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A STUDY FOR A 6 GeV UNDULATOR BASED SYNCHROTRON RADIATION SOURCE\*

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#### Abstract

A portial study for a 6 GeV unculator based synchrotron radiation source for production of high brightneos undulator radiation, in the A region, is presented. The basic lattice adopted for the storage ring is a hybrid FODO Chasman-Green lattice, making use of gradient in the dipoles. We discuss also the e beam current limits and the injection parameters.

#### Introduction

The actual trend for a large synchrotron radiation facility in to use a 6 GeV electron storage ring with a onall calttance of the electron beam and with a large number of straight section for the insertion of wiggler and undulators. A complete and detailed design for this kind of facility has been carried out by the ESRP group,<sup>1</sup> The European design is based on the Chasman-Groon<sup>2</sup> lattice that has been studied extensively. Prom The European design is based on the Chasmanthis study a number of problems associated with a low coltrance C-G lattice were in evidence, and study of possible alternate magnetic lattices became important.

For these reasons we present here a study of a acorage ring based on a magnetic structure recently proposed. The point that we want to emphasize is that wa try to pursue, where it is possible, a principle of simplicity for the architecture of the machine suggested not only by cost considerations but also by the requirement of relatively easy commissioning and operation. In addition the possibility to operate the Cachine at higher energy is kept open.

### Characteristics of the Storage Ring

The lattice of the storage ring consists of 28 poriods with 28 six meter long straight sections. One half of the standard cell is characterized by the following magnetic sequence:

$$\frac{0}{2}$$
, QF1,QD1,B.SD,  $\frac{QF}{2}$ , SF,  $\frac{C^{*}}{2}$ , SD,  $\frac{B}{2}$ 

ond has reflection symmetry. The dipoles have a verticol focusing gradient with a field index n = 106.4.

The layout of one poriod is shown in Fig. 1:

acഹരം -000 

### 33.58 meters

Fig. 1. Layout of one period.

The period length is 33.67 m with 20.35 m of free space and this ollows easy extraction of the radiation from the incertion devices, as well as from the bending magneto. The optical functions and the beam dimensions for one period are plotted in Fig. 2 and Fig. 3, respectively, while the main ring parameters are listed in Table I.



Fig. 2. 8 and off-energy n functions for one period.



Fig. 3. Horizontal and vertical r.m.s. electron beam dimensions for one period and for 10% coupling.

Table I. Main Rin	ng Parameters.
Energy	6 Gev
Circumference	942.78 .
Persode	29
Long etroighte	29x6 =
No of Dipolee	84x2, 24 m
Dipole field	6683 G
Dipole centrol gap	48 🚥
Hognetic radiue	29, 947
Field index n	106.4
No of Guadrupolee	112x70 cm
	112x35 cm
Max field gradient	111.5 hG/m
No of Sextuppies	168x40 cm
Nor Field 2nd densy.	140 6/-2
Hor. betatron tune	31, 32
Ver. betatron tune	16.32
Enangy loss/turn	3.83 May
Energy spread	. 15
Homentus comp.	4.1410
Hor. maitt. (0 coupl)	4. 9x10 arrest
Damping timber Ta	6.97 mm
Tv	R. R. man
Té	6.30
Hor, not, chron,	-46.7
Ver. not. chros.	-91.2
Closed orbit more	
ampl. Factore POx	75 1000 54 6 5 5 5 5 5
P <del>B</del> x	2
Pay	92
PBy	20 📾
•	0

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<sup>&</sup>quot;Research aupported by the U.S. Department of Energy

The combined function dipoles should not be a serious problem because with a maximum field of -.67T at 6 GeV, a field indem n = 105.4 and a magnetic length of 2.24 m they can be regarded as conventional. We checked with the computer code POISSON that a deviation of -

 $10^{-6}$  from the ideal field chope at ± 20 cm could be easily achieved.

For the chromaticity correction we use 6 sextupoles/ period subdivided in two families. This approach gives a satisfactory chromatic behavior and dynamic sporture (see Fig. 4) and provides for enough flexibility to extend the number of somtupole families to possibly six for correcting the additional chromatic aborrations introduced by incorporating a variety of law  $\beta$  insertions.



Pig. 4. Dynamical aperture as obtained with PATRICIA<sup>4</sup> at the long attaight section midpoint for  $\Delta p/p = 12$ and with synchrotron socillations for a corrected value of chromaticity  $\xi_{\rm H} = \xi_{\rm V} = 0$ .

### Current Limits

The threshold total average current  $I_L$  and  $I_T$ 

for the <u>longitudinal and transverse coupled bunch</u> modes are given by

$$\frac{1}{\tilde{T}_{a}} = L \frac{\alpha \omega_{o}}{2\pi \epsilon v_{o}} \frac{\sigma_{\theta}^{2\nu - 2}}{\sigma^{2}} R_{L,eff}^{(\nu,6)},$$

and

$$\frac{1}{T_{y}} \approx I_{T} \frac{ec}{4\pi E v} \frac{c^{2\nu}}{2^{\nu} ul} R^{(\nu,0)}_{T,eff}$$

where  $T_{\theta}$ ,  $T_{y}$  are the synchrotron and betatron damp-ing times,  $v_{y}$  and  $v_{\theta}$  the vertical and synchrotron

tunes,  $\mu$  the head-tail code number, s the symmetrical coupled bunch code number, M the number of bunches and the effective resistances are related to the resistive parts,  $R_L(\omega)$  and  $R_T(\omega)$ , of the longitudinal and transverse impedance by

$$R_{L,eff}^{(\nu,0)} \frac{1}{2} (nHre)^{2\nu} - R_{L} [(nH + 0 + \nu v_{0})v_{0}]_{e}^{-(nHre)^{2}\sigma_{\theta}^{2}},$$

and

$$\sum_{T,eff}^{(\mu,\alpha)} \sum_{n} \left[ (nH+\alpha-v_{y} + \frac{\xi}{\alpha} v)^{2\mu} R_{T} \left[ (nH+\alpha-v_{y}+v_{\alpha}) \omega_{0} \right],$$

$$e\pip \left[ -(nH+\alpha-v_{y} + \xi v_{y}/\alpha)^{2} \sigma_{\theta}^{2} \right]$$

We course that the dominant source of the coupled bunch instabilities are the RF cavities, and base our colculations on the adoption of LEP-Cavity (350 MHz) of CERN or VUV-Cavity (50MHz) of BNL. The important peraoffic mode impedances for these cavities have been reported in Ref. (5), (6) and (7). To calculate  $T_g$ and  $T_y$ , we assume the energy loss due to the radiation of the insertion devices to be 30% of that at the dipole magnets. To specify the RF-voltage and the synchronous phase angle, we require the energy acceptance of the RF-bucket to be 10  $\sigma_E$ .

The RF voltage and the synchronous phase angle for the 350 MHz cavity are 6.1 MV and 126.5°, and those for 5 MHz cavity are 5.3 MV and 109.8°. The results of the calculations are listed in the following tables.

### Table II. Longitudinal Coupled Bunch Instabilities

		frf=350	MHZ	
PAR	MSITIC NO	DES	THRESHOLD (	LURHENT (mA
F (#Hz)	٩	R (Hohe)	<b>۱- مر</b>	<b>μ</b> =2
508	40600	1.30	81	10713
620	40700	0. 75	60	±169
1163	50400	0. 33	110	3640
1204	70400	0. 36	98	3027
1745	68500	0.37	71	1039
1990	68700	0, 20	120	1 350
		FRF=50 N	HZ	
507	20278	0.20	121	147D
85 <del>9</del>	5371	0.19	102	431
1300	14723	0.24	102	188
1447	9295	0.40	70	104
1539	9815	0.41	78	1 U <b>O</b>

### Table III. Transverse Coupled Bunch Instabilities

PA	RASITIC MC	DES	THRESHOLD	CURRENT (#A)
f(⊫34g)	0	R (Notve/w)	0-4	<u>ا م</u> ا
614	70800	18.0	45	5370
782	55800	19.4	42	1264
1072	50100	12. 4	69	
1325	68600	19.4	45	1137
1593	68600	5.2	172	31.174
		FRF%50 NH2		
507	20.279	00000		

FRF-350 HHZ

507	20279	. 00800	116700	1400000
579	2184	. 00065	1518500	140000000

The brood band impedance may cause fast head-tail instabilities. We adopt here a crude estimate for the transverse fast head-tail mode threshold current. We assume it to be that current which is large enough to cause the rigid dipole mode frequency shift to equal the synchrotron frequency. The broad band impedance is chosen to be that of a 0 = 1 resonance at frequency free = 2c/b with shunt longitudinal  $Z_n/n$  at resonance to be is given by

$$X_{T}(\ell) = 1.5 \frac{2c}{b^{2}} \frac{1}{2\pi f_{res}} \frac{1-2x^{2}}{2x^{2}+(1-2x^{2})^{2}}$$

where  $x = f/f_{reo}$  and b = 2 cm is the effective chamber radius.

The single threshold current thus obtained is 1.9 mA for 350 MHz RF frequency and 2.1 mA for 50 MHz RF frequency.

# Storage Ring e or e Accumulation Rates

For the beam injector for the storage ring two systom are under study. These are a (1) 150 May Microtron - 6 GeV fast cycling Booster Synchrotron electron accelerator combination and a (11) 200 MeV e Linac -800 MeV et Linac - 6 GeV Booster Synchrotron positron source. The reason for contemplating the use of posicrons for the generation of synchrotron radiation in the storage ring is because of the deleterious effects encountered in present electron storage rings due to ion trapping in the potential well of the electrons, both in terms of substantial decrease in beam lifetime and in reducing the synchrotron radiation source brightness.

The parameters of the Booster synchrotron and Microtron preinjector, for the case of electron utilization in the storage ring, are summarized in Table IV.

## Table IV. Booster Synchrotron Elementary Parameters

Reas onera:	6.0 GeV
Been Current	5 -04
	10 Hz
	1. 5x10 ** e-red
	1.7 10 <sup>-9</sup> e-rod
Ey	
Eroargy oproduc	207 7 -
Lincusterence	
Revolution frequency	1.01 M12
Preinjacion alcration (	
Energy	0.15 GeV
Internetty (~ 1 jungs pulse)	20 mA
(	40 mA
Eniconces. En • Ey	10 <sup>-7</sup> e-rad
Enargy epread	0.071
Radiofrequency: (homeonic number)	317. 2 HHz + (h=315)
No e/bunch . witibunch wode	3. 9≈10 <sup>8</sup>
he e/bunch , ringle bunch mode	7. 8x10 <sup>0</sup>
Energy loss/turn	4.67 MeV
RF voltage (max), (g=1.8)	7.3-9 HV
RE covition . 5 calle . (L=2, 32 e)	4

For the positron source option the use of a Linear Accelerator-Booster Synchrotron combination is considered. The parameters are based on the LEP positron source design.<sup>8</sup> Since, however, a substantially longer pulse length is required in the present case, the electron preaccelerator parameters are acaied by maintaining the total number of electrons incident on the converter target the same  $(10^{12}/pulse)$ . The resultant parameters of the positron source are given in Table V. Using these source parameters, the overall transfer parameters have been evaluated for both the e and e case and are listed in Table VI.

### Table V. Positron Source

16. 4

Electron orein weter	100 NV ~ 0.4 A
Electron Lingo	200 HeV - 0.16
Converter - electron on target	1012 /pules
Poettron Linoc	600 MeV
Repetition note	10 Hz
Posttron/Electron ratio (04/GeV)	. 009
Positron Lings - 85% 'bits'	0,8
(positron/alectron) المر	0.004
Poestron current	0.64 =A
E¤ = Ey ( <u>s</u> 895¥)	3. 2x10 <sup>®</sup> a-rod
Emergy eprecid ( <u>&lt;</u> 85% ) (+/-)	0.01

# Table VI. Beam Transfer Parameters

## L'ANLTIANNER L'AIRSLE ANNER L'ANLTIANNER

PRETRUESTOR	41 CROTEOR	ALCROTHON	LINAC
CHERRY (GEY)	0-15	0.15	0.716 3-0-818 7
CURRENT (AÅ)	20	40	0.64
awar IFRATH (BSEC)	1	0-005	1
and note (W2)	10	10	10 (30)
6 . 6 (85%) (m.#AB)	1 10-7	2 10-*	3 10-4
(AC/E) (851) (+/-)	0.7 10-7	1 10-1	1 10-7
	(251)	(251)	(12-52)

## BORTER (E=6 GEV: C= 297-6 A: H= 315)

(	5	0-032	0-08	
PART/REAMS	3.1 10101	2-0 1 <b>0° c</b> ⊺	5-0 10° t	•
PAS"/BUCKET	1.0 10* **	2-0 10° £	1-6 10° €'	•
REP NATE (HZ)	10	10	10 (30)	
BOOSTED-STORAGE	ning ) (502)	(501)	(50%)	

### STORAGE RING (E = 6 GEV: C- 957-5 H. H = 1008)

Cusetst (#A)	200	)	10	200
PARTÉREAR	3.9 10	14 X	2.0 1011	3.9 1014
PART/BUCEET	3.9 10	•	2.0 10"	3.9 10°
	(418.) 0	. 43	3. 36	26.6(8.9)

### References

- 1. B. Buras, S. Tazzari, Report of the ESRP )1984).
- 2. R. Chasman, G. K. Green and M. Rowe, IEEE Trans.
- Nucl. Sci. <u>NS-22</u>, 1765 (1975).
- 3. G. Vignola, BNL Report 35678 (1984).
- 4. H. Wiedemann Report PEP 220 (1976).
- 5. D. Brandt, H. Henke, CERN LEP-Note 352 (1982).
- 6. A. Rofmann, K. Huebner, B. Zotter, IEEF Trans. Nucl. Sci. <u>NS-26</u>, 3514 (1979).
- 7. K. Batchelor, J. Galayda, B. Hawrylak, IEEE Trans. Nucl. Sci. <u>NS-28</u>, 2839 (1981).
- 8. LEP Design Report. CERN Staff Report LEP/TH/83-29.

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