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Hanford Production Reactor Heat Releases 1951-1971

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L. D. Kannberg

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HANFORD PRODUCTION REACTOR HEAT RELEASES 1951-1971

L. D. Kannberg

August 1978 (date of work) April 1992

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Pacific Northwest Laboratory Richland, Washington 99352



SUMMARY

Beginning in 1944, nine nuclear materials production reactors were constructed and operated on the Hanford Reservation. Eight of the reactors operated from 1955 through 1964; nine operated most of 1964. Operating reactor levels grew throughout the period reaching highest levels in the middle 1960's. Maximum average reactor power reached 23,501 MW $_{\rm t}$ in December of 1964. For 13 of 15 months maximum average power levels exceeded 20,000 MW $_{\rm t}$. For over 8 years maximum average power levels exceeded 15,000 MW $_{\rm t}$. Only one reactor now remains in operation.

All of the thermal energy produced in the reactors was released to the environment; 90 to 97% of that energy entered the Columbia River directly. The remaining 3 to 10% was transferred from retention basins to the atmosphere or ground water by surface heat transfer and leakage, respectively. The reactors operated with direct once-through cooling with effluents being discharged primarily at 70 to 90°C.

Numerous studies have been performed investigating the mixing characteristics of the effluent plumes. These studies have shown that the effluents mix rapidly vertically but slowly laterally until major topographic features in the river force extensive mixing by wakes and secondary flows. Flow management by dams also appears to have a significant influence on Columbia River thermal dynamics.

Studies on the persistence of the Hanford thermal discharges have indicated that the free flowing reach near the Hanford discharges experiences much more surface heat transfer than impounded waters either upstream or downstream of the Hanford reach. As a result, the bulk of the thermal additions introduced by the production reactors was dissipated before effluents reached the Washington-Oregon border.

Extensive study of the Hanford ecosystem and anadramous fish migrating through, to, and spawning in the Hanford reach has detailed the effects of thermal exposures on the local ecosystem and on salmonid fish. The general conclusion is that Hanford thermal discharges caused no detectable harm to the aquatic ecology nor did they injure in any measurable manner the salmon

or trout fisheries. However, dam effects on the aquatic ecology of the river, especially salmon and trout fisheries, may have masked Hanford thermal effects within natural variation.

CONTENTS

SUMMA	۱RY			•	•	•	•		•	•	•	•	•		•	•	•	•	•	•	•	•	•	iii
INTRO	טסט	СТ	10	N.		•	•	•		•		•			•	•		•	•	•		•	•	1
DESCF	RIP	ΤI	ON	OF	THE	RE	AC	TOR	COC	LI	NG	SYS	TEM	S.	•				•	•	•	•	•	4
	N	RE	AC	TOR	COC)LIN	NG S	SYST	ΓEM	•		•	•	•	•	•	•	•	•		•	•		9
HIST	RI	CA	L	HEA	r RE	LEA	\SE!	s.	•	•	•	•	•		•	•		•	•	•	•	•		12
	EN	IER	GY	0U	TPUT	•	•	•	•	•	•	•	•	•	•		•	•	•	•	•		•	12
	EN	ER	GΥ	TRA	ANSF	ER		•	•	•		•			•		•	•	•	•	•		•	19
	FΔ	TE	0	F E	FFLL	JENT	rs	•	•	•	•	•	•		•	•		•	•	•	•	•	•	20
THERM	1AL	. C	ΉΑ	NGE:	S.		•	•	•	•	•	•	•		•	•	•	•	•	•	•	•	•	22
ECOL(GI	CA	L	EFFI	ECTS	S OF	- TI	HE H	IANF	FOR	D 0	OISC	HAR	GES.	•			•	•	•	•	•	•	26
REFE	REN	ICE	S						_															29

TABLES

1.	Reactor Startup and Deactivation	1
2.	Retention Basin Statistics	9
3.	Selected Dam Statistics	23
	FIGURES	
1.	Hanford Reservation	2
2.	Typical Limited Area for Dual Production Reactor Plants	5
3.	Water Flow for a Typical Production Reactor Plant	6
4.	Schematic of Cooling Systems for N Reactor and Hanford Generating	10
	Plant	10
5.		14
6.		15
7.		16
8.		17

HANFORD PRODUCTION REACTOR HEAT RELEASES 1951-1971

INTRODUCTION

The Hanford Reservation consists of about 570 square miles of semiarid lands in southeastern Washington. The Reservation was created in the early 1940's to permit production of weapons-grade nuclear materials. The Hanford site was ideally suited to the task for several reasons, including sparse population, ample cooling water supply, proximity to large electrical supply facilities, favorable geology and geohydrology, and low precipitation.

Development of the site began with construction of B Reactor which was completed in September 1944. Eventually nine reactors were constructed; eight of which were employed solely for production of nuclear materials. The remaining N Reactor has produced steam for Washington Public Power Supply System's Hanford Generating Plant since 1966. The initial startup and deactivation dates of the nine reactors are given in Table 1.

TABLE 1. Reactor Startup and Deactivation

Reactor	Initial Startup	Deactivation
В	September 26, 1944	February 12, 1968
D	December 17, 1944	June 26, 1967
F	February 25, 1945	June 25, 1965
Н	October 29, 1949	April 21, 1965
DR	October 3, 1950	December 30, 1964
C	November 18, 1952	April 25, 1969
KW	January 4, 1955	February 1, 1970
KE	April 17, 1955	January 28, 1971
N	December 31, 1963	Currently in Operation

Because all of the reactors operated with once through cooling water from the Columbia River, the plants were distributed along the river as it flowed through the Reservation. Reactor areas (100 Areas) as well as other major facility sites and roads are shown in Figure 1 as they currently exist.

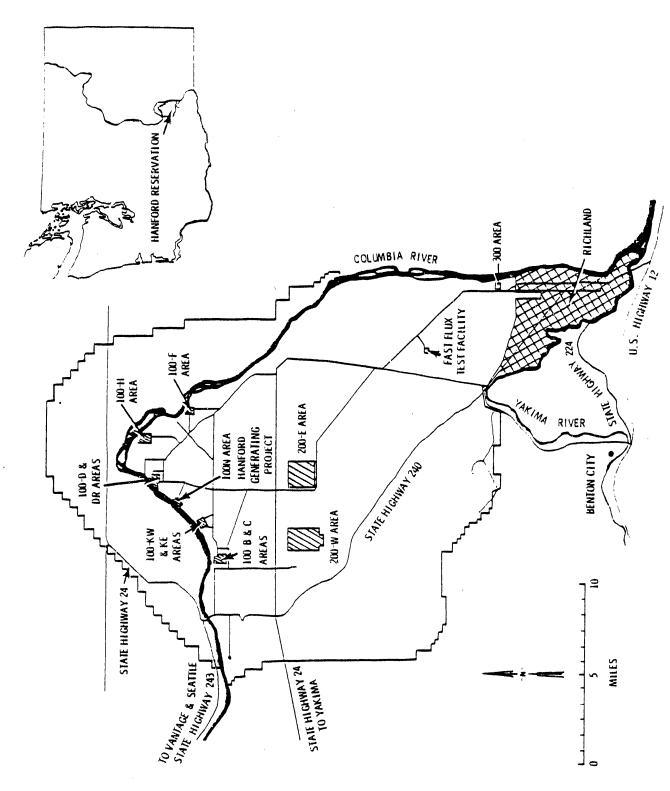


FIGURE 1. Hanford Reservation

The purpose of this report is to document and detail the thermal releases from the Hanford nuclear production reactors during the period 1951 through 1971, and to put these releases in historical perspective with respect to changing Columbia River flows and temperatures. This information can also be used as a foundation for further ecological evaluations.

When examining Hanford production reactor thermal releases to the Columbia River all related factors affecting the releases and the characteristics of the river should be considered. The major considerations in the present study were the characteristics of the releases themselves (primarily coolant flow rate, temperatures, discharge facilities, period of operation, and level of operation) and the characteristics of the river in that reach (primarily flow rate, temperature and mixing characteristics; the effects of dam construction were also taken into account. In addition, this study addressed ecological effects of thermal releases on aquatic species. Accordingly, this report includes discussion of the reactor cooling systems, historical heat releases, thermal mixing and transport studies, hydroelectric power development, and ecologic effects of Hanford production reactor heat releases on salmon and trout. Appendix A contains reactor operating statistics, and Appendix B provides computations of heat added to the Columbia River between Priest Rapids Dam and Richland, Washington.

DESCRIPTION OF THE REACTOR COOLING SYSTEMS

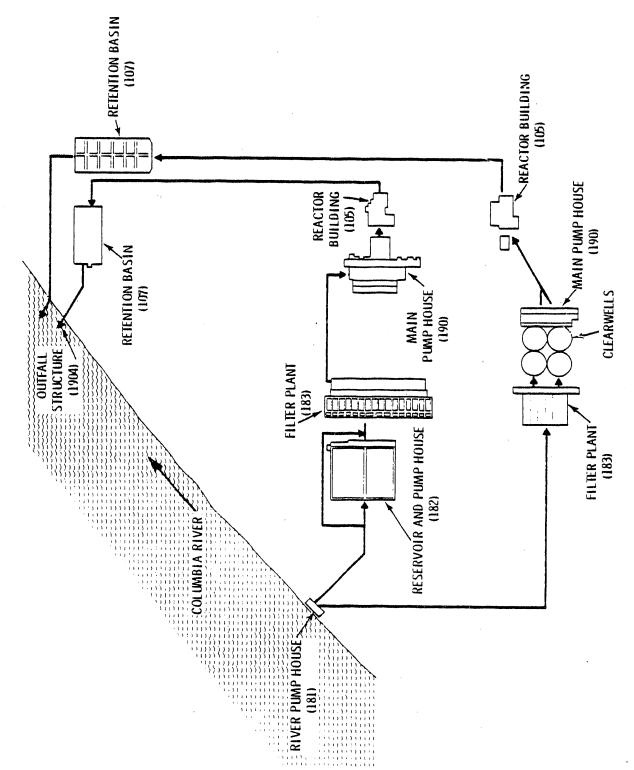
The cooling system used was direct once-through cooling with river water flowing directly through the reactors. The primary circulating system is shown in Figures 2 and 3. Figure 2 is an illustration of a typical dual production reactor area. Areas having dual production reactors were 100 B and C, 100 KW and KE, and 100 D and DR. Areas having single reactor facilities were 100 H and 100 F. The typical cooling system for the eight reactors is shown schematically in Figure 3 (the facilities at N Reactor are discussed later). Figure 3 also shows the buildings (designated by numbers) that were used for different facets of cooling treatment.

Columbia River water was obtained through pump houses which enclosed 5 to 14 vertical deepwell pumps; the bottoms of the pump bowls were approximately 11 ft below normal flow water elevations. (a) The intake channels from the pump houses into the river were dredged and lined with rock and concrete. River water entered the pump house deepwell through traveling screens which prevented entrance of fish and debris. Combinations of 30-in., 36-in., 42-in., and 48-in. lines passed circulating water from the river pump houses (181 Bldg.) to reservoirs (b) in the 182 Building and chemical treatment and filtering facilities in the 183 Building.

Although the Columbia River water is exceptionally pure it was necessary to filter and chemically treat it at the 183 Building to prevent filming in the reactor process tubes. Each reactor had a separate treatment plant consisting of a head house, raw water flume, mixing chambers, distribution

⁽a) Much of the information concerning details of the circulating water systems comes from References 1 and 2 which do not discuss 100-KE and 100-KW reactor areas.

⁽b) Prior to plant modification in 1956-1957 under project CG-558 the reservoirs were used as the principal water supply source for the filter plants and ultimately the reactors. Under project CG-558 flow modifications were made to various plant facilities to permit significantly higher coolant flow rates and thereby increase production of nuclear materials. After CG-558 the reservoirs were used primarily for "export water" used as a source for emergency cooling. Export water was water supplied to off-plant areas such as the 200 Area and to other reactor areas as needed.



Typical Limited Area for Dual Production Reactor Plants (Figure Modified from Reference 4) FIGURE 2.

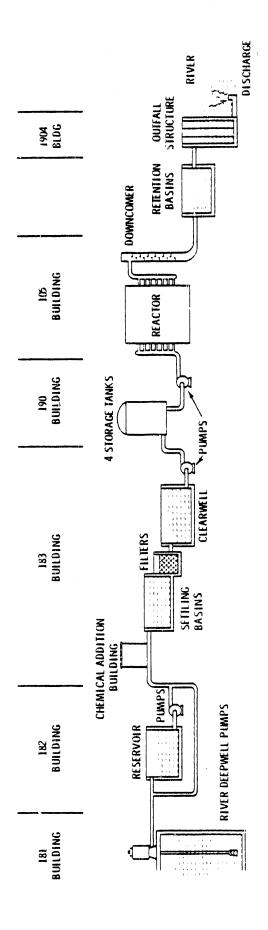


FIGURE 3. Water Flow for a Typical Production Reactor Plant (Figure Modified from Reference 4)

flume, flocculators, settling basins, collecting flume, influent flume, filters, effluent and backwash piping, effluent flumes, and clearwells.

In the head house, alum (used as a flocculating agent), sulphuric acid (to control pH), and chlorine (used as an algacide for control of algae in the settling basins) were metered into the raw river water. The combination was mixed in the mixing chambers and conducted to paddle-wheel flocculators and settling basins via the distribution flume. After particulates settled out, the circulating water entered gravity flow filter beds consisting of layers of crushed gravel, sand, and crushed anthracite coal. An organic polyelectrolyte filter aid was added during filtering to increase efficiency. The filters were backwashed with water from the clearwells as necessary to maintain proper operation.

From the filters the cooling water flowed by gravity into the clearwells. The clearwells, which served to collect and store waters from the filters, had storage capacities of approximately 3 x 10^6 to 10^7 gal. The filtered water was then pumped or gravity drained into four large storage tanks in the 190 Building. The storage tanks provided water to the coolant pumps that supplied cooling water to the reactor. Tank storage capacities varied from about 7 x 10^6 to 21 x 10^6 gal. For normal operating flow rates there was sufficient storage capacity to operate the reactor at full flow for more than an hour without supply from the clearwells. Intake of 182 Reservoir storage between reactor areas provided additional supplies if required.

The 190 Building also housed the primary coolant pumps that supplied high pressure cooling water to the reactors, and high tanks which could supply 300,000 gal of emergency cooling water if pressure in the piping from the 190 Building to the reactor was lost. Gravity flow of emergency cooling water from the export water system could supply coolant if supplies in the high tanks were exhausted.

Cooling water was supplied to the reactor building (105 Building) at 600 psi. Water flowed into vertical inlet risers which paralleled each side of the front face of the reactor. The coolant flowed from these risers through as many as 46 4-in. crossheaders to inlet nozzles on each process tube.

The coolant then flowed through the process tube and around the fuel element housed within the process tube. During irradiation the coolant was heated by the hot fuel element and adjacent graphite moderator. The coolant left the reactor in a similar manner, passing through outlet nozzles, to crossheaders, to two vertical risers which were interconnected above the reactor to a downcomer. The downcomer served to break the fall of water from the crossover piping to the effluent lines. The downcomer was vented to relieve trapped gases (air) and steam. Reactor outlet piping had a rated working pressure of 150 psi. From the downcomer the effluent moved by gravity from the reactor building through underground piping to large retention basins. The retention basins were designed to permit decay of shortlived radioisotopes. The basins served another purpose by containing high concentrations of radioactive substances released during fuel element failures until they could be removed to adjacent cribs for effective filtering through the ground.

The retention basins varied considerably in size although operation was similar in all of them. Effluent entered one end of the rectangular or round retention basins, flowed through or across the basins and exited from the other side. Several of the basins had baffles to prevent the effluent from channeling in the basins. The nominal dimensions, volumes, and estimated flow-through times for the retention basins are given in Table 2. In actuality, some channeling did occur thereby reducing travel times at certain plants.

The reactor effluents left the retention basins by overflowing a weir at one end of the basin. Effluent flowed into a downpipe to underground piping leading to the outfall structure or, as necessary, to a crib for isolation. The outfall structure consisted of three compartments. The effluent flowed into one compartment, then overflowed into an adjacent chamber which led via one or two effluent pipelines (depending on the plant) center of the river for submerged vertical single port discharge. If flow through the discharge effluent lines was obstructed, or if river water elevation was extremely high, water could overflow the second chamber into a third which led via a spillway to the river shore for shoreline surface

discharge. Submerged discharge in the center of the river was designed to provide rapid dilution with river waters, both thermally and radiologically.

TABLE 2. Retention Basin Statistics

Reactor Basin	Length (Dia.)ft	Bas Width, ft	Depth, ft	Volume 10 ³ /ft	Travel ^(a) <u>Time, hr</u>	Flow ^(b) Rate, gpm
107-B ^(c)	450	230	16	1656	2.38	87,000
107-CW	(330)		16	1368	1.96	87,000 ^(c)
107-CE	(330)		16	1368	1.78	96,000
107-D	450	230	16	1656	2.33	89,000
107-DR	450	230	16	1656	2.35	88,000
107-F	450	230	16	1656	2.33	89,000
107-H	600	270	15	2430	3.26	93,000
107-KE ^(d)	(250)		29	4270 ^(d)	2.59	206,000
107-KW ^(d)	(250)		29	4270 ^(d)	2.57	208,000

⁽a) Computed from assumed flow rate and calculated basin volume.

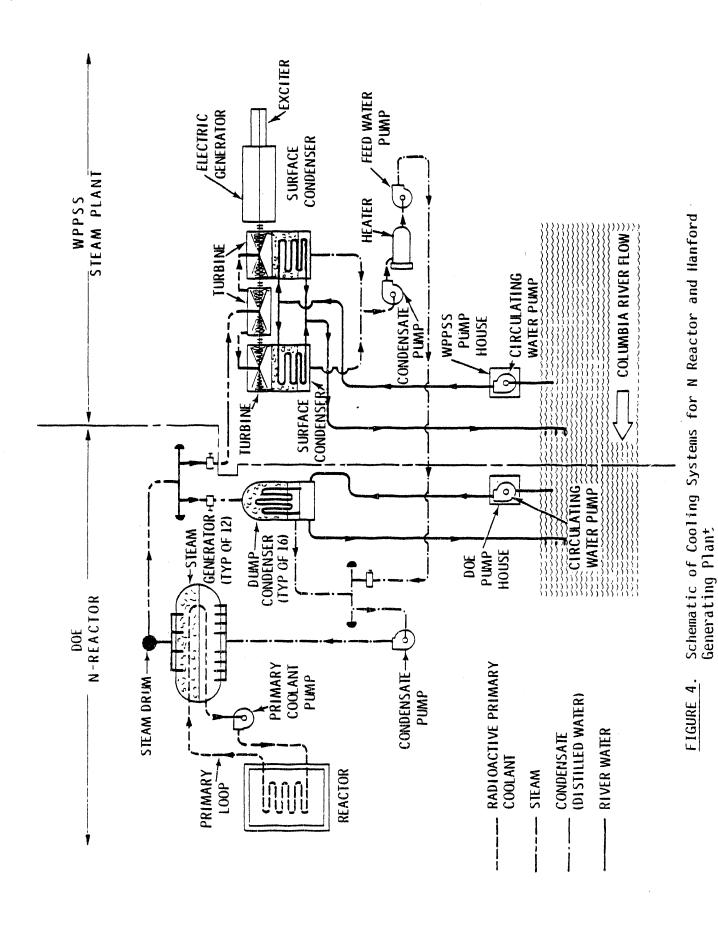
N REACTOR COOLING SYSTEM

N Reactor has a different cooling system because its main reactor colant loop produces steam. A schematic of the cooling systems for N Reactor and Hanford Generating Plant (HGP) is shown in Figure 4. There are essentially three circulating circuits. The primary system coolant picks up heat in the reactor and transfers it to the secondary system coolant in a steam generator. N Reactor is a pressurized water reactor using ultrapure water as the primary coolant, operating at approximately 1200-1500 psig. (2) In the steam generator energy from the primary coolant is transferred via a heat exchanger to the secondary coolant which boils to steam. Pressure in the secondary coolant in the steam generator is about 140 psig. (3) This low pressure steam is generally routed to the HGP where it is used to drive

⁽b) Nominal values for reactor flows in 1964.

⁽c) Because of excessive leakage from the 107-B retention basin effluent from B reactor was routed to 107-CW.

⁽d) Three basins of the size given. Volume is total of all three basins.



turbines, then condensed to liquid, and pumped back to the steam generator. During periods when HGP is not operating it is routed to "dump" condensers in the 100 N Area for condensation and return to the steam generator. In the condensers, thermal energy is transferred from the condensing steam to circulating water from the river. Water is pumped from the river through the condenser heat exchanger back to the river. This is true of both the dump condensers and the HGP condensers. The major difference is that if steam is routed to the HGP, a portion (slightly less than 25%) of the energy in the steam can be transformed into electrical energy rather than dumped into the river.

The intakes for N Reactor and HGP are very similar to the eight other production reactors; however, the discharges are somewhat different. N Reactor has a single port vertical outfall as do the other reactors but with a velocity cap to provide more rapid mixing. HGP employs an outfall having four vertical ports positioned 50-ft apart on a diffuser line across the central portion of the river providing even greater mixing than the single ports.

HISTORICAL HEAT RELEASES

The Hanford production reactors represent a unique collection of historical industrial facilities in regard to thermal energy releases to the environment. Several features of these facilities are not likely to be duplicated at any other industrially developed site. For example:

- No other facilities of any significant size discharged waste heat into the Columbia River for a considerable distance upstream and downstream of the reactor locations during the operating period of the reactors.
- The magnitude of the releases dwarf those of many comparable industrial facilities.
- Because of the nature of the plants and their discharges, excellent records exist providing reactor operating statistics.
- Reasonably coherent and consistent environmental analyses were performed throughout the plant operating period.
- The plant facilities were very similar and were operated in very similar manners.
- The sites are in a relatively compact arrangement.
- With the exception of the effects of dam construction and operation there was very little change in water quality entering the Hanford Reservation during the operating period.

For these reasons the Hanford reactor heat releases are a valuable reference point for future development in the Columbia Basin and at other sites around the nation.

ENERGY OUTPUT

When the production reactors were designed and constructed (primarily in the 1940's and early 1950's) the main concern was production of weaponsgrade nuclear materials. The early designs permitted small production rates for nuclear materials and waste heat. The reactor designs were made with little operational experience and very limited knowledge of optimal values for production parameters. Their output was intially small until the

design and operational characteristics were expanded to achieve greater production. The plants generally operated in two possible modes. Either the plant output was limited by the power level or the plant output was limited by the temperature of the effluent in the downcomer. During 1951-1955 power levels in the six older reactors rarely exceeded 6000 MW. However, in 1956 and 1957 these reactors underwent flow modifications under project CG-558. These modifications more than doubled the potential reactor sustained power levels. During the following years, as more experience was gained and minor modifications performed, the power level limits and downcomer temperatures limits were successively raised; in the middle 1960's all of the reactors operated at near peak power levels. Eight of the nine production reactors were operating in 1955 (N Reactor began in 1964); however, total maximum average heat release at that time was only 6000 to 9000 MW. In March 1964, the total maximum average heat release for these same reactors was nearly 21,000 MW.

Figures 3 through 8 illustrate the monthly energy released by the production reactors in the period 1951-1971. In these figures the total maximum average heat release is the sum of the monthly average power levels during reactor operation for all of the reactors operated that month. This total represents a reasonable estimate of the peak combined heat release during the month since there would likely have been only a small portion of the time that all reactors operated during the month. Also shown in the figures is the integrated power released by the reactors in gigawatt days (GWD). This number was obtained by multiplying the average power level during reactor operation by the time during the month that the reactor operated for each reactor and summing for all the reactors. The integrated power thus represents the total energy released to the environment during the month. The third curve shown in these figures is the mean energy release to the river during the month and is computed as the integrated power divided by the number of days in the month.

The development of production capacity at Hanford can readily be seen. X
The maximum heat release was in December 1964 when all the reactors were operating and river temperatures were low. The total maximum heat discharge

could have reached 23,501 MW during the month. Integrated power was 604.1 GWD and the mean monthly heat release computed to nearly 20,000 MT $_{\pm}$, 19,490 MW $_{\pm}$.

Six 1250 MW $_{\rm e}$ nuclear generated stations today would generate 7500 MW $_{\rm e}$ total maximum power, and at 33% thermodynamic efficiency, 15,000 MT $_{\rm t}$ total maximum heat release. Using an annual plant factor of 0.7 including a 1-month refueling outage, these six plants would yield 352.2 GWD integrated heat release monthly and a mean monthly (30 days) heat release rate of 11,730 MW $_{\rm t}$. The Hanford production reactors exceeded 15,000 MW $_{\rm t}$ in total maximum heat release rate for 8 years between August 1959 and August 1967. Monthly integrated power exceeded 353 GWD for over 8 years during the period from December 1958 to August 1967.

Total maximum heat release rate exceeded 20,000 MW $_{
m t}$ for 13 of 15 months between December 1963 and April 1965, and 10,000 MW $_{
m t}$ for more than 13 years between November 1956 and January 1970. Monthly integrated power exceeded 470 GWD in 19 months between March 1963 and April 1967; 235 GWD was exceeded for 13 years between June 1956 and June 1969. Data for the average power level during operation and the time operating efficiency (percent of month reactor operated) are given for each reactor by month in Appendix A for the period 1951-1971. Also given in Appendix A are the cooling water temperatures into and out of the reactor, and the nominal coolant flow rate for each reactor as recorded during the "last equilibrium operation."

The last equilibrium operation is the latest time (within the month) that the reactor operated stably at operational limits. These temperatures and flow rates should not be taken as maximum operating values, nor should they necessarily be considered as an average operating value for that parameter. Rather, they should be interpreted as typical operating values when reactor operation was stable. Computation of the power levels of the reactor using the flow rates and temperatures across the reactor will result in values not necessarily the same as those given in Appendix A. The average power levels during operation and the time operating efficiencies are considered accurate.

Table A-1 shows the total maximum average power level (or heat release) for that month (AVG. MW) and the integrated power (heat release) for the month for the combined reactors in GWD. When both N reactor and HGP were operating, the difference between the energy released by N reactor and the electrical production of $HGP^{(a)}$ is computed as N^* and represents the thermal energy release rate to the environment when both plants are operating. Examination of the table shows that after 1966 N Reactor rarely operated when HGP could not, making N^* a reasonable estimate of the N Reactor heat release to the environment. The total maximum average heat release is the sum of the average power levels during operation for all the reactors except when HGP was operating, for which N^* replaced the N Reactor contribution. The integrated heat release includes the N Reactor thermal contribution at its related time operating efficiency as well as subtracting HGP electrical generation at its related time operating efficiency. The integrated heat release represents the total energy released to the environment for the month. The mean monthly heat release rate to the environment may easily be computed as the integrated power, GWD, divided by the number of days in the month.

ENERGY TRANSFER

The energy produced by the reactors did not all reach the Columbia River—There were several mechanisms for energy transfer to the atmosphere and the ground before entering the river. For example, a certain amount of heat transfer occurred between the piping and the soil. No data exist to determine the magnitude of that heat transfer; however, it is expected to be relatively small due to the relative insulating value of soil. A far more signficant heat transfer mechanism for the eight reactors was the heat transfer to the atmosphere and ground from the retention basins. (b) During operation the hot effluent (occasionally greater than 90°C) passing through the retention basins transferred great quantities of heat and mass to the atmosphere in the form of vapor plumes. These plumes rose 1000 or 2000 ft

⁽a) All energy rates in the Appendices are given as thermal except for HGP energy rates which are electrical.

⁽b) N Reactor did not empty retention basins and experienced no known leakage between the dump condensers and the river shoreline.

in the air under certain conditions. When evaporative heat loss dominated heat transfer to the atmosphere. Many of the retention basins leaked large quantities of effluent to the ground waters which eventually flowed to the Columbia River near the plant sites.

While ground-water flow speeds into the Columbia River from the retention basins in the zones bordering the river were between 10 and 30 ft/day, normal ground-water influxes to the Columbia are estimated to contribute over four times the thermal energy leaked from reactor retention basins. $^{(4)}$ The piping between the 105 Reactor Buildings and the retention basins was also observed to leak. The water table was observed to rise in the regions of the retention basins and effluent lines. Large portions of these locally raised water tables were at elevated temperatures. The six older reactor areas had ground-water temperatures in excess of 70° C in extensive zones underneath the retention basins. Leakage from the retention basins is estimated to have been from 1 to 5% of the effluent flow from the reactor based on available information. $^{(4)}$

Based on temperature measurements of effluents in the downcomer and leaving the retention basins, an estimated 3 to 8% heat loss occurred as a result of heat transfer to the atmosphere. There was also considerable leakage from piping leading from the retention basins to the discharge in the center of the river, as evidenced by thermal plume surveys with infrared imagery. (5) It is therefore very difficult to estimate the true heat releases from the Hanford production reactors to the Columbia River. A reasonable estimate is that probably 3 to 10% of the reactor thermal energy generated was dissipated to the atmosphere before effluents entered the river, leaving 90 to 97% to enter the river.

FATE OF EFFLUENTS

Numerous studies have been performed to determine the fate of effluents that entered the river from the production reactors. Mixing near the discharges was observed to be rapid vertically so that even the highly buoyant discharges from the production reactors were completely mixed vertically within a few hundred yards of the outfall. Mixing laterally was observed to proceed much slower than vertically. Narrow ribbons of effluent plume were

often observed downstream until major river features (such as islands and bends in the river) enhanced lateral mixing. Lateral temperature profiles at Richland, Washington, demonstrated that complete lateral mixing was not obtained even to that point. Lateral mixing coefficients were observed to vary from about 0.5 ft^2 /sec to 12.6 ft^2 /sec depending on the river location and the buoyancy (lateral mixing increased for buoyant cases). (6) Generally acceptable values for lateral eddy diffusivities upstream of Locke Island are near 2 $ft^2/sec.$ Dilution of effluents near the discharge have been measured. (7) Dilution factors varied significantly for varying flow conditions and reactor discharges. The dilutions to the points where the plumes were first observed to strike the surface (about 50 ft downstream) were estimated to be from 2 to 7 for a river flow of 36,000 cfs. (a) For the same river flow dilution factors were estimated to be from 7 to 17 at 100 yd downstream from where the plume surfaced, and from 17 to 37 at 400 yd downstream. (a) As a general rule the dilution increased directly with river flow rate such that at a river flow of 360,000 cfs dilutions would be an order of magnitude larger than those estimated at 36,000 cfs. As would be expected, the data supporting those analyses display considerable scatter evidencing highly varying turbulent characteristics.

⁽a) Dilutions were computed based on maximum plume measured temperatures and efficiency and effluent temperatures recorded at the reactor downcomer.

THERMAL CHANGES

Because of the magnitude of energy released to the Columbia River by the production reactors, the importance of the river for commercial fishery on the Pacific Coast, and the emerging concern with thermal discharges as "pollution," numerous studies have been performed relating Hanford heat releases to 1) power development on the Columbia and 2) environmental effects of large heat releases. The emerging interest in the environment and resulting environmental regulation brought about an extensive effort by Hanford researchers to characterize and model the extent and persistence of the Hanford thermal discharges. Additional monitoring was performed on special studies and analyzed. (8-11) A temperature monitoring system already in existence on the Columbia was refined in 1964 to provided added data and remove biases that may have existed in prior monitoring programs. Analysis of data from this network and other studies with special computer routines and the development of various river reservoirs computer models for heat transfer and heat budget simulation led to several interesting observations ranging from the effects of the dams on the hydrothermal character of the Columbia River to the persistence of Hanford heat additions downstream of the Hanford Reservation.

The Columbia River flows generally east across the northern portion of the Hanford Reservation, then turns south forming the eastern boundary. The Columbia is the second largest river in the United States with a discharge at its mouth slightly larger than the Ohio River. (12) Because of the large discharge, low suspended sediment load, and steep side slopes characterizing the river, significant hydroelectric power development has occurred. At present the only nontidal free flowing reach of the river is the 49-mile length from the head of McNary Reservoir (behind McNary Dam) to Priest Rapids Dam [river mile (RM) 397]. Except for about 9.5 miles immediately below Priest Rapids Dam, this reach lies completely within or is bounded by the Hanford Reservation.

The period of major construction and operation of the Hanford production reactors (1951-1971) was also the period of major dam construction on the

Columbia. Table 3 shows the river mile, the total storage, and the completion date for all U.S. dams on the mainstem of the Columbia River. In addition to these dams other major dams on the Snake River (Ice Harbor, Lower Monumental, Little Goose, Lower Granite, and others) contribute to power development, navigation and flood control. However, since the Snake River enters the Columbia below the Reservation (about RM 325) flow control on the Snake has no effect on the Columbia River flow past the Hanford Reservation. Additional dam construction on the upper Columbia or its tributaries in Canada and the U.S. (Mica, Duncan, Hungry Horse, Libby, and Arrow) will increase storage volumes fivefold over that of U.S. dams on the mainstem of the Columbia and aid significantly in flow control.

TABLE 3. Selected Dam Statistics

Dam	River Mile	Reservoir Length mi	Storage Capacity 1000 acre-ft	Completion Year
Bonneville	146	48	87	1938
The Dalles	192	24	53	1957
John Day	216	75	535	1968
McNary	292	59	185	1953
Priest Rapids	397	56	44.8	1959
Wanapum	415	18	160.8	1965
Rock Island	453	20	8.6	1933
Rocky Reach	474	42	36	j 1961
Wells	516	28	125	1970
Chief Joseph	545	51	115	1955
Grand Coulee	597	151	5232	1941

Dam construction has had a major influence on Columbia River flows and temperature, thereby affecting both Hanford reactor operations and analyses of environmental effects of those operations. The impoundment of waters in the Snake and Upper Columbia Rivers has substantially reduced high water discharge. This is the intended effect of the 1971 Columbia Treaty between the United States and Canada, which provided for flood control on the Columbia

and its tributaries. The effective storage of spring and summer runoff waters has signficantly aided in meeting large power demands during the winter through hydroelectric generation. At the same time, storage has created a temporal shift in the river temperature cycle. For example, the construction of Grand Coulee Dam produced a permanent delay of about 30 days in arrival of peak temperatures at locations downstream. Similarly, waters with peak temperatures arrive at Priest Rapids about 7 to 10 days later than they reach Rock Island. Previously, peak temperatures were simultaneous at these locations. The shifts are generally attributed to increased flow times through reservoirs behind the dams.

Another temperature effect observed as a result of dam construction on the Upper Columbia is the lowering of peak and average temperatures. It has been predicted that the average August-September temperatures at Priest Rapids Dam after completion of the Canadian Dams will be nearly 2°C lower than the average 1961–1967 temperatures. (13) Construction of the Canadian Dams is predicted to lower temperatures of water emerging from Grand Coulee Dam by as much as as 4°C as compared to average peak temperatures for the period 1929 through 1957. Lower Columbia River temperatures and cycle shifting are most pronounced upstream from the mouth of the Snake River. The Columbia seems to equilibrate considerably between McNary Dam and Bonneville Dam. The bulk of this is due to climatological and hydrodynamic conditions characteristic of that reach. The Snake River raises temperatures in the Columbia particularly in late summer.

Additional findings concerning thermal characteristics of the Columbia River are as follows: (15)

- Dam impoundments respond much more slowly to thermal additions than free flowing river reaches evidencing larger heat transfer coefficients for free flowing rivers.
- Columbia River temperatures appear to be closely related to river management practices (hydroelectric and storage operations).
- Temperatures in the free flowing reach between Priest Rapids and Richland gain from 0.5 to 0.90°C in August and September due to natural heating in the absence of thermal discharges.

- The majority of thermal energy released by the production reactors in 1969 was dissipated to the atmosphere before effluents reached the confluence with the Snake. At the Oregon-Washington border between 60 and 95% of the thermal additions of the production reactors had been dissipated, with the average dissipation being 65%. At Bonneville only about 20% of the production reactor heat release (1969) remained in the river.
- An annual thermal addition of 4000 MW $_{\rm t}$ is attributable to the Snake River. During August and early September the addition is nearly twice the annual average. With the completion of the Canadian Treaty Dams this summer addition may rise to over 15,000 MW $_{\rm t}$.
- Thermal additions in winter persist further downstream than those same discharges in summer.
- ullet Studies concerning the thermal capacity of the Columbia indicate that there is a potential for addition of from 20 to 25 GW $_{\rm t}$ in the zone between Grand Coulee and Pasco, Washington, within state water quality criteria. $^{(16)}$

The data in Appendix B illustrate the magnitude of thermal changes in the Hanford reach of the Columbia. Specifically, these data include the monthly average Priest Rapids temperature, Richland temperature, Columbia River discharge; the computed heat additions between Priest Rapids and Richland (based on their temperatures and the flow of the Columbia); the monthly mean heat additions by the Hanford production reactors (which lie between these sampling points); and the difference between the computed means and the reactor heat additions for the period of June 1964 through December 1971. The values given in Appendix B demonstrate that flow management tends to have a large influence on the natural heat gain. During high flow periods computed natural monthly mean heat gains often exceeding 20,000 MW $_{\rm t}$ were observed. During low flow periods the Hanford production reactor contributions formed a large part of the gross thermal gain of the river.

ECOLOGICAL EFFECTS OF THE HANFORD DISCHARGES

As early as 1945 ecologists were studying the effects of the Hanford production reactor discharges on the flora and fauna of the Columbia River in the Hanford reach. Generally, these studies have endeavored to determine the effect of Hanford production reactor operations on economically important species, primarily salmon and trout.

Effects considered include thermal shock, thermal tolerance, upper thermal lethal limits, and, to a limited extent, temperature in regard to infectious diseases and gas bubble disease. Additional studies have been performed on migrating fish past the discharges, on the number of fish spawning in the Hanford reach, and on the effects of temperature on annual fish and insect cycles. These studies have demonstrated the following results: (17)

- "Cold water" fish such as salmon have a much narrower tolerant temperature band than other fish; duration of exposure plays a critical part in loss of equilibria and mortality.
- Field studies from March through September 1968 and 1969 were conducted to determine mortality of juvenile salmonids drifted through effluent plumes in liveboxes. Drifts through shoreline areas near seepage from retention basins resulted in significant mortalities among only a few test groups. Drifts through midriver effluent plumes resulted in losses only during unfavorable late summer conditions.
- "Columnaris" disease (a myxo-bacterial infection) associated with the Columbia River in warmer months has not been linked to the Hanford discharges. Mortality of fish subjected to large doses of Columnaris organisms was higher in warmer waters than cooler. Fish ladders appear to have much higher concentrations of the organism than other river locations.
- The problem of nitrogen supersaturation, which causes gas-bubble disease, may be enhanced in warmer water temperatures. Nitrogen supersaturation is linked primarily to entrainment and compression of air in dam spill-ways. Gas-bubble disease was not an obvious problem in the Hanford

- reach; however, heat releases at Hanford may have contributed in a very minor way to occurrence at downstream dams.
- Rainbow trout and chinook salmon were selectively preyed upon by larger fish after being subjected at sub-lethal exposures to water at lethal temperatures (i.e., thermally shocked) in the laboratory. Significant increases in predation rates were found when chinook salmon and rainbow trout received thermal doses that were 10 and 20% of doses causing equilibrium loss.
- Juvenile fish appeared to be more resistant to warm temperature effects than adults.
- Migrating fish appear to prefer shoreline areas particularly the area across from shoreline seepages of reactor effluents. Definite rheotaxis (thermal avoidance) was exhibited by migrating fish in the region of the shoreline effluent seepages near the reactor retention basins.
- Changes in the timing of emergence of caddisflies (Trichoptera) have been related to river temperatures. Caddisfly emergence occurred a few weeks earlier in waters immediately downstream of the effluent discharges, slightly later in well mixed waters further downstream, and latest upstream of the reactors. It is felt this would have little effect on annual biologic cycles of juvenile fish of which 96% of their diet is adult and larval insects (the bulk of which are midges).
- The annual census of spawning fall chinook salmon in the Hanford reach, begun in 1947, has failed to illustrate any deleterious effects of the Hanford discharges. Dam construction has displaced many spawning fish such that rearing nests in the Hanford reach have generally increased. This indicates that spawning in the Hanford reach has not been despoiled, and that Hanford heat releases have not resulted in a catastrophic fisheries disaster.
- Tests on manually spawned fertilized salmon eggs taken from fish captured below Priest Rapids and reared at temperatures elevated above those in the river showed normal mortality (for hatchery operations) and increased body weight (factor of 1.4 for each 2°F rise above

ambient to 12°F) for the eggs and young. The question exists whether or not warmer winter and spring waters might not increase body weight of migrants thereby improving survivorship until seaward migration. (Size of young at release from hatcheries is known to influence the number of adults returning.)

A general conclusion is that the Hanford production reactor thermal discharges have had no <u>detectable</u> harmful influence on the Hanford reach aquatic environment including salmon and trout.

Dam development on the Columbia and its tributaries has had a major effect on migrating salmon and trout. Although steps have been taken to mitigate the influence of dam construction on these anadromous fish (fish ladders, restocking, etc.), there is little doubt that dams have contributed to reducing or eliminating return of spawning fish to certain portions of the Columbia and its tributaries, increased mortality of spawning fish through mechanical stresses, increased incidence of infectious disease and gas bubble disease, and caused relocation of major spawning grounds.

The influences of dam construction and operation and other factors (e.g., irrigation return) on the Columbia River fisheries and the Hanford aquatic ecology tend to mask the effects of the Hanford production reactors, and consequently, a definitive link between changes in the aquatic ecology and fisheries and the operations at Hanford is difficult to establish. Without segregating the effects of dams, irrigation and Hanford operations, it is unlikely that any discernible deleterious environmental effect can be attributable to Hanford production reactor operations.

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APPENDIX A

HISTORICAL HAMFORD PRODUCTION REACTOR OPERATING STATISTICS

		T	7	,			
	GWD			62.8	58.1	55.7	61.1
AVG	Ş N N	2036	2025	2151	2167	2084	2215
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	HGP						
	Z						
	Κ						
	KE				,	,	,
TOR	I	485	469	493 94.2	490 82.5	78.7	489 85.4
REAC	u.	325	359	391 96.1	394 84.0	372 87.9	422 92.4
	DR	461	448	494 97.3	469 88.4	422 85.2	441 86.3
	۵	370	361	376 91.9	402 96.1	401 87.5	431 96.3
	ပ						
	8	395	388	397 90.9	412 96.7	398 94.0	432 100
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	19/1	2/51	3/51	4/51	5/51	15/9
	REACTOR	PARAMETER B C D DR F H KE KW N HGP N* MW	PARAMETER B C D DR F H KE KW N HGP N* MW AVG. OP. MW 395 370 461 325 485 8 2036 TEMP. IN- °C TEMP. IN- °C TEMP. OUT - °C TEMP. OUT - °C EMP. OUT - °C	REACTOR Avg. op. mw 395 370 461 325 485 RW N HGP N* Avg. T.O.E % FLOW - KGPM TEMP. IOL - °C Avg. op. mw 388 361 448 359 469 2025 Avg. op. mw 388 361 448 359 469 8 2025 TEMP. IN - °C TEMP. IN - °C TEMP. OUT - °C TEMP. OUT - °C Avg. out - °C	REACTOR Avg. op. mw 395 370 461 325 485 RW N HGP N* MW T.O.E % T.O.E % 170 G. MW 388 361 448 359 469 359 469 359 469 361 494 391 4942 4942 4942 4942 4944 4944 4944 4944 4944 4944 4944 4944 4944 4944 4944 4944	REACTOR PARAMETER B C D DR F H KE KW N HGP N* MW Avg. op. Mw 395 370 461 325 485 9 2036	REACTOR AVG. OP. MW 395 370 461 325 485 R K K N HGP N* MW TO. E

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	GWD	55.8	62.3	61.1	62.1	62.6	9.09
9/4	į N N	2194	2354	2386	2309	2314	2336
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	НВР						
	Z				,		
	ΚW						.1
	KE						
REACTOR	I	514 86.9	512 79.0	538 75.6 41.4	513 95.6 41.6	529 96.0 42.5	545 92.3 42.5
REAC	Ŧ	386 59.3	93.1	436 84.6 37.7	405 74.4 37.9	418 99.8 37.7	394 53.6 37.4
	DR	499 87.7	528 95.6	528 96.0 41.3	521 91.0 40.8	466 85.8 40.1	489 85.8 40.7
	D	403 84.9	439 82.5	434 74.2 37.4	440 87.4 36.6	456 81.9 36.7	477 93.8 38.1
	၁						
	В	392 88.2	398 78.2	450 96.1 36.5	430 81.8 36.9	445 87.1 36.7	431 86.7 36.4
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW. T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	7/51	8/51	19/6	10/51	13/11	12/51

<u>.</u>	GWD	62.5	0.19	6.99	6.89	72.6	70.8
AVG.		2273	2418	2563	2555	2562	2614
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	ндь					,	
	Z						
	ΚW						
	KE						
REACTOR	I	559 96.7 42.6	558 91.7 41.1	559 88.6 42.4	582 93.8 42.9	506 76.7 43.4	532 90.0 43.4
REA(LL	451 83.4 36.7	512 78.8 37.5	496 51.4 36.8	496 84.6 36.5	509 99.8 37.0	461 78.7 36.8
	DR	361 85.5 40.2	380 78.1 40.7	536 94.4 41.1	532 90. 1 40.8	548 97.0 41.6	546 96.3 42.0
	۵	462 90.2 37.5	478 92.1 38.1	448 91.1 38.1	513 94.6 38.7	532 93.2 39.0	551 94.5 39.7
	ပ						
	82	440 85.0 36.4	490 92.1 36.1	524 94.1 35.0	452 85.2 36.3	467 89.5 36.5	524 89.9 36.4
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	1/52	2/52	3/52	4/52	5/52	6/52

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·						REA(REACTOR							
DATE	PARAMETER	В	၁	D	DR	щ	I	KE	KW	Z	HGP	*	AVG.	GWD
1/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	466 18.2 37.8	697 99.7 64.1	540 74.6 38.5	563 92.6 42.6	448 59.2 38.3	617 92.6 47.7	ì					3331	78.8
2/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	494 82.3 38.3	733 93.9 64.0	384 14.0 44.5	558 91.5 42.5	543 91.7 38.4	655 94.6 47.8						3367	77.8
3/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	526 91.1 38.1	764 91.3 71.2	543 84.3 44.9	485 1.7 	548 87.1 38.7	641 96.4 47.3						3507	84.9
4/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	533 78.8 38.3	852 88.2 72.0	548 92.7 44.7	500 77.2 42.6	562 91.1 39.0	660 15.5 	n					3655	80.4
5/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	539 93.4 38.5	876 81.1 73.9	594 90.1 46.7	415 80.4 42.9	595 92.8 39.3	586 65.8 49.7						3605	93.6
6/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	559 88.9 38.6	871 87.7 75.1	653 89.2 47.2	369 94.5 43.3	576 54.9 39.2	634 87.6 51.0						3662	91.9

						REACTOR	:TOR						AVG.	
DATE	PARAMETER	89	ပ	Q	DR	L	I	KE	ΚW	Z	НСР	*2	MW	GWD
7/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	519 91.8 38.5	866 99.9 74.5	605 82.4 47.5	530 91.3 43.6	584 90.1 38.9	762 94.8 52.6						3866	116.7
8/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	557 93 39.0 19.2 75.2	939 89.2 74.1 18.4 70.6	598 87.5 47.3 20.0 70.6	334 99.9 43.4 19.3 67.4	562 92.3 38.5 19.6 76.7	732 90.8 52.5 19.6 74.4				4		3722	105.3
9/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C	521 78.8 38.9 18.0 72.1	978 80.4 73.7 16.8 71.3	640 92.6 47.4 17.8 71.6	351 99.9 43.2 17.9 66.3	581 87.4 39.2 17.8 78.9	638 65.0 52.5 18.0 69.5						3709	91.9
10/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	541 81.3 39.3 15.5 71.8	945 71.4 72.7 15.3 69.1	663 93.4 47.1 16.0 70.1	531 91.8 42.9 15.6 62.6	631 95.6 39.2 15.7 75.8	707 83.0 52.7 15.9 70.1						4018	105.8
11/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C	625 91.3 39.1 11.4 76.1	1000 92.0 72.2 10.8 65.5	649 82.9 46.5 12.4 68.3	512 87.9 42.5 12.1 59.1	633 86.9 40.0 12.1 75.3	795 90.3 52.2 11.9 76.0						4214	112.4
12/53	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	664 68.7 39.5 8.1 77.3	976 68.6 82.5 7.7 56.4	739 81.9 46.7 9.4 76.7	544 99.8 42.8 8.6 56.7	658 87.8 39.3 8.9 77.7	869 93.4 52.7 8.6 75.4						4450	117.7

	GWD	123.8	The second state of the second state of	98.5		114.1	114.8	119.5	130.1
AVG	Ş M M	4646		4470		4762	4891	4850	5045
	*		-						
	HGP								
	Z		**************************************						
	ΚW								
	KE								
REACTOR	I	754 71.7 52.8	5.8 5.8 56.6	889 89.6 52.5	6.4	877 81.1 52.5 6.5 74.3	891 84.1 52.4 9.7 79.3	797 66.7 52.3 12.3 77.8	899 95.6 52.6 14.1 82.6
REA	ч	704 77.3 38.8	4.9 68.8	628 70.0 45.2	6.4 74.0	713 78.7 45.5 6.9 76.3	737 82.3 45.6 9.6 78.2	701 68.6 45.0 12.6 78.0	718 89.0 45.9 14.3 80.3
	DR	593 95.9 12.5	5.8 64.9	388 94.1 42.7		566 75.7 43.1 6.3 66.8	642 83.0 43.0 9.4 73.8	652 94.9 43.1 12.7 68.7	620 77.8 42.8 14.0 70.7
	D	814 99.8	6.2	796 87.8 47.8	6.8	787 89.7 47.7 6.5 74.5	741 77.8 46.8 9.6 73.9	776 86.2 47.7 12.7 74.8	760 96.2 47.5 14.2 73.7
	ပ	1074 82.8 81.7	4.8 63.0	1096 69.4 81.5	5.6 63.6	1191 82.3 81.7 5.3 65.3	1172 70.9 82.0 8.6 64.5	1199 75.4 88.7 11.6 69.6	1227 73.6 89.2 13.4 67.6
	8	707 90.3		673 67.8 40.0		628 46.6 45.5 6.3 71.6	708 74.7 48.4 9.7 73.0	731 89.8 48.5 13.0 74.8	821 87.8 48.7 14.4 84.9
	PARAMETER	AVG. OP. MW T.O.E %	TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM	TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	1/54		2/54		3/54	4/54	5/54	6/54

						REACTOR	TOR						9/4	
DATE	PARAMETER	8	C	Q	DR	u.	I	KE	X M	Z	НВР	*	ž N N	GWD
7/54	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN. °C TEMP. OUT - °C	817 78.8 47.4 17.4 83.2	1182 75.7 88.8 16.1 67.3	739 92.2 48.3 17.7 76.1	610 89.6 42.8 16.5 76.3	781 96.1 45.5 17.5 82.0	908 89.9 52.5 17.3 83.1						5037	134.3
8/54	AVG. OP. MW T.O.E % FI.OW - KGPM TEMP. IN - °C TEMP. OUT - °C	829 75.1 48.7 18.5 85.7	1201 81.0 89.9 17.7 72.6	755 91.9 48.3 18.5 80.0	662 99.8 43.0 18.5 85.8	755 89.0 46.3 18.6 84.2	857 87.7 52.5 18.0 82.2						5059	135.6
9/54	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	809 88.7 48.1 17.2 84.2	1276 78.6 90.6 16.5 71.8	735 99.9 48.8 17 å 74.8	639 100.0 42.7 17.4 73.8	760 87.8 46.3 18.5 84.4	851 94.7 52.1 17.7 80.3						5070	137.0
10/54	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	851 82.9 47.7 13.6 85.7	1247 766 8.12*87.4 87.2 48.5 13.2 14.5 71.1 78.0	766 87.4 48.5 14.2 78.0	599 86.9 42.7 14.2 71.8	816 95.9 46.4 14.1 88.5	703 57.6 52.0 14.1 75.9						4982	127.0
11/54	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	897 88.6 47.7 11.5 85.7	1268 67.5 85.4 11.2	766 75.2 50.8 10.8 72.3	654 89.7 41.7 11.2 74.2	757 70.2 46.2 12.6 86.1	863 94.5 51.9 10.9 76.2						5205	124.8
12/54	AVG. OP. MW 1.0.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	961 87.3 47.8 7.4 89.2	1307 65.0 84.3 6.9 76.4	910 71.9 51.7 8.5 84.0	689 90.6 42.2 7.9 71.7	897 81.8 46.6 8.3 86.0	925 93.3 51.5 7.5 78.7						5689	141.5

 \star Data source lists suspected value of 8.12%. Value 81.2% was used in computation of GWD.

						REACTOR	CTOR						AVG	
DATE	PARAMETER	8	၁	D	DR	щ	I	KE	ΚW	Z	HGP	*	N N	GWD
1/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	918 75.5 48.1 6.2 85.6	1234 71.7 82.3 5.5 76.7	996 86.5 52.7 6.6 85.7	734 96.2 42.0 6.4 75.8	933 86.9 46.5 6.6 85.9	952 75.0 52.5 6.0 76.8						5767	144.8
2/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	841 67.6 48.2 5.2 84.1	1358 65.7 82.8 4.3 74.8	888 75.8 58.8 4.7 77.3	680 83.0 41.5 4.7 71.3	952 13.7 	944 80.6 52.2 4.7 80.0						5663	111.3
3/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	867 84.6 48.8 5.9 81.8	1350 69.5 81.8 5.1 74.8	951 73.9 53.2 5.5 84.2	735 93.0 41.1 6.0 75.1	864 95.6 45.9 6.3 78.5	959 78.5 52.6 5.5 80.0		861 93.4 124.0 4.5 37.7				6587	168.7
4/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	794 87.3 48.7 8.1 83.7	907 66.3 82.7 7.1	708 79.5 52.9 8.0	350 50.1 41.0 7.2 74.7	566 64.5 52.9 8.4 89.2	920 91.9 126.3* 8.0 81.3	168 63.9 124.3* 7.4 37.3	734 77.3 * 6.7 37.1				5327	120.2
5/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	819 89.5 48.8 12.1 84.4	838 63.7 83.0 11.2 78.2	641 78.3 52.4 12.7 84.9	593 77.8 49.8 12.0 82.3	627 67.7 47.6 12.6 89.6	724 77.8 52.9 12.5 83.7	903 89.7 128.2 11.6 43.4	914 88.3 127.1 10.9 45.5				6059	149.9
6/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	773 85.5 48.5 15.4 87.8	933 69.5 83.4 14.0 80.2	481 60.5 52.4 14.8 83.4	799 93.0 49.8 14.8 78.9	446 50.6 46.8 15.3 86.4	715 77.2 53.0 15.3 84.7	999 93.9 129.3 14.6 46.8	970 88.1 127.3 13.6 45.7				6116	147.4

*Data source is suspect for these values, they should probably be offset one column to the right.

						REA	REACTOR						AVG	
DATE	PARAMETER	8	၁	D	DR	ட	工	KE	KW	Z	HGP	*	N N	GWD
7/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	922 25.6 48.4 15.3 87.5	1365 74.2 84.1 16.2 82.3	866 41.6 52.8 17.5 86.4	885 82.7 50.1 17.0 85.4	836 67.1 47.3 17.4 89.3	931 92.2 53.5 16.8 85.0	1086 99.6 128.6 16.7 49.4	1055 83.0 128.7 15.8 50.0				7946	177.2.
8/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	938 86.3 48.4 19.3 89.4	1351 79.6 83.0 17.8 82.7	863 73.4 53.2 19.8 88.5	872 88.8 50.3 19.5 86.9	801 61.9 47.2 19.9 88.9	937 55.3 57.1 19.5 92.0	1006 83.1 128.5 18.5 52.2	1036 73.9 130.0 18.4 50.7				7804	183.2
9/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	861 91.1 48.2 17.5 90.0	1278 56.2 83.1 16.2 77.5	900 60.4 53.1 18.0 90.0	641 80.4 51.0 17.5 83.9	747 38.8 46.9 18.0 88.8	965 70.2 57.1 17.7 80.4	1068 89.8 126.4 16.7 51.5	1099 56.8 128.8 16.6 49.2				7559	153.4
10/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	912 96.4 47.8 14.0 84.5	1358 72.9 83.0 13.1 81.8	853 42.7 53.2 16.4 82.3	948 74.4 51.0 13.6 92.3	820 45.8 47.3 14.4 85.4	1020 63.5 56.9 14.4 87.4	1240 63.8 136.7 13.4 63.5	1386 80.2 127.4 12.7 64.0				8537	181.8
11/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	875 63.8 47.5 10.1 83.6	1313 57.6 82.1 9.0 71.8	878 48.3 52.1 9.3 82.3	1033 94.5 50.5 9.2 89.8	784 47.4 45.9 10.3 85.0	1071 85.1 56.7 9.8 85.1	1537 85.9 125.3 8.3 62.3	1592 77.7 127.9 8.9 62.9				9083	196.7
12/55	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	895 90.9 46.6 5.5 81.3	1413 68.3 83.8 5.5 78.2	843 19.6 52.0 6.3 80.3	862 74.9 49.6 5.9 85.4	867 69.6 47.0 6.7 84.9	915 64.9 56.1 6.3 80.5	1846 90.6 125.5 4.9 64.9	1763 90.1 125.0 4.4 61.8				9404	218.5

						REACTOR	:TOR						9//6	
DATE	PARAMETER	В	၁	D	DR	u.	I	KE	ΚW	z	HGP	*	ë M M M	GWD
1/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	784 57.8 47.1 1.8 75.2	1432 56.4 84.0 1.4 76.8	885 58.6 51.1 2.6 54.6	833 73.4 50.0 5.4 85.6	829 36.2 45.9 3.2 82.5	1042 64.0 55.7 5.9 82.5	1882 75.0 124.0 4.1 65.5	1814 79.5 122.5 2.1 63.4				9501	192.6
2/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	826 60.0 46.1 4.2 80.8	1461 73.7 83.8 3.6 78.5	633 41.8 49.9 3.4 77.9	828 72.3 49.8 4.8 80.9	888 45.3 47.0 5.4 81.5	957 69.5 55.4 5.0 84.0	1766 86.5 139.0 3.4 58.3	1849 91.5 136.0 3.0 64.0				9208	194.9
3/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	841 60.4 46.1 6.5 84.0	1504 74.3 83.2 5.0 79.5	886 62.7 49.9 6.5 82.5	898 73.7 50.3 5.9 77.8	781 48.5 46.9 6.4 70.8	1052 77.6 55.6 6.0 82.0	1930 90.0 140.0 4.8 59.8	1963 86.7 134.0 4.2 63.5				9855	231.8
4/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	897 87.0 45.8 10.0 84.2	1532 79.6 83.9 9.4 81.8	922 68.3 49.8 9.6 84.7	924 85.1 50.2 10.1 80.2	834 39.5 47.0 9.0 82.2	1119 70.1 56.4 8.5 86.0	1979 88.1 140.0 8.9 68.5	1823 84.3 138.0 8.0 62.2		·		10030	234.3
2/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C	842 83.3 46.0 14.3 84.3	1400 74.6 83.0 12.8 81.0	831 55.3 49.9 9.8 84.8	901 79.5 51.2 13.0 84.3	834 57.9 46.7 14.7 87.4	1015 63.0 11.0 12.6 86.6	1887 92.0 138.0 12.1 68.1	1789 84.2 140.0 12.6 66.0				9499	225.9
94/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	834 80.5 45.8 15.0 85.0	1492 84.4 84.4 13.9 84.0	853 73.5 50.1 14.0 85.0	933 95.1 51.0 15.0 84.8	858 43.8 7.6 14.3 84.6	942 61.2 16.8 14.3 86.2	2038 88.2 141.0 14.2 72.8	1875 88.6 136.0 14.0 70.9	:			9825	235.7

						REACTOR	TOR		ı				AVG	
DATE	PARAMETER	89	ပ	Q	DR	ட	I	KE	ΚW	Z	ндь	*2	MW	GWD
7/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	815 95.3 46.4 18.3 84.9	14.17 77.0 85.8 17.0 86.3	764 51.9 51.2 17.7 83.1	901 88.8 51.7 18.3 84.3	772 52.4 47.6 18.8 84.8	955 61.3 57.2 18.9 87.6	2146 83.3 143.0 17.8 79.6	1894 90.5 146.0 17.2 73.1				9694	235.0
8/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	772 77.8 46.5 19.8 84.8	1418 73.9 85.0 18.4 85.5	847 78.2 51.0 20.4 84.5	886 92.7 51.8 19.4 86.5	790 77.1 47.4 20.4 83.0	1010 71.4 56.7 21.1 91.0	1986 80.6 145.5 20.2 78.0	2069 86.7 147.0 19.0 77.5				9778	243.6
95/6	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	784 68.8 46.2 19.8 86.4	1299 76.3 86.0 18.4 82.2	841 87.1 50.3 19.9 87.4	902 90.9 51.5 19.1 87.4	793 72.3 47.0 19.0 85.5	982 75.6 56.4 18.4 87.8	1811 71.4 149.0 17.0 76.8	2202 82.4 147.0 18.0 72.1				9614	225.2
10/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	0 0 14.0	1276 92.9 84.2 13.0	879 91.2 49.5 15.6 85.8	904 86.0 51.5 16.5 84.9	805 75.2 48.0 14.9 86.5	1034 91.0 56.5 14.8 87.5	2261 85.3 149.0 13.0 79.2	2337 87.5 149.0 13.0 80.5			,	9496	256.8
11/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	0	1308 75.0 84.0 9.5 75.3	932 68.8 51.0 10.4 86.8	938 86.4 52.0 10.1 86.3	875 86.6 48.0 11.0 86.7	1079 86.8 56.3 10.5 87.7	2464 86.2 149.5 9.0 76.0	2448 83.8 148.5 8.9 77.9				10044	249.6
12/56	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	938 61.2 69.0 7.0 69.8	1411 78.9 84.0 7.3 73.5	963 84.9 51.3 9.6 87.3	1077 100.0 51.8 8.4 88.2	914 73.2 47.7 8.1 80.4	1045 73.1 56.0 9.6 82.7	2294 57.6 147.0 6.0 73.0	2573 88.2 148.0 6.6				11215	266.8

	GWD	5 266.7	237.2	256.9	285.8		3 272.7
AVG	MW	11625	11750	10999	11506	12026	11219
	* 2						
	HGP						
	Z					'	
	ΚW	2513 80.5 147.0 1.0 71.9	2529 84.9 150.0 2.6 77.0	2837 89.9 149.0 5.6 79.0	2824 83.9 150.5 7.8 84.0	2663 87.6 150.5 12.1 84.5	2565 85.0 155.5 16.4 83.9
	KE	2586 80.5 146.0 1.8 72.1	2686 84.1 148.0 3.9 78.0	2628 72.0 149.5 5.2 81.7	2678 85.7 45.5 7.5 78.3	2478 79.8 150.0 13.0 82.4	2576 80.2 161.0 15.8 82.8
TOR	I	1112 82.1 56.1 5.0 83.1	1161 84.8 56.1 5.8 86.0	1153 72.2 56.9* 7.8 88.8	1140 78.8 56.1 10.1 88.8	981 25.3	0
REACTOR	ıL	972 68.0 47.8 4.8 87.8	1008 83.2 48.2 5.2 90.0	1010 71.8 47.4 6.7 90.8	00000	1058 40.4 72.9 13.6 79.5	1074 75.0 73.0 16.9 80.0
	DR	7.0	1042 32.0 71.5 5.1 70.0	1100 78.1 68.9 7.5	1205 85.7 69.1 10.3 80.7	1151 78.0 69.2 13.1 82.2	1213 84.6 70.5 16.3 87.0
	a	1031 84.6 51.1 3.2 86.2	1029 37.8	00	1084 80.4 67.2 10.0 80.7	1116 63.8 71.0 13.0 77.3	1145 77.1 71.0 16.5 84.8
	ပ	1326 83.1 81.2 2.9 68.8	1265 64.1 81.6 4.4 72.0	1324 69.6 82.9 6.5 73.2	1348 74.1 83.0 8.1 74.9	1427 94.6 83.6 13.3 80.6	1410 86.6 85.0 15.5 83.5
	8	979 89.2 71.0 3.0 62.3	1030 69.9 70.2 3.5 66.0	1147 59.8 71.0 5.5 72.1	1227 86.4 71.0 9.1 79.9	1152 67.4 70.5 14.1 83.8	1236 73.6 71.7 16.2 87.8
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	1/57	2/57	3/57	4/57	5/57	6/57

* Value given in source is 56.9 gpm

	GWD	296.5	273.3	294.7	324.5	321.0	319.1
AVG.	MW	12725	11726	12451	12825	13273	13158
	* 2						
	нВР						·
	Z						
·	ΚW	2848 75.7 165.0 18.1 89.0	2706 81.7 165.5 18.2 87.0	2511 82.8 162.0 18.0 84.8	2739 85.8 164.0 14.8 81.8	2874 80.7 152.5 10.5 87.0	2918 82.0 155.5 6.0 79.9
	KE	2603 80.4 162.0 19.1 86.7	1576 45.7 165.5 	2300 85.0 164.0 18.1 82.1	2639 84.9 153.5 15.8 85.9	2794 82.3 152.0 12.7 85.3	2632 76.1 153.0 7.0 81.9
CTOR	I	1124 63.7 69.4 20.2 85.4	1186 80.2 69.0 21.4 89.2	1198 77.4 70.3 20.1 87.7	1201 78.9 71.4 16.7 87.1	1237 84.3 69.0 12.5 83.2	1245 83.7 70.3 8.8 82.6
REACTOR	ட	1222 90.5 73.2 19.6 87.1	1207 76.4 72.5 20.8 89.3	1276 80.0 71.5 19.9 91.9	1060 56.8 70.2 15.3 84.5	1246 82.1 71.2 11.1 83.8	1260 76.6 71.5 9.8 81.2
	DR	1254 78.2 71.8 19.0 88.3	1244 88.0 70.7 18.9 88.0	1268 82.0 70.0 19.3 90.0	1241 71.5 70.4 15.9 90.2	1253 76.8 69.8 12.0 88.2	1222 58.9 69.1 9.8 88.2
	Q	1216 83.4 70.9 19.0 89.0	1204 83.8 70.5 21.1 92.9	1218 72.3 71.0 18.9 88.0	1269 92.0 71.2 15.5 87.3	1242 78.8 71.0 13.6 84.6	1272 83.0 70.4 8.7 83.7
	ပ	1335 50.9 85.5 18.7 84.8	1368 74.3 85.8 19.0 85.6	1436 71.7 87.0 19.0 85.8	1352 85.1 82.0 14.8 86.5	1329 76.1 82.5 10.4 78.0	1372 78.7 71.2 7.6 77.4
	c	1123 73.1 71.0 19.1 91.3	1235 72.1 71.0 19.5 92.3	1244 71.7 71.0 19.4 93.0	1324 84.8 71.6 16.2 89.2	1298 82.0 71.5 10.6 84.1	1237 83.7 71.0 7.4 79.0
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	7/2/	8/57	9/57	10/57	11/57	12/57

						REACTOR	TOR				:		AVG	
DATE	PARAMETER	œ	ပ	۵	DR	ட	H	KE	ΚW	z	нСР	* 2	M M M	GWD
1/58	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	1333 74.1 70.8 7.6 82.8	1472 91.7 84.5 7.5 76.0	1265 87.5 71.0 8.3 80.8	1338 90.2 70.7 7.5 84.4	1297 71.4 71.4 9.2 83.2	1299 86.2 70.3 8.5 84.0	2765 74.9 152.5 7.5 81.9	2847 78.9 154.0 7.2 80.4				13616	341.1
2/58	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1286 80.8 70.8 8.0 84.1	1356 71.7 85.2 7.8 77.0	1291 88.7 70.9 8.0 83.8	1331 76.4 70.5 7.5 84.5	1329 89.3 72.4 8.0 81.6	1335 84.4 70.8 7.6 84.4	2877 78.7 153.5 7.2 81.0	2018 75.6 154.5 6.8 72.5	• .			12823	287.8
3/58	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1218 71.7 70.6 7.9 83.3	1454 80.6 85.5 7.8	1305 79.5 71.2 9.4 84.2	1323 78.3 69.6 7.8 86.3	1342 76.7 72.2 9.2 82.9	1331 80.7 71.1 7.2 82.3	2790 67.7 158.0 7.5 82.9	2454 70.4 155.5 7.0 83.8				13217	305.0
4/58	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1306 84.8 70.8 11.8 86.2	1460 86.2 90.2 11.0	1335 84.9 70.2 10.3 88.0	1261 64.1 70.6 9.0 85.3	1351 84.2 72.5 11.3 84.3	1374 45.7 71.5 9.7 87.3	2550 73.8 173.0 8.9 74.9	2796 91.1 157.0 9.8 77.5				13433	315.1
5/58	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1330 77.8 71.0 15.9 90.6	1425 79.7 92.3 14.2 84.2	1275 82.2 70.7 14.8 90.0	1256 69.2 73.1 14.1 87.2	1348 81.6 73.0 14.5 88.1	1386 86.7 71.5 15.0 92.6	2462 72.7 157.5 14.8 79.8	2589 82.9 172.5 15.0 78.2				13071	320.0
6/58	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1361 81.1 71.0 17.2 92.8	1582 88.1 94.0 18.0 86.1	1224 82.5 71.0 17.2 91.5	1368 90.3 73.4 16.2 90.7	1392 86.6 73.0 17.3 91.3	1363 84.0 74.1 17.1 90.8	2853 92.2 157.0 17.4 86.8	2814 88.6 172.5 16.5 84.0				13957	366.5

	GWD	338	329.4	324.7	341.6	267.2	370.1
	AVG.	13269	13160	13501	13383	13746	13798
	*						
	НСР						
	Z						
	ΚW	2536 80.6 173.5 20.4 83.0	2573 87.0 173.0 20.1 85.7	2804 87.0 172.5 18.8 85.5	2900 91.7 172.0 17.7 85.8	3090 7.8 	2385 80.9 171.0 8.0 71.9
	KE	2707 93.0 147.0 20.0 83.7	2711 80.1 174.0 21.3 87.6	2838 85.4 175.5 19.0 86.1	2508 76.9 172.0 18.0 83.9	2757 91.6 172.5 8.5 71.4	2859 84.1 172.5 8.1 77.7
REACTOR	Ξ	1326 84.7 74.5 21.7 93.5	1280 88.0 74.9 22.0 92.9	1273 78.6 76.8 20.2 92.5	1265 76.0 79.3 16.8 86.9	1365 93.7 80.9 9.5 78.2	1440 100.0 80.6 9.1 78.2
REAC	щ	1357 85.9 73.7 21.6 93.5	1321 82.1 75.5 22.6 91.2	1227 78.2 75.1- 21.5 89.0	1317 97.4 75.2 17.0 86.9	1252 65.7 80.5 10.2 75.7	1439 100.0 80.0 9.9 78.1
	DR	1347 66.9 73.6 21.4 93.5	1278 67.2 73.2 21.8 88.9	1278 71.5 74.2 19.1 91.0	1215 57.7 76.5 16.1 86.1	1245 63.1 76.9 9.3 79.0	1336 72.6 78.9 8.7 78.2
	O	1270 78.7 75.2 22.0 90.9	1242 87.0 77.5 22.4 89.8	1333 85.0 78.7 20.1 89.1	1399 94.5 78.7 16.9 86.8	1399 92.2 78.8 10.0 79.3	1403 90.2 80.2 9.5 78.1
	ပ	1460 77.1 94.5 20.7 87.5	1482 71.1 94.0 21.8 89.0	1481 74.3 95.0 18.5 87.7	1482 78.5 93.8 15.3 83.1	1284 62.3 93.5 8.6 79.1	1581 83.3 94.2 8.1 77.8
	83	1266 82.0 73.3 21.2 91.7	1273 79.4 72.3 21.9 91.6	1267 67.4 73.9 20.0 90.0	1297 77.1 75.3 16.2 87.4	1354 85.9 76.2 9.3 77.6	1355 86.6 76.8 8.1 79.2
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	7/58	8/58	9/58	10/58	11/58	12/58

					,	REACTOR	:TOR						27.6	
DATE	PARAMETER	В	၁	D	DR	u.	I	KE	ΚW	Z	HGP	*	MW	GWD
1/59	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C	1345 53.3 78.2 6.1 76.8	1509 69.2 94.8 5.7 76.3	1404 86.5 79.4 6.7 76.3	1360 78.9 78.4 6.1 75.6	1362 76.0 81.2 7.5 74.4	1368 70.6 81.4 6.2 77.3	2922 90.6 171.5 5.1 76.2	2824 85.7 171.5 5.6 74.8	,			14094	344.6
2/59	AVG. GP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1458 87.7 78.0 4.8 78.0	1695 75.5 94.5 4.7 77.8	1435 92.0 79.9 5.4 79.2	1502 99.9 80.0 4.4 79.3	1498 100.0 81.2 5.9 78.2	1494 83.5 81.2 5.0 80.3	3189 92.4 172.5 4.1 77.0	3038 92.4 171.5 3.8 74.6				15309	388.6
3/59	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1468 86.3 79.0 7.0 80.8	1760 74.3 95.3 6.0 79.5	1437 78.7 78.4 6.4 82.9	1466 82.9 80.2 6.0 83.8	1415 65.4 81.4 7.4 77.2	1599 100.0 81.8 6.9 81.9	2775 78.5 171.5 5.2 78.6	3119 87.5 171.0 5.2 77.3				15039	382.9
4/59	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1468 92.1 79.9 9.5 81.3	1625 70.3 94.2 9.5 86.0	1458 83.8 78.4 10.1 88.0	1426 80.7 80.2 9.0 86.2	1509 86.8 82.3 10.6 80.8	1530 83.4 82.5 9.0 83.4	2747 45.3 157.5 6.7 79.3	3148 84.5 173.5 8.5 81.3				14911	340.7
65/5	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1444 73.8 80.0 11.7 86.7	1737 82.2 95.0 12.1 85.2	1457 92.6 78.6 12.6 87.5	1479 89.3 79.3 11.5 86.5	1399 53.4 82.3 12.6 82.8	1480 81.5 83.0 12.0 86.0	2493 53.2 174.5 11.1 78.8	2752 81.0 176.5 12.0 78.4				14241	330.8
6/29	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1471 82.9 83.1 14.7 87.7	1693 81.9 95.2 14.3 87.2	1412 73.2 78.9 15.6 90.5	1471 81.4 79.5 14.4 87.6	1356 83.2 82.2 15.0 84.2	1428 80.4 85.2 14.7 85.7	3040 88.8 175.0 13.9 83.8	2882 89.0 178.0 13.9 78.5				14753	371.2

						REACTOR	:TOR						977	
DATE	PARAMETER	8	ပ	D	DR	Ŧ	H	KE	ΚW	Z	НВР	*	MW G	GWD
7/59	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	1477 89.1 83.0 18.6 90.9	1715 84.8 95.3 18.2 88.6	1429 90.6 81.0 18.0 92.1	1399 71.8 82.0 17.8 88.5	1483 80.8 82.2 18.1 87.6	1593 100.0 85.4 18.2 90.8	2739 76.0 175.0 17.4 85.4	2939 85.3 178.5 17.6 85.2				14774	385.9
8/59	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1457 77.5 82.8 18.8 91.1	1731 83.5 95.8 18.3 89.9	1484 83.0 81.0 18.8 92.8	1547 89.9 83.4 19.3 91.8	1462 87.7 85.4 19.5 88.3	1448 79.6 85.3 18.8 90.3	3044 83.5 174.5 18.6 90.8	3193 91.7 178.0 17.8 88.1				15366	406.1
65/6	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1499 83.3 82.8 17.2 88.2	1615 65.4 96.4 16.7 87.0	1520 94.3 81.1 17.7 92.0	1498 94.4 82.0 17.5	1401 70.5 83.6 17.6 86.3	1543 83.4 85.8 17.9 89.0	3142 88.2 174.5 16.5 89.1	3300 88.0 178.0 16.3 89.3				15527	393.3
10/29	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1454 79.6 80.3 13.6 87.2	1760 94.4 95.2 13.7 88.3	1548 89.9 79.0 13.7 92.3	1497 80.8 80.2 14.6	1460 83.5 83.4 16.4 91.8	1581 84.3 84.5 14.1	3153 82.8 175.5 12.9 87.1	3302 78.9 178.5 12.7 86.8				15755	408.8
11/59	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1619 87.8 80.0 9.9 87.8	1812 77.9 95.0 9.0 84.8	1449 72.1 78.8 11.1	1603 93.8 80.0 9.3	1274 93.8 83.6 9.9 87.8	1631 85.2 83.4 10.0	3317 92.8 174.0 8.5 86.5	3415 90.9 179.0 8.3 85.7				16120	424.5
12/59	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1405 75.4 82.9 7.6 80.8	1756 77.0 96.0 7.4 81.5	1597 90.0 79.0 6.5 86.8	1543 75.3 79.9 6.4 84.0	1610 80.7 83.4 8.5 86.1	1636 89.0 83.2 8.6 90.0	3325 80.2 176.0 7.0 86.2	3406 90.1 179.5 5.0 83.6				16278	418.3

Times and proceeds						REACTOR	TOR					•	0,74	
DATE	PARAMETER	В	ပ	D	DR	F	I	KE	KW	z	HGP	*	MW.G	GWD
1/60	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	1540 81.7 80.5 4.8 84.0	1743 79.9 94.8 4.0 87.1	1595 74.4 77.7 4.2 88.2	1556 88.9 79.6 4.8 87.2	1624 79.1 83.3 4.5 86.6	1684 82.4 83.5 5.2 89.5	3549 85.3 178.0 3.3 81.7	3507 85.7 179.5 3.3 83.4			·	16798	431.7
2/60	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1594 74.8 80.0 4.0 84.9	1781 73.0 94.5 4.2 85.2	1639 86.7 78.2 5.5 91.2	1533 69.2 80.0 4.6 89.3	1699 68.8 83.5 5.2 88.2	79.1 84.0 5.1 89.4	3372 78.3 180.0 4.0 83.5	3598 82.5 179.5 3.5 83.5				16924	380.0
3/60	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1544 80.1 81.0 5.6 85.0	1783 81.6 95.0 6.2 86.2	1632 79.2 78.9 6.9 92.0	1733 84.6 80.0 6.5 92.5	1590 74.8 82.4 8.1 89.8	1761 79.2 84.2 6.6 91.8	3289 85.2 180.5 5.3 79.0	3540 82.3 180.0 5.4 83.1				16872	335.9
4/60	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1619 71.9 80.5 8.9 90.3	1842 70.5 95.5 10.3 86.8	1710 91.5 82.0 10.9	1754 89.5 82.8 10.8 93.0	1553 84.3 83.4 9.8	1759 77.1 87.5 11.5	3378 80.9 181.0 10.9 83.1	3560 87.3 179.5 9.2 85.9			:	17175	423.1
2/60	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1635 88.6 81.0 13.1 92.2	1851 86.6 94.5 12.7 89.0	1601 81.2 82.2 11.8	1580 73.1 82.5 12.0 88.8	1604 89.1 86.1 13.2 88.0	1765 79.0 86.8 11.7 93.3	3574 93.3 182.0 12.7 87.5	3327 90.4 180.0 12.2 88.1				16937	454.8
09/9	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1584 82.3 84.0 16.3 90.2	1805 78.8 95.8 16.0 90.7	1659 88.8 83.7 15.8 93.2	1594 92.6 84.1 15.9 93.0	1531 83.1 86.5 16.3 89.1	1675 63.4 86.6 15.8 93.1	3589 91.9 183.5 15.8 90.5	3553 94.5 180.0 15.0 91.4				16990	435.2

	GWD	409.1	418.7	425.4	420.6	456.3	471.5
AVG	M M	16486	16172	16683	16975	17737	18092
	*						
	н						
	Z		·				
	Κ	3413 86.2 179.0 19.2 91.9	3343 84.0 182.0 17.9 90.6	3493 88.7 181.5 18.0	3447 86.9 181.5 13.9 91.3	3701 50.4 182.0 9.8 91.3	3872 86.3 182.0 6.0 89.6
	KE	3368 78.6 180.5 19.5 91.3	3169 73.4 180.5 18.5 91.1	3515 94.5 180.0 18.0 94.2	3620 86.1 180.5 14.2 92.7	3742 83.6 179.5 10.5 91.4	3497 74.9 180.5 6.8 86.0
REACTOR	I	1622 77.3 87.2 20.5 93.4	1631 86.7 87.2 20.2 93.1	1596 87.0 88.0 20.0 93.2	1564 72.5 87.2 17.9 90.8	1673 81.4 87.1 13.0 93.3	1834 92.5 86.7 10.3 93.2
REAC	щ	1550 69.9 86.9 20.6 91.2	1575 87.4 87.3 20.0 93.2	1613 90.6 86.1 19.8 93.0	1605 67.4 86.8 16.3 91.2	1723 84.6 86.8 11.9	1760 83.4 86.7 9.8 89.4
	DR	1618 89.8 83.9 19.7 93.2	1454 85.6 83.5 19.7 92.9	1569 77.7 84.8 19.0 94.2	1665 65.3 85.0 17.6 94.3	1574 82.4 85.0 11.2 90.3	1715 89.4 84.2 9.0 88.9
	۵	1556 72.8 84.8 19.2 93.2	1571 85.2 85.0 19.5 92.8	1577 67.7 84.8 19.0 93.4	1652 89.5 84.8 15.4 90.9	1718 86.1 84.9 11.0 91.8	1773 92.6 85.3 8.3 89.9
	ပ	1792 78.5 95.8 20.0 92.9	1825 94.2 96.0 18.5	1809 79.5 95.8 18.4 92.3	1835 80.2 96.0 14.4 91.2	1929 87.7 95.0 10.0 89.5	1922 77.8 95.3 7.7 90.8
	\(\Omega\)	1567 81.5 85.3 20.0 93.0	1604 79.8 85.3 18.5 91.4	1508 78.6 85.2 18.7 93.1	1587 75.7 85.7 14.6 91.6	1677 86.3 84.8 10.5 90.3	1719 82.2 85.0 6.8 89.3
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	09//	8/60	09/5	09/01	11/60	12/60

						REACTOR	TOR							
DATE	PARAMETER	8	ပ	D	DR	ч.	I	KE	ΚW	Z	HGP	*	MV G	GWD
19/1	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C	1758 78.1 84.5 6.0 86.8	2011 87.5 95.5 5.8 90.2	1750 75.3 85.6 5.3 86.2	1746 73.6 83.0 6.8 92.8	1775 80.3 86.7 6.9 88.0	1709 65.5 86.2 7.4 90.0	3802 85.2 181.0 5.6 89.6	3900 90.3 181.5 5.8 88.9		·		18451	466.3
2/61	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1783 85.3 84.8 6.0 89.8	2072 81.0 96.3 5.7 91.1	1864 83.9 86.0 6.7 92.0	1871 94.3 86.1 5.7 91.2	1755 72.1 84.4 6.4 89.3	1659 63.4 86.3 6.0 90.3	3505 84.6 181.0 4.9 88.3	3930 93.8 182.5 4.6 89.0				18439	433.9
3/61	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1733 72.8 85.8 6.2 88.8	1971 76.0 96.0 8.1 91.3	1871 83.0 86.3 7.9 92.0	1764 77.9 86.4 7.0 89.0	1800 68.5 88.3 7.9 90.3	1836 82.3 86.4 8.0 93.3	3818 72.6 182.0 7.8 90.2	3810 74.0 182.5 6.1				18603	434.7
4/61	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1787 84.3 86.2 11.7 92.5	2006 81.8 95.5 10.9 93.7	1799 78.7 86.8 11.3 93.3	1628 65.6 87.2 9.7 89.0	1860 87.6 89.1 11.8	1752 83.5 86.4 12.4 91.1	3793 80.7 183.0 10.7 89.2	3867 85.6 183.5 10.4 92.0				18492	452.8
5/61	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1726 73.3 87.5 13.2 93.5	1971 80.0 98.5 12.7 93.8	1834 83.6 87.2 12.5 93.4	1803 79.8 87.8 12.3 93.7	1759 70.4 90.3 12.6 90.0	1616 55.6 86.2 13.5 92.0	3851 86.1 182.5 12.2 92.9	3821 87.7 184.0 12.2 92.0				18381	453.1
19/9	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1760 78.3 88.0 17.2 93.1	1908 70.6 99.8 15.5 93.9	1732 68.6 87.5 16.1 93.2	1769 82.8 90.1 16.0 92.9	1742 77.5 89.9 15.4 93.7	1655 77.9 87.8 16.5 93.1	3804 86.6 183.5 16.0 94.8	3807 83.5 184.5 15.3 94.6				18177	434.7

						REACTOR	TOR						AVG	
DATE	PARAMETER	. B	၁	D	DR	u.	I	KE	ΚW	Z	HGP	*	j N E	GWD
19/2	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	1709 79.8 88.0 20.9 93.3	1990 94.9 100.0 20.5 94.6	1656 71.9 87.9 21.3 93.3	1129 42.2 88.0 20.3 65.6	1657 51.6 89.9 20.2 92.6	1645 93.7 87.1 21.7 93.5	3647 87.3 183.5 19.9 94.5	3641 90.1 185.0 20.0 94.8				17074	427.2
8/61	AWG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1596 75.8 88.4 21.1 93.5	1863 60.8 100.2 21.2 94.8	1607 70.8 88.2 21.0 93.2	1369 81.4 88.5 20.9 90.1	1401 89.4 90.0 20.9 93.6	1554 73.7 86.3 22.5 93.0	3558 85.0 184.0 20.7 94.7	3506 79.3 185.5 21.4 94.6				16454	396.7
19/6	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1669 68.4 88.6 19.0 93.5	1933 85.4 101.5 17.6 94.7	1541 61.7 88.0 19.0 93.3	1614 65.0 88.7 18.7	1663 67.7 90.1 18.9 93.4	1442 51.5 86.3 20.0 91.9	3508 82.8 184.5 17.4 94.2	3629 87.9 184.5 17.0				66691	382.7
19/01	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1612 70.1 88.2 14.4 91.7	1970 80.1 100.0 14.1 94.5	1618 76.9 88.0 15.0	1591 59.3 88.0 14.9	1738 68. 5 90. 3 15. 9 93. 4	1605 81.9 86.0 15.5 93.1	3745 81.2 185.5 14.0 92.9	3752 89.2 185.5* 13.7				17631	427.4
19/11	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1717 47.2 88.0 9.3 91.3	2081 84.7 100.0 9.6 94.8	1687 63.5 88.0 12.7 93.2	1756 83.1 87.8 10.8 91.3	1799 71.6 89.9 11.8 93.5	1570 65.3 86.0 13.6 92.2	3816 89.4 184.5 9.6 89.3	3972 90.6 185.0 9.1				18399	432.8
12/61	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1648 65.1 88.0 6.3 85.6	1965 47.6 97.7 7.3 89.2	1924 63.4 87.8 9.0 93.2	1746 80.0 87.7 8.8 90.5	1822 75.3 90.3 9.3 88.6	1710 75.7 84.9 8.8 92.5	3870 78.0 184.0 6.6 92.7	4023 91.9 184.5 6.9 90.7				18708	434.2

* Source of data gives suspect value of 18.55 KGPM

						REACTOR	TOR						AVG	
DATE	PARAMETER	8	ပ	O	DR	L.	I	KE	ΚW	z	НВР	*2	MW	GWD
1/62	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C	1631 35.2 88.0 5.0 85.0	2082 74.1 97.7 3.0 89.8	1610 65.7 87.1 5.8 51.9	1734 50.6 87.8 6.2 87.8	1756 86.9 90.8 6.2 78.8	1613 54.7 85.3 3.9 83.1	4248 86.2 188.0 4.9 92.0	3977 73.4 185.0 3.6 90.4				18651	404.3
2/62	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1769 67.1 88.0 5.2 86.3	2173 69.1 98.0 5.4	1631 62.3 87.0 6.3 81.3	1825 91.1 87.7 6.7 88.1	1611 36.1 90.7 6.4 78.2	1723 54.7 86.1 6.4 87.1	4326 91.5 188.8 5.0	3917 82.9 185.5 4.0 93.6				18975	408.8
3/62	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1730 82.9 88.0 7.2 91.9	2216 63.9 101.5 6.6	1930 64.9 87.0 7.1 93.4	1728 35.7 87.2 5.0 85.0	1749 88.1 88.7 8.5 88.0	1746 81.5 85.7 8.3 89.2	4298 78.4 187.6 5.9 93.6	4222 90.5 186.5 6.3 94.6				19619	461.1
4/62	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1684 33.3 88.2 8.3 92.2	2140 77.2 100.5 9.0	1762 70.9 87.0 9.0	1648 69.2 88.0 8.9 8.9	1790 81.3 89.5 8.5 87.2	1698 48.9 86.3 9.4 91.8	4155 81.9 188.6 8.3 94.6	4085 82.5 188.0 8.4 94.5				18962	409.8
5/62	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1761 84.9 89.0 12.5 93.3	2074 52.2 101.5 11.7	1813 83.7 87.0 12.1 93.4	1734 89.3 88.0 12.1	1762 50.1 88.9 12.2 92.8	1693 41.1 86.1 11.0	3988 83.4 193.7 12.0 94.5	4051 86.6 188.0 11.6 94.4				18876	435.7
6/62	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1761 80.1 89.5 17.2 93.2	1909 44.6 100.4 16.5 94.2	1745 82.3 87.0 16.2 93.3	1619 38.3 87.0 16.0 93.1	1724 68.1 89.3 15.1 93.4	1689 59.6 86.1 15.5 93.1	4087 86.8 200.8 15.7 94.2	3983 88.6 188.5 15.0 94.0				18535	407.6

	GWD	4 436.2	2 364	1 494.3	5 502.6	9 385.0	1 462.9
97.4		19024	19302	1981	19705	19219	19261
	*			·			
	HGP	·					
	z						
	ΚW	4349 82.3 205.5 3.5 84.8	4253 59.5 204.0 4.9 86.4	4353 94.9 204.0 5.6 87.6	4206 78.4 206.0 8.9 90.2	3804 30.4 207.0 13.5 91.9	4337 100.0 206.5 14.9 94.4
	KE	4162 84.0 206.0 4.9 86.6	3989 62.2 205.0 4.8 86.5	4215 82.4 205.0 6.0 87.5	4336 93.0 205.5 9.3 90.4	4399 35.7 205.0 10.7 91.6	4201 75.8 205.8 15.7 94.5
TOR	I	1489 28.0 	1805 96.2 84.8 6.4 93.0	1861 92.9 84.3 7.9 93.3	1827 86.8 84.2 10.1 93.3	1687 70.7 84.6 14.6 93.4	1719 100.0 84.5 16.5 93.4
REACTOR	щ	1726 50.6 90.3 5.7 85.0	1843 89.9 90.1 6.1 84.8	1835 83.6 89.5 6.3 86.0	1792 94.2 89.3 9.3 87.2	1791 87.2 89.9 13.0 90.4	1751 73.9 90.2 15.1 92.6
	DR	1646 81.0 86.1 5.2 81.4	1721 44.0 85.6 5.2 85.3	1658 72.6 86.3 7.6 87.9	1810 87.7 86.9 10.0 87.1	1749 90.3 87.4 14.0 92.0	1737 86.0 87.0 16.0 93.6
	D	1790 79.4 87.8 4.8 89.5	1893 76.7 87.8 5.6 92.0	1879 45.1 87.3 7.9 92.5	1867 84.5 87.7 10.4 92.8	1823 94.6 87.5 14.4 93.3	1737 46.8 87.3 15.9 93.4
	၁	2021 82.0 97.8 3.8 88.1	2069 71.2 97.8 4.7 88.3	2146 62.8 97.5 6.2 88.8	2062 76.5 97.5 9.6 9.6	2181 95.1 100.0 14.5 94.5	2039 80.5 100.0 16.4 95.0
	В	1841 70.2 89.3 6.3 86.9	1679 52.5 89.0 6.7 87.7	1864 90.1 89.0 8.2 88.4	1805 78.0 89.3 10.7 88.2	1785 87.3 89.8 15.2 92.5	1740 54.4 90.7 17.0 94.9
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	1/63	2/63	3/63	4/63	5/63	6/63

						REACTOR	TOR						AVG	
DATE	PARAMETER	8	၁	D	DR	L	Ξ	KE	ΚW	Z	HGP	*	N N	GWD
1/63	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	1718 79.9 90.5 19.4 94.5	1978 89.7 100.0 18.7 94.6	1672 82.1 87.8 18.5 93.5	1691 82.2 97.0 18.3 93.6	1778 92.9 89.8 17.8	1652 87.7 83.7 19.4 93.8	3991 76.1 206.0 18.0 94.9	3957 73.3 206.5 17.8 94.5			·	18437	463.4
8/63	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1698 85.4 90.4 20.4 95.0	1915 81.8 100.2 19.7 93.8	1674 99.9 87.5 20.0 93.5	1657 86.7 87.5 19.1 93.5	1727 89.9 87.5 19.3 93.5	1573 88.7 83.5 20.9 94.5	. 4023 64.4 206.2 18.6 94.8	3555 19.3 210.0 19.3 94.1				17822	382.9
89/6	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C	1725 88.7 90.0 20.2 94.3	1868 61.6 100.0 19.2 94.8	1627 82.3 87.7 20.8 93.0	1651 91.0 87.1 20.4 93.8	1666 72.8 89.8 19.2 94.1	1554 58.3 84.6 21.7 94.6	3682 47.2 206.0 18.9 94.6	4144 100.0 208.0 18.7 94.6				17917	405.7
10/63	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1748 86.3 90.4 15.3 94.3	2020 93.0 97.5 14.7	1675 75.8 87.8 14.2 94.0	1707 83.1 87.6 14.6	1755 87.7 89.7 14.4 94.0	1663 93.5 84.7 15.4 95.0	4111 23.6 205.0 18.0 94.3	3957 80.7 208.0 14.6 94.2				18636	413.3
11/63	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1895 92.6 89.5 10.7 93.3	2018 77.6 96.0 10.1	1821 95.0 87.8 11.4	1781 83.5 86.3 11.9	1778 76.3 89.5 11.6 93.8	1782 100.0 84.9 12.9 94.7	4304 92.0 205.5 10.0 91.4	3870 26.9 208.0 10.0 89.8				19249	440.3
12/63	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1894 84.7 89.9 8.6 90.8	2134 75.1 99.5 8.0 94.2	1914 90.7 88.0 8.2 94.6	1813 77.8 87.1 8.2 93.4	1805 77.0 89.3 7.8 91.0	1771 85.4 84.5 9.4 93.6	4148 76.0 206.0 7.3 88.5	4194 82.6 208.0 7.6 87.7				19673	492.0

<u>د</u>	ن		C	<u> </u>	REACTOR	CTOR	7	KW	Z	d DH	*	AVG.	ON S
1853	Commercial	220]		1873	1906	1840	4351	KW 4393	2	HGF	2	20366	GWD
		77.0 96.2 5.6 94.1	79.9 88.8 6.6 93.4	88.9 87.6 6.7 91.5	51.9 89.1 6.8 90.1	34.0 93.3 8.2 88.4	68.1 205.5 5.8 5.8 87.1	4353 100.0 207.5 5.3 85.8	V			2007	? ? ?
1895 81.5 89.3 6.0 94.5		2262 79.5 97.8 5.7 94.2	1999 87.3 78.8 5.4 93.6	1928 86.9 87.6 5.8 94.2	1900 86.7 88.8 6.5 90.8	1967 93.8 93.3 7.0 92.5	4102 43.1 207.5 4.7 85.5	4396 41.5 207.5 4.9 85.5	·			20449	387.7
2030 51.7 89.2 6.3 94.8		2237 85.7 96.2 6.4 95.0	1996 91.5 88.0 7.5 94.4	1943 66.9 87.5 7.7 93.7	1954 66.3 89.1 7.6 94.0	2042 93.1 93.3 8.5 93.5	4402 100.0 206.0 6.1 87.0	4314 70.7 208.0 6.3 86.0				20918	519.0
1853 21 77.1 83 89.5 96 9.9 9	26	2178 83.6 96.0 9.4 94.7	1823 38.5 88.8 9.6 94.2	1880 68.4 87.2 10.2 93.4	1749 71.5 89.6 9.6 94.3	1709 43.4 93.3 10.5 91.6	4189 68.4 207.0 9.9 90.5	4362 89.1 209.5 8.4 88.3				19744	419.5
1808 2.75.6 80.9 99.9 12.8 13.8 13.9 94.9	2 8 9 E 9	2101 80.8 99.6 13.9 93.5	1892 89.0 88.8 13.3	1835 85.2 87.2 13.4 94.5	1843 80.8 89.0 14.4 93.8	1949 96.5 93.3 13.0 93.6	4330 94.8 207.0 13.4 93.9	4369 84.8 209.5 12.8 92.8				20127	542.2
1855 20 91.9 80 90.0 99 15.9 15	76 76 76 76 76 76 76 76 76 76 76 76 76 7	2035 80.9 99.9 15.0 94.0	1860 83.6 89.0 14.5 94.0	1807 88.1 87.2 14.3 94.2	1841 86.6 89.0 15.4 94.2	1864 96.1 93.2 15.3 93.6	4305 75.9 208.5 14.8 94.9	4329 81.8 209.5 14.4 93.9				19886	500.8

	GWD	501.0	488.2	495.3	406.0	536.7	604.2
AVG.	N N	20648	20567	21529	21208	22493	23501
	*				·		
	НВР						_
	Z	1140 56.9 164.0 18.1	1560 27.4 375.0 20.0 71.1	2660 46.8 500.0 21.1 56.1	2456 23.3 v300.0 15.6 52.8	2932 63.0 300.0 14.4 56.7	3476 77.0 325.0 8.3 55.6
	KW	4250 82.2 209.5 17.5 94.5	4127 81.9 208.5 18.1 94.3	4270 95.3 210.0 16.7 94.4	3963 32.9 210.0 13.8 92.2	4320 84.4 209.0 9.6 89.3	4169 84.0 206.5 4.0 84.5
	KE	4277 89.8 209.0 17.8 94.9	4235 59.7 209.0 17.8 94.9	4102 62.5 210.0 16.3 94.9	4265 85.3 209.0 14.0	4347 85.0 210.0 9.9 89.6	4331 85.7 209.0 4.3 84.5
TOR	I	1851 75.6 93.3 19.1 93.6	1832 100.0 92.8 18.3 93.8	1756 76.1 92.6 19.8 93.9	1802 88.2 93.9 16.4 94.2	1794 86.1 93.2 12.5 89.9	1934 85.4 93.3 6.5 93.3
REACTOR	ᄠ	1741 88.8 89.3 19.6 94.4	1732 91.5 89.9 19.2 93.9	1681 86.4 89.9 18.0 93.0	1768 87.0 89.9 16.5 93.7	1812 82.0 89.8 11.7 92.0	1895 82.2 87.1 8.8 87.0
	DR	1762 88.6 87.8 18.0 94.5	1706 78.1 87.8 17.1 93.8	1696 84.8 88.0 16.5 93.1	1627 71.9 88.0 15.2 53.2	1807 95. 0 87. 5 10. 0 93. 1	1837 91.7 87.1 6.0 85.3
	Q	1800 94.8 89.2 18.1	1748 91.0 89.0 17.6	1743 87.1 89.0 16.5 94.0	1660 45.6 88.4 16.0 94.6	1713 70.2 89.3 11.2 93.1	1901 85.5 89.0 5.3 92.1
	ပ	2041 39.1 99.5 18.3 94.0	1976 86.0 100.0 17.6 93.7	1985 80.0 101.3 16.3 93.0	1980 68.7 99.2 15.4 94.9	2092 70.6 99.5 10.2 94.1	2204 73.6 100.1 5.0 91.0
	83	1786 65.3 89.2 19.0 91.2	1651 83.1 89.0 18.2 91.0	1636 79.3 88.2 16.8 92.8	1687 69.3 88.9 15.3 93.5	1676 76.0 89.1 10.6 88.3	1754 83.1 87.5 6.9 88.0
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	7/64	8/64	9/64	10/64	11/64	12/64

DATE	PARAMETER	6	ပ	Q	DR	REACTOR	TOR H	X	X	z	HGF	*	AVG.	GWD
1/65	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	1888 81.3 87.5 6.9	2157 84.8 99.8 7.6	1812 80.9 89.0 11.0		1987 100.0 88.7 10.0	2033 90.6 92.9 9.3	4332 74.0 208.2 6.2 86.2	3936 66.4 204.0 5.5 86.8	3025 77.4 325.0 6.1			21170	521.4
2/65	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1947 79.9 88.5 4.8 91.9	2167 80.9 99.5 5.6 93.5	1757 65.8 89.0 4.0 83.8		1872 73.4 89.5 6.4 93.0	1927 77.2 92.4 6.0 89.2	4351 88.1 208.0 5.0 84.7	4357 80.4 203.0 3.6 85.3	3060 76.1 325.0 4.4 51.7			21438	475.8
3/65.	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C	1855 62.2 89.1 6.6 89.9	2175 75.4 99.8 6.7 94.8	1811 91.4 86.0 6.2 89.2		1973 84.3 90.2 7.7 93.7	1893 89.7 93.1 7.4 88.8	4365 85.8 207.0 5.8 86.0	4192 83.2 205.0 4.6 85.8	0000			18264	477.8
4/65	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1950 87.2 89.2 10.4 94.2	2176 87.9 100.6 10.2 94.0	1774 82.1 86.1 10.0 89.3		1877 87.3 90.1 11.0 93.6	1719 87.3 93.2 10.0 79.0	4219 68.0 207.0 9.2 89.8	4221 76.3 206.5 8.8 89.6	2855 74.5 			20791	492.9
5/65	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1799 77.6 90.0 14.5 90.8	2052 67.7 100.8 13.6 94.6	1711 55.3 86.3 12.2 90.2		1817 88.8 89.8 14.0		4325 73.8 207.5 13.0 92.3	4336 86.8 206.5 12.5 93.5	3472 85.7 			19512	473.6
9/92	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1818 91.7 89.5 17.3 94.6	2060 81.0 101.2 16.7 94.9	1889 95.7 90.0 15.8 94.8		1737 86.2 89.8 15.5 91.8		4370 82.1 208.0 15.1 94.9	4174 77.1 208.0 15.0 94.7	2883 38.0 			18931	436.3

	Į				REACTOR	TOR						AVG	
B C D		۵		DR	ı	Ξ	KE	ΚW	2	НВР	* 2	MM	GWD
1710 1832 1761 82.7 66.6 80.9 89.5 101.2 89.9 20.6 19.3 20.3 95.0 94.8 94.9		1761 80.9 89.9 20.3 94.9					4314 94.9 208.5 18.8 94.7	4148 62.3 209.8 18.9 94.8	2800 56.0 			16565	382.0
1712 1925 1673 84.2 86.5 75.6 89.5 102.4 90.2 19.6 19.4 20.5 94.5 94.8 93.8	<u> </u>	16 75 90 20 20 93	673 5.6 10.2 10.5 13.8				1	4028 76.3 209.0 18.1 94.7	3337 62.1 			16773	391.3
1740 1922 1711 83.8 74.1 90.4 89.0 102.0 90.0 18.3 18.8 19.0 94.1 94.8 93.0		90 90 90 19 93	1711 30.4 30.0 19.0				4223 75.6 211.5 17.7 94.8	4165 73.9 208.5 17.8 94.6	3306 72.3 	·		17067	392.7
1745 1987 1722 85.4 45.0 80.6 89.1 102.2 90.4 15.5 18.9 19.4 93.7 94.7 94.9	ļ	172 80. 90. 19.	9 4 4 9	J.			4274 81.9 210.0 15.5 94.1	4296 92.2 211.0 14.9 94.2	3314 48.5 			17338	398.1
1836 2166 1875 79.0 87.6 39.6 88.7 108.8 92.2 10.6 13.9 14.2 94.2 94.7 94.0		187 39. 92. 14.	75				4251 81.6 210.0 10.0 88.6	4096 60.9 209.5 9.8 89.6	3374 70.9 			17598	373.4
1974 2151 2004 86.4 63.9 93.9 88.9 107.7 92.2 7.0 9.2 8.0 93.9 93.2 94.0		200 93. 92. 8.	46700				4371 82.4 208.0 6.5 86.6	4358 74.5 209.5 6.0 86.0	3200 61.0			18058	426.6

AVG.	N* MW GWD	18200 420.0	18942 411.1	19112 508.9	3400 18383 424.9	3602 18409 381.3	2534 17007 367.4
	нСР		3900 93.1 	3850 78.8 	142 29.7	168 2.0	328 24.2
	KW N	84 4225 333 .8 71.7 58.1 .0 209.5 .9 4.8 .7 84.7	4349 69.3 214.0 4.5 82.6	4383 89.3 214.0 8.8 87.0	52 4287 3542 4 42.2 89.2 5 214.0 9 8.3 5 86.6	4240 81.9 214.5 12.8 *	73 4194 2862 .8 63.9 52.3 .0 215.3
REACTOR	H KE	4284 76.8 208.0 5.9 85.7	4263 67.3 213.0 5.0 82.7	4380 95.7 213.5 9.5 87.2	4352 83.4 213.5 10.9 88.5	4362 78.4 214.0 13.2 90.2	4373 89.8 213.0 14.9
REA	DR F						
	C D	2348 2051 91.7 74.6 105.9 93.0 6.0 6.4 94.1 92.8	2358 2103 73.0 91.3 106.7 92.7 5.4 6.1 94.1 94.4	2387 2102 84.0 73.6 107.3 92.4 9.1 14.2 94.9 94.8	2366 2003 82.0 94.8 107.5 92.6 10.1 12.3 94.8 94.9	2286 1977 86.4 71.4 107.8 92.5 13.8 13.8 94.9 94.4	2208 1953 65.9 86.6 108.4 94.2 15.8 15.4
	AETER B	». MW 1961 % 82.2 KGPM 89.4 N- °C 5.5 UT - °C 93.8	% 1969 % 17.6 % KGPM 89.2 % 1. °C 5.3 % 1. °C 93.2	2010 % 85.8 % KGPM 90.3 N -°C 9.1	% 89.6 KGPM 87.6 N - °C 10.1	". MW 1938 % 100.0 KGPM 89.8 N - °C 14.2 UT - °C 94.4	MW 1745 % 61.7 KGPM 90.5 V - °C 14.8
	DATE PARAMETER	1/66 AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °	2/66 AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °	3/66 AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	4/66 AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °	5/66 AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °c	6/66 AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C

* N Reactor was in shutdown status essentially all month.

DATE	PARAMETER	c	· ن	Q	DR	REACTOR F H	TOR H	KE	X	z	HGP	*	AVG.	GWD
99/2	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C	1765 23.6 90.6 17.3 95.0	2159 15.0 108.1 15.6 94.7	1730 16.2 93.5 17.0 94.2				4395 20.4 213.0 15.2 92.8	4394 24.8 215.0 15.3 93.2	3160	374 16.1	2786	17229	109.1
8/66	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1663 20.1 90.6 19.4 94.0	2065 21.0 108.5 18.9 94.8	1804 26.8 93.9 19.9 94.8				3757 14.7 213.5 18.9 93.6	4213 23.5 215.0 18.0 94.8	2874	380 10.6	2494	15996	98.5
99/6	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1758 76.9 90.5 20.1 95.0	2133 93.4 108.9 19.3 94.8	1759 62.1 94.0 20.8 94.2				4188 93.0 213.0 18.5 95.0	4307 71.8 216.0 18.1 94.8	-3797 89.7 	405 88.1	3392	17537	434.2
10/66	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1805 90.5 89.9 15.0 94.5	2204 77.9 108.3 15.0 94.8	1877 100.0 94.0 16.3 94.0				4322 44.5 212.0 14.5 94.0	4211 80.8 198.0 14.5 93.0	2626	367 33.5	2259	16678	355.1
11/66	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C	1855 28.7 93.6 11.6	2217 79.9 104.9 12.0 94.1	1896 71.3 94.0 13.7 94.3				4373 85.1 212.0 11.7 89.9	4365 85.3 215.5 10.8 88.2	3515 87.5 	428 80.1	3087	17793	415.0
12/66	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1982 89.6 94.4 7.7 94.7	2335 84.6 107.4 8.4 94.5	2050 100.0 94.3 9.4 93.9				4360 85.1 212.5 7.9 86.2	4302 70.3 215.5 8.4 85.7	3355 85.1 	443	2912	17941	466.6

	GWD	468.6	423	417.8	477.7	394.7	435.9
AVG.	MW	18295	18460	18181	18247	17520	18861
	*2	3054	3135	3065	3047	2870	4123
	ндь	462 66.2	640 69.9	641 57.9	650 66.3	702 41.2	0
	Z	3516 73.4 	3775	3706 62.4 	3697	3572 62.4 	4123 43.9
	KW	4387 99.7 215.0 6.0 83.7	4305 79.9 216.5 5.5 82.7	4295 79.9 216.5 6.0 82.8	4363 83.1 216.5 8.2 85.2	4188 63.1 217.0 12.1 88.7	4373 87.1 216.5 15.8 92.4
,	KE	4354 78.4 212.0 6.4 84.3	4380 78.1 213.5 6.0 83.5	4393 80.3 197.5 5.9 90.0	4394 100.0 197.5 9.8 93.7	427 <u>8</u> 65.6 214.5 12.3 89.7	4369 87.1 213.0 15.5 93.4
TOR	I						
REACTOR	Ľ.						
	DR						
	a	2027 75.9 93.7 8.7 94.3	2043 86.2 93.8 8.0 8.0	2081 74.0 94.4 9.6 94.0	2001 81.6 89.8 9.5 94.5	1937 79.8 93.0 12.7 93.7	1924 98.1 92.8 15.2 94.9
	ပ	2417 80.9 107.2 7.6 94.8	2410 84.0 107.6 6.1 94.9	2455 74.6 107.3 6.8 94.8	2317 84.6 104.6 9.9 94.6	2262 100.0 104.4 13.3 95.0	2078 58.9 103.7 15.2 94.6
	æ	2056 75.9 95.0 6.9 6.9	2187- 100.0 94.3 6.7 94.7	1982 64.4 95.0 7.6 87.0	2125 100.0 94.9 10.1 95.0	1985 77.4 95.2 13.7 94.9	1994 100.0 94.4 16.0 94.9
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	1/67	2/67	3/67	4/67	5/67	6/67

						REACTOR	TOR						AVG.	
DATE	PARAMETER	8	၁	D	DR	щ	Ξ	KE	ΚM	z	НСР	*2	MW	GWD
19/1	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	1870 84.6 95.5 19.4 94.8	2074 94.0 103.5 19.3 94.9					4262 79.5 212.5 17.9 94.9	4310 86.0 216.5 18.7 94.5	3659 65.6	775 50.1	2884	15400	391.8
8/67	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1626 83.5 94.8 20.3 92.0	2017 100.0 103.3 20.1 94.7					4239 100.0 214.0 20.0 94.4	4211 78.2 216.5 19.3 93.8	3904 77.0 	774	3130	15223	413.2
29/6	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1774 68.2 95.8 19.4 93.1	1958 60.1 103.4 19.2 94.7					4145 77.2 214.0 19.0 94.2	4207 83.7 216.5 18.3 94.5	0	0	0	12084	273.2
10/67	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	1727 78.5 95.4 16.9 93.4	2081 85.8 101.7 15.5 94.2					4223 72.1 214.5 15.0 92.8	4301 72.2 215.5 14.2 91.6	0	0	0	12322	288
11/67	AVG. OP. MW T.O.E % FI.OW - KGPM TEMP. IN - °C TEMP. OUT - °C	1855 74.5 95.8 10.6 94.3	2110 65.0 102.2 10.7 93.9					4311 86.3 198.0 11.0 93.8	4400 100 215.0 10.0 87.7	0	0	0 0	12676	326
12/67	AVG. OP. MW T.O.E% FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	2071 94.7 94.7 8.1 95.0	2279 74.2 105.1 8.0 94.4					4355 84.2 194.5 7.5 93.3	4349 74.8 215.5 6.5 84.1	42 6.0 	383 0.66		12713	327.7

	GWD	328.3	348.4	336.5	328.1	323.1	257.8
	ÿ M M ⊗	14620	14852	13606	13456	13236	13382
	*	2225	2346	2487	2643	2593	2601
	HGP	564 79.4	63.9	672 67.6	702 72.0	682 69.5	664 70.3
	Z	2789 88.5 	2953 67.9 	3159 72.4	3345 75.0	3275 72.8	3265 75.3
	ΚW	4152 75.5 194.5 3.9 85.9	4256 90.7 192.5 4.6 89.0	4385 82.0 193.5 5.0 91.1	4172 75.3 195.0 9.9 94.6	4135 78.1 212.0 12.3 91.4	4259 23.7 212.0 13.0 92.0
	KE	4299 68.3 196.0 4.4 89.4	4340 86.5 193.0 5.5 92.1	4316 73.3 196.0 6.8	4355 93.9 194.5 10.9 94.6	4250 77.9 195.0 12.9 94.8	4346 87.7 207.5 15.2 94.8
TOR	I						
REACTOR	Ŧ						
	DR						
	D						
	၁	2331 59.5 105.9 6.5 93.9	2236 54.3 106.3 7.9 94.8	2418 93.6 106.2 8.0 94.9	2286 74.5 107.7 11.6 94.8	2258 87.4 107.7 14.4 95.0	2176 81.8 107.3 16.0 94.8
	В	1613 68.9 93.6 5.1 79.4	1674 93.7 93.2 5.4 79.6				
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	1/68	2/68	3/68	4/68	2/68	89/9

						REACTOR	TOR						AVG.	
DATE	PARAMETER	8	၁	D	DR	щ	I	KE	ΚW	z	ндь	*	MW	GWD
89/2	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C		2076 79.6 106.2 20.3 95.0					4183 80.5 207.5 19.2 94.3	3486 9.3	3670 50.6 	656 48.8	3014	12759	213.3
89/8	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C		1940 79.6 106.2 19.3 95.0					3933 58.8 207.5 18.6 92.6	4070 89.1 210.5 18.0 94.8	3417 50.1	740 45.0	2677	12620	274.7
89/6	AVG. OP. MW T.O.E % FLOW - KGPM TEMP IN - °C TEM2. OUT - °C		1935 32.6 106.6 19.4 94.6					3717 81.4 194.5 17.8	3942 100 196.5 17.3 94.2	3750	776	2974	12568	297.6
10/68	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C		2117 88.1 105.7 13.8 94.1					4039 100.0 193.0 13.8 93.7	3857 60.5 194.5 14.0 90.0	3679	774	2905	12918	326.1
11/68	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C		2173 69.6 105.4 10.5 94.0					3963 84.9 192.0 10.3 89.6	3845 89.2 193.5 10.6 89.0	3801 67.2	789	3012	12993	310.6
12/68	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C		2225 84.2 105.0 3.9 88.1					3935 80.2 190.5 4.0 83.2	3934 83.4 193.5 6.1 85.5	3716 51.8 	49.2	2939	13033	305.4

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						REACTOR	TOR:			·			978	
DATE	PARAMETER	8	၁	D	DR	Ŧ	I	KE	KW	Z	HGP	*	Ž M	GWD
69/1	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C		2196 51.8 100.8 2.4 93.9					3908 74.8 190.0 1.0 80.3	3818 84.7 192.0 0.5 80.0	3609 61.5 	769 56.2	2840	12762	281.5
2/69	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C		2311 65.7 98.9 2.8 94.2					3879 82.7 188.0 2.7 75.5	3738 70.5 191.5 2.0 81.0	3868 70.3 	732 68.6	3136	13064	268.2
3/69	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C		2183 75.6 99.7 7.3 94.0					3792 84.7 188.0 6.0 83.5	3652 74.5 191.0 5.9 83.5	3735 56.1 	769 53.8	2966	12593	287.2
4/69	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C		2069 80.8 101.4 9.4 94.0			N.		3369 26.0 190.0 9.5 87.4	3953 100.0 191.0 8.7 87.6	3856 88.8 	765 86.9	3091	12482	277.9
5/69	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C							3851 83.1 190.0 14.0 93.5	3757 51.5 192.0 11.0 90.3	3678 38.6 	754 36.8	2924	10532	194.6
69/9	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C							3902 91.1 190.0 16.6 94.6	3777 76.7 193.5 15.9 93.1	3717 59.6 	775 56.9	2942	10621	246.8

						REACTOR	TOR						AVG.	
DATE	PARAMETER	8	ပ	۵	DR	ш.	I	KE	ΚM	Z	ндь	*	MW	GWD
7/69	AVG. OP. MW							3758	3653	3524	229	2847	10258	188.5
	T.O.E %							43.7	79.7	5.15	42.5			
	FLOW - KGPM							10.00	19.00	! ! ! !				
	TEMP. OUT - °C		-					94.7	94.6	1				
03/0	AVA GO DVA							35.12	3720	-	C	C	7241	175 1
8/03	AVG. OF. MW							21.CC 68.89	86.7		00	>	147/	
	FLOW - KGPM							191.5	192.5					
	TEMP. IN - °C							19.3	19.3					
	TEMP. OUT - °C							94.8	94.7					
69/6	AVG OP MW							3651	3475	3079	709.	2370	9496	206.5
	T.O.F %							82.9	65.6	64.4	57.2			
	FLOW - KGPM							190.5	195.0					
	TEMP. IN -°C							17.9	8.7	!				
	TEMP. OUT - °C							94.0	6.06	! !				
10/69	AVG. OP. MW							3615	3757	3841	785	3056	10428	221.6
	T.O.E %							100 5	104.3	8/.0	82.9			
	FLOW - KGPM							14.9	15.1	 				
	TEMP. OUT - °C							92.4	89.4	1.				
11/60	70 ON V							3442	3646	3702	789	2913	10001	189.2
-								50.2	77.9	59.5	58.8			
	FLOW - KGPM							190.0	203.5	1				
	TEMP. IN -°C							1.71) - 0	! !				
	TEMP. OUT - °C							26.3	2.00					
12/69	1							3741	3911	3686	787	2899	10551	265.9
	T.O.E %			-				7.2.7	001	7./0	64.8			
	FLOW - KGPM	-						8.2	6.1	 				
	TEMP. OUT - °C							86.0	81.0	!				

						REACTOR	:TOR						976	
DATE	PARAMETER	8	၁	D	DR	ч	H	KE	ΚW	Z	HGP	*	MW	GWD
1/70	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C							3944 89.5 199.5 4.6 80.4	3946 77.4 202.5 4.1 79.0	3602 50.9 	769 47.5	2833	10723	249.6
2/70	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C							3920 1.1 199.5 4.6 80.4		3622 80.8 	770	2852	6772	66.5
3/70	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C					,		3390 22.3 199.5 4.6 80.4		3862 57.6 	749 53.6	3113	6503	79.9
4/70	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C							3903 82.9 199.5 8.6 84.2		3709 72.7 	784 70.1	2925	6828	161.5
5/70	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C							3778 71.7 200.0 13.5 87.1		3061 45.5 	714	2347	6125	118.0
0//9	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C							3777 71.9 200.0 17.5 91.5		0	0	0	3777	81.5

	GWD	73.3	48.9	109.1	109.2	163.1	133.1
AVG	Ş M M	3454	3653	5850	6116	6649	6582
	*	0	0	2331	2416	2830	2716
	ндр	0	0	686 31.5	716 21.4	795 88.2	800 45.8
	Z	0	0 0 1 1 1	3017 36.0	3132 23.9 	3625 90.1 	3516 48.5
,	ΚW				-		
	KE	3454 68.5 200.5 20.1 90.1	3653 43.2 202.5 20.2 89.7	3519 78.6 202.0 17.5 88.4	3700 79.1 202.0 13.2 85.1	3819 75.2 201.5 7.8 83.6	3866 76.4 202.0 6.0 81.6
REACTOR	I						
REAC	u.						
	DR						
	0						
	ပ						
	8						
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	7/70	8/70	9/70	10/70	11/70	12/70

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	GWD	149.7		1.7	48.0	82.2	9.09
	AVG.	6727		729	1720	2843	2790
	*	2798		729	1720	2843	2790
	HGP	801 78.7			775 51.8	843 95.5	848 67.7
	Z	3599 81.2 		729 7.5	2495 80.0 	3686 96.2 	3638 69.5
	KW		176				
	KE	3929 64.6 202.0 4.6 80.1	June 1971				
REACTOR	Ξ		1971 to				
REA(F		from February				
	DR		from Fe				
	D		s down				
	၁		N Reactor was				
	8		N Rea				
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	וק/ו	2/71-6/71	1//7	8/71	9/71	17/01

	GWD	72.6	45				
AVG.	MW.	2734	2561				
	* 2	2734	2561				
	HGP	849 82.8	808 50.7				
	Z	3583 87.2 	3369 55.2 				
	ΚW						
	KE						
TOR	I						
REACTOR	щ						
	DR						
	O						
	၁						
	&						
	PARAMETER	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN- °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN -°C TEMP. OUT - °C	AVG. OP. MW T.O.E % FLOW - KGPM TEMP. IN - °C TEMP. OUT - °C
	DATE	11/71	12/71				

APPENDIX B

COMPARISONS OF COLUMBIA RIVER HEAT GAIN WITH REACTOR ADDITIONS

DATE	PRIEST RAPIDS TEMPERATURE (DEG. C)		DIFF.	RIVER FLOW C) (KCFS)	COMPUTED HEAT (MM)	REACTOR HEAT (MW)	HEAT Diff. (MW)
6764	12.84	13.83	0.99	388.00	45518.	16693.	28825.
7764	15. 30		1. 21	295.81	42348.	16161.	26187.
8764	17.06		1.82	131.14	28324.	15748.	
9764	16.32		2.14	74. 32	18876.	16510.	2366.
10764	14.55	15. 75	1.20	87.11	12354.	13097.	-743.
11/64	, 10.80	12. 24	1.44	70.12	11937.	17890.	-5953.
12/64	6. 25	7.82	1.57	68, 48	12723.	19490.	-6767.
1/65	4. 45	6.10	1. 65	77.37	15173.	16819.	-1646.
2765	3. 33	5. 36	2.03	99, 24	23897.	16993.	6904.
3765	4. 11	6. 27	2. 15	88. 33	22553.	15413.	7140.
4765	6. 65	9.09	2.44	111.61	32270.	16430.	15840.
5765	10.01	11.03	1.02	235. 39	28524.	15277.	13247.
6765	13.35	14. 22	0.87	310, 50	32132.	14543.	17589.
7765	16.05	17. 28	1. 23	218.42	31727.	12323.	
8765	18.36	19.83	1.47	127.77	22321.	12623.	9698.
9765	17.31 15.30	18. 53	1.23	77. 23	11225.	13090.	
10/65 11/65	15.30 11.87	16.41 12.56	1. 11	63. 78	8411.	12842.	-4431.
12/65	11. 87 7. 79	12.06 8.44	. 0.69 0.65	70, 96 74, 15	5774.	12447.	-6673.
1/66	7. 75 4. 84	5. 92	9.65 1.08	67. 91	5698. 8657.	13761.	-8063.1
2/66	4: 14		2.11	80.39	20073.	13548. 14682.	-4891. 5391.
3/66	4. 45	6.80	2. 35	76. 79	20073. 21315.	14652. 16416.	
4766	7. 93	10.31	2.48	75. 88	22330.	14163.	
5766	10.59	12.05	1. 46	182.58	31547.	12300.	19247.
6766	12. 43	13.47	1.04	276.33	34163	12247.	21916
7766	15. 30	16. 18	0.88	229. 39	23937.	3519.	20418.
8766	17. 55	18. 77	1. 22	108.65	15740.	3177.	12563.
9766	17.48	19.36	1.88	72. 94	16249	14473.	1776.
10/66	14.63	15. 63	1.00	66. 74	7908.	11455.	-3547.
11766	11.63	12.57	0.94	65. 58	7305.	13833.	-6528.
12/66	8. 37	9. 49	1. 12	73. 71	9777.	15052	-5275.

DATE	PRIEST RAPIDS TEMPERATURE (DEG. C)	RICHLAND TEMPERATURE (DEG. C)	TEMP. DIFF. (DEG. C)	RIVER FLOW (KCFS)	COMPUTED HEAT (MW)	REACTOR HEAT (MN)	HEAT DIFF. (MW)
1767	5. 92	7. 36	1.44	75. 25	12858	15116.	-2258.
2/67	5. 25	e. 99	1.74	76.63	15793.	15107	686.
3767	4, 99	6. 64	1.65	90, 22	17678.	13477.	4201.
4767	<i>6</i> . 81	୫. ୫୭	2.00	89, 22	21109.	15923.	518 <i>6</i> .
5767	10.05	12.03	1.98	138. 60	32478.	12732.	19746.
6767	13. 27	13.88	0.61	430, 30	31104.	14530.	16574.
7767	16. 07	17.00	Ø. 93 (288.00	31596.	12639.	18957.

8767 9767		20, 22	1.67	125,00	24703.	13329.	11374.
9767	'' ଏକ ହଳ						
	,	19.39	1.19	80.85	11433.	9107.	2326.
10/67	15, 42	16.05	0.63	71.94	5390.	9290,	-3900.
11/67	11.34	11.96	0.62	74, 24	5483.	10867.	-5384.
12/67	7. 17	7, 93	មា. ៩៩	88, 62	6945.	10571.	-3626.
1/68	4, 65	5, 66	1.92	77.89	9378.	10590.	-1212.
2768		5.00	1. 67	73. 79	14594.	12014.	2580.
3768		୫. ଷ୍ଟ	1.42	108.39	18189.	11823.	6366.
4768	7.09	8, 83	1.74	100.07	20633.	10937.	9696.
5768		12.84	1.78	125.70	26573.	10423.	16150.
6768		14. 26	0.82	271.30	26256.	85 9 3.	17663.
7768		16, 99	ø. 93	226, 35	24832.	6881.	17951.
8768		18.75	1.24	112.53	16517.	8861.	7656.
9768		18.30	1. 14	90.88	12242.	9920	2322.
10/68		14. 95	9.71	76. 97	6473.	10519.	-4046.
11/68		11.40	0.55	78.67	5128.	10353.	-5225.
12/68		7. 36	0.59	91. 65	6447.	9852.	-3405.
1/69		2.71	0.26	104, 49	3275.	9081.	-580 <i>6</i> .
2/69		1.90	0.44	118.81	6185.	9248.	-3063.
3/69		4. 34	0.95	105.76	11386.	9265.	2621.
4/69		7. 97	0.76	185. 33	16764.	92 <i>6</i> 3.	7501.
5/69		11.44	0.63	234, 71	17586.	6277.	11309.
5769		15. 32	0.71	239.17	20029.	8227.	11802.
	,						
DATE	PRIEST RAPIDS	RICHLAND	TEMP.	RIVER	COMPUTED	REACTOR	HEAT
	TEMPERATURE	TEMPERATURE	DIFF.	FLOW	HEAT	HEAT ZMIAN	DIFF.

DATE	PRIEST RAPIDS TEMPERATURE (DEG. C)	TEMPERATURE	DIFF.		COMPUTED HEAT (MN)	HEAT	
7/69	17.11	17.87	0.76	189. 90	17131.	6081.	11050.
8769		19, 26			12658.		
9769	17.70	18, 60			8159.		
10/69		15. 15		82,46			
11/69		11.72	0.17	88.66	1786.		-4521.
12/69	7.64	8.03	0.38		4409.	8577.	
1778		5. 27	1.00	87, 21		8052.	
2/70	4. 14	4, 86	0.72	77.02	65 84.	2293.	
3/70	4.75	5, 72	0.96	85, 75	9768.	2577.	7191.
4770		7. 94	1.09	91.91	11908.	5383.	1 6525.
5770		11.72	0.85	131.10	13131.	3806.	9325.
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