

LA-DC-10338

RECEIVED BY DTIC FEB 13 1969

MASTER

N-2-7967

March, 1965

KINETICS EQUATION FOR A CLUSTER OF ROVER REACTORS

Gordon E. Hansen, Critical Assemblies Group, University of California, Los Alamos Scientific Laboratory, Los Alamos, New Mexico

I. Introduction

A kinetics equation is a set of ordinary differential equations governing the coarse time-dependence of effective neutron populations in one or more regions of space. The present interest is in obtaining a simplest form of kinetics equation capable of giving the time-dependence of fission rates in individual cores of a clustered array; moreover, it is desired that all parameters introduced here be defined in terms of computable functions of the basic nuclear properties of this system.

For the purpose of introducing notation and general rationale, we first review the derivation of the "point-reactor" kinetics equation. Secondly, we generalize to a "two-point" equation wherein space is divided into two "points", one corresponding to the reactor proper, and the other to the environment. The final generalization to the kinetics equation for a cluster of Rover reactors will then be essentially trivial.

II. "Point-Reactor" Kinetics Equation

We presume the system to be completely described, neutronically, by the macroscopic collision cross section, $\sigma(E, \vec{n}, \vec{r})$, the scattering kernel, $\sigma_s(E' \rightarrow E, \vec{n}' \rightarrow \vec{n})$, and the fission neutron kernels $\nu_p \sigma_f(E') \chi(E)$, $B \nu \sigma_f(E') \chi_d(E, \tau) p(\tau) d\tau$ (i.e., the delayed neutron emission kernel).

Handwritten signature

LASL-AEC-OFFICIAL

LASL-AEC-OFFICIAL

DISCLAIMER

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency Thereof, nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

DISCLAIMER

Portions of this document may be illegible in electronic image products. Images are produced from the best available original document.

We presume the system to be finite and isolated from any environment, i.e., no neutrons enter the system from outside. The flux distribution, $\phi(E, \vec{n}, \vec{r}, t)$, in this system is then given by the transport equation

$$\frac{1}{v} \frac{\partial \phi}{\partial t} + \Omega \cdot \nabla \phi + \sigma \phi = \int \phi(E', \vec{n}', \vec{r}, t) [\sigma_s + \nu_p \sigma_f \chi] dE' d\Omega' + S(E, \vec{n}, \vec{r}, t) + \int \phi(E', \vec{n}', \vec{r}, t - \tau) \beta \nu \sigma_f \chi_d p(\tau) d\tau dE' d\Omega' \quad (1)$$

and the prompt neutron reproduction number, k , of this system is defined by the eigenvalue problem

$$-\Omega \cdot \nabla \phi^+ + \sigma \phi^+ = \int [\sigma_s + \frac{1}{k} \nu_p \sigma_f \chi] (E - E', \vec{n} - \vec{n}') \phi^+(E', \vec{n}', \vec{r}) dE d\Omega' \quad (2)$$

Because the system is neutronicly isolated, Equations 1 and 2 are most conveniently solved for ϕ and ϕ^+ only within the system volume by applying the "isolation boundary conditions": $\phi = 0$ for incoming directions $\phi^+ = 0$ for outgoing directions \vec{n} .

By subtracting Equation 2 multiplied by ϕ from Equation 1 multiplied by ϕ^+ , and then integrating the result over the ranges of E and Ω and over the volume V , one formally obtains

$$\int_V \phi^+ \frac{1}{v} \frac{\partial \phi}{\partial t} dE d\Omega dV = \left(1 - \frac{1}{k}\right) \int_V \phi \nu_p \sigma_f \chi \phi^+ dE' d\Omega' dE d\Omega dV + \int_V \phi^+ S dE d\Omega dV + \int_V \phi(t - \tau) \beta \nu \sigma_f \chi_d p(\tau) \phi^+ d\tau dE d\Omega dE' d\Omega' dV - \int_V \phi \phi^+ \vec{n} \cdot d\vec{S} dE d\Omega \quad (3)$$

In this formal equation, the last, or surface integral, term represents the effective rate at which neutrons enter the region V from outside and this term is zero when the region V includes the system. In this section, we identify V with the volume of the system and omit the surface integral in Equation 3. This

equation is readily reduced to the "point-reactor" kinetics equation by an artifice which renders ϕ^+ absolutely independent of time: although reactivity variation is actually accomplished by material displacements, i.e., changes in the macroscopic cross sections, it is conveniently and essentially equivalently accomplished, mathematically, by a change in the prompt neutron emission factor, ν_p . From Equation 2, we see that when this factor is $\nu_p(t)$, then the eigenvalue, $k(t)$, is such as to make $\nu_p(t)/k(t)$ and thence the shape of ϕ^+ time independent. Since ϕ^+ is governed by a linear homogeneous equation in the phase space variables, it is defined only to within an arbitrarily time-dependent factor. This factor we choose constant so that the left-hand-side of Equation 3 may be rewritten as

$$\int_V \phi^+ \frac{1}{V} \frac{\partial \phi}{\partial t} dE d\Omega dV = \frac{d}{dt} \int_V \phi^+ \frac{1}{V} \phi dE d\Omega dV = \frac{d}{dt} N \quad (4)$$

We now normalize ϕ^+ such that at some time, $t = t_0$,

$$\frac{N}{l} = \int_V \phi \nu_p \sigma_f \chi \phi^+ dE' d\Omega' dE d\Omega dV = \int_V \phi \nu_p \sigma_f dE' d\Omega' dV \quad (5)$$

If the time dependence of ϕ is factorable, Equation 5 will hold at all times and the "prompt-neutron lifetime", l , will be a constant. Only for this case does N/l continue to equal the prompt neutron production rate and therefore be proportional to reactor power. To the extent that the time-dependence of ϕ is nearly factorable, l is nearly constant and N/l is nearly proportional to reactor power. In words, we merely call N the "effective" neutron population in the reactor, and N/l the "effective prompt neutron production rate". With the definition of these symbols

by means of Equations 4 and 5 and the additional definitions of "effective" delayed neutron fraction, β^* , and "effective" neutron source strength, S^* , as

$$\beta^* \int \frac{N}{l}(t-\tau)p(\tau)d\tau = \int_V \delta(t-\tau) \nu \sigma_f \chi_d \phi^+ p(\tau) d\tau dE' d\Omega' dE d\Omega dV \quad (6)$$

$$S^* = \int_V S \phi^+ dE d\Omega dV \quad (7)$$

We may rewrite Equation 3 as the "point-reactor" kinetics equation

$$\frac{dN}{dt} + \left(\frac{1}{k} - 1\right) \frac{N}{l} = \beta^* \int \frac{N}{l}(t-\tau)p(\tau)d\tau + S^* \quad (8)$$

Equation 8 is exact when the symbols are defined as above in Equations 2 to 7. It is not useful, however, unless $l \approx$ constant and N/l can be correlated with reactor power. To illustrate, consider a well-reflected reactor, perhaps even a Rover reactor, for which neutron residence time in the reflector is comparable to the decay time of prompt neutron linked fission chains. Here, the ratio of core neutron population to reflector neutron population depends rather sensitively on system reactivity (the so-called "time absorption" phenomenon) and the effective neutron population of the entire system is not a good index of core power. The time-dependence of flux shape can be partially accounted for by introducing two neutron population variables, say a core population and a reflector population, into a "two-point" kinetics equation. The particular choice is somewhat arbitrary but should lead to simple evaluation of reactor power. In the following development of a "two-point" kinetics equation, we shall designate the two regions of space simply as reactor and environment.

LEGAL NOTICE

This report was prepared as an account of Government sponsored work. Neither the United States, nor the Commission, nor any person acting on behalf of the Commission

A. Makes any warranty or representation, expressed or implied, with respect to the accuracy, completeness, or usefulness of the information contained in this report, or that the use of any information, apparatus, method, or process disclosed in this report may not infringe privately owned rights, or

B. Assumes any liabilities with respect to the use of, or for damages resulting from the use of any information, apparatus, method, or process disclosed in this report

As used in the above, "person acting on behalf of the Commission" includes any employee or contractor of the Commission, or employee of such contractor, to the extent that such employee or contractor of the Commission, or employee of such contractor prepares, disseminates, or provides access to, any information pursuant to his employment or contract with the Commission or his employment with such contractor.

III. "Two-point" Kinetics Equation

We presume the reactor is identified with the volume V and that the flux distribution is given by Equation 1. When isolated from its environment, the reproduction number is defined by Equation 2 with "isolation boundary conditions" on the surface of V . We classify neutrons in V at time t into two groups: those neutrons which were born in V and remained there to time t , and, the remainder. The corresponding fluxes are ϕ_1 and ψ_1 , with $\phi_1 + \psi_1$ equaling the total flux ϕ . The transport equations for ϕ_1 and ψ_1 in V are

$$\frac{1}{v} \frac{\partial \phi_1}{\partial t} + \Omega \cdot \nabla \phi_1 + \sigma \phi_1 = \int \phi_1 \sigma_s dE' d\Omega' + \int [\phi_1 + \psi_1] v_p \sigma_f \chi dE' d\Omega' + S(E, \vec{\Omega}, \vec{r}, t) + \int [\phi_1 + \psi_1] (t - \tau) B v \sigma_f \chi_d p(\tau) d\tau dE' d\Omega' \quad (1a)$$

$$\frac{1}{v} \frac{\partial \psi_1}{\partial t} + \vec{n} \cdot \nabla \psi_1 + \sigma \psi_1 = \int \psi_1 \sigma_s dE' d\Omega' \quad (1b)$$

with boundary conditions $\phi_1 = 0$ and $\psi_1 = \phi$ for incoming directions.

For convenience, we shall label the solution of Equation 2 ϕ_1^+ and the eigenvalue k_1 . Combining Equations 1a and 2 and also 1b and 2, we obtain the following analogues of Equation 3.

$$\int_V \phi_1^+ \frac{1}{v} \frac{\partial \phi_1}{\partial t} dE d\Omega dV = \left(1 - \frac{1}{k_1}\right) \int_V \phi_1 v_p \sigma_f \chi \phi_1^+ dE' d\Omega' dE d\Omega dV + \int_V \phi_1^+ S dE d\Omega dV \quad (3a)$$

$$+ \int_V \psi_1 v_p \sigma_f \chi \phi_1^+ dE' d\Omega' dE d\Omega dV + \int_V [\phi_1 + \psi_1] (t - \tau) B v \sigma_f \chi_d \phi_1^+ p(\tau) d\tau dE' d\Omega' dE d\Omega dV$$

$$\int_V \phi_1^+ \frac{1}{v} \frac{\partial \psi_1}{\partial t} dE d\Omega dV = - \frac{1}{k_1} \int_V \psi_1 v_p \sigma_f \chi \phi_1^+ dE' d\Omega' dE d\Omega - \oint_V \phi_1^+ \vec{n} \cdot d\vec{S} dE d\Omega \quad (3b)$$

The analogue of Equation 4 is

$$\int_V \phi_1^+ \frac{1}{v} \frac{\partial \phi_1}{\partial t} dE d\Omega dV = \frac{d}{dt} \int_V \phi_1^+ \frac{1}{v} \phi_1 dE d\Omega dV = \frac{d}{dt} N_1 \quad (4a)$$

$$\int_V \phi_1^+ \frac{1}{v} \frac{\partial \psi_1}{\partial t} dE d\Omega dV = \frac{d}{dt} \int_V \phi_1^+ \frac{1}{v} \psi_1 dE d\Omega dV \equiv \frac{d}{dt} N_1' \quad (4b)$$

and the analogue of Equation 5 is

$$\frac{N_1}{L_1} = \int_V \phi_1 v_p \sigma_f \chi \phi_1^+ dE' d\Omega' dE d\Omega dV = \int_V \phi_1 v_p \sigma_f dE' d\Omega' dV \quad (5a)$$

$$\frac{N_1'}{L_1'} = \int_V \psi_1 v_p \sigma_f \chi \phi_1^+ dE' d\Omega' dE d\Omega dV \quad (5b)$$

Similarly Equations 6 and 7 generalize to

$$B_1^* \int \frac{N_1}{L_1} (t-\tau) p(\tau) d\tau = \int_V \phi_1 (t-\tau) v \sigma_f \chi_d \phi_1^+ p(\tau) d\tau dE' d\Omega' dE d\Omega dV \quad (6a)$$

$$B_1^* \int \frac{N_1'}{L_1'} (t-\tau) p(\tau) d\tau = \int_V \psi_1 (t-\tau) v \sigma_f \chi_d \phi_1^+ p(\tau) d\tau dE' d\Omega' dE d\Omega dV \quad (6b)$$

$$S_1^* = \int_V \phi_1^+ S dE d\Omega dV \quad (7a)$$

$$S_1'^* = - \oint_V \phi_1^+ \vec{n} \cdot \vec{d} S dE d\Omega \quad (7b)$$

Finally, the analogue of Equation 8 is the "two-point" kinetics equation

$$\begin{aligned} \frac{dN_1}{dt} + \frac{(1-k_1)}{k_1} \frac{N_1}{L_1} &= B_1^* \int \frac{N_1}{L_1} (t-\tau) p(\tau) d\tau + S_1^* + \frac{N_1'}{L_1'} \\ &+ B_1'^* \int \frac{N_1'}{L_1'} (t-\tau) p(\tau) d\tau \end{aligned} \quad (8a)$$

$$\frac{dN_1'}{dt} + \frac{1}{k_1} \frac{N_1'}{L_1'} = S_1'^* \quad (8b)$$

The only parameter contained in (8a) and (8b) not defined in terms of basic nuclear parameters is $S_1'^*$, i.e., the surface integral of (7b) which represents the effective neutron current into V from the environment. This current, of course, depends on the nuclear parameters of the environment and these, as yet, remain unspecified.

Formally, one may represent $S_1'^*$ as

$$S_1'^*(t) = \langle \phi_1^+ \rangle \int \left(\frac{N_1}{L_1} + \frac{N_1'}{L_1'} \right) (t-\tau) p_{11}(\tau) d\tau \quad (9)$$

with $p_{11}(\tau)d\tau$ being the probability that a fission neutron, born at time t in V , leaves the reactor proper and then re-enters at time $t+\tau$ in $d\tau$; $\langle \phi_1^+ \rangle$ is the mean effectiveness for such a neutron coming into V ; $(N_1/L_1 + N_1'/L_1')$ is the total effective fission neutron production rate and is the index of reactor power. For brevity, we have omitted from the right-hand-side of Equation 9 a contribution due to delayed neutrons. This contribution indeed plays an important part in the kinetics of any system where $k_1 \rightarrow 0$, such as a cavity-reactor with the cavity considered as the reactor proper.

A feel for the various time delay parameters appearing in (8a) and (8b) may be obtained from the following typical prompt neutron regeneration loop: a neutron enters the reactor proper (the source for Equation 8b), and, in the meantime $k_1 l_1'$, diffuses into the core and produces a fission; the neutrons from this fission (the source for Equation 8a) produce a chain of fissions of mean time duration $k_1 l_1 / (1-k_1)$; some neutrons from this chain diffuse out of the reactor proper but eventually return to complete the loop -- the mean time being $\bar{\tau} = \int \tau p_{11}(\tau) d\tau / \int p_{11}(\tau) d\tau$.

IV. Kinetics Equation for a Cluster of Rover Reactors

A cluster of reactors can still be described as one reactor proper in V_1 plus an environment and the Equations 8a and 8b are still applicable. The source term, $S_1'^*$, however, depends on the power histories of each reactor of the cluster, and its evaluation

for an n-cluster array involves the solution of n such "two-point" kinetics equations. The whole set is generated from (8a) and (8b) by replacing the subscript 1 by $i = 1, 2, \dots, n$. The source term, $S_i'^*$, for the i^{th} reactor proper is then formally

$$S_i'^* = \langle \psi_i \rangle \sum_j \int \left(\frac{N_j}{L_j} + \frac{N_j^r}{L_j^r} \right) (t-\tau) p_{ji}(\tau) d\tau \quad (9a)$$

with $p_{ji}(\tau)d\tau$ the probability that a fission neutron born in j enters i a time τ in $d\tau$ later. The evaluation of p_{ji} may be quite complicated if there are important indirect paths from j to i such as perhaps ones which involve other elements of the cluster or the "environment" of the cluster-system. Nevertheless, once the macroscopic cross-sections of cluster-system and environment have been specified, a p_{ji} can, in principle, be computed by available Monte Carlo methods.

The set of $2n$ equations, described above, may be simplified somewhat in the application to a cluster of Rover reactors. Experimentally, a single Rover reactor has a well-defined Rossi- α and its time behavior thus is described by a point-reactor kinetics equation; we are thus permitted to choose, as the i^{th} reactor proper, the i^{th} Rover reactor and have $k_i \simeq 1$, i.e., each Rover reactor in the cluster is nearly critical. For this case, $N_i/L_i \gg N_i^r/L_i^r$, and we may approximate $(N_i/L_i + N_i^r/L_i^r) \simeq N_i/L_i$. With this approximation, Equation 8b is readily integrated to

$$\frac{N_i^r}{L_i^r} \simeq \langle \psi_i \rangle \sum_j \int_0^\infty \int_0^\tau \frac{N_j}{L_j} (t-\tau) p_{ji}(\tau-\tau') e^{-\tau'/L_i^r} d\tau d\tau'/L_i^r \quad (8c)$$

Substitution of this expression for N_i'/l_i' in (8a) reduces the set of $2n$ equations for the N_i and N_i' to a set of n equations for the N_i . Before making this substitution, it is convenient to introduce the symbols

$$\Delta k_{ji} = \langle \psi_i \rangle \int_0^\infty \int_0^\tau p_{ji}(\tau-\tau') e^{-\tau'/l_i'} d\tau d\tau'/l_i' \quad (10)$$

$$W_{ji}(\tau) = \int_0^\tau p_{ji}(\tau-\tau') e^{-\tau'/l_i'} d\tau'/l_i' / \int_0^\infty \int_0^\tau p_{ji}(\tau-\tau') e^{-\tau'/l_i'} d\tau d\tau'/l_i' \quad (11)$$

As seen from their definitions, Δk_{ji} represents the transfer probability of a fission neutron from j to i , and $W_{ji}(\tau)$ is the time distribution function for this transfer. Δk_{ii} is the transfer probability from i to i via its environment. With this symbolism, Equation 8a becomes

$$\frac{dN_i}{dt} + (1-k_i) \frac{N_i}{l_i} = \beta_i^* \int \frac{N_i}{l_i} (t-\tau) p(\tau) d\tau + \sum_j \Delta k_{ji} \int \frac{N_j}{l_j} (t-\tau) W_{ji}(\tau) d\tau + S_i^* \quad (12)$$

Equation 12 is the desired form of the kinetics equation for a cluster of Rover reactors. Computational procedures for evaluation of the parameters l_i , l_i' , etc., have been indicated. Seale and Chezem have examined solutions of this form of equation with $\Delta k_{ii} = 0$, $W_{ji}(\tau) = \delta(\tau-\tau_{ji})$ where τ_{ji} equals the effective mean drift time of neutrons between the boundaries of j and i , and with $p(\tau)$ corresponding to the Keepin-Wimett six delayed neutron groups. This is a shrewd choice of parameters for anticipated Rover reactor clusters although, strictly speaking, the choice $W_{ji}(\tau) = \delta(\tau-\tau_{ji})$ prevents Equation 12 from being representable as a finite set of ordinary differential equations: thus,

(

(1), k_{ii} decreases approximately as the inverse fourth power of reactor separation distance whereas k_{ji} ($j \neq i$) decreases only as the inverse square, and at anticipated separation distances $k_{ii} \ll k_{ji}$ ($j \neq i$); (2) the first moment of the distribution function $W_{ji}(\tau)$ is the sum of three mean times -- the time for a fission neutron to leak out of j , the drift time τ_{ji} from boundary of j to boundary of i , and the time from entrance to absorption in i -- and for the anticipated separation distances, the drift time term is dominant; furthermore the product of the Rossi- α by any τ_{ji} is small compared to unity and only the first moment of $W_{ji}(\tau)$ is of importance.

GEH:jf

DIST:

R. W. Spence/F. P. Durham, N-DO
J. D. Orndoff, N-2
C. G. Chezem, N-2
G. A. Graves, N-2
H. H. Helmick, N-2
R. L. Seale, N-2 Consultant
T. F. Wimett, N-2
J. E. Perry, N-4
J. D. Balcomb, N-4
R. J. Bohl, N-4
D. B. Hall, K-DO
H. B. Demuth, K-4
H. A. Sandmeier, T-DOT