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FAST NEUTRONS INCIDENT ON VANADIUM by

Alan B. Smith, James F. Whalen, and Kanji Takeuchi

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Reactor Physics Division

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# FAST NEUTRONS INCIDENT ON VANADIUM 

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#### Abstract

Total neutron cross sections and elastic and. inelastic neutron scattering cross sections are experimentally studied. Total neutron cross sections are determined with good resolution ( 21 keV ) from 0.1 to 1.45 MeV . Differential elastic and inelastic scattering angular distributions are measured at incident neutron energy intervals of $\lesssim 10 \mathrm{keV}$ from 0.3 to 1.5 MeV with incident neutron resolutions of $\sim 20 \mathrm{keV}$. The inelastic excitation of states at $330 \pm 10 \mathrm{keV}$ and $926 \pm 10 \mathrm{keV}$ is observed. The experimental. results are interpreted in terms of the optical model and statistical concepts, inclusive of resonance width fluctuations and correlations. The observed intermediate structure is discussed in the context of strongly overlapping resonances and distributions in resonance widths and spacings and in terms of an intermediate optical model. Comparison is made with previously reported experimental values and with the pertinent contents of the evaluated data file, ENDF-B.. Numerical tabulations of the experimental results are provided.


## I. INTRODUCTION

The objective of this study was to improve the understanding of total neutron cross sections and of the elastic and inelastic scattering cross sections of vanadium at incident energies up to 1.5 MeV . Natural vanadium is monoisotopic, lies near the peak of the $s$-wave strength function, is magic in neutron number, and has relatively low-lying states, which are appreciably excited by inelastic neutron scattering processes. These collective properties are unusual, and many of them have been associated with the prevalence of intermediate structure in neutron processes. ${ }^{1}$ The relatively large inelastic excitations make possible the comparison of such intermediate structure between several reaction channels. The present work gave considerable attention to the experimental accuracies and energy resolutions in an effort to well define the energy-dependent structure.

In the discussion, Section II outlines the techniques used in the experimental portions of the study. The experimental results are presented in Section III and comparisons made with previously reported values. Section IV is devoted to the physical interpretation of the measured results. A broad energy average of the measured values is described in terms of a conventional optical potential ${ }^{2}$ and statistical concepts ${ }^{3}$ inclusive of resonance width fluctuations. ${ }^{4}$ The observed intermediate structure is discussed in the context of (a) strongly overlapping compound nucleus resonances, ${ }^{5}$ (b) fluctuations in widths and spacings of isolated or partially overlapping resonances, ${ }^{6,7}$ and (c) an intermediate optical potential assuming reaction processes proceeding through "doorway" states. ${ }^{8,9}$ Section V compares the results of the present study with the comparable physical quantities in the evaluated data file ENDF-B. ${ }^{10}$ This comparison may prove of interest to the reactor physicist. Section VI consists of some brief summary remarks. The appendix presents experimental results in detailed tabular form.

## II. EXPERIMENTAL METHOD

Fast-neutron time-of-flight techniques were used in all the scattering measurements and a portion of the total cross-section determinations. The experimental neutron-scattering apparatus, inclusive of a pulsed and bunched Van de Graaff accelerator, a multiangle detection system, on-line computer usage, and associated data-processing procedures, has been described in detail and will not be further defined here. ${ }^{11,12}$ All measurements used the reaction ${ }^{7} \mathrm{Li}(\mathrm{p}, \mathrm{n})^{7} \mathrm{Be}$ as a neutron source, the intensity of which was monitored using "long counters" and proton-recoil scintillators. ${ }^{13}$ The scattering samples were right cylinders $(2.0 \mathrm{~cm}$ in diameter and 2.0 cm high) fabricated of natural vanadium metal. The chemical purity of the metal was $\gtrsim 98 \%$. Neutrons were incident upon the lateral surfaces of the scattering samples. All scattering measurements were made relative to the known differential elastic scattering cross sections of carbon and corrected for multiple scattering, incident-beam attenuation, and angular-resolution effects. ${ }^{11,14}$

Total neutron cross sections were determined from neutron transmissions measured using a pseudowhite pulsed-source technique or the monoenergetic source method. ${ }^{12,15}$ The latter method was used exclusively below incident neutron energies of $\sim 500 \mathrm{keV}$. All neutron transmission measurements and reduction to total cross sections were carried out in an automated manner as described in Ref. 12. Transmission samples of natural vanadium varied in geometry, but generally were such as to provide transmissions of greater than $50 \%$.

## A. Total Neutron Cross Sections

The experimental total cross-section results in the measured interval 0.l-1.45 MeV are shown in the upper portion of Fig. l. Numerical values are given in Table $V$ (in the appendix). At incident neutron energies of $<0.5 \mathrm{MeV}$, the experimental energy resolution was $1.5-2.5 \mathrm{keV}$. At higher energies, the velocity resolution was estimated to be $0.1-0.12 \mathrm{nsec} / \mathrm{m}$, from direct observation of the prompt gamma-ray burst and the width of narrow resonance peaks. The energy scale of the monoenergetic measurements was calibrated against the ${ }^{7} \mathrm{Li}(\mathrm{p}, \mathrm{n})^{7} \mathrm{Be}$ reaction threshold of $1.882 \mathrm{MeV} .{ }^{16}$ Energy calibration errors in this method should have been less than 3 keV . The time-of-flight measurements were calibrated against the velocity of light and spot-checked using the above monoenergetic method. The error in the time-of-flight energy scale was judged appreciably less than 10 keV , with the larger uncertainties at the higher energies. The stated crosssection errors were derived from counting statistics. "In scattering" corrections were estimated, found small, and neglected.


112-9505 Rev. 1
Fig. 1. Measured Total Neutron Cross Sections of Vanadium. Top, basic measured data; center, data averaged over a $50-\mathrm{keV}$ interval; bottom, data averaged over a $100-\mathrm{keV}$ interval.

Generally, the present results compared favorably with those obtained by other workers. ${ }^{17}$. Values reported by Cabe et al., in the interval $0.4-1.2 \mathrm{MeV}$ follow the energy average of the present higher-resolution values. ${ }^{18}$ The present work is consistent with the detailed results of Rohr and Friedland and of Firk et al., reported for incident neutron energies of $\$ 200 \mathrm{keV} .{ }^{19,20}$

## B. Elastic Cross Sections

The differential elastic neutron-scattering cross sections were determined at incident neutron-energy intervals of $\lesssim 10 \mathrm{keV}$ with an incident neutron-energy resolution of $20 \pm 5 \mathrm{keV}$. The angular range of the measurements at each incident energy was from $\sim 25$ to $\sim 155^{\circ}$, usually covered in eight angular intervals. Typical values of the laboratory scattering angles were $27,38,53,69,84,114,129$, and $154^{\circ}$. The scattering angles were not always identical, but were carefully determined at each measurement. Angular resolutions varied, but were of the order of a few degrees. As indicated by the illustrative time spectra of Fig. 2, the scattered neutron velocity resolution of $1.5-2.0 \mathrm{nsec} / \mathrm{m}$ was sufficient to resolve the elastic scattered neutrons from inelastic scattered components.


Fig. 2
Time-of-flight Spectra Obtained for Vanadium at a Laboratory Scattering Angle of $114^{\circ}$. Flight path was $\sim 203 \mathrm{~cm}$, and time per channel $\sim 1.05 \mathrm{nsec}$. Elastic and inelastic scattered neutron groups are evident. Backgrounds have been subtracted, and vertical bars indicate standard deviation of respective points. No detector-sensitivity correction has been made. Reaction Q values associated with the various neutron groups are indicated in MeV .

The experimental results were expressed in the following alternate forms:
and

$$
\begin{equation*}
\frac{\mathrm{d} \sigma}{\mathrm{~d} \Omega}=\frac{\sigma}{4 \pi}\left[1+\sum_{i=1}^{4} \omega_{\mathrm{i}} \mathrm{P}_{\mathrm{i}}\right] \tag{1}
\end{equation*}
$$


where $P_{i}$ are Legendre polynomials expressed in the laboratory system and $\sigma, \omega$, and $B$ are parameters derived by least-squares fitting Eq. 1 to experimentally measured differential distributions. The expansions of Eq. l were terminated at $i=4$, as the magnitudes of higher-order terms did not generally exceed their corresponding uncertainties. Expressed in either of the above forms, the results were descriptive of the measured data points (see Fig. 3), and parameter values obtained from measurements at slightly different incident energies or scattering angles were easily comparable. However, extrapolation of the results, expressed in the forms of Eq. l, beyond the measured angular interval of $\sim 25$ to $\sim 155^{\circ}$, is not necessarily valid.


Fig. 3
Experimentally Observed Elastic and Inelastic Angular Distributions for Vanadium (data points). Solid curve is obtained from the least-squares fit of Eq. I to the experimental elastic scattering measurements. The dotted curve is an eye guide to the inelastic scattering angular distribution.

As expected from the multiresonance nature of the total neutron cross section (see Fig. 1), the elastic scattering cross sections varied rapidly with incident energy. Small experimental variations in incident neutron energy and/or energy spread could, and did, result in quite different measured cross-section values. To provide consistent experimental results, the measured differential elastic cross sections were progressively averaged over a square energy increment with a width of several experimental resolutions. Figure 4 shows results obtained with a $50-\mathrm{keV}$ averaging increment. Table VI (in the appendix) lists the numerical parameter values derived from the differential measurements. Assay of the experimental errors was complex and subjective. Generally, it was estimated that the elastic scattering cross sections were determined to an accuracy of $\sim 8 \%$, inclusive of uncertainties in the cross section of the carbon standard. The stated uncertainties in the angular-distribution coefficients represent standard deviations derived from the least-squares fitting procedures.

The elastic scattering results were generally consistent with the total cross section (see Section A above) as indicated in Fig. 5 and with the reported total scattering results of Ref. 14. The agreement between the present results and those obtained using a soft fission spectrum ${ }^{21}$ was less satisfactory.
 112-9471 Rev. 2

Fig. 4
Differential Elastic Scattering Cross Sections of Vanadium Given in the Format of Eq. 1 . A $50-\mathrm{keV}$ average of the measurements is indicated by the data points. The solid and dashed curves are the result of calculation (O.M.) as described in Section IV.A.


112-9503 Rev. 1
Fig. 5. Comparison of Experimental Total Neutron Cross Sections (vertical bars) and Total Elastic Scattering Cross Sections (boxes) of Vanadium

## C. Inelastic Neutron Scattering

The inelastic excitation of states in vanadium at $330 \pm 10$ and $926 \pm 10 \mathrm{keV}$ was observed. The energy values were derived from the calibrated time scale of the velocity spectrometer and verified by observation of the excitation of the well-known $845-\mathrm{keV}$ state in iron, ${ }^{22}$ These levels were attributed to reported states at 320 and 930 keV , respectively. ${ }^{22}$ The latter published values were accepted as the more accurate. Additional. states in vanadium have been reported at 480,645 , and $1160 \mathrm{keV} .{ }^{22-24}$ In the se experiments, any state at $\sim 480 \mathrm{keV}$ would have been partly obscured by the presence of elastically scattered neutrons from the second neutron group of the ${ }^{7} \mathrm{Li}(\mathrm{p}, \mathrm{n})^{7} \mathrm{Be}$ source reaction. ${ }^{16}$ However, it was felt that a cross section for the excitation of a $480-\mathrm{keV}$ state of $\gtrsim 10.0 \mathrm{mb} / \mathrm{sr}$ would have resulted in an observable inelastically scattered neutron group. None was evident. Inelastic scattered neutrons $(Q=-0.32 \mathrm{MeV})$ resulting from the second source group were clearly seen (see Fig. 2). A nearby neutron
group at a somewhat higher scattered neutron energy due to the excitation of a $645-\mathrm{keV}$ state would have been observed if the respective cross section was $\gtrsim 2 \mathrm{mb} / \mathrm{sr}$. No group corresponding to such a magnitude was observed. The experimental results indicated an upper limit of $\sim 4 \mathrm{mb} / \mathrm{sr}$ for the excitation of any state in the vicinity of 1.16 MeV . Within this limitation, there was no evidence for such a level. Thus there was no positive evidence in the present experiments for states in vanadium at approximately 480,645 , and/or 1160 keV . If present, such states probably have spins and parities requiring $\ell \geq 2$ incident neutron momentum for appreciable excitation. This conclusion is consistent with the results of recent inelastic neutron-scattering measurements at higher incident energies ${ }^{25}$ and with the results of recent shell-model calculations. ${ }^{26}$

The differential cross sections for the excitation of the 320-and $930-\mathrm{keV}$ states were measured from several hundred keV of threshold to a maximum incident energy of 1.5 MeV . Generally the measurements were made at the same scattering angles as employed in the elastic scattering studies. Many of the measured inelastic angular distributions were essentially isotropic. (See Fig. 3, for example.) Thus the angle-integrated inelastic-excitation cross sections were reasonably obtained by averaging the differential measurements and multiplying by $4 \pi$. Even for the more anisotropic distributions observed, this approximate procedure was judged acceptable since it led to overestimates of the excitation cross sections by $\lesssim 5 \%$. The resulting angle-integrated excitation cross sections are shown in Fig. 6 and listed in Tables VII and VIII (in the appendix). As was true for the elastic cross sections, the results varied with energy because of the partially resolved resonance structure and experimental uncertainties in the precise incident energy and incident-energy spread. The uncertainties associated with the individual cross-section measurements are complex composites of statistical and instrumental effects and were subjectively estimated. Those indicated in Fig. 6 and Tables VII and VIII are best estimates of the standard deviation inclusive of uncertainties in the reference standard cross section of carbon.


Fig. 6
Measured Cross Sections for the Excitation of States in Vanadium at 0.32 and $0.93 \mathrm{MeV}_{8}$ (crosses). The solid curve was obtained by calculation as described in Section IV.A. Estimated experimental uncertainties are indicated by vertical bars of the data crosses. 113-501 Rev. 1

The measured differential cross sections for the excitation of the $320-\mathrm{keV}$ state were carefully assayed and the "better" angular distributions fitted, by the method of least squares, with the expression

$$
\begin{equation*}
\frac{\mathrm{d} \sigma}{\mathrm{~d} \omega}=\mathrm{B}_{0}+\mathrm{B}_{1} \mathrm{P}_{1}+\mathrm{B}_{2} \mathrm{P}_{2} \tag{2}
\end{equation*}
$$

The resulting $B_{i}$ parameters were found to be very energy-dependent and were smoothed by averaging over a $20-\mathrm{keV}$ incident energy increment. Figure 7 shows the resulting average energy dependence of these parameters. Though the parameters still vary appreciably, it is evident that (a) the cross section ( $\sigma=4 \pi B_{0}$ ) has the same magnitude and energy dependence as that shown in Fig. 6, and (b) $B_{1}$ tends to be less than $B_{2}$, both on the average and in magnitude of the fluctuations. Further, there appears to be a qualitative correlation between fluctuations in $B_{2}$ and $B_{0}$. Instrumental effects may have contributed to the structure and anisotropy. Such perturbations were most likely at forward angles; thus most affect the $\mathrm{B}_{1}$ coefficient. Such a premise is not strongly supported by the results of Fig. 7. Coincidence may have led to measurements locally correlated with compound-nucleus resonance structure, resulting in systematic perturbation of measured magnitudes or angular distributions. The abundance of data and the random mode of its procurement over a several-year period made this hypothesis unlikely.

The present results can be compared with the few previously reported values. Towle reports cross sections for the excitation of the 320 - and $930-\mathrm{keV}$ states at incident energies of $\sim 1.5 \mathrm{MeV}$ similar to the results of the present work. ${ }^{25}$ Results of ( $n: n^{\prime} \gamma$ ) measurements by Mather et al., at $0.8,1.0$, and 1.5 MeV are consistent with the values obtained in the present work when cognizance is taken of the anisotropy of the emitted quanta and the effects of branching ratios. ${ }^{27}$ Barrows reports ( $n: n^{\prime} \gamma$ ) results at incident energies of 1.83 MeV and above. ${ }^{28}$ When extrapolated downward to the $1.5-\mathrm{MeV}$ maximum energy of the present work, Barrows' results are slightly $(\sim 20 \%)$ higher than those reported here. This may in part be due to the use of the rapidly varying $\operatorname{Fe}\left(n ; n^{\prime} \gamma\right)(Q=-0.85 \mathrm{MeV})$ cross section as a reference standard in Barrows' work.
A. Optical Model and Statistical Calculations

The optical model and statistical methods were used in the phenomenological interpretation and extrapolation of the experimental results. ${ }^{2,3,30,31}$ The potential employed was based upon the surface absorption model of Moldauer. ${ }^{32}$ The latter has been extended by Engelbrecht and Fiedeldey to an equivalent nonlocal potential of the form ${ }^{29}$

$$
\mathrm{V}_{\mathrm{c}}(\mathrm{r})=-(\mathrm{V}+\mathrm{iU}) \mathrm{f}_{1}(\mathrm{r})-\mathrm{if}_{2}(\mathrm{r}) \mathrm{W}+\mathrm{V}_{\mathrm{so}}\left(\frac{\hbar}{\mu_{\pi} \mathrm{c}}\right)^{2} \underline{\sigma} \cdot \ell \frac{1}{\mathrm{r}} \frac{\mathrm{df}}{\mathrm{~d}} \mathrm{r},
$$

where

$$
\begin{align*}
\mathrm{f}_{1}(\mathrm{r}) & =\left[1+\exp \left(\frac{\mathrm{r}-\mathrm{R}_{1}}{\mathrm{a}_{1}}\right)\right]^{-1}, \\
\mathrm{f}_{2}(\mathrm{r}) & =\exp \left[-\left(\frac{\mathrm{r}-\mathrm{R}_{2}}{\mathrm{a}_{2}}\right)^{2}\right], \\
R_{1} & =r_{1}+r_{0} A^{1 / 3}, \quad R_{2}=R_{1}+r_{2}, \\
r_{0} & =1.16 \mathrm{f}, \quad \mathrm{r}_{1}=0.6 \mathrm{f}, \quad \mathrm{r}_{2}=0.5 \mathrm{f},  \tag{3}\\
\mathrm{a}_{1} & =0.62 \mathrm{f}, \quad \mathrm{a}_{2}=0.5 \mathrm{f}, \\
\mathrm{~V}^{*} & =V_{0}-0.25 \mathrm{E}, \\
\mathrm{~W}^{*} & =W_{0}-0.2 \mathrm{E}, \\
V_{\mathrm{S} 0} * & =7.0,
\end{align*}
$$

and

$$
U^{*}=0.125 \mathrm{E}-0.0004 \mathrm{E}^{2}
$$

If we let $E \rightarrow 0$ and $V \rightarrow 0$ and set $V_{0}=46$ and $W_{0}=14 \mathrm{MeV}$, Eq. 3 becomes the potential of Moldauer. This potential and the Hauser-Feshbach formalism give a good description of the low-energy observed elastic scattering (dashed curves of Fig. 4) and lead to calculated $\ell=0$ strength functions similar to those experimentally observed. ${ }^{34}$

A detailed description of the observed structure in the elastic scattering was sought by varying $\mathrm{V}_{0}$ and $\mathrm{W}_{0}$ ( $\mathrm{U}=0$, and other parameters maintained constant) to obtain the best fit to the individual observed elastic scattering angular distributions. ${ }^{33}$ The calculated results included compound

[^0]

112-9572
Fig. 8. Excited Structure of Vanadium 22
elastic scattering derived with the Hauser-Feshbach formula and the reported excited structure of vanadium ${ }^{22}$ (see Fig. 8). The angular distributions calculated using this fitting procedure were descriptive of measurement (Fig. 9) and followed the observed intermediate structure of the elastic scattering (see curves of Fig. 4). The $\mathrm{V}_{0}$ and $\mathrm{W}_{0}$ and associated transmission coefficients obtained from the fitting reflected the intermediate structure, fluctuating with energy as shown in Fig. 10.

The meaning of the above fluctuating parameters was not above question. However, above energies of about $1.1 \mathrm{MeV}, \mathrm{V}_{0}$ and $\mathrm{W}_{0}$ obtained from the fitting procedure approached asymptotic values of 43 and 8 MeV , respectively. Elastic scattering cross sections calculated from these "asymptotic parameters" were in reasonable agreement with experiment above $\sim 0.8 \mathrm{MeV}$ (see solid curves of Fig. 11), but the agreement degenerated at lower energies, and the calculated $\ell=0$ strength function was about half that reported from microscopic measurement.


112-9574 Rev. 1
Fig. 9. Comparison of Measured (points) and Calculated (lines) Differential Elastic Distributions of Vanadium at Selected Incident Neutron Energies (keV)


112-9506 Rev. 1
Fig. 10. Real (V) and Imaginary (W) Potential Values and Transmission Coefficients, $T(\ell, \mathrm{j})$ Obtained by Fitting Eq. 3 to the Measured Elastic Scattering Cross Sections of Vanadium. See Section IV.A for discussion.

1.13-498

Fig. 11. Measured (crosses) and Calculated (curves) Elastic Distributions of Vanadium. The "asymptotic potential" form of Eq. 3 was used. The HauserFeshbach formalism was employed to estimate compound elastic contributions. Curves denoted as $Q=0$ and $Q=1$ were obtained by applying correction factors as described in Section IV.A. All calculated results lead to essentially identical $\mathrm{B}_{1} \rightarrow \mathrm{~B}_{4}$ coefficients.

The fluctuating potential parameters obtained from the above fitting procedures and the Hauser-Feshbach formula were used to calculate the inelastic-excitation cross sections; the results are shown in Fig. 6. The calculated values qualitatively display structure similar to that experimentally observed, though the calculation was based upon the potential obtained entirely from the fit to the elastic data. Inelastic-excitation cross sections calculated from the "asymptotic potential" ( $\mathrm{V}_{0}=43, \mathrm{~W}_{0}=8$ ) were in fair agreement with experiment at energies above $\sim 1.0 \mathrm{MeV}$ (solid curves of Fig. 12), but were less descriptive at lower energies. The low-energy discrepancies tended to be independent of potential and were evident in other reported calculations employing different potentials. ${ }^{25,68}$ Results of calculations made with changes of one unit of spin for both the 320- and the $930-\mathrm{keV}$ states compared poorly with the experimental results. This, together with the previously reported evidence, ${ }^{25}$ made it difficult to accept spin-and-parity assignments differing from those shown in Fig. 8.

Compound nucleus resonance widths fluctuate in a statistically describable manner, and transmission coefficients are no longer described by $T=2 \pi<\Gamma>D^{-1}$ where $T \rightarrow l$. The effects of such resonancewidth fluctuation and interference have been extensively discussed by Moldauer. ${ }^{4,33,35}$ He derived a "corrected" transmission coefficient, $\theta_{\alpha}$, of the form
$\theta_{\alpha}=2 Q_{\alpha}^{-1}\left[1-\left(1 .-Q_{\alpha} T_{\alpha}\right)^{1 / 2}\right]$.
For well-isolated resonances $\Gamma \ll$ $\mathrm{D}, \mathrm{T}$ is small and $\theta \rightarrow \mathrm{T}$. Using the "asymptotic potential" and the correction factors of Eq. 4 , we calculated both elastic and inelastic cross sections for the limiting


113-500
Fig. 12. Calculated (curves) and Measured (crosses) Cross Sections for the Excitation of the 0.32 - and $0.93-\mathrm{MeV}$ States in Vanadium. The interpretation of the calculated curves is discussed in Section IV.A.
cases $Q=1$ (isolated resonances) and $Q=0$ (strongly overlapping resonances). The results are shown in Figs. 11 and 12. Results obtained with intermediate choices of the $Q$ parameter lay between the limits set by the above extreme cases. The correction factors and choice of the $Q$ parameter did not lead to calculated elastic scattering differing appreciably from that obtained with the Hauser-Feshbach formalism above. The effect of the correction factors on the calculated inelastic cross sections was appreciable (see Fig. 12), the corrected values lying 20-30\% below the Hauser-Feshbach results and being in poorer agreement with experiment. These qualitative effects of the correction factors were not appreciably dependent upon the choice of the optical potential. Generally, comparison with present experiments gave little guidance as to desirability or magnitude of correction terms, though comparisons by other workers at higher energies indicated the desirability of the fluctuation correction. ${ }^{25}$

It is interesting to examine the applicability of the "asymptotic potential" over a wide energy range, since the parameters of Eq. 3 are energy-dependent, and the volume absorption becomes significant at higher energies. The calculated total neutron cross section compares well with experiment to 10.0 MeV (present work and Ref. 36), as illustrated in Fig. 13. The calculated elastic angular distributions are in agreement with experimental results reported at incident energies of $2.35,3.0$, and 7.05 MeV , as shown in Figs. 14,15 , and 16 , respectively. ${ }^{25,37,38}$ At 14.7 MeV , the agreement with experiment ${ }^{39}$ is less satisfactory (see Fig. 17), although it is not clear whether the discrepancies are due to deficiencies in the calculation or experiment or both. Inelastic scattering calculated with the "asymptotic potential" and the Hauser-Feshbach formalism was in relatively good agreement with values measured ${ }^{25}$ at 2.35 MeV (see Fig. 14). Generally, the form of Eq. 3 with the "asymptotic potential" parameters appears widely applicable to the calculation of total, elastic, and inelastic cross sections of vanadium at energies above about 0.8 MeV . The model is less successful at lower energies and certainly is not unique.


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Fig. 13. Measured and Calculated Total Cross Sections of Vanadium. Data for $\mathrm{E}_{\mathrm{n}}<1.5 \mathrm{MeV}$ from present work, for $\mathrm{E}_{\mathrm{n}}>1.5 \mathrm{MeV}$ from the work of Galloway and Shrader. ${ }^{36}$


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Fig. 14. Calculated Elastic and Inelastic Distributions of Vanadium and the Results Measured by Towle 25 at 2.35 MeV . Solid curves were obtained using the "asymptotic potential" form of Eq. 3. For comparison, dashed curves are those calculated in Ref. 40.



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Fig. 15. Elastic Angular Distribution of Vanadium Calculated Using the "Asymptotic Potential" Form of Eq. 3, Compared with the Measured Values of Becker at $3.0 \mathrm{MeV} .{ }^{37}$

Fig. 16
Elastic Scattering from Vanadium at 7.05 MeV . Points are measured values reported by Holmqvist and Wiedling. ${ }^{38}$ The curve represents calculations using "asymptotic potential" of Eq. 3.

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Fig. 17
Elastic Angular Distribution of Vanadium Measured at 14.7 MeV by Western et al., ${ }^{39}$ Compared with Results Calculated from Eq. 3.

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## B. Correlations and Fluctuations

Correlations and fluctuations in the measured cross sections were examined with the intent of ascertaining the statistical properties of the observables and their physical significance. The interpretation took the forms of (a) a search for a quantitative measure of intermediate resonance structure, (b) an analysis based upon the premise of strongly overlapping resonances (Ericson fluctuations), $, 5,41,42$ and (c) a derivation of average level density from fluctuations in widths and spacings of compound nucleus resonances. ${ }^{6,7}$

## 1. Existence of Intermediate Resonance Structure

Intermediate structure can be attributed to measured cross sections by qualitative inspection. Such procedures can be deceptive. ${ }^{43,44}$ A quantitative approach uses the function ${ }^{7,44}$

$$
\begin{equation*}
C(R)=\frac{1}{N} \sum_{i=1}^{N}\left[\sigma\left(E_{i}\right)-\overline{\sigma\left(E_{i}\right)}\right]^{2} \tag{5}
\end{equation*}
$$

where

$$
\overline{\sigma\left(E_{i}\right)}=\frac{1}{R} \int_{E_{i}-R / 2}^{E_{i}+R / 2} \sigma(E) d E
$$

$C(R)$ increases with $R$, asymptotically approaching a constant value for $R$ much larger than the average structure width of the fluctuating cross
section. In the presence of two very different fluctuation widths ( $\Gamma_{1}$ and $\Gamma_{2}$, where $\left.\Gamma_{1} \ll \Gamma_{2}\right), C(R)$ increases with $R$, approaching an initial plateau value for $\Gamma_{1}<R<\Gamma_{2}$ then rises to a second and final plateau for $R>\Gamma_{2} . \Gamma_{1}$ can be associated with the compound nucleus width ( $\Gamma_{\mathrm{CN}}$ ), and $\Gamma_{2}$ with a much larger intermediate resonance width ( $\Gamma_{\text {IS }}$ ). The experimental resolution used in the present total cross-section measurements was $\lesssim \Gamma_{\mathrm{CN}}$, sufficent to clearly indicate intermediate structure if present to an applicable extent. Figure 18 shows the function $C(R)$ calculated from the total crosssection values determined in the present experiment. The function rises to a single oscillatory plateau characteristic of finite range deviations (FRD) inherent in the limited experimental sample. ${ }^{45,46}$ This form of $C(R)$ is consistent with a single average width of a few keV. The intermediate structure qualitatively apparent in the total neutron cross sections (see Fig. 1) must, if valid, be of such a magnitude as to be masked by FRD and statistical fluctuations in the $C(R)$ distribution. $C(R)$ derived from the measured elastic scattering cross sections oscillated with such an amplitude as to preclude any reasonable assay of intermediate structure. Such behavior was not unexpected, in view of the small energy range of the sample and the precision of the measurements. In the present experimental context, the use of the $C(R)$ function for the assay of intermediate structure led to inconclusive results.

2. Limit of Strongly Overlapping Resonances, $\Gamma \gg \mathrm{D}$

Fluctuations have been observed in cross sections at energies at which the compound nucleus width is expected to greatly exceed the spacing ( $\Gamma_{\mathrm{CN}} \gg \mathrm{D}_{\mathrm{CN}}$ ). ${ }^{7,17,47-49}$ Ericson performed a theoretical study of these fluctuations and related observable quantities to average compoundnucleus properties. ${ }^{5,41,42}$ As used here, his interpretation is based upon a number of assumptions, primary of which are: (a) The reactions are purely statistical, (b) $\Gamma \gg D$, (c) $\Gamma^{J} \rightarrow \Gamma=$ a constant, (d) experimental resolutions $<\Gamma$, and (e) no single- or several-particle resonance effects exist. Qualitatively, $\Gamma / D=n / 2 \pi$, where $n$ is the number of effective exit channels. ${ }^{50}$ In the present experiments, $n$ was probably not $\gg 2 \pi$; rather, $\ell=0$ strength functions ${ }^{19}$ indicated that $\Gamma / D$ was more nearly unity. $\Gamma J \rightarrow \Gamma=$ constant implies a number of available exit channels and a large nuclear moment of inertia, not particularly characteristic of the present experiments. The effect of several particle resonances may be appreciable over much of the
measured energy interval (see Section IV.C below). Further, the experimental resolution used,in the present total cross-section measurements was $\lesssim \Gamma$ only in limited and lower-energy regions. Thus an interpretation of the present work in the framework of Ericson fluctuations is open to considerable question. The approach is pursued here only in the spirit of a qualitative experimental assay.

Ericson derived the total cross-section correlation function ${ }^{5}$

$$
\begin{align*}
& F(\epsilon)=\langle[\sigma(E+\epsilon)-\langle\sigma(E)\rangle][\sigma(E)-\langle\sigma(E)\rangle]\rangle \\
& F(\epsilon)=\frac{\Gamma^{2}}{\epsilon^{2}+\Gamma^{2}} \kappa \frac{D_{0}}{\pi \Gamma} \frac{\left(\pi \lambda^{2}\right)^{2}}{(2 i+1)(2 I+1)} \sum_{\ell}(2 \ell+1) T_{\ell}^{2} \tag{6}
\end{align*}
$$

where $\kappa$ is a measure of the distribution of partial widths around the mean ( $\sim 1.5$ Porter-Thomas distribution ${ }^{56}$ ), $D^{J}=D_{0} /(2 \mathrm{~J}+1), \mathrm{T}_{\ell}=$ optical model transmission coefficient, and i and $I$ are the spins of the incident and target particles, respectively. In the ratio form,

$$
\begin{equation*}
C(\delta)=\frac{\langle\sigma(E+\delta) \cdot \sigma(E)\rangle}{\langle\sigma(E+\delta)\rangle\langle\sigma(E)\rangle}-1=\frac{1}{N}\left(1-Y^{2}\right) \frac{\Gamma^{2}}{\delta^{2}+\Gamma^{2}}, \tag{7}
\end{equation*}
$$

where $N=$ number of contributing independent channels and $Y=$ the proportion of direct reactions. Equation 7 is independent of $D_{0}$ and $\kappa .{ }^{5,46}$ Further,

$$
\left.\begin{array}{l}
C(0)=\frac{1}{N}\left(1-\dot{Y}^{2}\right), \\
F(0)=\kappa \frac{D_{0}}{\pi \Gamma} \frac{\left(\pi \lambda^{2}\right)^{2}}{(2 i+1)(2 I+1)} \sum_{\ell}(2 \ell+1) \mathrm{T}_{\ell}^{2} \cdot \tag{8}
\end{array}\right\}
$$

and

In the following, Eqs. 7 and 8 are used to obtain $N$ and $\Gamma$ from the measured cross sections and (with the $\mathrm{T}_{\ell}$ values calculated using the "asymptotic potential" of Section IV.A) the value of $D_{0}$. Corrections are made for the effect of the finite experimental resolution. ${ }^{51,52}$. These corrections are not negligible, particularly at higher energies, where the assumptions of the theory become more applicable to the experiment.

The lower portion of Fig. 19 shows $C(\delta)$ calculated from the measured total cross sections. The function decreases rapidly from a maximum at $\delta=0$ to about half-magnitude, then slowly decreases in an oscillatory manner with increasing $\delta$. The slow decrease at large $\delta$ is characteristic of a direct-reaction (DR) modulation, and the oscillations are attributed to the finite sample size. ${ }^{45,46}$ The DR modulation (shape scattering) could be removed from the measured data using results of a
suitable optical model calculation, but a model calculation of sufficient accuracy is difficult to achieve. As a phenomenological alternative, the DR component was determined by least-squares fitting the cubic

$$
\begin{equation*}
\delta_{c a l}=a+b E+c E^{2}+\mathrm{dE}^{3}(E \text { in } M e V) \tag{9}
\end{equation*}
$$

to the measured data. The order of the fit was such as to well describe the general energy dependence without unduly distorting the fluctuating structure. $\delta$ cal was subtracted from the measured cross sections, and a positive constant added to ensure nonnegative values. The resulting "fluctuating cross section," shown in Fig. 20 together with the directly measured values, was used in subsequent correlation analysis.
C(8)



Fig. 19
C( $\delta$ ) Evaluated from Total Neutron Cross Sections of Vanadium. Lower: $\mathrm{C}(\delta)$, Eq. 7, evaluated from the total neutron cross sections of vanadium. The effects of direct reactions and the finite sample range are evident. Upper: $C(\delta)$ evaluated from the total neutron corrected for direct reactions.

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Fig. 20
Measured Total Neutron Cross Sections of Vanadium. Lower: measured total neutron cross sections of vanadium. Results are identical to those shown in Fig. 5. Upper: measured total cross-section values after correction for DR contributions in the manner described in the text.


$F(\epsilon)$ and $C(\delta)$ (from Eqs. 6 and 7) were evaluated from the fluctuating total cross section over the entire measured energy interval and a number of subintervals thereof. Typical of the results is $C(\delta)$ calculated for the entire interval shown in the upper portion of Fig. 19. FRD oscillations remain evident and are of an rms magnitude consistent with the estimates of Hall. ${ }^{45,46}$ Neither in this example nor in any other $C(\delta)$ calculation was a significant deviation from a simple Lorentzian form noted as would be expected from appreciable intermediate resonance structure with a width $\Gamma_{I S} \gg \Gamma_{\mathrm{CN}}$. Table I summarizes $C(0), F(0), \Gamma$, and $D_{0}$ values, derived from the correlation analysis of the total cross sections, carried out over the entire measured interval and subintervals thereof using Eqs. 6-8. Uncertainties in the calculated $C(0)$ and $F(0)$ values are large; FRD alone led to standard deviations of $30 \%$ or more. The $\Gamma$ values are remarkably consistent, and $D_{0}$ shows the expected energy dependence. However, $D_{0}$ tends to be an order of magnitude larger and $\Gamma$ a factor of two to three larger than indicated by level density formulas, by results of detailed low-energy resonance studies, and by the analysis of average cross sections at low energies. ${ }^{19,53,54}$ These discrepancies tend to compensate when the $\ell=0$ strength function is estimated, resulting in a value about one-fifth of that reported from detailed resonance studies and about onethird to one-half of that obtained from average low-energy cross sections. In view of the inappropriateness of the theory in the present experimental context, the results are probably remarkable for their agreement with values obtained by other and more proper methods and tend to indicate that such analyses of total neutron cross sections are not sensitive to these theoretical concepts and underlying premises.

TABLE I. Results of Correlation Analysis of Measured Total Cross Sections

| Energy Interval, MeV | $\begin{aligned} & 0.1^{-} \\ & 1.44 \end{aligned}$ | $\begin{aligned} & 0.1- \\ & 0.42 \end{aligned}$ | $\begin{aligned} & 0.21- \\ & 0.53 \end{aligned}$ | $\begin{aligned} & 0.32- \\ & 0.64 \end{aligned}$ | $\begin{aligned} & 0.43- \\ & 0.75 \end{aligned}$ | $\begin{aligned} & 0.53- \\ & 0.86 \end{aligned}$ | $\begin{aligned} & 0.64- \\ & 0.97 \end{aligned}$ | $\begin{aligned} & 0.75- \\ & 1.07 \end{aligned}$ | $\begin{aligned} & 0.85- \\ & 1.18 \end{aligned}$ | $\begin{aligned} & 0.97- \\ & 1.29 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| C(0) C(0) | 0.0378 | 0.101 | 0.0473 | 0.0353 | 0.0300 | 0.0234 | 0.0180 | 0.0152 | 0.0112 | 0.0081 |
| F(0), $\mathrm{b}^{2}$ | 1.103 | 3.03 | 1.384 | 0.957 | 0.848 | 0.647 | 0.546 | 0.439 | 0.346 | 0.235 |
| $\Gamma, \mathrm{keV}$ | 4.0 | 5.1 | 4.4 | 3.7 | 3.8 | 3.8 | 3.9 | 4.0 | 3.2 | 3.0 |
| $\mathrm{D}_{0}, \mathrm{keV}$ | 410 | 540 | 304 | 223 | 225 | 189 | 171 | 162 | 115 | 83 |
| $\left.D=D_{0}(2)+1\right),{ }^{\text {a }}$ | 49 | 65 | 36 | 26 | 27 | 23 | 20 | 19 | 13 | 10 |
| $\Gamma /\left.0\right\|_{0} \times 10^{\text {a }, \mathrm{b}}$ | 0.96 | 1.5 | 2.0 | 2.0 | 1.8 | 2.0 | 2.2 | 2.2 | 2.4 | 2.8 |

${ }^{a}$ Assuming $2 \mathrm{~J}+1 \approx 8$.
ball values corrected to 1 eV .

As is evident from Eq. 7, correlations are damped as the number of exit channels increases and thus should become more pronouncedas the number of reaction channels is restricted. Therefore, to obtain more definitive results, $C(\delta)$ was evaluated for the $\mathrm{B}_{\ell}$ coefficients of the elastic channel and for the excitation cross section of the inelastic channel ( $\mathrm{Q}=-0.32 \mathrm{MeV}$ ). Unfortunately, these correlation functions all showed strong FRD oscillations because of the limited extent of the available
sample. These oscillations and the experimental resolutions appreciably exceeding $\Gamma_{C N}$ precluded any reasonable interpretation of the $C(\delta)$ derived from either the elastic or inelastic scattering measurements.

The cross correlation function

$$
\mathrm{C}_{\mathrm{ab}}=\kappa \mathrm{G}_{\mathrm{ab}}
$$

where
and

$$
\begin{equation*}
\left.G_{a b}=\frac{\left\langle\sigma_{a} \cdot \sigma_{b}\right\rangle}{\left\langle\sigma_{a}\right\rangle \cdot\left\langle\sigma_{b}\right\rangle}-1\right\} \tag{10}
\end{equation*}
$$

$$
\kappa=\left[\mathrm{C}_{\mathrm{a}}(0) \cdot \mathrm{C}_{\mathrm{b}}(0)\right]^{-1 / 2},
$$

is of interest. ${ }^{5,46} C_{a b}$ was determinedfor the $B_{\ell}$ coefficients of the elastic cross section, the elastic and total cross sections, and the elastic and inelastic $(Q=-0.32 \mathrm{MeV})$ cross sections. The results are given in Table II. As expected, $B_{0}$ (approximately elastic cross section) was strongly correlated with the total cross section (see Fig. 5). Between $B_{\ell}$ values, only the $B_{0}$ to $B_{1}$ correlation appears significantly larger than $F R D$ errors alone. This is in contrast to the concepts of Ericson, ${ }^{5}$ which indicate small correlations between even and odd $\mathrm{B}_{\ell}$ coefficients. There was no significant numerical correlation between elastic and inelastic cross sections, though experimental uncertainties and the limited range of the samples might have masked the small effect that seems qualitatively present from a visual inspection of the respective cross sections.

TABLE II. Cross-correlation Values

| Processes | $\mathrm{G}_{\mathrm{ab}} \mathrm{a}, \mathrm{b}$ | $\mathrm{C}_{\mathrm{ab}} \mathrm{b}$ |
| :--- | ---: | ---: |
| $\mathrm{B}_{0}$ and $\sigma_{\mathrm{T}}$ | $1.34 \times 10^{-2}$ | 0.77 |
|  | $\pm 0.36 \times 10^{-2}$ |  |
| $\mathrm{~B}_{0}$ and $\sigma_{\text {inel }}$ | $0.18 \times 10^{-2}$ | 0.088 |
|  | $\pm 0.40 \times 10^{-2}$ |  |
| $\mathrm{~B}_{0}$ and $\mathrm{B}_{1}$ | $1.4 \times 10^{-2}$ | - |
|  | $\pm 0.60 \times 10^{-2}$ |  |
| $\mathrm{~B}_{0}$ and $\mathrm{B}_{2}$ | $-1.6 \times 10^{-2}$ | - |
|  | $\pm 1.2 \times 10^{-2}$ |  |
| $\mathrm{~B}_{1}$ and $\mathrm{B}_{2}$ | $-1.5 \times 10^{-2}$ | - |
|  | $\pm 2.1 \times 10^{-2}$ |  |

[^1]3. Cross-section Fluctuations and Distributions of Widths and Spacings

In this section, structure in the measured total cross sections of vanadium is considered in the context of fluctuations in compound nucleus resonance spacings and widths after the manner of Carlson and Barschall ${ }^{7}$ and of Agodi and Pappalardo. ${ }^{6}$ It is assumed that the experimental resolution appreciably exceeds the average compound nucleus width, and experimental averages are constructed to ensure the validity of the premise. Within these averages, the interference between potential and compound scattering is neglected and the former's smooth energy dependence is removed by the cubic.fitting procedure described by Eq. 9. It is further as sumed that the partial widths are small compared to their spacings.

With the above premises, Carlson and Barschall derived the total cross section variance

$$
\begin{equation*}
\mathrm{s}^{2}(\text { variance })=\left(\pi \lambda^{2}\right)^{2} \sum_{\mathrm{J} \pi} \frac{\mathrm{~g}^{2}}{\left\langle\mathrm{~N}_{\mathrm{J} \pi}\right\rangle}\left[\mathrm{k}_{\mathrm{w}} \sum_{\ell \mathrm{s}}\left(\mathrm{~T}_{\ell \mathrm{s}}^{\mathrm{J}}\right)^{2}+\mathrm{k}_{\mathrm{n}}\left(\sum_{\ell \mathrm{s}} \mathrm{~T}_{\ell \mathrm{s}}^{\mathrm{J}}\right)^{2}\right] \tag{11}
\end{equation*}
$$

where $g=(2 \mathrm{~J}+1) /[2(2 \mathrm{I}+1)],\left\langle\mathrm{N}_{\mathrm{J} \pi}\right\rangle$ is the average number of levels of a given $J \pi$ in the energy interval $\triangle$, and $T{ }_{l}{ }_{s}$ are transmission coefficients. ${ }^{3}$ The derivation makes use of the definitions

$$
\begin{aligned}
& \mathrm{T}_{\ell \mathrm{s}}^{\mathrm{J}}=2 \pi\left\langle\Gamma_{\ell \mathrm{s}}^{\mathrm{J}}\right\rangle / D_{\mathrm{J} \pi} \\
& \mathrm{k}_{\mathrm{w}}=\text { variance } \Gamma_{\ell \mathrm{s}}^{\mathrm{J}}\left\langle\left\langle\Gamma_{\ell \mathrm{s}}^{\mathrm{J}}\right\rangle=\underset{\text {. widths, }}{ }{ }^{56}\right.
\end{aligned}
$$

and

$$
\begin{aligned}
k_{n}=\text { variance } N_{J \pi} /\left\langle N_{J \pi}\right\rangle:= & 0.27 \text { for a Wigner distribution of } \\
& \text { spacings. }{ }^{57} .
\end{aligned}
$$

Further, it is assumed that the distributions used in.calculating the variances are independent of quantum number and that the widths associated with differing quantum numbers and spacings for the same quantum number are uncorrelated. Some of these assumptions are not without question. ${ }^{4,58}$ If we separate the energy and spin dependence of the level density in the manner of Gilbert and Cameron, ${ }^{54}\left\langle N_{J \pi}\right\rangle / \Delta=G(E) H(J \pi)$, Eq. 11 reduces to

$$
\begin{equation*}
s^{2} \Delta=\left(\pi \lambda^{2}\right)^{2} \frac{1}{G(E)} \sum_{J \pi} \frac{\mathrm{~g}^{2}}{\mathrm{H}(\mathrm{~J} \pi)}\left[\mathrm{k}_{\mathrm{w}} \sum_{\ell \mathrm{s}}\left(\mathrm{~T}_{\ell \mathrm{s}}^{\mathrm{J}}\right)^{2}+\mathrm{k}_{\mathrm{n}}\left(\sum_{\ell \mathrm{s}} \mathrm{~T}_{\ell \mathrm{s}}^{\mathrm{J}}\right)^{2}\right] \tag{12}
\end{equation*}
$$

Using $T_{l s}^{J}$ obtained from the "asymptotic potential" of Eq. 3, $H(J \pi)$ from Ref. 54, and $S^{2}$ determined from averages of measured values over the interval $\Delta$, we can obtain $G(E)$. Table III gives the results for several energy intervals of the measured total cross sections and a number of averaging increments, $\triangle$. In the table, the level density derived from the present experiments, $\rho_{\text {exp }}=G(E) \cdot H(J \pi)$, is compared with that given by the formula of Gilbert and Cameron ( $\rho_{\text {theo }}$ ). ${ }^{54}$ For averaging increments $\Delta \gg \Gamma$ (i.e., $\Delta \gtrsim 25 \mathrm{keV}$ ), the $\rho_{\mathrm{exp}}$ values obtained from the experiments are within a factor of two of those given by the density formula and are similar to values deduced from resonance studies at low energies. ${ }^{19}$ The results were not particularly sensitive to the distributions of widths and spacings used in evaluating $\mathrm{k}_{\mathrm{w}}$ and $\mathrm{k}_{\mathrm{n}}$. Assuming exponential distributions ( $\mathrm{k}_{\mathrm{w}}=\mathrm{k}_{\mathrm{n}}=1$ ), or even neglecting width effects ( $\mathrm{k}_{\mathrm{w}}=0, \mathrm{k}_{\mathrm{n}}=1$ ), the results were similar to those obtained with Porter-Thomas and Wigner distributions. The $\left(\mathrm{k}_{\mathrm{w}}=0, \mathrm{k}_{\mathrm{n}}=1\right)$ assumption was that used by Agodi and Pappalardo. ${ }^{6}$ Within the experimental uncertainties of $30-50 \%$, the observed structure of the total cross section is consistent with the interpretation based upon recognized distributions of compound nucleus resonance widths and spacings. The distribution in spacings is a dominant factor, though the results are not sensitive to the detailed form of the distribution function.

TABLE III. Comparison of Experimentally and Theoretically Derived Level Densities

| AveragingIncrement |  | Energy Interval, MeV |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | 0.10-0.545 | 0.545-0.990 | 0.990-1.435 |
|  |  | Av $=0.327$ | Av $=0.767$ | $\mathrm{Av}=1.212$ |
| $\Delta \cong 1-3 \mathrm{keV}^{\mathrm{a}}$ | $\left\{\begin{array}{l} \mathrm{s}^{2} \Delta, \mathrm{~b}^{2} \mathrm{MeV} \\ \rho_{\exp }, \mathrm{MeV}^{-1} \\ \rho_{\text {theo }}, \mathrm{MeV}^{-1 \mathrm{~b}} \\ \rho_{\exp } / \rho_{\text {theo }} \end{array}\right.$ | $7.49 \times 10^{-3}$ | $1.8 \times 10^{-3}$ | $0.56 \times 10^{-3}$ |
|  |  | $3.37 \times 10^{3}$ | $2.77 \times 10^{3}$ | $8.16 \times 10^{3}$ |
|  |  | $1.27 \times 10^{3}$ | $1.73 \times 10^{3}$ | $2.34 \times 10^{3}$ |
|  |  | 2.6 (2.5, ${ }^{\text {c }} 1.3{ }^{\text {d }}$ ) | 1.59 (1.8, $\left.{ }^{\text {c }} 1.2 \mathrm{~d}\right)$ | 3.47 (4.5, c 3.2d) |
| $\Delta=10 \mathrm{keV}$ | $\left\{\begin{array}{l} \mathrm{S}^{2} \Delta, \mathrm{~b}^{2} \mathrm{MeV} \\ \rho_{\text {exp }}, \mathrm{MeV}^{-1} \\ \rho_{\text {exp }} / \rho_{\text {theo }} \end{array}\right.$ | $1.65 \times 10^{-2}$ | $0.38 \times 10^{-2}$ | $0.13 \times 10^{-2}$ |
|  |  | $1.53 \times 10^{3}$ | $1.34 \times 10^{3}$ | $3.50 \times 10^{3}$ |
|  |  | 1.20 (1.1, $0.6{ }^{\text {d }}$ ) | 0.78 (0.9, 0.59d) | 0.78 (1.93, ${ }^{\text {c }} 1.36{ }^{\text {d }}$ ) |
| $\Delta=25 \mathrm{keV}$ | $\left\{\begin{array}{l} \mathrm{S}^{2} \Delta, \mathrm{~b}^{2} \mathrm{MeV} \\ \rho_{\text {exp }}, \mathrm{MeV}^{-1} \\ \rho_{\text {exp }} / \rho_{\text {theo }} \end{array}\right.$ | $0.136 \times 10^{-1}$ | $0.477 \times 10^{-2}$ | $0.216 \times 10^{-2}$ |
|  |  | $1.85 \times 10^{3}$ | $1.09 \times 10^{3}$ | $2.14 \times 10^{3}$ |
|  |  | 1.46 ( $1.4,{ }^{\text {c }} 0.7{ }^{\text {d }}$ ) | 0.63 (0.7, c 0.5d) | 0.91 (1.2, c 0.8d) |
| $\Delta=50 \mathrm{keV}$ | $\left\{\begin{array}{l} \mathrm{S}^{2} \Delta, \mathrm{~b}^{2} \mathrm{MeV} \\ \rho_{\text {exp }}, \mathrm{MeV}^{-1} \\ \rho_{\text {exp }} / \rho_{\text {theo }} \end{array}\right.$ | $0.109 \times 10^{-1}$ | $0.495 \times 10^{-2}$ | $0.265 \times 10^{-2}$ |
|  |  | $2.37 \times 10^{3}$ | $1.05 \times 10^{3}$ | $1.76 \times 10^{3}$ |
|  |  | 1.82 ( $1.7,{ }^{\text {c }} 0.9^{\text {d }}$ ) | $0.61\left(0.7,{ }^{\text {c }} 0.6{ }^{\text {d }}\right.$ ) | $0.74\left(1.0,{ }^{\text {c }} 0.7{ }^{\text {d }}\right.$ ) |
| $\Delta=75 \mathrm{keV}$ | $\left\{\begin{array}{l} \mathrm{s}^{2} \Delta, \mathrm{~b}^{2} \mathrm{MeV} \\ \rho_{\text {exp }}, \mathrm{MeV}^{-1} \\ \rho_{\text {exp }} / \rho_{\text {theo }} \end{array}\right.$ | $0.106 \times 10^{-1}$ | $0.546 \times 10^{-2}$ | $0.234 \times 10^{-2}$ |
|  |  | $2.30 \times 10^{3}$ | $0.95 \times 10^{3}$ | $1.97 \times 10^{3}$ |
|  |  | 1.87 (1.7, ${ }^{\text {c }} 0.9 \mathrm{~d}$ ) | 0.549 (0.6, ${ }^{\text {c }} 0.4{ }^{\text {d }}$ ) | 0.842 (1.1, c 0.8d) |

[^2]The expression $2 \pi\langle\Gamma / D\rangle=T$ used in deriving Eq. 11 is known to be invalid when $T$ approaches unity as it tends to in the present experiments. Considering resonance interference and $\underline{S}$ matrix unitarity, Moldauer has derived the relation $2 \pi\langle\Gamma / D\rangle=\ln [1 /(1-T)]$, valid for large T. ${ }^{59}$ The use of this relation increased the level densities derived from experiment ( $\rho_{\exp }$ of Table III) by about a factor of three, to values appreciably larger than indicated by either level-density formulas or detailed resonance measurements. Such differences may, in part, be due to inappropriateness of Eq. 12 in the present experimental context. The equation is valid only for nonoverlapping resonances, and the Bethe randomness hypothesis ${ }^{6,55}$ is invoked to extend the validity to situations where partial widths alone are small compared to spacings. It is not clear that such an extrapolation is valid in the present experimental context.

## C. The Intermediate Optical Model

The intermediate structure quantitatively evident in the energyaveraged total, elastic, and inelastic cross sections of vanadium can be characterized by a width, $\Gamma_{I S}$, and a spacing, $D_{I S}$, large compared to that of the compound nucleus and small relative to that of the single-particle or diffraction "giant resonances" (i.e., $\Gamma_{\mathrm{CN}}<\Gamma_{\mathrm{IS}}<\Gamma_{\mathrm{SP}}, \mathrm{D}_{\mathrm{CN}}<\mathrm{D}_{\mathrm{IS}}<\mathrm{D}_{\mathrm{SP}}$ ). The observed structure in elastic and inelastic scattering processes ap! peared correlated in scattering angle (see Figs. 7 and 21).


Fig. 21
Differential Elastic Neutron Scattering Cross Sections of Vanadium Observed at Laboratory Angles of $27-154^{\circ}$. The curves are derived from the measured values expressed in the form of Eq. 1. The results have been averaged over a $50-\mathrm{MeV}$ energy interval to smooth local fluctuations. Actual measured values are indicated at $27^{\circ}$.

Structure of the type observed here has been interpreted in terms of "doorway state" processess. ${ }^{1,60,61}$ Many such interpretations tend to be qualitative comparisons with experiment. The "doorway state" has been quantitatively studied in the context of CN fine structure by Lejeune and Mahanx ${ }^{69}$ and by $\mathrm{Takeuchi}^{8}$ and can be related to the properties of nuclear
structure in the manner of Lemmer and Shakin, for example. ${ }^{70}$ Lipperheide, ${ }^{9,64}$ Feshbach et al., and Takeuchi ${ }^{8}$ have suggested an "intermediate optical model." The concept of an intermediate optical model has the advantages of simplicity of application and of avoiding excessive demands on experimental resolution. This concept is used in the present interpretation, the theoretical aspects of which follow Ref. 71.

Restricting the interpretation to the two open channels of $s$-wave elastic and inelastic scattering and assuming well-isolated doorway states and no direct reaction, the energy-averaged $T$-matrix for two open channels is ${ }^{8,71}$

$$
\begin{equation*}
\left\langle T_{f i}\right\rangle=T_{f i}^{p}+2 \pi \sum_{s} S_{f f}^{p} \frac{\left\langle\chi_{f}^{(+)} P H d \Phi_{s}\right\rangle\left\langle\phi_{s} d H P \chi_{i}^{(+)}\right\rangle}{E-E_{s}-\Delta_{s}+\frac{i}{2}\left(\Gamma_{s}^{\downarrow}+\Gamma_{s}^{\hat{s}}\right)} \tag{13}
\end{equation*}
$$

where
$\mathrm{T}^{\mathrm{P}}$ and $\mathrm{S}^{\mathrm{P}}$ are potential scattering T - and S-matrices,
$\chi^{(+)}$is the distorted wave satis fying outgoing-wave boundary conditions,
$E_{S}$ is the energy of the sth doorway state,
$\Gamma_{s}^{\downarrow}$ is the decay width of the $s$ th doorway to the CN ,
and
$\Gamma_{\mathrm{S}}^{\uparrow}$ is the decay width to the continuum.
The width $\Gamma_{\mathrm{S}}^{\uparrow}=\Gamma_{\mathrm{S}_{1}}^{\uparrow}+\Gamma_{\mathrm{S} 2}^{\hat{1}}$, where $\Gamma_{\mathrm{S} 1}^{\uparrow}$ and $\Gamma_{\mathrm{S} 2}^{\hat{1}}$ are elastic and inelastic contributions, respectively, and $P$ and $d$ are projection operators to the open channel and the doorway, respectively.

The wave equation for complex potential interactions in the presence of doorways is ${ }^{1,8,9,62-64}$

$$
\begin{equation*}
\left[P H P-\sum_{S} f_{\mathbf{S}}(E) \cdot \mathrm{PHd} \phi_{S}><\phi_{S} \mathrm{dHP}-\mathrm{E}\right] \chi=0 \tag{14}
\end{equation*}
$$

where

$$
f(E)=1 /\left(E-E_{s}+i \Gamma_{\mathbf{s}}^{\uparrow} / 2\right)
$$

From this complex potential equation, a $T$-matrix, $T^{C P}$, can in principle be derived equivalent to the energy-averaged T-matrix of Eq. 13, and the total, absorption, elastic, and inelastic cross sections are obtained. ${ }^{71}$ The total cross section is proportional to the $T$-matrix and is given by ${ }^{8,9,64}$

$$
\begin{equation*}
\left\langle\sigma_{\mathrm{c}}^{\mathrm{TOT}}\right\rangle=2 \pi \lambda_{\mathrm{c}}^{2}\left(-\operatorname{Im} \mathrm{T}_{\mathrm{cc}}^{\mathrm{cp}}\right) . \tag{15}
\end{equation*}
$$

The other cross sections follow from statistical considerations. The statistical properties of the T -matrix, $\mathrm{T}=\mathrm{T}^{\mathrm{DR}}+\mathrm{TCN}$, have been extensively studied in the absence of a doorway. ${ }^{4,66}$ In the presence of a doorway, the exact $T$-matrix can be written $T=T^{P O T}+T^{d}+T^{q} .^{1} T^{q}$ has the same structure as $T^{C N}$, and $T^{d}$ is assumed constant over an energy-averaging increment. Therefore $\mathrm{T}^{\mathrm{POT}}+\mathrm{T}^{\mathrm{d}}$ can be associated with $\mathrm{T}^{\mathrm{DR}}$, and $\mathrm{T}^{\mathrm{q}}$ with $\mathrm{T}^{\mathrm{CN}}$. With these associations, the energy-averaged cross sections are given by ${ }^{71}$

$$
\left\langle\sigma_{c c^{\prime}}\right\rangle=\sigma_{c c^{\prime}}^{o p^{t}}+\sigma_{c_{c^{\prime}}}^{\mathrm{fl}}
$$

where

$$
\begin{align*}
& \sigma_{\mathrm{cc}^{\prime}}^{\mathrm{opt}}=\pi \lambda_{\mathrm{c}^{2}}^{\|_{\mathrm{c}}} \mathrm{~T}_{\left.\mathrm{c}_{\mathrm{c}^{\prime}}^{\mathrm{cp}}\right|^{2},} \\
& \sigma_{\mathrm{c}^{\prime \prime}}^{\mathrm{fl}}=\pi \lambda_{\mathrm{c}}^{2} \frac{\mathrm{~T}_{\mathrm{c}}^{\mathrm{CN}} \mathrm{~T}_{\mathrm{c}^{\prime}}^{\mathrm{CN}}}{\sum_{\mathrm{c}^{\prime \prime}}}, \tag{16}
\end{align*}
$$

and

$$
T_{c}^{C N}=1-\sum_{c^{\prime \prime}}\left|\dot{\delta}_{c^{\prime \prime}}-i T_{c c^{\prime \prime}}^{c p}\right|^{2}
$$



In practice, the calculation of these quantities from the coupled complexpotential wave equation, Eq. 14, is difficult, and a simplified method is sought. For this purpose, the cross section is obtained from the following decoupled equations:
and

$$
\left.\begin{array}{l}
{\left[P_{1} H P_{1}-\sum_{S} F_{S 1}(E) P_{1} H d \phi_{S}><\phi_{S} d H P_{1}-E\right] \chi_{1}=0,} \\
{\left[P_{2} H P_{2}-\sum_{S} F_{s 2}(E) P_{2} H d \phi_{S}><\phi_{S} d H P_{2}-E\right] \chi_{2}=0,} \tag{17}
\end{array}\right\}
$$

where $P_{1}$ and $P_{2}$ are projection operators for elastic and inelastic channels, respectively, and

$$
\begin{equation*}
F_{s i}(E)=\frac{1}{E-E_{s}+\frac{i}{2}\left(\Gamma_{s}^{i}+\Gamma_{s}^{\uparrow}\right)_{j \neq i}} \tag{18}
\end{equation*}
$$

The cross sections calculated from Eq. 17 can be compared with the energyaveraged cross sections of Eqs. 15 and 16 .

The diagonal elements of the $T$-matrix derived from the decoupled Eqs. 17 are equivalent to those of $\mathrm{T}^{\mathrm{cp}}$ obtained from the coupled. Eq. 14, and the total cross section obtained from Eqs. 17 is equivalent to the energyaveraged total cross section. $\sigma_{11}^{\mathrm{opt}}$ of Eq. 16 is equal to that obtained from Eqs. 17, but the $\sigma_{12}^{\text {opt }}$ of Eq. 17 is zero. Assuming $\Gamma_{S 1}^{\uparrow}$ and $\Gamma_{S 2}^{\uparrow}$ are equal, we can use transmission coefficients following from the decoupled equations to simply express elastic and inelastic cross sections in the following form: ${ }^{71}$

$$
\left.\begin{array}{c}
\left\langle\sigma^{\mathrm{el}}\right\rangle=\left\langle\sigma_{\mathrm{OMHF}}^{\mathrm{el}}\right\rangle-\frac{\Gamma_{\mathrm{S} 1}^{\uparrow} \sigma_{11}^{\mathrm{HF}}}{\Gamma_{\mathrm{s} 2}} \\
\left\langle\sigma^{\mathrm{inel}}\right\rangle=\frac{\Gamma_{\mathrm{S}}^{\downarrow}}{\Gamma_{\mathrm{s}}^{\downarrow}+\Gamma_{\mathrm{s} 1}^{\downarrow}} \frac{\Gamma^{\uparrow}}{\Gamma_{\mathrm{s}}^{\uparrow}+\Gamma_{\mathrm{s}}^{\downarrow}} \sigma_{\mathrm{OMHF}}^{\mathrm{inel}}
\end{array}\right\}
$$

and

Both of the above expressions are the familiar optical-model HauserFeshbach results modified by rather simple correction factors dependent on doorway-state widths.

Equations 17 have been interpreted as conventional optical-model equations, modified only by the presence of the energy-dependent factor $\mathrm{F}_{\mathrm{si}}(\mathrm{E}) .^{71}$ In the present analysis, an optical potential of the following form was chosen:

$$
\mathrm{v}^{\mathrm{opt}}=-\overline{\mathrm{V}}+i \overline{\mathrm{~W}}+\overline{\mathrm{V}}_{\mathrm{so}} \underline{\underline{l}} \cdot \underline{s}+F_{1}+i F_{2},
$$

where
and

$$
\begin{equation*}
F_{1}=\sum_{S} S_{S} \frac{E-E_{S}}{\left(E-E_{S}\right)^{2}+\left(\frac{\Gamma_{S}}{2}+\frac{\Gamma \hat{s}}{4}\right)^{2}} \tag{20.}
\end{equation*}
$$

$$
F_{2}=\sum_{s} S_{s} \frac{-\Gamma_{S / 2}^{\downarrow}}{\left(E-E_{S}\right)^{2}+\left(\frac{\Gamma_{S}^{\downarrow}}{2}+\frac{\Gamma_{S}^{\uparrow}}{4!}\right)^{2}},
$$

$S_{s}$ being the strength of interaction with the $s$ doorway. The imaginary component, W, of Eq. 20 is due to reactions not proceeding through explicitly identified doorway states.

The potentials $\overline{\mathrm{V}}, \overline{\mathrm{W}}$, and $\mathrm{V}_{\text {so }}$ were assumed to follow the spacial distributions of the phenomenological potential given in Eq. 3. The doorways are classified as the $j \pi$ each with associated strengths, resonant energies, $E_{s}$, and widths, $\Gamma \frac{\downarrow}{J} \pi$. When averaged over energies large compared to those characteristic of the doorways, $\mathrm{F}_{1} \rightarrow 0, \mathrm{~F}_{2} \rightarrow$ constant, and Eq. 20 reduces to the "conventional" optical potential. ${ }^{8}$ Other aspects of the intermediate potential, such as nonlocality and energy dependence, have been extensively discussed. 8,9

General application of Eq. 20 to the interpretation of experiment leads to the adjustment of a large number of parameters descriptive of each of a number of contributing doorway states. This would be true, for example, of charged-particle reactions at relatively high energies involving a number of angular momenta. ${ }^{65}$ The number of parameters is sharply reduced in the consideration of the present experiments at incident energies $<1.0 \mathrm{MeV}$. $\ell=0$ processes are predominant with possible doorway configurations of $3^{-}$and $4^{-}$. Only the former can contribute to the inelastic channel $(Q=$ $-0.32 \mathrm{MeV}, \ell=0)$. The present interpretation is further simplified by assuming that the reactions are spin-independent and that possible doorway states do not appreciably overlap. Both assumptions are qualitative approximations, but they do permit a simple interpretation of the measured results in terms of the above intermediate model.

The procedure followed was to select, by inspection, average $\overline{\mathrm{V}}$ and $\bar{W}$ values and a limited number of doorways characterized by $E_{S}, \Gamma_{S}^{\downarrow}$, and a strength, $\mathrm{S}_{\mathrm{S}}$, and calculate Vopt from Eq. 20 for: comparison with the real and imaginary portions of the potential derived from a detailed fit to the measured elastic distributions (see Fig. l0). Commensurate with the as sumption of isolated doorways and the known compound nucleus structure, the number of doorway states considered was restricted to $\$ 5 / \mathrm{MeV}$. Doorway parameters were suitably adjusted where indicated, and the above procedure was repeated until a reasonable agreement was achieved between $V^{\circ}$ pt and the experimentally derived potential. The "intermediate" potential was then used to calculate elastic and inelastic distributions for direct comparison with the measured values. Rather good results were obtained after three or four iterations. Typical are the comparisons of real and imaginary portions of Vopt and the experimentally derived potential shown in Fig. 22, and the elastic and inelastic results as measured and as calculated from $V^{\text {opt }}$ shown in Fig. 23. The doorway parameters derived from these fitting procedures, assuming $\Gamma_{S 1}^{\dagger}=\Gamma_{S 2}^{\dagger}=\Gamma_{S}^{\uparrow} / 2$, are given in Table IV. To avoid an upper-energy "end effect," three additional doorways were postulated and distributed uniformly between 1.1 and 1.6 MeV . Their effect on the calculated results below ~0.8 MeV was small. No additional doorway states were assumed below the minimum experimental observed energy of $\sim 0.3 \mathrm{MeV}$.



Fig. 23
Comparison of Experimental Elastic Scattering Angular Distributions and Inelastic Cross Sections, EXP., of Vanadium with Those Calculated from the Intermediate Optical Potential and Statistical Theory, CAL.

113-1871

Fig. 22
Real (V) and Imaginary ( $W$ ) Portions of the Intermediate Optical Potential (Eq. 20), Calculated, Compared with the Phenomenological Optical Potential Derived from a Fit to the Measured Elastic Scattering Distributions, EXP. Positions of doorway states are indicated by arrows referring to Table IV values.

113-1872





TABLE IV. Doorway Potential Parameters Used with Eq. $20^{a}$

| No. of <br> State | $E_{S}, \mathrm{MeV}$ | $\Gamma \uparrow / \Gamma_{\mathrm{S}}^{\downarrow}$ | $\Gamma_{\mathrm{S}}($ tot $)$, <br> MeV | $\mathrm{T}_{0}$ <br> Peak | Strength, <br> $\mathrm{MeV}^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.28 | 0.3 | 0.31 | 0.74 | 1.80 |
| 2 | 0.48 | 2.02 | 0.135 | 0.88 | 0.70 |
| 3 | 0.60 | 3.52 | 0.11 | 0.54 | 0.22 |
| 4 | 0.70 | 1.99 | 0.17 | 0.89 | 0.99 |
| 5 | 0.93 | 2.33 | 0.27 | 0.78 | 0.97 |

a. Calculations used $\bar{V}=48.0 \mathrm{MeV}$ and $\bar{W}=6.5 \mathrm{MeV}$.
$V^{\text {opt }}$ qualitatively describes the features of the experimentally derived potential (see Fig. 22) with the more serious differences at the higher incident energies, where $\ell \neq 0$ contributions are of increasing importance. Vopt also provides a similar qualitative description of the measured elastic angular distributions (see Fig. 23). The.structure of the $B_{1}$ coefficient is particularly well portrayed by calculations based upon Vopt. The correlation between measured and calculated inelastic scattering is less satisfactory, but the former did not appreciably extend over much of the appropriate energy range of $V^{\circ} \mathrm{pt}$. From the doorway parameters (listed in Table IV) and $\mathrm{T}_{0}$ calculated at the peaks of the respective states, the ratios $\Gamma^{\hat{\uparrow}} / \Gamma^{\downarrow}$ and the total doorway width $\Gamma=\Gamma^{\uparrow}+\Gamma^{\downarrow}$ can be evaluated, ${ }^{1,8,71}$ with the results given in Table IV. Though speculative, the quantities are of magnitudes commensurate with the estimates of theory. ${ }^{1,8}$ Averaging $F_{1}$ and $F_{2}$ of Eq. 20 over energy intervals much greater than $\Gamma_{I S}$ or $D_{I S}$ leads to a vopt that reasonably describes the measured results averaged over a $200-\mathrm{keV}$ energy interval. However, the $s$-wave strength function calculated from $V^{\circ}{ }^{\circ}$ f for $E \rightarrow 0$ is approximately a factor of seven smaller than indicated by direct observation ${ }^{19}$ or systematics. ${ }^{57}$ This may reflect the presence of doorways near zero or negative energy not identified by the present experiments.

The above interpretation is consistent with the presently observed structure in the total and elastic scattering cross sections of vanadium. This interpretation is reasonably free of gross assumptions or the use of an unduly large number of parameters. It is a logical development of the general optical potential. The interpretation provides qualitative knowledge of the properties of doorway resonances without detailed understanding of CN resonance structure. Indeed, the method precludes a direct correlation between explicit $C N$ and doorway resonance parameters, in the manner of Monahan and Elwyn. ${ }^{67}$

## V. COMPARISON WITH ENDF-B

Since a motivation of the present work was the provision of fastneutron data for reactor design, it is instructive to compare the present results with the pertinent contents of the Evaluated Nuclear Data File-B (ENDF-B). ${ }^{10,68}$

As indicated in Fig. 24, the total cross sections determined in the present work compare reasonably well with the ENDF-B values. The ENDF-B evaluation was finished before the completion of the present work and therefore does not show the recently measured detailed resonance behavior. At higher energies, the ENDF-B values are in good agreement with the work of Galloway and Shrader ${ }^{36}$ and extrapolate well during the uncertain interval from 1.5 to 2.0 MeV . Throughout the range $0.3-10.0 \mathrm{MeV}$, the ENDF-B values are closely followed by the total cross section calculated using the potential of Section IV.A, as shown in Fig. 25. Elastic scattering cross sections contained within the ENDF-B file are in a somewhat different format from that used in Section III.B. However, when transformed to the present base (format of Eq. l), they are remarkably descriptive of the experimental values, as indicated in Fig. 26. Such differences as do exist are largely in regions of strong fluctuations. Figure 27 compares experimental and ENDF-B inelastic scattering values. The evaluation relied to an appreciable extent upon optical-model and statistical calculations, and these show the same tendency toward low cross sections for the excitation of the $320-\mathrm{keV}$ state, particularly near threshold, noted in Section IV.A. At higher energies, ENDF-B and experimental values reported by Towle are in good agreement. ${ }^{25}$


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Fig. 24. Total Cross Sections of Vanadium Derived from Present Work (top) and ENDF-B Data ${ }^{10}$ (lower)


113-492
Fig. 25. Total Cross Sections, Calculated as Described in Section IV.A, Compared with ENDF-B Values


Fig. 26
Elastic Scattering Cross Sections of Vanadium Determined in the Present Work (data points) and the Values Given by ENDF-B (solid curves)

Fig. 27
Measured and ENDF-B Inelastic Excitation Cross Sections of Vanadium. Data below 1.5 MeV (crosses) are from present work. Solid data circles are values reported by Towle. ${ }^{25}$ Solid curves are ENDF-B values. Reaction $Q$ values are indicated.

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Generally, the ENDF-B file gives a reasonable description of the results of the present experiments, though the latter show more detailed resonance structure and result in somewhat larger inelastic cross sections. Whether these are critical matters may depend upon the use of the information in the design of reactor systems. The ENDF-B values at energies $>1.5 \mathrm{MeV}$ closely correspond to other reported measurements of total and scattering cross sections and to the predictions of the optical model and statistical calculations outlined in Section IV.A.

## VI. CONCLUDING REMARKS

The observed total; elastic and inelastic scattering cross sections were characterized by both a fine and intermediate energy-dependent structure. Though of good resolution, the results did not provide a definition commensurate with compound-nucleus resonance analysis, and the interpretation was confined to the intermediate structure and the average energy dependence of the observed quantities.

A phenomenological optical-potential was shown descriptive of total and elastic scattering cross sections of vanadium over a wide energy range. Results of calculations based upon this potential and statistical theory were qualitatively descriptive of the observed inelastic scattering, but quantitatively deviated from measurement, particularly near the reaction thresholds. Consideration of alternative spin-parity assignments and/or the effects of resonance width fluctuations failed to enhance the agreement with the present experiments.

An attempt to use correlation analysis in a quantitative assay of the observed intermediate structure was inconclusive because of the effects of the finite sample range, the presence of direct reactions, and the uncertainties of the measurements.

The suitability of Ericson's concepts in the context of the present experiments is highly questionable. However, an interpretation based upon them led to reasonable strength functions, though the derived $\Gamma$ and $D$ were inconsistent with both experimental evidence and the basic premise ( $\Gamma \gg \mathrm{D}$ ).

An experimental interpretation of the observed structure in the total cross section based upon known compound-nucleus distributions in widths and spacings, assuming a nonoverlapping of partial resonance widths, resulted in compound-nucleus-level densities similar to those predicted by systematics and by extrapolation from detailed low-energy resonance studies. The result was not particularly sensitive to the form of the distributions of either $\Gamma$ or $D$, or even to the omission of the former.

The results of calculation using an intermediate optical potential, based upon the premise of a few isolated doorway states, were in qualitative agreement with the experimental elastic distributions and the phenomenological potential derived therefrom. This intermediate model used relatively few doorway parameters, and comparison with experiment led to parameter values of the magnitude expected from theoretical estimates. A wider application of the method may assist in determining some of the statistical properties of doorway states.

The latter two of the above interpretations of the intermediate structure appear physically applicable and result in qualitative agreement
with experiment. The approaches are not unique, and other interpretations have led to similar qualitative successes. ${ }^{59,67}$ The various interpretations are not necessarily mutually exclusive and may each appreciably contribute to the physical reality.

The present work indicates that the evaluated vanadium data (ENDF-B) often used in reactor calculations is reasonably representative of microscopic measurement and should be suitable for many applied studies. As increasingly fine energy groups are used in macroscopic calculation, it may become desirable to refine the evaluated data to take more cognizance of the observed fine-resonance structure. Further, it may be desirable to revise the evaluated file to bring it into better agreement with the results of the present and other recent studies of the inelastic neutron-scattering cross sections of vanadium. Such revisions will be appreciable near the first inelastic threshold ( $Q=-0.32 \mathrm{MeV}$ ).

## APPENDIX

## Tabulations of Measured Cross Sections

Tables V-VIII are provided for the use of those individuals interested in numerical values of the experimental quantities, either for pure or applied reasons.

TABLE V. Observed Total Neutron Cross Sections of Vanadium

| $E_{n}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{E}_{\mathrm{n}}, \mathrm{keV}$ | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{d}_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 100.79 | 4.58 | . 09 | 101.89 | 3,01 | . 09 |
| 102.89 | 2.42 | . 09 | 103.89 | 3.15 | . 09 |
| 104.89 | 2.39 | . 09 | 102.89 | 1.18 | . 09 |
| 106.89 | 1.97 | . 09 | 107.49 | 2.33 | . 09 |
| 108.99 | 1.65 | . 49 | 109.99 | 1, y 1 | . 09 |
| 110.99 | 1.97 | .09 | 111.99 | c.s6 | . 09 |
| 112.99 | 3.54 | .09 | 11J.Y9 | 3.47 | . 09 |
| 114.99 | 4.36 | . 0 | 112.49 | 2.46 | . 09 |
| 116.99 | 5.61 | . 09 | 11\%.99 | 6.78 | . 09 |
| 118.99 | 6.99 | .09 | 120.09 | 1.19 | . 09 |
| 121.09 | 8.61 | . US | 122.09 | 9.45 | . 09 |
| 123.09 | 9.64 | .us | $1<4.09$ | $10 .<0$ | . 09 |
| 125.09 | 10.32 | .09 | 120.09 | 10.54 | . 09 |
| 127.09 | 10.18 | . 04 | 120.10 | iv. 69 | - 09 |
| 129.10 | 12.19 | .us | 13 U.10 | 9.12 | . 09 |
| 131.09 | 9.40 | . 45 | 132.09 | 7.b1 | . 09 |
| 133.09 | 8.104 | .09 | 134.09 | 5.24 | . 09 |
| 135.09 | 6.02 | . 09 | 1360.09 | 6.96 | . 09 |
| 137.09 | 7.13 | .09 | 150.0\% | $\% .10$ | . 09 |
| 139.19 | 8.17 | . UG | 144.19 | 2.14 | . 09 |
| 141.19 | 8.93 | .09 | $14<.19$ | 8.27 | . 09 |
| 143.20 | 7.70 | .05 | 144.19 | 5.49 | . 09 |
| 145.19 | 5.07 | .ug | 140.19 | 5.87 | . 09 |
| 147.19 | 5.40 | . Uy | 140.19 | 4.99 | . 09 |
| 149.15 | 3.61 | .US | 15U.19 | S.5'2 | . 09 |
| 151.19 | 2.94 | .09 | 154.19 | 3.63 | . 09 |
| 153.19 | 5.13 | .09 | 154.19 | 5.28 | . 09 |
| 155.19 | 5.0 .7 | . 09 | 136.19 | 5.40 | . 09 |
| 157.19 | 4.74 | . 09 | 254.19 | 4.47 | . 09 |
| 159.19 | 5.28 | . 09 | 160.19 | 4.94 | . 09 |
| 161.15 | 6.05 | . U9 | 164.19 | 1.88 | . 09 |
| 163.15 | 8.43 | . | 164.19 | 9.84 | - 09 |
| 165.19 | 9.39 | .09 | 160.19 | 9.24 | . 09 |
| 167.15 | 9.49 | . | 108.19 | 9.17 | . 09 |
| 169.25 | 8.17 | . 49 | 170.29 | 6.03 | - 09 |
| 172.29 | 0.01 | .09 | 175.29 | 6.13 | . 09 |
| 174.29 | 5.97 | . 49 | 172.く9 | 5.14 | . 09 |
| 176.29 | 6.04 | . 09 | 177.49 | 5.86 | - 09 |
| 178.49 | 5.89 | . 19 | 27\%.49 | 6.16 | - 09 |
| 180.45 | 5.95 | . 49 | 181.49 | 6.28 | . 09 |

TABLE V（Contd．）

| $E_{n}$, keV | $\sigma_{T}, \mathrm{~b}$ | $d \sigma_{T}, \mathrm{~b}$ | $E_{n}$, keV | $\sigma_{T}, \mathrm{~b}$ | $d \sigma_{T}, \mathrm{~b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 182.49 | 6.57 | ． 49 | 183.49 | 6.03 | ． 09 |
| 184.49 | 7.50 | ． 09 | 185.49 | 1．51 | － 09 |
| 186.49 | 7.93 | －U9 | 181．0゙9 | 8.49 | ． 09 |
| 188.59 | 9.49 | ．US | 189．59 | 9．29 | ． 09 |
| 190.59 | 8.19 | ． 09 | 191．59 | 8.65 | ． 09 |
| 192.59 | 7.17 | －09 | 193.59 | 7．56 | ． 09 |
| 194.59 | 9.47 | ． 09 | 195．59 | 9.61 | ． 09 |
| 196.59 | 8.95 | ． 09 | $19 \%$ ．59 | 8.59 | ． 09 |
| 198.59 | 6.81 | ． 09 | 199．59 | 7.65 | －09 |
| 200．59 | 6.38 | ． 09 | ＜01． 29 | 5．58 | ． 09 |
| 202.59 | 5.11 | ． 09 | ＜03． 29 | 4．うく | ． 09 |
| 204.59 | 5.41 | －U9 | 20 2． 29 | 6.48 | ． 09 |
| 206.59 | 7.64 | .09 | 20\％．59 | 8.73 | －09 |
| 208.59 | 8.69 | ． 09 | 209．59 | 7.55 | ． 09 |
| 210.59 | 7.04 | ． 09 | 211． 29 | 6．21 | －09 |
| 212.59 | 6.39 | ． 09 | 215．59 | 6.04 | ． 09 |
| 214.59 | 6.57 | ． 09 | 215．59 | 6.42 | ．09 |
| 216．59 | 6.53 | ． 09 | 217.59 | 3.83 | .09 |
| 218.59 | 4． 42 | ． 49 | ＜19．59 | 3． 24 | ． 09 |
| 220.59 | 3.93 | ． 09 | 221．09 | 3.15 | ． 09 |
| 222.59 | 3.05 | ．US | 22S． 29 | 2.49 | .09 |
| 224.59 | 2.53 | ． 09 | 22ち．59 | 2.65 | ． 09 |
| 226．59 | 3.18 | ． 09 | c27．09 | 3.29 | ． 09 |
| 228.59 | 3.70 | ． 09 | 229．59 | 3．14 | ． 09 |
| 230.59 | 4.79 | ． 49 | 231． 39 | 5.02 | ． 09 |
| 232.59 | 7.01 | ． 09 | 255：39 | 6.27 | ． 09 |
| 234.59 | 6.70 | ． 09 | ＜35．j9 | 7.25 | ． 09 |
| 236.59 | 7.29 | ． 09 | 231．59 | 7.01 | ． 09 |
| 238.59 | 7.94 | ． 09 | 259．59 | 7．70 | ． 09 |
| 240.59 | 7.89 | ． 09 | 241．59 | 7．38． | ． 09 |
| 242.59 | 7.08 | ． 09 | 243．59 | 7.26 | ． 09 |
| 244.59 | 7．47 | ． 09 | 245．59 | 7．02 | ． 09 |
| 246.59 | 6.97 | ． 09 | 247．59 | 5.60 | －109 |
| 248.59 | 5.65 | ． 09 | 249：59 | 5.74 | ． 09 |
| 250.59 | 5.54 | ． 49 | 251．69 | 5.18 | ． 09 |
| 252.69 | 5.21 | － 49 | 2ち3．69 | 5．13 | ． 09 |
| 254.69 | 5.33 | ． 09 | ＜う5．69 | 2.67 | －09 |
| 256.69 | 5.88 | ． 49 | ＜57．09 | 5.05 | －09 |
| 258.69 | 5.16 | ． 09 | 259．69 | 4.12 | ． 09 |
| 260.69 | 3.92 | ． 09 | 261．69 | 3.37 | ． 09 |
| 262．69 | 3.06 | ． 09 | 265．70 | 3.07 | ． 09 |
| 264.69 | 4.31 | ． 09 | 265．10 | 4.42 | －09 |
| ＇266．06 | 4.18 | ．U9 | 261．09 | 4.43 | ． 09 |

TABLE V（Contd．）

| $E_{n}, \mathrm{keV}$ | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $d \sigma_{T}, \mathrm{~b}$ | $E_{n}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 268．69 | 4.30 | .09 | ＜64．69 | 3.69 | －09 |
| 270.69 | 2.90 | .09 | 271．09 | 2．48 | ． 09 |
| 272.70 | 2.54 | ． 49 | 275.69 | 2．19 | －09 |
| 274.69 | 2，58 | ． 49 | 275.69 | 4.50 | ． 09 |
| 276.69 | 5.13 | ． 49 | 277.69 | 5.15 | －09 |
| 278.69 | 5.45 | ． 09 | 279.69 | 5.52 5.99 | .09 |
| 280.69 | 5.88 | ． 09 | 281.09 285.69 | 5.99 6.49 | ． 09 |
| 282.69 | 6.30 | ． 09 | 283．69 | 5.83 | ． 09 |
| 284.69 | 6.11 | ． 09 | 285．09 | 5.40 | ． 09 |
| 287.69 | 5.35 | ． 49 | 280．09． | 5.68 | ． 09 |
| 289.69 | 5.85 | － 9 | 290.09 29.69 | 5.05 | .09 |
| 291.69 | 5.69 | ． 09 | 292．09 | 5.093 | ． 09 |
| 293.69 | 5.71 | ． 09 | 294．69 | 5，44 | ． 09 |
| 295.69 | 5.26 | ． 09 | 296.09 | 5，44 | ． 09 |
| 297.69 | 5.40 | ． 09 | 290．69 | 5.46 | ． 09 |
| 299.69 | 5.97 | ． 49 | 300．09 | 5.80 | ． 09 |
| 301.69 | 6.12 | ． 09 | 302．09 | 0.04 | ． 09 |
| 303.89 | 7.60 | ． 09 | 504．89 | 0．48 | ． 09 |
| 305.89 | 7.01 | ． 09 | 506：89 | $\%$ | ． 09 |
| 307.89 | 7.36 | － 49 | S10．89 | 5.46 | .09 |
| 309.89 | 6.6 ？ | －U9 | S14．89 | 4.80 | ． 09 |
| 311.89 | 4.58 | ． 49 | 312．89 | 4.80 | ． 09 |
| 313.89 | 5.19 | ． 09 | 314.89 | 4.98 | ． 09 |
| 315.89 | 4.98 | ． 09 | S10．09 | 4.80 | ， 09 |
| 317.89 | 5.59 | ． 09 | 518．89 | 6.41 | ． 09 |
| 319.89 | 6.47 | ． 09 | － | 5.03 | .09 |
| 321.99 | 5.94 | ． 09 | 322．99 | 4.11 |  |
| 323.99 | 4.45 | ． 09 | 324．99 | 4.11 | ． 09 |
| 325.99 | 3.49 | ． 49 | 520．99 | 4.19 | ． 09 |
| 327.99 | 5.08 | ． 09 | 320．99 | 5．01 | ．09 |
| 329.99 | 4.51 | ．U9 | S3U．99 | 5．97 | ． 09 |
| 331.49 | 5.22 | ． 09 | 53249 | 5．94 | ． 09 |
| 333.49 | 6． 44 | ． 09 | 534．49 | 5.81 | ． 09 |
| 335.49 | 5.71 | ． 09 | S30．49 | 4.95 | ． 09 |
| 337.49 | 5.63 | ． 09 | S4i．49 | 5.03 | ． 09 |
| 339.49 | 5.39 | ． 09 | 542．49 | 4.08 | ． 09 |
| 341.49 | 4.65 | ．09 | 342．49 | 4.47 | ． 09 |
| 343.49 | 4.69 | ． 09 | 5440．49 | 3.75 | .09 |
| 345.49 | 4.16 | ．09 | 540．49 | 3.29 | － 09 |
| 347.49 | 3.33 | ．09 | 550．49 | $2 .<6$ | .09 |
| 349.49 | 2.14 | ． 49 | ง5：．49 | 4.54 | ． 09 |
| 351.49 | 3.87 4.70 | ． 099 | 554．49 | 5.51 | ． 09 |
| 353.49 | 4.70 | ． 09 | くちゃ． |  |  |

TABLE V（Contd．）

| $\mathrm{E}_{\mathrm{n}}, \mathrm{keV}$ | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ | $E_{n}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d}_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 355.49 | 5.67 | ． 09 | 356.49 | 6.42 | ． 09 |
| 357.49 | 6.58 | ． 09 | 350．49 | 5.93 | .09 |
| 359.49 | 5.24 | ． 09 | 360．49 | 4．70 | .09 |
| 361.59 | 4.42 | .09 | 362．59 | 4．50 | ． 09 |
| 363.59 | 4.21 | .09 | 364．59 | 3.93 | ． 09 |
| 365.59 | 4.89 | .49 | 366.60 | 4.11 | ． 09 |
| 367.59 | 4.76 | ． 09 | 564， 99 | 4.96 | ． 09 |
| 369.59 | 4.99 | .09 | 370．ら9 | 5.39 | ． 09 |
| 371.59 | 5.00 | .09 | 372．59 | 4.74 | ． 09 |
| 373.59 | 4.90 | .$\cup 9$ | 374．39 | 4.47 | .09 |
| 375.60 | 4.42 | .09 | 570．79 | 4.35 | ． 09 |
| 377.59 | 3.68 | ． 09 | 376．59 | 3.11 | ． 09 |
| 379.59 | 3.06 | ． 39 | 38U．う9 | 2.99 | ． 09 |
| 381.60 | 3.05 | ． 09 | 38く．う9 | 3.13 | ． 09 |
| 383.59 | 2.88 | .09 | 384．59 | 3.14 | ． 09 |
| 385.59 | 3.10 | ． 09 | 386．59 | 2.45 | ． 09 |
| 387.59 | 2.09 | ．09 | 388．59 | 2.08 | .09 |
| 387.89 | 1.96 | .09 | 580．09 | 2.44 | ． 09 |
| 389.89 | 2.36 | .09 | 590．89 | 3．33 | ． 09 |
| 392.89 | 2.53 | .09 | 5yS． 89 | 2.99 | ． 09 |
| 394.89 | 3.75 | .09 | 3ソつ．す9 | 4．49 | ． 09 |
| 396.89 | 4.71 | .49 | 591．89 | 4.81 | ． 09 |
| 398.89 | 4.16 | ． 09 | SYy．09 | 4.83 | ． 09 |
| 400.89 | 4.07 | ． 09 | 401.89 | 4.32 | ． 09 |
| 402.89 | 4.01 | .09 | 40S．90 | 4．38 | ． 09 |
| 404.89 | 4.13 | ． 09 | 403098 | 4.60 | ． 09 |
| 406.89 | 4.70 | .09 | 407.89 | $4 .<4$ | ． 09 |
| 408.89 | 4.44 | .09 | 409．90 | 4，47 | ． 09 |
| 410.89 | 4.22 | .09 | 412.09 | 4.38 | ． 09 |
| 413.09 | 4.23 | ． 09 | 414.10 | 2．80 | ． 09 |
| 415.09 | 2.56 | ． 09 | 416.09 | 2．01 | ． 09 |
| 417.09 | 2.41 | ． 09 | 418.09 | 2．27 | ． 09 |
| 419.09 | 2.09 | .09 | 420.09 | 1．47 | ． 09 |
| 421.09 | 2.27 | ． 09 | 422.09 | 2.13 | ． 09 |
| 423.09 | 2.20 | .09 | 424.09 | 2．12 | ． 09 |
| 425.09 | 2.23 | .09 | 420.09 | 2，97 | ． 09 |
| 427.09 | 2.84 | ． 09 | 420.09 | 3.03 | ． 09 |
| 429.09 | 3.43 | .09 | 430.09 | 3.24 | ． 09 |
| 431.09 | 3.33 | ． 09 | 432.09 | 3.53 | ． 09 |
| 433.09 | 3.79 | ． 09 | 434．09 | 4.20 | ． 09 |
| 435.09 | 4.58 | ． 09 | 430.14 | 4.85 | ． 09 |
| 437.09 | 5.19 | .09 | 436.09 | 4.57 | ． 09 |
| 439.09 | 4.59 | .09 | 440.09 | S．28 | ． 09 |

TABLE V (Contd.)

| $\mathrm{E}_{\mathrm{n}}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $d \sigma_{T}, \mathrm{~b}$ | $E_{n}, \mathrm{keV}$ | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 441.09 | 2.36 | .09 | 442.09 | 2. 27 | .09 |
| 443.09 | 2.71 | . 00 | 444.09 | 3.57 | . 09 |
| 445.10 | 3.43 | . 05 | 446.09 | 5.07 | . 09 |
| 447.09 | 3.57 | . 09 | 440.09 | 3.52 | . 09 |
| 449.09 | 4.97 | .0\% | 450.09 | 5.12 | . 09 |
| 451.09 | 5.36 | . 09 | 452.09 | 5.44 | . 09 |
| 453.09 | 5.38 | .09 | 454.09 | 5.11 | -09 |
| 455.09 | 5.30 | .09 | 450.09 | 5.18 | . 09 |
| 457.09 | 4.82 | .uy | 450.09 | 4.82 | -09 |
| 459.09 | 5.00 | .0y | $400 . \cup 9$ | 3.43 | . 09 |
| 401.09 | 5.38 | . 09 | 402.09 | 5.92 | - 09 |
| 463.09 | 5.19 | . 09 | 464.49 | 4.06 | . 09 |
| 465.05 | 4.01 | . 4 | 460.09 | 4.48 | . 09 |
| 467.09 | 3.47 | .49 | 460.09 | 3.16 | . 09 |
| 469.09 | 3.19 | . 09 | 470.09 | 2.35 | - 09 |
| 471.09 | 2.53 | . U' | 472.09 | 2.47 | - 09 |
| 473.09 | 2.25 | .09 | 474.09 | 2.33 | . 09 |
| 475.19 | 2.37. | . UG | 470.19 | 2.49 | . 09 |
| 477.19 | 3.49 | - | 470.19 | 5.42 | . 09 |
| 479.19 | 3.18 | .09 | 40 V 19 | 5.56 | - 09 |
| 481.19 | 3.73 | . 09 | $40<.19$ | 4.09 | -09 |
| 483.19 | 3.45 | . 09 | 484.19 | 3.60 | - 09 |
| 485.19 | 3.89 | .09 | 480.19 | 5.67 | . 09 |
| 487.19 | 3.80 | .09 | 488.19 | 3.48 | . 09 |
| 489.19 | 3.57 | . 09 | 490.19 | 3.43 | . 09 |
| 491.19. | 3.06 | . 07 | 44く.19 | 3.6\% | . 09 |
| 493.19 | 3.47 | . 09 | 494.19 | 3.40 | . 09 |
| 495.19 | 3.13 | .us | 496.19 | 3.10 | -09 |
| 497.15 | 3.17 | . 09 | 440.19 | 3.12 | . 09 |
| 499.15 | 3.35 | . 0.9 | 200.19 | 3.46 | . 09 |
| 501.19 | 2.60 | .09 | 202.19 | 2.56 | -09 |
| 503.19 | 2.04 | . U9 | 2U4.19 | 1.10 | . 09 |
| 505.19 | 1.36 | . 49 | 200.19 . | 1.67 | - 09 |
| 505.58 | 1.41 | . 14 | 200.08 | - 7 | -15 |
| 506.58 | 1.35 | . 14 | 201.08 | . 87 | -15 |
| 507.59 | . 72 | . 15 | 206.u9 | 1.20 | . 14 |
| 508.00 | 1.38 | . 14 | 20y.10 | 1.46 | -14 |
| 514.21 | 4.66 | . 10 | 214.15 | 4.48 | -10 |
| 515.24 | 4.52 | . 10 | 212.16 | 4.35 | . 10 |
| 516.28 | 3.73 | . 11 | 210.19 | 4.11 | . 10 |
| 517.31 | 3.c1 | . 11 | 511.03 | 3.47 | . 11 |
| 518.35 | 3. 24 | . 11 | 210.08 | 5.44 | . 10 |
| 519.40 | ¢. 66 | .12 | 21\%.9゙2 | 3.56 | . 10 |


| $\mathrm{E}_{\mathrm{n}}, \mathrm{keV}$ | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ | $E_{n}$, keV | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 520.44 | 2.75 | .11 | 220．97 | 2.17 | －11 |
| 521.49 | 3.16 | .10 | วさく．U2 | 3．30 | .10 |
| 522.55 | 3．2゙ | .11 | 223．08 | 3.65 | .10 |
| 523．00 | 3．t5 | ． 10 | 224．13 | 3．5う | ． 10 |
| 524.06 | 3.01 | ． 10 | 222．＜0 | 3．24 | －10 |
| 525.73 | 3.28 | .10 | 220.26 | 2．99 | ． 11 |
| 526.79 | 3.1 .4 | .10 | 221．53 | 2，65 | .11 |
| 527.86 | 3.18 | .10 | 228．40 | く， 29 | ．11 |
| 528.94 | 2.10 | ． 12 | 524．47 | 2.29 | ． 11 |
| 530.01 | 2．03 | ． 11 | う30．ちら | 1．75 | .12 |
| 531.09 | 1.62 | .12 | 231．03 | 1.63 | ． 12 |
| 533.26 | 1．08 | ． 14 | 533.81 | 1.15 | ． 14 |
| 534.35 | 1．4．4 | .13 | 勺34．90 | 1.70 | ． 13 |
| 535.44 | 1．83 | .13 | りくら，サ9 | 1.89 | ．13 |
| 536.54 | 2．14 | ． 12 | づ1．U9 | 2.36 | －12 |
| 537.64 | 2．08 | ． 12 | 230.19 | 2.01 | ． 12 |
| 538.74 | 2．91 | ． 11 | こうy． 0 | 2.91 | ． 11 |
| 539.85 | 2.94 | ． 12 | 240.41 | 3．20 | $\bigcirc 11$ |
| 540.96 | 3．05 | ． 11 | 241.52 | 2.86 | .11 |
| 542.08 | 2.72 | ． 11 | 242．05 | 2．45 | ． 12 |
| 543.19 | 2.18 | ． 12 | 245.15 | 1，¢ 7 | ． 12 |
| 544.31 | 2.29 | ． 12 | 544.87 | 2．52 | ． 12 |
| 545.44 | 2.50 | ． 11 | 240．00 | 2.35 | ． 11 |
| 546.57 | 1.73 | .12 | $24 / .13$ | 1.65 | ． 12 |
| 547.70 | 1.75 | .12 | 246．26 | 1.67 | ． 12 |
| 548.83 | 1.88 | ． 12 | 24\％．40 | 2.62 | ． 11 |
| 549.97 | 2.79 | ． 11 | ううU．う4 | S．11 | .10 |
| 551.11 | 3.14 | .10 | りち1．69 | 3.18 | .10 |
| 552.26 | 2.69 | ． 11 | うち2．83 | C． 46 | ． 10 |
| 553.41 | 2.36 | ． 11 | つちら．988 | 2． 26 | ． 11 |
| 554.56 | 2.20 | ． 11 | 252．14 | 1.79 | ． 12 |
| 555.72 | 1.47 | .22 | 550.30 | 1.58 | ． 12 |
| 556.88 | 1.53 | ． 12 | 251．46 | 1.36 | ． 12 |
| 558．04 | 1.43 | .12 | 250.03 | 1.64 | ． 12 |
| 559.21 | 1.74 | .12 | つう9．80 | 1.00 | ． 11 |
| 560.38 | 1.90 | .12 | 20U． $\mathrm{U}^{\prime}$ | 1.98 | ． 11 |
| 561.56 | 1.91 | .11 | 20く．15 | 2．20 | ． 11 |
| 562.74 | ＇2． 54 | ． 111 | 205．33 | 2．＜6 | ． 11 |
| 563．92 | 1.82 | .11 | 264.31 | 2．11 | ． 11 |
| 565．11 | 1.72 | .11 | 260．10 | 1．84 | ． 11 |
| 566.50 | 1.35 | $.1<$ | 260.09 | 1． 21 | .12 |
| 567.49 | 1.11 | .12 | 260．j9 | 1．25 | ． 12 |
| 568.69 | 1.43 | .12 | 20y．く9 | 1．só | .12 |

TABLE V (Contd.)

| $E_{n}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $d \sigma_{T}, \mathrm{~b}$ | $E_{n}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 569.89 | 1.11 | . 12 | 270.50 | 1. 51 | - 12 |
| 571.10 | 1.64 | . 11 | 271.10 | 1.08 | -11 |
| 572.31 | 2.08 | .11 | 572.92 | 1.67 | -11 |
| 573.52 | 2.45 | .10 | 274:13 | 2,90 | - 10 |
| 574.74 | 3.23 | .09 | 275.35 | 4.07 | - 09 |
| 575.96 | 4.40 | .08 | 576.37 | 4.40 | - 09 |
| 577.19 | 4.50 | . 08 | 571.00 | 4.47 | - 08 |
| 578.42 | 4.23 | . 09 | 279.03 | 4.11 | . 08 |
| 579.65 | 4.35 | .08 | 280.27 | 4.29 | . 08 |
| 580.89 | 3.78 | .US | 281.31 | 3.57 | . 09 |
| 582.13 | 2.94 | . 10 | 282.15 | 2.23 | . 10 |
| 583.38 | 1.96 | . 11 | 584.00 | 2.47 | . 15 |
| 584.63 | 2.42 | . 10 | 282.25 | 2.24 | -10 |
| 585.88 | 2.15 | .11 | 586.51 | 2.40 | -10 |
| 587.14 | 2.62 | . 10 | 581.17 | 2.59 | -10 |
| 588.40 | 3.02 | . 10 | 289:03 | 3.47 | .10 |
| 589.67 | 3.69 | . 09 | 290.50 | 5.02 | . 09 |
| 590.94 | 3.29 | . 49 | 291:57 | 3.53 | . 09 |
| 592.21 | 3.10 | . 10 | 294.85 | 3.45 | - 09 |
| 593.49 | 2.03 | . 10 | 594.13 | 3.45 | -09 |
| 594.77 | 3.31 | . 49 | 292.42 | 5.63 | -09 |
| 596.06 | 4.18 | . 48 | 296.70 | 4.16 | -09 |
| 597.35 | 4.18 | .09 | 998.00 | 4.56 | - 08 |
| 598.65 | 4.12 | . 09 | 299.50 | 4.00 | -09 |
| 599.95 | 3.98 | . 09 | 600.60 | 3.49 | . 09 |
| 601.25 | 3.25 | . 09 | 001.90 | 3.48 | - 09 |
| 602.56 | 3.39 | . 09 | 605.21 | 3.23 | - 09 |
| 603.87 | 3.20 | . 09 | 004.53 | 2.95 | - 09 |
| 605.19 | 3.18 | . 09 | 602.85 | 3.55 | -09 |
| 006.51 | 2.98 | . 09 | 60\%.17 | 3.10 | - 09 |
| 607.84 | 2.92 | . 09 | 008.50 | 2.97 | - 09 |
| 609.17 | 3.33 | . 69 | 009.83 | 3.17 | . 09 |
| 610.50 | 3.69 | . 09 | 611.17 | 3.83 | - 09 |
| 611.84 | 3.59 | .09 | 612.51 | 3.03 | . 09 |
| 613.19 | 3.51 | .09 | 615.86 | 5.10 | . 09 |
| 614.53 | 2.88 | . 09 | 012.21 | 3.17 | . 09 |
| 015.89 | 2.98 | . 09 | 016.57 | 3.15 | : 09 |
| 617.24 | 3.43 | . 09 | 617.42 | 3.34 | -09 |
| 618.61 | 3.34 | . 09 | 617.29 | 3.50 | -09 |
| 019.97 | 3.49 | . 19 | 520.00 | 3.29 | . 09 |
| 621.34 | 2.81 | . 09 | 022.43 | 2.83 | - 09 |
| 622.72 | 2.76 | . 09 | 025.41 | 2.74 | - 09 |
| 624.10 | 2.73 | .09 | 624.19 | 3.06 | . 09 |


| $E_{n}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{E}_{\mathrm{n}}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $d \sigma_{T}, \mathrm{~b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 025.49 | 3.187 | ．U9 | 026.18 | 3.16 | ． 09 |
| 626.88 | 2.48 | ． 10 | 62\％． 7 | 2.10 | ． 10 |
| 628.27 | 2.12 | ． 10 | 028.97 | 2.20 | ． 10 |
| 629.67 | 1.81 | .10 | 63 ¢， 7 | 1.97 | ．10 |
| 631.07 | 1.46 | .15 | －S1．78 | 1.52 | －11 |
| 632.48 | 1.59 | ． 10 | 035.19 | 1，47 | ． 10 |
| 633.89 | 2.57 | ． 49 | 034.60 | 3，U | ． 09 |
| 635.31 | 3.63 | ． 48 | 030.42 | S．49 | ． 09 |
| 036.74 | 3.77 | ． 09 | $63 \% .45$ | 4.07 | .08 |
| 638.16 | 4.15 | ． 08 | 636．8゙8 | 4， 31 | ． 08 |
| 639.60 | 4.49 | ． 08 | $64 \cup .32$ | 4，16 | ． 08 |
| 641.04 | 3.98 | ． 08 | 041.76 | 3.90 | ． 08 |
| c42．48 | 3.86 | ． 08 | 645．20 | 3.40 | ． 09 |
| 043.93 | 3.00 | .09 | 644．65 | 2．81 | ． 09 |
| 645.38 | 2.42 | .10 | 046.11 | 2.13 | .10 |
| 646.84 | 2.34 | .15 | 047：27 | 2.29 | ． 15 |
| 648.30 | 2.35 | ． 11 | 64\％．03 | 2.29 | ． 11 |
| 649．77 | 2.76 | ． 11 | とうU．う0 | 3.43 | ． 10 |
| 651.24 | 3.55 | ． 10 | 651．98 | 3.10 | －10 |
| 652.72 | 3.83 | ． 10 | ర5S．46 | 4.10 | ． 09 |
| 654.20 | 4.15 | ． 09 | 6ち4．y4 | 4.80 | ． 09 |
| 655.69 | 4.97 | ． 09 | 050.43 | 4.39 | － 09 |
| 657.18 | 3.66 | ． 1 Ù | 051.93 | 3.16 | ． 10 |
| 658．68 | 3.20 | .10 | 659.43 | 3.40 | ． 10 |
| 660.18 | 3.77 | ． 10 | $06 \cup .94$ | 3.92 | － 09 |
| 661.69 | 4.31 | ． 19 | 062.45 | 4.62 | ． 09 |
| 663.21 | 4.83 | ．$\checkmark 9$ | 06.5 .76 | 4.54 | ． 09 |
| 664.72 | 4.49 | ． 09 | 005．49 | 4．16 | ． 09 |
| 666.25 | 4.01 | .09 | 061.41 | 5.48 | ． 10 |
| $667.7 \varepsilon$ | 2.77 | .10 | 068.55 | 2．44 | ． 11 |
| 669.31 | 2.42 | ． 11 | 070.18 | 2.04 | ． 11 |
| 670.86 | 2.12 | ． 11 | 671.03 | 2．37 | ． 11 |
| 672.40 | 2.29 | .11 | 075.18 | 2.66 | ． 11 |
| 673.95 | 3.10 | .10 | 674.73 | 3．00 | ． 10 |
| 675．51 | 3．03 | .10 | $676 .<9$ | 2，＜7 | ． 11 |
| 677.07 | 2.69 | .10 | 6\％1．86 | 2．00 | ． 11 |
| 678.64 | 2． 15 | ． 11 | 079.43 | 2．11 | ． 11 |
| 680.21 | 1.74 | $.1 \%$ | $001!0$ | 1.06 | ． 12 |
| 681.75 | 2.41 | .11 | 082．58 | 2.65 | ． 10 |
| 683.38 | 3.15 | ． 10 | 680．26 | 4.16 | ． 09 |
| 687.36 | 4．17 | ． 09 | 000.16 | $4 .<8$ | ． 09 |
| 688.97 | 4．27 | ． 08 | 08\％．17 | 4.50 | ． 09 |
| 690.58 | 4．80 | ． 08 | 641.38 | 4．47 | ． 09 |

TABLE V（Contd．）

| $E_{n}$, keV | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ | $E_{n}, \mathrm{keV}$ | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $d \sigma_{T}, \quad \mathrm{~b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 692．19 | 4．41 | －． 09 | 695．00． | 4.60 | .09 |
| 693.81 | 3.93 | .09 | 694．03 | 3.37 | .10 |
| 095.44 | 3．25 | ． 10 | 090.26 | 2.81 | ． 10 |
| 697.07 | 2.93 | ． 10 | 697． 09 | 2.60 | ． 10 |
| 698.71 | 2.53 | ． 10 | 699．54 | 2.37 | .11 |
| 700.36 | 2.83 | ． 10 | 701．18 | 2.94 | ． 10 |
| 702.01 | 3.24 | －U9 | 102.84 | 3．37 | ． 09 |
| 703.67 | 3， 55 | ． 09 | 704.50 | 4.23 | －09 |
| 705.33 | 3.08 | .09 | 706.16 | 3，61 | ． 09 |
| 707.00 | 3．91 | ． $09^{\circ}$ | $70 \% .83$ | 3.90 | － 09 |
| 708.67 | 4.21 | ． 08 | 709．21 | 4.33 | ． 08 |
| 710.35 | 4.01 | .09 | 711．19 | 3.52 | ． 09 |
| 712.04 | 2.97 | .10 | 712.88 | 3.11 | －10 |
| 713.73 | 2.70 | .10 | 114.58 | 2.55 | ． 10 |
| 715.43 | 2.54 | .10 | 716.28 | 3.07 | ． 09 |
| 717.13 | 3.04 | .10 | 11／．99 | 3：06 | $\bigcirc 10$ |
| 718.85 | 3.08 | ． 10 | 719.70 | 3.51 | ． 09 |
| 720.56 | 3.14 | ． 09 | 721.42 | 3.77 | ． 09 |
| 722.29 | 3.51 | .09 | 125.15 | 3．14 | ． 09 |
| 724.02 | 3.21 | ． 09 | 724.88 | 2.58 | ． 10 |
| 725.75 | 2.40 | .10 | 726.62 | 2.84 | －10 |
| 727.50 | 3.02 | .10 | 128.57 | 3.58 | － 09 |
| 729.24 | 3.77 | ． 09 | $73 \cup .12$ | 5.79 | － 09 |
| 731.00 | 3.65 | ． 09 | 731，08 | 5．82 | ． 09 |
| 732.76 | 3.74 | .09 | 135．64 | 3.25 | －09 |
| 734.53 | 3.13 | ． 09 | 130.42 | 3.57 | ． 09 |
| 736.30 | 3.13 | ．U9 | 157．19 | 3.42 | ． 09 |
| 738.09 | 3．52 | ． 09 | 130.98 | 3.22 | －09 |
| 739.87 | 2.96 | .09 | 740.77 | 3.01 | － 09 |
| 741.67 | 2.64 | ． 10 | 74く． 57 | 2． 26 | －10 |
| 743.47 | 2.87 | .09 | 744．37 | 2.58 | ． 10 |
| 745.28 | 2.19 | ． 10 | 140．18 | 2.02 | ． 10 |
| 747.09 | 1.00 | ． 11 | 148.00 | 1.14 | ． 10 |
| 748.91 | 1.71 | ． 11 | 749．82 | 1.47 | ． 15 |
| ．750．74 | 1.62 | .15 | 151．65 | 1.46 | ． 15 |
| 752.57 | 1.74 | ． 09 | 155.49 | 2.27 | ． 09 |
| 754.41 | 2.33 | .09 | ブち． 54 | 2.58 | － 09 |
| 756.26 | 3.02 | ． 08 | 157．19 | 2.76 | －08 |
| 758.12 | 2.82 | ． 48 | 159．0゙5 | 2.85 | ． 08 |
| 759.98 | 2.61 | ． 08 | 760.91 | 2.93 | ． 08 |
| 761.85 | 2.69 | ． 08 | 706．18 | 2.03 | ． 08 |
| 763.72 | 2.20 | .09 | 164.06 | 1.86 | ． 09 |
| 765.61 | 1.70 | .09 | 166.55 | 1．18 | ． 09 |

TABLE V (Contd.)


TABLE V (Contd.)

| $\mathrm{E}_{\mathrm{n}}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ | $E_{n}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 855.97 | 1.44 | . 12 | 051.09 | 1,14 | . 12 |
| 858.21 | 1.95 | . 11 | ه5\%. 53 | 2.60 | -10 |
| 860.46 | 2.59 | . 10 | 861.59 | 2.69 | -10 |
| 862.71 | 3.21 | . 10 | 063.05 | S.cic | - 10 |
| 864.98 | 3.45 | .49 | 006.12 | 3.75 | - 09 |
| 867.25 | 3.82 | .09 | 860.40 | 4.34 | . 09 |
| 869.54 | 4.95 | .08 | 37 V 68 | 4.86 | . 08 |
| 871.83 | 5.40 | . 08 | 574.98 | 4.92 | . 08 |
| 874.13 | 4.21 | . 48 | 675.29 | 3.75 | . 09 |
| 876.44 | 3.46 | . 09 | 871.00 | 3.65 | . 09 |
| 878.76 | 3.27 | .09 | 879.93 | 3.40 | - 09 |
| 881.09 | 3.70 | . 09 | 082.26 | 3.92 | - 09 |
| 883.43 | 4.30 | .08 | 884.61 | 4.71 | - 08 |
| 885.78 | 4.21 | . 08 | 886.96 | 4.21 | - 08 |
| 888.14 | 3.71 | .09 | 089.32 | 3.54 | -09 |
| 890.51 | 3.10 | . UG | 891.09 | 3.16 | . 09 |
| 892.88 | 3.17 | . 09 | 894.08. | 3.03 | . 09 |
| 895.27 | 3.25 | .09 | 896.47 | S.40 | . 09 |
| 897.67 | 3.10 | .09 | 898.87 | 2.47 | -10 |
| 900.07 | 2.79 | . 10 | 901.<8 | 2.13 | . 10 |
| 902.49 | 3.25 | .09 | 905.10 | 5.46 | - 09 |
| 904.91 | 4.00 | . 08 | $\pm 00.13$ | 4.51 | - 08 |
| 907.35 | 4.27 | . 08 | 90d.)7 | 4.21 | - 08 |
| 909.80 | 3.61 | . 08 | 911.02 | 5.72 | - 09 |
| 912.25 | 3.17 | . 09 | 913.48 | 3.04 | - 09 |
| 914.72 | 2.78 | . 49 | 412.95 | 2.29 | -10 |
| 917.19 | 2.48 | . 10 | 916.43 | 2.c2 | -10 |
| 919.68 | 2.39 | . 10 | 920.92 | $3 .<9$ | - 09 |
| 922.17 | 3.28 | .09 | 925.43 | 5.60 | -08 |
| 924.68 | 3.69 | . 08 | 923.94 | 3.81 | - 08 |
| 927.20 | 4.19 | .08 | 920.46 | 4.56 | - 08 |
| 929.72 | 4.55 | . 08 | 430.99 | 4.11 | - 08 |
| 932.26 | 4.11 | . 08 | 935.53 | 3.38 | - 09 |
| 934.81 | 3.10 | .09 | 930.49 | 3.12 | - 09 |
| 937.37 | 3.03 | . 09 | 430.65 | 3.13 | -09 |
| 939.94 | 3.10 | .09 | 941.23 | 3.27 | -09 |
| 942.52 | 2.97 | .09 | 945.81 | 3.53 | -13 |
| 945.11 | 3.32 | . 09 | 940.41 | 3.34 | - 09 |
| 947.71 | 2.87 | . 09 | 949.01 | 2,41 | - 09 |
| 950.32 | 2.70 | .09 | Y ¢1.03 | 2.64 | . 09 |
| 952.95 | 2.61 | . 09 | 954.26 | 3.61 | -09 |
| 955.58 | 3.43 | .48 | 956.90 | 3.21 | -09 |
| 958.23 | 3.05 | . 09 | yวy.つ5 | 2.44 | -09 |

TABLE V (Contd.)

| $E_{n}, \mathrm{keV}$ | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ | $E_{n}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 960.88 | 2.59 | .09 | 902.21 | 2.42 | . 09 |
| 963.55 | 2.68 | . 09 | 964.89 | 2.02 | . 09 |
| 966.23 | 3.15 | .09 | 468.92 | 3.90 | . 08 |
| 570.27 | 4.26 | . $0 \%$ | 971.62 | 4.02 | . 08 |
| 972.97 | 4.12 | . 08 | 974:33 | 3,76 | . 08 |
| 975.69 | 2.75 | . 09 | 977.06 | 3.26 | .09 |
| 978.42 | 3.44 | . 08 | 979.19 | 3,79 | . 08 |
| 981.16 | 3.75 | . 08 | 982.54 | 3.49 | . 08 |
| 983.92 | 3.18 | . 09 | 985.50 | 2.83 | . 09 |
| 986.68 | 2.77 | . 09 | 988.07 | 2.17 | . 09 |
| 989.46 | 2.75 | .09 | 990.8.8 | 2,80 | . 09 |
| - 992.25 | 2.95 | . 09 | 495.65 | 2.95 | . 09 |
| 995.05 | 3.05 | . 09 | 490.45 | 2.65 | .10 |
| 997.86 | 2.92 | .09 | 999.27 | 3.27 | - 09 |
| 1000.69 | 2.65 | . 10 | 1002.10 | 3.04 | . 09 |
| 1003.52 | 2.83 | .10 | 1004.95 | 3.24 | . 09 |
| 1006.37 | 3.17 | . 10 | 1007.00 | 3.35 | . 09 |
| 1009.23 | 2.84 | . 10 | 1010.07 | 2.64 | . 10 |
| 1012.11 | 3.17 | . 09 | 1015.55 | 3.47 | . 09 |
| 1014.99 | 3.77 | .09 | 1016.44 | 4.04 | . 08 |
| 1017.89 | 3.79 | .09 | 1020.00 | 3.22 | . 09 |
| 1019.34 | 3.25 | .09 | 1020.80 | $3.2 \%$ | . 09 |
| 1022.26 | 2.67 | . 10 | 1uく5.72 | 2.68 | . 10 |
| 1025.19 | 2.54 | . 10 | 1026.06 | 2.31 | . 10 |
| 1028.13 | 2.38 | . 10 | 1029.01 | 2.03 | . 10 |
| 1031.09 | 2.33 | .10 | 1032.57 | 2.44 | .10 |
| 1034.06 | 2.34 | .10 | 1US5.55 | 2.45 | .10 |
| 1037.04 | 2.38 | . 10 | 1040.03 | 2.31 | . 10 |
| 1041.53 | 2.52 | .10 | 1045.04 | 2.93 | . 09 |
| 1044.55 | 3.09 | . 09 | 1446.06 | 2.68 | . 09 |
| 1047.58 | 2.65 | . 09 | 1049.09 | 2.38 | .09 |
| 1050.62 | 2.15 | .10 | $105<.14$ | 2,58 | . 09 |
| 1053.67 | 2.15 | . 10 | 105 $2 .<0$ | 2.47 | . 14 |
| 1056.74 | 2.79 | . 14 | 1050.c8 | 2,85 | . 13 |
| 1059.82 | 2.93 | .13 | 1061.36 | 3.17 | . 09 |
| 1062.91 | 2.90 | . 04 | 1064.46 | 2.92 | . 09 |
| 1066.02 | 2.71 | .09 | 1061.28 | 2.75 | . 09 |
| 1069.14 | 3.20 | .09 | 1070./1 | 5.08 | . 09 |
| 1072.28 | 3. 38 | .09 | 1075.05 | 5.04 | . 09 |
| 1075.43 | 3.16 | . 09 | 107\%.01 | 3.28 | .09 |
| 1078.59 | 3.32 | . 49 | 1080.18 | 3.20 | . 08 |
| 1081.77 | 3.25 | .09 | 1003.56 | 3.31 | . 09 |
| 1084.96 | 3.44 | . 08 | 1086.26 | 3.50 | . 08 |

TABLE V (Contd.)

| $\mathrm{E}_{\mathrm{n}}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ | $E_{n}, \mathrm{keV}$ | $\sigma_{\mathrm{T}}, \mathrm{b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1088.17 | 3.46. | . 08 | 1089,78 | 3.50 | . 08 |
| 1091.39 | 3.27 | . 49 | 109S.00 | 3.47 | . 08 |
| 1094.62 | 3.31 | .09 | 1496.25 | 3.48 | . 08 |
| 1099.50 | 3.12 | . 14 | 1101,14 | 3.84. | . 09 |
| 1102.77 | 4.15 | .09 | 1104.41 | 4.65 | . 08 |
| 1106.06 | 4.16 | . 09 | 1107.71 | 4,31 | . 09 |
| 1109.36 | 4.15 | .09 | 1111.02 | 3.75 | . 09 |
| 1112.68 | 3.49 | . 09 | 1114,34 | 5.44 | . 09 |
| 1116.01 | 3.29 | . 09 | $111 \%$. 6 | 3.52 | -09 |
| 1119.35 | 3.96 | . 08 | 1121.03 | 4.09 | . 08 |
| 1122.71 | 4.02 | . 08 | 1124.40 | 3.61 | . 08 |
| 1126.09 | 3.55 | . 08 | 1127.79 | 3,44 | . 08 |
| 1129.48 | 3.48 | . 08 | 1131.19 | 3.38 | ! 08 |
| 1132.89 | 3.40 | . 08 | 1134.60 | 2.94 | . 08 |
| 1136.31 | 3.26 | .08 | 1138.03 | 3,54 | . 08 |
| 1139.75 | 4.12 | . 07 | 1141.48 | 4.31 | - 0.7 |
| 1143.21 | 4.10 | . 07 | 1144.94 | 3.52 | . 08 |
| 1146.68 | 2.64 | . 08 | 1148.42 | 2.59 | . 08 |
| 1150.16 | 2.65 | . 08 | 1151.91 | 2.82 | . 08 |
| 1153.67 | 2.87 | . 08 | 1155.42 | 3.34 | .07 |
| 1157.18 | 3.53 | . 07 | 1158.95 | 3.79 | . 07 |
| 1160.72 | 3.35 | . 07 | 1164.49 | 2.97 | . 08 |
| 1164.27 | 2.79 | . 08 | 1166.05 | 2.93 | . 08 |
| 1167.84 | 3.05 | . 08 | 1169.03 | 3.72 | . 07 |
| 1171.42 | 3.61 | . 07 | 1173.c2 | 3,69 | . 07 |
| 1175.02 | 3.49 | . 07 | 1176.83 | 3.87 | . 07 |
| 1178.64 | 4,07 | . 07 | 1180.45 | 4,03 | .07 |
| 1182.27 | 3.82 | . 07 | 1184.10 | 3.63 | . 07 |
| 1185.92 | 3.16 | . 07 | 1187.76 | 3,03 | . 07 |
| 1189.59 | 2.96 | . 07 | 1191.43 | 3.15 | . 07 |
| 1193.28 | 3.31 | . 07 | 1195.13 | 3.43 | . 07 |
| 1196.98 | 3.54 | . 07 | 1198.64 | 3.60 | . 07 |
| 1200.70 | 3.06 | . 07 | 1202.57 | 3.13 | . 07 |
| 1204.44 | 3.30 | . 07 | 1206.31 | 3.46 | . 07 |
| 1208.19 | 2.98 | . 07 | 1210.08 | 2.89 | . 07 |
| 1211.97 | 2.67 | . 08 | 1213.06 | 2.64 | .07 |
| 1215.76 | 2.47 | . 08 | 1217.66 | 2.75 | . 07 |
| 1219.57 | 3.23 | . 07 | 1221.48 | 3.14 | . 07 |
| 1223.39 | 3.30 | . 07 | 1225.31 | 3.53 | . 0.7 |
| 1227.24 | 3.44 | . 37 | 1229.17 | 3.75 | . 06 |
| 1231.10 | 3.51 | . 07 | 1233.04 | 2.88 | . 07 |
| 1234.98 | 2.68 | . 12 | 1256.93 | 3.25 | . 08 |
| 1238.88 | 3,54 | . 48 | 124 U.84 | 3.00 | . 08 |

TABLE V (Contd.)

| $E_{n}, \mathrm{keV}$ | $\sigma_{T}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\mathrm{T}}, \mathrm{b}$ | $E_{n}, \mathrm{keV}$ | $\sigma_{\mathrm{T}}, \mathrm{b}$ | ${ }^{\mathrm{d}}{ }_{\mathrm{T}}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1242.80 | 3.84 | . 07 | 1244.17 | 3.95 | . 07 |
| 1246.74 | 3,97 | .07 | $1<40.71$ | 3.92 | .07 |
| 1250.69 | 3.67 | . 07 | 1252.08 | 3.65 | . 08 |
| 1254.67 | 3.34 | . 08 | $1<56.67$ | 3.02 | . 08 |
| 1258.66 | 2.71 | . 08 | 1260.67 | 2.35 | . 09 |
| 1262.68 | 2.40 | . 09 | 1264.69 | 2.05 | . 08 |
| 1266.71 | 2.68 | . 0.8 | 1268.74 | 2.64 | . 08 |
| 1270.76 | 3.17 | . 08 | 1272.80 | 3.05 | . 08 |
| 1274.84 | 3.04 | . 08 | 1270.88 | 2.73 | .08 |
| 1278.93 | 2.72 | .08 | 1280.98 | 2, 81 | . 08 |
| 1283.04 | 2.83 | . 08 | 1285.10 | 3.43 | . 08 |
| 1287.17 | 3.58 | .08 | 1289,25 | 3.40 | . 08 |
| 1291.32 | 3.32 | . 08 | 1293.41 | 3.09 | . 08 |
| 1295.50 | 3.12 | . 08 | 1291.59 | 3, 23 | . 08 |
| 1299.69 | 3.18 | . 08 | 1301.79 | 3.75 | . 07 |
| 1303.90 | 3.77 | . 07 | 1506.02 | 3.97 | . 07 |
| 1308.14 | 3.75 | .07 | 1310.26 | 3.60 | - 08 |
| 1312.39 | 3.54 | . 38 | 1314,53 | 3,52 | .08 |
| 1316.67 | 3.21 | . 08 | 1510.81 | 3.43 | . 08 |
| 1320.96 | 3.76 | . 0.7 | 1325,12 | 4.05 | . 07 |
| 1325.28 | 3.90 | . 07 | 1527.45 | 3.90 | . 07 |
| 1329.62 | 3.77 | . 07 | 1331.80 | 3.12 | . 07 |
| 1333.98 | 3.49 | . 08 | 1330.17 | 3.18 | . 08 |
| 1338.36 | 3.39 | . 08 | 1540.56 | 3.48 | . 08 |
| 1342.77 | 3.47 | .11 | 1544.98 | 3.53 | $!11$ |
| 1347.19 | 3.40 | . 07 | 1549,42 | 3.44 | 9.07 |
| 1351.64 | 3.08 | . 07 | 1553.88 | 2.96 | $\bigcirc 07$ |
| 1356.11 | 2.68 | . 07 | 1550.s6 | 2.90 | .07 |
| 1360.61 | 2.92 | .07 | 2562.86 | 2.91 | . 07 |
| 1365.12 | 3.29 | . 06 | 1567.39 | 3.23 | .07 |
| 1369.66 | 3.05 | . 47 | 1571.94 | 3.49 | . 06 |
| 1374.22 | 3.15 | .07 | 1570.51 | 2.87 | . 07 |
| 1378.80 | 2.86 | . 07 | 1581.10 | 2,68 | . 07 |
| 1383.41 | 2.90 | .07 | 1585.72 | 2.93 | . 06 |
| 1388.04 | 2.98 | .06 | 1590.36 | 5.05 | . 06 |
| 1392.69 | 3.14 | .06 | 1595.03 | 3.16 | . 06 |
| 1397.37 | 3.21 | .06 | 1599.12 | 3.50 | . 06 |
| 1402.07 | 3.45 | . 06 | 1404.43 | 3.41 | . 06 |
| 1406.80 | 3.30 | . 06 | 1409.17 | 3.44 | . 06 |
| 1411.55 | 3.16 | .06 | 1413.93 | 3.26 | .06 |
| 1416.32 | 3.00 | . 06 | 1418./1 | 3.12 | .06 |
| 1421.12 | 3.23 | . 06 | 1423.52 | 3.25 | . 06 |
| 1425.94 | 3.47 | . 05 | 1428.56 | 3.63 | . 05 |
| 1430.79 | 4, 20 | . 05 | 1433.22 | 4.15 | . 05 |
| 1435.66 | 4.05 | . 05 | 1438.10 | 4.38 | . 05 |

TABLE VI．Differential Elastic Scattering Cross Sections of Vanadium，Expressed in Format of Eq．l

| $\mathrm{E}_{\mathrm{n}}, \mathrm{keV}$ | $\sigma_{\text {el }}, \mathrm{b}$ | $\omega_{1}$ | $\mathrm{d} \omega_{1}$ | $\omega_{2}$ | $\mathrm{d} \omega_{2}$ | $\omega_{3}$ | $\mathrm{d} \omega_{3}$ | $\omega_{4}$ | $\mathrm{d} \omega_{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 326.00 | 4.720 | ． 3550 | －USOU | ． 1270 | ． 0440 | ． 0880 | ． 0550 | －． 4250 | ． 0740 |
| 329.00 | 4.750 | ． 3500 | －0S00 | .1230 | ． 0450 | ． 0870 | ． 0560 | －． 0240 | ． 0760 |
| 337.00 | 4.560 | ． 380 | $\underline{-10510}$ | ． 1420 | ． 0470 | － 0770 | ． 0580 | －．0150 | $\underline{\square} 0790$ |
| 345.00 | 4.440 | ． 3 cco | －0360 | ． 1420 | ． 0530 | $\because 0510$ | ． 0660 | －． 0040 | － 4890 |
| 347.00 | 4.360 | ． 3980 | $\underline{-10540}$ | ． 1420 | ． 0510 | $\bigcirc 0610$ | ． 0630 | ． 0000 | $\bigcirc 0850$ |
| 355．00 | 4.210 | ． 4000 | －0540 | ． 1370 | ． 0510 | ． 0230 | ． 0630 | －． 0200 | ． 0860 |
| 357．00 | 4.130 | ． 4200 | $\because 0540$ | ． 1520 | ． 0510 | ． 0230 | ．06so | －． 0040 | － 4850 |
| 365.00 | 3.970 | ． $43<0$ | －0S20 | －1700 | ． 0480 | ． 0190 | ． 0600 | ． 0010 | －0800 |
| 367.00 | 3.930 | ．4330 | －0330 | ．1＊20 | ． 0500 | －． 0020 | ． 0620 | －． 0000 | － 0830 |
| 375.00 | 3.760 | ． 4220 | $\bigcirc 0330$ | ． 1350 | ． 049 U | －． 0090 | ． 0610 | －．0250 | －0820 |
| 377.00 | 3.650 | ． 4300 | $\underline{-0 S 40}$ | ． 1700 | ． 0510 | －． 0160 | ． 0640 | －．0200 | － 4800 |
| 385.00 | 3.580 | ． 4320 | －us6u | ． 2040 | ． 0530 | ． 0040 | ． 0600 | ． $00 \pm 0$ | －0890 |
| 387．00 | 3.570 | ． 4320 | －US40 | ． 2300 | ． 0510 | ． 0070 | ．U6S0 | ．0250 | $\bigcirc 0850$ |
| 392.00 | 3.540 | ． 4280 | －0， 04 | ． 2540 | ． 0500 | －0020 | ． 0620 | ． 0240 | $\underline{9} 0840$ |
| 395.00 | 3.550 | ． 4340 | －US10 | ． 2300 | ． 0460 | ． 0150 | ． 0580 | ． 0390 | ：0770 |
| 403．00 | 3.450 | ． 44 u0 | －0290 | ． 2300 | ． 0440 | ． 0030 | ．U550 | －U3U0 | $\bigcirc 0730$ |
| 406.00 | 3.390 | ． 4380 | －US10 | ． 2740 | ． 0470 | ． 0180 | ． 4580 | ． 0340 | ． 0780 |
| 414.00 | 3.370 | ． 4250 | －0300 | ． 3130 | ． 0450 | ． 0391 | ． 0560 | －U540 | $\bigcirc 0750$ |
| 417.00 | 3.370 | ．4210 | －0310 | ． 3040 | ． 0460 | ． 0310 | ． 0570 | ． 0600 | $\bigcirc 0770$ |
| 425.00 | 3.380 | ． $40<0$ | 20280 | ． 2970 | ． 0420 | ． 0280 | .4520 | ． 0380 | ． 0710 |
| 428.00 | 3.380 | ． $41<0$ | $\underline{-0280}$ | ． 3080 | ． 0420 | ． 0400 | ． 6530 | ．05S0 | $\because 0710$ |
| 436.00 | 3.490 | ． 4140 | $\underline{-0280}$ | ． 3210 | ． 0420 | ． 0450 | ． 0520 | ． 0450 | －0710 |
| 439.00 | 3.500 | ． 4150 | $\bigcirc 0260$ | ． 3300 | ．0380 | $\because 0430$ | ． 1480 | ． 0340 | －． 0650 |
| 447.00 | 3.510 | ．4\％10 | －0250 | ． 3240 | ． 0380 | .0420 | ． 0470 | ． 0250 | .0630 |
| 455.00 | 3.580 | ．4340 | －0260 | ． 3180 | ． 0380 | ． 0410 | .0470 | ． $0<10$ | ． 06640 |
| 457.00 | 3.590 | ．4360 | $\bigcirc 0<70$ | ． 3270 | .0400 | ． 0430 | ． 0500 | ． 0190 | －0670 |
| 465.00 | 3.580 | ． 4510 | 90250 | ． 3180 | ． 0380 | ． 0330 | .0410 | － $4<10$ | $\bigcirc 0630$ |
| 467.00 | 3.610 | ．4510 | $\bigcirc 0.050$ | ． 3120 | ．0380 | ． 0320 | ． $04 \%$ | ． 0220 | －1630 |
| 475.00 | 3.540 | ．4530 | .0240 | ． 3180 | ． 0350 | ． 0380 | .0440 | ． 0120 | ． 0590 |
| 477.00 | 3.550 | ． 5000 | $\because 0240$ | ． 3170 | ． 0350 | ． 0410 | ． 0440 | ． 0250 | － 0590 |
| 485.00 | 3.450 | ．5210 | －0220 | ． 3340 | ． 0330 | .0430 | ． 0410 | ．0190 | $\underline{.0550}$ |
| 487．00 | 3.400 | ． 5410 | －0210 | ． 3280 | ． 0320 | ． 0410 | ． 0400 | ． 0200 | －0530 |
| 495.00 | 3.360 | ． 5300 | －0200 | ． 3410 | ． 0300 | ． 0360 | － 0380 | ． 0240 | $\bigcirc .0510$ |
| 497．00 | 3.320 | ．5510 | $\bigcirc 0190$ | ． 3400 | ． 0290 | .0300 | － 3300 | ． 0100 | －． 1490 |
| 505.00 | 3.250 | ．5750 | －0190 | ． 3590 | ． 0280 | －0320 | ．0350 | ． 0300 | $\bigcirc 0470$ |
| 507.00 | 3.210 | ． 5830 | －0190 | ． 3530 | ． 0290 | ． 0350 | ． 0360 | ． 0330 | .0480 |
| 515.00 | 3.17 j | ． 58.0 | $\bigcirc 0210$ | ． 4010 | ．0320 | ． 0550 | ． 0390 | ． 0550 | ． 0530 |
| 517.00 | 3．130 | ． 5510 | $\bigcirc 0<10$ | ． 4120 | ． 0310 | ． 0690 | ． 0390 | ． 0000 | －0530 |
| 525.00 | 3.050 | ． 5800 | $\underline{0} 0200$ | ． 4450 | ．0300 | ． 0730 | ． $03 \%$ | ． 0540 | －0500 |
| 527.00 | 3.040 | ． 5110 | $.0<00$ | ． 4470 | .0300 | .0710 | ． 0370 | ． 0480 | ． 0500 |

TABLE VI (Contd.)

| $E_{n} ;$ keV | $\sigma_{e l}, \mathrm{~b}$ | $\omega_{1}$ | $\mathrm{d} \omega_{1}$ | $\omega_{2}$ | $\mathrm{d} \omega_{2}$ | $\omega_{3}$ | $\mathrm{d} \omega_{3}$ | $\omega_{4}$ | $\mathrm{d} \omega_{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 532.00 | 3.000 | . 5730 | -0210 | . 4550 | . 0310 | $\bigcirc 0700$ | . 0390 | . 0400 | $\underline{0520}$ |
| 535.00 | 2.990 | . 5750 | $\underline{-2210}$ | . 4720 | . 0320 | . 0770 | . 0400 | . 0510 | . 0540 |
| 54.1.00 | 2.950 | . 5500 | -0200 | . 4350 | . 0300 | . 0930 | .03/0 | .0570. | . 0500 |
| 543.00 | 2.900 | . 5500 | .0210 | . 5010 | .0310 | .1080 | . $\cup 390$ | .0610 | . 0530 |
| 553.00 | 2.810 | .4690 | . $0<20$ | . 4970 | . 0330 | .1030 | . 0410 | . 0340 | -0550 |
| 555.00 | 2.770 | . 4480 | 90240 | . 5060 | . 0350 | .1040 | .0440 | .03c0 | -0590 |
| 565.00 | 2.810 | . 3730 | $\bigcirc 0210$ | . 5080 | . 0320 | . 1070 | . 0400 | .0300 | 90540 |
| 567.00 | 2.180 | . 3490 | .0210 | . 5090 | . 0310 | . 0970 | . 0390 | . 0140 | . 0530 |
| 577.00 | 2.370 | .3070 | .0200 | . 4920 | . 0300 | .0860 | . 0310 | . 0110 | . 0490 |
| 580.00 | 2.890 | . 2820 | $\bigcirc 0200$ | . 4.900 | . 0300 | . 0880 | . 0380 | . 0070 | $\bigcirc 0510$ |
| 589.00 | 3.000 | . 2790 | -0200 | . 4780 | . 0290 | .0970 | . 0310 | . 0130 | $\bigcirc 0490$ |
| 597.00 | 5.070 | . $29<0$ | -uくu0 | . 4650 | . 0300 | . 1040 | . $03 \% 0$ | . 0180 | . 0500 |
| 605.00 | 3.070 | . 3130 | $\bigcirc 0200$ | . 4540 | . 0300 | . 0810 | . $03 \%$ | . 0170 | .0490 |
| 607.00 | 3.110 | . 3260 | $\underline{-10190}$ | . 4530 | . 0290 | . 0870 | -6360 | . U2s0 | -0490 |
| 615.00 | 3.140 | . 3410 | -0190 | . 4160 | . 0280 | . 0590 | . 0350 | . 0240 | $\underline{-0470}$ |
| 617.00 | 3.150 | . 3590 | 00190 | . 4730 | . 0290 | $\bigcirc 0530$ | . 0360 | . 0160 | .0480 |
| 625.00 | 3.150 | . 3590 | . 0180 | . 4930 | . 0280 | . 0350 | . 0350 | . 0150 | .0470 |
| 627.00 | 3.120 | . 370 | $\underline{0} 0180$ | . 4330 | . 0270 | -.0330 | . 0340 | .0080 | .0450 |
| 635.00 | 3.200 | . 3610 | -0180 | . 4720 | . 0270 | $\because 0330$ | . U350 | .0150 | -0450 |
| 637.00 | 3.190 | . 3620 | 00180 | . 4760 | . 0260 | . 0210 | .03S0 | .0050 | $\bigcirc 0440$ |
| 645.00 | 3.240 | . 3470 | $\bigcirc 0180$ | . 5140 | . 0250 | . 0320 | -0300 | . 0200 | .0440 |
| 647.00 | 3.240 | .3360 | . 0160 | . 5180 | . 0240 | . 0240 | . 0300 | .0150 | $\bigcirc 0410$ |
| 655.00 | 3.270 | .3120 | .0160 | . 5370 | . 0240 | . 0440 | . 0290 | .0S10 | $\bigcirc 0400$ |
| 657.00 | 3.310 | . 3040 | . 0150 | . 5430 | . 0230 | . 0510 | . 4290 | . 0300 | . 0390 |
| 665.00 | 3.340 | . 3020 | $\underline{0160}$ | . 5500 | . 0240 | . 0510 | . 0300 | . 0300 | . 0410 |
| 667.00 | 3.350 | .3010 | $\underline{0150}$ | . 5520 | . 0220 | . 0610 | . 0280 | . 0200 | $\bigcirc 0380$ |
| 675.00 | 3.370 | . 3010 | . 0160 | . 5400 | . 0240 | . 0780 | . 0360 | . 0250 | $\bigcirc 0410$ |
| 677.00 | 3.400 | . 30.90 | .0170. | . 5480 | . 0260 | . 0940 | . 0320 | - USく0 | $\bigcirc 0440$ |
| 685.00 | 3.450 | .3300 | 20180 | . 5320 | .0280 | . 1040 | . 0340 | . 0320 | . 0470 |
| 687.00 | 3.420 | .3450 | 0.0190 | . 5330 | . 0280 | . 1160 | . 0350 | . 0300 | $\bigcirc 0470$ |
| 695.00 | 3.430 | . 3600 | .0180 | . 5230 | . 0270 | .1130 | . 0340 | -02<0 | . 04450 |
| 697.00 | 3.410 | . 3710 | .0190 | . 5160 | . 0280 | .1150 | . U350 | . 0180 | $\bigcirc 0470$ |
| 705.00 | 3.430 | . 3960 | -0180 | . 5090 | . 0280 | .1070 | . 0340 | -.0010 | $\bigcirc 0470$ |
| 707.00 | 3.430 | .4030 | $\bigcirc 0190$ | . 5010 | . 0290 | -1010 | . 0360 | -. 0220 | $\bigcirc 0480$ |
| 715.00 | 3.440 | .4350 | $\bigcirc 0200$ | . 5120 | .0300 | . 0900 | . 0370 | -. 0200 | -0500 |
| 717.00 | 3.450 | . 4490 | -020 | . 5000 | . 0300 | . 0960 | . 0380 | -.0270 | $\bigcirc 0510$ |
| 725.00 | 3.400 | . 4850 | $\bigcirc 0220$ | . 5170 | - 0.320 | . 1010 | .0410 | -. 0020 | $\bigcirc 0540$ |
| 727.00 | 3.410 . | . 5030 | $\bigcirc 0220$ | . 5200 | . 0330 | .1020 | . 0410 | -. 0070 | $\bigcirc 0550$ |
| 735.00 | 3.300 | . 5390 | $\bigcirc 0240$ | . 5570 | . 0360 | .1000 | .0450 | . 0090 | $\underline{-} 0610$ |
| 737.00 | 3.260 | .5350 | -0240 | . 5750 | . 0350 | . 1000 | . 0440 | . 0090 | -0590 |
| 745.00 | 3.080 | . 5530 | $\underline{.0270}$ | . 5970 | . 0400 | -0820 | - 6500 | -.uUso | . $0670^{\circ}$ |
| 747.00 | 3.030 | . 5650 | $\underline{-0280}$ | . 6150 | . 0420 | -0850 | -6520 | . $00<0$ | . 0700 |
| 755.00 | 2.940 | . 5430 | .0260 | . 6370 | . 0380 | $\bigcirc 0730$ | . 4480 | .0060 | : 0640 |


| $0990 \%$ | $0 ヶ 2 \%$ | $05 \rightarrow 0^{\circ}$ | $0560^{\circ}$ | $0690^{\circ}$ | $0<78^{\circ}$ | $0970{ }^{\circ}$ | O75 5 ． | 08＊ $7^{\circ}$ ¢ | 00．SE6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0590^{\circ}$ | OT0ち． | 0860. | $0280^{\circ}$ | $0650^{\circ}$ | 0 ¢GL | $0970^{\circ}$ | $0+5 \varepsilon^{\circ}$ | 097 $0^{\circ}$ | 00＊L26 |
| $0990^{\circ}$ | OOOT | O6も？ | $0260^{\circ}$ | $0060{ }^{\circ}$ | OOEL． | $0970{ }^{-1}$ | 0 SSS． | $009^{\circ} \mathrm{E}$ | $00 \cdot 526$ |
| $0650{ }^{\circ}$ | $0810^{\circ}$ | $0 \rightarrow 60^{\circ}$ | $0090^{\circ}$ | $0 \leq 500^{\circ}$ | $009<^{\circ}$ | ns？ 0 | $0 \subset 8 己^{\circ}$ | Oヵ＊ 2 | $00^{\circ} \angle 56$ |
| $0590^{\circ}$ | $08.50^{\circ}$ | O6カロ＊ | $0 \forall 50{ }^{\circ}$ | ก6¢0＊ | $0 \leq ¢ C^{\circ}$ | 097\％ | $0 ヶ 92 *$ | $080^{\circ} \mathrm{S}$ | 00．5T6 |
| $00<0^{\circ}$ | $00.60^{\circ}$ | 0 ¢G！ | $0890^{\circ}$ | $0260^{\circ}$ | $08 \mathrm{C}{ }^{\circ}$ | $0970^{\circ}$ | $0 \div 52^{\circ}$ | $06 \varepsilon^{\circ} \mathrm{E}$ | $00^{\circ} \angle 06$ |
| $0 \angle 90^{\circ}$ | $0050^{\circ}$ | 0050 | $0860 \%$ | $00 \rightarrow 0{ }^{\circ}$ | $086 L^{\circ}$ | $0 \angle 20^{\circ}$ | $0>02^{\circ}$ | $065^{\circ} \mathrm{S}$ | $00^{\circ} 506$ |
| $0 E 10^{\circ}$ | $0>50^{\circ}$ | 0650. | $0690^{\circ}$ | O¢ $\square^{\circ}$ | 0 CCL | $0670^{\circ}$ | 0017 | 09？${ }^{\circ}$ | 00\％ 168 |
| $0 G \angle 0^{\circ}$ | $05.90^{\circ}$ | 0950. | $0990 \%$ | $0 ¢ \bigcirc 0^{\circ}$ | 0296 | $0050{ }^{\circ}$ | OR91＇ | 06？ $0^{\circ}$ | $00^{\circ} 968$ |
| $0 ¢ \angle 0^{\circ}$ | $0290^{\circ}$ | $0 ヶ G 0^{\circ}$ | 0080 ． | ロャカロ＊ | $068 L^{\circ}$ | $0670^{\circ}$ | On91． | $025^{\circ} \mathrm{S}$ | $00^{\circ} \angle 88$ |
| $0 \rightarrow<0^{\circ}$ | $0 ¢ 10^{\circ}$ | $0 G S 0^{\circ}$ | $0860{ }^{\circ}$ | $0 S \pm 0^{\circ}$ | 0 TEL＇ | $0050 \%$ | O1LI＇ | $0 \angle 0^{\circ} \mathrm{E}$ | $00^{\circ} 588$ |
| $0920^{\circ}$ | $0290^{\circ}$ | 0950. | OET\％ | $0 S \rightarrow 0$. | 0 OEL． | $0050{ }^{\circ}$ | OT． 6 I＇ | $0 \rightarrow 0{ }^{\circ} \mathrm{F}$ | $00^{\circ} \mathrm{E} 88$ |
| $0 \varepsilon \angle 0^{\circ}$ | $0 \rightarrow 80^{\circ}$ | $0 \rightarrow 50$ | OTIT． | $0 \rightarrow$ ロ＊ | OLE ${ }^{\circ}$ | 067.0 － | $0 \mathrm{OST} \mathrm{S}^{\circ}$ | $020{ }^{\circ} \mathrm{E}$ | 00．188 |
| $00<0 \%$ | $001.0^{\circ}$ | $07.50^{\circ}$ | 06TI： | $02 \rightarrow 0$－ | $0508^{\circ}$ | $0970 \%$ | 018 C | $066^{\circ} \mathrm{C}$ | $00^{\circ}+\angle 8$ |
| $0 \angle 90^{\circ}$ | $0 ¢ 90^{\circ}$ | $0050^{\circ}$ | 0こで。 | $0060{ }^{\circ}$ | $06 L^{\circ}$ | $0170^{\circ}$ | 0 OSI | O65＊ | $00^{\circ} \mathrm{Cl}$ く |
| $0690^{\circ}$ | $0 ¢ 90^{\circ}$ | 0 TS0． | 0こてた。 | 0 切0． | $08 \in L^{\circ}$ | 0870 － | O¢B．L | $0 \rightarrow 6^{\circ}$ ？ | 00＇LC8 |
| $0220^{\circ}$ | $05<0^{\circ}$ | 0 Sci． | 06ちち＂ | $0 \mathrm{E} \rightarrow 0^{\circ}$ | $0008^{\circ}$ | O67．0： | ORGI＇ | $099^{\circ}$ 2 | 00＇598 |
| $020^{\circ}$ | $08<0^{\circ}$ | 0 OSn＊ | OEST． | $0 \varepsilon \rightarrow 0$＊ | $0208^{\circ}$ | $067.0^{\circ}$ | $0<0 Z^{\circ}$ | $058^{\circ} 2$ | 00＇ 298 |
| 0 Tく0\％ | $0 \bigcirc 80^{\circ}$ | $0250^{\circ}$ | 086ち． | 0 ¢b0＊ | $0608^{\circ}$ | $0670^{\circ}$ | 0 ので | 0 080 | 00＇I98 |
| $01 \angle 0^{\circ}$ | $0880^{\circ}$ | $0250{ }^{\circ}$ | OZST： | $0260^{\circ}$ | $01.08^{\circ}$ | $0870^{\circ}$ |  | 0 ¢ $8^{\circ}$ ？ | $00 \cdot 098$ |
| $0890^{\circ}$ | $0 \angle 60^{\circ}$ | $0050{ }^{\circ}$ | 0ع91\％ | 切加 | $0 \rightarrow 08^{\circ}$ | $0170^{\circ}$ | 0 こちで。 | OSI？ | $00 \cdot 5 ¢ 8$ |
| $0990^{\circ}$ | $0 ¢ 60^{\circ}$ | 0 ロッワ | $0 \vee 9 \%$ | $00 \rightarrow 0$. | $06 \in L^{\circ}$ | $01700^{\circ}$ | $00+2$ | $0 \rightarrow L^{\circ}$ ？ | $00 \cdot \varepsilon ¢ 8$ |
| $0 \angle 90^{\circ}$ | $0 \times 60^{\circ}$ | 0 OSn＊ | 0595： | $0060^{\circ}$ | $0208^{\circ}$ | $0120{ }^{\circ}$ | OGGて＇ | 吅く？ | $00^{\circ} \mathrm{CG} 9$ |
| $0990{ }^{\circ}$ | $07.60^{\circ}$ | 0660. | OE9 \％ | $0060^{\circ}$ | O8E ${ }^{\circ}$ | $017.0^{\circ}$ | $009{ }^{\circ}$ | OEL＇こ | 00＇L59 |
| $0990^{\circ}$ | $0460^{\circ}$ | 0860. | OLくで＊ | $06500^{\circ}$ | 068 ${ }^{\circ}$ | $09700^{\circ}$ | 0 O．3 ${ }^{\circ}$ | $001{ }^{\circ} \mathrm{C}$ | 00．968 |
| $0590^{\circ}$ | $0560^{\circ}$ | $0960^{\circ}$ | $089 \%$ | $0650^{\circ}$ | 0／EL＇ | $0970^{\circ}$ | 09 CL | 0こぐ？ | $00^{\circ} \downarrow \downarrow 8$ |
| $0 ¢ 90^{\circ}$ | $0980^{\circ}$ | $0960{ }^{\circ}$ | $0 \angle 9 \%^{\circ}$ | $0850^{\circ}$ | 0¢ $1 L^{\circ}$ | $0 ¢ 70^{\circ}$ | $090{ }^{\circ}$ | 0 O1．2 | 00＇0b8 |
| Oع90＊ | $0780^{\circ}$ | $0<60$ | 059T＊ | $0850^{\circ}$ | $0 \leq 1 L^{\circ}$ | $0 \subseteq 70^{\circ}$ | OGOE＇ | 0てじ？ | 00＇8を8 |
| $0290^{\circ}$ | $0 \angle 90^{\circ}$ | 0 Cb0． | Oヤちら： | $0 \angle 50^{\circ}$ | $009 L^{\circ}$ | $0 S ? 0^{\circ}$ | OnOE | $0 \varepsilon \ll$ | O0＇0¢8 |
| $0290^{\circ}$ | $0 \cap<0^{\circ}$ | $0960^{\circ}$ | 06ET＊ | $0 \angle E 0^{\circ}$ | $0<6 L^{\circ}$ | $0 \subseteq 70^{\circ}$ | OTOE | 0こし＇こ | 00．828 |
| $0290^{\circ}$ | $0 \rightarrow 10^{\circ}$ | 0960. | OटET： | $0 \angle S 0^{\circ}$ | 0Sbl | 0 OPO： | O6TE． | $099^{\circ} 2$ | 00＇228 |
| $05.90^{\circ}$ | $0690^{\circ}$ | $0960^{\circ}$ | OOE 5＊ | $0 \angle 50^{\circ}$ | 0S¢ $L^{\circ}$ | $0570^{\circ}$ | 09？${ }^{\text {O }}$ | $0<9^{\circ} 2$ | 00．028 |
| $0 \angle 50^{\circ}$ | $09+0^{\circ}$ | $0560^{\circ}$ | $0 \angle 0 \%$ ． | $0 \rightarrow$ ¢0： | $080 L^{\circ}$ | 0 ¢ ？0\％ | $00 ¢ 8$. | $0<9^{\circ} \mathrm{C}$ | 00．058 |
| $0950{ }^{\circ}$ | 0650. | $0260^{\circ}$ | 0007. | OESO： | 0051 | $0270^{\circ}$ | $07.5 \varepsilon^{\circ}$ | $0 \angle 9^{\circ} \mathrm{C}$ | $00^{\circ} 808$ |
| $0990{ }^{\circ}$ | 0 C20． | 0660 | $0080^{\circ}$ | $00 \rightarrow 0^{\circ}$ | $000{ }^{\circ}$ | $0 \angle 20^{\circ}$ | $0>7.9$－ | $059^{\circ} \mathrm{Z}$ | 00\％ 162 |
| $0290^{\circ}$ | $0 \mathrm{OE} 0^{\circ}$ | $0960^{\circ}$ | $00 \angle 0{ }^{\circ}$ | $0 \angle 50^{\circ}$ | $0869^{\circ}$ | $0 ¢ 7.0{ }^{\circ}$ | $08 \angle 8{ }^{\circ}$ | 069 $069^{\circ}$ | 00.562 |
| $0290^{\circ}$ | $06.20^{\circ}$ | $0960^{\circ}$ | $0090{ }^{\circ}$ | $0 \angle 80^{\circ}$ | $090<^{\circ}$ | 0 O20＇ | 0ロで。 | $065^{\circ} 2$ | $00 \%$ 0068 |
| $05900^{\circ}$ | $0620^{\circ}$ | $06+0^{\circ}$ | $0<90^{\circ}$ | 0680＇ | 0 O02＊ | $0920^{\circ}$ | Oヶら女。 | $079{ }^{\circ}$ | $00^{\circ} \mathrm{G} 8 \mathrm{~L}$ |
| $0990 \%$ | $0+50^{\circ}$ | $0600{ }^{\circ}$ | $0590^{\circ}$ | $0060^{\circ}$ | 0¢69 | $0 \angle 70^{\circ}$ | $0 \geqslant 86^{\circ}$ | 019 0 0.7 | OO． 016 |
| $0590^{\circ}$ | $0950^{\circ}$ | $0650{ }^{\circ}$ | $0890 \%$ | 0680. | 0 ¢ \％${ }^{\circ}$ | $0920^{\circ}$ | $0566^{\circ}$ | $0<9{ }^{\circ}$ | $00 \cdot 96$ |
| O¢90＊ | $0520^{\circ}$ | $01.60^{\circ}$ | $0 \vdash \angle 0 \%$ | $0850{ }^{\circ}$ | ก959＊＊ | 057．0 | $0765^{\circ}$ | 012．2 | 00．29L |
| $0590^{\circ}$ | $0 ¢ T 0^{\circ}$ | $0860{ }^{\circ}$ | $05 \angle 0^{\circ}$ | $0650^{\circ}$ | $0 \tau \subseteq 9^{\circ}$ | $0970^{\circ}$ | $0 \rightarrow 5 c^{\circ}$ | 008＇ | 00＇s9l |
| $0890^{\circ}$ | OTT0＊ | $0050{ }^{\circ}$ | 0 L20． | $0060{ }^{\circ}$ | $0069^{\circ}$ | $0 \angle 70^{\circ}$ | 0 TCS | $0<8{ }^{\circ}$ | $00 \cdot 251$ |
| $\square$ ®p | ${ }^{*}$（ | $\varepsilon_{m p}$ | ${ }^{\varepsilon}{ }_{\square}$ | ${ }^{2} \times p$ | 2 m | $I_{\text {mp }}$ | $\mathbf{I}_{6}$ | $q \cdot{ }^{\prime}{ }_{0}$ |  |

TABLE IV（Contd．）

| $E_{n}$, keV | $\sigma_{e l}, \mathrm{~b}$ | $\omega_{1}$ | $d \omega_{1}$ | $\omega_{2}$ | $\mathrm{d} \omega_{2}$ | $\omega_{3}$ | $\mathrm{d} \omega_{3}$ | $\omega_{4}$ | $\mathrm{d} \omega_{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 937.00 | 3.460 | .3800 | ． 0250 | ． 8230 | ． 0380 | ． 0940 | ． 0470 | .1230 | ． 0640 |
| 945.00 | 3.380 | ． 4560 | $\because 0280$ | ． 8550 | .0410 | ． 0880 | ． 0510 | .1030 | －0690 |
| 947.00 | 3.360 | ． 4320 | $\bigcirc 0<60$ | ． 8520 | .0400 | ． 0930 | ． 0490 | .1090 | $\bigcirc 0600$ |
| 955.00 | 3.310 | ． 4600 | －US20 | ． 8770 | ． 0470 | $\bigcirc 0950$ | ． 0590 | .1320 | $\bigcirc$ |
| 957.00 | 3.300 | $.47 \% 0$ | －10320 | .8970 | ． 0490 | －1090 | .0600 | .1400 | .0810 |
| 965.00 | 3.230 | .5000 | － 0360 | ． 9240 | ． 0540 | .1160 | ． $06 \%$ | .1390 | $\bigcirc 0900$ |
| 967.00 | 3.200 | ． 50.50 | －03\％ | ． 9230 | .0560 | .1190 | ． 4690 | ．1350 | $\because 0930$ |
| 975.00 | 3.120 | ． 5200 | $\because 0380$ | ． 9540 | .0560 | .1210 | ． 0690 | ． 1270 | $\bigcirc 0930$ |
| 977.00 | 3.090 | ． 5230 | －03\％ | ． 9580 | ． 0550 | .1240 | ． 4680 | .1180 | ． 0910 |
| 985.00 | 3.040 | ． 5500 | －uSちu | ． 9520 | ． 0520 | .1360 | ． 0650 | .1190 | $\bigcirc 0870$ |
| 987.00 | 3.010 | ． 5540 | －US60 | ． 9320 | ． 0540 | .1390 | ． 0670 | .1080 | ． 0900 |
| 995.00 | 3.010 | ．ううく0 | －US\％ | ．9770 | ． 0550 | ． 1710 | .0680 | .1120 | ． 0920 |
| 997.00 | 3.000 | －5ラン0 | －US／0 | 1.0070 | .0550 | .1920 | .0680 | .1200 | $\bigcirc .0910$ |
| 1005.00 | 3.040 | ． 56.50 | －USOO | ．9980 | .0540 | .2060 | ． 0670 | .1200 | .0910 |
| 1007.00 | 3.020 | .5600 | －0350 | ． 9740 | ． 0520 | .2130 | ．0650 | .1100 | ． 0870 |
| 1015.00 | 2.960 | ． 5940 | ：US7U | 1.0190 | ． 0550 | .2360 | ． 0680 | .1000 | ． 0920 |
| 1017.00 | 2.930 | ． $59 \times 0$ | ！us | 1.0170 | ． 0570 | ． 2460 | ． 0700 | .1060 | ． 0940 |
| 1025.00 | 2.880 | ． 5900 | $\because 0500$ | 1．0360 | .0540 | ． 2610 | ． $06 / 0$ | .1060 | $\bigcirc .0900$ |
| 1027.00 | 2.860 | .5900 | －0360 | 1.0380 | .0530 | ． 2770 | ． 4660 | .1130 | .0890 |
| 1035.00 | 2.800 | ．5950 | $\because 0550$ | 1.0390 | ． 05.20 | $\because 2800$ | －U6ち0 | .1120 | $\bigcirc 0870$ |
| 1037.00 | 2.790 | ． 58.0 | －U350 | 1.0410 | ． 0530 | .2840 | ． 4660 | .1080 | －0880 |
| 1042.00 | 2.740 | ． 5910 | －US／0 | 1.0460 | ． 0550 | .2920 | ． 4680 | .1170 | .0920 |
| 1045.00 | 2.710 | ． $58<0$ | －0sl0 | 1.0210 | ． 0550 | .2830 | ． 0690 | .1090 | ． 09930 |
| 1053.00 | 2.650 | ． 5450 | ！ 4380 | 1.0410 | ． 0570 | ． 2940 | － 0710 | .1210 | .0950 |
| 1056.00 | 2.610 | ． 5200 | $\because 0580$ | 1.0430 | ． 0570 | ． 2810 | ． 0700 | .1270 | $\bigcirc .0950$ |
| 1064.00 | 2.530 | .4800 | $\bigcirc 0440$ | 1.0280 | .0650 | $\because 2690$ | ． 4810 | ． 0980 | $\because 1090$ |
| 1067.00 | 2.500 | ． 4200 | $\bigcirc 0400$ | 1.0170 | ． 0590 | $\therefore 2580$ | － 4750 | ． 0910 | $\bigcirc$ |
| 1073.00 | 2．510 | ． 41 ¢0 | $\bigcirc 0420$ | 1.0000 | ． 0620 | $\because 2570$ | ． 1770 | .1210 | $\because 1040$ |
| 1075.00 | 2.520 | .3800 | ：0410 | ． 9920 | ． 0610 | ． 2520 | ． 0760 | .1190 | $-1030$ |
| 1084.00 | 2.540 | ． 3640 | $\because 0400$ | ． 9740 | ． 0600 | .2170 | ． 0740 | .1200 | $\bigcirc 1000$ |
| 1086.00 | 2.550 | ． 3400 | $\bigcirc 0430$ | ． 9310 | ． 0640 | ． 2170 | .0790 | .1160 | $\because 1070$ |
| 1095.00 | 2.630 | ． 3040 | $\because 0430$ | 1.0000 | ． 0640 | .1890 | ． 0790 | .1200 | ． 1060 |
| 1103.00 | 2.730 | ． 2940 | $\bigcirc 0450$ | 1.0110 | ． 0670 | .1600 | ． 4830 | .1020 | $\because 1110$ |
| 1105.00 | 2.720 | ． 2980 | $\underline{.0460 ~}$ | 1.0170 | ． 0680 | ． 1550 | ． 0850 | .1010 | $\because 1140$ |
| 1113.00 | 2.840 | ． 31110 | －． 0440 | 1.0190 | ． 0650 | .1500 | ． 4810 | .1010 | $\because 1090$ |
| 1115.00 | 2.860 | $.31<0$ | $\because 0400$ | 1.0310 | ． 0600 | .1770 | ． 0740 | .1140 | －1000 |
| 1121.00 | 2．980 | －3＜00 | －0410 | $1.0220^{\circ}$ | ． 0610 | .1640 | ． 0760 | .1500 | $\because 1020$ |
| 1124.00 | 3.020 | ． 3410 | －uS90 | 1.0510 | ． 0580 | .1600 | － 4720 | .1340 | $\because 0970$ |
| 1133.00 | 3.060 | ． 3410 | －0400 | 1.0410 | ． 0590 | $\because 1800$ | ． 4730 | .1320 | －0980 |
| 1135.00 | 3.120 | ． 3600 | $\bigcirc 0410$ | 1.0360 | ． 0610 | .1860 | ． 0760 | .1390 | $\because 1010$ |
| 1144.00 | 3.150 | ． 3940 | － 0590 | 1.0510 | .0570 | .2400 | ． 0710 | .1020 | $\bigcirc 0960$ |
| 1147.00 | 3.170 | $.42<0$ | $\because 4400$ | 1.0550 | .0600 | ． 2570 | ． 0750 | .1720 | $\because 1000$ |
| 1156.00 | 3.1 .40 | ． 4360 | －US70 | 1.0400 | .0550 | .2960 | ． 1680 | ． 2120 | $\bigcirc 0920$ |

TABLE VI (Contd.)

| $E_{n}$, keV | $\sigma_{\text {el }}, \mathrm{b}$ | $\omega_{1}$ | $d \omega_{1}$ | $\omega_{2}$ | $\mathrm{d} \omega_{2}$ | $\omega_{3}$ | $d \omega_{3}$ | $\omega_{4}$ | $\mathrm{d} \omega_{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1159.00 | 3.160 | .4620 | !0S80 | 1.0340 | . 0560 | - 3140 | . 0690 | .2110 | -0930 |
| 1165.00 | 3.17 C | .4540 | $\bigcirc 0590$ | 1.0220 | . 0590 | . 3350 | . 0720 | .1990 | -0980 |
| 1176.00 | 3.180 | .4ち50 | - U420 | 1.0520 | .0630 | $\bigcirc 3240$ | - 4770 | . 2110 | -1040 |
| 1179.00 | 3.160 | . 4650 | $\bigcirc 0410$ | 1.0450 | . 0610 | $\bigcirc 3310$ | . 0760 | .2010 | -1010 |
| 1187.00 | 3.200 | . 4310 | $\underline{0} 050$ | 1.0580 | . 0570 | - 3490 | . 0700 | . 2000 | $\bigcirc 0940$ |
| 1190.00 | 3.190 | .4440 | $\because 0410$ | 1.0700 | .0620 | $\because 3550$ | . 0760 | . 2030 | .1020 |
| 1197.00 | 3.170 | .3750 | $\bigcirc 0430$ | 1.0710 | .0640 | -3270 | .0 .0790 | .1790 | .1070 |
| 1207.00 | 3.210 | . 3810 | $\bigcirc 0400$ | 1.0390 | .0610 | . 31.80 | .0740 | .1900 | $\bigcirc 1000$ |
| 1209.00 | 3.220 | .3810 | $\underline{9} 0410$ | 1.0960 | .0620 | $\bigcirc 3080$ | .0700 | . 1830 | $\because 1020$ |
| 1214.00 | 3.200 | .3930 | 0490 | 1.1030 | .0730 | .3040 | .0900 | .1670 | $\bigcirc 1210$ |
| 1216.00 | 3.180 | .3890 | $\therefore \cup 490$ | 1.1180 | . 0730 | $\bigcirc 2880$ | . 0900 | .1680 | -1210 |
| 1224.00 | 3.180 | .3860 | $\because 0460$ | 1.1140 | .0690 | . 2780 | -0850 | . 1860 | .1140 |
| 1226.00 | 3.280 | . 3490 | 0.0480 | 1.1140 | .0720 | $\because .2930$ | - 0890 | .1860 | .1200 |
| 1234.00 | 3.150 | . 3710 | -U440 | 1.1090 | .0650 | $\therefore 2610$ | . 0800 | .1810 | -1090 |
| 1236.00 | 3.120 | . 3940 | $\because 1440$ | 1.1080 | .0650 | .2570 | - 0810 | .1910 | .1090 |
| $12,44.00$ | 3.130 | .3730 | $\bigcirc 0430$ | 1.1170 | . 06640 | .2430 | . 0790 | . 2010 | $\therefore 1060$ |
| 1246.00 | 3.140 | .3900 | $\bigcirc 0450$ | 1.12 .90 | .0670 | .2340 | - 0820 | .1980 | $\because 1110$ |
| 1254.00 | 3.210 | .3650 | $\because 0430$ | 1.1310 | .0640 | .2310 | . 0780 | .2010 | .1060 |
| 1256.00 | 3.180 | .3700 | -0440 | 1.1430 | . 0660 | - 2280 | . 0810 | . 2060 | .1100 |
| 1259.00 | 3.180 | . 3800 | $\bigcirc 0450$ | 1.1480 | . 0670 | . 2240 | . 0820 | . 2120 | $\because 1110$ |
| 1267.00 | 3.190 | . 3590 | $\bigcirc 0440$ | 1.1540 | .0660 | .2190 | . 0810 | .2010 | .1100 |
| 1272.00 | 3.190 | $.33<0$ | -0550 | 1.1510 | . 0530 | . 2280 | . 0640 | . 2000 | $\bigcirc 0880$ |
| 1275.00 | 3.200 | . 3010 | $\bigcirc 0550$ | 1.1560 | . 0520 | -2260 | . 0640 | .1980 | $-0870$ |
| 1283.00 | 3.150 | .3400 | -0340 | 1.1530 | . 0520 | -2640 | . 0630 | .1980 | -0870 |
| 1286.00 | 3.120 | .3500 | $\because 0550$ | 1.1310 | .0530 | .2580 | . 0640 | .1700 | -0880 |
| 1292.00 | 3.160 | .3410 | :0380 | 1.1570 | . 0560 | . 2670 | . 0690 | . 1760 | -0940 |
| 1294.00 | 3.240 | .3610 | -0580 | 1.1950 | . 0570 | . 2600 | . 0700 | .1660 | -0970 |
| 1301.00 | 3.160 | .3650 | $\bigcirc 0390$ | 1.1900 | . 0590 | -2540 | . 0720 | .1620 | -0990 |
| 1303.00 | 3.080 | .3840 | . 0380 | 1.1940 | . 0570 | - 2650 | - 0700 | . 1570 | $\bigcirc 0970$ |
| 1307.00 | 3.050 | .4170 | $\because 0390$ | 1.1370 | . 0580 | . 2760 | . 0710 | . 1760 | -0980 |
| 1310.00 | 3.000 | . $4<8<0$ | $\bigcirc 0400$ | 1.1530 | .0600 | . 2540 | . 0740 | . 1490 | -1010 |
| 1320.00 | 3.060 | . 4450 | $\bigcirc 0410$ | 1.1750 | . 0610 | - 2850 | . 0750 | . 1920 | -1030 |
| 1330.00 | 3.080 | . 4600 | $\bigcirc 0430$ | 1.1850 | . 0650 | . 3000 | -0790 | -2200 | $\bigcirc 1090$ |
| 1334.00 | 3.110 | .4260 | $\bigcirc 0480$ | 1.1960 | .0710 | -2520 | - 0870 | . 2010 | -1190 |
| 1350.00 | 3.150 | .4400 | $\bigcirc 0420$ | 1.1780 | . 0630 | - 2480 | . 0770 | . 1920 | $-1060$ |
| 1360.00 | 3.190 | . 4810 | $\because 0420$ | 1.1270 | . 0630 | . 3160 | . 0770 | . 1880 | .1060 |
| 1376.00 | 3.200 | .4880 | $\bigcirc 0470$ | 1.1130 | . 0710 | -3120 | . 1860 | . 1640 | -1180 |
| 1386.00 | 3.150 | . 4950 | $\bigcirc 0550$ | 1.1080 | . 0820 | -3500 | . 1000 | . 1790 | -1380 |
| 1393.00 | 3.230 | . 4910 | - U 570 | 1.1040 | . 0850 | . 3570 | . 1040 | .1580 | -1420 |
| 1396.00 | 3.270 | .4890 | -0620 | 1.1160 | . 0920 | - 3520 | -1120 | .1660 | -1540 |
| 1406.00 | 3.240 | . 4940 |  | 1.1020 | . 0860 | -3700 | . 1050 | . 1580 | -1450 |
| 1413.00 | 3.270 | . 5240 | - U560 | 1.1130 | . 0840 | -3530 | .1020 | . 1610 | -1400 |
| 1416.00 | 3.280 | .5390 | .0570 | 1.1270 | .0860 | . 3840 | .1050 | . 2030 | .1440 |

TABLE VI (Contd.)

| $E_{n}$, keV | $\sigma_{\text {el }}, \mathrm{b}$ | $\omega_{1}$ | $\mathrm{d} \omega_{1}$ | $\omega_{2}$ | $\mathrm{d} \omega_{2}$ | $\omega_{3}$ | $\mathrm{d} \omega_{3}$ | $\omega_{4}$ | $\mathrm{d} \omega_{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1426.00 | 3.260 | . 5040 | . 0510 | 1.1310 | . 0770 | . 3650 | . 0940 | . 1920 | . 1290 |
| 1433.00 | 3.270 | . 5290 | -0520 | 1.1330 | . 0780 | . 4110 | . 0950 | . 2130 | $\because 1300$ |
| 1436.00 | 3.270 | . 5450 | $\underline{0500}$ | 1.1460 | . 0760 | .4310 | . 0920 | .2290 | -1260 |
| 1443.00 | 3.260 | . 5030 | $\bigcirc 0420$ | 1.1170 | .0630 | . 3750 | . 0760 | .2750 | $\because 1050$ |
| 1447.00 | 3.220 | . 5040 | $\underline{-10580}$ | 1.1230 | . 0570 | .3620 | . 0690 | .1940 | $\because 0950$ |
| 1450.00 | 3.190 | . 4840 | $\bigcirc 0390$ | 1.1440 | . 0590 | . 3940 | . 0720 | .2360 | $\because 0990$ |
| 1460.00 | 3.360 | .4980 | $\square 0410$ | 1.1460 | . 0610 | . 3590 | . 0740 | . 2000 | -1020 |
| 1464.00 | 3.310 | . $43 \%$ | $\pm 0430$ | 1.1590 | . 0650 | .3660 | . 0790 | .2960 | -1080 |
| 1.467 .00 | 3.340 | .3980 | -0570 | 1.1390 | . 0550 | . 3460 | . 0680 | .3080 | $\underline{0} 0930$ |

TABLE VII．Cross Sections for the Inelastic Excitations of the $320-\mathrm{keV}$ State in Vanadium by Neutron Scattering

| $\mathrm{E}_{\mathrm{n}}, \mathrm{MeV}$ | $\sigma_{i n}, \mathrm{~b}$ | $\mathrm{d} \sigma_{\text {in }}, \mathrm{b}$ | $\mathrm{E}_{\mathrm{n}}, \mathrm{MeV}$ | $\sigma_{\text {in }}, \mathrm{b}$ | d $\sigma_{\text {in }}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ． 650 | .330 | ．0ヶ4 | ．6500 | ． 2051 | ． 0391 |
| ． 674 | ． 389 | ． 056 | ． 6775 | ． 3845 | ． 0061 |
| ． 686 | ． 406 | ．051 | ． 0453 | ． $345 \%$ | ． 0572 |
| ． 695 | ． 475 | ． 049 | ． 1050 | ． 4207 | ． 0539 |
| ． 716 | ． 383 | ． 039 | ．1239 | ． 3755 | ． $0<74$ |
| ． 727 | ． 388 | ． 032 | ． 1359 | ． 3178 | ． 0275 |
| ． 734 | ． 356 | ． $02 \%$ | ． 1366 | ． 3140 | ．0352 |
| ． 740 | ． 371 | .040 | ． 7400 | ． 4750 | － 0110 |
| ． 753 | ． 333 | ． 023 | ． 1550 | ． 3345 | ． 0251 |
| ． 756 | ． 343 | ． 029 | ． 1659 | － 3 勺20 | ． $0<48$ |
| ． 767 | ． 351 | ． 028 | ． 7759 | ． 4281 | ． 0302 |
| ． 774 | .463 | ． 035 | ． 7760 | ． 4049 | ． 0.412 |
| ． 785 | ． 480 | .037 | ． 7866 | ，4504 | ． 0403 |
| ． 794 | ． 494 | ． 058 | ． 7966 | ．5ヶう1 | ． 0481 |
| ． 804 | ． 512 | ．0ゝ9 | ． 0006 | ，4857 | ． 0434 |
| ． 813 | ． 509 | ． 045 | ． 8149 | ． 6041 | ． 0640 |
| ． 827 | ． 513 | ． 039 | ．0359 | ． 4900 | ．0332 |
| ． 834 | ． 513 | ． 038 | ． 8360 | ． $5<442$ | ． 0455 |
| ． 844 | ． 487 | ． 035 | ． 4406 | .4904 | .0403 |
| ． 854 | ． 495 | ． 036 | ． 8506 | ． 5162 | ． 0452 |
| ． 865 | .474 | ． 031 | .8674 | ． 4399 | ．0ゝ24 |
| ． 873 | ． 440 | ． $0<6$ | ． 8749 | ． 4443 | ． 0333 |
| ． 876 | ． 432 | ． 037 | ． 8849 | ． 3943 | ．0502 |
| ． 886 | ． 385 | ． 034 | ． 8949 | ． 3918 | ． 0500 |
| ． 896 | ． 408. | ．035 | ． 9049 | ． 3967 | ． $0 \leq 00$ |
| ． 906 | ． 402 | ．035 | ． 9149 | ． 3496 | ． 0262 |
| ． 916 | ． 337 | ． 029 | ． 9249 | ． 3600 | ． $0<76$ |
| ． 926 | ． 384 | ． 033 | ． 9549 | ． 4362 | ． 0328 |
| ． 936 | ． 452 | ． 039 | ． 9433 | ． 4687 | ． 0406 |
| ． 944 | ． 409 | ． 049 | ． 9566 | ．4317 | ． 0375 |
| ． 963 | ． 405 | ． 035 | ． 9649 | ． 4185 | ． 0444 |
| ． 976 | ． 372 | ．032 | ． 9849 | ． 3627 | ． 0287 |
| ． 986 | ． 392 | ．094 | ． 4899 | ． 4016 | ． 0426 |
| ． 989 | ． 415 | .062 | 1.0050 | ．3933 | ． $0<696$ |
| 1.006 | .400 | .034 | 1.0100 | ． 3451 | ． 0423 |
| 1.010 | .336 | ．0り0 | 1.0200 | ． 4433 | ． 0385 |
| 1.035 | ． 419 | ． 031 | 1.0360 | ． 4097 | ． 0356 |
| 1.043 | ． 405 | .035 | 1.0450 | ． 3820 | ． 0405 |
| 1.055 | .432 | ． 046 | 1.0650 | ． 4468 | ． 0474 |
| 1.076 | ． 428 | .037 | 1．1．450 | ． 4 ＇2＇26 | ．0517 |

## TABLE VII（Contd．）

| $\mathrm{E}_{\mathrm{n}}, \mathrm{MeV}$ | $\sigma_{\text {in }}, \mathrm{b}$ | $\mathrm{d} \sigma_{\mathrm{in}}, \mathrm{b}$ | $\mathrm{E}_{\mathrm{n}}, \mathrm{MeV}$ | $\sigma_{\text {in }}, \mathrm{b}$ | $\mathrm{d} \sigma_{\text {in }}, \mathrm{b}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1.086 | .416 | ． 056 | 1．0950 | ．4223 | ． $0<86$ |
| 1.097 | .433 | －032 | 1．1．100 | ． 44.58 | ． 0301 |
| 1.104 | ． 44 | ． 033 | 1.1060 | ． 4617 | ． 0400 |
| 1.115 | ． 485 | ． 036 | 1.1100 | ． 5064 | .0438 |
| 1.124 | ． 493 | ． 056 | 1.1200 | ． 4 ¢50 | ． 0420 |
| 1.133 | ． 510 | ． 044 | 1．ようつ0 | .5220 | ． 0556 |
| 1.145 | ． 5 勺8 | －0と9 | 1.1500 | ． 4022 | ． 0421 |
| 1.163 | ． 420 | ． 056 | 1.1650 | ． 4567 | ． 0469 |
| 1.176 | ． 389 | ．033 | 1.1030 | ． 3933 | ． $0 \leq 40$ |
| 1.185 | ． 397 | ． 042 | 1.1950 | ． 4294 | ． 0220 |
| 1.197 | ． 443 | ． 033 | 1.2040 | ． 4300 | ． $0<665$ |
| 1.205 | ． 438 | ． 029 | 1.2070 | ． 4380 | ． 0531 |
| 1.214 | ．41） | ． $0<4$ | 1.2150 | ． 4081 | ． $0<74$ |
| 1.217 | ． 407 | ． 050 | 1.2240 | ． 4275 | ． 0263 |
| 1.225 | ． 427 | ． $0<8$ | 1.2270 | ． 4461 | ． 0336 |
| 1.233 | ． 438 | ． 029 | 1.2550 | ． 4428 | ． 0334 |
| 1.236 | ． 412 | ． 035 | 1.2400 | ． 4015 | ． 0425 |
| 1.240 | .413 | ． 061 | 1.2540 | ． 4133 | ．0＜879 |
| 1.255 | .400 | ． 050 | 1.2560 | ． 4173 | ．0563 |
| 1.265 | ． 409 | ． 050 | 1.2660 | ． 3924 | ． 0341 |
| 1.274 | $.4 \%$ | ． 035 | 1.2700 | ． 4789 | ． 0423 |
| 1.283 | ． 541 | ． 047 | 1．2850 | ． 5108 | ．0547 |
| 1.296 | ． 520 | ． 045 | 1．SUつ0 | ． 4811 | ．0s23． |
| 1.307 | ． 490 | ． 0.56 | $1.31<0$ | ． 4640 | ． 0349 |
| 1.313 | .451 | ． 039 | 1．3150 | ．4056 | ． 0495 |
| 1.325 | ． 408 | ． 043 | 1.3300 | ． 3912 | ． 0586 |
| 1.353 | ． 430 | ． $0<69$ | 1． 5 S40 | ． 4259 | ．0319 |
| 1.356 | ． 424 | ． 056 | 1.9650 | ． 4256 | ． 0522 |
| 1.306 | ． 4.29 | ． 057 | 1.3700 | ． 4178 | ． 0367 |
| 1.374 | ． 367 | ． 038 | 1.3860 | ． 4403 | ． 0385 |
| 1.395 | ． 448 | ． 034 | 1.4010 | ． 4405 | ． 0306 |
| 1.395 | ． 489 | ． 046 | 1.4000 | ． 3864 | ． 0336 |
| 1.413 | ． 400 | ． 034 | 1.4150 | ． 3860 | ． 0410 |
| 1.426 | ． 399 | ．004 | 1.4530 | ． 4010 | ． 0348 |
| 1.435 | ． 382 | ． 040 | $1.44 \%$ | ． 3613 | .0291 |
| 1.453 | ． 387 | .026 | 1.4550 | ． 38.27 | ． $0<889$ |
| 1.456 | ． 369 | ． 032 | 1.4640 | ． 3931 | ． $0<697$ |
| 1.466 | ． 417 | ． 036 | 1.4730 | ． 4069 | ．0353 |
| 1.475 | ． 384 | ． 040 | 1.4860 | ． 4052 | ．0351 |
| 1.490 | ． 400 | .043 | 1．4900 | ．3950 | ． 0593 |

TABLE VIII. Cross Sections for the Inelastic Neutron Excitations of the $930-\mathrm{keV}$ State in Vanadium

| $\mathrm{E}_{\mathrm{n}}, \mathrm{MeV}$ | $\sigma_{\text {in }}, \mathrm{b}$ | $\mathrm{d} \sigma_{\text {in }}, \mathrm{b}$ |
| :--- | :--- | :--- |
| 1.250 | .094 | .057 |
| 1.300 | .0850 | .0186 |
| 1.350 | .175 | .040 |
| 1.360 | .1603 | .0693 |
| 1.400 | .145 | .021 |
| 1.4100 | .1025 | .0258 |
| 1.450 | .125 | .019 |
| 1.4650 | .1438 | .0673 |
| 1.500 | .998 | .027 |

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[^0]:    *All energies in MeV.

[^1]:    ${ }^{\mathrm{a}}$ The indicated uncertainties are lower limits, only pertaining to errors associated with the finiteenergy range of the experimental samples. ${ }^{46}$
    ${ }^{\text {b Defined by Eq. }} 10$.

[^2]:    ${ }^{\text {a }}$ Raw experimental data, resolution as per Section III.A, $\gtrsim 1 \mathrm{keV}$.
    $b_{\text {Calculated from form of Gilbert and Cameron. }}{ }^{54}$
    ${ }^{c}$ Ratio assuming exponential distribution of widths and spacings ( $k_{w}=1, k_{n}=1$ ).
    dRatio assuming only exponential spacing distribution ( $\mathrm{k}_{\mathrm{w}}=0, \mathrm{k}_{\mathrm{n}}=1$ ).

