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HIGH-YIELD HYDROGEN PRODUCTION BY CATALYTIC GASIFICATION OF COAL OR BIOMASS

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Abstract

Gasification of coal or wood, catalyzed by soluble metallic cations to maximize reaction rates and hydrogen yields, offers a potential for large-scale, economical hydrogen production with near-commercial technology. With optimum reaction conditions and catalysts, product gas rich in both hydrogen and methane can be used in fuel cells to produce electricity at efficiencies nearly double those of conventional power plant. If plantation silvaculture techniques can produce wood at a raw energy cost competitive with coal, further enhancement of product gas yields may be possible, with zero net contribution of CO_2 to the atmosphere.

1. INTRODUCTION

The rates of reactions in gasification of coal or wood are determined partially by their carbonaceous structure, but mainly by the quantity and chemical form of metallic elements, either inherent in their ash or added as catalysts. Reactivity is defined for the steam-char reaction $(C + H_2O \rightarrow H_2 + CO)$ as follows:

$$dC/dT = kC^n$$
 [Eq. 1]

where C = the remaining weight fraction of carbon in the reaction system.

- k = the reactivity rate constant, hr^{-1} .
- n = the order of reaction, approximately n = 1 in most cases.

This is the dominant reaction determining overall rates of coal gasification. Addition of salts or minerals high in mobile calcium, potassium, or sodium may increase reactivities by over an order of magnitude. This, in turn, can decrease gasifier residence time and thus the capital investment per throughput. Proper selection of these catalysts, as well as those containing iron, can result in product gases containing over 45% hydrogen and 10% methane in fluidized-bed gasifiers. The objective of ongoing programs at the Energy and Environmental Research Center (EERC) is to optimize catalyst selection and identify gasifier design problems by tests ranging from thermogravimetric analysis (TGA) of 20- to 50-mg samples to pilot plant operations of possibly 50 kg/hr (1-3). Reactivity is determined by TGA using 20- to 50-mg samples of coal (4-6) or wood (7). Proper catalyst selection can be a major factor in optimization of reaction rates and product gas compositions for the full range of coal-to-hydrogen applications shown in Figure 1.

The reactivity of low-rank coals (lignite and subbituminous) is intrinsically higher than that of bituminous coals because their ash levels tend to be high, with more metallic cations organically bound to the coal rather than as grains of stable minerals. In general, sodium and potassium are better catalysts than calcium, and all three are more effective to the extent of their chemical mobility (soluble, volatile, or ionized). The degree of reactivity enhancement by added catalyst is most striking with some bituminous coals and wood, where the addition of a high ratio of potassium ions to fixed carbon may increase the steam-char reaction rate by 350%. Selection of catalysts will be primarily a site-specific, and coal-specific, economic decision. Since most catalytic metals leave the gasifier as soluble salts, they can be recycled by ash leaching.

2. FFECTS OF CATALYSIS ON REACTIVITIES

Coals vary widely in their intrinsic or self-catalyzed reactivity, as shown in TGA data (dC/dt) in Figure 2, which is attributed to their ash content plus the kind and chemical form of metallic elements in it. Table I shows a comparison of analyses of several coals plus wood. The wood is hybrid poplar, which showed the greatest economic potential as an energy crop among species under study in the U.S. While ash content has no consistent correlation with geologic age, the proportion of metallic cations organically bound to the carbonaceous structure increases in younger coals. Wood, though a coal of zero age with all cations except silicon and aluminum in organically bonded form, fails to show a higher reactivity solely because of its extremely low ash levels. Table II shows TGA data for a variety of coals and wood, with the addition of various catalysts at various temperatures. Catalysis allows economic operation at a lower temperature, making gasification more energy efficient and permitting greater control over product gas composition. In Figure 3, further TGA data shows the effects of adding potassium-bearing catalysts to a subbituminous coal and wood to increase their reactivity at a common temperature. While underutilized low-rank coals (lignite and subbituminous) are attractive gasification feedstocks for hydrogen production, the greatest benefit of catalyst addition is with bituminous coals.

3. INTEGRATION OF CATALYTIC GASIFIERS WITH FUEL CELLS

With increased reactivity, gasifiers may operate at lower temperatures than would otherwise be feasible. Combined with higher pressures and iron-containing catalysts, this enables high levels of methane and hydrogen. Such gasifiers, integrated with advanced fuel cells, can produce electric power at overall efficiencies probably exceeding 60% (6,8,9). Thus could electric power could be produced from half the amount of coal required by conventional power plants, operating at 32-35% efficiency, producing half the CO₂ per kilowatt. Such a system is shown conceptually in Figures 4 and 5. In such a system, enhanced reactivity of bituminous coal, achieved by recycled potassium catalyst, could enable operation at around 650°C, which is an optimum temperature to promote the exothermic methanation reaction, $C + 2H_2 \rightarrow 2CH_4$, which is further encouraged at higher pressures. The advanced fuel cell oxidizes hydrogen to produce electricity and reduces methane at an electrode surface by the endothermic reaction shown in Figure 5, providing more hydrogen and cooling for the fuel cell, eliminating costly external cooling and heat recovery. Conveniently, the optimum operating temperature for this kind of fuel cell is also 650°C, which would eliminate the need for gas cooling. Thus, with the addition of an electrochemical hydrogen transfer device in the excess hydrogen return line, such a system can approach autothermal operation, reduce the number of heat transfer and energy recovery steps, greatly reduce the oxygen requirement, achieve higher conversion efficiencies, and reduce capital components. In supporting efforts at EERC [10] on catalyst selection for hydrogen-methane coproduction, preliminary results indicate some combination of mobile potassium and iron compounds may be optimal, with a fluidized bed of limestone.

4. PILOT-SCALE CATALYTIC GASIFICATION TESTS

Following TGA tests as an inexpensive screening step, further evaluation of catalysts and reactor conditions is done in EERC's small, continuous process unit shown schematically in Figure 6, originally used for pyrolysis research. Heat is supplied externally. To match this performance in a larger-scale gasifier requires the introduction of some oxygen and burning additional coal to supply heat, resulting in some product dilution by CO_2 . If the ideal autothermal operation

described above can be achieved oxygen will not be needed. Some preliminary results comparing the effects of temperature, pressure, and potassium impregnation on the gasification of Wyodak coal in a fluidized limestone bed are summarized in Table III, along with some corresponding data for wood, which was done first, under poorly controlled reactor conditions. These are the first two data sets generated by the experimental device in a newly modified configuration, however, and not part of orderly experimental matrix. Evaluation of data to determine yields is still in progress. The data of Table III is of present interest to show the high percentages of hydrogen and methane possible and their sensitivity to the four experimental parameters shown. The runs using coal proceeded smoothly, with steady-state conditions and no problems of feed plugging or bed agglomeration, as experienced in the earlier runs with wood chips. This confirms earlier observations, using larger gasifiers with coal, that a homogenous catalyst, impregnated onto the feed, avoids mechanical problems caused by heterogenous catalysts.

5. EXTENSION OF COAL GASIFICATION TECHNOLOGY TO BIOMASS

Coal gasification is well established commercially, with great reserves of nextgeneration technology available for accelerated development as favorable economic conditions arise or as national policies promote energy independence or greater conversion efficiency. Extension of this technology to wood depends only upon minor changes in component design and raising enough wood economically. Economic studies indicate that hybrid poplars can be grown and harvested by the year 2000 at a delivered energy cost comparable to the present upper limits of coal-mining The integrated gasifier-fuel cell concept [8,9] of Figure 4 is costs [11]. expected to achieve roughly twice the conversion efficiency of conventional coalfired power plants, thus halving the CO_2 emission per kW. Substituting wood for coal would eliminate CO2 completely. The key is finding enough suitable land to grow the trees. As a good example, the state of Minnesota, U.S.A., has significant areas of marginally utilized land that have demonstrated high growth rates of Populus species. The current population of about 3,388,600 has an annual power consumption of 13,560 kWhr per capita [12]. Assuming three observed levels of productivity [11], in annualized dry metric tons per hectare, conversion to electric power at 60% efficiency would require the plantation areas shown in Figure 7.

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INDEED I, ANALISES OF VARIOUS COALS AND WOOD							
	<u>Coal A¹</u>	<u>Coal B²</u>	<u>Coal C³</u>	Wood 4			
Geologic Age 1,000,000 Years	200-400	70-100	50-70	0			
Proximate, Wt% dry basis							
Volatiles (900°C) Fixed Carbon Ash	41 46 12	45 46 9	47 46 7	83 13 4-			
Ash, XRFA ⁵ , % as oxides							
SiO_2 Al_2O_3 Fe_2O_3 CaO MgO K_2O Na_2O SO_3 Other (P. Ti, Etc.)	44 18 18 8 1 3 0 7 1	26 13 7 24 9 1 3 15 2	38 14 8 14 5 1 3 15 2	$5.2 \\ 1.7 \\ 3.8 \\ 44.3 \\ 15.3 \\ 14.5 \\ 1.6 \\ 6.0 \\ 7.6 \\ $			

1 Typical bituminous, Illinois or Indiana

² Typical subbituminous, Wyoming.

³ Typical lignite, North Dakota.
 ⁴ Specific Hybrid Poplar, Experimental Plantation, NE Minnesota.
 ⁵ X-Ray Fluorescence, for elemental analysis.

TABLE II: REACTIVITY DATA FOR VARIOUS COALS AND WOOD (Reactivity, k^{-1} , as determined by TGA)

<u>Temperature,°C</u>	<u>650</u>	700	750	800
Bituminous Coal ¹				
Raw		0.07	0.14	0,33
+20% Limestone	ga uni		0.59	1.45
+10% K ₂ CO ₂			4.36	
+10% Limestone +10% K ₂ CO ₂			5.38	
+19% Hot Wood Ash Leachate		0.61	3.01	5,15
Subbituminous Coal ²				
Raw	0.37	1.16	1.31	3.06
+10% K ₂ CO ₃	1.25	4.3	8.24	13.48
Lignite ³				
Raw	0.30	1.35	2.10	3:56
+20% Limestone	0.48	0,81	6.49	15,50
+10% K ₂ CO ₃	1,35	4,06	8.17	34.90
Wood ⁴				
Raw		0.13	0.33	3.10
+10% Wood Ash		4,18	9.84	18.24

1, 2, 3, 4 - see TABLE I

TABLE III: CONTINUOUS PROCESS U FLUID	NIT GAS (IZED BED	COMPOSIT OF LIME	ION OF W STONE	YODAK CO	AL AND W	OOD IN
Wyodak Coal			·····			······································
Temperature, °C:	700	700	700	700	600	700
Pressure, Atm.:	2.4	6.1	2.4	2.4	2.4	2.4
Catalyst:	None	None	None	←4.4% KC	OH Impre	gnated→
Steam/Carbon, mol:	2	2	1	2	2	1
Product Gas, dry, inert-free						
%H ₂ %CO %CO ₂ %CH ₄ %C ₂ & C ₂₊ Hybrid Poplar Wood Temperature, °C: Pressure, Atm.:	56.8 6.0 29.3 7.7 0.2 600 2.4	62.6 0.7 26.9 9.5 0.3 650 2.4	58.6 8.2 25.0 8.0 0.3 700 2.4	63.1 8.7 25.4 2.7 0.0 700 4.4	60.0 2.1 28.7 9.0 0.3 650 4.4	56.2 16.6 19.6 7.5 0.2 650 7.8
Catalyst:	.	Dry	wood ash	, 30% of	feed	
Steam/Carbon, mol:	3,0	1.1	1.1	1.1	1.0	1.0
Product, Dry and Inert-Free						
%H ₂ %CO %CO ₂ %CH ₄	48.0 8.0 35.0 7.0	52.0 6.0 34.0 6.0	50.0 12.0 30.0 6.0	51.8 15.6 26.5 5.2	51.3 7.7 28.0 10.0	61.5 38.5
760 ₂ & 0 ₂₊	2.0	5.0	2.0	0.0	5.0	

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Fig. 1 - Multiple Markets for Hydrogen from Coal

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Fig. 3 - Effects of Potassium Catalyst Addition on Reactivities of Coals and Wood

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Fig. 4 - Catalytic Fluid-Bed Gasifier Integrated with Molten Carbonate Fuel Cell



Fig. 5 - Advanced Molten Carbonate Fuel Cell



Fig. 6 - EERC's Small, Pilot-Scale Continuous Process Unit



Fig. 7 - Biomass Potential for Electric Power Supply in Minnesota



