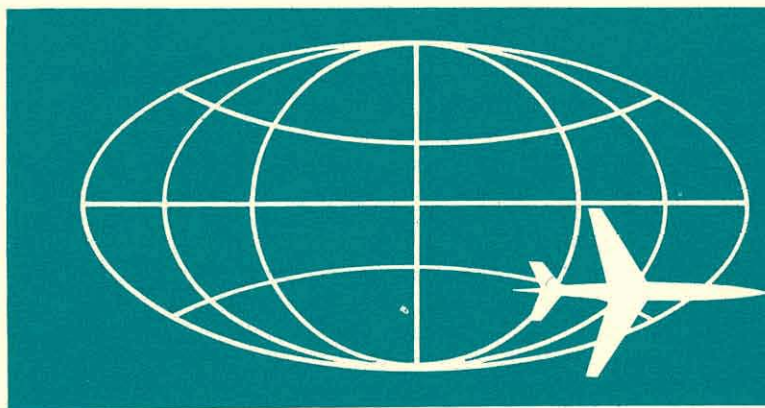


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Program ODD -

A One-Dimensional Multigroup Code for  
The IBM-7090 (ANP Program No. 657)

P. G. Fischer  
F. D. Wenstrup  
T. A. Hoffman

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APEX 702  
(Informal)

UC-34 Physics  
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PROGRAM ODD - A ONE-DIMENSIONAL MULTIGROUP CODE FOR THE  
IBM-7090 (ANP PROGRAM NO. 657)

P. G. Fischer, F. D. Wenstrup, T. A. Hoffman

June 30, 1961

UNITED STATES AIR FORCE

CONTRACT NO. AF 33(600)-38062

UNITED STATES ATOMIC ENERGY COMMISSION

CONTRACT NO. AT(11-1)-171

**GENERAL  ELECTRIC**

AIRCRAFT NUCLEAR PROPULSION DEPARTMENT

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ABSTRACT

This report discusses the physical and mathematical reactor models which are used in Program ODD. In addition, the report contains the FORTRAN II source program listings, decimal data input sheets and input and output for a sample case.

Program ODD was designed to make use of the Revised Nuclear Data System at ANPD which consists of twenty-five energy group cross-section data including high energy inelastic scattering matrices, resonance parameters for the resolved resonances and thermalization scattering matrices for the near thermal energy region.

The most unique aspect of the program is the mathematical technique employed for eliminating inner iterations and slow convergence rates occasioned by the "up-scattering" in the thermalization region of the energy lattice. Direct inversion of the energy matrix coupling the thermal and last four epithermal groups provides simultaneous consistent solutions for these groups within each power iteration.



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## 1.0 INTRODUCTION

Program ODD is a one-dimensional multigroup code using the diffusion approximation to the Boltzman equation to determine neutron fluxes and criticality in a reactor core. In these aspects it is very similar to many existing codes written at ANPD and at many other installations, and it is perhaps in order at this point to justify, or attempt to justify, the existence of still another such code. Actually, a special-purpose code, since it makes most efficient use of machine time, rapidly pays for itself in repetitive production use and this is generally justification enough. In addition, existing multigroup codes are either designed for a particular nuclear data system or, more usually, require extensive decimal input with associated high error probability in production use. With this background then, Program ODD can be justified as the basis production diffusion code corresponding to the ANPD Revised Nuclear Data System\* although both are really justified together. Thus the Nuclear Data System was designed to contain the maximum energy detail which could be used on multigroup codes, both diffusion and transport, completely contained within a 32,000 word memory for problems of typical ANP complexity. Such a goal is realizable only with a specially designed nuclear data system and specially designed calculational codes.

The basic calculational blocks of Program ODD consist of: (a) composition data preparation; (b) regional data preparation; (c) one-dimensional diffusion calculations.

The composition data preparation portion, other than the use of a 25-group data tape, performs almost identically to the precalculational portions of Program C<sub>5</sub>\*\* after which it was modeled. This section of the program processes of up to 100 compositions consisting of up to 30

---

\* "IBM-7090 Programs to Compile and Modify a Nuclear Data Tape",  
F. D. Wenstrup, etc., APEX 708

\*\* Program C<sub>5</sub>, Direct and Adjoint Bare Reactor Program ..., XDC 59-6-220

materials each. In addition to the usual homogenization procedures involving material self-shielding factors, Behrens corrections for enhanced diffusion on the presence of lumped voids, etc., the program provides for adjustment of resonance-region absorption and fission cross sections on the basis of computed or input specified self-shielding factors. The processed composition data are stored on an auxiliary tape which may be used directly in future calculations or to which additional data may be added in future runs.

The second logical program block selects, on the basis of input data, a maximum of 20 of the previously processed compositions for use in a single one-dimensional calculation. A given region of the reactor core may be specified then by a single composition or any mixture of these 20 compositions. This latter provision is useful for multiregion reactor cores which differ only in moderator-to-fuel ratio or void fraction, for example.

The one-dimensional multigroup calculation uses the basic Gauss-Seidel iteration scheme to converge on the fundamental space mode of the neutron flux. The only really unique feature is the simultaneous inversion of the last five groups, which avoids the necessity of inner iterations and poor convergence which generally occur in the presence of "up-scattering". The space detail is limited to 150 lattice points in up to 100 regions (utilizing only 20 compositions or mixtures thereof). The present version contains no convergence acceleration procedures since the typical ANP reactor has a dominance ratio between the fundamental and first harmonic modes of about 5 and this produces satisfactory convergence in 8-10 power iterations.

After the convergence of the flux solution, various regional averages are computed and flux gradients are calculated if requested. The program provides automatic calculation of both adjoint and direct flux solutions if desired, and any number of individual reactor analyses, making use of the same composition tape, may be run sequentially. If only the regional data, e.g., region boundaries or external boundary conditions, are changed, the composition tape is not reread.

Each of these logical program blocks is discussed separately in Sections 2.0, 3.0, and 4.0, respectively. Section 5.0 contains the program input sheets; Section 6.0 discusses the operating instructions and machine set-up and gives the input and output for the sample case; and Section 7.0 gives the unassembled program listings.

## 2.0 COMPOSITION DATA PREPARATION

### 2.1 General Discussion

As the name implies, this portion of the program processes and combines the material cross sections read from the Reactor Nuclear Data Tape (RNDT)\* into the format required for the multigroup diffusion calculation,

$$\begin{aligned}
 -D(N)\nabla^2\phi(N) + \Sigma_r(N)\phi(N) = \frac{1}{\lambda} S(N) \sum_{N'} \nu\Sigma_f(N')\phi(N') \\
 + \sum_{N' \neq N} \Sigma_s(N'/N)\phi(N') . \quad (2.1)
 \end{aligned}$$

Thus, a homogeneous reactor region\*\* is characterized by the following parameters:

- $D_r(N), D_z(N)$  - group N diffusion coefficients for the radial and axial directions (cm). (The possible anisotropy arises from homogenization of coolant passages);
- $\Sigma_r(N)$  - macroscopic group removal cross section ( $\text{cm}^{-1}$ );
- $S(N)$  - fraction of fission neutrons emitted into group N;
- $\nu\Sigma_f(N)$  - macroscopic group fission production cross section ( $\text{cm}^{-1}$ );

\* The program does provide for decimal input of cross-sections, but, this was anticipated as a supplement to rather than a replacement for the RNDT.

\*\* The present version of the program assumes a cylindrical reactor consisting of stacked concentric annular regions. This restriction could be quite easily removed, however.

$\Sigma_s(N'/N)$  - macroscopic cross section for scatter transfer from group  $N'$  to group  $N$ .

The detailed program logic within this section is intelligible only with reference to the actual format of the data tape itself which is described elsewhere\*, but it is perhaps in order to summarize the required information. Thus, the data tape contains basically: (a) 25 group cross sections  $\sigma_s$ ,  $\xi\sigma_s$ ,  $\sigma_{tr}$ ,  $\sigma_a$ ,  $\nu\sigma_f$ , and  $\xi_1\sigma_{s1}$ ; (b) high-energy scatter-transfer matrices  $\sigma_s(N'/N)$ ; (c) resonance parameters for resolved resonances; (d) near-thermal scatter-transfer matrices  $\sigma_s(N'/N)$ ; (e) gamma ray energy production cross sections  $\sigma(N_n/M_\gamma)$ . Before homogenizing or mixing the individual material cross sections, the following operations are then performed: (a) on the basis of the specified material temperature, the corresponding thermal transfer matrix is selected and used also to adjust  $\sigma_s$  and  $\sigma_{tr}$  in the near-thermal region; (b) the resonance region  $\sigma_a$  and  $\sigma_{tr}$  are adjusted for self-shielding; (c) the scatter-transfer matrix is completed as required, since the data tape contains only a compressed matrix. The macroscopic cross sections are then computed as

$$\Sigma_x(N) = \sum_i N^i g^i(N) \sigma_x^i(N) \quad (2.2)$$

where  $N^i$  is input specified atomic density in atoms/barn-cm and the  $g^i(N)$  are spatial self-shielding factors, specified as input data if not unity.

In the following sections, the calculations outlined above are discussed in more detail.

## 2.2 Scatter Transfer Matrix

The RNDT contains scatter-transfer matrices coupling the last (lowest energy) five groups for ten discrete temperatures between 68°F. and 4500°F.

\* APEX 708 - "IBM-7090 Programs to Compile and Modify a Nuclear Data Tape", F. D. Wenstrup, et. al.

Rather than attempt an involved interpolation procedure to insure consistency, the nearest "standard" temperature is assigned if the input specified material temperature is non-standard. The near-thermal scattering cross sections are then adjusted as

$$\sigma'_s(N) = \sum_{N'} \sigma_s(N'/N) \quad , \quad 21 \leq N \leq 25 \quad (2.3)$$

$$\sigma'_{tr}(N) = \frac{\sigma_{tr}(N)}{\sigma_s(N)} \sigma'_s(N) \quad , \quad (2.4)$$

where the unprimed symbols refer to the quantities as read directly from the tape.

The high-energy scatter-transfer matrix appearing on the tape covers, for all practical purposes, only the region of inelastic scattering, since except for the very light elements, elastic scattering produces transfers only to the next (lower in energy) group. For this region of simply elastic scattering\*, the transfer cross sections are computed from

$$\sigma_s(N/N+1) = \frac{\xi \sigma_s(N)}{\Delta u(N)} \quad , \quad (2.5)$$

$$\sigma_s(N/N) = \sigma_s(N) - \sigma_s(N/N+1) \quad , \quad (2.6)$$

where  $\Delta u(N)$  is the lethargy width of group N. Equation (2.5) is derived assuming a flat-in-lethargy flux over group N, and initial correlation results seem to indicate that this is too gross an assumption. The same assumption has been used in processing the inelastic scattering matrix, for example, but a better physical representation could be quite easily incorporated, based on the ratio of scattering to losses within each group.

\* For the purposes of this section the elements hydrogen, helium, and lithium may be assumed to scatter inelastically throughout the entire energy range.

The various parts of the scatter-transfer matrix are then assembled as a 25-by-25 matrix.

### 2.3 Resonance Region Cross Sections

The 25-group cross sections on the RNDT represent, in the region from 1 ev to 1 Kev, averages over many isolated resonances for the heavier elements. Since these average cross sections are computed with a  $1/E$  flux weighting, they are appropriate only in the case of infinitely dilute quantities of the resonance absorbers; for finite dilution and especially in heterogeneous dispersion of resonance materials, the neutron flux-in-lethargy is characterized by minima corresponding to the cross section maxima, and this produces average cross sections lower than the infinite-dilution values. To attempt to account for this effect, Program ODD makes use of the resonance data also present on the RNDT to adjust the normal group cross sections. Thus, either homogeneous or heterogeneous (slab geometry) self-shielding factors can be calculated or the desired self-shielding factors may be supplied as decimal input. Effective resonance integrals are then computed for each group and used to reduce the basic 25-group absorption and fission production cross sections. The homogeneous effective integral calculation employs the so-called narrow resonance approximation\*. The heterogeneous slab geometry self-shielding calculation assumes no scattering within the absorber region, and a uniform incident flux from an adjacent moderator region\*\*.

#### 2.3.1 Homogeneous Resonance Integral

In the narrow resonance approximation, the effective integral over an isolated resonance may be written,

$$I_{\text{eff}} \approx \frac{I_0}{1 + \frac{N_i \sigma_0}{\Sigma_s}} \quad (2.7)$$

\* See, for example, "Resonance Absorption in Nuclear Reactors", L. Dressner, Pergamon Press, New York (1960), Ch. 2

\*\* The physical formulation and numerical procedure used in Program ODD are discussed in detail in XDC 61-4-17

where  $I_0$  is the infinite-dilution integral,  $\sigma_0$  is the peak cross section in the resonance,  $N_i$  is the absorber atomic density, and  $\Sigma_s$  is the background (constant) scattering cross section (macroscopic).

The effect of finite material temperature, Doppler broadening, may be approximately accounted for by adjusting the peak cross section in equation (2.7). Thus,

$$I_{\text{eff}}(T^\circ\text{K}) \approx \frac{I_0}{1 + \frac{N_i \sigma_0}{\Sigma_s} \psi(\theta, 0)} \quad (2.8)$$

where

$$\psi(\theta, x) = \frac{1}{\sqrt{4\pi\theta}} \int_{-\infty}^{\infty} \frac{\exp\left[-\frac{(x-y)^2}{4\theta}\right]}{1 + y^2} dy \quad (2.9)$$

is the Doppler-broadened isolated Breit-Wigner expression, and where  $\theta = R \cdot T$ . Equation (2.8) represents an additional approximation over (2.7) since it assumes that the broadened resonance retains a simple Breit-Wigner shape with only the peak cross section reduced.

The actual absorption and fission cross section adjustments are performed as

$$\Sigma'_a(N) = \Sigma_a(N) - \sum_{i,j} \frac{N_i I_0^j}{\Delta u(N)} \left[ 1 + \frac{\Sigma_s(N)}{N_i \sigma_{O_i}^j \psi(\theta_i^j, 0)} \right]^{-1} \quad (2.10)$$

$$v\Sigma'_f(N) = v\Sigma_f(N) - \sum_{i,j} \frac{N_i I_0^j \eta_i^j}{\Delta u(N)} \left[ 1 + \frac{\Sigma_s(N)}{N_i \sigma_{O_i}^j \psi(\theta_i^j, 0)} \right]^{-1} \quad (2.11)$$

where the summation is over all materials,  $i$ , and all resonances,  $j$ , whose energies  $E_{O_i}^j$  fall within group  $N$ , of lethargy width  $\Delta u(N)$ . The



quantities  $E_0$ ,  $I_0$ ,  $\sigma_0$ ,  $\eta$ ,  $R$  used in these equations are available on the RNDT while  $N_i$  and  $T_i$  are decimal input.

### 2.3.2 Heterogeneous Resonance Integral

For the case of heterogeneous dispersal of absorber material, the adjusted resonance-region cross sections are computed as

$$\Sigma'_a(N) = \Sigma_a(N) - \frac{1}{\Delta u(N)} \sum_{i,j} N_i I_{O_i}^j L_i^j \quad (2.12)$$

$$v\Sigma'_f(N) = v\Sigma_f(N) - \frac{1}{\Delta u(N)} \sum_{i,j} N_i I_{O_i}^j \eta_i^j L_i^j \quad (2.13)$$

The self-shielding factors can be computed, under the assumption of a purely absorbing slab and a uniform incident flux as\*

$$L = \frac{1}{\pi\tau} \int_{-\infty}^{\infty} \left[ \frac{1}{2} - E_3(\psi\tau) \right] dx \quad (2.14)$$

where  $\tau$  is the absorber-slab thickness, and  $E_3$  is the exponential integral of order three. The quantity  $\psi(\theta, x)$  is given by equation (2.9).

If the self-shielding factors are supplied as input data, equations (2.12) and (2.13) are used directly.

### 2.4 Diffusion Coefficient Calculations

The basic diffusion coefficient calculation in use at ANPD involves the calculation of a "size" correction based on the ratio of system total buckling to the total cross section\*\*. Thus

$$D(N) = \frac{1}{3[\Sigma_{tr}(N) + \Sigma_a(N) + \gamma(N)\Sigma_t(N)]} \quad (2.15)$$

\* KAPL-1241 - "The Absorption of Neutrons in Doppler Broadened Resonances" (1954) - G. M. Roe

\*\* APEX 121 - "Critical Mass Calculation for Bare Hydrogen Moderated Reactors by Means of Transport Theory" - D. S. Selengut

where

$$\Sigma_t(N) = \Sigma_s(N) + \Sigma_a(N) \quad (2.16)$$

The parameter  $\gamma(N)$  is calculated from

$$\gamma(N) = .26001 \alpha(N)^2 + .043502 \alpha(N)^4 + .0048942 \alpha(N)^6 \quad (2.17)$$

where

$$\alpha(N)^2 = K^2(N)/\Sigma_t(N) \quad , \quad (2.18)$$

with the total buckling calculated from input dimensions and an energy-dependent extrapolation distance. Equation (2.17) is used as an approximation to

$$\gamma(N) = 1 - \frac{\alpha(N) \tan^{-1} \alpha(N)}{3[\alpha(N) - \tan^{-1} \alpha(N)]} \quad .$$

The diffusion parameters  $D_r(N)$ ,  $D_z(N)$  are calculated as

$$D_r(N) = [1 + \epsilon_r(N)]D(N) \quad (2.19)$$

$$D_z(N) = [1 + \epsilon_z(N)]D(N) \quad (2.20)$$

with the Behrens\* factors are given by

$$\epsilon_r(N) = V_F^2 \left[ \frac{Y(N)}{e^{Y(N)} - 1} + Q_r Y(N) - 1 \right] e^{-X(N)} \quad (2.21)$$

\*See D. J. Behrens, "The Migration Length of Neutrons in a Reactor"

AERE T/R877, 1956; the attenuation factor  $e^{-X(N)}$  is added to account for absorption (fuel) in the void region.

and a similar expression for  $\epsilon_z(N)$  involving  $Q_z$ . In equation (2.21),  $V_F$  is the volume fraction of the void (fuel) region which is calculated from input data,  $X(N)$  is the optical thickness of the fuel region,  $Y(N)$  is the optical thickness of the moderator (scattering) region. The quantity  $Q$  is dependent on void geometry and may be different for the radial and axial directions. If the "Behrens" calculation is not requested;

$$\epsilon_r = \epsilon_z = 0 \quad .$$

## 2.5 Miscellaneous Calculations

### 2.5.1 Group Removal Cross Sections

Equation (2.1) does not contain either the group absorption cross section or the "scatter-in" cross section for the group itself. Instead, these are combined as

$$\Sigma_r(N) = \Sigma_a(N) + \Sigma_s(N) - \Sigma_s(N/N) \quad (2.22)$$

and then

$$\Sigma'_s(N/N) = 0 \quad . \quad (2.23)$$

### 2.5.2 Transmission Coefficients

For anticipated future needs, the present composition data preparation program includes calculation of transmission coefficients for a rod, annulus, or plate-type geometrical arrangement.

For a solid cylindrical rod of diameter  $D_0$ , in a channel of diameter  $D_{CH}$ , the energy dependent transmission fraction is

$$t(N) = 1 - \frac{D_0}{D_{CH}} \left[ \frac{(1 - \alpha_n)g_n}{1 - \alpha_n(1 - g_n/2\sigma_n)} \right] \quad (2.24)$$

with

$$\alpha_n = \frac{\Sigma_s(N)}{\Sigma_s(N) + \Sigma_a(N)} , \quad (2.25)$$

$$\sigma_n = \frac{D_0}{2} [\Sigma_s(N) + \Sigma_a(N)] , \quad (2.26)$$

$$g_n = \frac{4}{3} \sigma_n^2 \left[ I_0(\sigma_n)K_1(\sigma_n) - I_1(\sigma_n)K_0(\sigma_n) \right. \\ \left. + \frac{I_1(\sigma_n)K_1(\sigma_n)}{\sigma_n} + 2\sigma_n \left( I_0(\sigma_n)K_0(\sigma_n) + I_1(\sigma_n)K_1(\sigma_n) \right) - 2 \right] , \quad (2.27)$$

where I and K are the familiar Bessel functions.

For an annulus of thickness  $\epsilon$ , outer diameter  $D_0$ , and channel diameter  $D_{CH}$ ,

$$t(N) = 1 - \frac{D_0}{D_{CH}} \left[ \frac{(1 - \alpha_n)\sigma_n k_n}{1 - \sigma_n f_n} \right] , \quad (2.28)$$

with  $\alpha_n$  defined by (2.25) and,

$$\sigma_n = \epsilon [\Sigma_s(N) + \Sigma_a(N)] \quad (2.29)$$

$$k_n = \frac{1}{\sigma_n} [1 - 2E_3(2\sigma_n)] \quad (2.30)$$

$$f_n = \frac{1}{2\sigma_n} \left[ E_3(2\sigma_n) - 2E_3(\sigma_n) + \frac{1}{2} \right] \quad (2.31)$$

where  $E_3$  is the exponential integral of order three.

For a plate of thickness  $\epsilon$ ,

$$t(N) = 1 - \frac{2\alpha_n \sigma_n \left[ \frac{1}{2} - E_3(\sigma_n) \right]}{\alpha_n \sigma_n + \left[ \frac{1}{2} - E_3(\sigma_n) \right]} \quad (2.32)$$

with

$$\alpha_n = \frac{\Sigma_a(N)}{\Sigma_s(N)} \quad (2.33)$$

$$\sigma_n = \epsilon [\Sigma_s(N) + \Sigma_a(N)] \quad (2.34)$$

### 2.5.3 Gamma Energy Source Matrix

Although the present version of Program ODD does not provide a calculation of the space dependent gamma ray source due to fission, capture, and inelastic scattering, provision has been included for the necessary cross section calculations.

Gamma ray energy production cross sections (Mev barns) can be read from the RNDT for each element and combined to produce the composition source matrix,

$$\Sigma_\gamma(N/M) = \sum_i N^i g^i(N) \sigma_\gamma(N/M) \quad , \quad (2.35)$$

where N is the twenty-five-neutron-group index and M is an arbitrary gamma ray group index. The arbitrary character of the gamma-group index may be used to introduce any particular reaction cross section, e.g. (n, $\alpha$ ), by designating the alpha particle as an additional gamma ray group.

### 2.6 Composition Data Tape Format

After each composition composed of up to 30 materials is processed, the five parameters  $D_r$ ,  $D_z$ ,  $\Sigma_r$ ,  $v\Sigma_f$ , S for each of the twenty-five groups followed by the 25 x 25 matrix  $\Sigma_s(N/N')$  are written on tape as a single record. If the gamma ray production matrix has been calculated, it is written as a second record, otherwise a single word record is written to simulate it.

Each composition so processed is identified by two words of binary coded decimal information provided as input and a program calculated logical record number corresponding to the first of the two records

described above. After all desired compositions have been processed, this index information is written as the final tape record, followed by an end-of-file.

A restart case in which additional information is added to the composition tape, begins by reading in the existing index information and positioning the tape to the end of the previously written composition data. A total of 100 compositions may be written on a single tape.

A restart case in which no additional composition data is needed merely bypasses this portion of the program.

### 3.0 REGIONAL DATA PREPARATION

#### 3.1 General

The primary purpose of this portion of the program is to select up to twenty of the previously processed compositions from the Composition Data Tape, storing them in proper memory locations in a compressed format. This program block also checks the regional input data for consistency wherever possible to avoid later program malfunction.

#### 3.2 Composition Data Storage

The composition data, as written on tape by the preceding program block consists of  $5 \times 25 + 25 \times 25 = 750$  words for each composition. Actually, the scatter-transfer matrix is almost triangular since up-scattering occurs only among the last five groups. In addition the diagonal terms on this matrix are all zero (see section 2.5.1), so that the matrix may be compressed in memory to only  $190 + 100 + 25 = 315$  versus 625 as read from tape. These numbers represent respectively:

- (a) The maximum number of non-zero elements for down-scattering within the first twenty groups;
- (b) The maximum number of non-zero elements for down-scattering from the first twenty to the final five groups;
- (c) The maximum number of non-zero elements coupling the final five groups.

All of the composition data are stored as a single array in fast memory with access via an input specified list of compositions. Thus, the fourth specified composition's data begins  $440 \times 3 = 1320$  locations from the beginning of the array.

### 3.3 Consistency Requirements

Besides the table of Compositions needed to process the Composition Data Tape, the regional description of the reactor consists of:

- (a) left-hand reactor boundary,  $R_0 \geq 0$ ;
- (b) right-hand region boundaries,  $R_1 < R_2 < R_3 \dots < R_N$ ;
- (c) number of intervals in each region,  $N_1 \neq 0, N_2 \neq 0, \dots, N_N \neq 0$ ;
- (d) regional material identification consisting of 2 words of BCD information which must either be identical to one of the names in the Composition table or the first of the two words must be (1)MIX(2);
- (e) regional mixing densities defining how the material properties are to be computed if the identification begins with (1)MIX(2), at least one non-zero density out of NMIX possible;
- (f) dimension for computing transverse leakage in each region,  $H_1 \neq 0, H_2 \neq 0, \dots, H_N \neq 0$ .

If all the above requirements are satisfied, the program proceeds to the actual one-dimensional diffusion calculation.

## 4.0 ONE-DIMENSIONAL CALCULATION

### 4.1 General

The reduction of the diffusion equation (2.1) to a set of algebraic equations using the central difference approximation has been covered in detail in a previous document\* and will not be repeated here. As is well known, such a procedure produces a tri-diagonal matrix equation set for the space equations and such a system is well adapted for applying the Gauss\*\* elimination scheme for matrix inversion.

\* XDC 60-3-68

\*\* See, for example, "Methods of Applied Mathematics", Hildebrand, F. B., Prentice-Hall, New Jersey, 1952

Assuming a known fission distribution (the first term on the right side of equation (2.1)), the energy matrix, i.e., the twenty-five-group equations, form an almost triangular set. Thus, except for the final five groups, inversion of the energy matrix can be accomplished by solving the individual-group equations in succession, and this leads to the familiar Gauss-Seidel iteration scheme for solving (2.1)\*. Rather than resort to "inner" iterations required to obtain a consistent flux solution in the presence of the up-scattering in the final five groups, these latter are treated as a "single" group. The "forward elimination" in the space solution then requires inversion of a 5 x 5 matrix at each lattice point, although, of course, this is required only once per problem and the "back substitution" requires matrix multiplication at each lattice point. Such a procedure increases the required storage somewhat but is easily feasible when only a small number of groups are involved and more importantly yields easily predictable convergence rates which are now the same as the no "up-scattering" analysis. This latter point is very necessary for a "production" type analysis code.

#### 4.2 Diffusion Difference Equations

If the differentials in the one-dimensional analogue of Equation (2.1) are replaced by central differences over a lattice, the resulting equation is a three-point algebraic equation. Although the program inserts equally spaced lattice points within a given region, no attempt is made to formulate the difference equation for this case. Instead, the equations are formulated for the case of possibly unequally spaced points spanning a boundary between material regions; all other ordinary points are simply special cases of the general equation. Thus, the basic\*\* diffusion difference equation is

---

\* See, for example, APEX 539, Program F<sub>2</sub>

\*\* The difference equation used for the "combined" five thermal groups is not exactly of this form, but the differences are only trivial for the present discussion.



$$D_2(N)\varphi_{n+1}^K(N) = \left[ \beta_n D_1(N) + D_2(N) + \delta_n \Sigma_1'(N) + \gamma_n \Sigma_2'(N) \right] \varphi_n^K(N) \\ - \beta_n D_1(N)\varphi_{n-1}^K(N) - F_n^{K-1}(N) - S_n^K(N) \quad (4.1)$$

In equation (4.1), the subscripts 1,2 refer to the left and right-hand material regions, respectively, while  $n-1$ ,  $n$ ,  $n+1$  designate the three successive lattice points; the superscripts  $K$ ,  $K-1$  define the iteration sequence, while the primed symbols for the removal cross section include the trasverse leakage.

$$F_n^{K-1}(N) = \left[ \delta_n S_1(N) \sum_{N'} \frac{\nu \Sigma_{f1}(N')}{\lambda^{K-1}} + \gamma_n S_2(N) \sum_{N'} \frac{\nu \Sigma_{f2}(N')}{\lambda^{K-1}} \right] \varphi_n^{K-1}(N') \quad (4.2)$$

$$S_n^K(N) = \left[ \delta_n \sum_{N' < N} \Sigma_{s1}(N'/N) + \gamma_n \sum_{N' < N} \Sigma_{s2}(N'/N) \right] \varphi_n^K(N') \quad (4.3)$$

The three geometric coefficients  $\beta_n$ ,  $\gamma_n$ ,  $\delta_n$  do not depend on energy group or material properties. If the single space dimension is along a cartesian coordinate (slab geometry),

$$\beta_n = \frac{h_2}{h_1} \quad , \quad (4.4)$$

$$\gamma_n = \frac{h_2^2}{2} \quad , \quad (4.5)$$

$$\delta_n = \frac{h_1 h_2}{2} \quad (4.6)$$

where  $h_1, h_2$  are the lattice spacing to the left (n-1) and right (n+1) neighboring lattice points. For cylindrical geometry,

$$\beta_n = \frac{h_2}{h_1} \frac{1 + \left| \frac{r_n - \frac{h_1}{2}}{r_n + \frac{h_1}{2}} \right|}{1 + \left| \frac{r_n + \frac{h_2}{2}}{r_n - \frac{h_2}{2}} \right|}, \quad (4.7)$$

$$\gamma_n = \frac{h_2}{2} \frac{\left( r_n + \frac{h_2}{2} \right) - \left( r_n - \frac{h_2}{2} \right) \left| \frac{r_n - \frac{h_2}{2}}{r_n + \frac{h_2}{2}} \right|}{1 + \left| \frac{r_n - \frac{h_2}{2}}{r_n + \frac{h_2}{2}} \right|}, \quad (4.8)$$

$$\delta_n = \frac{h_2}{2} \frac{\left( r_n + \frac{h_1}{2} \right) - \left( r_n - \frac{h_1}{2} \right) \left| \frac{r_n - \frac{h_1}{2}}{r_n + \frac{h_1}{2}} \right|}{1 + \left| \frac{r_n + \frac{h_2}{2}}{r_n - \frac{h_2}{2}} \right|}. \quad (4.9)$$

The absolute value signs in 4.7, 4.8, 4.9 insure the proper numerical behavior for  $r \rightarrow 0$ , where  $r$  designates the distance (cm) of each lattice point from the origin. These equations are derived by requiring continuity of both flux and current across the region boundary.

Equation (4.1), which can be used for the interior points of the space lattice, must be supplemented by two additional equations for the exterior boundary points. These are obtained by using a Taylor

expansion over a small interval near the boundary, retaining only the first derivative. Assuming the boundary conditions are given as right and left albedos  $A^-$ ,  $A^+$ , one obtains then

$$\varphi_1(N) = \varphi_0(N) + \frac{h_-}{2D_1(N)} \left[ \frac{1 - A^-(N)}{1 + A^-(N)} \right] \varphi_0(N) , \quad (4.10)$$

$$\varphi_{N-1}(N) = \varphi_N(N) - \frac{h_+}{2D_N(N)} \left[ \frac{1 - A^+(N)}{1 + A^+(N)} \right] \varphi_N(N) , \quad (4.11)$$

where  $h_-$ ,  $h_+$  are assigned by the program as  $10^{-3}$  times a normal interval in the external boundary regions.

#### 4.3 Method of Solution

The tri-diagonal matrix equation set (4.1) for any one of the first twenty groups is solved by the familiar elimination, substitution technique. Thus, defining

$$V_1(N) = 1 + \frac{h_-}{2D_1(N)} \left[ \frac{1 - A^-(N)}{1 + A^-(N)} \right] \quad (4.12)$$

$$W_1(N) = 0 \quad (4.13)$$

successive elimination of the  $n-1$  component from equation (4.1) yields the recursion relations\*

$$V_{n+1}(N) = \frac{1}{D_2(N)} \left[ A_n(N) - \frac{\alpha_n D_1(N)}{V_n(N)} \right] , \quad (4.14)$$

$$W_{n+1}^K(N) = \frac{1}{D_2(N)} \left[ F_n^{K-1}(N) + S_n^K(N) + \frac{\beta_n D_1(N) W_n^K(N)}{V_n(N)} \right] , \quad (4.15)$$

\* If the lattice point  $n$  is not actually a boundary point, then obviously  $D_1(N) = D_2(N)$ .

with

$$\varphi_n^K(N) = \frac{1}{V_{n+1}(N)} \left[ \varphi_{n+1}^K(N) + w_{n+1}^K(N) \right] , \quad (4.16)$$

$$A_n(N) = \beta_n D_1(N) + D_2(N) + \delta_n \Sigma_1'(N) + \gamma_n \Sigma_2'(N) . \quad (4.17)$$

The right-hand boundary condition, equation (4.11), may be combined with equation (4.16) for the last two lattice points to yield

$$\varphi_n^K(N) = \frac{w_n^K(N)}{[B(N)V_n(N) - 1]} , \quad (4.18)$$

where

$$B(N) = 1 + \frac{h}{2D_n(N)} \left[ \frac{1 - A^+(N)}{1 + A^+(N)} \right] . \quad (4.19)$$

It should be noted that  $V_n(N)$  defined by equation (4.14) is iteration independent and need be evaluated only once per problem. The iteration sequence consists of successive solution of (4.15) and (4.16), supplemented by (4.18).

The last five groups, which are coupled by both "up" and "down" scattering are solved by defining, in analogy to (4.14), the matrix (5 x 5)

$$\left[ V_{jk} \right]_{n+1} = \frac{1}{D_2(j)} \left\{ \left[ A_{jk} \right]_n - \beta_n D_1(j) \left[ V_{jk}^{-1} \right]_n \right\} \quad (4.20)$$

where,

$$\begin{aligned} \left[ A_{jk} \right]_n &= \left[ \beta_n D_1(j) + D_2(j) + \delta_n \Sigma_1'(j) + \gamma_n \Sigma_2'(j) \right] \delta_{jk} \\ &- \left[ \delta_n \Sigma_{s_1}(K/j) + \gamma_n \Sigma_{s_2}(K/j) \right] \end{aligned} \quad (4.21)$$

where  $\delta_{jk}$  is the Kronecker delta. Equation (4.20) is started with the diagonal matrix

$$\left[ v_{jk} \right]_1 = \left\{ 1 + \frac{h}{2D_1(j)} \left[ \frac{1 - A^-(j)}{1 + A^-(j)} \right] \right\} \delta_{jk} , \quad (4.22)$$

in analogy to (4.12). Equation (4.15) now becomes

$$\left[ w_j^K \right]_{n+1} = \frac{1}{D_2(j)} \left\{ S_n^K(j) + \beta_n D_1(j) \left[ v_{jk}^{-1} \right]_n \left[ w_k^K \right]_n \right\} , \quad (4.23)$$

where it is explicitly assumed that no fission emission occurs within the "thermal" groups and  $S_n^K(j)$  now includes only the scattering from the higher twenty groups. Finally, the flux equations become,

$$\left[ \phi_k^K \right]_n = \left[ v_{jk}^{-1} \right]_{n+1} \left\{ \left[ \phi_k^K \right]_{n+1} + \left[ w_k^K \right]_{n+1} \right\} \quad (4.24)$$

and

$$\left[ \phi_j^K \right]_N = \left[ \left\{ \beta_k \delta_{jk} + v_{jk}^{-1} \right\}_{jk}^{-1} \right]_N \left[ v_{k\ell}^{-1} \right]_N \left[ w_\ell^K \right]_N . \quad (4.25)$$

As before, equation (4.20) is iteration independent and need be solved only once; actually, only the inverse matrices  $v_{jk}^{-1}$  need be stored.

Since the basic neutron diffusion equation (2.1) is linear and homogeneous, the normalization of the flux solution is completely arbitrary. For convenience, the flux normalization is fixed by imposing the auxiliary condition

$$\lambda^K = \int r^k dr \sum_N v \Sigma_f(N) \phi^K(N) . \quad (4.26)$$

5.0 PROGRAM INPUT SHEETS

PROGRAM ODD

Twenty-Five Group, One-Dimensional Diffusion Code

ANP IBM-7090 Program Number 657

Name - 12 BCD Characters

2BNAM,2,	
----------	--

Problem Identification - 18 BCD Characters

2BDENT,3,	
-----------	--

Date - 12 BCD Characters

2BDATE,2,	
-----------	--

Composition Data Tape Name - 12 BCD Characters

5CDTNAM,2,	
------------	--

3CDT,	1	,
-------	---	---

This card must be punched if an existing composition data tape is to be used.

→ MORE,		,
---------	--	---

= 1 → The next case is a composition data preparation case.  
= 2 → The next case is a regional data preparation case.

Composition Data Preparation Input

Composition Name - 12 BCD Characters

2CASEID,2,	①
------------	---

Spectrum Code Number

3SPEC,	
--------	--

(May be given as zero for a non-fissionable composition)

Material Input Table\*

RNDT Material Code Numbers

3CMAT,					
--------	--	--	--	--	--

Material Atom Density (barn cm)<sup>-1</sup> or Volume Fraction

3DMAT,					
--------	--	--	--	--	--

Material Weight (gm) - Give Corresponding DMAT = 0

3WMAT,					
--------	--	--	--	--	--

Material Temperature (°F)

3TMAT,					
--------	--	--	--	--	--

Behrens Region Code: 0 - Fuel, 1 - Moderator

4NBEHR,					
---------	--	--	--	--	--

Type Resonance Calculation (Use only if NCØDE(5) = 2,3)

4IRES,					
--------	--	--	--	--	--

0 - Calculate resonance self-shielding factors for this material.

1 - Resonance self-shielding factors given for this material.

\* NOTE: This table may be extended to 30 materials by use of page ODD - 3.



Materials Nos. 6 through 30

Material Input Table (continued)

N\* RNDT Material Code Numbers

3CMAT,	=,					
--------	----	--	--	--	--	--

N Material Atom Density (barn cm)<sup>-1</sup> or Volume Fraction

3DMAT,	=,					
--------	----	--	--	--	--	--

N Material Weight (gm) - Give Corresponding DMAT = 0

3WMAT,	=,					
--------	----	--	--	--	--	--

N Material Temperature (°F)

3TMAT,	=,					
--------	----	--	--	--	--	--

N Behrens Region Code: 0 - Fuel, 1 - Moderator

4NBEHR,	=,					
---------	----	--	--	--	--	--

N Type Resonance Calculation (Use only if NCODE(5) = 2,3)

4IRES,	=,					
--------	----	--	--	--	--	--

- 0 - Calculate resonance self-shielding factors for this material.
- 1 - Resonance self-shielding factors given for this material.

\* N increases by 5 for each set used.

Material Cell Corrections\*

Material No. 1

3GFAC,						
--------	--	--	--	--	--	--

3GFAC,	5 =					
--------	-----	--	--	--	--	--

3GFAC,	10 =					
--------	------	--	--	--	--	--

3GFAC,	15 =					
--------	------	--	--	--	--	--

3GFAC,	20 =					
--------	------	--	--	--	--	--

\* Cell corrections may be given at every level - when not given,  $g = 1.0$ .

Material Nos. 2 through 30

3GFAC,	$N =$					
--------	-------	--	--	--	--	--

3GFAC,	$(N + 5)$					
--------	-----------	--	--	--	--	--

3GFAC,	$(N + 10)$					
--------	------------	--	--	--	--	--

3GFAC,	$(N + 15)$					
--------	------------	--	--	--	--	--

3GFAC,	$(N + 20)$					
--------	------------	--	--	--	--	--

\*  $N = 25 \times (\text{Material Number} - 1)$ .

Composition Geometry\*

Geometry for Volume Calculation

3GVØL,			
	$X, H, \text{ or } R$	$Y \text{ or } OD$	$Z \text{ or } ID$

Geometry for Size Correction to the Diffusion Coefficient

3GDIFC,			
	$X + 2S$	$Y + 2S$	$Z + 2S$
	$H + 2S$	$D + 2S$	
	$R + S$		

Geometry for Behrens' Correction

3GBEHR,				
	$D_1 \text{ or } l_{\text{fuel}}$	$D_2 \text{ or } l_{\text{moderator}}$	$D_3 \text{ or } VF_{\text{fuel}}$	$Q$

Geometry for Transmission Calculation

3GTRAN,			
	$D_0$	$D_{ch}$	$\epsilon$

Fuel Region Thickness (for resonance self shielding calculation)

3FT,		This card is given in NCØDE(5) = 2
------	--	------------------------------------

\* NOTE: All dimensions are given in centimeters.

Spatial Self-Shielding Factors\*

Material No. 1

3ELFAC,						
---------	--	--	--	--	--	--

3ELFAC,	5 =					
---------	-----	--	--	--	--	--

3ELFAC,	10 =					
---------	------	--	--	--	--	--

3ELFAC,	15 =					
---------	------	--	--	--	--	--

3ELFAC,	20 =					
---------	------	--	--	--	--	--

\* This table may be extended to provide spatial self-shielding factors at each resonance energy for this material. When not given, ELFAC = 1.0.

Material Nos. 2 through 20

N\*

3ELFAC,	=					
---------	---	--	--	--	--	--

(N + 5)

3ELFAC,	=					
---------	---	--	--	--	--	--

(N + 10)

3ELFAC,	=					
---------	---	--	--	--	--	--

(N + 15)

3ELFAC,	=					
---------	---	--	--	--	--	--

(N + 20)

3ELFAC,	=					
---------	---	--	--	--	--	--

\*N = (Material Number 1) × NCØDE(6).

Control Input

	#1	#2	#3	#4	#5	#6
4NCØDE,						
→ MØRE,						

Calculation CodesNCØDE

- #1 - Type Geometry
  - 0 - Slab
  - 1 - Cylinder
  - 2 - Sphere
- #2 - Behrens' Calculation
  - 0 - No
  - 1 - Isotropic
  - 2 - Anisotropic
- #3 - Transmission Calculation
  - 0 - No
  - 1 - Yes
- #4 - Gamma Source Calculation
  - 0 - No
  - 1 - Yes
- #5 - Resonance Calculation
  - 0 - No
  - 1 - Homogeneous
  - 2 - Inhomogeneous (calculate slab geometry spatial self-shielding factors)
  - 3 - Inhomogeneous (spatial self-shielding factors given as input)
- #6 - Maximum Number of Self-Shielding Factors Given for Any One Material  
(enter only if NCØDE(5) = 3)
- #7 - Type Output
  - 0 - Normal
  - 1 - Long
  - 2 - Short

MØRE

- 0 - There are no more cases to be processed
- 1 - The next case is a composition reference case
- +1 - The next case is a composition change case
- 2 - The next case is a regional reference case
- +2 - The next case is a regional change case

Regional Data Preparation Input

Regional Case Identification - 12 BCD Characters

2CASEID,2,	①
------------	---

Composition Table\*

First Composition Name - 12 BCD Characters

5C/MP,2,	①
----------	---

Second Composition Name - 12 BCD Characters

E23437,2,	①
-----------	---

Third Composition Name - 12 BCD Characters

E23435,2,	①
-----------	---

Fourth Composition Name - 12 BCD Characters

E23433,2,	①
-----------	---

Fifth Composition Name - 12 BCD Characters

E23431,2,	①
-----------	---

Sixth Composition Name - 12 BCD Characters

E23429,2,	①
-----------	---

Seventh Composition Name - 12 BCD Characters

E23427,2,	①
-----------	---

\* NOTE: Mixable compositions (if any) must be listed first. This table may be extended to include 20 compositions, the absolute address decreasing by 2 for each additional composition.

Region Input

First Region

Composition Name - 12 BCD Characters\*

5REG,2,	①
---------	---

$R_0$	Outer Radius Region 1	No. of Intervals**	Equiv. Perpendicular Dimension
3R,	,	EN,	HE,

Enter "NMIX" Effective Composition Volume Fractions if this is a Mixable Region

3EFFV,	,	,	,	,	,
--------	---	---	---	---	---

Second Region

Composition Name - 12 BCD Characters

E23397,2,	①
-----------	---

$R_0$	Outer Radius Region 2	No. of Intervals	Equiv. Perpendicular Dimension
3R,	2 =,	EN, =,	HE, =,

$N^\dagger$  Enter "NMIX" Composition Volume Fractions if this is a Mixable Region

3EFFV,	=,	,	,	,	,
--------	----	---	---	---	---

\* To define this region as a mixable region, enter the first 6 BCD characters as ① MIX ②.

\*\* A negative number of intervals is given in those regions over which the power is to be integrated to obtain the "CORE" power.

$\dagger N = NMIX \times (\text{Mixable Region Number} - 1).$

Region Input (continued)\*

Third Region

Composition Name - 12 BCD Characters

E23395,2, ①

Outer Radius Region 3		No. of Intervals		Equiv. Perpendicular Dimension	
3R,	3=,	EN,	2=,	HE,	2=,

N Enter "NMIX" Composition Volume Fractions if this is a Mixable Region

3EFFV,	=,	,	,	,	,
--------	----	---	---	---	---

Fourth Region

Composition Name - 12 BCD Characters

E23393,2, ①

Outer Radius Region 4		No. of Intervals		Equiv. Perpendicular Dimension	
3R,	4=,	EN,	3=,	HE,	3=,

N Enter "NMIX" Composition Volume Fractions if this is a Mixable Region

3EFFV,	=,	,	,	,	,
--------	----	---	---	---	---

\* This table may be extended to include a maximum of 100 regions and 150 lattice points. The absolute address decreases by 2 for each additional region composition name.



## FISSION SOURCE DISTRIBUTION\*\*

$F_n^+$  - Fission Source on the Right at nth Lattice Point\*

	$F_1^+$	$F_2^+$	$F_3^+$	$F_4^+$	$F_5^+$	$F_6^+$
3FP,=,						
	$F_7^+$	$F_8^+$	$F_9^+$	$F_{10}^+$	$F_{11}^+$	$F_{12}^+$
①						
	$F_{14}^+$	$F_{15}^+$	$F_{16}^+$	$F_{17}^+$	$F_{18}^+$	$F_{19}^+$
①						

This table may be extended to provide a fission source on the right at each lattice point.

\*The numerical solution technique employed does not allow for sources on external boundaries.  $F_1$  refers to the source at a point interted by the program just inside the left boundary.

$F_n^-$  - Fission Source on the Left at nth Lattice Point\*

	$F_1^-$	$F_2^-$	$F_3^-$	$F_4^-$	$F_5^-$	$F_6^-$
3FM,=,						
	$F_7^-$	$F_8^-$	$F_9^-$	$F_{10}^-$	$F_{11}^-$	$F_{12}^-$
①						
	$F_{14}^-$	$F_{15}^-$	$F_{16}^-$	$F_{17}^-$	$F_{18}^-$	$F_{19}^-$
①						

This table may be extended to provide a fission source on the left at each lattice point.

\*\*To use this table to provide a source guess, both  $F^+$  and  $F^-$  must be given at all points of interest. The program initializes  $F^+$  and  $F^-$  to 1 at every lattice point and any input values are superimposed on this initialization.

Control InputAlbedo on the Left

	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>4</sub>	...	A <sub>25</sub>
3ALFT,						

Albedo on the Right

	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>4</sub>	...	A <sub>25</sub>
3ARGT,						

Convergence Criterion

$$|K^P - K^{P-1}| < \epsilon$$

3EPSK,		If not given $\epsilon = 1.0 \times 10^{-7}$
--------	--	---

Maximum Number of Iterations

4LMAX,		If not given LMAX = 100
--------	--	----------------------------

Number of Mixable Compositions

4NMIX,	
--------	--

	#1	#2	#3	#4	#5	#6
4NCODE,						

→ MORE,	
---------	--

Calculation CodesNCODE

- |                        |                           |
|------------------------|---------------------------|
| #1 - Number of Regions | #4 - Not Operative        |
| #2 - Type Flux         | #5 - Gradient Calculation |
| 0 - Direct             | 0 - No                    |
| 1 - Adjoint            | 1 - Yes                   |
| 2 - Adjoint and Direct |                           |
| #3 - Type Geometry     | #6 - Type Output          |
| 0 - Slab               | 0 - Normal                |
| 1 - Cylinder           | 1 - Short                 |

MORE

- 0 - There are no more cases to be processed.
- 2 - The next case is a regional reference case.
- +2 - The next case is a regional change case.

## 6.0 PROGRAMMING AND OPERATING INSTRUCTIONS

Program ODD is designed to be run on an IBM 7090 using the FORTRAN monitor system and is presently written as five "chain" program blocks. The tape assignments given below could be easily modified if desired.

<u>TAPE UNIT</u>	<u>TAPE UNIT</u>
A-1 System	B-1 Utility
A-2 Input	B-2 Utility
A-3 Output	B-3 Composition Data Tape
A-4 Chain Tape	B-5 Utility
A-5 RNDT	

A listing of the input and output for a sample case are given in the following pages.

## INPUT - PROGRAM ODD

---

2BNAM,2,F.O.WENSTRUP

---

2BDENT,3,URANYL-F CANS

---

2RDATE,2,3/15/61

---

5CDTNAM,2,UCRL BEO-C U

---

→MORE,-1,

---

2CASEID,2, H/U 43.9

---

3SPEC,500.0,

---

3CMAT,92.235,92.238,1.10,8.16,

---

3DMAT,1.3786-3,9.6185-5,6.0521 2,3.3210-2,

---

3TMAT,68.0,68.0,68.0,68.0,

---

3GVOL,32.3,25.4,0.0,

---

3GDIFC,32.3,25.4,

---

4NCODE,1,0,0,0,0,0,1,

---

→MORF,-1,

---

2CASEID,2, H/U 62.7

---

3SPEC,500.0,

---

3CMAT,92.235,92.238,1.10,8.16,

---

3DMAT,1.0147-3,7.0796-5,6.3622 2,3.3982-2,

---

3TMAT,68.0,68.0,68.0,68.0,

---

3GVOL,31.7,25.4,0.0,

---

3GDIFC,31.7,25.4,

---

4NCODE,1,0,0,0,0,0,1,

---

→MORE,-2,

---

2CASEID,2, H32.3-D25.4

---

5COMP,2, H/U 43.9

---

5RFG,2, H/U 43.9

---

3R,0.0,16.15,EN,-20,HE,25.4,

---

3ALFT,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,

---

1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,1.0,

---

3ARGT,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,

---

0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,0.0,

---

3EPSK,1.0-5,

---

4NMIX,0,

---

4NCODE,1,0,0,0,0,0,

---

→MORE,0,

---

-----  
OUTPUT - PROGRAM ODD  
-----

4-766

F.D.WENSTRUP

ODD

PUT RNDI 207 ON A-5

-----  
CHARGE 54323, SEQUENCE 4-766, CHANNELS , TAPES , MODE 1, UNIT 4314  
DATE 05/13/61, PROG. NO. 657, BG. 4315, START 14.30 STOP  
-----  
START TIME AFTER INSTRUCTIONS ON 1 STOP COMMENT CARD FOLLOWED 14.300

```
-----  
$      XEQ  
$      CHAIN(L,B1)  
-----
```

-----  
 IN PROGRAM RNDT4 ,THERE WAS A  
 CHECKSUM ERROR, CARD ORIGIN 000426  
 -----

\$ CHAIN(2,B1)

EXIT	30474	(TES)	30472	CHAIN	30236	COS	30070
SIN	30074	SOFT	30031	LOG	27740	F3COMP	27523
E3	27142	EXP	27046	BESJ	25212	BESI	25216
BESK	25222	BESY	25226	BSF	25064	FSFBT	25066
FSFDI	25066	MOVE	24752	(EFT)	24741	(STB)	24663
(WLR)	24705	(TSB)	24620	(RLR)	24641	(BST)	24565
(WER)	24507	(WTC)	24541	(RWT)	24471	(RER)	24437
(RDC)	24462	(SPH)	24145	NOPAGE	23603	ANPIPM	23637
(STH)	24054	(STHM)	24057	RESTC	23542	LINES	23552
PAGES	23544	NEWSET	23557	HDING	23566	NOHEAD	23605
COLUMN	23575	BOTTOM	23612	WOT	22556	ERROR	22330
ERRORA	22327	(DIP)	21111	(IOB)	20422	(EXB)	20474
(IOH)	16620	(FIL)	20230	(RTN)	20241	(IOU)	16602
(TRC)	16541	(IOS)	16453	(RDS)	16530	(WRS)	16531
(BSR)	16532	(WEF)	16533	(REW)	16534	(ETT)	16535
(RCH)	16536	(TEF)	16537	(TCO)	16540	(FPT)	16427
RSS	16000	PSI	14371	ERRCDP	14210	ENDCDP	14026
WOTCD	11566	WTCO	11400	GRPAR	11030	PLATE	10741
ANULUS	10601	ROD	10271	BEHR	07524	HETRES	07225
HOMRES	07115	MIX	05617	NANDW	05464	THERM	04774
AUXND	03012	RNDT4	02344	RNDT3	01730	RNDT2	01404
RNDT1	01205	CID	01017	START	00475	00000	00174



\$ CHAIN(3,B1)							
EXIT	12753	CHAIN	12516	(WER)	12445	(WTC)	12477
(TES)	12433	(TSB)	12377	(RLR)	12420	(RWT)	12364
(RER)	12332	(RDC)	12355	(SPH)	12040	NOPAGE	11476
ANPIPM	11532	(STH)	11747	(STHM)	11752	RESTO	11435
LINES	11445	PAGES	11437	NEWSSET	11452	HDING	11461
NOHEAD	11500	COLUMN	11470	BOTTOM	11505	WOT	10451
ERROR	10223	EBRORA	10222	(DIP)	07004	(IOB)	06315
(EXB)	06367	(IOH)	04513	(FIL)	06123	(RTN)	06134
(IOU)	04475	(TRC)	04434	(IOS)	04346	(RDS)	04423
(WRS)	04424	(BSR)	04425	(WEF)	04426	(REW)	04427
(ETT)	04430	(RCH)	04431	(TEF)	04432	(TCO)	04433
(FPT)	04322	POMIX	03604	PCKDT	03147	REGCK	02740
000000	00163						

\$ CHAIN(4,B1)							
EXIT	11025	CHAIN	10570	(TES)	10565	(WER)	10516
(WTC)	10550	NOPAGE	10147	ANPIPM	10203	(STH)	10420
(STHM)	10423	RESTO	10106	LINES	10116	PAGES	10110
NEWSET	10123	HDING	10132	NOHEAD	10151	COLUMN	10141
BOTTOM	10156	ERROR	07040	ERRORA	07037	(IOH)	05226
(FIL)	06636	(RTN)	06647	(IOU)	05210	(TRC)	05147
(IOS)	05061	(BDS)	05136	(WRS)	05137	(BSR)	05140
(WEF)	05141	(REW)	05142	(ETT)	05143	(RCH)	05144
(TEF)	05145	(TCO)	05146	(FPT)	05035	TMIX	04305
RPAR	03674	RANDC	03545	HOMRC	02304	MATINV	01553
GCOE	00231	000000	00152				

-----				
\$	CHAIN(5,B1)			
EXIT	07477	(IES)	07475	CHAIN 07241 (FPT) 07215
STINT	07117	CTINT	07010	TMIX 06254 RPAR 05643
PMIX	05372	TSPAR	05100	SPAR 04343 POWER 03664
SORRC	00664	000000	00155	

\$ DATA EXECUTION							
EXIT	15256	CHAIN	15021	(TES)	15016	(WER)	14747
(WTC)	15001	(STB)	14662	(WLR)	14704	(RWT)	14646
(EFT)	14637	(SPH)	14351	NOPAGE	14007	ANPIPM	14043
(STH)	14260	(STHM)	14263	RESTO	13746	LINES	13756
PAGES	13750	NEWSET	13763	HDING	13772	NOHEAD	14011
COLUMN	14001	BOTTOM	14016	WOT	12762	(IOB)	12272
(EXB)	12344	(IOH)	10470	(FIL)	12100	(RTN)	12111
(IOU)	10452	(TRC)	10411	(IOS)	10323	(RDS)	10400
(WRS)	10401	(BSR)	10402	(WEF)	10403	(REW)	10404
(ETT)	10405	(RCH)	10406	(TEF)	10407	(TCO)	10410
(FPT)	10277	STINT	10201	CTINT	10072	TMIX	07336
TSPAR	07044	SPAR	06307	RPAR	05676	GPHI	02073
PREP	01242	000000	00163				

H/U 43.9 F.D.WENSTRUP URANYL-F CANS

COMPOSITION DATA PREPARATION

CALCULATION REQUEST SUMMARY

GEOMETRY - CYLINDER

H = 3.23000E 01 OD = 2.54000E 01 ID = 0.

NO BEHRENS CALCULATION

NO TRANSMISSION CALCULATION

NO GAMMA SOURCE CALCULATION

NO RESONANCE SELF-SHIELDING CALCULATION

GEOMETRY FOR SIZE CORRECTION TO THE DIFFUSION COEFFICIENT

H+2S = 3.23000E 01 D+2S = 2.54000E 01

COMPOSITION VOLUME IN CC - 1.636665E 04

COMPOSITION SPECTRUM CODE NO. - 500.0000

MATERIAL CODE NO.	MATERIAL WEIGHT	DENSITY OR VOLUME FRACTION	MATERIAL TEMP	BEHRENS REGION NO.
92.2350	8.805351E 03	1.378600E-03	68.00	0
92.2380	6.222101E 02	9.618500E-05	68.00	0
1.1000	1.657261E 03	6.052100E-02	68.00	0
8.1600	1.443849E 04	3.321000E-02	68.00	0

H/U 43.9 F.D. WENSTRUP URANYL-F CANS

MATERIAL CELL CORRECTIONS

CODE NO.	CODE NO.	CODE NO.	CODE NO.	CODE NO.
92.2350	92.2380	1.1000	8.1600	0.

GROUP	G-FACTOR	G-FACTOR	G-FACTOR	G-FACTOR	G-FACTOR
1	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
2	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
3	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
4	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
5	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
6	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
7	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
8	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
9	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
10	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
11	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
12	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
13	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
14	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
15	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
16	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
17	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
18	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
19	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
20	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
21	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
22	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
23	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
24	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
25	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00

H/U 43.9

F.D.WENSTRUP

URANYL-F CANS

GROUP	ENERGY	DELTA(U)	1/V-FACTORS
1	1.28403E 07	0.50000E-00	5.04280E-05
2	7.78801E 06	0.50000E-00	6.47508E-05
3	4.72367E 06	0.50000E 00	8.31417E-05
4	2.86505E 06	0.50000E-00	1.06756E-04
5	1.73774E 06	0.50000E 00	1.37078E-04
6	1.05399E 06	0.50000E-00	1.76011E-04
7	6.39279E 05	0.50000E-00	2.26003E-04
8	3.87742E 05	0.50000E-00	2.90193E-04
9	2.35177E 05	0.75000E 00	3.97938E-04
10	1.11090E 05	0.10000E 01	6.12145E-04
11	4.08677E 04	1.00000E 00	1.02080E-03
12	1.50344E 04	1.00000E 00	1.68301E-03
13	5.53084E 03	1.00000E 00	2.77481E-03
14	2.03468E 03	1.00000E 00	4.57489E-03
15	7.48518E 02	0.13250E 01	8.24544E-03
16	1.98958E 02	0.12750E 01	1.57732E-02
17	5.55951E 01	0.95000E 00	2.73051E-02
18	2.15009E 01	0.97500E 00	4.42043E-02
19	8.10998E 00	0.11000E 01	7.44599E-02
20	2.69958E 00	1.00000E 00	1.25598E-01
21	9.93119E-01	0.87500E 00	2.00217E-01
22	4.13994E-01	1.00000E 00	3.20725E-01
23	1.52300E-01	0.11475E 01	5.50453E-01
24	4.83444E-02	0.64750E 00	8.54416E-01
25	2.53012E-02	0.	

HZU 43.9 F.D.WENSTRUP URANYL-F CANS

COMPOSITION CROSS SECTIONS

GROUP	DIFFUSION	SCATTER	TRANSPORT	ABSORPTION	EXTRAPOLATION
1	3.60162E 00	1.00311E-01	4.72123E-02	1.10046E-02	1.22044E 01
2	3.15268E 00	1.35316E-01	6.64681E-02	7.51575E-03	9.60344E 00
3	2.52505E 00	2.03631E-01	1.02086E-01	2.73757E-03	6.77808E 00
4	2.58202E 00	2.18315E-01	1.02007E-01	2.01356E-03	6.83038E 00
5	1.77691E 00	3.12930E-01	1.63264E-01	1.97172E-03	4.29991E 00
6	1.33978E 00	4.30918E-01	2.28479E-01	1.87911E-03	3.08432E 00
7	1.04922E 00	6.05835E-01	3.01468E-01	1.99963E-03	2.34127E 00
8	1.06129E 00	6.14190E-01	2.97898E-01	2.20649E-03	2.36751E 00
9	7.62075E-01	7.62692E-01	3.32337E-01	2.57028E-03	2.12148E 00
10	7.88076E-01	9.90150E-01	4.10431E-01	3.17925E-03	1.71780E 00
11	6.82448E-01	1.18173E 00	4.75210E-01	5.15264E-03	1.47909E 00
12	6.27363E-01	1.29340E 00	5.16540E-01	7.29688E-03	1.35634E 00
13	6.02984E-01	1.34165E 00	5.35334E-01	1.02165E-02	1.30235E 00
14	5.91190E-01	1.35417E 00	5.41412E-01	1.52348E-02	1.27639E 00
15	5.71209E-01	1.35661E 00	5.43895E-01	3.25353E-02	1.23259E 00
16	5.45812E-01	1.36358E 00	5.50943E-01	5.27245E-02	1.17697E 00
17	4.91141E-01	1.37851E 00	5.65984E-01	1.05876E-01	1.05751E 00
18	4.71039E-01	1.35501E 00	5.42163E-01	1.58754E-01	1.01367E 00
19	5.36322E-01	1.37063E 00	5.45393E-01	6.91760E-02	1.15609E 00
20	5.33938E-01	1.39995E 00	5.56170E-01	6.12710E-02	1.15072E 00
21	4.48030E-01	1.39701E 00	6.23888E-01	1.13308E-01	9.63787E-01
22	3.21576E-01	1.43967E 00	7.36959E-01	2.93442E-01	6.89537E-01
23	2.27863E-01	1.57053E 00	9.91251E-01	4.66227E-01	4.87486E-01
24	1.57444E-01	1.81354E 00	1.31218E 00	8.00685E-01	3.36274E-01
25	1.42079E-01	2.45675E 00	9.17502E-01	1.42571E 00	3.03216E-01



H/U 43.9 F.D.WENSTRUP URANYL-F CANS

## COMPOSITION GROUP PARAMETERS

GROUP	DIFFUSION RADIAL	DIFFUSION LONGITUDINAL	REMOVAL (ABSP+SCAT)	FISSION	SOURCE
1	3.60162E 00	3.60162E 00	7.82298E-02	1.00015E-02	6.02440E-03
2	3.15268E 00	3.15268E 00	8.99118E-02	6.49052E-03	5.61236E-02
3	2.52505E 00	2.52505E 00	1.16516E-01	5.17266E-03	1.63906E-01
4	2.58202E 00	2.58202E 00	1.47959E-01	5.17609E-03	2.31561E-01
5	1.77691E 00	1.77691E 00	2.01002E-01	4.75155E-03	2.10909E-01
6	1.33978E 00	1.33978E 00	2.71337E-01	4.34236E-03	1.47657E-01
7	1.04922E 00	1.04922E 00	3.52373E-01	4.35245E-03	8.81369E-02
8	1.06129E 00	1.06129E 00	4.20239E-01	4.78751E-03	4.77978E-02
9	9.62075E-01	9.62075E-01	4.69241E-01	5.53517E-03	3.16200E-02
10	7.88076E-01	7.88076E-01	5.61889E-01	7.26133E-03	1.25488E-02
11	6.82448E-01	6.82448E-01	6.84003E-01	9.85706E-03	2.88050E-03
12	6.27363E-01	6.27363E-01	7.53355E-01	1.34878E-02	6.48500E-04
13	6.02984E-01	6.02984E-01	7.84531E-01	1.82338E-02	1.45100E-04
14	5.91190E-01	5.91190E-01	7.95716E-01	2.61328E-02	3.24000E-05
15	5.71209E-01	5.71209E-01	7.14795E-01	5.34903E-02	7.95000E-06
16	5.45812E-01	5.45812E-01	7.48766E-01	8.09990E-02	1.02000E-06
17	4.91141E-01	4.91141E-01	9.03333E-01	1.61183E-01	9.50000E-08
18	4.71039E-01	4.71039E-01	9.47776E-01	2.31836E-01	0.
19	5.36322E-01	5.36322E-01	8.28550E-01	5.74768E-02	0.
20	5.33938E-01	5.33938E-01	8.71232E-01	1.08649E-01	0.
21	4.48030E-01	4.48030E-01	1.45643E 00	2.29546E-01	0.
22	3.21576E-01	3.21576E-01	1.02928E 00	5.82001E-01	0.
23	2.27863E-01	2.27863E-01	1.10060E 00	9.59469E-01	0.
24	1.57444E-01	1.57444E-01	1.90553E 00	1.62850E 00	0.
25	1.42079E-01	1.42079E-01	2.52952E 00	2.88837E 00	0.

H/U 43.9

F.D. WENSTRUP

URANYL-F CANS

## COMPOSITION SCATTER TRANSFER MATRIX

FROM	TO	1	2	3	4	5
1	0.		2.55239E-02	1.64232E-02	1.06366E-02	6.41333E-03
2	0.		0.	3.72629E-02	1.64852E-02	1.07438E-02
3	0.		0.	0.	5.31826E-02	2.33545E-02
4	0.		0.	0.	0.	6.52125E-02
5	0.		0.	0.	0.	0.
6	0.		0.	0.	0.	0.
7	0.		0.	0.	0.	0.
8	0.		0.	0.	0.	0.
9	0.		0.	0.	0.	0.
10	0.		0.	0.	0.	0.
11	0.		0.	0.	0.	0.
12	0.		0.	0.	0.	0.
13	0.		0.	0.	0.	0.
14	0.		0.	0.	0.	0.
15	0.		0.	0.	0.	0.
16	0.		0.	0.	0.	0.
17	0.		0.	0.	0.	0.
18	0.		0.	0.	0.	0.
19	0.		0.	0.	0.	0.
20	0.		0.	0.	0.	0.
21	0.		0.	0.	0.	0.
22	0.		0.	0.	0.	0.
23	0.		0.	0.	0.	0.
24	0.		0.	0.	0.	0.
25	0.		0.	0.	0.	0.

H/U 43.9

F.D.WENSTRUP

URANYL-F CANS

## COMPOSITION SCATTER TRANSFER MATRIX

FROM	TO	6	7	8	9	10
1	3.46500E-03	1.98663E-03	1.15359E-03	8.84117E-04	4.73704E-04	
2	7.27088E-03	4.42036E-03	2.59008E-03	1.97719E-03	1.05374E-03	
3	1.45997E-02	9.01956E-03	5.46511E-03	4.37225E-03	2.41216E-03	
4	3.15499E-02	1.94064E-02	1.18232E-02	9.55766E-03	5.33427E-03	
5	9.48208E-02	4.09636E-02	2.49704E-02	2.02895E-02	1.14040E-02	
6	0.	1.31074E-01	5.44909E-02	4.43639E-02	2.50322E-02	
7	0.	0.	1.70749E-01	9.48864E-02	5.36323E-02	
8	0.	0.	0.	2.39260E-01	1.13104E-01	
9	0.	0.	0.	0.	3.02024E-01	
10	0.	0.	0.	0.	0.	
11	0.	0.	0.	0.	0.	
12	0.	0.	0.	0.	0.	
13	0.	0.	0.	0.	0.	
14	0.	0.	0.	0.	0.	
15	0.	0.	0.	0.	0.	
16	0.	0.	0.	0.	0.	
17	0.	0.	0.	0.	0.	
18	0.	0.	0.	0.	0.	
19	0.	0.	0.	0.	0.	
20	0.	0.	0.	0.	0.	
21	0.	0.	0.	0.	0.	
22	0.	0.	0.	0.	0.	
23	0.	0.	0.	0.	0.	
24	0.	0.	0.	0.	0.	
25	0.	0.	0.	0.	0.	

H/U 43.9 F.D. WENSTRUP URANYL-F CANS

COMPOSITION SCATTER TRANSFER MATRIX

FROM	TO 11	12	13	14	15
1	1.68677E-04	6.11985E-05	2.23950E-05	8.22177E-06	3.51036E-06
2	3.76255E-04	1.36707E-04	5.00518E-05	1.83788E-05	7.84353E-06
3	8.70718E-04	3.17593E-04	1.16448E-04	4.27832E-05	1.82718E-05
4	1.93962E-03	7.09627E-04	2.60489E-04	9.57466E-05	4.08980E-05
5	4.16660E-03	1.52752E-03	5.61159E-04	2.06325E-04	8.81413E-05
6	9.17257E-03	3.36708E-03	1.23756E-03	4.55108E-04	1.94435E-04
7	1.96767E-02	7.22648E-03	2.65653E-03	9.76995E-04	4.17409E-04
8	4.15342E-02	1.52595E-02	5.61030E-03	2.06340E-03	8.81579E-04
9	1.04117E-01	3.82690E-02	1.40722E-02	5.17592E-03	2.21144E-03
10	3.58430E-01	1.26607E-01	4.65709E-02	1.71317E-02	7.31997E-03
11	0.	4.34252E-01	1.54616E-01	5.68800E-02	2.43040E-02
12	0.	0.	4.77045E-01	1.70049E-01	7.26594E-02
13	0.	0.	0.	4.95097E-01	2.05001E-01
14	0.	0.	0.	0.	5.77123E-01
15	0.	0.	0.	0.	0.
16	0.	0.	0.	0.	0.
17	0.	0.	0.	0.	0.
18	0.	0.	0.	0.	0.
19	0.	0.	0.	0.	0.
20	0.	0.	0.	0.	0.
21	0.	0.	0.	0.	0.
22	0.	0.	0.	0.	0.
23	0.	0.	0.	0.	0.
24	0.	0.	0.	0.	0.
25	0.	0.	0.	0.	0.

H/U 43.9

F.D.WENSTRUP

URANYL-F CANS

## COMPOSITION SCATTER TRANSFER MATRIX

FROM	T0	16	17	18	19	20
1	9.15487E-07	2.17692E-07	8.55015E-08	3.45456E-08	1.08958E-08	
2	2.04397E-06	4.86039E-07	1.90898E-07	7.71294E-08	2.43269E-08	
3	4.76568E-06	1.13327E-06	4.45108E-07	1.79839E-07	5.67219E-08	
4	1.06678E-05	2.53685E-06	9.96380E-07	4.02572E-07	1.26973E-07	
5	2.29916E-05	5.46761E-06	2.14747E-06	8.67653E-07	2.73661E-07	
6	5.07194E-05	1.20617E-05	4.73738E-06	1.91407E-06	6.03703E-07	
7	1.08885E-04	2.58941E-05	1.01703E-05	4.10914E-06	1.29603E-06	
8	2.29969E-04	5.46896E-05	2.14801E-05	8.67869E-06	2.73729E-06	
9	5.76880E-04	1.37190E-04	5.38832E-05	2.17707E-05	6.86655E-06	
10	1.90954E-03	4.54120E-04	1.78361E-04	7.20642E-05	2.27293E-05	
11	6.34017E-03	1.50780E-03	5.92207E-04	2.39272E-04	7.54673E-05	
12	1.89546E-02	4.50773E-03	1.77047E-03	7.15330E-04	2.25618E-04	
13	5.34784E-02	1.27181E-02	4.99518E-03	2.01823E-03	6.36555E-04	
14	1.46534E-01	3.48483E-02	1.36871E-02	5.53006E-03	1.74420E-03	
15	4.94869E-01	1.14919E-01	4.51359E-02	1.82365E-02	5.75184E-03	
16	0.	4.31552E-01	1.64726E-01	6.65550E-02	2.09917E-02	
17	0.	0.	5.02864E-01	1.96531E-01	6.19867E-02	
18	0.	0.	0.	5.31642E-01	1.62695E-01	
19	0.	0.	0.	0.	4.85162E-01	
20	0.	0.	0.	0.	0.	
21	0.	0.	0.	0.	0.	
22	0.	0.	0.	0.	0.	
23	0.	0.	0.	0.	0.	
24	0.	0.	0.	0.	0.	
25	0.	0.	0.	0.	0.	

H/U 43.9 F.D.WENSTRUP URANYL-F CANS

COMPOSITION SCATTER TRANSFER MATRIX

FROM	T0	21	22	23	24	25
1	3.69773E-09	1.67092E-09	6.63758E-10	0.	0.	0.
2	8.25588E-09	3.73065E-09	1.48196E-09	0.	0.	0.
3	1.92498E-08	8.69857E-09	3.45542E-09	7.65946E-10	8.40998E-10	8.40998E-10
4	4.30910E-08	1.94719E-08	7.73501E-09	1.71458E-09	1.88259E-09	1.88259E-09
5	9.28730E-08	4.19672E-08	1.66711E-08	3.69539E-09	4.05749E-09	4.05749E-09
6	2.04880E-07	9.25808E-08	3.67768E-08	8.15213E-09	8.95093E-09	8.95093E-09
7	4.39839E-07	1.98753E-07	7.89528E-08	1.75011E-08	1.92159E-08	1.92159E-08
8	9.28960E-07	4.19776E-07	1.66752E-07	3.69631E-08	4.05850E-08	4.05850E-08
9	2.33032E-06	1.05302E-06	4.18301E-07	9.27227E-08	1.01808E-07	1.01808E-07
10	7.71370E-06	3.48565E-06	1.38464E-06	3.06926E-07	3.37001E-07	3.37001E-07
11	2.56115E-05	1.15733E-05	4.59737E-06	1.01908E-06	1.11893E-06	1.11893E-06
12	7.65684E-05	3.45996E-05	1.37443E-05	3.04664E-06	3.34517E-06	3.34517E-06
13	2.16029E-04	9.76189E-05	3.87782E-05	8.59575E-06	9.43802E-06	9.43802E-06
14	5.91934E-04	2.67482E-04	1.06255E-04	2.35529E-05	2.58608E-05	2.58608E-05
15	1.95202E-03	8.82074E-04	3.50395E-04	7.76703E-05	8.52809E-05	8.52809E-05
16	7.12400E-03	3.21918E-03	1.27879E-03	2.83462E-04	3.11237E-04	3.11237E-04
17	2.10366E-02	9.50596E-03	3.77615E-03	8.37040E-04	9.19058E-04	9.19058E-04
18	5.52144E-02	2.49501E-02	9.91120E-03	2.19696E-03	2.41224E-03	2.41224E-03
19	1.59203E-01	7.22568E-02	2.87033E-02	6.36251E-03	6.98595E-03	6.98595E-03
20	4.78738E-01	2.09372E-01	8.31712E-02	1.84361E-02	2.02426E-02	2.02426E-02
21	0.	1.34312E 00	2.04168E-01	4.14875E-02	3.15918E-02	3.15918E-02
22	7.83944E-03	0.	5.39276E-01	1.07142E-01	8.15823E-02	8.15823E-02
23	1.46459E-06	4.82709E-02	0.	3.41489E-01	2.44615E-01	2.44615E-01
24	2.53682E-07	8.00763E-03	5.12924E-01	0.	5.83916E-01	5.83916E-01
25	2.22090E-07	7.00911E-03	4.25485E-01	6.71316E-01	0.	0.

H/U 62.7 F.D.WENSTRUP URANYL-F CANS

COMPOSITION DATA PREPARATION

CALCULATION REQUEST SUMMARY

GEOMETRY - CYLINDER

H = 3.17000E 01 OD = 2.54000E 01 ID = 0.

NO BEHRENS CALCULATION

NO TRANSMISSION CALCULATION

NO GAMMA SOURCE CALCULATION

NO RESONANCE SELF-SHIELDING CALCULATION

GEOMETRY FOR SIZE CORRECTION TO THE DIFFUSION COEFFICIENT

H+2S = 3.17000E 01 D+2S = 2.54000E 01

COMPOSITION VOLUME IN CC - 1.606263E 04

COMPOSITION SPECTRUM CODE NO. - 500.0000

MATERIAL CODE NO.	MATERIAL WEIGHT	DENSITY OR VOLUME FRACTION	MATERIAL TEMP	BEHRENS REGION NO.
92.2350	6.360669E 03	1.014700E-03	68.00	0
92.2380	4.494643E 02	7.079600E-05	68.00	0
1.1000	1.709814E 03	6.362200E-02	68.00	0
8.1600	1.449969E 04	3.398200E-02	68.00	0

H/U 62.7 F.D.WENSTRUP URANYL-F CANS

MATERIAL CELL CORRECTIONS

CODE NO.	CODE NO.	CODE NO.	CODE NO.	CODE NO.
92.2350	92.2380	1.1000	8.1600	0.

GROUP	G-FACTOR	G-FACTOR	G-FACTOR	G-FACTOR	G-FACTOR
1	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
2	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
3	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
4	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
5	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
6	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
7	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
8	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
9	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
10	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
11	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
12	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
13	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
14	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
15	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
16	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
17	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
18	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
19	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
20	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
21	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
22	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
23	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
24	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00
25	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00	1.00000E 00



H/U 62.7 F.D.WENSTRUP URANYL-F CANS

GROUP	ENERGY	DELTA(U)	1/V-FACTORS
1	1.28403E 07	0.50000E-00	5.04280E-05
2	7.78801E 06	0.50000E-00	6.47508E-05
3	4.72367E 06	0.50000E 00	8.31417E-05
4	2.86505E 06	0.50000E-00	1.06756E-04
5	1.73774E 06	0.50000E 00	1.37078E-04
6	1.05399E 06	0.50000E-00	1.76011E-04
7	6.39279E 05	0.50000E-00	2.26003E-04
8	3.87742E 05	0.50000E-00	2.90193E-04
9	2.35177E 05	0.75000E 00	3.97938E-04
10	1.11090E 05	0.10000E 01	6.19145E-04
11	4.08677E 04	1.00000E 00	1.02080E-03
12	1.50344E 04	1.00000E 00	1.68301E-03
13	5.53084E 03	1.00000E 00	2.77481E-03
14	2.03468E 03	1.00000E 00	4.57489E-03
15	7.48518E 02	0.13250E 01	8.24544E-03
16	1.98958E 02	0.12750E 01	1.57732E-02
17	5.55951E 01	0.95000E 00	2.73051E-02
18	2.15009E 01	0.97500E 00	4.42043E-02
19	8.10998E 00	0.11000E 01	7.44599E-02
20	2.69958E 00	1.00000E 00	1.25598E-01
21	9.93119E-01	0.87500E 00	2.00217E-01
22	4.13994E-01	1.00000E 00	3.20725E-01
23	1.52300E-01	0.11475E 01	5.50453E-01
24	4.83444E-02	0.64750E 00	8.54416E-01
25	2.53012E-02	0.	

H/U 62.7 F.D. WENSTRUP URANYL-F CANS

COMPOSITION CROSS SECTIONS

GROUP	DIFFUSION	SCATTER	TRANSPORT	ABSORPTION	EXTRAPOLATION
1	3.59745E 00	1.02588E-01	4.80994E-02	1.04899E-02	1.21268E 01
2	3.13710E 00	1.38474E-01	6.76556E-02	7.09649E-03	9.50475E 00
3	2.50010E 00	2.08956E-01	1.04128E-01	2.26648E-03	6.67796E 00
4	2.55278E 00	2.25426E-01	1.04368E-01	1.48559E-03	6.71209E 00
5	1.74553E 00	3.23947E-01	1.67534E-01	1.45594E-03	4.20440E 00
6	1.31081E 00	4.46644E-01	2.34825E-01	1.38898E-03	3.00787E 00
7	1.02439E 00	6.27710E-01	3.09973E-01	1.47896E-03	2.28125E 00
8	1.03508E 00	6.38668E-01	3.06749E-01	1.63257E-03	2.30396E 00
9	9.36832E-01	7.94336E-01	3.42637E-01	1.89434E-03	2.06222E 00
10	7.66014E-01	1.03284E 00	4.23702E-01	2.34397E-03	1.66766E 00
11	6.62418E-01	1.23414E 00	4.91562E-01	3.79900E-03	1.43431E 00
12	6.08686E-01	1.35148E 00	5.34975E-01	5.38143E-03	1.31487E 00
13	5.85643E-01	1.40206E 00	5.54591E-01	7.53733E-03	1.26395E 00
14	5.76251E-01	1.41446E 00	5.60223E-01	1.12424E-02	1.24330E 00
15	5.62126E-01	1.41624E 00	5.62042E-01	2.39995E-02	1.21237E 00
16	5.43766E-01	1.42132E 00	5.67214E-01	3.89072E-02	1.17221E 00
17	5.02686E-01	1.43223E 00	5.78261E-01	7.81019E-02	1.08248E 00
18	4.86907E-01	1.41512E 00	5.60789E-01	1.17129E-01	1.04806E 00
19	5.34789E-01	1.43247E 00	5.65116E-01	5.13877E-02	1.15247E 00
20	5.30284E-01	1.46286E 00	5.76009E-01	4.58919E-02	1.14246E 00
21	4.51656E-01	1.45923E 00	6.46662E-01	8.46650E-02	9.71521E-01
22	3.36925E-01	1.50365E 00	7.65106E-01	2.18016E-01	7.22697E-01
23	2.40799E-01	1.64087E 00	1.03208E 00	3.46655E-01	5.15327E-01
24	1.69342E-01	1.89600E 00	1.36913E 00	5.94755E-01	3.61783E-01
25	1.65362E-01	2.57214E 00	9.54203E-01	1.05847E 00	3.53014E-01

H/U 62.7

F.D.WENSTRUP

URANYL-F CANS

## COMPOSITION GROUP PARAMETERS

GROUP	DIFFUSION RADIAL	DIFFUSION LONGITUDINAL	REMOVAL (ABSP+SCAT)	FISSION	SOURCE
1	3.59745E 00	3.59745E 00	7.99500E-02	7.36148E-03	6.02440E-03
2	3.13710E 00	3.13710E 00	9.23853E-02	4.77726E-03	5.61236E-02
3	2.50010E 00	2.50010E 00	1.20458E-01	3.80727E-03	1.63906E-01
4	2.55278E 00	2.55278E 00	1.53647E-01	3.80979E-03	2.31561E-01
5	1.74553E 00	1.74553E 00	2.09181E-01	3.49731E-03	2.10909E-01
6	1.31081E 00	1.31081E 00	2.82924E-01	3.19614E-03	1.47657E-01
7	1.02439E 00	1.02439E 00	3.67741E-01	3.20356E-03	8.81369E-02
8	1.03508E 00	1.03508E 00	4.39503E-01	3.52378E-03	4.77978E-02
9	9.36832E-01	9.36832E-01	4.91553E-01	4.07409E-03	3.16200E-02
10	7.66014E-01	7.66014E-01	5.89096E-01	5.34460E-03	1.25488E-02
11	6.62418E-01	6.62418E-01	7.16997E-01	7.25516E-03	2.88050E-03
12	6.08686E-01	6.08686E-01	7.89215E-01	9.92752E-03	6.48500E-04
13	5.85643E-01	5.85643E-01	8.21060E-01	1.34208E-02	1.45100E-04
14	5.76251E-01	5.76251E-01	8.31240E-01	1.92347E-02	3.24000E-05
15	5.62126E-01	5.62126E-01	7.40854E-01	3.93708E-02	7.95000E-06
16	5.43766E-01	5.43766E-01	7.70220E-01	5.96182E-02	1.02000E-06
17	5.02686E-01	5.02686E-01	9.15849E-01	1.18636E-01	9.50000E-08
18	4.86907E-01	4.86907E-01	9.46091E-01	1.70640E-01	0.
19	5.34789E-01	5.34789E-01	8.49245E-01	4.23050E-02	0.
20	5.30284E-01	5.30284E-01	8.96882E-01	7.99697E-02	0.
21	4.51656E-01	4.51656E-01	1.49582E 00	1.68954E-01	0.
22	3.36925E-01	3.36925E-01	9.90881E-01	4.28374E-01	0.
23	2.40799E-01	2.40799E-01	1.01229E 00	7.06204E-01	0.
24	1.69342E-01	1.69342E-01	1.75379E 00	1.19863E 00	0.
25	1.65362E-01	1.65362E-01	2.21742E 00	2.12594E 00	0.

H/U 62.7 F.D. WENSTRUP URANYL-F CANS

COMPOSITION SCATTER TRANSFER MATRIX

FROM	TO	1	2	3	4	5
1	0.		2.66407E-02	1.70863E-02	1.09460E-02	6.50062E-03
2	0.		0.	3.88165E-02	1.71992E-02	1.10488E-02
3	0.		0.	0.	5.53842E-02	2.43535E-02
4	0.		0.	0.	0.	6.80202E-02
5	0.		0.	0.	0.	0.
6	0.		0.	0.	0.	0.
7	0.		0.	0.	0.	0.
8	0.		0.	0.	0.	0.
9	0.		0.	0.	0.	0.
10	0.		0.	0.	0.	0.
11	0.		0.	0.	0.	0.
12	0.		0.	0.	0.	0.
13	0.		0.	0.	0.	0.
14	0.		0.	0.	0.	0.
15	0.		0.	0.	0.	0.
16	0.		0.	0.	0.	0.
17	0.		0.	0.	0.	0.
18	0.		0.	0.	0.	0.
19	0.		0.	0.	0.	0.
20	0.		0.	0.	0.	0.
21	0.		0.	0.	0.	0.
22	0.		0.	0.	0.	0.
23	0.		0.	0.	0.	0.
24	0.		0.	0.	0.	0.
25	0.		0.	0.	0.	0.

H/U 62.7

F.D.WENSTRUP

URANYL-F CANS

## COMPOSITION SCATTER TRANSFER MATRIX

FROM	TO	6	7	8	9	10
1	3.46884E-03	1.98666E-03	1.16222E-03	9.01595E-04	4.89991E-04	
2	7.38590E-03	4.47258E-03	2.62960E-03	2.02483E-03	1.09192E-03	
3	1.50909E-02	9.27411E-03	5.62096E-03	4.51822E-03	2.51117E-03	
4	3.29482E-02	2.01831E-02	1.22804E-02	9.94504E-03	5.57315E-03	
5	9.87089E-02	4.28654E-02	2.60910E-02	2.12062E-02	1.19433E-02	
6	0.	1.36442E-01	5.71198E-02	4.64906E-02	2.62551E-02	
7	0.	0.	1.77753E-01	9.95454E-02	5.62860E-02	
8	0.	0.	0.	2.50120E-01	1.18754E-01	
9	0.	0.	0.	0.	3.16640E-01	
10	0.	0.	0.	0.	0.	
11	0.	0.	0.	0.	0.	
12	0.	0.	0.	0.	0.	
13	0.	0.	0.	0.	0.	
14	0.	0.	0.	0.	0.	
15	0.	0.	0.	0.	0.	
16	0.	0.	0.	0.	0.	
17	0.	0.	0.	0.	0.	
18	0.	0.	0.	0.	0.	
19	0.	0.	0.	0.	0.	
20	0.	0.	0.	0.	0.	
21	0.	0.	0.	0.	0.	
22	0.	0.	0.	0.	0.	
23	0.	0.	0.	0.	0.	
24	0.	0.	0.	0.	0.	
25	0.	0.	0.	0.	0.	

H/U 62.7

F.D.WENSTRUP

URANYL-F CANS

## COMPOSITION SCATTER TRANSFER MATRIX

FROM	TO	11	12	13	14	15
1		1.76144E-04	6.41709E-05	2.35198E-05	8.64003E-06	3.68979E-06
2		3.93156E-04	1.43376E-04	5.25685E-05	1.93137E-05	8.24434E-06
3		9.11540E-04	3.33330E-04	1.22340E-04	4.49653E-05	1.92065E-05
4		2.03350E-03	7.45201E-04	2.73726E-04	1.00638E-04	4.29914E-05
5		4.37260E-03	1.60470E-03	5.89758E-04	2.16876E-04	9.26544E-05
6		9.63203E-03	3.53804E-03	1.30075E-03	4.78397E-04	2.04393E-04
7		2.06671E-02	7.59403E-03	2.79226E-03	1.02700E-03	4.38788E-04
8		4.36322E-02	1.60366E-02	5.89707E-03	2.16903E-03	9.26736E-04
9		1.09399E-01	4.02210E-02	1.47919E-02	5.44094E-03	2.32472E-03
10		3.76219E-01	1.33086E-01	4.89560E-02	1.80093E-02	7.69501E-03
11		0.	4.56067E-01	1.62538E-01	5.97945E-02	2.55493E-02
12		0.	0.	5.01036E-01	1.78762E-01	7.63824E-02
13		0.	0.	0.	5.19998E-01	2.15505E-01
14		0.	0.	0.	0.	6.06219E-01
15		0.	0.	0.	0.	0.
16		0.	0.	0.	0.	0.
17		0.	0.	0.	0.	0.
18		0.	0.	0.	0.	0.
19		0.	0.	0.	0.	0.
20		0.	0.	0.	0.	0.
21		0.	0.	0.	0.	0.
22		0.	0.	0.	0.	0.
23		0.	0.	0.	0.	0.
24		0.	0.	0.	0.	0.
25		0.	0.	0.	0.	0.

H/U 62.7 F.D.WENSTRUP URANYL-F CANS

COMPOSITION SCATTER TRANSFER MATRIX

FROM	T0	16	17	18	19	20
1	9.62361E-07	2.28847E-07	8.98824E-08	3.63156E-08	1.14541E-08	
2	2.14863E-06	5.10943E-07	2.00679E-07	8.10314E-08	2.55733E-08	
3	5.00975E-06	1.19134E-06	4.67915E-07	1.89054E-07	5.96282E-08	
4	1.12142E-05	2.66683E-06	1.04743E-06	4.23199E-07	1.33478E-07	
5	2.41694E-05	5.74776E-06	2.25750E-06	9.12110E-07	2.87683E-07	
6	5.33179E-05	1.26797E-05	4.98011E-06	2.01214E-06	6.34635E-07	
7	1.14463E-04	2.72209E-05	1.06914E-05	4.31968E-06	1.36244E-06	
8	2.41751E-04	5.74919E-05	2.25807E-05	9.12337E-06	2.87754E-06	
9	6.06436E-04	1.44220E-04	5.66441E-05	2.28862E-05	7.21838E-06	
10	2.00738E-03	4.77388E-04	1.87500E-04	7.57567E-05	2.38939E-05	
11	6.66503E-03	1.58506E-03	6.22551E-04	2.51532E-04	7.93341E-05	
12	1.99258E-02	4.73870E-03	1.86118E-03	7.51983E-04	2.37178E-04	
13	5.62185E-02	1.33697E-02	5.25113E-03	2.12164E-03	6.69171E-04	
14	1.54042E-01	3.66338E-02	1.43884E-02	5.81342E-03	1.83357E-03	
15	5.19862E-01	1.20807E-01	4.74486E-02	1.91709E-02	6.04656E-03	
16	0.	4.53272E-01	1.73166E-01	6.99652E-02	2.20672E-02	
17	0.	0.	5.28060E-01	2.06601E-01	6.51628E-02	
18	0.	0.	0.	5.58394E-01	1.71032E-01	
19	0.	0.	0.	0.	5.09596E-01	
20	0.	0.	0.	0.	0.	
21	0.	0.	0.	0.	0.	
22	0.	0.	0.	0.	0.	
23	0.	0.	0.	0.	0.	
24	0.	0.	0.	0.	0.	
25	0.	0.	0.	0.	0.	

H/U 62.7 F.D.WENSTRUP URANYL-F CANS

COMPOSITION SCATTER TRANSFER MATRIX

FROM	T0	21	22	23	24	25
1	3.88720E-09	1.75654E-09	6.97768E-10	0.	0.	0.
2	8.67889E-09	3.92180E-09	1.55790E-09	0.	0.	0.
3	2.02362E-08	9.14428E-09	3.63247E-09	8.05192E-10	8.84090E-10	8.84090E-10
4	4.52989E-08	2.04696E-08	8.13134E-09	1.80243E-09	1.97905E-09	1.97905E-09
5	9.76316E-08	4.41176E-08	1.75253E-08	3.88474E-09	4.26539E-09	4.26539E-09
6	2.15378E-07	9.73245E-08	3.86612E-08	8.56983E-09	9.40956E-09	9.40956E-09
7	4.62376E-07	2.08937E-07	8.29982E-08	1.83978E-08	2.02005E-08	2.02005E-08
8	9.76559E-07	4.41285E-07	1.75296E-07	3.88570E-08	4.26645E-08	4.26645E-08
9	2.44972E-06	1.10697E-06	4.39735E-07	9.74737E-08	1.07025E-07	1.07025E-07
10	8.10894E-06	3.66425E-06	1.45559E-06	3.22652E-07	3.54268E-07	3.54268E-07
11	2.69238E-05	1.21663E-05	4.83294E-06	1.07129E-06	1.17626E-06	1.17626E-06
12	8.04917E-05	3.63724E-05	1.44486E-05	3.20274E-06	3.51657E-06	3.51657E-06
13	2.27098E-04	1.02621E-04	4.07651E-05	9.03619E-06	9.92161E-06	9.92161E-06
14	6.22264E-04	2.81187E-04	1.11699E-04	2.47597E-05	2.71858E-05	2.71858E-05
15	2.05204E-03	9.27270E-04	3.68349E-04	8.16500E-05	8.96506E-05	8.96506E-05
16	7.48902E-03	3.38412E-03	1.34431E-03	2.97986E-04	3.27185E-04	3.27185E-04
17	2.21145E-02	9.99303E-03	3.96963E-03	8.79928E-04	9.66149E-04	9.66149E-04
18	5.80435E-02	2.62285E-02	1.04190E-02	2.30953E-03	2.53584E-03	2.53584E-03
19	1.68097E-01	7.59591E-02	3.01740E-02	6.68852E-03	7.34390E-03	7.34390E-03
20	5.02796E-01	2.20100E-01	8.74327E-02	1.93808E-02	2.12798E-02	2.12798E-02
21	0.	1.41115E 00	2.14630E-01	4.36132E-02	3.32105E-02	3.32105E-02
22	8.08653E-03	0.	5.66384E-01	1.12632E-01	8.57624E-02	8.57624E-02
23	1.53964E-06	5.06579E-02	0.	3.57889E-01	2.57089E-01	2.57089E-01
24	2.66681E-07	8.41789E-03	5.37966E-01	0.	6.12646E-01	6.12646E-01
25	2.33470E-07	7.36824E-03	4.47201E-01	7.04384E-01	0.	0.



CRL BEQ-C-U F.D.WENSTRUP URANYL-F CANS

INDEX RECORD

COMPOSITION DATA TAPE UCRL BEQ-C-U

2 COMPOSITIONS

5 RECORDS

DESIGNATION

RECORD NO.

H/U 43.9

1

H/U 62.7

3

H32.3-D25.4

F.D.WENSTRUP

URANYL-F CANS

## CALCULATION SUMMARY

NUMBER OF GROUPS = 25

NUMBER OF REGIONS = 1

TOTAL NUMBER OF INTERVALS = 20

NUMBER OF COMPOSITIONS = 1

MAXIMUM NUMBER OF ITERATIONS = 99

CONVERGENCE FACTOR = 9.9999999E-06

## DIRECT FLUX CALCULATION

## SLAB GEOMETRY

LEFT-HAND BOUNDARY 0.

RIGHT-HAND BOUNDARY 1.6150000E 01

GROUP	LEFT ALBEDO	GROUP	RIGHT ALBEDO
1	1.0000000E 00	1	0.
2	1.0000000E 00	2	0.
3	1.0000000E 00	3	0.
4	1.0000000E 00	4	0.
5	1.0000000E 00	5	0.
6	1.0000000E 00	6	0.
7	1.0000000E 00	7	0.
8	1.0000000E 00	8	0.
9	1.0000000E 00	9	0.
10	1.0000000E 00	10	0.
11	1.0000000E 00	11	0.
12	1.0000000E 00	12	0.
13	1.0000000E 00	13	0.
14	1.0000000E 00	14	0.
15	1.0000000E 00	15	0.
16	1.0000000E 00	16	0.
17	1.0000000E 00	17	0.
18	1.0000000E 00	18	0.
19	1.0000000E 00	19	0.
20	1.0000000E 00	20	0.
21	1.0000000E 00	21	0.
22	1.0000000E 00	22	0.
23	1.0000000E 00	23	0.
24	1.0000000E 00	24	0.
25	1.0000000E 00	25	0.

REGIONAL DATA

REGION	NUMBER OF INTERVALS	RIGHT-HAND BOUNDARY	BUCKLING DIMENSION	COMPOSITION IDENTIFICATION
1	-20	1.615000E 01	2.540000E 01	H/U 43.9

H32.3-D25.4      F.D.WENSTRUP      URANYL-F CANS

COMPOSITIONS

H/U 43.9

H32.3-D25.4 F.D.WENSTRUP URANYL-F CANS

RADIUS	FISSION SOURCE	EXTERNAL SOURCE
0.	1.42297E 00	0.
0.001	1.42297E 00	0.
0.807	1.41965E 00	0.
1.615	1.40970E 00	0.
2.422	1.39316E 00	0.
3.230	1.37009E 00	0.
4.037	1.34058E 00	0.
4.845	1.30475E 00	0.
5.652	1.26272E 00	0.
6.460	1.21463E 00	0.
7.267	1.16062E 00	0.
8.075	1.10083E 00	0.
8.882	1.03537E 00	0.
9.690	9.64312E-01	0.
10.497	8.87632E-01	0.
11.305	8.05215E-01	0.
12.112	7.16788E-01	0.
12.920	6.21870E-01	0.
13.727	5.19644E-01	0.
14.535	4.08541E-01	0.
15.342	2.84680E-01	0.
16.149	1.35596E-01	0.
16.150	1.35407E-01	0.

H32.3-D25.4

F.D.WENSTRUP

URANYL-F CANS

## RELATIVE FLUX DISTRIBUTIONS

RADIUS	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5
0.	3.48386E-03	3.15030E-02	8.75931E-02	1.21304E-01	1.14933E-01
0.001	3.48386E-03	3.15030E-02	8.75931E-02	1.21304E-01	1.14933E-01
0.807	3.47631E-03	3.14329E-02	8.73926E-02	1.21026E-01	1.14667E-01
1.615	3.45369E-03	3.12230E-02	8.67916E-02	1.20193E-01	1.13868E-01
2.422	3.41615E-03	3.08744E-02	8.57935E-02	1.18310E-01	1.12541E-01
3.230	3.36393E-03	3.03892E-02	8.44034E-02	1.16883E-01	1.10692E-01
4.037	3.29738E-03	2.97706E-02	8.26290E-02	1.14424E-01	1.08328E-01
4.845	3.21694E-03	2.90223E-02	8.04798E-02	1.11446E-01	1.05462E-01
5.652	3.12316E-03	2.81492E-02	7.79679E-02	1.07965E-01	1.02106E-01
6.460	3.01670E-03	2.71569E-02	7.51076E-02	1.04003E-01	9.82758E-02
7.267	2.89834E-03	2.60522E-02	7.19160E-02	9.95817E-02	9.39904E-02
8.075	2.76896E-03	2.48430E-02	6.84130E-02	9.47301E-02	8.92706E-02
8.882	2.62961E-03	2.35383E-02	6.46214E-02	8.94303E-02	8.41405E-02
9.690	2.48145E-03	2.21486E-02	6.05683E-02	8.38702E-02	7.86277E-02
10.497	2.32586E-03	2.06860E-02	5.62852E-02	7.79443E-02	7.27646E-02
11.305	2.16437E-03	1.91647E-02	5.18094E-02	7.17553E-02	6.65894E-02
12.112	1.99882E-03	1.76012E-02	4.71861E-02	6.53669E-02	6.01489E-02
12.920	1.83132E-03	1.60153E-02	4.24792E-02	5.88569E-02	5.35014E-02
13.727	1.66439E-03	1.44307E-02	3.77304E-02	5.23220E-02	4.67221E-02
14.535	1.50106E-03	1.28764E-02	3.30530E-02	4.58847E-02	3.99105E-02
15.342	1.34502E-03	1.13887E-02	2.85504E-02	3.97031E-02	3.32029E-02
16.149	1.20116E-03	1.00164E-02	2.43786E-02	3.39970E-02	2.68039E-02
16.150	1.20103E-03	1.00151E-02	2.43747E-02	3.39916E-02	2.67978E-02

H32.3-D25.4 F.D.WENSTRUP URANYL-F CANS

RELATIVE FLUX DISTRIBUTIONS

RADIUS	GROUP 6	GROUP 7	GROUP 8	GROUP 9	GROUP 10
0.	9.34928E-02	7.23887E-02	5.82887E-02	6.31644E-02	5.97096E-02
0.001	9.34928E-02	7.23887E-02	5.82887E-02	6.31644E-02	5.97096E-02
0.807	9.32756E-02	7.22205E-02	5.81531E-02	6.30176E-02	5.95708E-02
1.615	9.26245E-02	7.17162E-02	5.77469E-02	6.25773E-02	5.91545E-02
2.422	9.15424E-02	7.08780E-02	5.70718E-02	6.18455E-02	5.84626E-02
3.230	9.00339E-02	6.97096E-02	5.61306E-02	6.08254E-02	5.74980E-02
4.037	8.81056E-02	6.82158E-02	5.49273E-02	5.95212E-02	5.62649E-02
4.845	8.57659E-02	6.64031E-02	5.34670E-02	5.79384E-02	5.47683E-02
5.652	8.30248E-02	6.42791E-02	5.17559E-02	5.60837E-02	5.30145E-02
6.460	7.98941E-02	6.18524E-02	4.98009E-02	5.39646E-02	5.10106E-02
7.267	7.63871E-02	5.91331E-02	4.76100E-02	5.15897E-02	4.87648E-02
8.075	7.25187E-02	5.61320E-02	4.51919E-02	4.89685E-02	4.62857E-02
8.882	6.83056E-02	5.28607E-02	4.25561E-02	4.61111E-02	4.35827E-02
9.690	6.37661E-02	4.93318E-02	3.97127E-02	4.30281E-02	4.06655E-02
10.497	5.89207E-02	4.55583E-02	3.66721E-02	3.97305E-02	3.75436E-02
11.305	5.37927E-02	4.15538E-02	3.34455E-02	3.62295E-02	3.42258E-02
12.112	4.84092E-02	3.73322E-02	3.00443E-02	3.25356E-02	3.07187E-02
12.920	4.28028E-02	3.29076E-02	2.64804E-02	2.86582E-02	2.70246E-02
13.727	3.70144E-02	2.82936E-02	2.27658E-02	2.46036E-02	2.31368E-02
14.535	3.10968E-02	2.35025E-02	1.89126E-02	2.03727E-02	1.90321E-02
15.342	2.51232E-02	1.85448E-02	1.49332E-02	1.59564E-02	1.46551E-02
16.149	1.92105E-02	1.34376E-02	1.08482E-02	1.13341E-02	9.89648E-03
16.150	1.92047E-02	1.34324E-02	1.08441E-02	1.13294E-02	9.89141E-03

H32.3-D25.4

F.D.WENSTRUP

URANYL-F CANS

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## RELATIVE FLUX DISTRIBUTIONS

RADIUS	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15
0.	4.76137E-02	4.21665E-02	3.95485E-02	3.80251E-02	4.75149E-02
0.001	4.76137E-02	4.21665E-02	3.95485E-02	3.80251E-02	4.75149E-02
0.807	4.75029E-02	4.20684E-02	3.94564E-02	3.79365E-02	4.74042E-02
1.615	4.71709E-02	4.17742E-02	3.91805E-02	3.76711E-02	4.70724E-02
2.422	4.66190E-02	4.12853E-02	3.87218E-02	3.72299E-02	4.65209E-02
3.230	4.58496E-02	4.06037E-02	3.80822E-02	3.66148E-02	4.57519E-02
4.037	4.48659E-02	3.97322E-02	3.72646E-02	3.58283E-02	4.47685E-02
4.845	4.36720E-02	3.86745E-02	3.62721E-02	3.48736E-02	4.35748E-02
5.652	4.22729E-02	3.74349E-02	3.51088E-02	3.37545E-02	4.21754E-02
6.460	4.06742E-02	3.60183E-02	3.37793E-02	3.24753E-02	4.05756E-02
7.267	3.88822E-02	3.44302E-02	3.22887E-02	3.10409E-02	3.87812E-02
8.075	3.69038E-02	3.26767E-02	3.06424E-02	2.94562E-02	3.67979E-02
8.882	3.47463E-02	3.07637E-02	2.88458E-02	2.77260E-02	3.46315E-02
9.690	3.24169E-02	2.86974E-02	2.69040E-02	2.58549E-02	3.22866E-02
10.497	2.99223E-02	2.64830E-02	2.48212E-02	2.38460E-02	2.97662E-02
11.305	2.72683E-02	2.41240E-02	2.25995E-02	2.17001E-02	2.70696E-02
12.112	2.44575E-02	2.16207E-02	2.02372E-02	1.94140E-02	2.41909E-02
12.920	2.14872E-02	1.89670E-02	1.77257E-02	1.69776E-02	2.11160E-02
13.727	1.83439E-02	1.61458E-02	1.50460E-02	1.43714E-02	1.78203E-02
14.535	1.49950E-02	1.31211E-02	1.21627E-02	1.15631E-02	1.42667E-02
15.342	1.13728E-02	9.82642E-03	9.01817E-03	8.50676E-03	1.04087E-02
16.149	7.35135E-03	6.15254E-03	5.53460E-03	5.15480E-03	6.20725E-03
16.150	7.34700E-03	6.14858E-03	5.53090E-03	5.15128E-03	6.20286E-03



H32.3-D25.4 F.D.WENSTRUP URANYL-F CANS

## RELATIVE FLUX DISTRIBUTIONS

RADIUS	GROUP 16	GROUP 17	GROUP 18	GROUP 19	GROUP 20
0.	4.22351E-02	2.80081E-02	2.48784E-02	2.68059E-02	2.25045E-02
0.001	4.22351E-02	2.80081E-02	2.48784E-02	2.68059E-02	2.25045E-02
0.807	4.21367E-02	2.79428E-02	2.48203E-02	2.67433E-02	2.24520E-02
1.615	4.18416E-02	2.77471E-02	2.46465E-02	2.65559E-02	2.22945E-02
2.422	4.13512E-02	2.74217E-02	2.43574E-02	2.62443E-02	2.20328E-02
3.230	4.06673E-02	2.69680E-02	2.39543E-02	2.58097E-02	2.16678E-02
4.037	3.97927E-02	2.63879E-02	2.34387E-02	2.52539E-02	2.12009E-02
4.845	3.87310E-02	2.56834E-02	2.28128E-02	2.45789E-02	2.06339E-02
5.652	3.74861E-02	2.48574E-02	2.20787E-02	2.37873E-02	1.99687E-02
6.460	3.60626E-02	2.39128E-02	2.12391E-02	2.28817E-02	1.92076E-02
7.267	3.44655E-02	2.28527E-02	2.02968E-02	2.18649E-02	1.83528E-02
8.075	3.26997E-02	2.16803E-02	1.92542E-02	2.07395E-02	1.74063E-02
8.882	3.07696E-02	2.03983E-02	1.81139E-02	1.95077E-02	1.63697E-02
9.690	2.86787E-02	1.90087E-02	1.68772E-02	1.81708E-02	1.52440E-02
10.497	2.64287E-02	1.75121E-02	1.55444E-02	1.67286E-02	1.40285E-02
11.305	2.40177E-02	1.59069E-02	1.41137E-02	1.51787E-02	1.27211E-02
12.112	2.14393E-02	1.41881E-02	1.25802E-02	1.35154E-02	1.13171E-02
12.920	1.86799E-02	1.23461E-02	1.09350E-02	1.17298E-02	9.80935E-03
13.727	1.57179E-02	1.03656E-02	9.16385E-03	9.80897E-03	8.18909E-03
14.535	1.25230E-02	8.22439E-03	7.24651E-03	7.73914E-03	6.44829E-03
15.342	9.06000E-03	5.89188E-03	5.15484E-03	5.51284E-03	4.58632E-03
16.149	5.30128E-03	3.32509E-03	2.85174E-03	3.15390E-03	2.62493E-03
16.150	5.29737E-03	3.32236E-03	2.84930E-03	3.15152E-03	2.62294E-03

H32.3-D25.4 F.D.WENSTRUP URANYL-F CANS

RELATIVE FLUX DISTRIBUTIONS

RADIUS	GROUP 21	GROUP 22	GROUP 23	GROUP 24	GROUP 25
0.	1.19717E-02	2.39704E-02	2.21491E-02	7.71569E-03	5.12916E-03
0.001	1.19717E-02	2.39704E-02	2.21491E-02	7.71569E-03	5.12916E-03
0.807	1.19438E-02	2.39144E-02	2.20974E-02	7.69768E-03	5.11718E-03
1.615	1.18600E-02	2.37467E-02	2.19424E-02	7.64367E-03	5.08128E-03
2.422	1.17208E-02	2.34678E-02	2.16846E-02	7.55388E-03	5.02159E-03
3.230	1.15266E-02	2.30788E-02	2.13252E-02	7.42865E-03	4.93835E-03
4.037	1.12782E-02	2.25813E-02	2.08653E-02	7.26846E-03	4.83186E-03
4.845	1.09765E-02	2.19770E-02	2.03067E-02	7.07387E-03	4.70251E-03
5.652	1.06226E-02	2.12680E-02	1.96514E-02	6.84557E-03	4.55075E-03
6.460	1.02176E-02	2.04565E-02	1.89012E-02	6.58426E-03	4.37705E-03
7.267	9.76274E-03	1.95450E-02	1.80584E-02	6.29065E-03	4.18189E-03
8.075	9.25903E-03	1.85353E-02	1.71247E-02	5.96539E-03	3.96569E-03
8.882	8.70735E-03	1.74291E-02	1.61015E-02	5.60893E-03	3.72876E-03
9.690	8.10809E-03	1.62269E-02	1.49893E-02	5.22146E-03	3.47123E-03
10.497	7.46098E-03	1.49281E-02	1.37871E-02	4.80266E-03	3.19289E-03
11.305	6.76476E-03	1.35299E-02	1.24924E-02	4.35161E-03	2.89313E-03
12.112	6.01694E-03	1.20270E-02	1.10999E-02	3.86646E-03	2.57074E-03
12.920	5.21368E-03	1.04111E-02	9.60074E-03	3.34410E-03	2.22367E-03
13.727	4.34991E-03	8.66933E-03	7.97940E-03	2.77900E-03	1.84833E-03
14.535	3.41969E-03	6.78015E-03	6.20376E-03	2.15916E-03	1.43702E-03
15.342	2.41531E-03	4.69427E-03	4.19085E-03	1.44969E-03	9.67191E-04
16.149	1.31846E-03	2.26719E-03	1.70780E-03	5.21858E-04	3.46810E-04
16.150	1.31727E-03	2.26435E-03	1.70478E-03	5.20523E-04	3.45827E-04

H32.3-D25.4 F.D.WENSTRUP URANYL-F CANS

ITERATION	EIGENVALUE
1	1.5555020E 01
2	1.0206854E 00
3	1.0347557E 00
4	1.0400402E 00
5	1.0421952E 00
6	1.0430922E 00
7	1.0434676E 00
8	1.0436248E 00
9	1.0436908E 00
10	1.0437184E 00
11	1.0437300E 00
12	1.0437348E 00

H32.3-D25.4 F.D.WENSTRUP URANYL-F CANS

AVERAGES - REGION NO 1

VOLUME FRACTION 0.1000000E 01  
 (REGION/CORE) AVERAGE POWER 1.0000000E 00

GROUP	AVERAGE FLUX
1	0.2615795E-02
2	0.2337613E-01
3	0.6395762E-01
4	0.8859464E-01
5	0.8278365E-01
6	0.6693763E-01
7	0.5166679E-01
8	0.4159723E-01
9	0.4504021E-01
10	0.4250901E-01
11	0.3384519E-01
12	0.2993027E-01
13	0.2803485E-01
14	0.2692147E-01
15	0.3359191E-01
16	0.2981577E-01
17	0.1974807E-01
18	0.1752461E-01
19	0.1886650E-01
20	0.1582470E-01
21	0.8413460E-02
22	0.1681920E-01
23	0.1551648E-01
24	0.5402672E-02
25	0.3591940E-02

-----  
+ THIS PROGRAM PROCESSED ALL AVAILABLE CARDS  
STOP TIME BEFORE MACHINE RESTORED I STANDARD SET-UP 14.360  
-----  
RESTORE MACHINE TO STANDARD SET UP - - - PUSH START.

STOP 14.37

## 7.0 UNASSEMBLED PROGRAM LISTING

```

*      CHAIN(1,B1)                BLOCK CDP
C
*      657                        CONTROL PROG.
C
COMMON Q
C
DIMENSION Q(13764)
C
DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),
3NCODE(10),RNDT(2000),NRNDT(2000),IMAT(30),FG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),RMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),
7EPSR(25),FPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),RNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),FG),(Q(9309),FV),(Q(9333),DELTAU)
C
EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),RMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),FPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
1 CONTINUE
CALL START
IF (XABSF(MORE)-1) 5, 5, 128
5 CONTINUE
IF DIVIDE CHECK 6, 6
6 CONTINUE
CALL CID
10 CONTINUE
IF (NDT) 30, 30, 15
15 CONTINUE
CALL RNDT1
20 CONTINUE

```

```
CALL RNDT2
25 CONTINUE
CALL RNDT3
30 CONTINUE
DO 65 I=1,30
IF (CMAT(I)) 35, 65, 35
35 CONTINUE
IF (ABSF(CMAT(I))-1.0E+6) 40, 45, 45
40 CONTINUE
CALL RNDT4
GO TO 50
45 CONTINUE
MN=I
CALL AUXND
50 CONTINUE
CALL THERM
55 CONTINUE
CALL NANDW
60 CONTINUE
CALL MIX
65 CONTINUE
REWIND NDT
REWIND KTAPE
IF (SENSE LIGHT 3) 66, 66
66 CONTINUE
IF (NCODE(5)-1) 68, 67, 68
67 CONTINUE
CALL HOMRES
68 CONTINUE
IF (NCODE(2)) 70, 75, 70
70 CONTINUE
CALL REHR
75 CONTINUE
NGT=NCODE(3)+1
GO TO (100,80,85,90), NGT
80 CONTINUE
CALL ROD
GO TO 100
85 CONTINUE
CALL ANULUS
GO TO 100
90 CONTINUE
CALL PLATE
100 CONTINUE
CALL GRPAR
105 CONTINUE
CALL WTCB
110 CONTINUE
CALL WOTCB
115 CONTINUE
IF (XABSF(MORE)-1) 130, 120, 125
120 CONTINUE
KASF=MORE
GO TO 5
125 CONTINUE
```



```
CALL ENDCDP  
CALL PAGES(NPAGE)  
DO 126 I=1,15000  
CDTNAM(I)=0.0  
126 CONTINUE  
128 CONTINUE  
CALL CHAIN(2,B1)  
130 CONTINUE  
CALL ENDCDP  
CALL EXIT  
END(0,0,0)
```

```

*      657              SUBROUTINE START
C
SUBROUTINE START
C
COMMON Q
C
DIMENSION Q(13764)
C
DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),
3NCODE(10),RNDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
EQUIVALENCE (Q(2),BDATF),(Q(6),BDENT),(Q(9),BNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPFC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)
C
EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),FPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
CALL MOVE(-12,72H
1              ,CASEID)
DO 5 I=1,314
CDT(I)=0.0
5 CONTINUE
NPAGE=1
NWOT=2
NDT=R
KDT=9
ITAPE=5
JTAPE=6
KTAPE=7
REWIND NDT
REWIND KDT
REWIND ITAPE

```

```

REWIND JTAPE
REWIND KTAPE
READ, DIP, BNAM, RDATE, RIDENT, CDT, CDTNAM,
INDT, KDT, ITAPE, JTAPE, KTAPE, MORE, NWOT
IF (SENSE LIGHT 1) 10, 15
10 CONTINUE
CALL ERRORA
CALL EXIT
15 CONTINUE
CALL HDING(Q(I2))
IF (CDT(1)) 20, 60, 20
20 CONTINUE
CALL FSFBT(KDT,1)
BACKSPACE KDT
BACKSPACE KDT
READ TAPE KDT, (CDT(I), I=1,303)
IF ((CDTNAM(1) CDT(1))+(CDTNAM(2)-CDT(2))) 25, 30, 25
25 CONTINUE
CALL ERRORA
CALL EXIT
30 CONTINUE
IF (XABSF(MORE)-1) 35, 40, 45
35 CONTINUE
CALL ERRORA
CALL EXIT
40 CONTINUE
NRCD*=NCDT(3)
BACKSPACE KDT
GO TO 70
45 CONTINUE
REWIND KDT
DO 50 I=1,15000
CDTNAM(I)=0.0
50 CONTINUE
GO TO 90
60 CONTINUE
IF (XABSF(MORE)-1) 65, 70, 65
65 CONTINUE
CALL ERRORA
CALL EXIT
70 CONTINUE
DO 75 I=1,15000
DO 75 J=1,4
RDATA(I,J)=J.0
75 CONTINUE
DO 80 I=1,25
DO 80 J=1,30
GFAC(I,J)=1.0
80 CONTINUE
DO 85 I=1,6690
CMAT(I)=0.0
85 CONTINUE
90 CONTINUE
RETURN
END(0,0,0)

```

```

*      657              SUBROUTINE CID
C
SUBROUTINE CID
C
COMMON Q,IRES
C
DIMENSION Q(13764),IRES(30)
C
DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GREHR(4),GTRAN(3),GDIFC(3),
3NCOD:(10),RNDT(2000),NRNDT(2000),IMAT(30),FG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),FXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),RNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GREHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASF),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)
C
EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),FT),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MGMIN),(Q(12130),MGMAX),
7(Q(12131),MGPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
IF (KASE) 1, 1, 20
1 CONTINUE
DO 2 IR=1,30
IRES(IR)=0
2 CONTINUE
DO 5 I=1,1500
DO 5 J=1,4
RDATA(I,J)=1.0
5 CONTINUE
DO 10 I=1,25
DO 10 J=1,30
GFAC(I,J)=1.0
10 CONTINUE
DO 15 I=1,6690
CMAT(I)=0.0

```

```
15 CONTINUE  
GO TO 23  
20 CONTINUE  
DO 22 I=1,1730  
IMAT(I)=0  
22 CONTINUE  
23 CONTINUE  
READ DIP CASEID,CMAT,DMAT,ELFAC,GBEHR,GDIFC,GFAC,  
1GTRAN,GVOL,NBEHR,IRES,NCODE,SPEC,TMAT,WMAT,FT,MORE  
IF (SENSE LIGHT 1) 25, 30  
25 CONTINUE  
CALL ERRORA  
CALL ERRCDP  
30 CONTINUE  
CALL HDING(Q(12))  
RETURN  
END(0,0,0)
```

```

* 657 SUBROUTINE RNDT1
C
SUBROUTINE RNDT1
C
COMMON Q,IRES
C
DIMENSION Q(13764),IRES(30)
C
DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),
3NCODE(10),RNDT(2000),NRNDT(2000),IMAT(30),FG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),RMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),BNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPF),
3(Q(321),JTAPF),(Q(322),KTAPF),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)
C
EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),RMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),FT),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
NPASS=1
1 CONTINUE
REWIND NDT
READ TAPE NDT, (RNDT(I),I=1,2000)
NMAT=0
DO 35 J=1,30
IF (CMAT(J)) 5, 35, 5
5 CONTINUE
NMAT=NMAT+1
IF (ABS(CMAT(J))-1.0E+6) 7, 25, 25
7 CONTINUE
K=2
10 CONTINUE
IF (RNDT(4*K-1)-CMAT(J)) 12, 30, 12
12 CONTINUE

```

```
K=K+1  
IF (K-500) 10, 15, 15  
15 CONTINUE  
IF (NPASS-2) 17, 20, 20  
17 CONTINUE  
NPASS=2  
GO TO 1  
20 CONTINUE  
CALL ERRORA  
CALL FRRCDP  
25 CONTINUE  
IMAT(J)=J+3000  
GO TO 35  
30 CONTINUE  
IMAT(J)=NRNDT(4*K)  
35 CONTINUE  
RETURN  
END(0,0,0)
```

```

*      657              SUBROUTINE RNDT2
C
SUBROUTINE RNDT2
C
COMMON Q,IRES
C
DIMENSION Q(13764),IRES(30)
C
DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),
3NCODE(10),RNDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),Sigr(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
EQUIVALENCE (Q(2),RDATE),(Q(6),BDENT),(Q(9),BNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU))
C
EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),Sigr),(Q(10858),S),
4(Q(10883),FT),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
DIMENSION FU(143)
C
READ TAPE NDT, (FU(I),I=1,143)
DO 10 I=1,24
EG(I)=EU(I+69)
FV(I)=EU(I+119)
10 CONTINUE
EG(25)=EU(94)
DO 20 I=1,24
DELTAU(I)=LOGF(EG(I)/EG(I+1))
IF DIVIDE CHECK 15, 20
15 CONTINUE
CALL FRRORA
CALL ERRCDP
20 CONTINUE

```



```
DELTAU(25)=0.0  
NREC=2  
RETURN  
END(0,0,0)
```

```

*      657              SUBROUTINE RNDT3
C
SUBROUTINE RNDT3
C
COMMON Q,IRES
C
DIMENSION Q(13764),IRES(30)
C
DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),
3NCODF(10),RNDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),Sigr(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),BNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTARE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)
C
EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),Sigr),(Q(10858),S),
4(Q(10883),FT),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
DIMENSION SP(40)
C
ISPEC=0
IF (SPEC) 1, 70, 5
1 CONTINUE
READ DIP SP
IF (SENSE LIGHT 1) 2, 45
2 CONTINUE
CALL FRRORA
CALL FRRCDP
5 CONTINUE
MPASC=1
7 CONTINUE
K=2
10 CONTINUE

```

```

      IF (RNDT(4*K-1)-SPEC) 12, 25, 12
12  CONTINUE
      K=K+1
      IF (K-500) 10, 15, 15
15  CONTINUE
      IF (NPASS-2) 17, 20, 20
17  CONTINUE
      NPASS=2
      GO TO 7
20  CONTINUE
      CALL ERRORA
      CALL ERRCDP
25  CONTINUE
      ISPEC=NRNDT(4*K)
      NRS=ISPEC-NREC 1
      IF (NRS) 30, 32, 27
27  CONTINUE
      DO 23 I=1,NRS
      READ TAPE NDT
28  CONTINUE
      GO TO 32
30  CONTINUE
      CALL ERRORA
      CALL FRRCDP
32  CONTINUE
      READ TAPE NDT, (SP(I),I=1,40)
      IF (SPEC-SP(4)) 35, 40, 35
35  CONTINUE
      CALL ERRORA
      CALL ERRCDP
40  CONTINUE
      DO 42 I=1,25
      SP(I)=SP(I+4)
42  CONTINUE
45  CONTINUE
      DO 47 I=1,25
      S(I)=SP(I)*DELTAU(I)
47  CONTINUE
      IF (ISPEC) 50, 70, 50
50  CONTINUE
      NREC=ISPEC
      J=1
      DO 60 I=1,30
      IF (IMAT(I)) 60, 60, 52
52  CONTINUE
      IF (IMAT(I)-IMAT(J)) 55, 60, 60
55  CONTINUE
      J=I
60  CONTINUE
      IF (NREC-IMAT(J)) 70, 62, 65
62  CONTINUE
      BACKSPACE NDT
      NREC=NREC-1
      GO TO 70
65  CONTINUE

```

```
REWIND NDT  
-----  
NREC=0  
70 CONTINUE  
-----  
RETURN  
-----  
END(0,0,0)  
-----
```

657

SUBROUTINE RNDT4

SUBROUTINE RNDT4

COMMON Q, IRES

DIMENSION Q(13764), IRES(30)

```

DIMENSION CDT(303), NCDT(303), CDTNAM(2), ELFAC(1500,4),
1RDATA(1500,4), GFAC(25,30), CMAT(30), DMAT(30), WMAT(30),
2TMAT(30), NBEHR(30), GVOL(3), GBEHR(4), GTRAN(3), GDIFC(3),
3NCODE(10), RNDT(2000), NRNDT(2000), IMAT(30), EG(25), FV(24),
4DELTAU(25), SIGS(25), SIGTR(25), SIGA(25), SIGFN(25),
5BFSIG(25), BMSIG(25), SIGST(25,25), SIGNG(25,25), DIFFC(25),
6DIFFR(25), DIFFZ(25), SIGR(25), S(25), EXTRAP(25),
7EPSR(25), EPSZ(25), TFAC(25), SIG(520), NSIG(520),
8TRASIG(25,25), RES(1000), ENGAM(34,18)

```

```

EQUIVALENCE (Q(2), BDATE), (Q(6), BIDENT), (Q(9), BNAM),
1(Q(11), CASID), (Q(12), CASEID), (Q(13), CDT, NCDT), (Q(316), NPAGE),
2(Q(317), NWOT), (Q(318), NDT), (Q(319), KDT), (Q(320), ITAPE),
3(Q(321), JTape), (Q(322), KTape), (Q(323), MORE), (Q(324), CDTNAM),
4(Q(326), NRCDT), (Q(327), ELFAC, RDATA), (Q(6327), GFAC),
5(Q(7077), CMAT), (Q(7107), DMAT), (Q(7137), WMAT), (Q(7167), TMAT),
6(Q(7197), NBEHR), (Q(7227), GVOL), (Q(7230), GBEHR), (Q(7234), GTRAN),
7(Q(7237), GDIFC), (Q(7240), SPEC), (Q(7241), NCODE), (Q(7251), KASE),
8(Q(7252), VCOMP), (Q(7253), RNDT, NRNDT), (Q(9253), NREC),
9(Q(9254), IMAT), (Q(9284), EG), (Q(9309), FV), (Q(9333), DELTAU)

```

```

EQUIVALENCE (Q(9358), SIGS), (Q(9383), SIGTR), (Q(9408), SIGA),
1(Q(9433), SIGFN), (Q(9458), BFSIG), (Q(9483), BMSIG),
2(Q(9508), SIGST), (Q(10133), SIGNG), (Q(10758), DIFFC),
3(Q(10783), DIFFR), (Q(10808), DIFFZ), (Q(10833), SIGR), (Q(10858), S),
4(Q(10883), FT), (Q(10884), EXTRAP), (Q(10909), EPSR),
5(Q(10934), EPSZ), (Q(10959), TFAC), (Q(10984), SIG, NSIG),
6(Q(11504), TRASIG), (Q(12129), MOPMIN), (Q(12130), MOPMAX),
7(Q(12131), MOPMAX), (Q(12132), RES), (Q(13132), NRES), (Q(13133), ENGAM),
8(Q(13758), MGMIN), (Q(13759), MGMAX), (Q(13760), MGPMAX),
9(Q(13761), DF), (Q(13762), NW), (Q(13763), NTM), (Q(13764), MN)

```

1 CONTINUE

MN=1

DO 15 I=1,30

IF (IMAT(I)) 15, 15, 5

5 CONTINUE

IF (IMAT(I)-3000) 10, 15, 15

10 CONTINUE

IF (IMAT(I)-IMAT(MN)) 12, 15, 15

12 CONTINUE

MN=I

15 CONTINUE

NRS=IMAT(MN)-NREC-1

16 CONTINUE

IF (NRS) 80, 20, 17

17 DO 18 I=1,NRS

```
      READ TAPE NDT
18 CONTINUE
20 CONTINUE
      DO 32 J=1,2780
      SIG(J)=0.0
32 CONTINUE
      READ TAPE NDT, (SIG(I),I=1,520)
      NREC=IMAT(MN)
      IF(CMAT(MN)-SIG(4)) 25, 30, 25
25 CONTINUE
      CALL ERRORA
      CALL ERRCDP
30 CONTINUE
      IF (SIG(510)) 40, 40, 35
35 CONTINUE
      MOMIN=NSIG(510)
      MOMAX=NSIG(511)
      MOPMAX=NSIG(512)
      READ TAPE NDT, ((TRASIG(I,J),J=MOMIN,MOPMAX),I=MOMIN,MOMAX)
      NREC=NREC+1
40 CONTINUE
      IF (SIG(513)) 50, 50, 45
45 CONTINUE
      READ TAPE NDT
      NREC=NREC+1
50 CONTINUE
      IF (SIG(516)) 60, 60, 55
55 CONTINUE
      NRES=NSIG(516)
      NTRES=5*NRES
      READ TAPE NDT, (RES(I),I=1,NTRES)
      NREC=NREC+1
60 CONTINUE
      IF (NCODE(4)) 75, 75, 65
65 CONTINUE
      IF (SIG(517)) 75, 75, 70
70 CONTINUE
      MGMIN=NSIG(517)
      MGMAX=NSIG(518)
      MGPMAX=NSIG(519)
      READ TAPE NDT, ((FNGAM(I,J),J=MGMIN,MGPMAX),I=MGMIN,MGMAX)
      NREC=NREC+1
75 CONTINUE
      DF=SIG(209)
      NW=NSIG(520)
80 CONTINUE
      IMAT(MN)=MN+3000
      RETURN
      END
```

657

SUBROUTINE AUXND

SUBROUTINE AUXND

COMMON Q, IRES

DIMENSION Q(13764), IRES(30)

```

DIMENSION CDT(303), NCDT(303), CDTNAM(2), ELFAC(1500,4),
1RDATA(1500,4), GFAC(25,30), CMAT(30), DMAT(30), WMAT(30),
2TMAT(30), NBEHR(30), GVOL(3), GREHR(4), GTRAN(3), GDIFC(3),
3NCODE(10), RNDT(2000), NRNDT(2000), IMAT(30), EG(25), FV(24),
4DELTAU(25), SIGS(25), SIGTR(25), SIGA(25), SIGFN(25),
5BFSIG(25), BMSIG(25), SIGST(25,25), SIGNG(25,25), DIFFC(25),
6DIFFR(25), DIFFZ(25), SIGR(25), S(25), EXTRAP(25),
7EPSR(25), EPSZ(25), TFAC(25), SIG(520), NSIG(520),
8TRASIG(25,25), RES(1000), ENGAM(34,18)

```

```

EQUIVALENCE (Q(2), RDATE), (Q(6), BDENT), (Q(9), BNAM),
1(Q(11), CASID), (Q(12), CASEID), (Q(13), CDT, NCDT), (Q(316), NPAGE),
2(Q(317), NWOT), (Q(318), NDT), (Q(319), KDT), (Q(320), ITAPE),
3(Q(321), JTAPE), (Q(322), KTAPE), (Q(323), MORE), (Q(324), CDTNAM),
4(Q(326), NRCDT), (Q(327), FLFAC, RDATA), (Q(6327), GFAC),
5(Q(7077), CMAT), (Q(7107), DMAT), (Q(7137), WMAT), (Q(7167), TMAT),
6(Q(7197), NBEHR), (Q(7227), GVOL), (Q(7230), GREHR), (Q(7234), GTRAN),
7(Q(7237), GDIFC), (Q(7240), SPEC), (Q(7241), NCODE), (Q(7251), KASE),
8(Q(7252), VCOMP), (Q(7253), RNDT, NRNDT), (Q(9253), NREC),
9(Q(9254), IMAT), (Q(9284), EG), (Q(9309), FV), (Q(9333), DELTAU)

```

```

EQUIVALENCE (Q(9358), SIGS), (Q(9383), SIGTR), (Q(9408), SIGA),
1(Q(9433), SIGFN), (Q(9458), BFSIG), (Q(9483), BMSIG),
2(Q(9508), SIGST), (Q(10133), SIGNG), (Q(10758), DIFFC),
3(Q(10783), DIFFR), (Q(10808), DIFFZ), (Q(10833), SIGR), (Q(10858), S),
4(Q(10883), FT), (Q(10884), EXTRAP), (Q(10909), EPSR),
5(Q(10934), EPSZ), (Q(10959), TFAC), (Q(10984), SIG, NSIG),
6(Q(11504), TRASIG), (Q(12129), MOMIN), (Q(12130), MOMAX),
7(Q(12131), MOPMAX), (Q(12132), RES), (Q(13132), NRES), (Q(13133), ENGAM),
8(Q(13758), MGMIN), (Q(13759), MGMAX), (Q(13760), MGPMAX),
9(Q(13761), DF), (Q(13762), NW), (Q(13763), NTM), (Q(13764), MN)

```

```

DIMENSION SS(34), XISS(34), STR(34), SA(34), XISS1(34),
1SNF(34), TM4500(30), TM4000(30), TM3500(30), TM3000(30), TM2500(30),
2TM2000(30), TM1500(30), TM1000(30), TM500(30), TM68(30)

```

1 CONTINUE

MN=MN

IF (KASE) 5, 5, 65

5 CONTINUE

DO 7 I=1, 34

SS(I)=0.0

XISS(I)=0.0

STR(I)=0.0

SA(I)=0.0

XISS1(I)=0.0

SNF(I)=0.0

7 CONTINUE

DO 10 I=1,30  
 TM4500(I)=0.0  
 TM4000(I)=0.0  
 TM3500(I)=0.0  
 TM3000(I)=0.0  
 TM2500(I)=0.0  
 TM2000(I)=0.0  
 TM1500(I)=0.0  
 TM1000(I)=0.0  
 TM500(I)=0.0  
 TM68(I)=0.0

10 CONTINUE

DF=0.0  
 MOMIN=0  
 MOMAX=0  
 MOPMAX=0  
 M1MIN=0  
 M1MAX=0  
 M1PMAX=0  
 NRFS=0  
 MGMIN=0  
 MGMAX=0  
 MGPMAX=0  
 NW=0

RFAD DIP CODE, SS, XISS, STR, SA, XISS1, SNF, DF,  
 1 TM4500, TM4000, TM3500, TM3000, TM2500, TM2000,  
 2 TM1500, TM1000, TM500, TM68, MOMIN, MOMAX,  
 3 MOPMAX, M1MIN, M1MAX, M1PMAX, MGMIN, MGMAX,  
 4 MGPMAX, TRASIG, RES, ENGAM  
 IF (SENSE LIGHT 1) 15, 20

15 CONTINUE

CALL ERRORA  
 CALL ERRCDP

20 CONTINUE

IF (CODE-CMAT(MN)) 22, 25, 22

22 CONTINUE

CALL ERRORA  
 CALL ERRCDP

25 CONTINUE

SIG(4)=CODE  
 DO 30 I=1,34  
 SIG(I+4)=SS(I)  
 SIG(I+38)=XISS(I)  
 SIG(I+72)=STR(I)  
 SIG(I+106)=SA(I)  
 SIG(I+140)=XISS1(I)  
 SIG(I+174)=SNF(I)

30 CONTINUE

SIG(209)=DF  
 DO 35 I=1,30  
 SIG(I+209)=TM4500(I)  
 SIG(I+239)=TM4000(I)  
 SIG(I+269)=TM3500(I)  
 SIG(I+299)=TM3000(I)



```

SIG(I+329)=TM2500(I)
SIG(I+359)=TM2000(I)
SIG(I+389)=TM1500(I)
SIG(I+419)=TM1000(I)
SIG(I+449)=TM500(I)
SIG(I+479)=TM68(I)
35 CONTINUE
NSIG(510)=MOMIN
NSIG(511)=MOMAX
NSIG(512)=MOPMAX
NSIG(513)=M1MIN
NSIG(514)=M1MAX
NSIG(515)=M1PMAX
NSIG(516)=NRES
NSIG(517)=MGMIN
NSIG(518)=MGMAX
NSIG(519)=MGPMAX
NSIG(520)=NW
WRITE TAPE ITAPE, (SIG(I),I=1,520)
IF (MOMIN) 45, 45, 40
40 CONTINUE
MMAX=(MOMAX-MOMIN+1)*(MOPMAX-MOMIN 1)
WRITE TAPE ITAPE, (TRASIG(I),I=1,MMAX)
45 CONTINUE
IF (NRES) 55, 55, 50
50 CONTINUE
NTRES=5*NRES
WRITE TAPE ITAPE, (RFS(I),I=1,NTRES)
55 CONTINUE
IF (MGMIN) 100, 100, 60
60 CONTINUE
MMAX=(MGMAX-MGMIN+1)*(MGPMAX-MGMIN 1)
WRITE TAPE ITAPE, (ENGAM(I),I=1,MMAX)
GO TO 100
65 CONTINUE
READ TAPE ITAPE, (SIG(I),I=1,520)
IF (SIG(4)-CMAT(MN)) 67, 68, 67
67 CONTINUE
CALL FRRORA
CALL FRRCDP
68 CONTINUE
IF (SIG(510)) 75, 75, 70
70 CONTINUE
MOMIN=NSIG(510)
MOMAX=NSIG(511)
MOPMAX=NSIG(512)
READ TAPE ITAPE, ((TRASIG(I,J),J=MOMIN,MOPMAX),I=MOMIN,MOMAX)
75 CONTINUE
IF (SIG(516)) 85, 85, 80
80 CONTINUE
NRES=NSIG(516)
NTRES=5*NRES
READ TAPE ITAPE, (RFS(I),I=1,NTRES)
85 CONTINUE
IF (SIG(517)) 95, 95, 90

```

---

90 CONTINUE

MGMIN=NSIG(517)

MGMAX=NSIG(518)

MGPMAX=NSIG(519)

READ TAPE ITAPE, ((ENGAM(I,J),J=MGMIN,MGPMAX),I=MGMIN,MGMAX)

---

95 CONTINUE

100 CONTINUE

---

RETURN

END(0,0,0)

---

657

## SUBROUTINE THERM

SUBROUTINE THERM

COMMON Q,IRES

DIMENSION Q(13764),IRES(30)

```

DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),
3NCODF(10),RNDT(2000),NRNDT(2000),IMAT(30),FG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)

```

```

EQUIVALENCE (Q(2),RDATE),(Q(6),RDEMT),(Q(9),RNAME),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORF),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)

```

```

EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),RMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),FT),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)

```

1 CONTINUE

MN=MN

TFMP=TMAT(MN)

TMAT(MN)=ARSF(TMAT(MN))

IF(TMAT(MN)) 4, 2, 4

2 CONTINUE

CALL FRRORA

CALL ERRCDP

4 CONTINUE

IF(TMAT(MN)-SIG(480)) 5, 6, 7

5 CONTINUE

TMAT(MN)=SIG(480)

6 CONTINUE

NTM=480

GO TO 60

```
7 CONTINUE
  IF (TMAT(MN)-SIG(450)) 10, 14, 15
10 CONTINUE
  IF ((TMAT(MN)-SIG(480))-(SIG(450)-TMAT(MN))) 5, 12, 12
12 CONTINUE
  TMAT(MN)=SIG(450)
14 CONTINUE
  NTM=450
  GO TO 60
15 CONTINUE
  IF (TMAT(MN)-SIG(420)) 16, 19, 20
16 CONTINUE
  IF ((TMAT(MN)-SIG(450))-(SIG(420)-TMAT(MN))) 12, 18, 18
18 CONTINUE
  TMAT(MN)=SIG(420)
19 CONTINUE
  NTM=420
  GO TO 60
20 CONTINUE
  IF (TMAT(MN)-SIG(390)) 21, 24, 25
21 CONTINUE
  IF ((TMAT(MN)-SIG(420))-(SIG(390)-TMAT(MN))) 18, 23, 23
23 CONTINUE
  TMAT(MN)=SIG(390)
24 CONTINUE
  NTM=390
  GO TO 60
25 CONTINUE
  IF (TMAT(MN)-SIG(360)) 26, 29, 30
26 CONTINUE
  IF ((TMAT(MN)-SIG(390))-(SIG(360)-TMAT(MN))) 23, 28, 28
28 CONTINUE
  TMAT(MN)=SIG(360)
29 CONTINUE
  NTM=360
  GO TO 60
30 CONTINUE
  IF (TMAT(MN)-SIG(330)) 31, 34, 35
31 CONTINUE
  IF ((TMAT(MN)-SIG(360))-(SIG(330)-TMAT(MN))) 28, 33, 33
33 CONTINUE
  TMAT(MN)=SIG(330)
34 CONTINUE
  NTM=330
  GO TO 60
35 CONTINUE
  IF (TMAT(MN)-SIG(300)) 36, 39, 40
36 CONTINUE
  IF ((TMAT(MN)-SIG(330))-(SIG(300)-TMAT(MN))) 33, 38, 38
38 CONTINUE
  TMAT(MN)=SIG(300)
39 CONTINUE
  NTM=300
  GO TO 60
40 CONTINUE
```

```

      IF (TMAT(MN)-SIG(270)) 41, 44, 45
41  CONTINUE
      IF ((TMAT(MN)-SIG(300))-(SIG(270)-TMAT(MN))) 38, 43, 43
43  CONTINUE
      TMAT(MN)=SIG(270)
44  CONTINUE
      NTM=270
      GO TO 60
45  CONTINUE
      IF (TMAT(MN)-SIG(240)) 46, 49, 50
46  CONTINUE
      IF ((TMAT(MN)-SIG(270))-(SIG(240)-TMAT(MN))) 43, 48, 48
48  CONTINUE
      TMAT(MN)=SIG(240)
49  CONTINUE
      NTM=240
      GO TO 60
50  CONTINUE
      IF (TMAT(MN)-SIG(210)) 51, 54, 55
51  CONTINUE
      IF ((TMAT(MN)-SIG(240))-(SIG(210)-TMAT(MN))) 48, 55, 55
55  CONTINUE
      TMAT(MN)=SIG(210)
54  CONTINUE
      NTM=210
60  CONTINUE
      A1=SIG(NTM+5)+SIG(NTM+6) SIG(NTM+7)+SIG(NTM+8)+SIG(NTM 9)
      B1=SIG(NTM+10) SIG(NTM+11)+SIG(NTM 12)+SIG(NTM+13)+SIG(NTM+14)
      C1=SIG(NTM+15) SIG(NTM+16)+SIG(NTM 17)+SIG(NTM+18)+SIG(NTM+19)
      D1=SIG(NTM+20) SIG(NTM+21)+SIG(NTM 22)+SIG(NTM+23)+SIG(NTM+24)
      SIG(93)=SIG(93)/SIG(25)*A1
      SIG(94)=SIG(94)/SIG(26)*B1
      SIG(95)=SIG(95)/SIG(27)*C1
      SIG(96)=SIG(96)/SIG(28)*D1
      SIG(97)=SIG(NTM+2)
      IF DIVIDE CHECK 65, 70
65  CONTINUE
      CALL ERRORA
      CALL FRRCDP
70  CONTINUE
      SIG(25)=A1
      SIG(26)=B1
      SIG(27)=C1
      SIG(28)=D1
      SIG(29)=SIG(NTM+1)
      SIG(131)=SIG(NTM+3)
      SIG(199)=SIG(NTM+4)
      TMAT(MN)=TEMP
      RETURN
      END(0,0,0)

```

```

*      657              SUBROUTINE NANDW
C
SUBROUTINE NANDW
C
COMMON Q,IRES
C
DIMENSION Q(13764),IRES(30)
C
DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GREHR(4),GTRAN(3),GDIFC(3),
3NCODF(10),RNDT(2000),NRNDT(2000),IMAT(30),FG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),BNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCNT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GREHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)
C
EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),FT),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
MN=MN
IF (NCODE(1)-1) 5, 10, 15
5 CONTINUE
VCOMP=GVOL(1)*GVOL(2)*GVOL(3)
GO TO 25
10 CONTINUE
VCOMP=.78539816*GVOL(1)*(GVOL(2)**2-GVOL(3)**2)
GO TO 25
15 CONTINUE
VCOMP=4.1887902*GVOL(1)**3
25 CONTINUE
IF (DMAT(MN)) 45, 30, 45
30 CONTINUE
DMAT(MN)=WMAT(MN)/DF/VCOMP
IF DIVIDE CHECK 35, 40

```

```
35 CONTINUE  
CALL ERRORA  
CALL ERRCDP  
40 CONTINUE  
GO TO 50  
45 CONTINUE  
WMAT(MN)=DMAT(MN)*DF*VCOMP  
50 CONTINUE  
RETURN  
END(0,0,0)
```

```

*      657              SUBROUTINE MIX
C
C      SUBROUTINE MIX
C
C      COMMON Q,IRES
C
C      DIMENSION Q(13764),IRES(30)
C
C      DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GREHR(4),GTRAN(3),GDIFC(3),
3NCODE(10),RNDT(2000),NRNDT(2000),IMAT(30),FG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5RFSIG(25),RMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),FXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
C      EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),BNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),FLFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GREHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)
C
C      EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),RFSIG),(Q(9483),RMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),FT),(Q(10884),FXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
1 CONTINUE
  MN=MN
  IF (TMAT(MN)) 5, 10, 10
5 CONTINUE
  READ DIP SIG,TRASIG,RES,ENGAM,DF,NRES,
  IMOMIN,MOMAX,MOPMAX,MGMIN,MGMAX,MGPMAX,S,BETA,FM,DELTAU
  IF (SENSE LIGHT 1) 8, 10
8 CONTINUE
  CALL FRRORA
  CALL FRRCDP
10 CONTINUE
  DO 15 I=1,25
  SIGS(I)=SIGS(I)+DMAT(MN)*GFAC(I,MN)*SIG(I+4)
  SIGTR(I)=SIGTR(I)+DMAT(MN)*GFAC(I,MN)*SIG(I+72)
  SIGA(I)=SIGA(I)+DMAT(MN)*GFAC(I,MN)*SIG(I+106)

```



```

SIGFN(I)=SIGFN(I)+DMAT(MN)*GFAC(I,MN)*SIG(I+174)
15 CONTINUE
IA=4
DO 20 I=21,25
DO 20 J=21,25
IA=IA+1
IB=NTM+IA
TRASIG(I,J)=SIG(IB)
20 CONTINUE
IF (MOMIN) 30, 25, 30
25 CONTINUE
IA=20
GO TO 35
30 CONTINUE
IA=MOMIN-1
IF (IA) 35, 42, 35
35 CONTINUE
DO 40 I=1,IA
TRASIG(I,I+1)=SIG(I+38)/DELTAU(I)
TRASIG(I,I)=SIG(I+4)-SIG(I+38)/DELTAU(I)
IF DIVIDE CHECK 37, 38
37 CONTINUE
CALL ERRORA
CALL ERRCDP
38 CONTINUE
40 CONTINUE
42 CONTINUE
IF (MOMIN) 45, 75, 45
45 CONTINUE
IF (MOMAX-MOPMAX) 50, 55, 60
50 CONTINUE
IA=MOMAX+1
GO TO 65
55 CONTINUE
TRASIG(MOMAX,MOMAX+1)=SIG(MOMAX+38)/DELTAU(MOMAX)
IF DIVIDE CHECK 57, 58
57 CONTINUE
CALL ERRORA
CALL FRRCDP
58 CONTINUE
IA=MOMAX+1
GO TO 65
60 CONTINUE
TRASIG(MOPMAX,MOPMAX+1)=SIG(MOPMAX+38)/DELTAU(MOPMAX)
IF DIVIDE CHECK 62, 63
62 CONTINUE
CALL ERRORA
CALL ERRCDP
63 CONTINUE
IA=MOPMAX+1
65 CONTINUE
DO 70 I=IA,20
TRASIG(I,I+1)=SIG(I+38)/DELTAU(I)
TRASIG(I,I)=SIG(I+4)-SIG(I+38)/DELTAU(I)
IF DIVIDE CHECK 67, 68

```

```

67 CONTINUE
  CALL ERRORA
  CALL ERRCDP
68 CONTINUE
70 CONTINUE
75 CONTINUE
  DO 80 I=1,25
  DO 80 J=1,25
  SIGST(I,J)=SIGST(I,J)+DMAT(MN)*GFAC(I,MN)*TRASIG(I,J)
80 CONTINUE
  IF (NCODE(2)) 85, 125, 85
85 CONTINUE
  IF (NBEHR(MN)) 100, 90, 100
90 CONTINUE
  DO 95 I=1,25
  BFSIG(I)=BFSIG(I)+DMAT(MN)*GFAC(I,MN)*SIG(I+106)
95 CONTINUE
  GO TO 125
100 CONTINUE
  IF (NCODE(2)) 115, 105, 105
105 CONTINUE
  DO 110 I=1,25
  RMSIG(I)=RMSIG(I)+DMAT(MN)*GFAC(I,MN)*
  1(SIG(I+4)+SIG(I+106))
110 CONTINUE
115 CONTINUE
  DO 120 I=1,25
  BMSIG(I)=BMSIG(I)+DMAT(MN)*GFAC(I,MN)*
  1(SIG(I+72)+SIG(I+106))
120 CONTINUE
125 CONTINUE
  IF (NCODE(4)) 145, 145, 130
130 CONTINUE
  IF (MGMIN) 135, 145, 135
135 CONTINUE
  NTNG=NTM/30+18
  DO 137 J=1,18
  ENGAM(25,J)=ENGAM(NTNG,J)
137 CONTINUE
  DO 140 I=1,25
  DO 140 J=1,18
  SIGNG(I,J)=SIGNG(I,J)+DMAT(MN)*GFAC(I,MN)*ENGAM(I,J)
140 CONTINUE
145 CONTINUE
  IF (NCODE(5)-1) 180, 148, 175
148 CONTINUE
  IF (SFENSE LIGHT 3) 160, 150
150 CONTINUE
  NRES1=0
  DO 155 I=1,1500
  DO 155 J=1,4
  RDATA(I,J)=0.0
155 CONTINUE
160 CONTINUE
  NRES2=NRES1+NRES

```

```
NRES1=NRES1+1
I=0
DO 170 K=NRES1,NRES2
I=I+1
IA=I NRES
IB=I 2*NRES
IC=I 3*NRES
ID=I 4*NRES
RDATA(K,1)=RES(I)
RDATA(K,2)=DMAT(MN)*RES(IA)
RDATA(K,3)=DMAT(MN)*RES(IA)*RES(ID)
RDATA(K,4)=DMAT(MN)*RES(IR)*PSI(RES(IC)*((TMAT(MN)-32.)*
15./9.+273.13),0)
170 CONTINUE
NRES1=NRES2
SENSE LIGHT 3
GO TO 180
175 CONTINUE
DO 176 I=1,1500
RDATA(I,4)=0.0
176 CONTINUE
I=0
DO 178 K=1,NRES
I=I+1
IA=I NRES
IR=I 2*NRES
IC=I 3*NRES
ID=I 4*NRES
KA=K 200
KB=K 400
KC=K 600
RDATA(K,4)=RES(I)
RDATA(KA,4)=DMAT(MN)*RES(IA)
RDATA(KB,4)=RES(IC)*((TMAT(MN)-32.)*5./9.+273.13)
RDATA(KC,4)=DMAT(MN)*RES(IR)*FT
178 CONTINUE
CALL HETRES
180 CONTINUE
RETURN
```

```

* 657 SUBROUTINE HOMRES
C
SUBROUTINE HOMRES
C
COMMON Q, IRES
C
DIMENSION Q(13764), IRES(30)
C
DIMENSION CDT(303), NCDT(303), CDTNAM(2), ELFAC(1500,4),
1RDATA(1500,4), GFAC(25,30), CMAT(30), DMAT(30), WMAT(30),
2TMAT(30), NBEHR(30), GVOL(3), GBEHR(4), GTRAN(3), GDIFC(3),
3NCODE(10), RNDT(2000), NRNDT(2000), IMAT(30), EG(25), FV(24),
4DELTAU(25), SIGS(25), SIGTR(25), SIGA(25), SIGFN(25),
5RFSIG(25), RMSIG(25), SIGST(25,25), SIGNG(25,25), DIFFC(25),
6DIFFR(25), DIFFZ(25), SIGR(25), S(25), FXTRAP(25),
7EPSR(25), EPSZ(25), TFAC(25), SIG(520), NSIG(520),
8TRASIG(25,25), RES(1000), ENGAM(34,18)
C
EQUIVALENC F (Q(2),RDATA), (Q(6),RDFNT), (Q(9),PNAM),
1(Q(11),CASID), (Q(12),CASEID), (Q(13),CDT,NCDT), (Q(316),NPAGE),
2(Q(317),NWOT), (Q(318),NDT), (Q(319),KDT), (Q(320),ITAPE),
3(Q(321),JTAPE), (Q(322),KTAPE), (Q(323),MORE), (Q(324),CDTNAM),
4(Q(326),NRCDT), (Q(327),ELFAC,RDATA), (Q(6327),GFAC),
5(Q(7077),CMAT), (Q(7107),DMAT), (Q(7137),WMAT), (Q(7167),TMAT),
6(Q(7197),NBEHR), (Q(7227),GVOL), (Q(7230),GBEHR), (Q(7234),GTRAN),
7(Q(7237),GDIFC), (Q(7240),SPEC), (Q(7241),NCODE), (Q(7251),KASE),
8(Q(7252),VCOMP), (Q(7253),RNDT,NRNDT), (Q(9253),NREC),
9(Q(9254),IMAT), (Q(9284),FG), (Q(9309),FV), (Q(9333),DELTAU)
C
EQUIVALENC F (Q(9358),SIGS), (Q(9383),SIGTR), (Q(9408),SIGA),
1(Q(9433),SIGFN), (Q(9458),RFSIG), (Q(9483),BMSIG),
2(Q(9508),SIGST), (Q(10133),SIGNG), (Q(10758),DIFFC),
3(Q(10783),DIFFR), (Q(10808),DIFFZ), (Q(10833),SIGR), (Q(10858),S),
4(Q(10883),FT), (Q(10884),EXTRAP), (Q(10909),EPSR),
5(Q(10934),EPSZ), (Q(10959),TFAC), (Q(10984),SIG,NSIG),
6(Q(11504),TRASIG), (Q(12129),MOMIN), (Q(12130),MOMAX),
7(Q(12131),MOPMAX), (Q(12132),RES), (Q(13132),NRES), (Q(13133),ENGAM),
8(Q(13758),MGMIN), (Q(13759),MGMAX), (Q(13760),MGPMAX),
9(Q(13761),DF), (Q(13762),NW), (Q(13763),NTM), (Q(13764),MN)
C
DO 20 K=1,20
DO 15 I=1,1500
IF (RDATA(I,1) FG(K+1)) 15, 10, 10
10 CONTINUE
IF (RDATA(I,4)) 15, 15, 11
11 CONTINUE
SIGA(K)=SIGA(K)-1.0/DELTAU(K)*(1.0/(1.0+SIGS(K)/RDATA(I,4)))*
1RDATA(I,2)
SIGFN(K)=SIGFN(K)-1.0/DELTAU(K)*(1.0/(1.0+SIGS(K)/RDATA(I,4)))*
1RDATA(I,3)
RDATA(I,1)=0.0
15 CONTINUE
20 CONTINUE
25 CONTINUE
RETURN

```

END(0,0,0)

```

*      657              SUBROUTINE HETRES
C
C      SUBROUTINE HFTRES
C
C      COMMON Q,IRES
C
C      DIMENSION Q(13764),IRES(30)
C
C      DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),
3NCOD(10),RNDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),FNGAM(34,18)
C
C      EQUIVALENCE (Q(2),RDATA),(Q(6),RDFNT),(Q(9),RNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DFLTAU)
C
C      EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),FT),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
C      MN=MN
C      IF (IRES(MN)) 50, 5, 25
5 CONTINUE
C      DO 20 K=1,20
C      DO 15 I=1,200
C      IA=I 200
C      IB=I 400
C      IC=I 600
C      IF (RDATA(I,4) EG(K+1)) 15, 10, 10
10 CONTINUE
C      SIGA(K)=SIGA(K)-RDATA(IA,4)/DFLTAU(K)*(1.0-
IRSS(RDATA(IC,4),RDATA(IB,4)))
C      SIGFN(K)=SIGFN(K)-RDATA(IA,4)/DFLTAU(K)*(1.0
IRSS(RDATA(IC,4),RDATA(IB,4)))
14 CONTINUE

```

```
      RDATA(I,4)=0.0
15 CONTINUE
20 CONTINUE
      GO TO 50
25 CONTINUE
      DO 45 K=1,20
      DO 40 I=1,200
      IA=I 200
      IF (RDATA(I,4) FG(K+1)) 40, 30, 30
30 CONTINUE
      IB=I (MN-1)*NCODE(6)
      SIGA(K)=SIGA(K)-RDATA(IA,4)/DELTAU(K)*(1.0-ELFAC(IR))
      SIGFN(K)=SIGFN(K)-RDATA(IA,4)/DELTAU(K)*(1.0-ELFAC(IR))
      RDATA(I,4)=0.0
40 CONTINUE
45 CONTINUE
50 CONTINUE
      RETURN
      END
```

```

*      657              SUBROUTINE BEHR
C
C      SUBROUTINE BEHR
C
C      COMMON Q
C
C      DIMENSION Q(13764)
C
C      DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GREHR(4),GTRAN(3),GDIFC(3),
3NCODF(10),RNDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5RFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),Sigr(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RFS(1000),ENGAM(34,18)
C
C      EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),BNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),FLFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GREHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)
C
C      EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),RFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),Sigr),(Q(10858),S),
4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),FPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
C      DIMENSION FX(25),WHY(25)
C
C      IF (GRFHR(4)) 25, 5, 25
5 CONTINUE
IF (ARSF(GRFHR(3)-GRFHR(2))-0.1*GRFHR(2)) 10, 15, 15
10 CONTINUE
ELF=(GRFHR(2)**2-GRFHR(1)**2)/GRFHR(1)
ELM=(GRFHR(3)**2-GRFHR(2)**2+GREHR(1)**2)/GRFHR(1)
IF DIVIDE CHECK 12, 13
12 CONTINUE
CALL ERRORA
CALL FRRCDP
13 CONTINUE
GO TO 20
15 CONTINUE

```



```

ELF=GREHR(2)-GREHR(1)
ELM=(GBEHR(3)**2-GREHR(2)**2+GREHR(1)**2)/(GBEHR(2)+GBEHR(1))
IF DIVIDE CHECK 17, 18
17 CONTINUE
CALL ERRORA
CALL ERRCDP
18 CONTINUE
20 CONTINUE
VFF=(GBEHR(2)**2-GBEHR(1)**2)/GBEHR(3)**2
IF DIVIDE CHECK 22, 23
22 CONTINUE
CALL ERRORA
CALL ERRCDP
23 CONTINUE
QFAC=1.3333333
GO TO 30
25 CONTINUE
ELF=GBEHR(1)
ELM=GBEHR(2)
VFF=GBEHR(3)
QFAC=GBEHR(4)
30 CONTINUE
VFM=1.0-VFF
IF (NCODE(2)-1) 60, 35, 45
35 CONTINUE
QMR=0.50*QFAC
QMZ=QMR
DO 40 I=1,25
EX(I)=ELF*BFSIG(I)/VFF
WHY(I)=ELM*BMSIG(I)/VFM
IF DIVIDE CHECK 36, 37
36 CONTINUE
CALL ERRORA
CALL ERRCDP
37 CONTINUE
EPSR(I)=VFF**2*FXPF(-FX(I))*(WHY(I)/(EXP(WHY(I))-1.0)
1QMR*WHY(I)-1.0)
IF DIVIDE CHECK 38, 39
38 CONTINUE
CALL ERRORA
CALL ERRCDP
39 CONTINUE
EPSZ(I)=EPSR(I)
40 CONTINUE
GO TO 60
45 CONTINUE
QMR=0.3750*QFAC
QMZ=).750*QFAC
DO 50 I=1,25
EX(I)=ELF*BFSIG(I)/VFF
WHY(I)=ELM*BMSIG(I)/VFM
IF DIVIDE CHECK 46, 47
46 CONTINUE
CALL ERRORA
CALL ERRCDP

```

47 CONTINUE

---

EPSR(I)=VFF\*\*2\*EXPF(-EX(I))\*(WHY(I))/(EXPF(WHY(I))-1.0)  
1QMR\*WHY(I)-1.0)

---

EPSZ(I)=VFF\*\*2\*EXPF(-FX(I))\*(WHY(I))/(EXPF(WHY(I))-1.0)  
1QMZ\*WHY(I)-1.0)

---

IF DIVIDE CHECK 48, 49

48 CONTINUE

---

CALL ERRORA

CALL ERRCDP

---

49 CONTINUE

50 CONTINUE

---

60 CONTINUE

RETURN

---

END(n,0,0)

657

## SUBROUTINE ROD

SUBROUTINE ROD

COMMON Q

DIMENSION Q(13764)

```

DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GREHR(4),GTRAN(3),GDIFC(3),
3NCODF(10),RNDT(2000),NRNDT(2000),IMAT(30),FG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),RMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),FXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)

```

```

EQUIVALENCE (Q(2),RDATE),(Q(6),RDENT),(Q(9),BNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GREHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPFC),(Q(7241),NCODF),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)

```

```

EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),FPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)

```

RD=GTRAN(1)/GTRAN(2)

DO 12 I=1,25

TPA=SIGS(I)/(SIGS(I)+SIGA(I))

TPOT=GTRAN(I)/2.0\*(SIGS(I)+SIGA(I))

IF (2.0-TPOT) 1, 1, 2

1 CONTINUE

TPG=1.0

GO TO 11

2 CONTINUE

BIO=RESIF(TPOT,0)

IF (SENSE LIGHT 1) 3, 4

3 CONTINUE

CALL ERRORA

CALL ERRCDP

4 CONTINUE

```
BI1=RESIF(TPOT,1)
IF (SENSE LIGHT 1) 5, 6
5 CONTINUE
CALL FRRORA
CALL ERRCDP
6 CONTINUE
BK0=RESKF(TPOT,0)
IF (SENSE LIGHT 1) 7, 8
7 CONTINUE
CALL FRRORA
CALL ERRCDP
8 CONTINUE
BK1=RESKF(TPOT,1)
IF (SENSE LIGHT 1) 9, 10
9 CONTINUE
CALL FRRORA
CALL FRRCDP
10 CONTINUE
TPG=1.3333333*TPOT**2*(BI0*BK1-BI1*BK0+BI1*BK1/TPOT+
1(TPOT+TPOT)*(BI0*BK0+BI1*BK1)-2.0)
11 CONTINUE
TFAC(I)=1.0-(RD*((1.0-TPA)*TPG/(1.0-TPA*(1.0 TPG/
1(TPOT+TPOT))))))
12 CONTINUE
RETURN
END(0,0,0)
```

\* 657

## SUBROUTINE ANULUS

SUBROUTINE ANULUS

COMMON Q

DIMENSION Q(13764)

```

DIMENSION CDT(303),NCDT(303),CDTNAM(2),FLFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NRFHR(30),GVOL(3),GRFHR(4),GTRAN(3),GDIFC(3),
3NCODE(10),RNDT(2000),NRNDT(2000),IMAT(30),FG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)

```

```

EQUIVALENCE (Q(2),RDATE),(Q(6),RDFENT),(Q(9),RNAME),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCNT),(Q(327),FLFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GRFHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)

```

```

EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)

```

RD=GTRAN(1)/GTRAN(2)

DO 5 I=1,25

TPA=SIGS(I)/(SIGS(I)+SIGA(I))

TPOT=GTRAN(3)\*(SIGS(I)+SIGA(I))

EF1=F3(TPOT)

EF2=F3(TPOT+TPOT)

TPK=(1.0-EF2-EF1)/TPOT

TPF=(EF2-EF1-EF1+0.5)/(TPOT+TPOT)

TFAC(I)=1.0-(RD\*(1.0-TPA)\*TPOT\*TPK)/(1.0-TPA\*TPF)

5 CONTINUE

RETURN

END(0,0,0)

\* 657 SUBROUTINE PLATE

C SUBROUTINE PLATE

C COMMON Q

C DIMENSION Q(13764)

C DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),  
 1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),  
 2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),  
 3NCODE(10),RNDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),  
 4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),  
 5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),  
 6DIFFR(25),DIFFZ(25),Sigr(25),S(25),FXTRAP(25),  
 7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),  
 8TRASIG(25,25),RES(1000),ENGAM(34,18)

C EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),BNAM),  
 1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),  
 2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),  
 3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),  
 4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),  
 5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),  
 6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),  
 7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),  
 8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),  
 9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)

C EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),  
 1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),  
 2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),  
 3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),Sigr),(Q(10858),S),  
 4(Q(10883),TM), (Q(10884),EXTRAP),(Q(10909),EPSR),  
 5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),  
 6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),  
 7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRFS),(Q(13133),ENGAM),  
 8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),  
 9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)

C DO 5 I=1,25  
 TPA=SIGA(I)/SIGS(I)  
 TPOT=GTRAN(1)\*(SIGS(I)+SIGA(I))  
 TFAC(I)=1.0-2.0\*TPA\*TPOT\*E3COMP(TPOT)/  
 1(TPA\*TPOT+E3COMP(TPOT))  
 5 CONTINUE  
 RETURN  
 END(0,0,0)

\* 657 SUBROUTINE GRPAR

SUBROUTINE GRPAR

C  
COMMON Q

C  
DIMENSION Q(13764)

C  
DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),  
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),  
2TMAT(30),NBEHR(30),GVOL(3),GREHR(4),GTRAN(3),GDIFC(3),  
3NCODF(10),RNDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),  
4DELTAU(25),SIG(25),SIGTR(25),SIGA(25),SIGFN(25),  
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),  
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),  
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),  
8TRASIG(25,25),RES(1000),ENGAM(34,18)

C  
EQUIVALENCE (Q(2),BDATF),(Q(6),BDENT),(Q(9),BNAM),  
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),  
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),  
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),  
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),  
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),  
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),  
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),  
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),  
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)

C  
EQUIVALENCE (Q(9358),SIG(5)),(Q(9383),SIGTR),(Q(9408),SIGA),  
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),  
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),  
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),  
4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),EPSR),  
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),  
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),  
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),  
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),  
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)

C  
DIMENSION CAPPA(25)

C  
DO 60 I=1,25  
IF (GDIFC(I)) 10, 5, 10  
5 CONTINUE  
DIFFC(I)=1.0/(3.0\*(SIGTR(I)+SIGA(I)))  
GO TO 50  
10 CONTINUE  
EXTRAP(I)=0.71050/(SIGTR(I)+SIGA(I))  
NST=NCODE(I)+1  
GO TO (15,20,25), NGT  
15 CONTINUE  
CAPPA(I)=9.87/(GDIFC(1)+2.0\*EXTRAP(I))\*\*2+  
19.87/(GDIFC(2)+2.0\*EXTRAP(I))\*\*2+9.87/(GDIFC(3)+2.0\*EXTRAP(I))\*\*2  
GO TO 30

```
20 CONTINUE
  CAPP(A(I))=9.87/(GDIFC(1)+2.0*EXTRAP(I))**2+
  123.13/(GDIFC(2)+2.0*EXTRAP(I))**2
  GO TO 30
25 CONTINUE
  CAPP(A(I))=9.87/(GDIFC(1)+EXTRAP(I))**2
30 CONTINUE
  ALPH=CAPP(A(I))/(SIGS(I)+SIGA(I))**2
  IF (ALPH-1.0E-11) 35, 40, 40
35 CONTINUE
  EPS=0.0
  GO TO 45
40 CONTINUE
  EPS=0.26001*ALPH+0.043502*ALPH**2+0.0048942*ALPH**3
45 CONTINUE
  DIFFC(I)=1.0/(3.0*(SIGTR(I)+SIGA(I)+EPS*(SIGS(I)+SIGA(I))))
50 CONTINUE
  DIFFR(I)=(1.0+EPSR(I))*DIFFC(I)
  DIFFZ(I)=(1.0+EPSZ(I))*DIFFC(I)
  SIGR(I)=SIGA(I)+SIGS(I)-SIGST(I,I)
  SIGST(I,I)=0.0
60 CONTINUE
  RETURN
  END(0,0,0)
```



```

*      657              SUBROUTINE WTCD
C
SUBROUTINE WTCD
C
COMMON Q
C
DIMENSION Q(13764)
C
DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NRFHR(30),GVOL(3),GREHR(4),GTRAN(3),GDIFC(3),
3NCODE(10),RNDT(2000),NRNDT(2000),IMAT(30),FG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
EQUIVALENCE (Q(2),RDATA),(Q(6),RDATA),(Q(9),BNAM),
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GREHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)
C
EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
IF (CDT(1)) 10, 5, 10
5 CONTINUE
CDT(1)=CDTNAM(1)
CDT(2)=CDTNAM(2)
NRCDT=1
10 CONTINUE
NN=NRCDT+(NRCDT-1)/2+3
CDT(NN)=CASEID
CDT(NN+1)=CASID
NCDT(NN+2)=NRCDT
WRITE TAPE KDT, (DIFFR(I),DIFFZ(I),SIGR(I),SIGFN(I),
1S(I),I=1,25),(SIGST(I,J),J=1,25),I=1,25)
NRCDT=NRCDT+1
IF (NCODE(4)) 20, 20, 15
15 CONTINUE

```

```
WRITE TAPE KDT, ((SIGNG(I,J),J=1,18),I=1,25)  
GO TO 25  
20 CONTINUE  
WRITE TAPE KDT, SIGNG(1,1)  
25 CONTINUE  
NRCDT=NRCDT+1  
RETURN  
END(0,0,0)
```

```

*      657              SUBROUTINE WOTCD
C
C      SUBROUTINE WOTCD
C
C      COMMON Q
C
C      DIMENSION Q(13764)
C
C      DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),
2TMAT(30),NBEHR(30),GVOL(3),GREHR(4),GTRAN(3),GDIFC(3),
3NCOD:(10),RNDDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),
8TRASIG(25,25),RES(1000),ENGAM(34,18)
C
C      EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),BNAM),
1(Q(11),CASEID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),
4(Q(326),NRCDDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GREHR),(Q(7234),GTRAN),
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),
8(Q(7252),VCOMP),(Q(7253),RNDDT,NRNDT),(Q(9253),NREC),
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)
C
C      EQUIVALENCE (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),
1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),
4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),EPSR),
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)
C
C      CALL WOT(NWOT)
C      PRINT 1000
C      IF (NCODE(1)-1) 5, 10, 15
C
C      5 CONTINUE
C      PRINT 1001
C      PRINT 2001, GVOL(1),GVOL(2),GVOL(3)
C      GO TO 20
C
C      10 CONTINUE
C      PRINT 1002
C      PRINT 2002, GVOL(1),GVOL(2),GVOL(3)
C      GO TO 20
C
C      15 CONTINUE
C      PRINT 1003
C      PRINT 2003, GVOL(1)
C
C      20 CONTINUE

```

```
IF (NCODE(2)-1) 25, 30, 35
25 CONTINUE
   PRINT 1005
   GO TO 40
30 CONTINUE
   PRINT 1006
   GO TO 32
35 CONTINUE
   PRINT 1007
32 CONTINUE
   IF (GBEHR(4)) 33, 34, 33
33 CONTINUE
   PRINT 2006, GREHR(1),GBEHR(2),GREHR(3),GREHR(4)
   GO TO 40
34 CONTINUE
   PRINT 2007, GREHR(1),GRFHR(2),GRFHR(3)
40 CONTINUE
   NGT=NCODE(3)+1
   GO TO (45,50,55,60), NGT
45 CONTINUE
   PRINT 1010
   GO TO 65
50 CONTINUE
   PRINT 1011
   GO TO 61
55 CONTINUE
   PRINT 1012
   GO TO 61
60 CONTINUE
   PRINT 1013
61 CONTINUE
   IF (NCODE(3)-2) 62, 63, 64
62 CONTINUE
   PRINT 2011, GTRAN(1),GTRAN(2)
   GO TO 65
63 CONTINUE
   PRINT 2012, GTRAN(1),GTRAN(2),GTRAN(3)
   GO TO 65
64 CONTINUE
   PRINT 2013, GTRAN(1)
65 CONTINUE
   IF (NCODE(4)) 70, 70, 75
70 CONTINUE
   PRINT 1015
   GO TO 80
75 CONTINUE
   PRINT 1016
80 CONTINUE
   IF (NCODE(5)) 90, 85, 90
85 CONTINUE
   PRINT 1020
   GO TO 95
90 CONTINUE
   PRINT 1021
95 CONTINUE
```

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      IF (GDIFC(1)) 96, 100, 96
96 CONTINUE
  PRINT 1022
      IF (NCODE(1)-1) 97, 98, 99
97 CONTINUE
  PRINT 1023, GDIFC(1),GDIFC(2),GDIFC(3)
  GO TO 100
98 CONTINUE
  PRINT 1024, GDIFC(1),GDIFC(2)
  GO TO 100
99 CONTINUE
  PRINT 1025, GDIFC(1)
100 CONTINUE
  PRINT 1026, VCOMP,SPEC
  PRINT 1030
  DO 110 I=1,30
    IF (CMAT(I)) 105, 110, 105
105 CONTINUE
  PRINT 1031, CMAT(I),WMAT(I),DMAT(I),TMAT(I),NBEHR(I)
110 CONTINUE
  IF (NCODE(7)-1) 111, 115, 138
111 CONTINUE
  DO 114 J=1,25
    K=26 J
    DO 113 I=1,30
      IF (CMAT(I)) 112, 113, 112
112 CONTINUE
      IF (GFAC(K,I)-1.0) 115, 113, 115
113 CONTINUE
114 CONTINUE
  PRINT 1034
  GO TO 130
115 CONTINUE
  I1=0
  I2=0
  DO 120 K=1,6
    I1=I2+1
    I2=5*K
    PRINT 1035, (CMAT(I),I=I1,I2)
    PRINT 1036, (I,(GFAC(I,J),J=I1,I2),I=1,25)
    IF (CMAT(5*K+1)) 120, 130, 120
120 CONTINUE
130 CONTINUE
  IF (NCODE(7)-1) 132, 131, 138
131 CONTINUE
  PRINT 1040, (I,EG(I),DELTAU(I),FV(I),I=1,24)
  PRINT 1041, EG(25),DELTAU(25)
132 CONTINUE
  IF (NCODE(2)) 134, 133, 134
133 CONTINUE
  IF (NCODE(3)) 134, 135, 134
134 CONTINUE
  PRINT 1045, (I,TFAC(I),EPSR(I),EPSZ(I),BFSIG(I),BMSIG(I),I=1,25)
135 CONTINUE
  IF (NCODE(7)-1) 138, 136, 138

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136 CONTINUE
PRINT 1050, (I,DIFFC(I),SIGS(I),SIGTR(I),SIGA(I),EXTRAP(I),I=1,25)
138 CONTINUE
PRINT 1055, (I,DIFFR(I),DIFFZ(I),SIGR(I),SIGFN(I),S(I),I=1,25)
IF (NCODE(7)-1) 139, 139, 170
139 CONTINUE
DO 140 J=1,25,5
J1=J 1
J2=J 2
J3=J 3
J4=J 4
PRINT 1060, J,J1,J2,J3,J4,(I,SIGST(I,J),SIGST(I,J1),SIGST(I,J2),
1SIGST(I,J3),SIGST(I,J4),I=1,25)
140 CONTINUE
IF (NCODE(4)) 170, 170, 150
150 CONTINUE
DO 160 J=1,15,5
J1=J 1
J2=J 2
J3=J 3
J4=J 4
PRINT 1065, J,J1,J2,J3,J4,(I,SING(I,J),SING(I,J1),SING(I,J2),
1SING(I,J3),SING(I,J4),I=1,25)
160 CONTINUE
170 CONTINUE
RETURN
C
1000 FORMAT(1H1//18X,34H COMPOSITION DATA PREPARATION //29H CALCUL
ATION REQUEST SUMMARY)
C
1001 FORMAT(/17H GEOMETRY - SLAB)
C
2001 FORMAT(6H X = 1PE12.5,7H Y = 1PE12.5,7H Z = 1PE12.5)
C
1002 FORMAT(/21H GEOMETRY - CYLINDER)
C
2002 FORMAT(6H H = 1PE12.5,8H OD = 1PE12.5,8H ID = 1PE12.5)
C
1003 FORMAT(/19H GEOMETRY - SPHERE)
C
2003 FORMAT(6H R = 1PE12.5)
C
1005 FORMAT(24H NO BEHRENS CALCULATION)
C
1006 FORMAT(31H ISOTROPIC BEHRENS CALCULATION)
C
2006 FORMAT(7H LF = 1PE12.5,7H LM = 1PE12.5,7H VF = 1PE12.5,6H Q =
11PE1,5)
C
1007 FORMAT(33H ANISOTROPIC BEHRENS CALCULATION)
C
2007 FORMAT(7H D1 = 1PE12.5,8H D2 = 1PE12.5,8H D3 = 1PE12.5)
C
1010 FORMAT(29H NO TRANSMISSION CALCULATION)
C

```

1011 FORMAT(30H ROD TRANSMISSION CALCULATION)  
 C  
 2011 FORMAT(6H D = 1PE12.5,9H DCH = 1PE12.5)  
 C  
 1012 FORMAT(34H ANNULUS TRANSMISSION CALCULATION)  
 C  
 2012 FORMAT(7H OD = 1PE12.5,9H DCH = 1PE12.5,7H T = 1PE12.5)  
 C  
 1013 FORMAT(32H PLATE TRANSMISSION CALCULATION)  
 C  
 2013 FORMAT(6H T = 1PE12.5)  
 C  
 1015 FORMAT(29H NO GAMMA SOURCE CALCULATION)  
 C  
 1016 FORMAT(26H GAMMA SOURCE CALCULATION)  
 C  
 1020 FORMAT(41H NO RESONANCE SELF-SHIELDING CALCULATION)  
 C  
 1021 FORMAT(38H RESONANCE SELF-SHIELDING CALCULATION)  
 C  
 1022 FORMAT(59H GEOMETRY FOR SIZE CORRECTION TO THE DIFFUSION COEFFICIENT)  
 C  
 1023 FORMAT(9H X+2S = 1PE12.5,9H Y+2S = 1PE12.5,9H Z+2S = 1PE12.5)  
 C  
 1024 FORMAT(9H H+2S = 1PE12.5,10H D+2S = 1PE12.5)  
 C  
 1025 FORMAT(8H R+S = 1PE12.5)  
 C  
 1026 FORMAT(/29H COMPOSITION VOLUME IN CC - 1PF13.6/34H COMPOSITION SPECTRUM CODE NO. - 0PF9.4)  
 C  
 1030 FORMAT (/10H MATERIAL5X,8HMATERIAL6X,10HDENSITY OR4X,8HMATERIAL51X,7HREHRENS/10H CODE NO.6X,6HWEIGHT5X,15HVOLUME FRACTION3X,4HTEMP26X,10HREGION NO./)  
 C  
 1031 FORMAT(0PF11.4,1P2E15.6,0PF10.2,I9)  
 C  
 1034 FORMAT(////60H CELL CORRECTIONS FOR ALL MATERIALS AT ALL LEVELS AIRE UNITY)  
 C  
 1035 FORMAT(1H1///23X,25HMATERIAL CPLL CORRECTIONS///10X,8HCODE NO.5X,81HCODE NO.5X,8HCODE NO.5X,8HCODE NO.5X,8HCODE NO.//0PF18.4,0P4F13.4?)  
 C  
 1036 FORMAT(///7H GROUP3X,8HG-FACTOR5X,8HG-FACTOR5X,8HG-FACTOR5X,8HGFACTOR5X,8HG-FACTOR//(I6,1PE14.5,1P4E13.5))  
 C  
 1040 FORMAT(1H1///7H GROUP4X,6HENERGY6X,8HDELTA(U)3X,11H1/V-FACTORS/(I16,1PE14.5,0PE13.5,1PE13.5))  
 C  
 1041 FORMAT(6H 251PF14.5,1PE13.5)  
 C  
 1045 FORMAT(1H1///8X,63HTRANSMISSION BEHRENS FAC. BEHRENS FAC. BEHRENS FUEL BEHRENS MOD/7H GROUP3X,7HFACTORS7X,6HRADIAL4X,12HLONGITUDINA

2L3X,9HX-SECTION4X,9HX-SECTION//((I6,1PE14.5,1P4E13.5))

C  
1050 FORMAT(1H1///23X,26HCOMPOSITION CROSS SECTIONS///18H GROUP DIFFU  
SION5X,7HSCATTER5X,9HTRANSPORT4X,24HABSORPTION EXTRAPOLATION//((I6,  
21PE14.5,1P4E13.5))

C  
1055 FORMAT(1H1///22X,28HCOMPOSITION GROUP PARAMETERS///9X,9HDIFFUSION4  
1X,9HDIFFUSION5X7HREMOVAL/7H GROUP3X,6HRADIAL5X,24HLONGITUDINAL (A  
2BSP+SCAT)4X,7HFISSION7X,6HSOURCE//((I6,1PE14.5,1P4E13.5))

C  
1060 FORMAT(1H1///18X,35HCOMPOSITION SCATTER TRANSFER MATRIX///7X,2HTOI  
15,4I13/5H FROM/(I4,1PE15.5,1P4E13.5))

C  
1065 FORMAT(1H1///18X,35HCOMPOSITION N-GAMMA TRANSFER MATRIX///7X,2HTOI  
15,4I13/5H FROM/(I4,1PE15.5,1P4E13.5))

C  
FND



\* 657 SUBROUTINE ENDCDP

SUBROUTINE ENDCDP

C

COMMON Q

C

DIMENSION Q(13764)

C

DIMENSION CDT(303),NCDT(303),CDTNAM(2),ELFAC(1500,4),  
 1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),  
 2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),  
 3NCODF(10),RNDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),  
 4DELTAU(25),SIGG(25),SIGTR(25),SIGA(25),SIGFN(25),  
 5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),  
 6DIFFR(25),DIFFZ(25),SIGR(25),S(25),EXTRAP(25),  
 7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),  
 8TRASIG(25,25),RES(1000),ENGAM(34,18)

C

EQUIVALENCE (Q(2),BDATE),(Q(6),BDENT),(Q(9),BNAM),  
 1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),  
 2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),  
 3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),  
 4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),  
 5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),  
 6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),  
 7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),  
 8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),  
 9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)

C

EQUIVALENCE (Q(9358),SIGG),(Q(9383),SIGTR),(Q(9408),SIGA),  
 1(Q(9433),SIGFN),(Q(9458),BFSIG),(Q(9483),BMSIG),  
 2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),  
 3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),  
 4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),FPSR),  
 5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),  
 6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),  
 7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),  
 8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),  
 9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)

C

NCO=(NRCDT-1)/2  
 NCDT(3)=NRCDT  
 WRITE TAPE KDT, (CDT(I),I=1,303)  
 END FILE KDT  
 REWIND KDT  
 CALL WOT(NWOT)  
 CASEID=CDT(1)  
 CASID=CDT(2)  
 CALL HDING(Q(12))  
 MI=3 3\*NCO  
 PRINT 1000, NCDT(1),NCDT(2),NCO,NCDT(3),(NCDT(I),I=4,MI)  
 RETURN

000 FORMAT(1H1///30X,12HINDEX RECORD//18X,22HCOMPOSITION DATA TAPE 2A6  
 1///121,20H COMPOSITIONS 13,8H RECORDS//18X,11HDESIGNATION13

2X,10HRECORD NO.//(18X,2A6,I18))

C

END(n,0,0)

---

SUBROUTINE ERRCDP

---

C  
COMMON Q

---

C  
DIMENSION Q(13764)

---

C  
DIMENSION CDT(303),NCDT(303),CDTNAM(2),FLFAC(1500,4),  
1RDATA(1500,4),GFAC(25,30),CMAT(30),DMAT(30),WMAT(30),  
2TMAT(30),NBEHR(30),GVOL(3),GBEHR(4),GTRAN(3),GDIFC(3),  
3NCODE(10),RNDT(2000),NRNDT(2000),IMAT(30),EG(25),FV(24),  
4DELTAU(25),SIGS(25),SIGTR(25),SIGA(25),SIGFN(25),  
5BFSIG(25),BMSIG(25),SIGST(25,25),SIGNG(25,25),DIFFC(25),  
6DIFFR(25),DIFFZ(25),SIGR(25),S(25),FXTRAP(25),  
7EPSR(25),EPSZ(25),TFAC(25),SIG(520),NSIG(520),  
8TRASIG(25,25),RES(1000),ENGAM(34,18)

---

C  
EQUIVALENC (Q(2),RDATA),(Q(6),RDEMT),(Q(9),RNAM),  
1(Q(11),CASID),(Q(12),CASEID),(Q(13),CDT,NCDT),(Q(316),NPAGE),  
2(Q(317),NWOT),(Q(318),NDT),(Q(319),KDT),(Q(320),ITAPE),  
3(Q(321),JTAPE),(Q(322),KTAPE),(Q(323),MORE),(Q(324),CDTNAM),  
4(Q(326),NRCDT),(Q(327),ELFAC,RDATA),(Q(6327),GFAC),  
5(Q(7077),CMAT),(Q(7107),DMAT),(Q(7137),WMAT),(Q(7167),TMAT),  
6(Q(7197),NBEHR),(Q(7227),GVOL),(Q(7230),GBEHR),(Q(7234),GTRAN),  
7(Q(7237),GDIFC),(Q(7240),SPEC),(Q(7241),NCODE),(Q(7251),KASE),  
8(Q(7252),VCOMP),(Q(7253),RNDT,NRNDT),(Q(9253),NREC),  
9(Q(9254),IMAT),(Q(9284),EG),(Q(9309),FV),(Q(9333),DELTAU)

---

C  
EQUIVALENC (Q(9358),SIGS),(Q(9383),SIGTR),(Q(9408),SIGA),  
1(Q(9433),SIGFN),(Q(9458),RFSIG),(Q(9483),BMSIG),  
2(Q(9508),SIGST),(Q(10133),SIGNG),(Q(10758),DIFFC),  
3(Q(10783),DIFFR),(Q(10808),DIFFZ),(Q(10833),SIGR),(Q(10858),S),  
4(Q(10883),TM),(Q(10884),EXTRAP),(Q(10909),EPSR),  
5(Q(10934),EPSZ),(Q(10959),TFAC),(Q(10984),SIG,NSIG),  
6(Q(11504),TRASIG),(Q(12129),MOMIN),(Q(12130),MOMAX),  
7(Q(12131),MOPMAX),(Q(12132),RES),(Q(13132),NRES),(Q(13133),ENGAM),  
8(Q(13758),MGMIN),(Q(13759),MGMAX),(Q(13760),MGPMAX),  
9(Q(13761),DF),(Q(13762),NW),(Q(13763),NTM),(Q(13764),MN)

---

C  
5 CONTINUE

---

CALL WOT(NWOT)

CASEID=CDT(1)

CASID=CDT(2)

CALL HDING(Q(12))

NCO=(NRCDT-1)/2

NCDT(3)=NRCDT

WRITE TAPE KDT, (CDT(I),I=1,303)

END FILE KDT

REWIND KDT

10 CONTINUE

MI=3 3\*NCO

PRINT 1000, NCDT(1),NCDT(2),NCO,NCDT(3),(NCDT(I),I=4,MI)

CALL EXIT

RETURN

---

```
C  
1000 FORMAT(1H1///30X,12HINDEX RECORD//18X,22HCOMPOSITION DATA TAPE 2A6  
1///I?1,20H COMPOSITIONS I3,8H RECORDS///18X,11HDESIGNATION13  
2X,10HRECORD NO.//(18X,2A6,I18))  
C  
END(0,0,0)
```

657

## FUNCTION RSS

FUNCTION RSS(TAU,THETA)

```

C
C THIS PROGRAM COMPUTES THE SELF-SHIELDING FACTORS
C FOR A RESONANCE ABSORBING SLAB
C THIS ROUTINE REQUIRES THE ENCLOSURE OF
C ERROR,SQRT,EXP,E3COMP,E3,LOG,PSI,SIN,COS
C

```

DIMENSION A(15),H(15)

```

C
A(1)=0.095012510
A(2)=0.28160355
A(3)=0.45801678
A(4)=0.61787624
A(5)=0.75540441
A(6)=0.86563120
A(7)=0.94457502
A(8)=0.98940093
A(9)=0.19304368
A(10)=1.0266649
A(11)=2.5678767
A(12)=4.9003531
A(13)=8.1821534
A(14)=12.734180
A(15)=19.395728

```

```

C
H(1)=0.18945061
H(2)=0.18260342
H(3)=0.16915652
H(4)=0.14959599
H(5)=0.12462897
H(6)=0.095158512
H(7)=0.062253524
H(8)=0.027152459
H(9)=0.40931895
H(10)=0.42183128
H(11)=0.14712635
H(12)=0.20633514E-1
H(13)=0.10740101E-2
H(14)=0.15865464E-4
H(15)=0.31703155E-7

```

```

C
IF(TAU) 100,105,110
100 CALL ERROR
105 RSS=1.0
GO TO 50
110 CONTINUE

```

```

C
XHALF= 1.0+(1.5+0.01*THETA)*SQRT(TAU+THETA)

```

```

C
SUM=0
DO 15 J=1,5
VALU:=0
DO 12 N=1,8

```

---

```
VALUE=VALUE+H(N)*E3COMP(TAU*PSI(THETA,XHALF*(A(N)+FLOATF(J-1))))
```

```
12 CONTINUE  
SUM=SUM+VALUE*XHALF
```

---

```
15 CONTINUE  
VALUE=0
```

---

```
DO 20 N=9,15
```

```
VALUE=VALUE+EXPF(A(N))*H(N)*F3COMP(TAU*PSI(THETA,A(N)+5.0*XHALF))
```

---

```
20 CONTINUE  
RSS=((VALUE+SUM)*0.63661977)/TAU
```

---

```
C
```

```
50 CONTINUE  
RETURN  
END(0,0,0)
```

---

```

*      657              FUNCTION PSI
-----
      FUNCTION PSI(THETA,DELTA)
C
C      THIS PROGRAM COMPUTES THE DOPPLER BROADENING
C      FUNCTION FOR NEUTRON ABSORPTION CROSS SECTIONS
C      THIS ROUTINE REQUIRES THE ENCLOSURE OF
C      ERROR,SQRT,EXP,LOG,SIN,COS
C
      DIMENSION XK120(101)
C
      IF(THETA-0.20) 6,6,14
C
      6 SUM1=THETA/50.0
      SUM2=SQRTF(SUM1+SUM1)
      XK120(1)=DELTA 50.0*SUM2
      DO 7 M=1,100
      XK120(M+1)=XK120(1)+FLOATF(M)*SUM2
      7 CONTINUE
C
      DO 8 M=1,101
      XK120(M)=1.0/(1.0+XK120(M)*XK120(M))
      8 CONTINUE
C
      MAX=99
      9 DO 10 M=1,MAX
      XK120(M)=0.5*(XK120(M)+XK120(M+2))
      10 CONTINUE
      IF(MAX-1) 13,13,11
      11 MAX=MAX-2
      GO TO 9
      13 CONTINUE
      PSI=XK120(1)
      GO TO 220
C
      14 CONTINUE
C
      T100=SQRTF(THETA)
      T200=2.0*THETA
      T400=4.0*THETA
      X100=DELTA/(2.0*T100)
      X110=X100*X100
      X200=X100/T100
      X300=EXPF(-X110)
C
      IF(THETA-2.0) 150,160,160
      150 SUM1=26.25*LOGF(1.0+THETA-0.05*THETA**2-0.01*THETA**3)
      IF(DELTA-SUM1) 170,155,155
      155 PSI=(1.0/(1.0+DELTA*DELTA))*EXPF(6.0*THETA/(1.0+DELTA*DELTA))
      GO TO 220
      160 SUM1=18.75*SQRTF(THETA)
      IF(DELTA-SUM1) 170,155,155
      170 CONTINUE
C
C      COMPUTE SERIES NUMBER 1
-----

```

```

C
SUM1=-1.0/T200
EN=2.0
UTERM=SUM1/(T200*(2.0*EN-1.0))
12 SR1=SUM1+UTERM
IF(ARSF(SUM1/SR1-1.0)-0.00000001) 20,20,15
15 SUM1=SR1
EN=EN+1.0
UTERM=UTERM/(T200*(2.0*EN-1.0))
GO TO 12
20 CONTINUE

C
IF(DFLTA) 24,22,24

C
22 SR2=0
SR3=0
SR4=0
SR5=0
GO TO 120

C
24 CONTINUE

C
COMPUTE SERIES NUMBER 2

C
XTERM=-1.0
AMOUNT=0
USTART=1.0/T200
DO 50 M=1,1000
FM=FLOATF(M)
USTART=USTART/(T200*(2.0*EM+1.0))
SUM1=USTART
EN=EM+1.0
UTERM=USTART/(T200*(2.0*EN+1.0))
25 SUM2=SUM1+UTERM
IF(ARSF(SUM1/SUM2-1.0)-0.00000001) 40,40,30
30 SUM1=SUM2
EN=EN+1.0
UTERM=UTERM/(T200*(2.0*EN+1.0))
GO TO 25
40 XTERM=(-XTERM*X110)/FM
VALUE=XTERM*SUM2
SR2=AMOUNT+VALUE
IF(ARSF(ARSF(AMOUNT/SR2) 1.0)-0.00000001) 55,55,45
45 AMOUNT=SR2
50 CONTINUE
55 CONTINUE

C
COMPUTE SERIES NUMBER 3

C
SUM1=1.0
FN=1.0
UTERM=1.0/T400
58 SR3=SUM1+UTERM
IF(ARSF(SUM1/SR3-1.0)-0.00000001) 65,65,60
60 EN=EN+1.0

```



```

SUM1=SR3
UTERM=UTERM/(T400*EN)
GO TO 58
65 CONTINUE
C
C COMPUTE SERIES NUMBER 4
C
SUM1=X100
EN=1.0
UTERM=((2.0*EN 1.0)/(EN*(2.0*EN+1.0)))*X110*SUM1
70 SR4=SUM1+UTERM
IF(ARSF(SUM1/SR4-1.0)-0.00000001) 75,75,73
73 EN=EN+1.0
SUM1=SR4
UTERM=((2.0*EN 1.0)/(EN*(2.0*EN+1.0)))*X110*UTERM
GO TO 70
75 CONTINUE
C
C COMPUTE SERIES NUMBER 5
C
XTERM=X100/X110
AMOUNT=0
USTART=0.5
DO 100 M=1,1000,2
EM=FLOATF(M)
USTART=USTART/(EM*(EM+1.0)*THETA)
SUM1=USTART
EN=0.5*(EM+1.0)+1.0
UTERM=USTART/(T400*EN)
78 SUM2=SUM1+UTERM
IF(ARSF(SUM1/SUM2-1.0)-0.00000001) 85,85,80
80 EN=EN+1.0
SUM1=SUM2
UTERM=UTERM/(T400*EN)
GO TO 78
85 XTERM=-XTERM*X110
VALUE=XTERM*SUM2
SR5=AMOUNT+VALUE
IF(ARSF(ARSF(AMOUNT/SR5) 1.0)-0.00000001) 105,105,90
90 AMOUNT=SR5
100 CONTINUE
105 CONTINUE
C
120 CONTINUE
C
PSI=((0.88622695*X300*EXPF(1.0/T400)+T100*
1(SR1 SR2))*COSF(X200)+(X300*SR3*SR4+SR5)*
2SINF(X200))/T100
C
220 CONTINUE
C
RETURN
END(0,0,0)

```

```

*      CHAIN(2,B1)                BLOCK FDP
C
*      657          CONTROL PROGRAM - FDP
C
C      PROGRAM FPREP          THOMAS A HOFFMAN
C      THIS PROGRAM IS PART OF THE REACTOR PHYSICS ONE DIMENSIONAL
C      DIFFUSION CALCULATION-PROGRAM ODD-ANP NO. 657
C
C      COMMON FOR PROGRAM FPREP
C      COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPF,JTAPF,KTAPF,MORE,D,COMP,
1REG,NMIX,R,EN,HE,FFFV,ALFT,ARGT,LMAX,EPSK,NCODE,SFXM,SEXP,
2FM,FP,NR,TEMP,NRSAV,NRPRES,NTWORD,N1WORD,N2WORD,NOGPS,NOGPCN,
3NCOMP,NRSPAS,JSAIR
C
C      DIMENSION FOR PROGRAM FPREP
C      DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN
1(100),HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SEXM(150),
2SEXP(150),FM(150),FP(150),NR(20),TEMP(1000),NCDT(303)
C
C      EQUIVALENCE FOR FPREP
C      EQUIVALENCE (Q(12),CASID),(Q(9),RNAME),(Q(6),BDENT),(Q(2),BDATE),
1(CDT,NCDT)
C
C      BEGIN EXECUTABLE PART OF PROGRAM FPREP
C
C      PRESFT VALUES FOR NUMBFR OF ITERATIONS, CONVERGENCE FACTOR,
C      WRITE OUTPUT CONTROL, NUMBER OF GROUPS AND NUMBER OF TYPES
C      OF GROUP CONSTANTS
C
C      SENSE LIGHT 0
C      IF (MORE) 1, 500, 502
500 CONTINUE
C      GO TO 900
502 CONTINUE
C      SENSE LIGHT 3
C      GO TO 2
1 CONTINUE
C      LMAX=99
C      EPSK=1.0E-7
C      NWOT=2
C
C      PRESFT FISSION DENSITIFS LEFT AND RIGHT TO ONE
C
300 DO 301 I=1,150
C      FM(I)=1.0
C      FP(I)=1.0
301 CONTINUE
C
C      SET PAGE NUMBERING
C
2 CALL NEWSET (NPAGE+1)
C      NOGPS=25
C      NOGPCN=5
C
C      READ INPUT DATA

```

```

3 CONTINUE
  READ DIP CASEID,CDT,NDT,ITAPF,JTAPF,KTAPF,MORF,COMP,REG,NMIX,
  IR,EN,HE,EFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SEXM,SFXP,FM,FP,NWOT,NOGPS,
  2NOGPCN,KDT,FND
  IF (SENSE LIGHT 1) 900,4
C
C   SET PAGE HEADING AND WRITE OUTPUT CONTROL
C
4 CALL HDING (Q(12))
  CALL WOT(NWOT)
C
C   BEGIN INPUT CONSISTENCY CHECK,PRESET ERROR INDICATOR
C
5 ISAIR=0
  PRINT 6
6 FORMAT (1H1)
  IF (NCODE(1)) 7,8,9
7 PRINT 10
10 FORMAT (6X,43HTHE NUMBER OF REGIONS IS A NEGATIVE NUMBER.)
  GO TO 900
8 PRINT 11
11 FORMAT (6X,30HTHE NUMBER OF REGIONS IS ZERO.)
  GO TO 900
9 IF (NCODE(1)-100) 100,100,13
13 PRINT 14
14 FORMAT (6X,47HTHE NUMBER OF REGIONS IS MORE THAN ONE HUNDRED.)
  GO TO 900
C
C   DETERMINE NUMBER OF COMPOSITIONS
C
100 NCOMP=0
  J=1
  DO 101 I=1,20
    IF (COMP(J)) 102,103,102
102 NCOMP=NCOMP+1
  J=J+2
101 CONTINUE
103 IF (NCOMP) 104,105,12
104 PRINT 106
106 FORMAT (6X,62HTHE NUMBER OF COMPOSITIONS IS CALCULATED AS A NEGATI
  IVE NUMBER.)
  GO TO 900
105 PRINT 107
107 FORMAT (6X,49HTHE NUMBER OF COMPOSITIONS IS CALCULATED AS ZERO.)
  GO TO 900
C
C   CHECK REGIONAL AGAINST COMPOSITION DATA
C
12 CALL REGCK (8H MIX ,NCODE,NCOMP,REG,COMP,ISAIR)
C
C   CHECK COMPOSITION AGAINST INDEX DATA
C
24 I=NCNT(3)
  J=1

```

```

DO 25 K=1,NCOMP
L=4
DO 26 M=1,I
IF ((COMP(J)-CDT(L))+(COMP(J+1)-CDT(L+1))) 27,28,27
27 L=L+1
26 CONTINUE
ISAIP=1
PRINT 29,COMP(J),COMP(J+1)
29 FORMAT (6X,12HCOMPOSITION 2A6,38H NOT PRESENT ON COMPOSITION DATA
1TAPF.)
28 J=J+1
25 CONTINUE
C
C CHECK NUMBER OF MIXABLES WITH NUMBER OF COMPOSITIONS
C
30 IF (NMIX-NCOMP) 33,33,31
31 PRINT 32,NMIX,NCOMP
32 FORMAT (6X,I2,60H COMPOSITIONS TO BE MIXED. MAXIMUM ALLOWABLE IN T
1HIS CASE IS I3,1H.)
ISAIP=1
C
C CHECK NUMBER OF RADII WITH NUMBER OF REGIONS
C
33 J=0
I1=NCODE(1)
DO 34 I=1,I1
IF (R(I+1)) 35,36,35
35 J=J+1
34 CONTINUE
36 IF (J-NCODE(1)) 37,38,37
37 ISAIP=1
PRINT 39,NCODE(1),J
39 FORMAT (6X,21HNUMBER OF REGIONS IS I3,20H.NUMBER OF RADII IS I3,16
1H PLUS INNERMOST.)
C
C CHECK IF RADII ARE MONOTONICALLY INCREASING
C
38 A=R(J)
I1=NCODE(1)
DO 40 I=1,I1
J=I-1
IF (A-R(I+1)) 41,42,42
42 PRINT 44,J,A,I,R(I+1)
44 FORMAT (6X,7HREGION I3,8H RADIUS=IPE12.7,9H, REGION I3,8H RADIUS=IPE
1F12.7,1H.)
ISAIP=1
41 A=R(I)
40 CONTINUE
C
C CHECK NUMBER OF DIMENSIONS WITH NUMBER OF REGIONS
C
47 J=0
I1=NCODE(1)
DO 48 I=1,I1
IF (HF(I)) 49,50,49

```

```

49 J=J+1
48 CONTINUE
50 IF (NCODE(1)-J) 51,52,51
51 PRINT 53,J,NCODE(1)
53 FORMAT (6X,28HNUMBER OF DIMENSIONS EQUALS I3,26H NUMBER OF REGIONS
1 EQUALS I3,1H.)
   ISAIR=1
C
C CHECK NUMBER OF INTERVALS WITH NUMBER OF REGIONS
C
52 J=0
   I1=NCODE(1)
   DO 54 I=1,I1
     IF (FN(I)) 55,56,55
55 J=J+1
54 CONTINUE
56 IF (NCODE(1)-J) 57,401,57
57 PRINT 59,J,NCODE(1)
59 FORMAT (6X,30HNUMBER OF SETS OF INTERVALS = I3,22H, NUMBER OF REGI
IONS = I3,1H.)
C
C CHECK TOTAL NUMBER OF INTERVALS
C
401 TOTAL=0.0
   I1=NCODE(1)
   DO 400 I=1,I1
     TOTAL=TOTAL+ARSF(EN(I))
400 CONTINUE
   IF (TOTAL-147.0) 58,58,402
402 ITOTAL=TOTAL
   PRINT 403,ITOTAL
403 FORMAT (6X,28HTOTAL NUMBER OF INTERVALS = I3,31H, TOTAL ALLOWABLE
NUMBER = 147.)
   ISAIR=1
C
C DETERMINE IF ANY ERRORS
C
58 IF (ISAIR) 901,60,200
60 CONTINUE
   IF (SENSE LIGHT 3) 200, 510
510 CONTINUE
C
C GENERATE TABLE OF INDEX RECORD NUMBERS CORRESPONDING TO
C ICOMPOSITIONS
C
   I=NCDT(3)
   J=1
   DO 61 K=1,NCOMP
     L=4
     DO 62 M=1,I
       IF ((COMP(J)-CDT(L))+(COMP(J+1)-CDT(L+1))) 63,64,63
63 L=L+2
62 CONTINUE
     GO TO 902
64 NR(K)=NCDT(L+2)

```

```

      J=J+2
61 CONTINUE
C
C   INITIALIZE FOR PROCESS COMPOSITION COMPOSITION DATA TAPE
C   SUBROUTINE
C
      NRSAV=0
      NRSPAS=0
      N1WORD=NOGPS*NOGPCN
      N2WORD=NOGPS*NOGPS
      N1WORD+N2WORD
C
C   ENTER LOOP
C
65 DO 66 I=1, NCOMP
      CALL PCKDT (NRSAV, NRSPAS, NR, KDT, NCOMP, D, TEMP, NOGPS, NOGPCN,
1NRPRES, N1WORD, N2WORD, ISAIR)
      IF (ISAIR) 903, 66, 200
66 CONTINUE
      REWIND KDT
C
C   PRINT OUT
C
200 ITOTAL=TOTAL
      IF (ISAIR) 907, 255, 256
256 PRINT 257
257 FORMAT (1H1)
255 PRINT 201, NOGPS, NCODE(1), ITOTAL, NCOMP, LMAX, FPSK
201 FORMAT (1H024X, 19HCALCULATION SUMMARY//25X, 18HNUMBER OF GROUPS =I
13, /25X, 19HNUMBER OF REGIONS =I4, /25X, 27HTOTAL NUMBER OF INTERVALS
2=I4, /25X, 24HNUMBER OF COMPOSITIONS =I3, /25X, 30HMAXIMUM NUMBER OF I
3TERATIONS =I4, /25X20HCONVERGENCE FACTOR =1PE14.7//)
202 IF (NCODE(2)) 904, 204, 203
203 PRINT 205
205 FORMAT (25X, 24HADJOINT FLUX CALCULATION)
      GO TO 207
204 PRINT 206
206 FORMAT (25X, 23HDIRECT FLUX CALCULATION)
207 IF (NCODE(3)) 905, 209, 208
208 PRINT 210
210 FORMAT (25X, 20HCYLINDRICAL GEOMETRY)
      GO TO 212
209 PRINT 211
211 FORMAT (25X, 13HSLAB GEOMETRY)
C
C   PRINT BOUNDARIES AND ALBEDOS
C
212 I1=NCODE(1)
      DO 213 I=1, I1
      IF (R(I+1)) 213, 214, 213
213 CONTINUE
      I=NCODE(1)
214 PRINT 215, R(1), R(I+1)
215 FORMAT (1H0/2X, 18HLEFT-HAND BOUNDARYIPE14.7, 3X, 19HRIGHT-HAND BOUND
1ARY1PF14.7//)

```

216 PRINT 217

217 FORMAT (8X,20HGROUP LEFT ALBEDO15X,21HGROUP RIGHT ALBEDO)

DO 218 I=1,NOGPS

PRINT 219,I,ALFT(I),I,ARGT(I)

219 FORMAT (9X,I2,1PF18.7,I17,1PF19.7)

218 CONTINUE

C

C PAGE 2 REGIONAL DATA

C

220 PRINT 221

221 FORMAT (1H1///26X,13HREGIONAL DATA///12X,9HNUMBER OF5X,10HRIGHT-HA  
IND8X,8HBUCKLING7X,11HCOMPOSITION/2X,6HREGION4X,9HINTERVALS6X,8HBOU  
NDARY9X,9HDIMENSION4X,14HIDENTIFICATION)

J=1

I1=NCODE(1)

DO 222 I=1,I1

L=FN(I)

IF (1-35\*(I/35)) 223,224,223

223 PRINT 225,I,L,R(I+1),HF(I),RFG(J),RFG(J+1)

225 FORMAT (I6,I12,1PF20.7,1PF17.7,3X,2A6)

J=J+2

GO TO 222

224 PRINT 226,I,L,R(I+1),HF(I),RFG(J),RFG(J+1)

226 FORMAT (1H1///26X,13HREGIONAL DATA///12X,9HNUMBER OF5X,10HRIGHT-HA  
IND8X,8HBUCKLING7X,11HCOMPOSITION/2X,6HREGION4X,9HINTERVALS6X,8HBOU  
NDARY9X,9HDIMENSION4X,14HIDENTIFICATION/I6,I12,1PF20.7,1PF17.7,3X,  
32A6)

J=J+2

222 CONTINUE

C

C TEST IF MIXABLES AND PRINT NEXT PAGE

C

C

C

PRINT COMPOSITIONS

C

228 PRINT 230

230 FORMAT (1H1///28X,12HCOMPOSITIONS///)

J=1

DO 231 I=1,NCOMP

PRINT 232,COMP(J),COMP(J+1)

232 FORMAT (29X,2A6)

J=J+2

231 CONTINUE

C

C PRINT MIXABLES IF ANY

C

227 IF (NMIX) 906,280,229

229 CALL POMIX (6H MIX ,NCODE,REG,NMIX,COMP,EFFV,ISAIR,NCOMP)

C

C TEST IF D IS TO BE PRINTED

C

280 IF (NCODE(2)-10) 250,275,250

C

PRINT OUT D TABLE

C

275 PRINT 276

276 FORMAT (1H1//)  
I=0

285 DO 277 J=1,440

K=(I\*440)+J

L=((I+1)\*440)+J

M=((I+2)\*440)+J

N=((I+3)\*440)+J

PRINT 278,D(K),D(L),D(M),D(N)

278 FORMAT (8X,1PF13.7,1PE15.7,1PE15.7,1PE15.7)

277 CONTINUE

I=I+4

IF (NCOMP-I) 250,250,279

279 PRINT 284

284 FORMAT (1H1//)

GO TO 285

C

C DETERMINE IF ERROR

C

250 IF (ISAIR) 900,251,900

C

C CLEAR FPREP COMMON LEAVE FN COMMON ALONE

C

251 DO 252 I=1,1029

NR(I)=0

252 CONTINUE

C

C SET UP PAGE NUMBER FOR FN

C

253 CALL PAGES(NPAGE)

C

C BRING IN FN

C

254 CONTINUE

CALL CHAIN(3,R1)

C

C FINAL STOP FOR ERRORS

C

900 REWIND KDT

CONTINUE

CALL EXIT

C

C ISAIR IS NEGATIVE.STATEMENT 58.

C

901 CALL ERRORA

ISAIR=1

GO TO 200

C

C COMPOSITION CANNOT BE FOUND IN INDEX.CONSISTENCY CHECK HAS  
C FAILED TO DIAGNOSE PROPERLY.STATEMENTS 60-64.

C

902 CALL ERRORA

ISAIR=1

GO TO 200

C



C     ISAIR IS NEGATIVE COMING FROM PCKDT SUBROUTINE. STATEMENTS  
65-66 AND PCKDT.

C  
903 CALL FRRORA  
   ISAIR=1  
   GO TO 200

C  
C     NCODF(3) IS NEGATIVE. STATEMENT 202.  
C

C  
904 CALL FRRORA  
   ISAIR=1  
   GO TO 207

C  
C     NCODF(3) IS NEGATIVE. STATEMENT 207.  
C

C  
905 CALL FRRORA  
   ISAIR=1  
   GO TO 212

C  
C     NMIX IS NEGATIVE. STATEMENT 227.  
C

C  
906 CALL FRRORA  
   ISAIR=1  
   GO TO 250

C  
C     ISAIR IS NEGATIVE. STATEMENT 200  
C

C  
907 CALL FRRORA  
   ISAIR=1  
   GO TO 256  
   END (0,0,0)

```
* 657          PROGRAM ODD      HOFFMAN
C
C SUBROUTINE REGCK (A,NCODE,NCOMP,REG,COMP,ISAIR)
C
C DIMENSION FOR REGCK SUBROUTINE
C DIMENSION REG(200),COMP(40),NCODE(20)
C
C BEGIN EXECUTABLE PART OF SUBROUTINE REGCK
C
1 I=1
  I1=NCODE(1)
  DO 2 J=1,I1
    K=1
    DO 3 L=1,NCOMP
      IF ((REG(I)-A) 4,5,4
4 IF (((REG(I)-COMP(K))+(REG(I+1)-COMP(K+1)))) 6,5,6
6 K=K+1
3 CONTINUE
  ISAIR=1
  PRINT 7,J
7 FORMAT (6X,22HCOMPOSITION IN REGION I3,32H NOT GIVEN IN COMPOSITIO
  IN INPUT.)
5 I=I+1
2 CONTINUE
  RETURN
END (0,0,0)
```

```

*      657          PROGRAM ODD          HOFFMAN
      SUBROUTINE PCKDT (NRSAV,NRSPAS,NR,KDT,NCOMP,D,TFMP,NOGPS,
      INOGPCN,NRPRES,NTWORD,NIWORD,N2WORD,ISAIR)
C
C      DIMENSION FOR PCKDT SUBROUTINE
      DIMENSION NR(20),D(8800),TEMP(1000)
C
C      BEGIN EXECUTABLE PART OF SUBROUTINE PCKDT
C
      1 DO 2 I=1,NTWORD
        TEMP(I)=0.0
      2 CONTINUE
C
C      FIND NEXT RECORD TO PROCESS
C
      I=1
      6 DO 3 J=1,NCOMP
        IF (NR(I)-NR(J)) 3,3,4
      3 CONTINUE
        GO TO 5
      4 I=I+1
        GO TO 6
C
C      DETERMINE RECORD SPACING
C
      5 NRPRES=NR(I)
        NR(I)=NR(I)+1000
        NRSPAS=NRPRES-NRSAV-1
        IF (NRSPAS) 900,7,8
C
C      SPACE TAPE
C
      8 DO 9 J=1,NRSPAS
        READ TAPE KDT
      9 CONTINUE
C
C      READ RECORD INTO TEMP
C
      7 READ TAPE KDT,(TEMP(J),J=1,NTWORD)
        NRSAV=NRPRES
C
C      FIND POSITION OF COMPOSITION IN D TABLE
C
      10 J=I-1
        K=J*440
C
C      TRANSFER GROUP CONSTANTS INTO D TABLE
C
      11 DO 12 L=1,NIWORD
        M=L+K
        D(M)=TEMP(L)
      12 CONTINUE
C
C      I=COMPOSITION POSITION

```

```

C      J=COMPOSITION POSITION LESS ONE
C      K=INITIAL ADDRESS OF I COMPOSITION IN TABLE D
C
13  L=K+N1WORD+1
    M=N1WORD-NOGPS
C
C      L=INITIAL MATRIX ADDRESS OF I COMPOSITION IN TABLE D
C      M=INITIAL MATRIX ADDRESS OF TEMP LESS THE NUMBER OF
C      GROUPS PLUS ONE
C
C      INITIALIZE FOR LOOP TO TRANSFER FULL TEMP MATRIX TO REDUCED
C      TABLE D MATRIX
C
14  I1=NOGPS-5
    I2=2
    DO 15 I3=1,I1
    DO 16 I4=I2,NOGPS
    I5=M I4+(I3*NOGPS)
    D(L)=TEMP(I5)
    L=L+1
16  CONTINUE
    I2=I2+1
15  CONTINUE
C
C      REVERSE FOR GROUPS 21 THROUGH 25
C
17  I1=I1+1
    I2=21
    DO 18 I3=I1,NOGPS
    DO 19 I4=I2,NOGPS
    I5=M I4+(I3*NOGPS)
    D(L)=TEMP(I5)
    L=L+1
19  CONTINUE
18  CONTINUE
    GO TO 20
900 CALL ERRORA
    ISAIR=1
    REWIJD KDT
20  RETURN
    END (0,0,0)

```

```

*      657          PROGRAM ODD      HOFFMAN
C
SUBROUTINE POMIX (A,NCODE,REG,NMIX,COMP,FFFV,ISAIR,NCOMP)
C
C      DIMENSION FOR POMIX SUBROUTINE
C      DIMENSION REG(200),COMP(40),EFFV(500),NCODE(20)
C
C      BEGIN EXECUTABLE PART OF SUBROUTINE POMIX
C
1 PRINT 2
2 FORMAT (1H1///15X,37HREGIONS CONTAINING MIXED COMPOSITIONS///)
  I=5
  J=1
  I1=1
  I2=NMIX
  I3=NCODE(1)
  DO 3 K=1,I3
  IF (A-REG(J)) 4,5,4
5 IF (J-50*(I/50)) 6,7,6
6 PRINT 8,K,REG(J),REG(J+1)
8 FORMAT (16X,13HREGION NUMBER14,2X,15HIDENTIFICATION 2A6//)
  I=I+1
  IF (I-50*(I/50)) 22,10,22
22 I=I+1
  IF (I-50*(I/50)) 9,10,9
9 PRINT 13
13 FORMAT (20X,11HCOMPOSITION9X,14HMIXING DENSITY)
  I=I+1
  IF (I-50*(I/50)) 14,15,14
7 PRINT 11
11 FORMAT (1H1///15X,37HREGIONS CONTAINING MIXED COMPOSITIONS///)
  I=5
  GO TO 6
10 PRINT 12
12 FORMAT (1H1///15X,37HREGIONS CONTAINING MIXED COMPOSITIONS///)
  I=5
  GO TO 9
15 PRINT 16
16 FORMAT (1H1///15X,37HREGIONS CONTAINING MIXED COMPOSITIONS///)
  I=5
14 L=1
  DO 17 M=I1,I2
  PRINT 18,COMP(L),COMP(L+1),FFFV(M)
18 FORMAT (19X,2A6,9X,1PE14.7)
  L=L+2
  I=I+1
  IF (I-50*(I/50)) 17,20,17
20 PRINT 21
21 FORMAT (1H1///15X,37HREGIONS CONTAINING MIXED COMPOSITIONS///)
  I=5
17 CONTINUE
  I1=I2+1
  I2=I2+NMIX
  PRINT 23
23 FORMAT (1H )

```

```
I=I+1  
IF (I-50*(I/50)) 4,24,4  
24 PRINT 25  
25 FORMAT (1H1///15X,37HREGIONS CONTAINING MIXED COMPOSITIONS///)  
I=5  
4 J=J+2  
3 CONTINUE  
RETURN  
END (0,0,0)
```

```
*      CHAIN(3,B1)                BLOCK F1
*      657          CONTROL F-1
C
COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPE,KTAPE,MORE,D,
1COMP,REG,NMIX,R,EN,HE,EFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SEXM,
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DEL,NCOMP
3,A,M,N
C
DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),FN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SEXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100)
C
DIMENSION A(5,5)
C
CALL RANDC(6H MIX )
CALL GCOE
CALL HOMRC
CALL CHAIN(4,R1)
CALL EXIT
END(0,0,0)
```

```

*      657          SUBROUTINE GCOE
C
SUBROUTINE GCOF
C
COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPE,KTAPE,MORE,D,
1COMP,REG,NMIX,R,EN,HE,EFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SEXM,
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DEL,NCOMP
3,A,M,N
C
DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SFXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100)
C
DIMENSION A(5,5)
C
SRFTF(H1,H2)=H2/H1
SGAMF(H1,H2)=H2**2/2.
SDELF(H1,H2)=H1*H2/2.
CBETF(R,H1,H2)=H2/H1*(1. ABSF((R-H1/2.)/(R+H1/2.)))/(1.+ABSF((R+H2
1/2.)/(R-H2/2.)))
CGAMF(R,H1,H2)=H2/2.*(R+H2/2.-(R-H2/2.)*ABSF((R-H2/2.)/(R+H2/2.)))
1/(1. ABSF((R-H2/2.)/(R+H2/2.)))
CDELF(R,H1,H2)=H2/2.*(R+H1/2.-(R-H1/2.)*ABSF((R-H1/2.)/(R+H1/2.)))
1/(1. ABSF((R+H2/2.)/(R-H2/2.)))
NRG=NCODE(1)
IF DIVIDE CHECK 2,2
2 CONTINUE
END=0.0
DO5J=1,NRG
H(J)=(R(J+1)-R(J))/ARF(FN(J))
IF DIVIDE CHECK 305,306
305 CONTINUE
CALL ERRORA
CALL FXIT
306 CONTINUE
END=END+ARF(FN(J))
5 CONTINUE
N=XFIXF(END)
AR(1)=R(1)
AR(2)=R(1)+.001*H(1)
AR(3)=R(1)+H(1)
J=1
DO 25 I=3,N
IF(AR(I)-R(J+1)+0.1*H(J))26,27,27
27 CONTINUE
AR(I)=R(J+1)
J=J+1
26 CONTINUE
AR(I-1)=AR(I)+H(J)
25 CONTINUE
AR(N-2)=R(NRG+1)-.001*H(NRG)
AR(N-1)=R(NRG+1)
M=N+2

```



```

N=N+2
J=1
HA=.001*H(1)
HB=.999*H(1)
IF(NCODE(3)-1)100,101,101
100 CONTINUE
BETA(2)=SBETF(HA,HB)
BETA(3)=SBETF(HB,H(1))
GAM(2)=SGAMF(HA,HB)
GAM(3)=SGAMF(HB,H(1))
DEL(2)=SDELF(HA,HB)
DEL(3)=SDELF(HB,H(1))
DO 103 I=4,N
IF(AR(I)-R(J+1))414,413,413
413 CONTINUE
BETA(I)=SBETF(H(J),H(J+1))
GAM(I)=SGAMF(H(J),H(J+1))
DEL(I)=SDELF(H(J),H(J+1))
J=J+1
GO TO 15
414 CONTINUE
BETA(I)=SBETF(H(J),H(J))
GAM(I)=SGAMF(H(J),H(J))
DEL(I)=SDELF(H(J),H(J))
15 CONTINUE
103 CONTINUE
HA=.999*H(NRG)
HB=.001*H(NRG)
BETA(N-1)=SBETF(H(NRG),HA)
BETA(N)=SBETF(HA,HB)
GAM(N-1)=SGAMF(H(NRG),HA)
GAM(N)=SGAMF(HA,HB)
DEL(N-1)=SDELF(H(NRG),HA)
DEL(N)=SDELF(HA,HB)
GO TO 9
101 CONTINUE
BETA(2)=CBETF(AR(2),HA,HB)
BETA(3)=CBETF(AR(3),HB,H(1))
GAM(2)=CGAMF(AR(2),HA,HB)
GAM(3)=CGAMF(AR(3),HB,H(1))
DEL(2)=CDELF(AR(2),HA,HB)
DEL(3)=CDELF(AR(3),HB,H(1))
DO 102 I=4,N
IF(AR(I)-R(J+1))11,12,12
12 CONTINUE
BETA(I)=CBETF(AR(I),H(J),H(J+1))
GAM(I)=CGAMF(AR(I),H(J),H(J+1))
DEL(I)=CDELF(AR(I),H(J),H(J+1))
J=J+1
GO TO 16
11 CONTINUE
BETA(I)=CBETF(AR(I),H(J),H(J))
GAM(I)=CGAMF(AR(I),H(J),H(J))
DEL(I)=CDELF(AR(I),H(J),H(J))
16 CONTINUE

```

```
102 CONTINUE
-----
HA=.999*H(NRG)
HB=.001*H(NRG)
-----
BETA(N-1)=CBETF(AR(N-1),H(NRG),HA)
BETA(N)=CBETF(AR(N),HA,HB)
-----
GAM(N-1)=CGAMF(AR(N-1),H(NRG),HA)
GAM(N)=CGAMF(AR(N),HA,HB)
-----
DEL(N-1)=CDELFF(AR(N-1),H(NRG),HA)
DEL(N)=CDELFF(AR(N),HA,HB)
-----
9 CONTINUE 00
IF DIVIDE CHECK 307,308 00
-----
307 CONTINUE 00
CALL FRRORA
-----
CALL EXIT
-----
308 CONTINUE 00
RETURN
END(0,0,0)
```

## MATRIX INVERSION SUBROUTINE

J B RABIN

MA

SUBROUTINE MATINV(A,NR,NC)

MA

COMMON A,NR,NC

MA

DIMENSION A(5,5),LAREL(5)

```

      DO 38 I=1,NR
38 LABEL(I)=I
      DO 24 I=1,NR
      1 DO 24 I=1,NR
      2 FRE=0.0
      3 DO 7 M=I,NR
      4 IF(ABS(A(M,I))-FRE) 7,7,5
      5 FRE=ABS(A(M,I))
      6 IBIG=M
      7 CONTINUE
      9 IF(IBIG-I) 10,14,10
      10 DO 13 M=1,NC
      11 FRE=A(I,M)
      12 A(I,M)=A(IBIG,M)
      13 A(IBIG,M)=FRE
      M=LAREL(I)
      LAREL(I)=LAREL(IBIG)
      LAREL(IBIG)=M
      14 FRE=A(I,I)
      15 A(I,I)=1.0
      16 DO 17 M=1,NC
      17 A(I,M)=A(I,M)/FRE
      18 DO 24 J=1,NR
      19 IF(J I) 20,24,20
      20 FRE=A(J,I)
      21 A(J,I)=0.0
      22 DO 23 K=1,NC
      23 A(J,K)=A(J,K)-FRE*A(I,K)
      24 CONTINUE
      25 M=NR 1
      26 DO 36 I=1,M
      27 DO 30 J=I,NR
      28 IF(LAREL(J)-I) 30,29,30
      29 IF(I J) 31,36,31
      30 CONTINUE
      31 DO 34 K=1,NR
      32 FRE=A(K,I)
      33 A(K,I)=A(K,J)
      34 A(K,J)=FRE
      35 LAREL(J)=LAREL(I)
      36 CONTINUE
      37 RETURN
      END(0,0,0)

```

MA

\* 657 SUBROUTINE HOMRC

C  
SUBROUTINE HOMRC

C  
COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPE,KTAPE,MORE,D,  
1COMP,REG,NMIX,R,EN,HE,FFFV,ALFT,ARGT,LMAX,EPSK,NCODE,SEXM,  
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DEL,NCOMP  
3,A,M,N

C  
DIMENSION Q(12),CDT(303),D(8800),COMP(40),RFG(200),R(101),EN(100),  
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SFXM(150),  
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),  
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),  
4NCOMP(100)

C  
DIMENSION RXST(5),DIF(5),TSCAT(5,5)

C  
DIMENSION A(5,5)

C  
DO16KH=1,20  
IF(NCODE(2)-1)4,5,5  
4 CONTINUE  
K=KH  
GO TO 6  
5 CONTINUE  
K=1+20-KH  
6 CONTINUE  
J=1  
CALL RPAR(RXS,DIFC,K,J,6H MIX )  
ALFT(K)=1.+(AR(2)-AR(1))/(2.\*DIFC)\*(1.-ALFT(K))/(1.+ALFT(K))  
IF DIVIDE CHECK 7,8  
7 CONTINUE  
CALL ERRORA  
CALL EXIT  
8 CONTINUE  
KN=N\*(K-1)+1  
V(KN)=ALFT(K)  
KM=KN+1  
DO9I=2,N  
V(KM)=BETA(I)\*DIFC\*(1.-1./V(KM-1)) DEL(I)\*RXS  
IF(AR(I)-R(J+1))10,11,11  
11 CONTINUE  
J=J+1  
CALL RPAR(RXS,DIFC,K,J,6H MIX )  
10 CONTINUE  
V(KM)=1.+(V(KM)+GAM(I)\*RXS)/DIFC  
IF DIVIDE CHECK 12,13  
12 CONTINUE  
CALL ERRORA  
CALL EXIT  
13 CONTINUE  
KM=KM+1  
9 CONTINUE  
ARGT(K)=1.0+(AR(M)-AR(N))/(2.\*DIFC)\*(1.-ARGT(K))/(1.+ARGT(K))  
IF DIVIDE CHECK 14,15

```

14 CONTINUE
  CALL ERRORA
  CALL FXIT
15 CONTINUE
16 CONTINUE
  J=1
  CALL TMIX(1,DIF,RXST,TSCAT,6H MIX )
  DO50K=1,5
  KA=20+K
  ALFT(KA)=1.+(AR(2)-AR(1))/(2.*DIF(K))*(1.-ALFT(KA))/(1.+ALFT(KA))
  IF DIVIDE CHECK 17,18
17 CONTINUE
  CALL ERRORA
  CALL FXIT
18 CONTINUE
  DO2L=1,5
  IF(K L)8,19,3
19 CONTINUE
  VM(K,L,1)=1./ALFT(KA)
  GO TO 2
 3 CONTINUE
  VM(K,L,1)=0.0
 2 CONTINUE
50 CONTINUE
  DO26I=2,N
  DO27K=1,5
  DO28L=1,5
  IF(NCODE(2)-1)40,41,41
40 CONTINUE
  VM(K,L,I)=-BETA(I)*DIF(K)*VM(K,L,I-1)-DEL(I)*TSCAT(L,K)
  GOTO42
41 CONTINUE
  VM(K,L,I)=-BETA(I)*DIF(K)*VM(K,L,I-1)-DEL(I)*TSCAT(K,L)
42 CONTINUE
  IF(K L)28,29,28
29 CONTINUE
  VM(K,L,I)=VM(K,L,I)+BETA(I)*DIF(K) DEL(I)*RXST(K)
28 CONTINUE
27 CONTINUE
  IF (AR(I)-R(J+1)) 110,111,111
111 CONTINUE
  J=J+1
  CALL TMIX(J,DIF,RXST,TSCAT,6H MIX )
110 CONTINUE
  DO32K=1,5
  DO33L=1,5
  IF(NCODE(2)-1)45,46,46
45 CONTINUE
  VM(K,L,I)=(VM(K,L,I)-GAM(I)*TSCAT(L,K))/DIF(K)
  GOTO47
46 CONTINUE
  VM(K,L,I)=(VM(K,L,I)-GAM(I)*TSCAT(K,L))/DIF(K)
47 CONTINUE
  IF(K L)33,34,33
34 CONTINUE

```

```
VM(K,L,I)=VM(K,L,I)+1.+(GAM(I)*RXST(K))/DIF(K)  
33 CONTINUE  
32 CONTINUE  
CALL MATINV(VM(1,1,I),5,5)  
26 CONTINUE  
DO 60 K=1,5  
KA=20+K  
ARGT(KA)=1.+(AR(M)-AR(N))/(2.*DIF(K))*(1.-ARGT(KA))/(1.+ARGT(KA))  
DO 51 L=1,5  
A(K,L)=-VM(K,L,N)  
IF(K L)51,52,51  
52 CONTINUE  
A(K,L)=A(K,L)+ARGT(KA)  
51 CONTINUE  
60 CONTINUE  
CALL MATINV(A(1,1),5,5)  
RETURN  
END(0,0,0)
```

\* 657

## SUBROUTINE RANDC

SUBROUTINE RANDC(A)

C

```
COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPE,KTAPE,MORE,D,  
1COMP,REG,NMIX,R,EN,HE,EFFV,ALFT,ARGT,LMAX,EPK,NCODE,SEXM,  
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DEL,NCOMP  
3,A,M,N
```

C

```
DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),FN(100),  
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SEXM(150),  
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),  
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),  
4NCOMP(100)
```

C

```
MIX=0  
NRG=NCODE(1)  
DO2J=1,NRG  
IF(RFG(2*J-1)-A)4,5,4  
4 CONTINUE  
DO3I=1,20  
IF(RFG(2*J-1)-COMP(2*I-1))3,6,3  
6 CONTINUE  
IF(RFG(2*J)-COMP(2*I))3,7,3  
3 CONTINUE  
CALL ERRORA  
CALL EXIT  
7 CONTINUE  
NCOMP(J)=I  
GO TO 2  
5 CONTINUE  
MIX=MIX+1  
NCOMP(J)=MIX  
2 CONTINUE  
RETURN  
END(0,0,0)
```

\* 657 SUBROUTINE RPAR

C SUBROUTINE RPAR(RXS,DIFC,K,J,E)

C COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPE,KTAPE,MORF,D,  
1COMP,REG,NMIX,R,EN,HE,EFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SFXM,  
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DFL,NCOMP  
3,A,M,N

C DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN(100),  
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SFXM(150),  
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),  
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),  
4NCOMP(100)

C DIMENSION A(5,5)

C IF(REG(2\*J-1)-F)2,3,2

3 CONTINUE

NA=NMIX\*(NCOMP(J)-1)+1

RXS=0

DIFC=0

SUM=0

MA=5\*(K-1)+1

DO4 I=1,NMIX

RXS=RXS+D(MA+2)\*EFFV(NA)

IF(NCODE(3)-1)5,6,6

5 CONTINUE

DIFC=EFFV(NA)/D(MA+1)+DIFC

SUM=EFFV(NA)/D(MA)+SUM

GO TO 7

6 CONTINUE

DIFC=EFFV(NA)/D(MA)+DIFC

SUM=EFFV(NA)/D(MA+1)+SUM

7 CONTINUE

NA=NA+1

MA=MA+440

4 CONTINUE

IF(NCODE(3)-1)8,9,9

8 CONTINUE

RXS=RXS+23.13/(HE(J)+4.2624/SUM)\*\*2/SUM

DIFC=1./DIFC

GO TO 10

9 CONTINUE

RXS=RXS+9.87/(HE(J)+4.2624/SUM)\*\*2/SUM

DIFC=1./DIFC

10 CONTINUE

RETURN

2 CONTINUE

NA=440\*(NCOMP(J)-1)+5\*K-4

IF(NCODE(3)-1)11,12,12

11 CONTINUE

RXS=D(NA+2)+23.13\*D(NA)/(HE(J)+4.2624\*D(NA))\*\*2

DIFC=D(NA+1)

GO TO 10



---

12 CONTINUE

$RXS = D(NA+2) + 9.87 * D(NA+1) / (HE(J) + 4.2624 * D(NA+1)) ** 2$

DIFC = D(NA)

---

GO TO 10

END(0,0,1)

---

657

## SUBROUTINE TMIX

SUBROUTINE TMIX(J,A,B,C,E)

```
COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPF,KTAPE,MORE,D,
1COMP,REG,NMIX,R,EN,HE,EFFV,ALFT,ARGT,LMAX,EPSK,NCODE,SEXM,
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DFL,NCOMP
```

```
DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SFXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(2750),
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100)
```

```
DIMENSION A(5),B(5),C(5,5),SUM(5)
```

```
DO16K=1,5
A(K)=0.0
B(K)=0.0
SUM(K)=0.0
DO17L=1,5
C(K,L)=0.0
```

17 CONTINUE

16 CONTINUE

```
IF(RFG(2*J-1)-F)2,3,2
```

2 CONTINUE

```
KA=440*(NCOMP(J)-1)+101
```

```
KD=KA+314
```

```
KE=KA
```

```
DO7K=1,5
```

```
KR=KA+5*(K-1)
```

```
B(K)=D(KR+2)
```

```
A(K)=1./D(KE)
```

```
SUM(K)=1./D(KE-1)
```

```
KF=KE+5
```

```
DO8L=1,5
```

```
LA=KD+L
```

```
C(K,L)=D(LA)
```

8 CONTINUE

```
KD=KD+5
```

7 CONTINUE

```
GO TO 9
```

3 CONTINUE

```
KA=101
```

```
KD=415
```

```
KC=NMIX*(NCOMP(J)-1)+1
```

```
DO10I=1, NMIX
```

```
KE=KA
```

```
DO11K=1,5
```

```
KR=KA+5*(K-1)
```

```
B(K)=B(K)+EFFV(KC)*D(KR+2)
```

```
A(K)=A(K)+EFFV(KC)/D(KE)
```

```
SUM(K)=SUM(K)+EFFV(KC)/D(KE+1)
```

```
DO12L=1,5
```

```
LA=KD+L
```

```
C(K,L)=C(K,L)+FFFV(KC)*D(LA)
12 CONTINUE
KD=KD+5
KE=KF+5
11 CONTINUE
KA=KA+440
KD=KA+314
KC=KC+1
10 CONTINUE
9 CONTINUE
DO18K=1,5
IF(NCODE(3)-1)19,20,20
19 CONTINUE
R(K)=B(K)+23.12/(HF(J)+4.2624/A(K))**2/A(K)
A(K)=1./SUM(K)
GOTO18
20 CONTINUE
R(K)=B(K)+9.87/(HF(J)+4.2624/SUM(K))**2/SUM(K)
A(K)=1./A(K)
18 CONTINUE
RETURN
END(0,0,0)
```

```

*   CHAIN(4,B1)                BLOCK F2
C
*   657          CONTROL F-2
C
COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPF,KTAPE,MORE,D,
1COMP,REG,NMIX,R,EN,HE,EFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SEXM,
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DEL,NCOMP
3,A,M,N
C
DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SFXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(2750),
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100)
C
DIMENSION DIF(5),RXST(5),TSCAT(5,5)
C
DIMENSION A(5,5)
C
L=0
2 CONTINUE
L=L+1
CALL SORRC
CALL POWER
IF (NCODE(3)-1) 3, 4, 4
3 CONTINUE
REAC=STINT(FP,FM,1,M,0)
GO TO 5
4 CONTINUE
REAC=CTINT(FP,FM,1,M,0)
5 CONTINUE
IF(RFAC)7,6,7
6 CONTINUE
IF (L-1) 9, 9, 10
9 CONTINUE
DOBI=1,150
FP(I)=1.0
FM(I)=1.0
8 CONTINUE
GO TO 2
7 CONTINUE
RK(L)=REAC
DO 15 I=1,150
FP(I)=FP(I)/REAC
FM(I)=FM(I)/REAC
15 CONTINUE
IF(L 1)2,2,11
11 CONTINUE
IF(L LMAX)12,10,10
12 CONTINUE
IF(ARSF(RK(L-1)/RK(L)-1.)-FPSK)10,10,2
10 CONTINUE
DO500K=1,20
CALL RPAR(RXS,DIFC,K,1,6H MIX )
ALFT(K)=(ALFT(K)-1.)*DIFC/(AR(2)-AR(1))*2.

```

---


$$ALFT(K) = (1. - ALFT(K)) / (1. + ALFT(K))$$


---


$$J = NCODE(1)$$


---


$$CALL RPAR(RXS, DIFC, K, J, 6H MIX )$$


---


$$ARGT(K) = (ARGT(K) - 1.) * DIFC / (AR(M) - AR(M-1)) * 2.$$


---


$$ARGT(K) = (1. - ARGT(K)) / (1. + ARGT(K))$$


---

500 CONTINUE

$$J = 1$$


---


$$CALL TMIX(J, DIF, RXST, TSCAT, 6H MIX )$$


---


$$DO 501 K = 1, 5$$


---


$$KA = 20 + K$$


---


$$ALFT(KA) = (ALFT(KA) - 1.) * DIF(K) / (AR(2) - AR(1)) * 2.$$


---


$$ALFT(KA) = (1. - ALFT(KA)) / (1. + ALFT(KA))$$


---

501 CONTINUE

$$CALL TMIX(NCODE(1), DIF, RXST, TSCAT, 6H MIX )$$


---


$$DO 502 K = 1, 5$$


---


$$KA = 20 + K$$


---


$$ARGT(KA) = (ARGT(KA) - 1.) * DIF(K) / (AR(M) - AR(M-1)) * 2.$$


---


$$ARGT(KA) = (1. - ARGT(KA)) / (1. + ARGT(KA))$$


---

502 CONTINUE

$$CALL CHAIN(5, R1)$$


---


$$CALL EXIT$$


---


$$END(0, 0, 0)$$


---

```

*   657           SUBROUTINE SORRC
C
C   SURROUTINE SORRC
C
C   COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPE,KTAPF,MORE,D,
1COMP,REG,NMIX,R,EN,HF,FFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SFXM,
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DEL,NCOMP
3,A,M,N
C
C   DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),FN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SEXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100)
C
C   DIMENSION SCATI(20)
C
C   DIMENSIONDIF(5),RXST(5),TSCAT(5,5)
C
C   DIMENSIONTSCATI(5)
C
C   DIMENSION A(5,5)
C
C   DIMENSION SUMT(5)
C
C COMPUTES ITERATION DEPENDENT QUANTITIES
C
C   IF(NCODE(2)-1)2,3,3
2 CONTINUE
DO35K=1,20
J=1
CALL RPAR(RXS,DIFC,K,J,6H MIX )
CALL SPAR(S,SCATI,K,J,6H MIX )
KM=N*(K-1)+1
W(1)=0.0
DO10J=2,N
W(I)=BETA(I)*DIFC/V(KM)*W(I-1)+DEL(I)*S*FM(I)
DO15L=1,20
IF(L K)11,16,16
11 CONTINUE
LM=I M*(L-J)
W(I)=W(I)+DEL(I)*SCATI(L)*PHI(LM)
15 CONTINUE
16 CONTINUE
IF(AR(I)-R(J+1))17,18,18
18 CONTINUE
J=J+1
CALL RPAR(RXS,DIFC,K,J,6H MIX )
CALL SPAR(S,SCATI,K,J,6H MIX )
17 CONTINUE
DO19L=1,20
IF(L K)20,21,21
20 CONTINUE
LM=I M*(L-1)
W(I)=W(I)+GAM(I)*SCATI(L)*PHI(LM)

```

```

19 CONTINUE
21 CONTINUE
  W(I)=(W(I)+GAM(I)*S*FP(I))/DIFC
  KM=KM+1
10 CONTINUE
  KN=M*K
  KP=KN-K
  PHI(KN)=W(N)/(ARGT(K)*V(KP)-1.)
  DO25 I=1,N
  IA=M-I
  PHI(KN-1)=(PHI(KN)+W(IA))/V(KP)
  KN=KN-1
  KP=KP-1
25 CONTINUE
35 CONTINUE
  DO50 K=1,750
  W(K)=0
50 CONTINUE
  J=1
  CALL TMIX(J,DIF,RXST,TSCAT,6H MIX )
  DO51 I=2,N
  IA=5*(I-1)+1
  LB=IA-5
  DO52 K=1,5
  SUM=0
  DO53 L=1,5
  SUM=SUM+VM(K,L,I-1)*W(LR)
  LB=LB+1
53 CONTINUE
  LB=LB-5
  W(IA)=BETA(I)*DIF(K)*SUM
  IA=IA+1
52 CONTINUE
  IA=IA-5
  DO55 K=21,25
  CALL SPAR(S,SCATI,K,J,6H MIX )
  DO54 L=1,20
  LM=M*(L-1)+I
  W(IA)=W(IA)+DEL(I)*SCATI(L)*PHI(LM)
54 CONTINUE
  IA=IA+1
55 CONTINUE
  IA=IA-5
  IF(AR(I)-R(J+1))56,57,57
57 CONTINUE
  J=J+1
  CALL TMIX(J,DIF,RXST,TSCAT,6H MIX )
56 CONTINUE
  KA=1
  DO59 K=21,25
  CALL SPAR(S,SCATI,K,J,6H MIX )
  DO60 L=1,20
  LM=M*(L-1)+I
  W(IA)=W(IA)+GAM(I)*SCATI(L)*PHI(LM)
60 CONTINUE

```

```

W(IA)=W(IA)/DIF(KA)
IA=IA+1
KA=KA+1
59 CONTINUE
51 CONTINUE
LB=5*N-4
DO62K=1,5
SUMT(K)=0
DO63L=1,5
SUMT(K)=SUMT(K)+VM(K,L,N)*W(LB)
LB=LB+1
63 CONTINUE
LR=LR-5
62 CONTINUE
LC=25*M-4
DO64K=1,5
PHI(LC)=0
DO65L=1,5
PHI(LC)=PHI(LC)+A(K,L)*SUMT(L)
65 CONTINUE
LC=LC+1
64 CONTINUE
DO66I=1,N
LC=25*M-5*I+1
IA=M I
LA=LC
DO67K=1,5
PHI(LC-5)=0
LB=5*IA-4
DO68L=1,5
PHI(LC-5)=VM(K,L,IA)*(PHI(LA)+W(LB))+PHI(LC-5)
LA=LA+1
LB=LB+1
68 CONTINUE
LA=LA-5
LC=LC+1
67 CONTINUE
66 CONTINUE
RETURN
3 CONTINUE
DO100K=1,750
W(K)=0
100 CONTINUE
J=I
CALL TMIX(J,DIF,RXST,TSCAT,6H MIX )
DO101I=2,N
IA=5*(I-1)+1
LR=IA-5
DO102K=1,5
SUM=0
DO103L=1,5
SUM=SUM+VM(K,L,I-1)*W(LR)
LB=LB+1
103 CONTINUE
LB=LB-5

```



```

W(IA)=BETA(I)*DIF(K)*SUM
IA=IA+1
102 CONTINUE
IA=IA-5
DO105K=21,25
CALL SPAR(S,SCATI,K,J,6H MIX )
W(IA)=W(IA)+DFL(I)*S*FM(I)
IA=IA+1
105 CONTINUE
IA=IA-5
IF(AR(I)-R(J+1))106,107,107
107 CONTINUE
J=J+1
CALL TMIX(J,DIF,RXST,TSCAT,6H MIX )
106 CONTINUE
KA=1
DO100K=21,25
CALL SPAR(S,SCATI,K,J,6H MIX )
W(IA)=(W(IA)+GAM(I)*S*FP(I))/DIF(KA)
IA=IA+1
KA=KA+1
109 CONTINUE
101 CONTINUE
LB=5*N-4
DO112K=1,5
SUMT(K)=0
DO112L=1,5
SUMT(K)=SUMT(K)+VM(K,L,N)*W(LB)
LB=LB+1
113 CONTINUE
LB=LB-5
112 CONTINUE
LC=25*M-4
DO114K=1,5
PHI(LC)=0
DO115L=1,5
PHI(LC)=PHI(LC)+A(K,L)*SUMT(L)
115 CONTINUE
LC=LC+1
114 CONTINUE
DO116I=1,N
LC=25*M-5*I+1
IA=M-I
LA=LC
DO117K=1,5
PHI(LC-5)=0
LB=5*IA-4
DO118L=1,5
PHI(LC-5)=VM(K,L,IA)*(PHI(LA)+W(LB))+PHI(LC-5)
LA=LA+1
LB=LB+1
118 CONTINUE
LA=LA-5
LC=LC+1
117 CONTINUE

```

```

116 CONTINUE
DO 185 KH=1,20
K=21 KH
J=1
CALL RPAR(RXS,DIFC,K,J,6H MIX )
CALL SPAR(S,SCATI,K,J,6H MIX )
KM=N*(K-1)+1
W(1)=0.0
DO150 I=2,M
W(I)=BETA(I)*DIFC/V(KM)*W(I-1)+DEL(I)*S*FM(I)
DO150 L=1,20
IF(L K)156,156,151
151 CONTINUE
LM=I M*(L-1)
W(I)=W(I)+DEL(I)*SCATI(L)*PHI(LM)
156 CONTINUE
155 CONTINUE
CALL TSPAR(J,K,TSCATI,6H MIX )
LB=20*M+5*I-4
DO125 L=1,5
W(I)=W(I)+DEL(I)*TSCATI(L)*PHI(LB)
LB=LB+1
125 CONTINUE
IF(AR(I)-R(J+1))157,158,158
158 CONTINUE
J=J+1
CALL RPAR(RXS,DIFC,K,J,6H MIX )
CALL SPAR(S,SCATI,K,J,6H MIX )
CALL TSPAR(J,K,TSCATI,6H MIX )
157 CONTINUE
DO159 L=1,20
IF(L K)161,161,160
160 CONTINUE
LM=M*(L-1)+I
W(I)=W(I)+GAM(I)*SCATI(L)*PHI(LM)
161 CONTINUE
159 CONTINUE
LB=20*M+5*I-4
DO126 L=1,5
W(I)=W(I)+GAM(I)*TSCATI(L)*PHI(LB)
LB=LB+1
126 CONTINUE
W(I)=(W(I)+GAM(I)*S*FP(I))/DIFC
KM=KM+1
150 CONTINUE
KN=M*K
KP=KN-K
PHI(KN)=W(N)/(ARGT(K)*V(KP)-1.)
DO 175 I=1,N
IA=M I
PHI(KN-1)=(PHI(KN)+W(IA))/V(KP)
KN=KN-1
KP=KP-1
175 CONTINUE
185 CONTINUE

```

RETURN  
END(0,0,0)

657

## SUBROUTINE POWER

## SUBROUTINE POWER

```

COMMON Q,CDT,NPAGF,NWOT,NDT,KDT,ITAPF,JTAPF,KTAPF,MORE,D,
1COMP,REG,NMIX,R,FN,HE,FFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SFXM,
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DEL,NCOMP
3,A,M,N

```

```

DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),FN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SFXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100)

```

```

DIMENSION A(5,5)

```

```

DIMENSION FPAR(25)

```

```

J=1
CALL PMIX(J,FPAR,6H MIX )
FP(1)=0
FM(1)=0
IA=1
DO20K=1,25
FP(1)=FP(1)+FPAR(K)*PHI(IA)
IF(K 20)21,23,22
21 CONTINUE
IA=IA+M
GO TO 20
23 CONTINUE
IA=IA+M
GO TO 20
22 CONTINUE
IA=IA+1
20 CONTINUE
DO10I=2,N
IA=I
FM(I)=0
DO 11K=1,25
FM(I)=FM(I)+FPAR(K)*PHI(IA)
IF(K 20)12,9,13
12 CONTINUE
IA=IA+M
GO TO 11
9 CONTINUE
IA=IA+(M-1)+5*(I-1)+1
GO TO 11
13 CONTINUE
IA=IA+1
11 CONTINUE
IF(AR(I)-R(J+1))14,15,15
15 CONTINUE
J=J+1
CALL PMIX(J,FPAR,6H MIX )

```

```
IA=I
FP(I)=0
DO16K=1,25
FP(I)=FP(I)+FPAR(K)*PHI(IA)
IF(K 20)17,19,18
17 CONTINUE
IA=IA+M
GO TO 16
19 CONTINUE
IA=IA+(M-I)+5*(I-1)+1
GO TO 16
18 CONTINUE
IA=IA+1
16 CONTINUE
GO TO 10
14 CONTINUE
FP(I)=FM(I)
10 CONTINUE
FP(M)=0
FM(M)=0
IA=M
DO25K=1,25
FM(M)=FM(M)+FPAR(K)*PHI(IA)
IF(K 20)26,27,28
26 CONTINUE
IA=IA+M
GO TO 25
27 CONTINUE
IA=IA+5*N+1
GO TO 25
28 CONTINUE
IA=IA+1
25 CONTINUE
RETURN
END(0,0,0)
```

```

*      657          SUBROUTINE SPAR
C
SUBROUTINE SPAR(SOR,SCATI,K,J,E)
C
COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPF,KTAPF,MORE,D,
1COMP,REG,NMIX,R,EN,HE,FFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SEXM,
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DEL,NCOMP
3,A,M,N
C
DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SEXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100)
C
DIMENSION A(5,5)
C
DIMENSION SCATI(20)
C
SOR=0
DO25L=1,20
SCATI(L)=0
25 CONTINUE
IF(RFG(2*J-1)-E)2,3,2
3 CONTINUE
NA=NMIX*(NCOMP(J)-1)+1
MA=5*K-4
DO4I=1,NMIX
IF(NCODE(2)-1)5,6,6
5 CONTINUE
IF(D(MA+4))7,8,7
7 CONTINUE
SOR=D(MA+4)
8 CONTINUE
LA=124+K+440*(I-1)
IF(K 21)50,50,51
50 CONTINUE
KA=K
GO TO 52
51 CONTINUE
KA=21
52 CONTINUE
DO9L=2,KA
SCATI(L-1)=FFFV(NA)*D(LA)+SCATI(L-1)
LA=LA+25-L
9 CONTINUE
GO TO 10
6 CONTINUE
SOR=SOR+EFFV(NA)*D(MA+3)
LA=125+440*(I-1)
DO11L=1,20
IF(L K)12,13,13
12 CONTINUE
LA=LA+(25-L)
11 CONTINUE

```

```

13 CONTINUE
  DO14L=K,19
  SCATI(L+1)=EFFV(NA)*D(LA)+SCATI(L+1)
  LA=LA+1
14 CONTINUE
10 CONTINUE
  NA=NA+1
  MA=MA+440
  4 CONTINUE
  RETURN
  2 CONTINUE
  NA=440*(NCOMP(J)-1)+5*K-4
  IF(NCODE(2)-1)15,16,16
15 CONTINUE
  SOR=D(NA+4)
  LA=440*(NCOMP(J)-1)+124+K
  IF(K-21)30,30,31
30 CONTINUE
  KA=K
  GO TO 32
31 CONTINUE
  KA=21
32 CONTINUE
  DO17L=2,KA
  SCATI(L-1)=D(LA)
  LA=LA+25-L
17 CONTINUE
  RETURN
16 CONTINUE
  SOR=D(NA+3)
  LA=440*(NCOMP(J)-1)+126
  DO18L=1,15
  IF(L K)19,20,20
19 CONTINUE
  LA=LA+(25-L)
  GO TO 18
20 CONTINUE
  SCATI(L+1)=D(LA)
  LA=LA+1
18 CONTINUE
  RETURN
  END(0,0,0)

```

```

*      657          SUBROUTINE TSPAR
C
SUBROUTINE TSPAR(J,K,SCATI,E)
C
COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPE,KTAPE,MORE,D,
1COMP,REG,NMIX,R,EN,HE,FFV,ALFT,ARGT,LMAX,FPSK,NCODE,SEXM,
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DEL,NCOMP
3,A,M,N
C
DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN(100),
1HE(100),FFV(500),ALFT(25),ARGT(25),NCODE(20),SEXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100)
C
DIMENSION A(5,5)
C
DIMENSION SCATI(20)
C
DO 15 L=1,5
SCATI(L)=0
15 CONTINUE
IF(RFG(2*J-1)-E)2,3,2
3 CONTINUE
NA=NMIX*(NCOMP(J)-1)+1
DO 4 I=1,NMIX
LA=145+440*(I-1)
DO 5 L=2,21
IF(K L)6,7,7
7 CONTINUE
LA=LA+(25-L)
5 CONTINUE
6 CONTINUE
DO 8 L=1,5
SCATI(L)=D(LA)*EFFV(NA)+SCATI(L)
LA=LA+1
8 CONTINUE
NA=NA+1
4 CONTINUE
RETURN
2 CONTINUE
NA=145+440*(NCOMP(J)-1)
DO 10 L=2,21
IF(K L)11,12,12
12 CONTINUE
NA=NA+(25-L)
10 CONTINUE
11 CONTINUE
DO 13 L=1,5
SCATI(L)=D(NA)
NA=NA+1
13 CONTINUE
RETURN
END(0,0,0)

```



```

* 657 SUBROUTINE PMIX
C
SUBROUTINE PMIX(J,FPAR,F)
C
COMMON Q,CDT,NPAGF,NWOT,NDT,KDT,ITAPF,JTAPF,KTAPF,MORE,D,
1COMP,REG,NMIX,R,FN,HF,FFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SEXM,
2SEXP,FM,FP,VM,W,PHI,RK,V,AR,H,BETA,GAM,DFL,NCOMP
3,A,M,N
C
DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SEXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),
3RK(100),V(3000),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100)
C
DIMENSION A(5,5)
C
DIMENSION FPAR(25)
C
IF(REG(2*J-1)-F)2,3,2
2 CONTINUE
KB=440*(NCOMP(J)-1)+1
DO 5K=1,25
IF(NCODE(2)-1)6,7,7
6 CONTINUE
FPAR(K)=D(KB+3)
KR=KR+5
GO TO 5
7 CONTINUE
FPAR(K)=D(KB+4)
KR=KR+5
5 CONTINUE
RETURN
3 CONTINUE
NA=NMIX*(NCOMP(J)-1)+1
DO 4I=1,25
FPAR(K)=0
KR=5*(K-1)+1
DO 8J=1,NMIX
IF(NCODE(2)-1)9,10,10
9 CONTINUE
FPAR(K)=FPAR(K)+EFFV(NA)*D(KB+3)
GO TO 11
10 CONTINUE
IF(D(KB+4))11,11,12
12 CONTINUE
FPAR(K)=D(KB+4)
11 CONTINUE
KR=KR+440
NA=NA+1
8 CONTINUE
NA=NA-NMIX
4 CONTINUE
RETURN
END(0,0,0)

```

```
*      657          SUBROUTINE CTINT
C
C      FUNCTION CTINT(A,B,N1,N3,N)
C
C      COMMON Q,AR
C
C      DIMENSION Q(22187),AR(1050),A(2),R(2)
C
C      CTINT=0.0
C      N2=N3-1
C      DO 5 I=N1,N2
C      J=N+I
C      CTINT=CTINT+(A(J)*AR(I)+B(J+1)*AR(I+1))*(AR(I+1)-AR(I))/2.
5 CONTINUE
C      RETURN
C      END(0,0,0)
```

```
* 657 SUBROUTINE STINT
FUNCTION STINT(A,B,N1,N3,N)
C
COMMON Q,AR
C
DIMENSION Q(22187),AR(1050),A(2),B(2)
C
STINT=0.0
N2=N3-1
DO 5 I=N1,N2
J=N+I
STINT=STINT+(A(J)+B(J+1))*(AR(I+1)-AR(I))/2.
5 CONTINUE
10 CONTINUE
RETURN
END
```

CHAIN(5,B1) BLOCK F3

C

\* 657 CONTROL F-3

C

COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPE,KTAPE,MORE,D,  
1COMP,REG,NMIX,R,EN,HE,FFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SEXM,  
2SEXP,FM,FP,VM,W,PHI,RK,APHI,VOL,APOW,B,AR,H,BETA,GAM,DEL,NCOMP,  
3A,M,N

C

DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN(100),  
1HE(100),FFFV(500),ALFT(25),ARGT(25),NCODE(20),SEXM(150),  
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),  
3RK(100),AR(153),H(100),BETA(150),GAM(150),DEL(150),  
4NCOMP(100),APHI(2500),VOL(100),APOW(100),R(300),A(5,5)

C

CALL WOT(NWOT)

CALL NEWSET(NPAGE+1)

CALL HDING(Q(12))

CALL PREP

NRG=NCODE(1)

NA=2

NR=2

DO2J=1,NRG

NA=NA+XFIXF(ARSE(FN(J)))

IF(J NRG)7,8,8

8 CONTINUE

NA=NA+1

7 CONTINUE

WRITE OUTPUT TAPE 3,1000,AR(NB-1),FP(NB-1),SEXP(NR-1),(

1AR(I),FM(I),SEXM(I),I=NR,NA)

NB=NA+1

2 CONTINUE

IF (NCODE(6)-1) 3, 4, 4

3 CONTINUE

DO5K=1,20,5

KA=K

KB=K 4

WRITE OUTPUT TAPE 3,1001,(I,I=KA,KB)

JN=M\*(K-1)+1

DO9I=1,M

JM=I 4\*M+JN-1

WRITE OUTPUT TAPE 3,1002,AR(I),(PHI(JA),JA=JN,JM,M)

JN=JN+1

9 CONTINUE

5 CONTINUE

WRITE OUTPUT TAPE 3,1001,(I,I=21,25)

DO10I=1,M

JM=5\*I-4+20\*M

JN=JM+4

WRITE OUTPUT TAPE 3,1002,AR(I),(PHI(JA),JA=JM,JN)

10 CONTINUE

4 CONTINUE

DO12L=1,100

IF(RK(L))12,13,12

12 CONTINUE

```

LIT=100
GO TO 14
13 CONTINUE
LIT=L-1
14 CONTINUE
WRITE OUTPUT TAPE 3,1003,(I,RK(I),I=1,LIT)
DO 26 J=1,NRG
WRITE OUTPUT TAPE 3, 1012, J,VOL(J),APOW(J)
DO 25 K=1,25
KA=25*(J-1)+K
WRITE OUTPUT TAPE 3, 1007, K,APHI(KA)
25 CONTINUE
26 CONTINUE
DO 27 I=1,100
RK(I)=0.0
27 CONTINUE
IF (NCODE(5)-1) 30, 28, 30
28 CONTINUE
CALL GPHI
30 CONTINUE
CALL PAGES(NPAGE)
IF (NCODE(2)-2) 45, 32, 45
32 CONTINUE
NCODE(2)=0
M1=25*M
WRITE TAPE KTAPE, (PHI(I),I=1,M1)
IF (NCODE(5)-1) 40, 34, 40
34 CONTINUE
M1=1
M2=M
DO 36 I=1,20
WRITE TAPE KTAPE, (GPHIP(J),J=M1,M2),(GPHIM(J),J=M1,M2)
M1=M2+1
M2=(I+1)*M
36 CONTINUE
DO 38 I=1,5
M1=20*M+I
M2=25*M
WRITE TAPE KTAPE, (GPHIP(J),J=M1,M2,5),(GPHIM(J),J=M1,M2,5)
38 CONTINUE
40 CONTINUE
END FILE KTAPE
REWIND KTAPE
CALL CHAIN(3,R1)
45 CONTINUE
IF (XABSF(MORE)-2) 55, 50, 55
50 CONTINUE
CALL CHAIN(2,P1)
55 CONTINUE
CALL EXIT

```

C  
1000 FORMAT  
SPACE

RADIUS	FISSTON SOURCE	EXTERNAL SOURCE
--------	-------------------	--------------------

-0PF3	-1PE5	-1PE5			
REPEAT 1					
END OF FORMAT					
C					
1001 FORMAT					
RESTORE					
RELATIVE FLUX DISTRIBUTIONS					
SPACE					
RADIUS	GROUP -I	GROUP -I	GROUP -I	GROUP -I	GROUP -I
END OF FORMAT					
C					
1002 FORMAT					
-0PF3	-1PE5	-1PE5	-1PE5	-1PE5	-1PE5
END OF FORMAT					
C					
1003 FORMAT					
RESTORE					
ITERATION EIGENVALUE					
-I	-1PE7				
REPEAT 1					
END OF FORMAT					
C					
1007 FORMAT					
-I	-E7				
END OF FORMAT					
C					
1012 FORMAT					
RESTORE					
AVERAGES REGION NO -I					
SPACE					
VOLUME FRACTION -F7					
(REGION/CORE) AVERAGE POWER -F7					
SPACE					
GROUP AVERAGE FLUX					
END OF FORMAT					
C					
END(0,0,0)					

657

## SUBROUTINE PRFP

## SUBROUTINE PRFP

C

```
COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPF,KTAPF,MORF,D,
1COMP,REG,NMIX,R,EN,HE,FFFV,ALFT,ARGT,LMAX,FPSK,NCODE,SFXM,
2SEXP,FM,FP,VM,W,PHI,RK,APHI,VOL,APOW,B,AR,H,BETA,GAM,DEL,NCOMP,
3A,M,N
```

C

```
DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),EN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SFXM(150),
2SEXP(150),FM(150),FP(150),VM(5,5,150),W(750),PHI(3750),
3RK(100),AR(153),H(100),BETA(150),GAM(150),DEL(150),
4NCOMP(100),APHI(2500),VOL(100),APOW(100),B(300),A(5,5)
```

C

```
C THIS BLOCK NORMALIZES POWER DISTRIBUTION
C AND CALCULATES REGIONAL AVERAGES
```

C

```
NRG=NCODE(1)
AP=0.0
VCORF=0.0
KN=2
KP=1
DO100J=1,NRG
KN=KN+XFIXF(ARSF(EN(J)))
IF(J NRG)101,102,102
102 CONTINUE
KN=KN+1
101 CONTINUE
IF(EN(J))103,104,104
103 CONTINUE
IF(NCODE(3)-1)2,3,3
2 CONTINUE
AP=AP+STINT(FP,FM,KP,KN,0)
VCORF=VCORF-R(J)+R(J+1)
GOTO104
3 CONTINUE
AP=AP+CTINT(FP,FM,KP,KN,0)
VCORF=VCORF+R(J+1)**2/2. R(J)**2/2.
104 CONTINUE
KP=KN
100 CONTINUE
DO 20 I =1,N
FP(I)=FP(I)*VCORF/AP
FM(I 1)=FM(I+1)*VCORF/AP
20 CONTINUE
VTOT=0.0
KN=2
KP=1
DO450J=1,NRG
KN=KN+XFIXF(ARSF(FN(J)))
IF(J NRG)451,452,452
452 CONTINUE
KN=KN+1
451 CONTINUE
```

```

IF(NCODE(3)-1)23,24,24
23 CONTINUE
VOL(J)=R(J+1)-R(J)
APOW(J)=STINT(FP,FM,KP,KN,0)/VOL(J)
GOTO454
24 CONTINUE
VOL(J)=R(J+1)**2/2.-R(J)**2/2.
APOW(J)=CTINT(FP,FM,KP,KN,0)/VOL(J)
454 CONTINUE
VTOT=VTOT+VOL(J)
KP=KN
450 CONTINUE
DO 200 K=1,20
KP=1
KN=2
KM=M*(K-1)
DO201J=1,NRG
KN=KN+XFIXF(ARSF(FN(J)))
IF(J NRG)202,203,203
203 CONTINUE
KN=KN+1
202 CONTINUE
KA=K 25*(J-1)
IF(NCODE(3)-1)204,205,205
204 CONTINUE
APHI(KA)=STINT(PHI,PHI,KP,KN,KM)/VOL(J)
GOTO206
205 CONTINUE
APHI(KA)=CTINT(PHI,PHI,KP,KN,KM)/VOL(J)
206 CONTINUE
KP=KN
201 CONTINUE
200 CONTINUE
DO 56 K=1,5
KM=20*M+K
KA=20+K
J=1
SUM=0.0
DO 55 I=1,N
IF(NCODE(3)-1)51,52,52
51 CONTINUE
SUM=SUM+(PHI(KM)+PHI(KM+5))*(AR(I+1)-AR(I))/2.
GO TO 50
52 CONTINUE
SUM=SUM+(AR(I)*PHI(KM)+AR(I+1)*PHI(KM+5))*(AR(I+1)-AR(I))/2.
50 CONTINUE
IF(AR(I+1)-R(J 1))53,54,54
54 CONTINUE
APHI(KA)=SUM/VOL(J)
J=J+1
SUM=0.0
KA=KA+25
53 CONTINUE
KM=K 4+5
55 CONTINUE

```



56 CONTINUE

DO207J=1,NRG

VOL(J)=VOL(J)/VTOT

207 CONTINUE

RETURN

END(0,0,0)

```

*      657          SUBROUTINE GPFI
C
C      SUBROUTINE GPFI
C
C      THIS SUBROUTINE COMPUTES FLUX GRADIENTS USING
C      A CENTRAL DIFFERENCE APPROXIMATION EXCEPT AT
C      REGION INTERFACES AND NEAR THE INNER AND
C      OUTER BOUNDARIES      REQUIRED STORAGE 7500
C      MAXIMUM IS OBTAINED BY OVERLAY ON VM AND V
C
C      COMMON Q,CDT,NPAGE,NWOT,NDT,KDT,ITAPE,JTAPE,KTAPE,MORE,D,
1COMP,REG,NMIX,R,EN,HE,FFV,ALFT,ARGT,LMAX,FPSK,NCODE,SEXM,
2SEXP,FM,FP,GHIP,W,PHI,RK,GPHIM,AR,H,BETA,GAM,DFL,NCOMP,
3A,M,N
C
C      DIMENSION Q(12),CDT(303),D(8800),COMP(40),REG(200),R(101),FN(100),
1HE(100),EFFV(500),ALFT(25),ARGT(25),NCODE(20),SFXM(150),SEXP(150),
2FM(150),FP(150),GHIP(3750),W(750),PHI(3750),RK(100),
3GPHIM(3000),AR(153),H(100),BETA(150),GAM(150),DFL(150),
4NCOMP(100),A(5,5)
C
C      DIMENSION SCATI(20),TSCATI(5),TSCAT(5,5),DIF(5),
1RXST(5),RTEMP(153)
C
C      CALL WOT(NWOT)
DO 100 I=1,153
RTEMP(I)=AR(I)
100 CONTINUE
DO 2 K=1,20
KM=1 M*(K-1)
J=1
CALL RPAR(RXS,DIFC,K,J,6H MIX )
GPHIM(KM)=0.0
GHIP(KM)=(1.-ALFT(K))/(1.+ALFT(K))/(2.*DIFC)*PHI(KM)
CALL SPAR(S,SCATI,K,J,6H MIX )
GPHIM(KM+1)=S*FM(2)-RXS*PHI(KM+1)
GPHIM(KM+2)=S*FM(3)-RXS*PHI(KM+2)
IF(NCODE(2)-1)3,4,4
3 CONTINUE
DO 5L=1,20
IF(L K)6,5,5
6 CONTINUE
LA=M*(L-1)+2
GPHIM(KM+1)=GPHIM(KM+1)+SCATI(L)*PHI(LA)
GPHIM(KM+2)=GPHIM(KM+2)+SCATI(L)*PHI(LA+1)
5 CONTINUE
GO TO 7
4 CONTINUE
DO 8L=1,20
IF(L K)8,8,9
9 CONTINUE
LA=M*(L-1)+2
GPHIM(KM+1)=GPHIM(KM+1)+SCATI(L)*PHI(LA)
GPHIM(KM+2)=GPHIM(KM+2)+SCATI(L)*PHI(LA+1)
8 CONTINUE

```

```

CALL TSPAR(J,K,TSCATI,6H MIX )
LA=20*M+6
DO10L=1,5
GPHIM(KM+1)=GPHIM(KM+1)+TSCATI(L)*PHI(LA)
GPHIM(KM+2)=GPHIM(KM+2)+TSCATI(L)*PHI(LA+5)
LA=LA+1
10 CONTINUE
7 CONTINUE
GPHIM(KM+1)=-GPHIM(KM+1)*(.001*H(1))/(2.*DIFC)+(PHI(KM 1)-
1PHI(KM))/.001*H(1)
GPHIM(KM+2)=-(.997*H(1))/(2.*DIFC)*GPHIM(KM+2)+(PHI(KM 2)
1-PHI(KM+1))/.997*H(1)
GPHIP(KM+1)=GPHIM(KM+1)
GPHIP(KM+2)=GPHIM(KM+2)
KM=KM+3
MA=M 3
DO11J=4,MA
IF(AR(I)-R(J+1))12,13,13
12 CONTINUE
GPHIM(KM)=(PHI(KM+1)-PHI(KM-1))/(2.*H(J))
GPHIP(KM)=GPHIM(KM)
KM=KM+1
GO TO 11
13 CONTINUE
GPHIM(KM)=S*FM(I)-RXS*PHI(KM)
IF(NCODE(2)-1)14,15,15
14 CONTINUE
DO16L=1,20
IF(L K)17,16,16
17 CONTINUE
LA=M*(L-1)+I
GPHIM(KM)=GPHIM(KM)+SCATI(L)*PHI(LA)
16 CONTINUE
GO TO 18
15 CONTINUE
DO19L=1,20
IF(L K)19,19,20
20 CONTINUE
LA=M*(L-1)+1
GPHIM(KM)=GPHIM(KM)+SCATI(L)*PHI(LA)
19 CONTINUE
LA=20*M+5*I-4
DO21L=1,5
GPHIM(KM)=GPHIM(KM)+TSCATI(L)*PHI(LA)
LA=LA+1
21 CONTINUE
18 CONTINUE
GPHIM(KM)=(PHI(KM)-PHI(KM-1))/H(J) H(J)/(2.*DIFC)*GPHIM(KM)
J=J+1
CALL RPAR(RXS,DIFC,K,J,6H MIX )
CALL SPAR(S,SCATI,K,J,6H MIX )
CALL TSPAR(J,K,TSCATI,6H MIX )
GPHIP(KM)=S*FP(I)-RXS*PHI(KM)
IF(NCODE(2)-1)22,26,26
22 CONTINUE

```

```

DO23L=1,20
IF(L K)24,23,23
24 CONTINUE
LA=M*(L-1)+I
GPHIP(KM)=GPHIP(KM)+SCATI(L)*PHI(LA)
23 CONTINUE
GO TO 25
26 CONTINUE
DO27L=1,20
IF(L K)27,27,28
28 CONTINUE
LA=M*(L-1)+I
GPHIP(KM)=GPHIP(KM)+SCATI(L)*PHI(LA)
27 CONTINUE
LA=20*M+5*I-4
DO29L=1,5
GPHIP(KM)=GPHIP(KM)+TSCATI(L)*PHI(LA)
LA=LA+1
29 CONTINUE
25 CONTINUE
GPHIP(KM)=(PHI(KM+1)-PHI(KM))/H(J) H(J)/(2.*DIFC)*GPHIP(KM)
KM=KM+1
11 CONTINUE
GPHIP(KM)=S*FP(M-2)-RXS*PHI(KM)
GPHIP(KM+1)=S*FP(M-1)-RXS*PHI(KM+1)
IF(NCODE(2)-1)30,31,31
30 CONTINUE
DO32L=1,20
IF(L K)33,32,32
33 CONTINUE
LA=M*L
GPHIP(KM)=GPHIP(KM)+SCATI(L)*PHI(LA-2)
GPHIP(KM+1)=GPHIP(KM+1)+SCATI(L)*PHI(LA-1)
32 CONTINUE
GO TO 35
31 CONTINUE
DO36L=1,20
IF(L K)36,36,37
37 CONTINUE
LA=M*L
GPHIP(KM)=GPHIP(KM)+TSCATI(L)*PHI(LA-2)
GPHIP(KM+1)=GPHIP(KM+1)+TSCATI(L)*PHI(LA-1)
36 CONTINUE
LA=25*M
DO38L=1,5
GPHIP(KM)=GPHIP(KM)+TSCATI(L)*PHI(LA-14)
GPHIP(KM+1)=GPHIP(KM+1)+TSCATI(L)*PHI(LA-9)
LA=LA+1
38 CONTINUE
35 CONTINUE
GPHIP(KM)=(PHI(KM+1)-PHI(KM))/(.997*H(J))+(.997*H(J))/
1(2.*DIFC)*GPHIP(KM)
GPHIP(KM)=GPHIP(KM)
GPHIP(KM+1)=(PHI(KM+2)-PHI(KM+1))/(.001*H(J))+(.001*H(J))/
1(2.*DIFC)*GPHIP(KM+1)

```

```

GPHIM(KM+1)=GPHIP(KM+1)
KM=KM+2
GPHIM(KM)=-((1. ARGT(K))/(1.+ARGT(K)))/(2.*DIFC)*PHI(KM)
GPHIP(KM)=0.0
2 CONTINUE

C
C GRADIENTS AT THERMAL
DO50K=1,5
J=1
CALL TMIX(J,DIF,RXST,TSCAT,6H MIX )
KM=20*M+K
KA=20+K
GPHIM(KM)=0.0
GPHIP(KM)=((1.-ALFT(KA))/(1.+ALFT(KA)))/(2.*DIF(K))*PHI(KM)
CALL SPAR(S,SCATI,KA,J,6H MIX )
GPHIM(KM+5)=-RXST(K)*PHI(KM+5)
GPHIM(KM+10)=-RXST(K)*PHI(KM+10)
IF(NCODE(2)-1)53,54,54
53 CONTINUE
DO51L=1,20
LA=M*(L-1)+2
GPHIM(KM+5)=GPHIM(KM+5)+SCATI(L)*PHI(LA)
GPHIM(KM+10)=GPHIM(KM+10)+SCATI(L)*PHI(LA+1)
51 CONTINUE
LA=KM
DO52L=1,5
GPHIM(KM+5)=GPHIM(KM+5)+TSCAT(L,K)*PHI(LA+5)
GPHIM(KM+10)=GPHIM(KM+10)+TSCAT(L,K)*PHI(LA+10)
LA=LA+1
52 CONTINUE
GO TO 55
54 CONTINUE
LA=KM
DO56L=1,5
GPHIM(KM+5)=GPHIM(KM+5)+TSCAT(K,L)*PHI(LA+5)
GPHIM(KM+10)=GPHIM(KM+10)+TSCAT(K,L)*PHI(LA+10)
LA=LA+1
56 CONTINUE
GPHIM(KM+5)=GPHIM(KM+5)+S*FM(I+1)
GPHIM(KM+10)=GPHIM(KM+10)+S*FM(I+2)
55 CONTINUE
GPHIM(KM+5)=GPHIM(KM+5)*(.001*H(1))/(2.*DIF(K))-
1*(PHI(KM+10)-PHI(KM+5))/(.001*H(1))
GPHIM(KM+10)=GPHIM(KM+10)*(.997*H(1))/(2.*DIF(K))-
1*(PHI(KM+15)-PHI(KM+10))/(.997*H(1))
GPHIP(KM+5)=GPHIM(KM+5)
GPHIP(KM+10)=GPHIM(KM+10)
KM=KM+15
DO60I=4,MA
IF(AR(I)-R(J+1))61,62,62
61 CONTINUE
GPHIM(KM)=(PHI(KM+5)-PHI(KM-5))/(2.*H(J))
GPHIP(KM)=GPHIM(KM)
KM=KM+5
GO TO 60

```

```

62 CONTINUE
  GPHIM(KM)=-RXST(K)*PHI(KM)
  IF(NCODE(2)-1)64,65,65
64 CONTINUE
  DO63L=1,5
  LA=20*M+5*I-5+L
  GPHIM(KM)=GPHIM(KM)+TSCAT(L,K)*PHI(LA)
63 CONTINUE
  DO66L=1,20
  LA=M*(L-1)+I
  GPHIM(KM)=GPHIM(KM)+SCATI(L)*PHI(LA)
66 CONTINUE
  GO TO 67
65 CONTINUE
  DO68L=1,5
  LA=20*M+5*I-5+L
  GPHIM(KM)=GPHIM(KM)+TSCAT(K,L)*PHI(LA)
68 CONTINUE
  GPHIM(KM)=GPHIM(KM)+S*FM(I)
67 CONTINUE
  GPHIM(KM)=(PHI(KM)-PHI(KM-1))/H(J) H(J)/(2.*DIF(K))*
1GPHIM(KM)
  J=J+1
  CALL TMIX(J,DIF,RXST,TSCAT,6H MIX )
  CALL SPAR(S,SCATI,KA,J,6H MIX )
  GPHIP(KM)=-RXST(K)*PHI(KM)
  IF(NCODE(2)-1)69,70,70
69 CONTINUE
  DO71L=1,5
  LA=20*M+5*I-5+L
  GPHIP(KM)=GPHIP(KM)+TSCAT(L,K)*PHI(LA)
71 CONTINUE
  DO72L=1,20
  LA=M*(L-1)+I
  GPHIP(KM)=GPHIP(KM)+SCATI(L)*PHI(LA)
72 CONTINUE
  GO TO 73
70 CONTINUE
  DO74L=1,5
  LA=20*M+5*I-5+L
  GPHIP(KM)=GPHIP(KM)+TSCAT(K,L)*PHI(LA)
74 CONTINUE
  GPHIP(KM)=GPHIP(KM)+S*FP(I)
73 CONTINUE
  GPHIP(KM)=(PHI(KM+5)-PHI(KM))/H(J) H(J)/(2.*DIF(K))
1*GPHIP(KM)
  KM=KM+5
60 CONTINUE
  GPHIP(KM)=-RXST(K)*PHI(KM)
  GPHIP(KM+5)=-RXST(K)*PHI(KM+5)
  IF(NCODE(2)-1)80,81,81
80 CONTINUE
  DO82L=1,5
  LA=KM-1+L
  GPHIP(KM)=GPHIP(KM)+TSCAT(L,K)*PHI(LA)

```

```

      GPHIP(KM+5)=GPHIP(KM+5)+TSCAT(L,K)*PHI(LA+5)
82 CONTINUE
   DO83 L=1,20
      LA=M*L-2
      GPHIP(KM)=GPHIP(KM)+SCATI(L)*PHI(LA)
      GPHIP(KM+5)=GPHIP(KM+5)+SCATI(L)*PHI(LA+1)
83 CONTINUE
      GOTO85
81 CONTINUE
      GPHIP(KM+5)=GPHIP(KM+1)+S*FP(M-1)
      GPHIP(KM)=GPHIP(KM)+S*FP(M-2)
   DO84 L=1,5
      LA=KM-1+L
      GPHIP(KM)=GPHIP(KM)+TSCAT(K,L)*PHI(LA)
      GPHIP(KM+5)=GPHIP(KM+5)+TSCAT(L,K)*PHI(LA+5)
84 CONTINUE
85 CONTINUE
      GPHIP(KM)=(PHI(KM+5)-PHI(KM))/(.997*H(J))+(.997*H(J))
      1/(2.*DIF(K))*GPHIP(KM)
      GPHIM(KM)=GPHIP(KM)
      GPHIP(KM+5)=(PHI(KM+10)-PHI(KM+5))/(.001*H(J))+(.001*
      1H(J))/(2.*DIF(K))*GPHIP(KM+5)
      GPHIM(KM+5)=GPHIP(KM+5)
      KM=KM+10
      GPHIP(KM)=0.0
      GPHIM(KM)=-((1. ARGT(K+20))/(1.+ARGT(K+20)))/(2.*DIF(K))*PHI(KM)
50 CONTINUE
      IF (NCODE(6)-1) 110, 150, 150
110 CONTINUE
      DO 125 I=1,20,2
      KA=I
      KB=I 1
      PRINT 1001, (NG,NG=KA,KB)
      PRINT 1005
      M2=(I+1)*M
      DO 120 J=1,M
      M1=(I-1)*M+J
      PRINT 1002, RTEMP(J),(GPHIM(L),GPHIP(L),L=M1,M2,M)
120 CONTINUE
125 CONTINUE
      DO 135 I=1,3,2
      KA=I 20
      KB=I 21
      PRINT 1001, (NG,NG=KA,KB)
      PRINT 1005
      DO 130 J=1,M
      M1=20*M+5*(J-1)+I
      M2=M1+1
      PRINT 1002, RTEMP(J),GPHIM(M1),GPHIP(M1),GPHIM(M2),GPHIP(M2)
130 CONTINUE
135 CONTINUE
      NG=25
      PRINT 1003, NG
      DO 140 J=1,M
      M1=20*M+5*J

```

---

```
PRINT 1002, RTEMP(J),GPHIM(M1),GPHIP(M1)
```

```
140 CONTINUE
```

```
150 CONTINUE
```

```
RETURN
```

---

```
C
```

```
1001 FORMAT(1H17773IX,14HFLUX GRADIENTS//19X,6HGROUP I2,21X,6HGROUP I2)
```

```
C
```

```
1002 FORMAT(0PF8.3,1PE15.5,1PE13.5,1PE15.5,1PE13.5)
```

```
C
```

```
1003 FORMAT(1H17773IX,14HFLUX GRADIENTS//19X,6HGROUP I2//7H RADIUS8X,4H  
1LEFT9X,5HRIGHT)
```

```
C
```

```
1005 FORMAT(7HORADIUS8X,4HLEFT9X,5HRIGHT10X,4HLEFT9X,5HRIGHT)
```

```
C
```

```
END
```

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