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**STOP BANDWIDTHS OF NONLINEAR
BEAM-BEAM RESONANCES**

G. PARZEN

December 8, 1979

ACCELERATOR DEPARTMENT

**BROOKHAVEN NATIONAL LABORATORY
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ABSTRACT

A general expression is given for the stop bandwidths, Δv , of nonlinear beam-beam resonances, which is expanded in powers of $y(s)$, the vertical beam orbit, and which is valid under certain assumptions regarding the orbits and charge distributions near the interaction regions. This result is applied to obtain results for the rms Δv due to random vertical orbit errors, and due to random errors in N_{β} at the crossing points. Numerical results are given for the ISABELLE storage accelerator.

I. INTRODUCTION

Results are derived for stop bandwidths, Δv_N , of nonlinear resonances due to the beam-beam interaction of horizontally crossing beams. A general result is first given for Δv_N , which involves only the charge distributions $\rho(x,y)$ and not the fields themselves, which is based on the assumptions that $\beta_y(s)$ can be regarded as constant in the interaction region, and that the beam paths near the crossing points may be curved vertically but are straight lines crossing at an angle α horizontally. Assuming that the charge distribution is Gaussian vertically, the result is expanded in powers of $y(s)$, the vertical orbit near the crossing points.

These general results are applied to obtain results for the, rms Δv_N , due to random vertical orbit errors, and due random errors in β_y at the crossing points. Numerical results are given for the ISABELLE storage accelerator.

II. THEORY and GENERAL RESULTS

The half-width of the stop band of the nonlinear resonance $Nv_y = q$ is given by the often derived formula¹⁻³

$$\Delta v_N = \frac{F(N)}{2^{N-2}} \frac{1 + \beta^2}{\beta} \frac{1}{4\pi} \int ds \frac{\beta_y}{B\rho} (\sqrt{\beta_y \epsilon})^{N-2} \frac{1}{(N-1)!} D_y^{N-1} E_y \exp(iN\phi), \quad (2.1)$$

where E_y is the field acting on the test beam due to the other beam and $D_y^n \equiv \partial^n / \partial y^n$. The factor $F(N)$ is often omitted and is given by

$$\begin{aligned} F(N) &= 1, & N &= 2 \\ &= 0.9, & N &= 3 \\ &= 0.5, & N &= 4 \\ &= \pi^{(N-2)/2}, & N &\geq 5 \end{aligned} \quad (2.2)$$

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1. E. Keil, CERN Report CERN/ISR-TH/72-25 (1972)
 2. P.M. Hanney & E. Keil, CERN Report CERN/ISR-TH/73-55 (1973)
 3. G. Guignard, CERN Report CERN 78-11 (1978)

It is assumed in this note that the factors β_y and $\exp(iN\phi)$ do not vary rapidly and can be treated as constant and evaluated at the crossing point of the two beams. It can be shown⁴ that under certain conditions

$$\int ds D_y^{n-1} E_y = 4\pi \int ds D_y^{n-2} \rho, \quad (2.3)$$

where $\rho(x,y)$ is the charge density distribution of the beam creating the field E_y . The required conditions are that the position of the test beam relative to the other be given by

$$\begin{aligned} x &= \alpha s, \\ y &= y(s), \end{aligned} \quad (2.4)$$

where the beams are crossing in the horizontal plane and α is the angle between them which is assumed to be small. The result, Eq.(2.3) follows from the invariance of the interaction integrals when the test beam is displaced by an amount Δs in the longitudinal direction of the other beam. Equation (2.4) says that the test beam moves along a straight line horizontally, but its path can be curved vertically.

It will be assumed that $\rho(x,y)$ is Gaussian in the vertical direction and is given by

$$\rho(x,y) = \rho_1(x) \exp(-y^2/2\sigma_y^2) / (2\pi\sigma_y^2)^{\frac{1}{2}}. \quad (2.5)$$

One thus finds for Δv_N

$$\Delta v_N = \Delta v \cdot \frac{f(N) e^{iN\phi}}{2^{(N-2)/2} (N-1)!} \alpha \int ds \rho_1(x) D_\mu^{N-2} e^{-\mu^2} \quad (2.6)$$

$$\mu^2 = y^2/2\sigma_y^2,$$

$$\Delta v = \frac{1 + \beta^2 \frac{\beta}{B\rho} \frac{I}{v}}{\beta} \frac{1}{(2\pi)^{\frac{1}{2}} \sigma_y \alpha}$$

$$\begin{aligned} f(N) &= 1, & N &= 2 \\ f(N) &= 0.9 \pi^{\frac{1}{2}}, & N &= 3 \\ f(N) &= 0.5 \pi, & N &= 4 \\ f(N) &= 1, & N &\geq 5, \end{aligned}$$

4. M. Cornacchia & G. Parzen, Forthcoming BNL Report (1979)

and $(\beta\epsilon/\pi)^{\frac{1}{2}} = 2 \sigma_y$ was used. Δv is the linear beam-beam v -shift.

We will now expand the integrand in powers of y , and keep just the lowest terms. One can show that for n odd

$$D_y^n e^{-y^2} = e^{-y^2} \left[(2y)^n - \frac{n(n-1)}{1!} (2y)^{n-2} + \frac{n(n-1)(n-2)(n-3)}{2!} (2y)^{n-4} \dots - \frac{n!}{((n-1)/2)!} 2y \right] \quad (2.7)$$

and for n even

$$D_y^n e^{-y^2} = e^{-y^2} \left[(2y)^n - \frac{n(n-1)}{1!} (2y)^{n-2} + \frac{n(n-1)(n-2)(n-3)}{2!} (2y)^{n-4} \dots - \frac{n!/2}{(n/2-1)!} (2y)^2 + \frac{n!}{(n/2)!} \right]$$

Keeping just the lowest powers in y we find for odd N

$$\Delta v_N = \Delta v \frac{f(N)}{2^{(N-1)/2}} \frac{1}{((N-1)/2)!} A, \quad (2.8)$$

$$A = \alpha \int ds \rho_1(x) y/\sigma_y \cdot \exp(in\phi).$$

For even N

$$\Delta v_N = \Delta v \frac{f(N)}{2^{(N-2)/2}} \frac{1}{((N-2)/2)!} \frac{1}{N-1} \cdot A,$$

$$A = \alpha \int ds \rho_1(x) \left[1 - (N-1) \frac{y^2}{2\sigma_y^2} \right] \exp(in\phi).$$

ϕ is the phase, $v\phi = \int ds (1/\beta_y)$

If $y(s) = 0$ at the crossing points, then Eq. (2.8) gives nonzero results only for the even resonances, which is the case in the absence of vertical orbit errors.

III. Δv_n DUE TO VERTICAL ORBIT ERRORS AT THE CROSSING POINTS

Vertical orbit errors at the crossing points make the beam-beam interactions different at the crossing points and generate resonances which lie close to the working line in v_x, v_y space. The results given by Eq. (2.8) have to be summed over all the crossing points. In computing the integral over s , $y(s)$ may be considered as constant and evaluated at the crossing points.

For N odd, the rms value of the stop band half-width is given by:

$$\Delta v_{N, \text{rms}} = \Delta v \frac{f(N)}{2^{(N-1)/2} [(N-1)/2]!} \cdot N_{\text{cp}}^{1/2} y_{\text{rms}}/2\sigma_y, \quad (3.1)$$

where N_{cp} is the number crossing points and y_{rms} is the rms value of the vertical orbit error at the crossing points.

For N even, Δv_N is proportional to y^2 . The quantity A in Eq. (2.8) becomes

$$A = (N-1) \sum_k e^{iN\phi_k} y_k^2 / 2\sigma_y^2,$$

where the sum over k is over all the crossing points.

For the moment it will be assumed that N is not a multiple of N_{cp} and $\sum_k \exp(iN\phi_k) = 0$. Then one can write

$$A = (N-1) \sum_k e^{iN\phi_k} (y_k^2 - \langle y^2 \rangle) / 2\sigma_y^2,$$

where $\langle y^2 \rangle$ is the average value of y_k^2 , and the average value of A^2 is given by

$$\langle A^2 \rangle = \frac{(N-1)^2}{4\sigma_y^4} \sum_{kk'} \langle e^{iN(\phi_k - \phi_{k'})} [y_k^2 - \langle y^2 \rangle] [y_{k'}^2 - \langle y^2 \rangle] \rangle.$$

Since $[y_k^2 - \langle y^2 \rangle]$ and $[y_{k'}^2 - \langle y^2 \rangle]$ are uncorrelated,

$$\begin{aligned} \langle A^2 \rangle &= \frac{(N-1)^2}{4\sigma_y^4} \sum_k \langle [y_k^2 - \langle y^2 \rangle]^2 \rangle \\ &= \frac{(N-1)^2}{4\sigma_y^4} \cdot N_{\text{cp}} [\langle y^4 \rangle - \langle y^2 \rangle^2], \end{aligned}$$

and

$$A_{\text{rms}} = (N-1) \cdot N_{\text{cp}}^{\frac{1}{2}} [\langle y^4 \rangle - \langle y^2 \rangle^2]^{\frac{1}{2}} / 2\sigma_y^2$$

Now $\langle y^2 \rangle = y_{\text{rms}}^2$ and for a Gaussian distribution $\langle y^4 \rangle = 3 y_{\text{rms}}^2$. Thus,

$$A_{\text{rms}} = (N-1) N_{\text{cp}}^{\frac{1}{2}} \cdot 1.41 y_{\text{rms}}^2.$$

For N even, and N not a multiple of N_{cp} , the rms value of Δv_N is given by

$$\Delta v_{N,\text{rms}} = \Delta v \frac{f(N)}{2^{(N-2)/2}} \frac{1.41}{[(N-2)/2]!} N_{\text{cp}}^{\frac{1}{2}} y_{\text{rms}}^2 / 2\sigma_y^2 \quad (3.2)$$

If N is even, and N is a multiple of N_{cp} , then $\sum_k \exp(iN\phi_k) = N_{\text{cp}}$, and Δv_N has a nonzero average value.

$$\langle \Delta v_N \rangle = \Delta v \frac{f(N)}{2^{(N-2)/2}} \cdot N_{\text{cp}} y_{\text{rms}}^2 / 2\sigma_y^2, \quad (3.3)$$

And around this average value, Δv_N has a statistical fluctuation whose rms value $[\Delta v_N - \langle \Delta v_N \rangle]_{\text{rms}}$, is given by Eq. (3.2).

For this case, one can introduce a pseudo $\Delta v_{N,\text{rms}}$ defined by the requirement that $2 \Delta v_{N,\text{rms}}$ gives roughly the peak Δv_N , and the pseudo $\Delta v_{N,\text{rms}}$ is given by

$$\Delta v_{N,\text{rms}} = \Delta v \frac{f(N)}{2^{(N-2)/2}} \frac{(0.5 N_{\text{cp}} + 1.41 N_{\text{cp}}^{\frac{1}{2}})}{[(N-2)/2]!} y_{\text{rms}}^2 / 2\sigma_y^2,$$

where N is even and a multiple of N_{cp} .

IV. Δv_N DUE TO RANDOM ERRORS IN β_y AT THE CROSSING POINTS

Random errors in β_y at the crossing point can excite resonances close to the working line. The linear beam-beam ν -shift, Δv , will be different at each crossing point. If one assumes that σ_y is due entirely to betatron oscillation, then $\Delta v \propto \beta_y^{\frac{1}{2}}$ and

$$\frac{\Delta v}{\nu} = \frac{1}{2} \frac{\Delta \beta_y}{\beta_y}. \quad (4.1)$$

Only even resonance are generated and from Eq. (2.8), the rms value of the stop band width is given by

$$\Delta v_{N,rms} = \Delta v \frac{f(N)}{2^{(N-2)/2} [(N-2)/2]!} \frac{1}{N-1} N^{\frac{1}{2}} \frac{1}{N_{cp}} \frac{1}{2} \left(\frac{\Delta \beta_y}{\beta_y} \right)_{rms}, \quad (4.2)$$

where $(\Delta \beta_y / \beta_y)_{rms}$ is the rms value of the error in the vertical β -function at the crossing points.

V. NUMERICAL RESULTS FOR ISABELLE

The results given in Sections III and IV can be applied to compute the stop-band half widths, Δv , due to random vertical orbit errors, and random errors in β_N at the crossing points for the ISABELLE storage accelerator.

Results are given below at two energies, 30 GeV and 400 GeV. For the even order resonance, the contributions due to random vertical orbit errors, $\Delta v_{N,y}$ and due to random errors in β_y , $\Delta v_{N,\beta}$ are given separately and Δv_N is the rms sum of these two contributions. For the odd order resonance, Δv_N is due to the vertical orbit errors only. It was assumed that the rms error in the vertical orbit at the crossing points is the same as 30 GeV and 400 GeV and is $y_{rms} = 0.05$ mm. It may be possible to correct the orbit better at 400 GeV because of the smaller size of the beam.

30 GeV

$\alpha = 0.011$, $I = 8$ A, $\beta_y = 7.5$ m, $\sigma_y = 0.75$ mm, $y_{rms} = 0.05$ mm,

$N_{cp} = 6$, $(\Delta \beta_y / \beta_y)_{rms} = 0.045$, $\Delta v = 0.0058$.

N	Δv_N	N	$\Delta v_{N,\beta}$	$\Delta v_{N,y}$	Δv_N
		2	3.20 E-4	4.46 E-5	3.23 E-4
3	7.55 E-4	4	8.37 E-5	3.47 E-5	9.06 E-5
5	1.18 E-4	6	7.99 E-6	1.03 E-5	1.31 E-5
7	1.97 E-5	8	9.51 E-7	9.21 E-7	1.32 E-6
9	2.47 E-6	10	9.25 E-8	1.15 E-7	1.48 E-7
11	2.47 E-7	12	7.57 E-9	2.15 E-8	2.28 E-8
13	2.05 E-8	14	5.33 E-10	9.57 E-10	1.09 E-9
15	1.46 E-9	16	3.30 E-11	6.85 E-11	7.60 E-11
17	9.18 E-11	18	1.82 E-12	8.03 E-12	8.23 E-12
19	5.10 E-12	20	9.05 E-14	2.38 E-13	2.54 E-13

400 GeV

$\alpha = 0.011$, $I = 8$ A, $\beta_y = 7.5$ m, $\sigma_y = 0.21$ mm, $y_{\text{rms}} = 0.05$ mm,

$N_{\text{cp}} = 6$, $(\Delta\beta_y/\beta_y)_{\text{rms}} = 0.045$, $\Delta\nu = 0.00156$.

N	$\Delta\nu_N$	N	$\Delta\nu_{N,\beta}$	$\Delta\nu_{N,y}$	$\Delta\nu_N$
		2	8.87 E-5	1.61 E-4	1.84 E-4
3	7.24 E-4	4	2.25 E-5	1.19 E-4	1.21 E-4
5	1.14 E-4	6	2.15 E-6	3.55 E-5	3.56 E-5
7	1.89 E-5	8	2.55 E-7	3.16 E-6	3.16 E-6
9	2.37 E-6	10	2.48 E-8	3.94 E-7	3.95 E-7
11	2.37 E-7	12	2.03 E-9	7.39 E-8	7.40 E-8
13	1.97 E-8	14	1.43 E-10	3.29 E-9	3.29 E-9
15	1.41 E-9	16	8.87 E-12	2.35 E-12	2.35 E-10
17	8.80 E-11	18	4.89 E-13	2.75 E-11	2.75 E-11
19	4.89 E-12	20	2.43 E-14	8.15 E-13	8.16 E-13