DUQUESNE LIGHT COMPANY SHIPPINGPORT ATOMIC POWER STATION

TEST RESULTS

DLCS 2130201 T-641124-A

MODIFIED PURIFICATION SYSTEM PERFORMANCE TEST

CORE I, SEED 2

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Section 2 of 3 Sections

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CORE I, SEED 2

Purpose

To determine the effectiveness of purification in controlling plant radioactivation rates.

Conclusions

The effectiveness of purification in controlling plant radioactivation rates was determined through comparison of the actual effects produced from plant operation with and without purification. With the Purification System in service, there was no appreciable difficulty in maintaining the reactor coolant within reference water specifications. In addition, there was no discernable increase of crud deposition in the Reactor Coolant System as determined by direct radiation measurements of the purification hairpin loop. However, without demineralization as a controlling agent, the gross non-volatile gamma activity levels of the reactor coolant increased and the specific activities of long-lived fission products were at higher levels.

Some conclusions can be made as to the effect of no purification flow on general plant contamination levels. Although the general levels of water borne activities increased during the test period, the associated plant systems did not exceed their limits.

Description of Test Equipment and Test Procedure

Following the completion of DLCS 3620101, Reactivity Lifetime, general plant radiation levels were determined, the resin was discharged from the 1BD demineralizer, and a new test section of piping was installed in the lBD purification hairpin loop. The no purification test was performed in accordance with the approved test procedure of DLCS 21301, Modified Purification System Performance Test, issued June 15, 1960. The plant was operated for 1475 EFPH with the IAC purification loop isolated and the IBD purification loop in service without resin in the demineralizer. Coolant flow rate through the IBD purification loop was regulated at approximately 20,000 lb/hr, providing flow conditions similar to those of normal purification. The Coolant Sampling System was utilized to obtain reactor coolant water samples from the 1BD demineralizer influent, for chemical and radiochemical analyses. The 1BD hairpin loop was used for direct measurement of the radiation increase due to crud build-up in the Reactor Coolant System. At the beginning of the run, and every 300 EFPH thereafter, the hairpin loop was temporarily isolated; puring each isolation, radiation level measurements were taken at the vertical and horizontal leg shield penetrations provided on the

hairpin loop. After 1475 EFPH of plant operation without by-pass purification, the test was terminated, general plant radiation levels were determined and the test section of piping was removed from the hairpin loop for performance of an analysis in accordance with DLCS 36501, Analysis and Radiation Measurements of Hairpin Loop Sections of the Purification System.

The 1BD hairpin loop was not drained and surveyed the first time it was isolated, (June 24, 1960) since the plant heat-up was already in progress.

A portable Jordan radiation survey meter with the ionization chamber on an extension cord was used to determine the radiation levels of the hairpin loop. Table V contains the meter calibration data.

Results

DLCS 2130201, Modified Purification System Performance Test, was started June 23, 1960 and concluded September 12, 1960. The plant was operated for about 1475 EFPH while the 1BD purification loop was in service with no resin in its demineralizer and the 1AC purification loop was isolated. Plant operation with no purification extended between 773.1 and 2247.7 EFPH of Core I Seed 2. The data recorded for this period was included in Tables I, II, III and IV.

Table I summarizes the analytical data related to reactor coolant chemical control. Reference water specifications for reactor coolant were maintained within the prescribed limits, although conductivity increased slightly during the test and averaged higher than values obtained previously. Four additions of LiOH·H2O were required for pH control of the Reactor Coolant System.

The observed values of gross non-volatile gamma activity after 15 minute decay increased at start-up of the plant and remained about a factor of 2 higher than the gross gamma levels experienced with the Rurification System in service. The initial increase of activity was due to a burst of fission prodicts and crud during start-up. Without the aid of purification these activities and crud are removed only by plant leakage. The long-lived gross non-volatile gamma activity after 120 hour decay increased from an average value of 2,000 cpm/ml, before the test began, to 9,000 cpm/ml after the test began. The long-lived activities ranged up to an average of 17,000 cpm/ml near the midpoint of the test, then decreased to values similar to those observed at the beginning of the test. The long-lived activity was due almost entirely to Iodine-133 and Xenon-133. Iodine-133 accounted for 62% of the long-lived activity and Xenon-133 for about 30%.

All data for fission product activities are reported in Table II. The data shows some scattering, but in general, the specific activities of fission products in the reactor coolant were at higher levels, without the use of purification, than during any previous phase of plant operation. The activity levels of short-lived fission products fluctuated slightly after the initial build-up, and did not differ significantly from levels observed during half-purification operation of Seed 1. The activity of Cesium-138 (32 minutes half-life) is a typical example

which averages about 16,500 dpm/ml during both periods. The intermediate and long-lived fission products showed increased activity levels over previous Seed 2 observations. The trend of Cesium fission products demonstrates the circumstances. The specific activities of Cesium-136 (13 days half-life) and Cesium-137 (30 years half-life) increased by factors of 2 and 5 respectively, immediately after start-up June 23, 1960, and they continued to increase until midway through the run. Cesium-136 activity increased by a factor of 100, to 850 dpm/ml; Cesium 137 activity increased by a factor of 20, to 2990 dpm/ml. There also was a significant increase in Iodine-131 (8.05 days half-life) fission product activity. It increased to a maximum of 64,000 dpm/ml, which is the highest value observed during Seed 2. While this increase is large, it was probably due to load swings and student training, since the iodine activity levels declined with steady state operation near the end of the run. Evidence which might indicate the effectiveness of purification is the observation of Bromine-82 (35 hours half-life). It was never detected during Seed 1 operation or during Seed 2 operation when the Purification System was in service. However, during no purification its specific activity attained a maximum value of 2,000 dpm/ml.

At this time, the data indicate that purification is effective at controlling the concentration of long-lived fission products, but it is difficult to evaluate the effectiveness of purification in controlling fission products, since crucial to the analysis is a comparison of activity levels while establishing the effects of any relevant variables. For example, when comparing no purification data with Seed 1 data, there is no way of establishing that the fission product activity was equivalent during both periods (additions of iodine products from fuel may be different, etc.). Also, there are considerations necessary when making comparisons with previous Seed 2 data. The limited data, acquired prior to operation without purification, suggests the possibility that fission product activity had not reached equilibrium, due to the purification half-life.

Data for reactor coolant corrosion products are shown in Table III. The concentration of water borne corrosion products was approximately 45 ppm when the plant returned to power after being cooled down for several days, The concentration after two days operation decreased to a range of 2 to 6 ppb and increased during power and temperature transients to approximately 10 to 15 ppb.

A summary of data concerning the radiation intensities (on contact) of the 1BD hairpin loop is given in Table IV. There was no trend apparent throughout the test and there were no significant changes in radiation levels. The radiation levels measured 3 hours after isolation of the hairpin loop varied between 20 and 55 mr/hr. The levels indicated that there was no discernable increase of crud deposition in the Reactor Coolant System during no purification operation. This conclusion was corroborated by test results DLCS 3410102 and 05, External Radiation Levels of Reactor Coolant Loop Piping and Components, performed June 10-18, 1960, and September 12-16, 1960, respectively. These results indicated that there was no significant increase in radiation levels from operation

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without purification. The majority of the points surveyed in the coolant loops had radiation levels varying from 2 to 5 mr/hr. These results also report the existance of "hot spots" with levels ranging from 90 to 400 mr/hr. This verifies that there is corrosion product "Plate Out", but none of the hot spots showed significant changes in radiation level over the no purification period.

One problem of operation with no purification is the build-up of activity on the secondary side of the Heat Exchangers. The small leaks which are normally not a problem remained constant, however the amount of activity introduced per ml of leakage increased. This means that the constant risk of contaminating the boiler was present during the no purification test.

Radiation surveys can give an indication of crud build-up, however, a more complete evaluation will be available with the issuance of DLCS 36501, Analysis and Radiation Measurement of Hairpin Loop Sections of the Purification System, which is being performed on the test section of piping installed for the no purification test.

DUQUESNE LIGHT COMPANY POWER STATIONS DEPARTMENT SHIPPINGPORT ATOMIC POWER STATION MODIFIED PURIFICATION SYSTEM PERFORMANCE TEST DLCS 2130201 (T-641124-A)

TABLE I
REACTOR COOLANT CHEMISTRY

,	1			<u> </u>	1		Gross Non	-volatile		•		Che	mic	1 6	dditions
	İ	Elect.			1	ŀ		ctivity		Ana:	lysis				
	Sample	Cond	pH at	Li	02	C1	cpm/ml			cc/l		Ho			LION
Date	Source		25 C	ppm	ppm	ppm	15 min.	120 hr.	Total			H ₂ Ft)		8.5
															<u> </u>
6/23/60	BD-BIX	11.5	9.71	İ	0.005	Į	[į		40	į į	80	. ,		
24		11.6	9.73	0.37			79.76	18.13		38]				
25	BD-BIX	10.2	9.60	0.32	1		56.84	17.60		35	•			. 4	115
.26	BD-BIX	30.2	10.12			€0.05	85.10	9.55		33					
27	BD-BIX	1		1] .		56.56	8.22		30	•				
28	BD-BIX	30.0	10.10	ŀ			85.48	15.73		24				•	
29	BD-BIX			0.89	0.005	₹0.05	89.11	6.49		20		90	•		
30	BD-BIX		1	1	1	, , , , ,	62.28	2.71		51]			
	BD-BIX	29.9	10.09		1		101.67	8.87		38		l '			
2	BD-BIX	1			0.000	.	104.37	7.13		30					
3	BD-BIX	27.1	9.98	0.82		l .	109.37	11.35	' '	28	1	•			
4	BD-BIX			""	İ	1	90.19	6.84		24		[
5	BD-BIX	24.0	10.00	0.74		Ì	111.67	10.02		20		l ·	٠.		•
6	BD-BIX	- ' ' '		\		<0.05	101.98	5.09		38		Ī			
	BD-BIX			1.	0.010	10.03	98.09	3.03		30	ł .	•			
9 8 4	BD-BIX	22.6	9.95	0.71	l		94.75	6.30		25	ŀ		• • •	<i>;</i>	
of of riti	BD-BIX	22.0	1 7.33	10.71	0.000		99.70	6.75		25	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			į	
Swings 10 6 8 2 Training	BD-BIX	17.6	9.90	1	0.000	<0.05	33.70	1 0.73	1	20		ŀ			
명 11 교	BD-BIX	17.0	3.30	į .	ļ ·	70.03	91.58	15.79		18	l	80			-
	BD-BIX	16.4	9.81	0.48	ł	l .	41.08	17.66		36	Į į	المعا		.	•
2 12 up	BD-BIX	10.4	9.01	10.40		<0.05	41.02			32				•	' .
13 pn 14 S	BD-BIX		Ì		0.000	10.03		22.19		32		ļ ·			
15	1					[41.05			ł	ļ. ,	·	•	i	y wy
16	BD-BIX	14.9	9.60	0 20	40 005	1	38.94	1]	1	<u> </u>				227
17	BD-BIX		t .		₹0.005					.32	, .				1221
	BD-BIX	24.0	10.00	0.78	₹0.005	40.03	60.06	1	٠,٠,						
18	BD-BIX			}	}	} .	68.26	24.18		۱.,		l	· .		
19	BD-BIX			1	1 .	·	·	·		44		95			
20	BD-BIX			1						35	l	l		: ,	: }
. 21	BD-BIX				! .	1				30					
22	BD-BIX		1 .		1.	1	83.98	21.65	28	24	4				
23	BD-BIX					1			[·]	21		80			
24	BD-BIX	20.20	9.89	1	ļ	<0.05			.	39					
25	BD-BIX	l .	[1	1		84.64	15.56	36	30	6.				· , ·
26	BD-BIX	19.6	9.89	1			47.41	16.40] [27	1	}			
2.7	BD-BIX	1	1	1	0.005	<0.05	79.07	9.43	ļ	25	!	1			
28	BD-BIX	l		1	1	[]	84.15			21	1	85			
29	BD-BIX	16.5	9.80	1 .			77.88	1 .		41] :			•	
30	BD-BIX		l .	!	<u>.</u>	1.	1 :			36		•			151
- 31	}]	[1		₹0.05	1	1] ·		ł	l		. v	
;	i ·			1		1	1		ļ ·		l	'			

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TABLE I (cont'd)

REACTOR COOLANT CHEMISTRY

1				1	T :	1.		Cross Nor	-volatile				Chanda	- T A	ditions
1			Elect.			,	l		ctivity	Caa	Andi	lysis	Chemic	BT W	ditions
l	./		Cond.	pH at	Li	02	C1		× 10 ³						
l	Date	Source		25 C	ppm	ppm	ppm	15 min.	120 hr.		cc/l	Inert	H ₂ Ft3		LIOH
r	<u> Dace</u>	Dogree	THILLOS	25 0	1 PPI	T PPIII	PPI	LJ WIR.	120 HF.		AZ.	Inert	Pto		· :8s
1	8/ 1/60	RD-RTX].		·1] /				一个	24	ĺ			
	2	BD-BIX		1			ı				24	ļ	80		
ı	3	BD-BIX		·	'	·	⟨0.05				37	100	00	•	
	4	BD-BIX	23.7	10.00	1	0.000	X0.03	111.78	28.52	44	24				
	5	BD-BIX	23.7	10.00	Ĭ	0.000		111.70	20.32	Test	27				·
ı	6	BD-BIX		· ·		ļ					28				
	7	BD-BIX		l .	l	ĺ		93.18	18.65	₩	44		·75		
ı	8	BD-BIX			1		l	93.10	10.05		38	İ	./3	٠.	
	9	BD-BIX		1	1	1		113.40	29.31	33	30				
1	10	BD-BIX				0.000		186.36	17.87	P	30	[•	
	11	BD-BIX	23.9	10.00		0.000		120.37	1/.0/	—Midway	30	<u> </u>			
l	12	BD-BIX	22.0	9.60	0.74		,	120.37		1	24				
1	. 13	BD-BIX	22.0	3.00	10.74	0.000		117.27	<i>:</i>	27	23	4			1 240
ľ	14	BD-BIX	22.8	9.81		0.000	l:	11/.4/	15.00	41 -	20	4	٠.		240
١	15	DD-DIK	22.0	3.01	1		.,	. 1	13.00		42	1 '			
1	16	BD-BIX	22.5			١ .		89.42	12.84	41	38	3	85		
1	17	BD-BIX	42.1	9.89	0 80	<0.005		09.42	12.04	4,1	41	ا د ا	00		- 25
l	18	BD-BIX	42.1	9.09	10.03	K 0.005	i .		20.73		32	'			
ı	19	BD-BIX			•				13.17	28					
	20	BD-BIX		l	ļ	K0.005		106.70		28	26	2			
۱	21	BD-BIX	27.5	9.99	0.91	0.003		111.00	15.60	·	25				·
İ	22	BD-BIX	27.3	9.98	0.90						25		00		ł
ı	23	עדם-חם	27.0	9.90	10.90			105.10			43	1	80		
1	24	BD-BIX		·		(0 005		110 (0						. •	
ı	25		,			(0.005		110.60	10 (1		33			. ' .	
ı		BD-BIX	27.1	0 07		•	*	100.04	12.61	·	33			٠,	
ľ	26	BD-BIX	27.1	9.97	0.84	10.00=		96.90	10.99		30				
	27	BD-BIX	06.7	10.00		(0.005			8.92		27				
ĺ	28	BD-BIX	26.7	10.04	0.82	,	,		l		22				[
۱	29	BD-BIX			Ī		ŀ	94.74	10.74		46		90		Į.
1	30	BD-BIX	•	ł		[ļ	99.59	8.34		43		,		
	31	BD-BIX	•		.	1	1	100.51	8.04		35				
ŀ	9/ 1/60	L		1		1 .	ľ	104.33	8.08].	31		•		
۱	2	BD-BIX		1				83.79	8.52		ا ا				٠.
1	3	BD-BIX			0.78		<u> </u>	98.74	6.37	. :	24		80		
1	4	BD-BIX	22.4	9.98		,	'	121.45	5.90		43				· ·
1	5	BD-BIX		'			1	89.62			36)
	6	BD-BIX	23.4	9.95	0.66			, 89.81			31		•		
1	7	BD-BIX		1 .		<0.005		97.91	· .		28	1	•		
1	8	BD-BIX			j i			96.85			23				
-	,	BD-BIX	23.0		0.69	ì					20	.			1
1				<u> </u>	<u> </u>		<u> </u>								

REACTOR COOLANT FISSION PRODUCT SPECIFIC ACTIVITIES

	Reac	Level				1.· v-v-	**		Speci				- 10											н-3
Date	Hrs.	% .	Cs-136	Cs-137	Cs-138	Cs.¬139	Kr85m	Kr-87	Kr-88	Br-82	Br-83	Br-84	Xe-133	Xe-135	I-131	I-133	Sr-89	Sr-90	Sr-91	Sr-92	Ba-139	Ba-140	A-41	4c/1
6/23/60 24 25 26 27 28 29 30 7/ 1/60 2 3	12 2 22 46 71 95 119	74 52 100 100 100 100 100 100 100	0.0075 0.284	0.142	12.5 13.7 17.5	4.2	4.97	4.32	14.0 13.5				49.3	16.4		5.25 16.2 14.6	0.0018		0.132	0.049	0.300		5.45	118.4
5 6 7 8 9	308 332 356 380 406	100 100 75 80 100			15.0 16.7				16.3	0.578	1	-	·		14.1 17.7	13.0 14.7	0.0642			0.038		0.0025		! !
11 12 13 14 15		* * *	0.478	1.215											45. 63. 64.	15.8 12.6 11.1								
17 18 19 20 21		72			8.55		2.38	1.28					26.4	9.90	44.3 45.3 47.0 40.5 45.	4.80 8.82 20.5 14.6 27.1							5.40	

^{*} Training School Operation - Criticality once per shift and approximately 1/2 hour at 35% reactor power

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TABLE II (cont'd)

REACTOR COOLANT FISSION PRODUCT SPECIFIC ACTIVITIES

		Reac								Spec	ific	Acti		7 - 10	000 d	pm/m1	 [-		
ı	Date	Power Hrs.		Cc-136	Cs-137	Co-139	Co. 1 20	Kr-85m	ע - עד 19 - עד								T-133	Sr-89	Sr-90	10 01	Ta - 00	In 100			H-3
	Date	nts.	/6	CS-130	08-13/	C8-130	CS-139	Kr-oom	Kr-0/	KT-00.	BT-02	BF-63	BT -04	xe-133	xe-133	1-131	1-133	Sr-69	Sr-90	Sr-91	Sr-92	Ba-139	Ba-140	A-41	c/1
	7/23/60 24	90	1													<u> </u>									
	25 26	50 64	4	0.514	2.27	17.5				10.9	0.678	1.15	1.47	,		45	37.5								
	27	56	7	0.521	2.24					10.9	0.078	1.15	1.47			42.6	24.7.	0.0112		0.085	0.088	0.751	0.0085		
	28 29	38 40	5			·				·	İ			٠,	·	60.5	39.5			· .					
	30 31		· 0					٠.													l .				·
	8/ 1/60 2	3 2	60 75	0.651	2.71			4.50	3.90	23.6 16.9	0.470	2.36	1.62	68.0	21.8	49.5	12.0	0.0116				•	0.0098	2 58	
	3	12 36	100 100	0.650	2.99	17.8		3.75		-		3.50			16.9					0.077	0.086		0.0070		1 1
۰	5	48	100			14.5		3.75	3.30	13.7				40.7	10.9	45.2	15.8				1			5.20	
	7	66 1	100 46	-	ļ `								·						·						150.2
	.9	13 · 37	100 100	0.645	2.36	13.2		4.78	3.92	19.1	1.35	3.35		70.5	16.9	38.8	21.3	0.0469				0.954	0.0421	2.38	
	10 11	67 80	100 100	0.722	2.53	18.9				15.0									İ	000	0.182	i			
	12 13	99 	103			17.2				19.0						30.3	19.0		٠.	0.050	0.102				
-	14						•	:									r	'		'					
	15 16	5 21	100 104							16.9	0.835	2.94				40.0	16.0					0.885	0.0040		
	17 18	46 73	100	0.854	2.64	17.2	3.85	3.26	2.62	•		•		85.5	9.20									1.74	
	19 20	3 30	100 100		2.72					20.4						43.6	41.8								
	21	54 79	106		2 71	16.1		, .				-						,							265.1
			100	0.402	1	10.1			·	L										<u> </u>	<u> </u>				

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MODIFIED PURIFICATION SYSTEM PERFORMANCE TEST DLCS 2130201 (T-641124-A)

TABLE II (cont'd)

REACTOR COOLANT FISSION PRODUCT SPECIFIC ACTIVITIES

	Reac Power						·		Snoo	1610	Act		y - 10	ስስስ ፈ	nm /m1				·					
Date	Hrs.		Cs- 36	Cs-137	Cs-138	Cs-139	Kr-85m	Kr-87	Kr-88	Br-82	Br-83	Br-84	Xe-133	Xe-135	1-131	I-133	Sr-89	Sr-90	Sr-91	Sr-92	Ba-139	Ba-140	A-41	H-3 ⊮c/1
%/23/60 24 25	103 122 150	104 104 105	0.422	2.45	15.0	·	2.95	5.1	13.8	1.98	3.98		73.2	10.1	35.6	20.7	0.045		0.061	0.065		0.034	3.52	
26 27 28	171 196			2.48	17.8	-	,		17.3						29.5	16.6								
29 30 31	243 267 297			2.79 1.40	17.0 18.9	2.23	 	-		1.35	3.89				18.8	12.9					0.640			
9/ 1/60 2 3		100 100 100					. :		15.3				٠		21.7	17.4								
4 5 6	391 416 439	100 100 100							19.3	2.04	4.21				16.2		0.045				0.837			
7 8 9 10	458 488 506 530	100 100 100 100			16.0			ļ:	14.4				·		17.5	16.5			0.074	0.072		0.008		
12	0		0.760	2.48				<u> </u>	ļ. 															

TABLE III

REACTOR COOLANT CORROSION PRODUCTS

: [In S	Servic	Out Se	rvice		Crud Weight	Crud	% Fe ₃ 0 ₄	Fe mg/mg	Co mg/mg	Sp Activity (cpm/mg)106				uced Activi pm/mg at T ^O	ty			% of Total
		Time			Source	mg					TO + 120hr3	Fe-59	Co-58	Co-60	Mn-54	Zr-95	Hf-181	Cr-51	Activity
Γ	(1 ₆ .5)																	 	, necestery
6	/23/6		6/24/60				45.20	1		· .		l			1		: _		ł
	24				BD-BIX		44.20	90.8	0.63	0.0031	11.70	2.60 x 106		1.58×10^7	1.81 x 106	1.10 x 10 ⁵	6.80×10^{5}	2.85 x 106	79.8
. 4	25 Ş	141			BD-BIX		8.61							1				}	`
	26	1920			BD-BIX		10.66			1	i		'	l :				1	ŀ
4,	27	145			BD-BIX		9.00			'				1	1			:	1
	28	142			BD-BIX		5.24	98.2			19.0		٠.				٠, .		ŀ
	29.		7/ 1/60		BD-BIX		5.05										•		
17	/ 1/6	50 132			BD-BIX		4.28									1 %			
		112			BD-BIX		3.85	95.4			15.9					• •	. 2.	i	1
		. 104			BD-BIX		7.08				•			· ·			. '	l _	· .
٠ [.	11	150 112			BD-BIX		11.61	1					•		1.			[]	1
	13	125			BD-BIX BD-BIX		7.09				,,,,	•	•		ľ .		-		1
. [14	085			BD-BIX		8.05	1			19.0		•				•	1-	1
	16	141			BD-BIX		18.61	1]	•	İ		,			ļ.]	1
	-18	092			BD-BIX		14.87								i				
-	19				BD-BIX		16.78	ł .					•	i e				1	1
	20	090			BD-BIX		1.07	1		1			•				ľ		
1	21	085			BD-BIX		8.71			0.00084	16.30	2 87 - 106	1 96 - 106	2.49×10^{7}	2 07 - 106	2 22 - 105	0 54 - 105	1 75 - 106	88.4
	22	095			BD-BIX		1.82	98.6		0.00004	1 20.30	2.07 2.10	1.30 X 10	2.49 2 10	2.07 X 10	2.33 X 10	7.34 X 10	11.73 × 10°	00.4
٠.	23	- 163			BD-BIX		3.04			}	15.00	-		1 .	.[`	<u>}</u>		1
.	25	1040			BD-BIX		2.99	1			23.00								ı
14	28		8/ 1/60		BD-BIX		10.30												
8	/.1/6	090	4		BD-BIX		5.65	1 [1	l				1	İ	,	· ·	1
	4	093	8	0950	BD-BIX	12.66	10.08	98.8		Ī	17.30						ŀ		
1.	. 8	101	15	1130	BD-BIX	19.11	8.25	92.0			19.30				9	,		1	
1	15	: 114	22 .	1100	BD-BIX	23.41	6.42	94.0			[•			1		1	1	
Ī	22	110	29	0845	BD-BIX	13.06	3.90	93.5	0.657	0.00018	16.10	2.64 x 106	2.54 x 106	1.85 × 10 ⁷	2.01 x 106	0.9 x 105	12.2 x 105	0.81 x 106	73.2
	29	1015	9/ 6/60	0945	BD-BIX	14.23	2.82				16.00			· ·			20	:	1
9	/ 6/6	50 0956	12	0900	BD-BIX	6.20	1.95	97.0											1 .
L		4					<u> </u>				<u> </u>			L	<u> </u>		İ	ļ. ·	1

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MODIFIED PURIFICATION SYSTEM PERFORMANCE TEST DLCS2130201 (T-641124-A)

TABLE IV

1BD HAIRPIN LOOP RADIATION LEVELS

						·
			Gross	Radiati	on Levels	
		Total	Gen.	Vertical	Horizontal	
		Core I	Output	Section	Section	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
Date	Time	EFPH	mw	mr/hr	mr/hr	Remarks
	ľ					
6/24/60	1120	6592.4	60	3,2	25	Loop filled and isolated
6/24/60	1210	<u> </u>	·			Loop returned to service
7/ 7/60	1045	6879.6	67			Loop isolated.
7/ 7/60	1400		1	30	40	
7/ 7/60	1608]	33	40	
7/ 8/60	0220		ļ	30	35	· .
7/8/60	0710	6900.2	~"67 ·	· ·		Loop returned to service
8/ 5/60	0600	7180.8	48	,		Loop isolated
8/ 5/60	0900	 .		43	50	·
8/ 5/60	1100			35	40	-
8/ 5/60	2100			30	40	
8/ 5/60	2120	7193.8	67			Loop returned to service
8/22/60	0610	7533.9	66		,	Loop isolated
8/22/60	0910			21	24	
8/22/60	1116			18	22	
8/22/60	2110			10	12	·
8/22/60	2130	7549.8	66			Loop returned to service
9/ 1/60	0600	7784.7	67			Loop isolated
9/ 1/60	0907	1,,04.,	١ ٠,	30	28	2007 20014100.
9/ 1/60	1105		ĺ	24	35	
9/ 1/60	2105	}		35	28	
9/ 1/60	2110	7800.6	67) 33	20	Loop returned to service
9/ 9/60		7985.0	66			Loop isolated
9/ 9/60	0905	7,505.0	00	51	55	nooh rootaten"
9/ 9/60	1100			42	44	
	2100			32	25	
9/ 9/60]	,	23	28	ARIGNALIS TA MISEL (BELIA) (CO.
9/ 9/60	2100	0001	67	23	40	7
9/ 9/60	2130	8001.1	67			Loop returned to service
<u></u>	1	l	<u> </u>	}	I	<u> </u>

TABLE V
METER CALIBRATION DATA

Jordan Survey Meter No. 733 (with extension cord on probe)

	Cali	bration	Date (Sour	cce Co 6	0)
6/1	0/60	7/7	/60	8/5	/60
mr	/hr	mr	/hr	mr	/hr
Calc.	Meas.	Calc.	Meas.	Calc.	Meas.
. 5	5	5	5.7	:5	5
10	11.5	10	12	10	11
· 1.5	16	25	28	25	28
54	54	50	60	50	58
100	105	100	115	100	110
150	145	150	155	250	255
250	250	250	250	500	500
500	500	500	500	1000	1000
1000	1000;	1000	1000	1500	1500
1500	1500	1500	1500 / 1		

Log of Events

June 1960		
June 24	Reactor critical, system temperature 500 F and pressure 1800 psig. The main unit generator was placed on the line and gross output increased to 58 mw. The 1A, 1B and 1C reactor coolant pumps on fast speed. The 1D coolant loop isolated with the 1D reactor coolant pump off. The 1AC purification demineralizer was isolated. The 1BD purification demineralizer is in service without resin. (The resin was flushed from the 1BD demineralizer on June 17, 1960)	
1120	1BD hairpin loop isolated	
1210		
1218	1BD hairpin loop returned to service	
1355	Load increased to 67.5 mw gross Load decreased to 57 mw gross	
1800	Load increased to 60 mw gross	
1824	Safety shutdown and main generator off the line	
1024	Safety Shutdown and main generator off the fine	
June 25		
Julie 25		
0440	Reactor critical with primary system temperature 497 F and pressure 1800 psig.	
0658	Generator synchornized	
1710	Load increased to 32 mw gross	
1011	Load increased to 67.5 mw gross	
June 27		
0658	Load decreased to 62 mw gross	·
1710	Load decreased to 52 mw gross	
1015	1D coolant loop depressurized to primary storage tank pressure	
1610	Load decreased to 47 mw gross	
1835	Load increased to 67 mw gross	
June 28		
0300	1D coolant loop steam flushed and drained	
0620	Load decreased to 53 mw gross	
0645	Load decreased to 47 mw gross	
1108	Load increased to 61.5 mw gross	
1323	Load increased to 67.5 mw gross	
June 30		
0708	Load decreased to 54 mw gross	
0935	Load increased to 67 mw gross	
	en en en en en en en en en en en en en e	

July 1	
1838 1914 1950 2320	Throttle tripped and main generator off the line Generator synchronized Load increased to 48 mw gross Load increased to 67 mw gross
July 7	
0703 0950 1045 1300	Load decreased to 50 mw gross Load increased to 67 mw gross 1BD hairpin loop isolated 1D coolant loop filled to top of 1D reactor coolant pump vent
July 8	
0710 0720 1110 2210	1BD hairpin loop returned to service Load decreased to 56 mw gross Load increased to 67 mw gross 1D reactor coolant loop drained
July 9	
1645 1721 1750	Main generator taken off the line All control rods placed on the bottom of the reactor 1A, 1B and 1C reactor coolant pumps transferred to slow speed
July 10	
0630	1A and 1C reactor coolant pumps removed from service
July 11	
1122	Reactor critical, primary system at temperature of 494 F and pressure of 1750 psig. 1A, 1B and 1C reactor coolant pumps on fast speed
1229	Main generator on the line at load of 45 mw gross
1420	Load increased to 60 mw gross
1820	Main generator taken off the line

Log of Events (cont'd)

July 11 to	
July 17	From July 12 through July 15, students from the Nuclear Training
	School performed station start-ups and shutdowns, and the reactor
	was critical for a total of approximately 26 hours. On July 14
	the 1AC purification demineralizer was flushed and on July 15 the
	1D reactor coolant loop was filled, hydro-tested, and made avail-
	able for service.
	On July 1/ the primary system was cooled to 170 F and 450 psig to
• •	permit placing the 1D loop in service. The plant was heated up
	with flow in four loops and all the reactor coolant pumps operat-
	ing on slow speed.
July 18	
•	
0545	1B reactor coolant pump removed from service. 1A, 1C and 1D
	reactor coolant pumps transferred to fast speed.
0620	Reactor critical, primary system at temperature of 494 F and
2	pressure of 1790 psig.
0920	Main generator put on the line and load increased to 35 mw gross.
1318	Load increased to 57 mw gross
1710	Load decreased to 17 mw gross
1855	Load decreased to 5 mw gross
2025	Load increased to 25 mw gross
7 1 30	
July 19	
0306	Load increased to 34 mw gross
1028	Load increased to 41 mw gross
1312	Load increased to 48 mw gross
1801	Main generator taken off the line
1828	All control rods placed on the bottom of the reactor
July 20	
Cancello	
0249	Reactor critical, primary system at temperature of 490 F and
	pressure of 1800 psig.
0418	Main generator put on the line and load increased to 47 mw gross
0550	Load increased to 61 mw gross
0627	Load decreased to 48 mw gross

Load decreased to 34 mw gross Load increased to 61 mw gross Load increased to 64 mw gross

1120 1707 1930

July 21	
0627	Load decreased to 25 mw gross
1125	Main generator taken off the line
1205	All control rods placed on the bottom of the reactor
1804	Reactor critical, primary system at temperature of 480 F and
	pressure of 1800 psig.
1928	Main generator put on the line and load increased to 25 mw gr
7 7 9 00	
July 22	
0040	Load increased to 54 mw gross
0250	Load increased to 60 mw gross
0703	Load decreased to 34 mw gross
1155	Load increased to 48 mw gross
1733	Load increased to 40 mw gross
<u> 1</u> 735	Load Increased to 00 mw gross
July 23	
	¥ ·
0729	Main generator taken off the line
0804	All control rods placed on the bottom of the reactor
1243	Reactor critical, primary system at temperature of 510 F and
	pressure of 1800 psig.
1412	Main generator put on the line
1420	Load increased to 15 mw gross
1457	Load increased to 25 mw gross
1957	Load increased to 34 mw gross
,,	
July 24	
0050	Load increased to 48 mw gross
0550	Load increased to 57 mw gross
2000	Main generator taken off the line
2037	All rods placed on the bottom of the reactor
July 25	
0039	Reactor critical, primary system at temperature of 520 F and pressure of 1960 psig.
0147	Main generator put on the line
0154	Load increased to 25 mw gross
0710	Load increased to 34 mw gross
1212	Load increased to 48 mw gross
1730	Load increased to 54 mw gross
1953	Load increased to 58 mw gross
	Edge Thoropole to be my Prope

July 26	
0652	Main generator taken off the line
0730	All rods placed on the bottom of the reactor
1120	Reactor critical, primary system at temperature of 490 F and
1120	pressure of 1785 psig.
1153	Main generator put on the line and at 10 mw gross
1210	Load increased to 43 mw gross
1510	Load increased to 48 mw gross
1955	Load increased to 54 mw gross
2055	Load increased to 57 mw gross
203,3	
July 27	
. 0650	Load decreased to 33 mw gross
1406	Main generator taken off the line
1440	All control rods placed on the bottom of the reactor
1906	Reactor critical, primary system at temperature of 507 F and
	pressure of 1950 psig.
2022	Main generator put on the line
2100	Load increased to 34 mw gross
2130	Load increased to 45 mw gross
2325	Load increased to 60 mw gross
July 28	
0120	Load increased to 65 mw gross, primary system at temperature of
0120	520 F and pressure of 1985 psig.
0618	Main generator taken off the line
0652	All control rods placed on the bottom of the reactor
0912	1A, 1C and 1D reactor coolant pumps transferred to slow speed
1108	Reactor critical, primary system at temperature of 517°F
1150	Main generator placed on the line
1220	Load at 25 mw gross
1223	Load decreased to 21 mw gross
1720	Main generator taken off the line
1802	All control rods placed on the bottom of the reactor
2002	Reactor critical, primary system at temperature of 478 F and
	pressure of 1800 psig
2100	Main generator put on the line
2110	Load increased to 21 mw gross
2317	Safety shutdown and main generator off the line
2323	1A, 1C and 1D reactor coolant pumps transferred to fast speed

TEST RESULTS DLCS 2130201 T-641124-A

MODIFIED PURIFICATION SYSTEM PERFORMANCE TEST

July 29	
0521	1A, 1C and 1D reactor coolant pumps transferred to slow speed
0602	Reactor critical, primary system temperature at 483.5°F and pressure of 1800 psig
0725	Main generator put on the line and increasing to 21 mw gross
0800	Load increased to 22.5 mw gross
1506	Main generator taken off the line
1530	All control rods placed on the bottom of the reactor
1555	1A, 1C and 1D reactor coolant pumps transferred to fast speed
1755	1A, 1C and 1D reactor coolant pumps transferred to slow speed
1838	Reactor critical, primary system at temperature of 473 F and pressure of 1800 psig.
1924	Main generator put on the line
1940	Load increased to 20 mw gross
July 30	
0020	Main generator taken off the line
0044	All control rods placed on the bottom of the reactor
0315	Reactor critical, primary system at temperature of 473.5 F and
	pressure of 1800 psig.
0359	Main generator put on the line and at 5 mw gross
0405	Load increased to 22 mw gross
0851	Main generator taken off the line
0904	1A, 1C and 1D reactor coolant pumps transferred to fast speed. 1B reactor coolant pump put in service on fast speed.
1114	All reactor coolant pumps transferred to slow speed
2011	All reactor coolant pumps transferred to fast speed
July 31	
0940	All reactor coolant pumps transferred to slow speed
1849	All reactor coolant pumps transferred to fast speed
2219	1A, 1C and 1D reactor coolant pumps transferred to slow speed.
	1B reactor coolant pump removed from service.
2308	Reactor critical, primary system at temperature of 510 F and
	pressure of 1900 psig.
August 1	
0117	Main generator put on the line and at 5 mw gross
0122	Load increased to 15 mw gross
0648	Main generator taken off the line.
0710	All control rods placed on the bottom of the reactor

August 1	
1 0907	1A, 1C and 1D reactor coolant pumps transferred to fast speed.
0057	1B reactor coolant pump put in service on fast speed.
0957 1017	1B reactor coolant pump removed from service Reactor critical
1140	•
	Main generator put on the line
1152 1355	Load increased to 40 mw gross
	Load decreased to 5 mw gross
1445	Load increased to 23 mw gross Load increased to 43 mw gross
1514	
1535	Load decreased to 35 mw gross, primary system at temperature of
1750	500 F and pressure of 1800 psig.
2050	Load increased to 55 mw gross
2030	Load decreased to 43 mw gross
2140	Load increased to 63 mw gross Load decreased to 43 mw gross
2200	
•	Load decreased to 23 mw gross Load decreased to 5 mw gross
2232 2245	
2243	Load increased to 63 mw gross
August 2	
0650	Load decreased to 20 mw gross
0825	Load increased to 59 mw gross
0915	Load decreased to 50 mw gross
0942	Load decreased to 40 mw gross
1230	Load increased to 50 mw gross
1807	Load increased to 64.5 mw gross
August 4	
0845	Load decreased to 50 mw gross
1108	Load decreased to 38 mw gross
1313	Load increased to 45 mw gross
1530	Load increased to 60 mw gross
1615	Load increased to 64 mw gross
	noun incicated to 04 mm group
August 5	
0033	Main generator taken off the line
0105	All control rods placed on the bottom of the reactor
0240	1B reactor coolant pump put in service on fast speed
0346	Reactor critical, primary system at temperature of 500 F

August 5	
0436	Main generator put on the line and at 8 mw gross
05 30	Load increased to 48 mw gross
0600	1BD hairpin loop isolated
1510	Load increased to 60 mw gross
1747	Load increased to 66 mw gross
2120	1BD hairpin loop returned to service
	- 100 married 100p recorded to our vree
August 7	
- VE	
1205	Load decreased to 28 mw gross
1510	Load increased to 48 mw gross
2050	Load increased to 65 mw gross, primary system at temperature of
	500 F and pressure of 1785 psig
· ·	
August 8	
0120	Load increased to 66 mw gross
August 9	
0707	Load decreased to 47 mw gross
0830	Load increased to 66 mw gross
August 10	
0840	Load decreased to 60.5 mw gross
0930	Load increased to 65.5 mw gross
August 11	
0652	Load decreased to 50 mw gross
0703	Load decreased to 37 mw gross
0727	Load increased to 49 mw gross
0920	Load increased to 66 mw gross
August 13	
0825	Performed rapid station shutdown in accordance with DLCS 34401
1013	1B reactor coolant pump removed from service
1015	1B reactor coolant loop main hydraulic valves closed
1751	1B reactor coolant pump put in service at slow speed with loop
	by-pass valve open.
1225	Performed xenon transient test DLCS 1560109

•	
August 14	
1833	1B reactor coolant pump removed from service
1838	1B reactor coolant pump put in service at slow speed
August 15	
0046	1B reactor coolant pump removed from service
0047	1B reactor coolant loop main hydraulic valves opened and 1B
0047	reactor coolant pump put in service at fast speed.
0100	1B reactor coolant loop by-pass valve closed
0620	Reactor critical, primary system at temperature 500 F and
•	pressure of 1790 psig.
0702	Main generator put on the line
0710 0729	Load increased to 37 mw gross Load increased to 58 mw gross
1115	Load increased to 50 mw gross Load increased to 63 mw gross
1710	Load increased to 66 mw gross
August 18	
1602	Main generator taken off the line
August 19	
Adgust 19	
0029	Main generator put on the line and at 10 mw gross
0035	Load increased to 47 mw gross
0650	Load increased to 66 mw gross
A 22	
August 22	
0610	1BD hairpin loop isolated
2130 .	1BD hairpin loop returned to service
August 26	
0315	Safety insertion
0313	Safety Insertion
September 1	
0 600	1BD hairpin loop isolated
2110	1BD hairpin loop returned to service

September 6	
1640 1743	Load decreased to 50 mw gross Load increased to 61 mw gross
September 7	
1305 1400	Load decreased to 50 mw gross Load increased to 66 mw gross
September 9	
0600 2130	1BD hairpin loop isolated 1BD hairpin loop returned to service

Results Prepared By Thomas X. Seberry h.	30
Results Reviewed By Shward Ines	
Approved (Duquesne Light Company) Learge Whatel Date	7-21-61