> D - <sup>3</sup> P	[13.95]	1051810	8219000	5	5	3.8(+4)	0.11	0.025	-0.28	C-	2
33.		<sup>1</sup> D - <sup>1</sup> P	[13.84]	1051810	8275000	5	3	8700	0.015	0.0034	-1.12	D	2
34.		<sup>1</sup> D - <sup>1</sup> P	[13.84]	1051810	8275000	5	7	2.58(+5)	1.04	0.237	0.72	C-	2
35.		<sup>1</sup> S - <sup>1</sup> P	[14.24]	1254730	8275000	1	3	1.41(+5)	1.29	0.060	0.111	C-	2
36.	2s3s-2s3p	<sup>3</sup> S - <sup>3</sup> P				3	9		0.13		-0.41	D	interp.
37.		<sup>1</sup> S - <sup>1</sup> P				1	3		0.056		-1.25	E	interp.
38.	2s3p-2s3d	<sup>3</sup> P - <sup>3</sup> D				9	15		0.029		-0.58	E	interp.
39.		<sup>1</sup> P - <sup>1</sup> D				3	5		0.052		-0.81	E	interp.

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XXI

## Forbidden Transitions

Transition probabilities for magnetic dipole and electric quadrupole transitions within the  $2s2p$  and  $2p^2$  configurations were calculated by Feldman *et al.*<sup>1</sup> using scaled Thomas-Fermi wavefunctions with allowance for configuration interaction and relativistic effects. We modified their transition probability data by the application of experimental wavelengths, i.e., we first converted their  $A$ -values into line strength data utilizing their theoretical transition energies and then reconverted the line strengths into  $A$ -values with wavelengths derived from experimental data. This approach should normally yield transition probabilities that are more accurate than those based on theoretically determined wavelengths.

The one E2 transition listed, which is relatively strong compared to other E2 transitions, has been taken from the multiconfiguration relativistic Hartree-Fock calculations of Anderson and Anderson,<sup>2</sup> and has been included to indicate the small magnitude of the E2 line strengths.

## References

- <sup>1</sup>U. Feldman, G. A. Dozick, Ch.-Ch. Cheng, and A. K. Bhatia, *J. Appl. Phys.* **51**, 190 (1980).
- <sup>2</sup>E. K. Anderson and E. M. Anderson, *Opt. Spectrosc. (USSR)* **52**, 478 (1982).

Cr XXI: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	S (at. u.)	Accuracy	Source
1.	2s2p-2s2p	'P - 'P	1566.4	341170	405070	3	5	M1	3450	2.46	C+	1
			[4329.7]	318080	341170	1	3	M1	218	1.97	C+	1
2.		'P - 'P	[381.62]	405070	667110	5	3	M1	6000	0.037	D	1
			[306.80]	341170	667110	3	3	M1	6000	0.022	D-	1
			-	-	-	3	3	E2	23	1.1(-4) <sup>a</sup>	D-	2
			[286.51]	318080	667110	1	3	M1	1.1(+4)	0.030	D	1
3.	2p <sup>2</sup> -2p <sup>2</sup>	'P - 'P	[2777.0]	911130	947130	3	5	M1	520	2.07	C	1
			[2156.8]	864780	911130	1	3	M1	1720	1.92	C	1
4.		'P - 'D	[955.29]	947130	1051810	5	5	M1	6800	1.1	D+	1
			[710.83]	911130	1051810	3	5	M1	6300	0.42	D+	1
5.		'P - 'S	[290.99]	311130	1254790	3	1	M1	9.2(+4)	0.084	D	1

<sup>a</sup>The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

Cr XXII

Li Isoelectronic Sequence

Ground State: 1s<sup>2</sup>2s <sup>1</sup>S<sub>1/2</sub>

Ionization Energy: 1721.4 eV = 13882000 cm<sup>-1</sup>

Allowed Transitions

List of tabulated lines

Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.	Wavelength (Å)	No.
2.190	5	8.04	17	9.493	8	26.8	18
2.191	2	8.07	10	9.809	14	27.5	22
2.196	1	8.10	17	9.865	14	27.7	22
2.198	4	8.20	16	12.623	7	28.0	22
2.199	1,3,4	8.27	16	12.664	7	222.96	6
2.202	3	8.52	9	13.149	13	279.74	6
2.208	4	8.78	15	13.292	13		
7.82	11	8.85	16	13.208	13		

Transition probabilities for the strongest inner-shell transitions to doubly excited  $n = 2$  states are taken from the multiconfiguration Dirac-Fock (MCDF) calculations of Hata and Grant.<sup>1</sup> Their results are in good agreement with the  $Z$ -expansion perturbation calculations of Vainshtein and Safronova,<sup>2</sup> who included relativistic corrections at the level of the Pauli approximation.

Oscillator strengths for lines of the principal ( $2s-2p$ ) resonance multiplet are the results of the MCDF calculations of Cheng *et al.*,<sup>3</sup> which include a perturbative treatment of the Breit interaction and the Lamb shift. The results of the MCDF calculations of Armstrong *et al.*<sup>4</sup> were interpolated to provide  $f$ -values for the  $2p-3d$  transitions.

The  $f$ -value for the  $3d-4f$  transition was taken from a study of systematic trends along isoelectronic sequences by Smith and Wiese.<sup>5</sup> The tabulated data for many additional transitions were taken from the theoretical analysis of Martin and Wiese,<sup>6</sup> which was based on a generalized study of systematic trends for several spectral series of the lithium isoelectronic sequence.

Results of the relativistic Hartree-Fock calculations of Kim and Desclaux<sup>7</sup> for several ions of the Li sequence were incorporated into the data of Ref. 6 for the  $2s-3p$  transitions. For all other transitions for which the results of Ref. 6 are quoted here, no relativistic calculations were available. However, the relativistic calculations of Younger and Weiss<sup>8</sup> for the hydrogen isoelectronic sequence provide a means of assessing the magnitude of relativistic corrections since the Li sequence is very similar in structure to the H sequence. For those transitions for which relativistic effects were estimated to be significant (specifically, whenever the ratio of the weighted relativistic hydrogenic  $f$ -values  $gf_A$  of any two lines within a multiplet was found to deviate from the corresponding  $LS$ -coupling line strength ratio by more than 5% for the appropriate value of the nuclear charge  $Z$ ), the  $f$ -values were excluded from the compilation. A more detailed discussion of this comparison is given in Ref. 6.

Although the  $2p-3s$  multiplet did not satisfy the criterion described in the paragraph above, we have nevertheless quoted the multiplet  $f$ -value obtained by Onello<sup>9</sup> using a  $Z$ -expansion technique based on a variational calculation for O VI that allowed for large-scale configuration interaction. The resulting multiplet oscillator strengths for Fe XXIV and Ni XXVI are in very good agreement with data derived from the results of calculations that included relativistic effects.<sup>10</sup> We thus felt that the results of Ref. 9 should be sufficiently accurate for inclusion in this compilation.

Transition probability data are available for numerous transitions involving doubly excited states with the spectator electron occupying the  $n=3$  shell, or higher.<sup>12</sup> These have not been tabulated, however, since they belong to, or are very close to belonging to, the unresolved satellites of the helium-like ion.

## References

- <sup>1</sup>J. Hata and I. P. Grant, *Mon. Not. R. Astron. Soc.* **211**, 549 (1984).
- <sup>2</sup>L. A. Vainshtein and U. I. Safronova, *At. Data Nucl. Data Tables* **21**, 49 (1978).
- <sup>3</sup>K. T. Cheng, Y.-K. Kim, and J. P. Desclaux, *At. Data Nucl. Data Tables* **24**, 111 (1979).
- <sup>4</sup>L. Armstrong, Jr., W. R. Fielder, and D. L. Lin, *Phys. Rev. A* **34**, 1114 (1976).
- <sup>5</sup>M. W. Smith and W. L. Wiese, *Astrophys. J. Suppl. Ser.* **23**, No. 196, 103 (1971).
- <sup>6</sup>G. A. Martin and W. L. Wiese, *J. Phys. Chem. Ref. Data* **5**, 537 (1976).
- <sup>7</sup>Y.-K. Kim and J. P. Desclaux, *Phys. Rev. Lett.* **36**, 139 (1976) and private communication.
- <sup>8</sup>S. M. Younger and A. W. Weiss, *J. Res. Nat. Bur. Stand., Sect. A* **79**, 629 (1975).
- <sup>9</sup>J. S. Onello, *Phys. Rev. A* **11**, 743 (1975).
- <sup>10</sup>M. A. Hayes, *Mon. Not. R. Astron. Soc.* **189**, 55P (1979).
- <sup>11</sup>B. C. Fawcett, A. Ridgeley, and T. P. Hughes, *Mon. Not. R. Astron. Soc.* **188**, 365 (1979).
- <sup>12</sup>L. A. Vainshtein and U. I. Safronova, *At. Data Nucl. Data Table* **25**, 311 (1980).

Cr XIII: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (st. u.)	log $gf$	Accuracy	Source								
1.	$1s^22s-1s(^2S)2p(^2P)$	$^2S - ^2P$	2.196			2	6	4.1(+5) <sup>a</sup>	0.000	0.0013	-0.75	D	1								
														2	4	3.4(+4)	0.0049	7.1(-5)	-2.01	D	1
														2	2	1.1(+6)	0.000	0.0012	-0.80	C	1
2.	$1s^22s-1s(^2S)2p(^1P)$	$^2S - ^2P$	[2.191]			2	2	2.5(+6)	0.18	0.0028	-0.44	C	1								
3.	$1s^22p-1s2p^1$	$^2P - ^2D$	[2.202]			4	6	1.6(+6)	0.17	0.0061	-0.16	C	1								
														2	4	2.9(+6)	0.28	0.0048	-0.18	C	1

Cr XXX: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ ( $\text{cm}^{-1}$ )	$E_2$ ( $\text{cm}^{-1}$ )	$g_1$	$g_2$	$A_{21}$ ( $10^6 \text{ s}^{-1}$ )	$f_{12}$	$S$ (at. u.)	$\log gf$	Accuracy	Source
4.		$^3P - ^3P$	[2.196]			4	4	4.5(+6)	0.33	0.0094	0.12	C	1
			[2.199]			2	2	3.9(+6)	0.28	0.0041	-0.25	C	1
			[2.203]			4	2	1.3(+6)	0.047	0.0014	-0.72	C	1
5.		$^3P - ^3S$	[2.190]			4	2	1.7(+6)	0.061	0.0018	-0.61	C	1
6.	2s-2p	$^3S - ^3P$	239.15	0	418140	2	6	26.4	0.0630	0.107	-0.867	B+	3
			222.98	0	448470	2	4	32.9	0.0490	0.0719	-1.009	B+	3
			279.74	0	357470	2	2	16.5	0.0122	0.0055	-1.413	B+	3
7.	2s-3p	$^3S - ^3P$	12.637	0	7913500	2	6	5.19(+4)	0.373	0.0310	-0.128	E	6
			12.623	0	7922000	2	4	5.13(+4)	0.245	0.0204	-0.310	E	6
			12.664	0	7896400	2	2	5.28(+4)	0.127	0.0106	-0.595	B	6
8.	2s-4p	$^3S - ^3P$	9.493	0	10530000	2	6	2.5(+4)	0.10	0.0063	-0.70	C+	6
9.	2s-5p	$^3S - ^3P$	[8.52]			2	6	1.2(+4)	0.040	0.0022	-1.10	C+	6
10.	2s-6p	$^3S - ^3P$	[8.07]			2	6	7240	0.0212	0.00113	-1.373	C+	6
11.	2s-7p	$^3S - ^3P$	[7.82]			2	6	4510	0.0124	6.38(-4)	-1.606	C+	6
12.	2p-3s	$^3P - ^3S$	13.54	418140	7805000	6	2	1.9(+4)	0.017	0.0045	-0.99	D	9
13.	2p-3d	$^3P - ^3D$	13.245	418140	7963100	6	10	1.54(+5)	0.677	0.177	0.608	B	interp.
			13.292	448470	7971800	4	6	1.54(+5)	0.611	0.107	0.388	B	interp.
			13.149	357470	7962600	2	4	1.29(+5)	0.671	0.0581	0.128	B	interp.
			[13.308]	448470	7962600	4	4	2.6(+4)	0.068	0.012	-0.57	B	interp.
14.	2p-4d	$^3P - ^3D$	9.852	418140	10570000	6	10	4.9(+4)	0.12	0.023	-0.14	B	6
			9.865	448470	10590000	4	6	4.9(+4)	0.11	0.014	-0.37	B	ls
			9.809	357470	10550000	2	4	4.1(+4)	0.12	0.0077	-0.62	B	ls
			9.865	448470	10550000	4	4	7900	0.012	0.0015	-1.24	C+	ls
15.	2p-5d	$^3P - ^3D$	8.83			6	10	2.31(+4)	0.0450	0.00785	-0.569	C+	6
			[8.85]			4	6	2.29(+4)	0.0404	0.00471	-0.791	C+	ls
			[8.78]			2	4	1.96(+4)	0.0453	0.00282	-1.043	C+	ls
			[8.85]			4	4	3800	0.0045	5.2(-4)	-1.75	D	ls
16.	2p-6d	$^3P - ^3D$	8.35			6	10	1.26(+4)	0.0220	0.00363	-0.879	C+	6
			[8.37]			4	6	1.26(+4)	0.0198	0.00218	-1.102	C+	ls
			[8.30]			2	4	1.07(+4)	0.0221	0.00121	-1.354	C+	ls
			[8.37]			4	4	2100	0.0022	2.4(-4)	-2.06	D	ls
17.	2p-7d	$^3P - ^3D$	8.08			6	10	7720	0.0126	0.00201	-1.121	C+	6
			[8.10]			4	6	7690	0.0113	0.00121	-1.343	C+	ls
			[8.04]			2	4	6530	0.0127	6.7(-4)	-1.597	C+	ls
			[8.10]			4	4	1200	0.0012	1.3(-4)	-2.31	D	ls
18.	3s-4p	$^3S - ^3P$	[26.8]	7805000	10630000	2	6	7100	0.43	0.10	-0.07	C	6



Cr III: Allowed transitions - Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_u$ (cm <sup>-1</sup> )	$E_l$ (cm <sup>-1</sup> )	$g_u$	$g_l$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_u$	S (m.u.)	log $g^l$	Accuracy	Source
19.	3-5p	3S - 3P				2	6		0.187		-0.87	C	6
20.	3-5p	3S - 3P				2	6		0.047		-1.08	C	6
21.	3-7p	3S - 3P				2	6		0.0009		-1.908	C	6
22.	3p-4d	3P - 3D	37.6	7913300	16570000	6	10	1.7(+0)	0.59	0.44	0.55	B	6
			[37.5]	7922000	16580000	4	6	1.7(+0)	0.58	0.26	0.22	B	6
			[37.7]	7906400	16550000	2	4	1.4(+0)	0.60	0.15	0.08	B	6
			[38.0]	7922000	16550000	4	4	2700	0.055	0.029	-0.53	C+	6
23.	3p-5d	3P - 3D				6	10		0.136		-0.882	C+	6
24.	3p-6d	3P - 3D				6	10		0.0553		-0.475	C+	6
25.	3p-7s	3P - 3S				6	2		0.0013		-1.97	C-	6
26.	3p-7d	3P - 3D				6	10		0.0220		-0.761	C+	6
27.	3d-4f	3D - 3F				10	14		1.00		1.000	B	5
28.	4s-5p	3S - 3P				2	6		0.473		-0.824	C	6
29.	4s-6p	3S - 3P				2	6		0.123		-0.59	C	6
30.	4s-7p	3S - 3P				2	6		0.056		-0.95	C	6
31.	4p-5d	3P - 3D				6	10		0.583		0.544	C+	6
32.	4p-6d	3P - 3D				6	10		0.141		-0.073	C+	6
33.	4p-7s	3P - 3S				6	2		0.0060		-1.44	C-	6
34.	4p-7d	3P - 3D				6	10		0.0516		-0.432	C+	6

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XXII

## Forbidden Transitions

The single magnetic dipole transition within the  $1s^2 2p$  configuration has the line strength of 1.33 in the absence of relativistic effects in the wavefunctions.<sup>1</sup> It is estimated that these effects are negligible, since comprehensive relativistic calculations by Cheng *et al.*<sup>2</sup> for the analogous transition in the  $1s^2 2s^2 2p$  configuration of the boron sequence show that such relativistic corrections are negligible until much more highly charged ions.

The listed transition probability data are also expected to be quite accurate since the energy levels are derived from experimental data.

An electric quadrupole transition at the same wavelength is estimated to be of negligible strength, as calcu-

lated by Bhatia<sup>3</sup> for this transition in the case of Mn XXIII. (He obtains a ratio of about  $10^{-3}$  for the ratio of E2 to M1 line strengths).

## References

<sup>1</sup>W. L. Wiese, M. W. Smith, and B. M. Miles, "Atomic Transition Probabilities", Vol. II, NSRDS-NBS 22, U.S. Govt. Print. Office, Washington, DC 1969.

<sup>2</sup>K. T. Cheng, Y.-K. Kim, and J. P. Descloux, *At. Data Nucl. Data Tables* 24, 111 (1979).

<sup>3</sup>A. K. Bhatia, private communication (1986).

Cr XXII: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (at. u.)	Accuracy	Source
1.	$2p-2p$	$^3P^o - ^3P^o$	[1098.9]	357470	448470	2	4	M1	6760	1.33	B	<i>interp.</i>

## Cr XXIII

## He Isoelectronic Sequence

Ground State:  $1s^2\ ^1S_0$ Ionization Energy:  $7481.8\text{ eV} = 60344000\text{ cm}^{-1}$ 

## Allowed Transitions

## List of tabulated lines

Wavelength ( $\text{\AA}$ )	No.	Wavelength ( $\text{\AA}$ )	No.	Wavelength ( $\text{\AA}$ )	No.	Wavelength ( $\text{\AA}$ )	No.
1.7235	17	2.107	3,7,10	9.0513	31	35.722	45
1.7238	16	2.109	7	9.2126	32	74.234	55
1.7632	15	2.113	9	11.852	21	74.878	56
1.7640	14	2.119	5	12.093	22	76.447	58
1.8557	13	2.129	6	12.271	27	77.226	59
1.8578	12	2.1818	2	12.512	73	225.3	19
2.095	11	2.1923	1	23.553	41	326.3	18
2.101	4,8	7.9233	25	23.820	42	462.9	18
2.102	3	8.0619	26	23.979	48	467.5	20
2.103	7	8.0762	35	24.265	49	471.0	18
2.104	7	8.2126	36	34.193	39		
2.105	7	8.8497	23	34.609	40		
2.106	3	9.0127	24	35.256	44		

Oscillator strengths for transitions of the  $1s^2-1s2p$  array are taken from the results of Drake,<sup>1</sup> who incorporated accurate nonrelativistic matrix elements and Dirac hydrogenic matrix elements into a  $Z$ -expansion technique in order to provide  $f$ -values which would accurately reflect correlation effects for low- $Z$  ions and relativistic effects for high- $Z$  ions of the helium isoelectronic sequence. The  $f$ -values for the  $1s^2\ ^1S - 1snp\ ^3P$  ( $n=3-5$ ) transitions were interpolated from results of the relativistic random phase approximation (RRPA) calculations of Johnson and Lin.<sup>2</sup> Data for other  $s-p$  and  $p-s$  transitions were interpolated from the RRPA results of Lin *et al.*,<sup>3</sup> with the exception of the  $2s-2p$  transitions, where we tabulate the actual published RRPA  $A$ -values of these same authors.<sup>4</sup>

The charge expansion results of Laughlin<sup>5</sup> are given for various  $p-d$  and  $d-p$  transitions, as well as transitions between  $4d$  and  $4f$  levels. For those multiplets involving no change in principal quantum number ( $3p-3d$ ,  $4p-4d$ ,  $4d-4f$ ) the  $f$ -values should be considered rather uncertain, since they are sensitive to energy differences. Oscillator strengths for the  $2p-3d$  transitions, and for  $1s3p\ ^3P - 1s3d\ ^3D$ , were interpolated from the variational calculations of Weiss.<sup>6</sup> Both of these calculations indicate that, unlike the triplets, the  $nd\ ^3D$  energy levels ( $n=3,4$ ) lie below the  $np\ ^3P$  levels, and the  $4f\ ^3F$  lies below the  $4d\ ^3D$ .

Brown and Cortez<sup>7</sup> have provided  $f$ -values for numerous  $d-f$  and  $f-d$  transitions for the isoelectronic sequence

by fitting  $Z$ -expansion formulas to the results of variational calculations for the low- $Z$  ions. Their results for transitions between the lower-lying  $D$  and  $F^o$  terms are tabulated here.

Transition probabilities for the stronger transitions involving the doubly excited  $n=2$  states are taken from the comprehensive, charge expansion perturbation theory calculations of Vainshtein and Safronova.<sup>8</sup> Numerous data are also available for transitions involving doubly excited states where the spectator electron has principal quantum number  $n=3$ .<sup>9</sup> However, these data are not tabulated here since most of the transitions are very close to belonging to the unresolved satellites of the H-like ions, if they do not in fact do so.

## References

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- L. A. Vainshtein and U. I. Safronova, *At. Data Nucl. Data Tables* **28**, 311 (1980).

## Cr XIII: Allowed transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_u$ (cm <sup>-1</sup> )	$E_l$ (cm <sup>-1</sup> )	$g_u$	$g_l$	$A_{ul}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{ul}$	$S$ (a. u.)	log $gf$	Accuracy	Source
1.	1s <sup>2</sup> -1s2p	'S - 'P'	[2.1923]	0	[45614900]	1	3	2.34(+5)	0.0505	3.64(-4)	-1.297	B	1
2.		'S - 'P'	[2.1818]	0	[45832900]	1	3	3.37(+6)	0.721	0.00518	-0.142	B	1
3.	1s2s-2s2p	'S - 'P'	2.104	[45389100]	[92920000]	3	9	2.1(+6)	0.41	0.0085	0.09	C	8
			[2.102]	[45389100]	[92960000]	3	5	2.1(+6)	0.23	0.0048	-0.16	C	8
			[2.106]	[45389100]	[92870000]	3	3	2.0(+6)	0.13	0.0028	-0.40	C	8
			[2.107]	[45389100]	[92850000]	3	1	2.0(+6)	0.044	9.2(-4)	-0.88	C	8
4.		'S - 'P'	[2.101]	[45619000]	[93220000]	1	3	2.0(+6)	0.40	0.0027	-0.40	C	8
5.	1s2p-2s <sup>2</sup>	'P' - 'S											
			[2.119]	[45614900]	[92800000]	3	1	2.7(+5)	0.0061	1.3(-4)	-1.74	D	8
6.		'P' - 'S	[2.129]	[45832900]	[92800000]	3	1	5.1(+5)	0.012	2.4(-4)	-1.46	D	8
7.	1s2p-2p <sup>2</sup>	'P' - 'P	2.106	[45658200]	[93140000]	9	9	3.9(+6)	0.26	0.016	0.36	D+	8
			[2.107]	[45695600]	[93160000]	5	5	2.3(+6)	0.15	0.0053	-0.12	C	8
			[2.105]	[45614900]	[93130000]	3	3	9.6(+5)	0.064	0.0013	-0.72	D	8
			[2.109]	[45695600]	[93130000]	5	3	1.7(+6)	0.068	0.0024	-0.47	C	8
			[2.107]	[45614900]	[93070000]	3	1	3.8(+6)	0.084	0.0018	-0.60	C	8
			[2.103]	[45614900]	[93160000]	3	5	1.2(+6)	0.13	0.0028	-0.40	C	8
			[2.104]	[45601400]	[93130000]	1	3	1.4(+6)	0.28	0.0019	-0.55	C	8
8.		'P' - 'D											
			[2.101]	[45695600]	[93290000]	5	5	7.9(+5)	0.052	0.0018	-0.58	D	8
9.		'P' - 'P											
			[2.113]	[45832900]	[93160000]	3	5	5.9(+5)	0.066	0.0014	-0.70	D	8
10.		'P' - 'D	[2.107]	[45832900]	[93290000]	3	5	3.3(+6)	0.37	0.0076	0.04	C	8
11.		'P' - 'S	[2.095]	[45832900]	[93560000]	3	1	3.5(+6)	0.077	0.0016	-0.64	C	8
12.	1s <sup>2</sup> -1s3p	'S - 'P'											
			[1.8578]	0	[53826600]	1	3	8.4(+4)	0.013	8.0(-5)	-1.89	E	interp.
13.		'S - 'P'	[1.8557]	0	[53888200]	1	3	8.97(+5)	0.139	8.49(-4)	-0.857	C+	interp.
14.	1s <sup>2</sup> -1s4p	'S - 'P'											
			[1.7640]	0	[56688900]	1	3	3.2(+4)	0.0045	2.6(-5)	-2.35	E	interp.
15.		'S - 'P'	[1.7632]	0	[56714400]	1	3	3.68(+5)	0.0514	2.98(-4)	-1.289	C+	interp.
16.	1s <sup>2</sup> -1s4p	'S - 'P'											
			[1.7238]	0	[58010100]	1	3	1.6(+4)	0.0022	1.2(-5)	-2.66	E	interp.

Cr XIII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ ( $\text{cm}^{-1}$ )	$E_2$ ( $\text{cm}^{-1}$ )	$g_1$	$g_2$	$A_{21}$ ( $10^8 \text{ s}^{-1}$ )	$f_{12}$	$S$ (at. u.)	$\log gf$	Accuracy	Source
17.		'S - 'P'	[1.7235]	0	[58023100]	1	3	1.86(+5)	0.0248	1.41(-4)	-1.606	C+	interp.
18.	1s2s-1s2p	'S - 'P'	371.6	[45389100]	[45658200]	3	9	6.71	0.0417	0.153	-0.903	B	4
			[326.3]	[45389100]	[45695600]	3	5	10.1	0.0269	0.0866	-1.094	B	4
			[442.9]	[45389100]	[45614900]	3	3	3.80	0.0112	0.0489	-1.475	B	4
			[471.0]	[45389100]	[45601400]	3	1	3.36	0.00372	0.0173	-1.952	B	4
19.		'S - 'P'	[225.3]	[45389100]	[45832900]	3	3	1.93	0.00147	0.00327	-2.356	B	4
20.		'S - 'P'	[467.5]	[45619000]	[45832900]	1	3	3.32	0.0326	0.0502	-1.486	B	4
21.	1s2s-1s3p	'S - 'P'											
			[11.852]	[45389100]	[53826600]	3	3	5.8(+4)	0.123	0.0144	-0.433	C	interp.
22.		'S - 'P'	[12.093]	[45619000]	[53888200]	1	3	5.6(+4)	0.368	0.0147	-0.434	C	interp.
23.	1s2s-1s4p	'S - 'P'											
			[8.8497]	[45389100]	[56688900]	3	3	2.6(+4)	0.030	0.0026	-1.05	C+	interp.
24.		'S - 'P'	[9.0127]	[45619000]	[56714400]	1	3	2.4(+4)	0.089	0.0026	-1.05	C+	interp.
25.	1s2s-1s5p	'S - 'P'											
			[7.9233]	[45389100]	[58010100]	3	3	1.3(+4)	0.012	9.4(-4)	-1.44	C+	interp.
26.		'S - 'P'	[8.0619]	[45619000]	[58023100]	1	3	1.3(+4)	0.037	9.8(-4)	-1.43	C+	interp.
27.	1s2p-1s3s	'P' - 'S'											
			[12.271]	[45614900]	[53764300]	3	3	6200	0.014	0.0017	-1.38	C-	interp.
28.		'P' - 'S'	[12.512]	[45832900]	[53825000]	3	1	1.9(+4)	0.015	0.0019	-1.35	C+	interp.
29.	1s2p-1s3d	'P' - 'D'					9	15	0.69		0.79	C+	interp.
30.		'P' - 'D'					3	5	0.70		0.32	C+	interp.
31.	1s2p-1s4s	'P' - 'S'											
			[9.0513]	[45614900]	[56663000]	3	3	2500	0.0031	2.8(-4)	-2.03	D	interp.
32.		'P' - 'S'	[9.2126]	[45832900]	[56687600]	3	1	7300	0.0031	2.8(-4)	-2.03	C	interp.
33.	1s2p-1s4d	'P' - 'D'					9	15	0.12		0.03	C	5
34.		'P' - 'D'					3	5	0.12		-0.44	C	5
35.	1s2p-1s5s	'P' - 'S'											
			[8.0762]	[45614900]	[57997000]	3	3	1300	0.0013	1.0(-4)	-2.41	D	interp.

Cr XXIII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{21}$ (10 <sup>8</sup> s <sup>-1</sup> )	$f_{\lambda}$	$S$ (at. u.)	log $g^f$	Accuracy	Source
36.		'P - 'S	[8.2126]	[45832900]	[58009300]	3	1	3900	0.0013	1.1(-4)	-2.41	C	interp.
37.	1s3s-1s3p	'S - 'P				3	3		0.018		-1.27	E	interp.
38.		'S - 'P				1	3		0.057		-1.24	D	interp.
39.	1s3s-1s4p	'S - 'P	[34.193]	[53764300]	[56688900]	3	3	7800	0.136	0.0659	-0.389	C	interp.
40.		'S - 'P	[34.609]	[53825000]	[56714400]	1	3	7500	0.405	0.0461	-0.393	C	interp.
41.	1s3s-1s5p	'S - 'P				3	3		0.035	0.0081	-0.98	C	interp.
42.		'S - 'P	[23.553]	[53764300]	[58010100]	3	3	4200	0.035	0.0081	-0.98	C	interp.
43.	1s3p-1s3d	'P - 'D	[23.820]	[53825000]	[58023100]	1	3	4080	0.104	0.00816	-0.983	C+	interp.
44.	1s3p-1s4s	'P - 'S				9	15		0.012		-0.97	D	interp.
45.		'P - 'S	[35.256]	[53826600]	[56663000]	3	3	1800	0.033	0.011	-1.00	C-	interp.
46.	1s3p-1s4d	'P - 'D	[35.722]	[53888200]	[56687600]	3	1	5300	0.034	0.012	-0.99	C	interp.
47.		'P - 'D				9	15		0.60		0.73	C	5
48.	1s3p-1s5s	'P - 'S				3	5		0.62		0.27	C	5
49.		'P - 'S	[23.979]	[53826600]	[57997000]	3	3	8%	0.0077	0.0018	-1.64	D	interp.
50.	1s3d-1s3p	'D - 'P	[24.265]	[53888200]	[58009300]	3	1	2600	0.0077	0.0018	-1.64	C	interp.
51.	1s3d-1s4p	'D - 'P				5	3		0.0022		-1.96	F	5
52.		'D - 'P				15	9		0.012		-0.74	C	5
53.	1s4s-1s4p	'S - 'P				5	3		0.011		-1.26	C	5
54.		'S - 'P				3	3		0.025		-1.12	E	interp.
55.	1s4s-1s5p	'S - 'P				1	3		0.080		-1.10	F	interp.
56.		'S - 'P	[74.234]	[56663000]	[58010100]	3	3	1830	0.151	0.111	-0.344	C	interp.
57.	1s4s-1s4d	'P - 'D	[74.878]	[56687600]	[58023100]	1	3	1800	0.45	0.11	-0.35	D	interp.
58.	1s4p-1s5s	'P - 'S				9	15		0.021		-0.72	D	5
		'P - 'S	[76.447]	[56688900]	[57997000]	3	3	630	0.055	0.042	-0.78	D	interp.

Cr XXIII: Allowed transitions — Continued

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	$A_{ul}$ (10 <sup>6</sup> s <sup>-1</sup> )	$f_{os}$	$S$ (n. u.)	log $gf$	Accuracy	Source
59.		'P' - 'S	[77.226]	[56714400]	[58009300]	3	1	1800	0.055	0.042	-0.78	C	<i>interp.</i>
60.	1s4d-1s4p	'D' - 'P'				5	3		0.0034		-1.77	E	5
61.	1s4d-1s4f	'D' - 'F'				15	21		8.5(-4)		-1.89	E	5
62.	1s4d-1s5f	'D' - 'F'				15	21		0.89		1.13	B	7
63.		'D' - 'F'				5	7		0.89		0.65	B	7
64.	1s4f-1s4d	'F' - 'D'				7	5		4.5(-4)		-2.50	E	5
65.	1s4f-1s5d	'F' - 'D'				21	15		0.0089		-0.73	C	7
66.		'F' - 'D'				7	5		0.0089		-1.21	C	7
67.	1s5s-1s5p	'S' - 'P'				3	3		0.031		-1.03	E	<i>interp.</i>
68.		'S' - 'P'				1	3		0.10		-1.00	E	<i>interp.</i>

\*The number in parentheses following the tabulated value indicates the power of ten by which the value has to be multiplied.

Cr XXIII

Forbidden Transitions

The results of multi-configuration Dirac-Fock calculations by Hata and Grant<sup>1</sup> have been selected for this tabulation. Their work includes both a very detailed consideration of configuration interaction—with configurational wavefunction sets containing as many as 51 interacting states—as well as a fully relativistic treatment based on the Dirac Hamiltonian. Their calculated wavelengths are in very close agreement with experiment, and the agreement between an experimentally determined lifetime<sup>2</sup> for the 2p <sup>3</sup>P<sub>2</sub> state and the theoretical

result is excellent, the difference being only 5%. A comprehensive comparison table containing all experimental data on these He-sequence transitions is given in the introduction to the forbidden lines of Ti XXI.

References

<sup>1</sup>J. Hata and I. P. Grant, Mon. Not. R. Astr. Soc. 211, 549 (1984).  
<sup>2</sup>H. D. Dohmann, R. Mann, and E. Pfeng, Z. Phys. A 269, 101 (1982).

Cr XXIII: Forbidden transitions

No.	Transition Array	Multiplet	$\lambda$ (Å)	$E_1$ (cm <sup>-1</sup> )	$E_2$ (cm <sup>-1</sup> )	$g_1$	$g_2$	Type of transition	$A_{ul}$ (s <sup>-1</sup> )	$S$ (n. u.)	Accuracy	Source
1.	1 <sup>2</sup> -1s2s	'S' - 'S'	[2.2034]	0	[45383500]	1	3	M1	9.37(+7) <sup>2</sup>	1.11(-4)	B	1
2.	1s <sup>2</sup> -1s2p	'S' - 'P'	[2.1886]	0	[45691370]	1	5	M2	3.45(+9)	0.131	B	1

\*The number in parentheses following the tabulated value indicates the power of ten by which this value has to be multiplied.

## Cr XXIV

## H Isoelectronic Sequence

Ground State:  $1s^2 S_{1/2}$ Ionization Energy:  $7894.87 \text{ eV} = 63675900 \text{ cm}^{-1}$ 

## Allowed Transitions

Electric dipole transition probability data for this hydrogen-like ion can be obtained directly, in a non-relativistic approximation, from the data for neutral hydrogen.<sup>1</sup> The oscillator strength is independent of  $Z$  along the entire isoelectronic sequence and is therefore identical to the value for the hydrogen atom. Line strengths scale as  $Z^{-2}$  and transition probabilities scale as  $Z^4$ , i.e.,

$$S_Z = Z^{-2} S_H, \quad A_Z = Z^4 A_H.$$

For higher nuclear charges in this sequence, relativistic corrections will cause these values to deviate increasingly from the non-relativistic ones. The first effect of relativity will be to alter the transition energies, or wavelengths, from the non-relativistic, even though the line strength itself is still well approximated by the non-relativistic value. In this case, experimental energies should be used in the standard conversion formulas, given in the general introduction to this volume, to calculate the most accurate values of  $f$  and  $A$ . It should be noted that the relativistic removal of the  $j$ -degeneracy introduces dipole transitions which do not occur in the non-relativistic theory, e.g.,  $2s_{1/2} - 2p_{1/2}$ .

For very high  $Z$ , it is necessary to use the four-component Dirac spinors rather than two-component Schroedinger functions in theoretical calculations, and this introduces relativistic corrections to the line strengths themselves. Several recent systematic studies of the problem<sup>2,3</sup> indicate that these corrections are not large for stages of ionization in the range 20-30. Corrections for  $Z = 30$  are usually no larger than 5-10% and generally substantially less than 5%. If an accuracy greater than this is required, the reader is referred to these papers<sup>2,3</sup> for a more detailed error analysis.

## References

- <sup>1</sup>W. L. Wiese, M. W. Smith, and B. M. Glennon, *Atomic Transition Probabilities - Hydrogen through Neon (A Critical Data Compilation)*, Vol. I, 157 pp., Nat. Stand. Ref. Data Ser., Nat. Bur. Stand. (U.S.), 4 (May 1966).
- <sup>2</sup>S. M. Younger and A. W. Weiss, *J. Res. Nat. Bur. Stand., Sect. A* 79, 629 (1975).
- <sup>3</sup>S. J. Rose, *Rutherford Appleton Laboratory Report RL-82-114* (December 1982).