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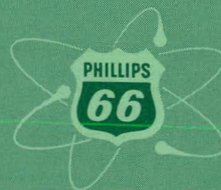
SPORT

A SYSTEM FOR PROCESSING REACTOR
TRANSIENT DATA ON THE IBM-7040 COMPUTER

B. J. Power, R. N. Hagen, and S. O. Johnson

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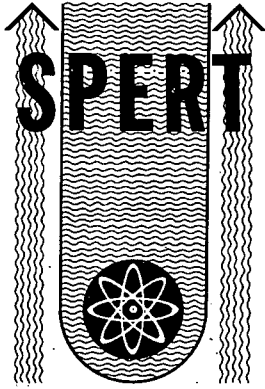
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SPORT
A SYSTEM FOR PROCESSING REACTOR
TRANSIENT DATA ON THE IBM-7040 COMPUTER

by

B. J. Power
R. N. Hagen
S. O. Johnson

PHILLIPS
PETROLEUM
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Atomic Energy Division

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ABSTRACT

To facilitate the processing and analysis of data recorded during transient tests in the Spert reactors, a system of programs for the IBM-7040 computer has been developed to (a) smooth and store data so they are readily accessible, (b) calculate from the power history the reactivity and energy release as functions of time, and (c) provide a means by which frequency response analyses of data can be made. This report describes the mathematics employed in the various programs in the system and the procedures necessary to process data with the system. Test and sample problems are presented, and a complete listing of the source program is included.

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SPORT
A SYSTEM FOR PROCESSING REACTOR
TRANSIENT DATA ON THE IBM-7040 COMPUTER

I. INTRODUCTION

SPORT (System for Processing Reactor Transient Data) is a combination of IBM-7040 computer programs which have been developed for the routine processing of transient data obtained from the Spert reactors. The system consists of three programs, SMOOTH [1], REACTIVITY [2], and FREQUENCY RESPONSE [3], originally developed for the IBM-7040 computer, and routines for the initial preparation of the raw data.

The data preparation section of SPORT contains routines to (a) normalize and shift the input data, (b) compute the natural logarithm of the data, and (c) composite data from several differently scaled channels into a single data trace.

The SMOOTH program is used to eliminate noise from the input data. The program is, in effect, an adjustable low-pass filter having a sharp cut-off characteristic. Data may be automatically recirculated through the SMOOTH program in order to achieve the desired degree of smoothing. The technique used in the program also yields the smoothed first derivative of the input data.

The REACTIVITY program is used to derive the reactivity as a function of time from the power history of a reactor. The energy release is also calculated by this program. Input data for this program must first be processed by the SMOOTH program.

The FREQUENCY RESPONSE program is used to calculate the ratio of the unilateral Fourier transforms of two input variables. This program was written primarily for the purpose of obtaining the frequency response of a linear system from the transient response of the system.

The programs contained in SPORT are normally used in sequence such that the output of one program is used as input to another. Although the programs can be used separately, SPORT normally provides for the automatic sequencing of the programs. This feature has eliminated much of the manual data handling formerly required to process transient reactor data.

This report presents descriptions of the mathematical methods used in each program in SPORT and instructions in the mechanics of processing data with the system. Section II contains a discussion of options available for initial data preparation and a description of the calculational procedure used in each of the three programs, SMOOTH, REACTIVITY, and FREQUENCY RESPONSE. Section III, a description of the input format, is presented in three subsections:

- (1) The processing options which are available to the user
- (2) The necessary control cards
- (3) The control card sequence.

Section IV contains a description of the output formats of the various programs and examples of each type of output. Section V presents some sample problems which illustrate the use of SPORT. In Section VI, problems which have been used to test various portions of the system are described. In Section VII, computer operating times are estimated. Proofs of some theorems used in Section II, listings of the source programs, a listing of a program to prepare data for input to SPORT, and a listing of a program to read a binary tape produced with SMOOTH are contained in the appendixes.

II. PROGRAM LOGIC AND MATHEMATICS

1. DATA PREPARATION

Due to the nature of data which may be processed by SPORT and the various processes which may be applied to data, it is necessary to provide a means for initial data preparation. Data preparation is accomplished before entering the major programs (SMOOTH, REACTIVITY, and FREQUENCY RESPONSE) and may be considered in three phases: (a) normalization and shifting of data, (b) compositing data recorded from several channels into one data trace, and (c) calculation of the natural logarithm of the data.

A routine for normalizing and shifting data is provided in order to convert raw data into physical units and to aid in the formation of composite traces from several differently scaled data channels. Normalization and shifting of data is accomplished by a simple linear transformation of the form

$$X_{\gamma} = \gamma X + s \quad (1)$$

where $X \equiv$ input data point (either abscissa or ordinate)

$\gamma \equiv$ normalizing coefficient

$s \equiv$ data shift

$X_{\gamma} \equiv$ normalized and shifted point.

Of particular interest in data preparation is the problem of compositing data from several channels into one data trace which covers a wide range of values. For example, in power transients where the power may vary from an initial value of a few watts to hundreds of megawatts, several instruments covering various ranges of data must be used in recording the data. Data recorded on the low range instruments (which saturate early in the transient) must be fitted to the data obtained from the higher range instruments so that one trace of data covering the entire transient is obtained. To form a good composite data trace from two data channels, it is necessary that both the overlapping data points and the slopes of the curves very nearly correspond. To form a composite trace, the data values which are to overlap in the composite channel are plotted; the normalizing and shifting coefficients required to make data values correspond are determined; and the data are adjusted according to Equation (1). No means are provided for correcting errors in the slope of data since such an error generally indicates nonlinearities in the recording instrument. Hence, a general method for correcting errors in slope cannot be devised.

As discussed in Section II-3, power data for calculating reactivity must be in logarithmic form when used as input to the REACTIVITY program. Since power data may not be recorded in logarithmic form, it is necessary to provide a means by which the logarithm of data may be calculated. A standard subroutine for evaluating the natural logarithm of data is used. If a logarithm to another base is desired, it may be obtained through the use of the normalizing coefficient; ie,

$$\log_m x = \left(\log_m e \right) \left(\log_e x \right) \quad (2)$$

2. THE SMOOTH PROGRAM

2.1 Introduction

The SMOOTH program was written primarily for the purpose of removing noise from digitized experimental data. Briefly, the technique used in SMOOTH is that of least-squares fitting of parabolas to sections of input data. In general, a parabola is fitted to the first n data points (where n is designated by the user), and one smoothed point is taken from this parabola. The second smoothed point is obtained by fitting a parabola to the second through the $n + 1$ data point, the third smoothed point by fitting to the third through the $n + 2$ data point, and so on. The smoothed data generated by the program are given at equal time increments. It is not necessary, however, that the input data be given at equal time increments.

2.2 Solution of Equations

The process used in the SMOOTH program is illustrated in Figure 1. In Figure 1, input data points, $[t_i, f(t_i)], [t_{i+1}, f(t_{i+1})], \dots, [t_{i+5}, f(t_{i+5})]$, are represented by x's; and smoothed data points, $[\tau_j, F_j(\tau_j)]$ and $[\tau_{j+1}, F_{j+1}(\tau_{j+1})]$, are represented by circles. It should be noted that the time value of the output points, τ_j and τ_{j+1} , may not necessarily correspond with any input time point. The first parabola, $F_j(\tau)$, is obtained by a least-squares fitting of a parabola to the five data points, $f(t_i), f(t_{i+1}), \dots, f(t_{i+4})$. These points are used since τ_j is "centered" (as defined below) among the time points $t_i, t_{i+1}, \dots, t_{i+4}$. The smoothed value is obtained by evaluating $F_j(\tau_j)$. The time point τ_{j+1} is centered among the points $t_{i+1}, t_{i+2}, \dots, t_{i+5}$; so this smoothed point is obtained by fitting a parabola $F_{j+1}(\tau)$ to $f(t_{i+1}), f(t_{i+2}), \dots, f(t_{i+5})$ and evaluating

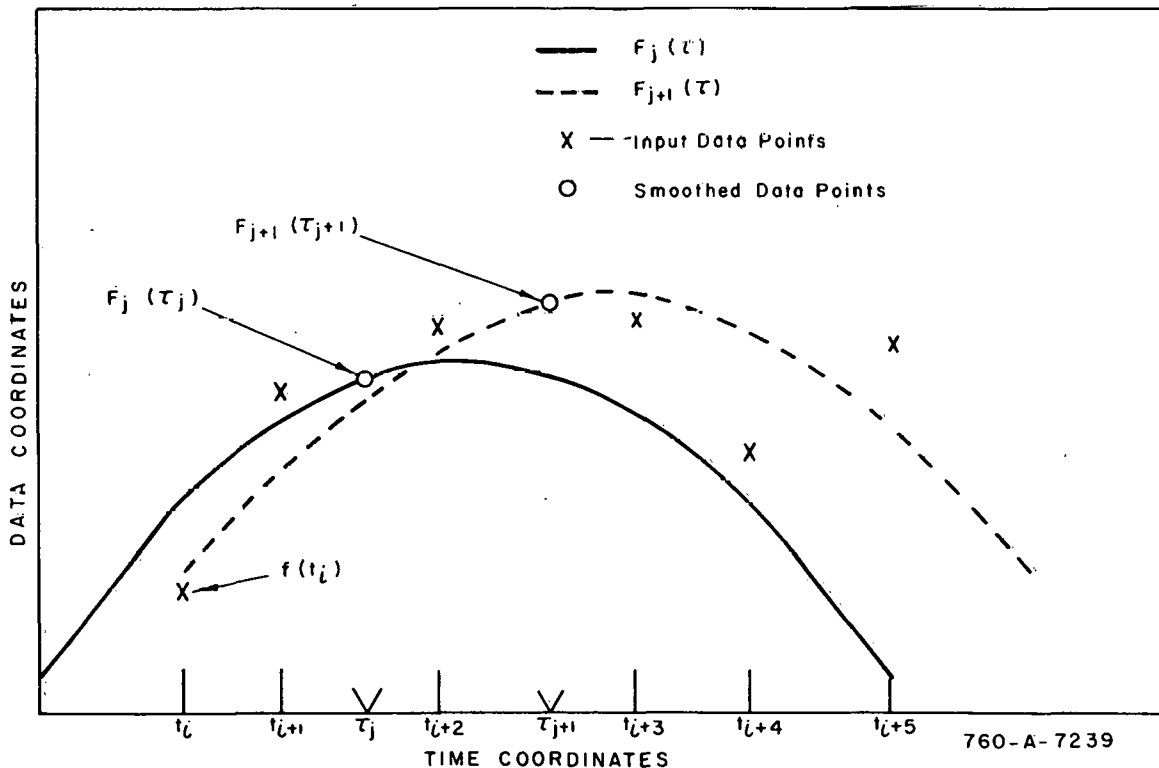


Fig. 1 Process used in the SMOOTH program.

$F_{j+1}(\tau_{j+1})$. The definition of the expression "centered", the method of least-squares fitting of a parabola to n data points, a description of a time shift employed in SMOOTH to increase its accuracy, and the equations which are solved in the program are discussed in detail in the following paragraphs.

The symbol, t_i , in this discussion, used to represent time values of input data points while the symbol, τ_j , is used to represent time values of the smoothed data points. (The problem is complicated by the fact that there may be time shifts in either or both of the time scales; but in this discussion, reference is made only to time values corresponding to the time scale on the input data.) In using the program, τ_0 , the time point at which the first smoothed point is desired must be furnished as an input parameter. Data time points, $t_i, t_{i+1}, \dots, t_{i+m}$ are then found so that τ_0 is centered among these points. The definition of centered, then, is that

$$\frac{1}{2}[t_{i+\frac{1}{2}m-1} + t_{i+\frac{1}{2}m}] < \tau_0 \leq \frac{1}{2}[t_{i+\frac{1}{2}m} + t_{i+\frac{1}{2}m+1}] \quad (3)$$

(In this case, smoothing is on $m + 1$ points; so it is apparent from Equation (3) that smoothing must always be on an odd number of points.) A parabola is fitted to the data values $f(t_i), f(t_{i+1}), \dots, f(t_{i+m})$; and the smoothed value is taken to be the value of the parabola at the point, τ_0 . The time step, $\Delta\tau$, is then added to τ_0 ; ie,

$$\tau_1 = \tau_0 + \Delta\tau \quad (4)$$

and the process is repeated.

To determine a least-squares fit of a function, $g(x)$, to points $h(x_1), h(x_2), \dots, h(x_n)$, it is necessary to find the parameters of $g(x)$ which make the sum

$$\sum_{k=1}^n [h(x_k) - g(x_k)]^2$$

a minimum. In the case of the SMOOTH program, the problem is to fit a parabola to a given number of data points, say n . If the parabola is written

$$F(t) = at^2 + bt + c \quad (5)$$

then it is necessary to minimize the sum

$$v^2(a, b, c) = \sum_{k=1}^n [f(t_{i+k}) - at_{i+k}^2 - bt_{i+k} - c]^2 \quad (6)$$

This function will be a minimum when

$$\frac{\partial v^2}{\partial a} = \frac{\partial v^2}{\partial b} = \frac{\partial v^2}{\partial c} = 0 \quad (7)$$

Equations (6) and (7) reduce to the matrix equation

$$\begin{bmatrix} n & \Sigma t_{i+k} & \Sigma t_{i+k}^2 \\ \Sigma t_{i+k} & \Sigma t_{i+k}^2 & \Sigma t_{i+k}^3 \\ \Sigma t_{i+k}^2 & \Sigma t_{i+k}^3 & \Sigma t_{i+k}^4 \end{bmatrix} \begin{bmatrix} c \\ b \\ a \end{bmatrix} = \begin{bmatrix} \Sigma f(t_{i+k}) \\ \Sigma f(t_{i+k}) t_{i+k} \\ \Sigma f(t_{i+k}) t_{i+k}^2 \end{bmatrix} \quad (8)$$

or

$$T \cdot S = P \quad (9)$$

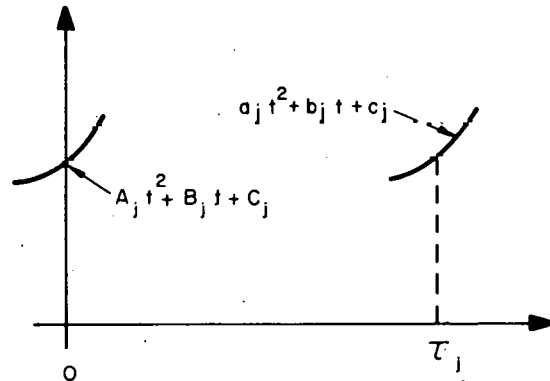
where

$$\Sigma = \sum_{k=1}^n$$

and T, S, and P are the matrices in Equation (8). The problem, then, reduces to one of matrix inversion where

$$S = T^{-1} \cdot P \quad (10)$$

It should be noted that the matrix, T, is dependent only upon time; and that in certain time intervals, poor accuracy is obtained in evaluating T^{-1} . To improve the accuracy of this calculation, a time shift is employed in SMOOTH so that the time used in the calculation is equal to the time of the data point minus τ_j , the time point at which the smoothed value is to be calculated. This shifts the time values, t_{i+1}, \dots, t_{i+n} , to points near the origin and maintains better accuracy in the calculation of T^{-1} . Figure 2 illustrates this time shift. The coefficients calculated by SMOOTH at a time point, τ_j , say A_j, B_j, C_j , are related to the coefficients a_j, b_j , and c_j given by Equation (10) by the following equation:



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Fig. 2 Time shift used in the SMOOTH program.

$$A_j t^2 + B_j t + C_j = a_j (t + \tau_j)^2 + b_j (t + \tau_j) + c_j \quad (11)$$

Therefore, C_j is the smoothed data value at τ_j , and B_j is the slope of the smoothed function at τ_j .

With the time shift described above, the time matrix becomes

$$\bar{T}_j = \begin{bmatrix} n & \Sigma(t_k - \tau_j) & \Sigma(t_k - \tau_j)^2 \\ \Sigma(t_k - \tau_j) & \Sigma(t_k - \tau_j)^2 & \Sigma(t_k - \tau_j)^3 \\ \Sigma(t_k - \tau_j)^2 & \Sigma(t_k - \tau_j)^3 & \Sigma(t_k - \tau_j)^4 \end{bmatrix} \quad (12)$$

and the coefficients A_j, B_j, C_j are given by the matrix equation

$$\bar{S}_j = \bar{T}_j^{-1} \cdot P \quad (13)$$

A case of special interest is that of data points at constant time intervals, Δt . In this case,

$$\Sigma(t_k - \tau_j) = \Delta t \sum_{-\frac{1}{2}(n-1)}^{\frac{1}{2}(n-1)} k = 0 \quad (14)$$

$$\Sigma(t_k - \tau_j)^2 = 2\Delta t^2 \sum_1^{\frac{1}{2}(n-1)} k^2 \equiv K_1 \quad (15)$$

$$\Sigma(t_k - \tau_j)^3 = \Delta t^3 \sum_{-\frac{1}{2}(n-1)}^{\frac{1}{2}(n-1)} k^3 = 0 \quad (16)$$

$$\Sigma(t_k - \tau_j)^4 = 2\Delta t^4 \sum_1^{\frac{1}{2}(n-1)} k^4 \equiv K_2 \quad (17)$$

Equation (12) then becomes

$$\bar{T} = \begin{bmatrix} n & 0 & K_1 \\ 0 & K_1 & 0 \\ K_1 & 0 & K_2 \end{bmatrix} \quad (18)$$

and

$$C_j = \frac{1}{K_1(nK_2 - K_1^2)} [K_2 \Sigma f(t_{i+k}) - K_1 \Sigma f(t_{i+k}) t_k^{*2}] \quad (19)$$

$$B_j = \frac{1}{K_1} \Sigma f(t_{i+k}) t_k^* \quad (20)$$

$$A_j = \frac{1}{nK_2 - K_1^2} [n \sum f(t_{i+k}) t_k^{*2} - K_1 \sum f(t_{i+k})] \quad (21)$$

where

$$t_k^* = t_{i+k} - \tau_j \quad (22)$$

For data points at constant time intervals, considerable computer time can be saved by using Equations (19), (20), and (21).

The output from SMOOTH consists of a listing of the identification number, the time values, and the coefficients A, B, and C (corresponding to a parabola, $F(t) = At^2 + Bt + C$) and plots of the coefficients B and C. It should be recalled from the above discussion that these coefficients correspond to a parabola fitted to data points centered about the origin (as shown in Figure 3). The smoothed data value is evaluated as $F(0)$ which reduces to the value of coefficient C. Therefore, the parameter labeled coefficient C, both in the listings and in the plots, represents the smoothed data values. In a similar manner, the derivative of $F(t)$ evaluated at $t = 0$ is the derivative of the smoothed data (and an approximation of the derivative of the original data) at each output point. But the derivative of $F(t)$ evaluated at $t = 0$ is simply the coefficient B. Therefore, in output from the SMOOTH program and in subsequent discussions in this report, the coefficients C and B are used to represent the smoothed data values and the derivative of the smoothed data values, respectively.

2.3 Filter Characteristics of the SMOOTH Program

The primary objective of the SMOOTH program is to reduce the noise in the input data without significantly distorting the "signal". In order to properly apply the SMOOTH program to a given set of data points, it is quite helpful to have available the characteristics of the program normally associated with filters; ie, the impulse response, the step response, and the frequency response. These characteristics are derived and discussed in this section.

It should be noted that the SMOOTH program differs from ordinary or "physically realizable" filters in two respects: (a) The time span of the input data considered in determining the output is finite. (b) The output at a particular time is determined from future as well as past input data. That is, while in an ordinary filter use of future data is not possible and all past data is theoretically considered in determining the output, in the SMOOTH program a finite range of both past and future data is used to determine the output.

In the following derivations, two assumptions are utilized. First, it is assumed that the past and future time spans of data considered by the program are equal. This assumption is valid only for input data which are digitized at equal time increments. Second, for mathematical convenience, it is assumed that the input data are continuous rather than discrete. This assumption is equivalent to assuming that the discrete data points are of sufficient density to provide an accurate representation of the initially continuous data. Thus, the results of this section apply only to input data which have been digitized at equal time increments and for which the digitizing interval is such that the digitized data are an accurate representation of the initial (continuous) data.

The method of filtering used in the SMOOTH program is to approximate the input data, $f(t)$, by a function of the form,

$$F(t) = a(t)t^2 + b(t)t + c(t)$$

where $a(t)$, $b(t)$, and $c(t)$ are defined such that

$$v^2(t) = \frac{1}{\delta t} \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} \{f(\tau) - [a(t)\tau^2 + b(t)\tau + c(t)]\}^2 d\tau \quad (23)$$

is minimized. Equation (23) can be rewritten as

$$v^2(t) = \frac{1}{\delta t} \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} \{f(\tau) - [A(t) \{\tau-t\}^2 + B(t) \{\tau-t\} + C(t)]\}^2 d\tau \quad (24)$$

where

$$A(t) = a(t) \quad (25)$$

$$B(t) = b(t) + 2a(t)t \quad (26)$$

and

$$C(t) = a(t)t^2 + b(t)t + c(t) \quad (27)$$

Note that, as indicated by Equation (27),

$$C(t) = F(t) \quad (28)$$

Hence,

$$\frac{dF(t)}{dt} = t^2 \frac{da}{dt} + 2at + t \frac{db}{dt} + b + \frac{dc}{dt} \quad (29)$$

or, by Equation (26),

$$\frac{dF(t)}{dt} = t^2 \frac{da}{dt} + t \frac{db}{dt} + \frac{dc}{dt} + B \quad (30)$$

In using the output of the SMOOTH program, the coefficient B is taken as an approximation to $dF(t)/dt$. This approximation is reasonable since in the actual input to SMOOTH, the function $f(t)$ is represented by a set of discrete points. Between points the function is approximated by the appropriate parabola so that in the immediate vicinity of a point, the coefficients a , b , and c are constant. The consequences of the approximation

$$\frac{dF(t)}{dt} \approx B(t)$$

are discussed later in the development of the frequency response of SMOOTH.

In order to minimize $v^2(t)$, it is necessary that

$$\frac{\partial v^2}{\partial A} = 0, \quad \frac{\partial v^2}{\partial B} = 0, \quad \text{and} \quad \frac{\partial v^2}{\partial C} = 0 \quad .$$

Thus, from Equation (24),

$$\frac{\partial v^2}{\partial A} = - \frac{2}{\delta t} \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} \{f(\tau) - [A \{\tau-t\}^2 + B \{\tau-t\} + C]\} \{\tau-t\}^2 d\tau = 0 \quad (31)$$

$$\frac{\partial v^2}{\partial B} = - \frac{2}{\delta t} \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} \{f(\tau) - [A \{\tau-t\}^2 + B \{\tau-t\} + C]\} \{\tau-t\} d\tau = 0 \quad (32)$$

and

$$\frac{\partial v^2}{\partial C} = - \frac{2}{\delta t} \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} \{f(\tau) - [A \{\tau-t\}^2 + B \{\tau-t\} + C]\} d\tau = 0 \quad (33)$$

Then, for Equation (31),

$$\frac{\delta t^5}{2^4 \cdot 5} A(t) + \frac{\delta t^3}{2^2 \cdot 3} C(t) = I_2(t) \quad (34)$$

from Equation (32),

$$\frac{\delta t^3}{2^2 \cdot 3} B(t) = I_1(t) \quad (35)$$

and from Equation (33),

$$\frac{\delta t^3}{2^2 \cdot 3} A(t) + \delta t C(t) = I_0(t) \quad (36)$$

where

$$I_2(t) = \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} f(\tau) [\tau-t]^2 d\tau \quad (37)$$

$$I_1(t) = \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} f(\tau) [\tau-t] d\tau \quad (38)$$

and

$$I_0(t) = \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} f(\tau) d\tau \quad (39)$$

Simultaneous solution of Equations (34), (35), and (36) yields

$$C(t) = \frac{9}{4\delta t} I_0 - \frac{15}{\delta t^3} I_2 \quad (40)$$

[where $C(t) = F(t)$].

and

$$B(t) = \frac{12}{\delta t^3} I_1 \quad (41)$$

[where $D(t) \simeq \frac{dF(t)}{dt}$].

2.31 Impulse Response. If the input function $f(t)$ is a unit impulse at $t = 0$,

$$I_0 = \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} u_1(\tau) d\tau = u\left(t + \frac{\delta t}{2}\right) - u\left(t - \frac{\delta t}{2}\right) \quad (42)$$

and

$$I_2 = \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} (\tau-t)^2 u_1(\tau) d\tau = t^2 \left[u\left(t + \frac{\delta t}{2}\right) - u\left(t - \frac{\delta t}{2}\right) \right] \quad (43)$$

Substituting Equations (42) and (43) into Equation (40) yields for the impulse response of the SMOOTH program,

$$C(t) = \frac{9}{4\delta t} - \frac{15}{\delta t^3} t^2 \left[u\left(t + \frac{\delta t}{2}\right) - u\left(t - \frac{\delta t}{2}\right) \right] \quad (44)$$

The anticipatory and finite memory characteristics are clearly illustrated by the sketch of the impulse response given in Figure 3. The input impulse is "anticipated" for $t > -\frac{\delta t}{2}$, but is "forgotten" when $t > \frac{\delta t}{2}$. In contrast an ordinary filter has no anticipatory properties, but in theory will "remember" the impulse forever.

2.32 The Step Response. If a unit step function is applied to the SMOOTH program at $t = 0$,

$$\begin{aligned} I_0 &= \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} u(\tau) d\tau \\ &= t \left[u\left(t + \frac{\delta t}{2}\right) - u\left(t - \frac{\delta t}{2}\right) \right] \\ &\quad + \frac{\delta t}{2} \left[u\left(t + \frac{\delta t}{2}\right) + u\left(t - \frac{\delta t}{2}\right) \right] \end{aligned} \quad (45)$$

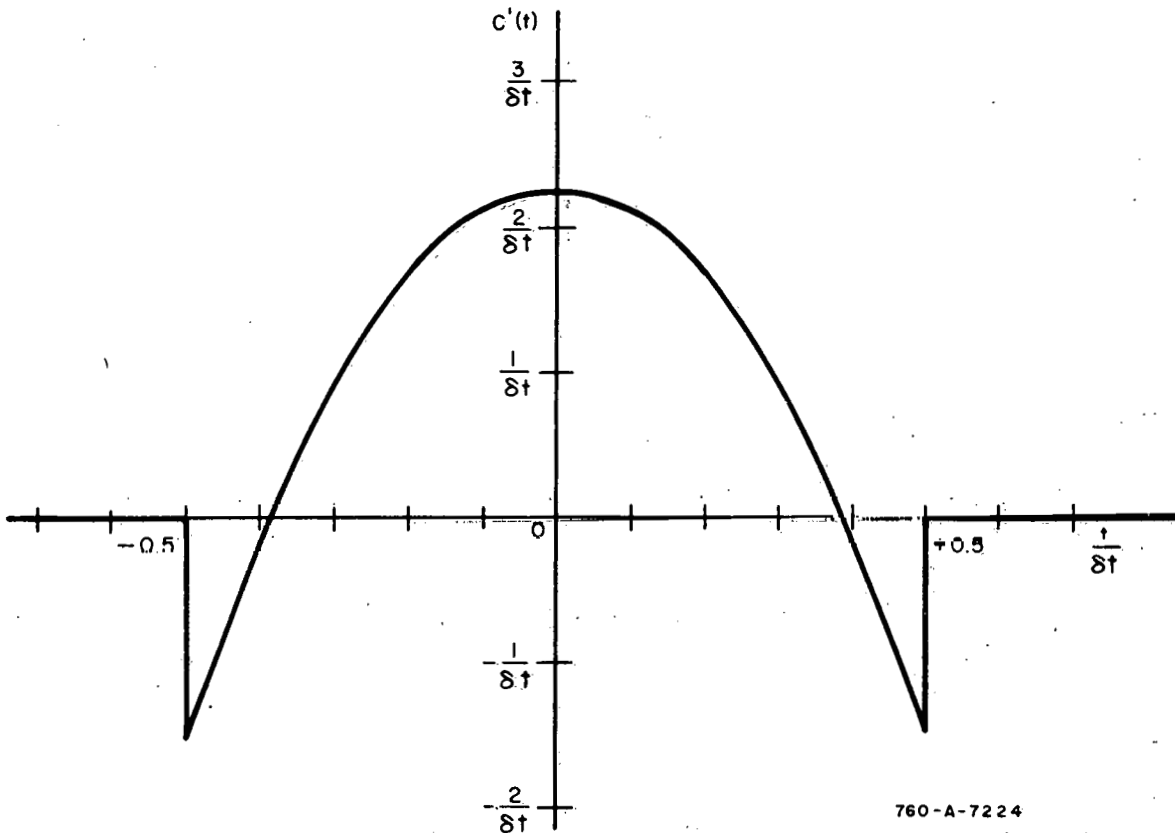


Fig. 3 Response of SMOOTH to the impulse function.

and

$$\begin{aligned}
 I_2 &= \int_{t-\frac{\delta t}{2}}^{t+\frac{\delta t}{2}} (\tau-t)^2 u(\tau) d\tau \\
 &= \frac{t^3}{3} \left[u\left(t+\frac{\delta t}{2}\right) - u\left(t-\frac{\delta t}{2}\right) \right] \\
 &\quad + \frac{t^3}{24} \left[u\left(t+\frac{\delta t}{2}\right) + u\left(t-\frac{\delta t}{2}\right) \right] . \quad (46)
 \end{aligned}$$

Substituting Equations (45) and (46) into Equation (40) and rearranging yields for the step response of the SMOOTH program,

$$\begin{aligned}
 c(t) &= \left[\frac{9}{4\delta t} t - \frac{5}{\delta t^3} t^3 \right] \left[u\left(t + \frac{\delta t}{2}\right) - u\left(t - \frac{\delta t}{2}\right) \right] \\
 &\quad + \frac{1}{2} \left[u\left(t + \frac{\delta t}{2}\right) + u\left(t - \frac{\delta t}{2}\right) \right] . \quad (47)
 \end{aligned}$$

As shown in Figure 4, the step response overshoots the magnitude of the applied step by about 8 percent. However for time greater than $\frac{\delta t}{2}$, the output is precisely equal to the magnitude of the applied step.

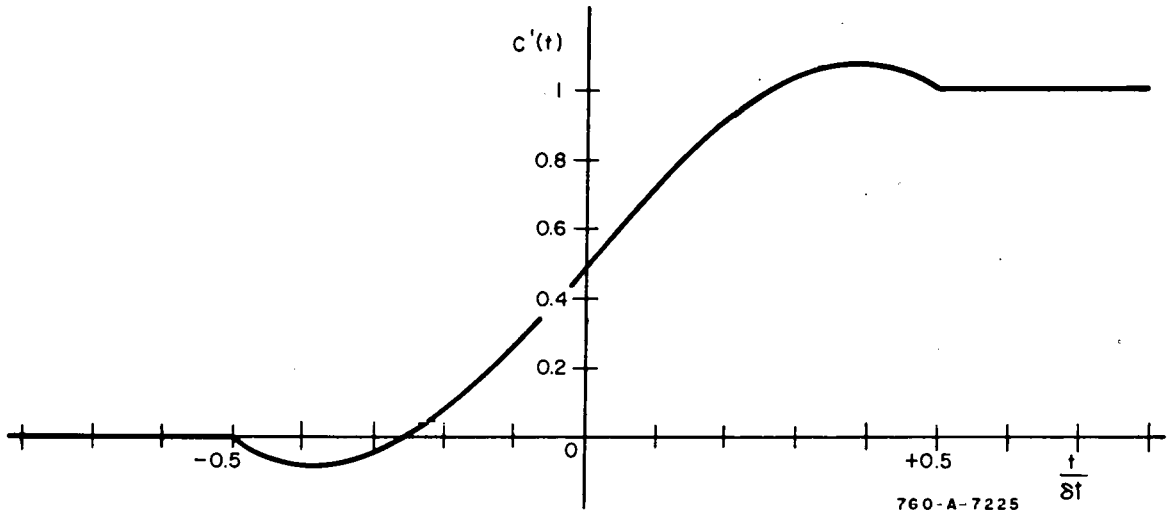


Fig. 4 Response of SMOOTH to the unit step function.

2.33 Frequency Response. The frequency response of the SMOOTH program may be derived by the common procedure of obtaining the Laplace transform of the impulse response. However, the procedure must be slightly altered because of the anticipatory nature of the SMOOTH program response. Since the ordinary Laplace transformation is unilateral, negative values of time cannot be considered. Therefore, in order to obtain the Laplace transform of the impulse response, it is necessary to apply the impulse at a time such that no response is obtained for times less than zero, ie, at $t \geq \frac{\delta t}{2}$.

Thus, let the input function, $f(t)$, be a unit impulse at $t = \frac{\delta t}{2}$, ie,

$$f(t) = u_1 \left(t - \frac{\delta t}{2} \right) .$$

The transfer function is then

$$G(s) = \frac{\bar{C}(s)}{u_1(s)} \quad (48)$$

where $\bar{C}(s)$ is the Laplace transform of the response to a unit impulse $u_1(t - \frac{\delta t}{2})$.

From Equation (44),

$$c\left(t - \frac{\delta t}{2}\right) = \left[\frac{9}{4\delta t} - \frac{15}{\delta t^3} \left(t - \frac{\delta t}{2}\right)^2 \right] \left[u(t) - u(t - \delta t) \right] \quad (49)$$

Then,

$$\begin{aligned} \bar{C}(s) &= L \left[c\left(t - \frac{\delta t}{2}\right) \right] \\ &= \frac{15}{\delta t^2 s^2} \left[1 + e^{-\delta t s} \right] \\ &\quad - \left[\frac{3}{2\delta t s} + \frac{30}{\delta t^3 s^3} \right] \left[1 - e^{-\delta t s} \right] \end{aligned} \quad (50)$$

and

$$\bar{u}_1(s) = L\left[u\left(t - \frac{\delta t}{2}\right)\right] = e^{-\frac{\delta t}{2}s} \quad (51)$$

Substituting Equations (50) and (51) into Equation (48) and rearranging yields for the transfer function of SMOOTH:

$$G(s) = \frac{15}{\delta t^2 s^2} \left[e^{\frac{\delta t}{2}s} + e^{-\frac{\delta t}{2}s} \right] - \left[\frac{3}{2\delta t s} + \frac{30}{\delta t^3 s^3} \right] \left[e^{\frac{\delta t}{2}s} - e^{-\frac{\delta t}{2}s} \right] \quad (52)$$

The frequency response may be obtained by the usual procedure of setting $s = j\omega$. Thus, from Equation (52),

$$G(j\omega) = -\frac{15}{\delta t^2 \omega^2} \left[e^{j\frac{\delta t\omega}{2}} + e^{-j\frac{\delta t\omega}{2}} \right] - \left[\frac{3}{2j\delta t\omega} - \frac{30}{j\delta t^3 \omega^3} \right] \left[e^{j\frac{\delta t\omega}{2}} - e^{-j\frac{\delta t\omega}{2}} \right] \quad (53)$$

or

$$G(j\omega) = -\frac{30}{\delta t^2 \omega^2} \cos \frac{\delta t\omega}{2} - \left[\frac{3}{\delta t\omega} - \frac{60}{\delta t^3 \omega^3} \right] \sin \frac{\delta t\omega}{2} \quad (54)$$

It can easily be determined from Equation (54) that the frequency response, $G(j\omega)$, is always real and has an infinite number of zeros located on the positive real axis of the complex plane. It is positive in the frequency range between $\omega = 0$ and the first zero of $G(j\omega)$, negative between the first and second zeros, positive between the second and third zeros, etc. Further, it can be shown that

$$\lim_{\omega \rightarrow 0} G(j\omega) = 1$$

Thus, the SMOOTH program is a zero-phase, low-pass filter. It has an attenuation of 0.7 (3dB) at $\omega\delta t \approx 6.6$.

As shown in Figure 5, the roll-off characteristic preceding the first zero is rather sharp; but the effectiveness of the SMOOTH program in filtering high frequencies is reduced by the lobes between successive zeros. As discussed in a following subsection, however, the attenuation of high frequencies can be

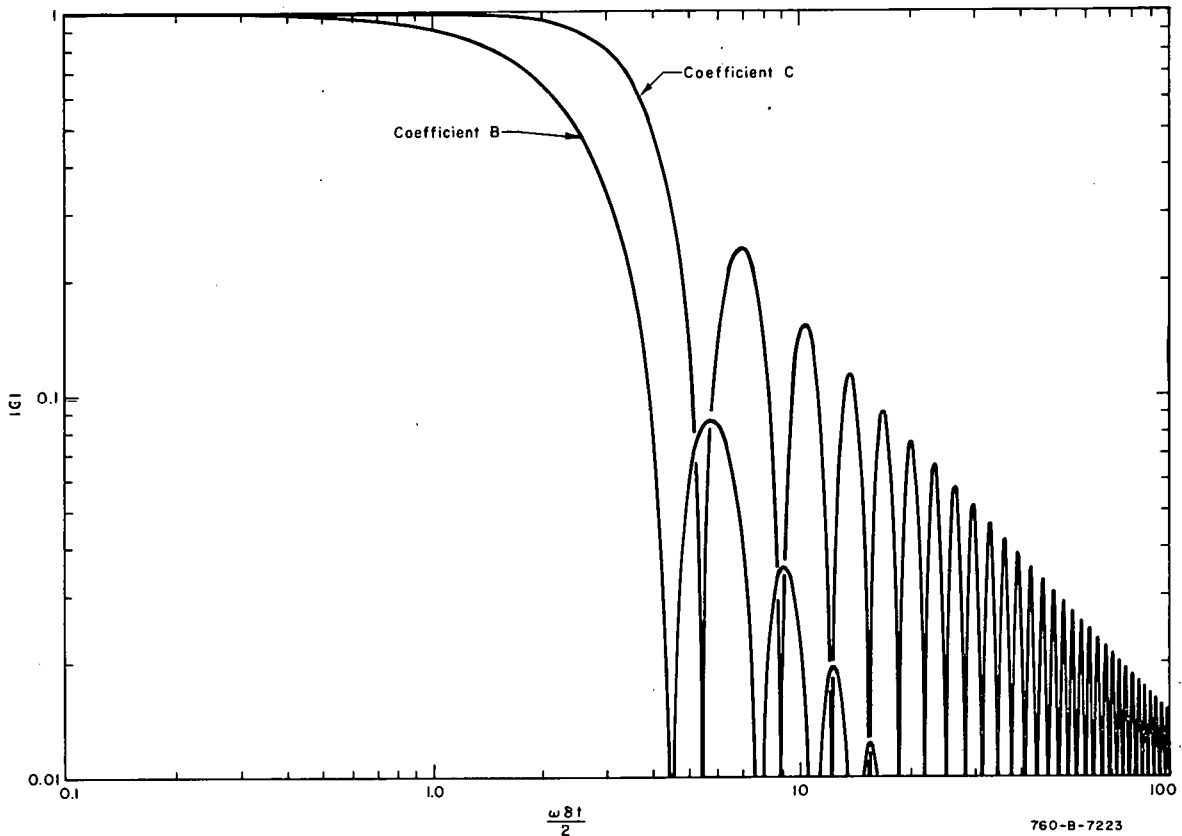


Fig. 5 Frequency response of SMOOTH for coefficients C and B.

markedly increased by multiple smoothing without significantly altering the low frequency transfer function.

Because the SMOOTH program automatically computes a smoothed derivative of the input data and because this derivative is used in the REACTIVITY program, the transfer function which is, in effect, applied to the derivative of the input data is also of interest. If $B(t)$ is an approximation to $df(t)/dt$, then the transfer function of interest is

$$G'(s) = \frac{\bar{B}(s)}{s\bar{f}(s)} \quad (55)$$

where $\bar{B}(s)$ is the transform of the $B(t)$ which results when $f(t)$ is applied. The transfer function, $G'(s)$, is then a measure of the deviation of $B(t)$ from $df(t)/dt$. If, as before, $f(t) = u(t - \frac{\delta t}{2})$; by Equations (38) and (41),

$$B(t) = -\frac{12}{\delta t^3} \left(t - \frac{\delta t}{2}\right) [u(t) - u(t - \delta t)] \quad (56)$$

so that

$$B(s) = \frac{6}{\delta t^2 s} \left[1 + e^{-\delta t s}\right] - \frac{12}{\delta t^3 s^2} \left[1 - e^{-\delta t s}\right] \quad (57)$$

By Equation (55),

$$G'(s) = \frac{6}{\delta t^2 s^2} \left[e^{\frac{\delta t}{2}s} + e^{-\frac{\delta t}{2}s} \right] - \frac{12}{\delta t^3 s^3} \left[e^{\frac{\delta t}{2}s} - e^{-\frac{\delta t}{2}s} \right] \quad (58)$$

The frequency response of the effective filter applied in obtaining the derivative of the input data is, thus,

$$G'(j\omega) = -\frac{12}{\delta t^2 \omega^2} \cos \frac{\omega \delta t}{2} + \frac{24}{\delta t^3 \omega^3} \sin \frac{\omega \delta t}{2} \quad (59)$$

Thus, the filtering process used in obtaining $\frac{dF(t)}{dt}$ is somewhat different from that used in obtaining $F(t)$. This difference is a consequence of the neglect of the derivatives of a , b , and c in Equation (25). The magnitude of $G'(j\omega)$ is shown in Figure 5 along with the magnitude of $G(j\omega)$. The fact that $G'(j\omega)$ is, on the average, smaller than $G(j\omega)$ at high frequencies is helpful in obtaining a smooth derivative because the differentiation amplifies the high frequency components of the noise. On the other hand, the selection of a δt to minimize the distortion of the desired signal does not ensure that the distortion of the derivative of the signal will also be minimized. Thus, in the selection of the δt to be used in smoothing a particular set of data, attention must be directed to both the input signal and its derivative and the filtering processes applied to each.

2.34 Multiple Smoothing. Multiple smoothing consists in recycling the output, $C(t)$, in the SMOOTH program through the program any desired number of times. It is equivalent to the common procedure of placing several filters in series in order to obtain the desired attenuation of unwanted frequency components. Since

$$\bar{C}(s) = \bar{F}(s) G(s)$$

the output of the SMOOTH program resulting from one recycle, call it $C_1(t)$, will be

$$C_1(t) = L^{-1} [\bar{C}(s) G(s)] = L^{-1} [f(s) [G(s)]^2] \quad (60)$$

In general, then, the output after n passes ($n-1$ recycles) will be

$$C_{n-1}(t) = L^{-1} [\bar{f}(s) [G(s)]^n]$$

So that the transfer function for n passes is simply

$$G_n(s) = [G(s)]^n \quad (61)$$

Because of the sharp roll-off characteristic of $G(j\omega)$ prior to the first zero, it is possible by multiple smoothing to markedly reduce the high frequency lobes without significantly changing the shape of the transfer function below the first zero. To illustrate, on Figure 6 are plotted the transfer functions resulting from one, two, and three passes through the SMOOTH program. Thus, by utilizing three passes, essentially all frequency components above the first zero of $G_3(s)$ will be attenuated by a factor greater than 100.

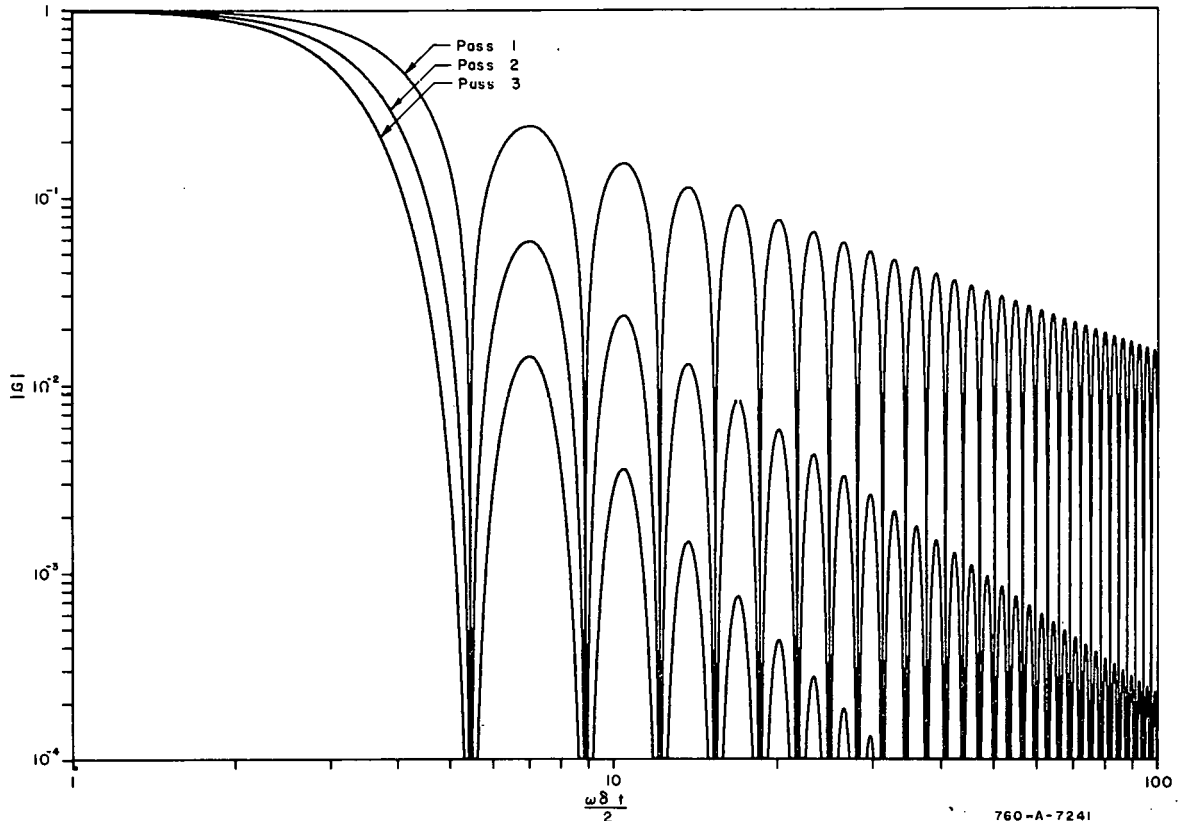


Fig. 6 Transfer functions for one, two, and three passes through SMOOTH.

Because only $C_{n-1}(t)$ is entered as input on the n th pass through SMOOTH,

$$G'_n(s) = G'(s) [G(s)]^{n-1} \quad (62)$$

so that the ratio $G'_n(s)/G_n(s)$ is independent of the number of cycles through the SMOOTH program.

3. THE REACTIVITY PROGRAM

3.1 Introduction

The REACTIVITY program was written for the purpose of calculating the reactivity of a reactor from recorded power data. In this calculation, the applicability of the lumped-parameter reactor kinetic equations is assumed. Up to 50 delayed neutron groups may be used. Power data to be used as input to this program must be in natural logarithmic form and must first be processed by the SMOOTH program. Initial conditions are entered by specifying either (a) the initial asymptotic exponential period of the power rise or (b) the initial concentrations of the delayed neutron precursors. The output of this program consists of the instantaneous values of (a) the reactivity, (b) the compensated reactivity when the initial reactivity perturbation is a step, (c) the linear power, (d) the energy released, and (e) the ratio of the compensated reactivity to the energy released.

3.2 Solution of Equations

In the REACTIVITY program, it is assumed that the time behavior of the reactor can be adequately described by the system of equations

$$\dot{\phi}(t) = \frac{\rho(t) - \bar{\beta}}{\Lambda} \phi(t) + \sum_{i=1}^n \lambda_i C_i(t) + s \quad (63)$$

$$\dot{C}_i(t) = \frac{\bar{\beta}_i}{\Lambda} \phi(t) - \lambda_i C_i(t) \quad (64)$$

where

$\phi(t) \equiv$ power of the reactor

$\rho(t) \equiv$ reactivity

$\Lambda \equiv$ prompt neutron generation time

$C_i(t) \equiv$ concentration of i^{th} delayed neutron precursor

$\lambda_i \equiv$ decay constant of the i^{th} delayed neutron precursor group

$\beta_i \equiv$ effective fraction of delayed neutrons produced by i^{th} precursor group

$\bar{\beta} \equiv \sum \bar{\beta}_i$

$s \equiv$ source equivalence.

This system of equations can be written in a more convenient form by defining

$$r_i \equiv \bar{\beta}_i / \bar{\beta} \quad (65)$$

and

$$\omega_i(t) \equiv \frac{\Lambda \lambda_i}{\bar{\beta} r_i} C_i(t) \quad (66)$$

and substituting these quantities into Equations (63) and (64). The system of equations then reduces to

$$\dot{\phi}(t) = \frac{\rho(t) - \bar{\beta}}{\Lambda} \phi(t) + \sum_{i=1}^n \frac{\bar{\beta} r_i}{\Lambda} \omega_i(t) + s \quad (67)$$

$$\dot{\omega}_i(t) = \lambda_i \phi(t) - \lambda_i \omega_i(t) \quad (68)$$

From Equation (67)

$$\frac{\dot{\phi}(t)}{\bar{\beta}} \equiv \dot{\phi}(t) = 1 + \frac{1}{\phi(t)} \left[\frac{\Lambda}{\bar{\beta}} \dot{\phi}(t) - \sum_{i=1}^n r_i \omega_i(t) \right] - \frac{\Lambda}{\bar{\beta}} \frac{s}{\phi(t)} \quad (69)$$

Experimental power data to be used in REACTIVITY must first be converted to natural logarithmic form (see Input Format for SMOOTH) and processed by the SMOOTH program. When $\ln \phi$ is used as input to SMOOTH, a parabola is fitted to a prescribed number of data points (say ϕ_{j-2} , ϕ_{j-1} , ϕ_j , ϕ_{j+1} , ϕ_{j+2}) such that

$$\ln \phi_j^*(t) \approx A_j t^2 + B_j t + C_j$$

where

$$\phi_j^*(t) = \phi(t + t_j)$$

(i.e., $\phi(t)$ is shifted by t_j). Therefore,

$$\ln \phi(t_j) = \ln \phi_j^*(0) = C_j \quad (70)$$

and

$$\left. \frac{\dot{\phi}(t)}{\phi(t)} \right|_{t=t_j} = \left. \frac{d}{dt} \ln \phi_j^*(t) \right|_{t=0} = B_j \quad (71)$$

Hence, from Equation (69)

$$\phi(t_j) = 1 + \frac{\Lambda}{\beta} B_j - \frac{1}{\phi(t_j)} \sum_{i=1}^n f_i \omega_i(t_j) - \frac{\Lambda}{\beta} \frac{s}{\phi(t_j)} \quad (72)$$

The parameters Λ/β and f_i are input data; therefore, to complete the solution, $\phi(t_j)$ and the ω_i 's must be calculated. From Equation (70)

$$\phi(t_j) = e^{C_j} \quad (73)$$

To evaluate $\omega_i(t)$, Equation (68) may be solved to give

$$\omega_i(t) = e^{-\lambda_i t} \int \lambda_i e^{\lambda_i \tau} \phi(\tau) d\tau + e^{-\lambda_i t} \cdot K$$

where K is constant. If $\omega_i(t-\delta)$ is known, $\omega_i(t)$ may be calculated by

$$\omega_i(t) = e^{-\lambda_i t} \int_{t-\delta}^t \lambda_i e^{\lambda_i \tau} \phi(\tau) d\tau + \omega_i(t-\delta) e^{-\lambda_i \delta} \quad (74)$$

For the purpose of calculating

$$\int_{t-\delta}^t e^{\lambda_i \tau} \phi(\tau) d\tau$$

it is convenient to have coefficients which correspond to linear data rather than to logarithmic data. The relation between the two sets of coefficients is as follows:

If
$$A_j t^2 + B_j t + C_j = \ln \phi^*(t) \quad (75)$$

and

$$a_j t^2 + b_j t + c_j = \phi^*(t) \quad (76)$$

then, at $t=0$,

$$c_j = e^{C_j} \quad (77)$$

$$b_j = c_j B_j \quad (78)$$

and

$$a_j = c_j [A_j + \frac{1}{2} B_j^2] \quad (79)$$

Furthermore, since the coefficients a_j , b_j , and c_j correspond to $\phi^*(t)$ at $t=0$, it is convenient to make the following transformation:

$$\begin{aligned} e^{-\lambda_i t} \int_{t-\delta}^t \lambda_i e^{\lambda_i \tau} \phi(\tau) d\tau &= \int_{t-\delta}^t \lambda_i e^{\lambda_i(\tau-t)} \phi(\tau) d\tau \\ &= \int_{-\delta}^0 \lambda_i e^{\lambda_i \tau} \phi(\tau+t) d\tau \\ &= \int_{-\delta}^0 \lambda_i e^{\lambda_i \tau} \phi^*(\tau) d\tau \end{aligned} \quad (80)$$

where $\phi^*(\tau) = \phi(\tau+t)$. Therefore,

$$\omega_i(t) = \omega_i(t-\delta) e^{-\lambda_i \delta} + \int_{-\delta}^0 \lambda_i e^{\lambda_i \tau} \phi^*(\tau) d\tau \quad (81)$$

Since

$$\phi^*(\tau) = a_j \tau^2 + b_j \tau + c_j$$

the following may be written:

$$\begin{aligned} \int_{-\delta}^0 \lambda_i e^{\lambda_i \tau} \phi^*(\tau) d\tau &= \int_{-\delta}^0 \lambda_i e^{\lambda_i \tau} (a_j \tau^2 + b_j \tau + c_j) d\tau \\ &= \frac{e^{\lambda_i \tau}}{\lambda_i^2} \left[a_j (\lambda_i^2 \tau^2 - 2\lambda_i \tau + 2) + \lambda_i b_j (\lambda_i \tau - 1) + \lambda_i^2 c_j \right] \Big|_{-\delta}^0 \end{aligned}$$

$$= \frac{1}{\lambda_i^2} \left\{ a_j \left[2 - e^{-\lambda_i \delta} (\lambda_i^2 \delta^2 + 2\lambda_i \delta + 2) \right] \right. \\ \left. + b_j \lambda_i \left[e^{-\lambda_i \delta} (\lambda_i \delta + 1) - 1 \right] + c_j \lambda_i^2 \left[1 - e^{-\lambda_i \delta} \right] \right\} \quad (82)$$

Defining constants K_{1i} , K_{2i} , and K_{3i} as

$$K_{1i} \equiv \frac{1}{\lambda_i^2} \left[2 - e^{-\lambda_i \delta} (\lambda_i^2 \delta^2 + 2\lambda_i \delta + 2) \right] \quad (83)$$

$$K_{2i} \equiv \frac{1}{\lambda_i} \left[e^{-\lambda_i \delta} (\lambda_i \delta + 1) - 1 \right] \quad (84)$$

and

$$K_{3i} \equiv (1 - e^{-\lambda_i \delta}) \quad (85)$$

Equation (82) can be written as

$$\int_{-\delta}^0 \lambda_i e^{\lambda_i \tau} \phi^*(\tau) d\tau = [a_j K_{1i} + b_j K_{2i} + c_j K_{3i}] \quad (86)$$

and Equation (81) can be written as

$$\omega_i(t) = \omega_i(t-\delta) e^{-\lambda_i \delta} + a_j K_{1i} + b_j K_{2i} + c_j K_{3i} \quad (87)$$

The initial values for ω_i [ie, $\omega_i(t_0)$] may be obtained by two methods: (a) the user may furnish these values as input data; or (b) they may be calculated as described below. (See Input Format, Section III-3.25, page 51.) To calculate $\omega_i(t_0)$ it is assumed that, for all $t < t_0$.

$$\phi(t) = K_1 e^{\alpha t} \quad (88)$$

Then

$$c_i(t) = K_2 e^{\alpha t} \quad (89)$$

and

$$\frac{1}{c_i(t)} \dot{c}_i(t) \Big|_{t=t_0} = \alpha \quad (90)$$

From Equation (64)

$$c_i(t_0) = \frac{\bar{\beta}_i \phi(t_0)}{\Lambda(\lambda_i + \alpha)} \quad (91)$$

and from Equation (66),

$$\omega_i(t_0) = \frac{\lambda_i \phi(t_0)}{\lambda_i + \alpha} \quad (92)$$

With initial values for $\omega_i(t_0)$, $\omega_j(t_1)$ may be calculated from Equation (87); having calculated $\omega_i(t_1)$, $\omega_i(t_2)$ may be calculated in the same manner; and so forth.

From Equations (72), (73), (77), and (87), one obtains finally

$$\begin{aligned} \$(t_j) = 1 + \frac{\Lambda}{\beta} B_j - \frac{1}{c_j} \sum_{i=1}^n f_i \left[\omega_i(t_j - \delta) e^{-\lambda_i \delta} + a_j K_{1i} + b_j K_{2i} \right. \\ \left. + c_j K_{3i} \right] - \frac{\Lambda}{\beta} \frac{s}{c_j} \end{aligned} \quad (93)$$

Equation (93) is the expression used in the REACTIVITY program to calculate the reactivity of the reactor from smoothed power data.

The value for $\$(t_0)$ is calculated from the inhour equation,

$$\$(t_0) = \left[\frac{\Lambda}{\beta} + \sum_{i=1}^n \frac{f_i}{\lambda_i + \alpha} \right] \alpha \quad (94)$$

The compensated reactivity of the system is calculated as

$$\$_c(t) = \$(t) - \$(t_0) \quad (95)$$

It should be noted that both the calculation of $\$(t_0)$, as described by Equation (94), and the calculation of $\$_c(t)$, as defined by Equation (95), are valid only for step transients. The energy released, $E(t)$, is calculated by

$$\begin{aligned} E(t_j) &= E(t_j - \delta) + \int_{-\delta}^0 \phi^*(t) dt \\ &= E(t_j - \delta) + a_j \frac{\delta^3}{3} - b_j \frac{\delta^2}{2} + c_j \delta \end{aligned} \quad (96)$$

where the initial energy, $E(t_0)$, may be entered as input data or may be calculated as (see Input Format Section III-3.25, page 51).

$$E(t_0) = \frac{\phi(t_0)}{\alpha} \quad (97)$$

(Note: If initial energy is to be calculated, the initial period must not be zero.)

The ratio

$$b(t) = \$_c(t)/E(t) \quad (98)$$

is also calculated.

4. THE FREQUENCY RESPONSE PROGRAM

4.1 Introduction

The behavior of a linear system may be described mathematically by an expression of the form

$$O(s) = I(s) G(s) \quad (99)$$

where $I(s)$ is the Laplace transform of the input to the system, and $O(s)$ is the Laplace transform of the resultant output of the system.

The function $G(s)$ is called the transfer function of the system. If $G(s)$ is known for a particular linear system, then the time response of that system to any Laplace transformable input function can be determined by finding the inverse Laplace transform of the function, $O(s)$. Thus, the function, $G(s)$, mathematically characterizes a linear system. An experimental determination of $G(s)$ is therefore often desirable.

As is well known [4], the form of the transfer function can be determined from a knowledge of the frequency response of the system. Hence, the most common method of determining the transfer function is to directly measure the frequency response of the system. That is, the magnitude and phase of the system output relative to a sinusoidal input is determined for various input frequencies. While this method is usually quite accurate, it can be experimentally cumbersome if, for example, the response at very low frequencies is desired or if it is difficult to introduce a sinusoidal input.

Since the transfer function of a linear system is unique, it can easily be shown that the frequency response can be determined from the transient response of the system. Corresponding to Equation (99), the transfer function, $G(s)$, is defined by

$$G(s) = \frac{O(s)}{I(s)} = \frac{L[o(t)]}{L[i(t)]} \quad (100)$$

Hence, $G(s)$ may be determined from the response of a system in the time domain, $o(t)$, to an arbitrary Laplace transformable input function, $i(t)$. While this method tends to be less accurate than that of directly measuring the frequency response (because the experimental data must be processed by numerical techniques), it does allow the frequency response of a linear system to be determined from the results of a single transient experiment.

The FREQUENCY RESPONSE program has been written for the purpose of computing the frequency response from the transient response of a system. This program will numerically evaluate, at designated values of ω_k , the function

$$G(\omega_k) = \frac{\int_0^{\infty} A(t) e^{-i\omega_k t} dt}{\int_0^{\infty} B(t) e^{-i\omega_k t} dt} \quad (101)$$

$A(t)$ and $B(t)$ must be described as pointwise functions at evenly spaced time increments; ie,

$$t_j - t_{j-1} = \Delta t = \text{constant} \quad .$$

Furthermore, $A(t)$ and $B(t)$ must be defined in such a manner that, for some time value t_n , $A(t_m)$ and $B(t_m)$ are constant for $m \geq n$. The restrictions placed upon $A(t_j)$ and $B(t_j)$ are discussed in detail in Section II-4.2.

By means of an option, $B(t)$ may be specified to be a unit impulse so that

$$\int_0^{\infty} A(t) e^{-i\omega_k t} dt \quad (102)$$

is calculated.

The output of the program is as follows:

- (1) Radian Frequencies (ω_k - designated by the user)
- (2) The real part of $G(\omega_k)$
- (3) The imaginary part of $G(\omega_k)$
- (4) $|G(\omega_k)|$
- (5) Phase angle of $G(\omega_k)$ in degrees
- (6) $20 \log_{10} |G(\omega_k)|$
- (7) $\log_{10} \omega_k$.

Careful consideration must be given to the accuracy that may be expected from this program. This is discussed in detail in Section II-4.3.

4.2 Solution of Equations

The purpose of the FREQUENCY RESPONSE program is to calculate the ratio of the unilateral Fourier transforms of digitized experimental data of the form

$$[t_j, f(t_j)]; \quad j = 0, 1, 2, 3, \dots, n \quad .$$

As was pointed out in the introduction, the transfer function is defined by the ratio of the Laplace transforms of the output and input, ie,

$$G(s) = \frac{L[o(t)]}{L[i(t)]} \quad .$$

However, for the purpose of a frequency response analysis, it is sufficient to consider the unilateral Fourier transforms; ie, s is replaced with $i\omega$.

The Laplace transform of $f(t)$ exists if $f(t)$ satisfies the following restrictions:

- (1) The function $f(t)$ must be piecewise regular.
- (2) There exists an α such that, for the real part of $s > \alpha$,

$$\int_0^{\infty} f(t) \cdot e^{-st} dt \text{ converges} \quad .$$

(3) For numerical evaluation of this integral, it is sufficient that $f(t)$ satisfy the further restriction that there exists t_n such that for all $t_m \geq t_n$,

$$f(t_m) = f(t_n) .$$

Any function which describes a physical phenomenon satisfies restrictions 1 and 2. Consequently, in determining the applicability of this program only condition 3 must be of concern.

If $f(t)$ satisfies conditions 1, 2, and 3, the unilateral Fourier transform may be numerically evaluated as follows:

$$\int_0^{\infty} f(t) e^{-i\omega t} dt = \int_0^{\infty} [f(t) - f(t_n)] e^{-i\omega t} dt + \int_0^{\infty} f(t_n) e^{-i\omega t} dt . \quad (103)$$

Since it is assumed that $f(t) = f(t_n)$, a constant, for $t \geq t_n$,

$$\int_0^{\infty} f(t) e^{-i\omega t} dt = \int_0^{t_n} [f(t) - f(t_n)] e^{-i\omega t} dt + \int_0^{\infty} f(t_n) e^{-i\omega t} dt \quad (104)$$

Now

$$\int_0^{\infty} f(t_n) e^{-st} dt = \frac{f(t_n)}{s}$$

and

$$\lim_{s \rightarrow i\omega} \int_0^{\infty} f(t_n) e^{-st} dt = \frac{f(t_n)}{i\omega} . \quad (105)$$

Hence, to complete the evaluation of $\int_0^{\infty} f(t) e^{-i\omega t} dt$, it remains to evaluate

$$\begin{aligned} \int_0^{t_n} [f(t) - f(t_n)] e^{-i\omega t} dt &= \int_0^{t_n} f(t) e^{-i\omega t} dt \\ &+ \frac{f(t_n)}{i\omega} (e^{-i\omega t_n} - 1) . \end{aligned} \quad (106)$$

Consider the integral

$$\int_0^{t_n} f(t) e^{-i\omega t} dt = \int_0^{t_n} f(t) [\cos \omega t - i \sin \omega t] dt . \quad (107)$$

In order to evaluate Equation (107), the function $f(t)$ is approximated by a series of straight lines, so that in the interval $t_{j-1} \leq t \leq t_j$,

$$f(t) = f_{j-1} + \frac{f_j - f_{j-1}}{t_j - t_{j-1}} [t - t_{j-1}] . \quad (108)$$

It is assumed for convenience that $t_j - t_{j-1}$ is constant, so that

$$f(t) = f_{j-1} + \frac{f_j - f_{j-1}}{\Delta t} (t - t_{j-1}) \quad (109)$$

Then, considering the first term on the right-hand side of Equation (107) and letting $t_0 = 0$,

$$\begin{aligned} & \int_0^{t_n} f(t) \cos \omega t \, dt \\ &= \sum_{j=1}^n \int_{t_{j-1}}^{t_j} \left[f_{j-1} + \frac{f_j - f_{j-1}}{\Delta t} (t - t_{j-1}) \right] \cos \omega t \, dt \quad (110) \end{aligned}$$

which reduces to

$$\begin{aligned} & \int_0^{t_n} f(t) \cos \omega t \, dt \\ &= \frac{f_n}{\omega} \sin \omega t_n - \frac{2}{\omega^2 \Delta t} \sin \frac{\omega \Delta t}{2} \sum_{j=1}^n (f_j - f_{j-1}) \sin \omega \left(t_{j-1} + \frac{\Delta t}{2} \right). \quad (111) \end{aligned}$$

In a similar manner,

$$\begin{aligned} & \int_0^{t_n} f(t) \sin \omega t \, dt = \sum_{j=1}^n \int_{t_{j-1}}^{t_j} \left[f_{j-1} + \frac{f_j - f_{j-1}}{\Delta t} (t - t_{j-1}) \right] \sin \omega t \, dt \\ &= \frac{f_0}{\omega} - \frac{f_n}{\omega} \cos \omega t_n + \frac{2}{\omega^2 \Delta t} \sin \frac{\omega \Delta t}{2} \sum_{j=1}^n (f_j - f_{j-1}) \cos \omega \left(t_{j-1} + \frac{\Delta t}{2} \right). \quad (112) \end{aligned}$$

Then for

$$G(\omega) = \frac{L[A(t)]}{L[B(t)]}$$

and two pointwise functions, $A(t_j)$ and $B(t_j)$, we define

$$R'_{N_k} = \text{real part of the numerator of } G(\omega)$$

$$I'_{N_k} = \text{imaginary part of the numerator of } G(\omega)$$

$$R'_{D_k} = \text{real part of the denominator of } G(\omega)$$

$$I'_{D_k} = \text{imaginary part of the denominator of } G(\omega).$$

Then, by noting that

$$\frac{f(t_n)}{i\omega} (e^{-i\omega t_n} - 1) = \frac{f(t_n)}{\omega} [-\sin \omega t_n + i(1 - \cos \omega t_n)] \quad (113)$$

and by employing Equations (104), (105), (106), (111), and (112),

$$R'_{N_k} = \frac{2}{\omega_k^2 \Delta t} \sin \frac{\omega_k \Delta t}{2} \sum_{j=1}^n (A_j - A_{j-1}) \sin \omega_k (t_{j-1} + \frac{\Delta t}{2}) \quad (114)$$

$$I'_{N_k} = \left\{ -\frac{A_0}{\omega_k} + \frac{2}{\omega_k^2 \Delta t} \sin \frac{\omega_k \Delta t}{2} \sum_{j=1}^n (A_j - A_{j-1}) \cos \omega_k (t_{j-1} + \frac{\Delta t}{2}) \right\} \quad (115)$$

$$R'_{D_k} = \frac{2}{\omega_k^2 \Delta t} \sin \frac{\omega_k \Delta t}{2} \sum_{j=1}^n (B_j - B_{j-1}) \sin \omega_k (t_{j-1} + \frac{\Delta t}{2}) \quad (116)$$

and

$$I'_{D_k} = \left\{ -\frac{B_0}{\omega_k} + \frac{2}{\omega_k^2 \Delta t} \sin \frac{\omega_k \Delta t}{2} \sum_{j=1}^n (B_j - B_{j-1}) \cos \omega_k (t_{j-1} + \frac{\Delta t}{2}) \right\} \quad (117)$$

Multiplying the numerator and denominator of $G(\omega)$ [ie, Equations (114), (115), (116), and (117)] by

$$-\frac{\omega_k^2 \Delta t}{2 \sin \frac{\omega_k \Delta t}{2}}$$

$G(\omega_k)$ may be written with the real and imaginary parts of the numerator and denominator as follows:

$$R_{N_k} = \sum_{j=1}^n (A_j - A_{j-1}) \sin \omega_k (t_{j-1} + \frac{\Delta t}{2}) \quad (118)$$

$$I_{N_k} = \frac{A_0 \omega_k \Delta t}{2 \sin \frac{\omega_k \Delta t}{2}} + \sum_{j=1}^n (A_j - A_{j-1}) \cos \omega_k (t_{j-1} + \frac{\Delta t}{2}) \quad (119)$$

$$R_{D_k} = \sum_{j=1}^n (B_j - B_{j-1}) \sin \omega_k \left(t_{j-1} + \frac{\Delta t}{2} \right) \quad (120)$$

and

$$I_{D_k} = \frac{B_0 \omega_k \Delta t}{2 \sin \frac{\omega_k \Delta t}{2}} + \sum_{j=1}^n (B_j - B_{j-1}) \cos \omega_k \left(t_{j-1} + \frac{\Delta t}{2} \right) \quad (121)$$

The function $G(\omega_k)$ may now be computed from

$$G(\omega_k) = \frac{R_{N_k} + i I_{N_k}}{R_{D_k} + i I_{D_k}} \quad (122)$$

For cases in which the unilateral Fourier integral of a single function, $A(t)$, rather than the ratio of two integrals is desired, an option is provided so that

$$R_{D_k} = - \frac{\omega_k^2 \Delta t}{2 \sin \frac{\omega_k \Delta t}{2}} \quad (123)$$

and $I_{D_k} = 0$. (See FREQUENCY RESPONSE Control Card: ratio control, page 54.)

Note that this option is equivalent to an input in which $B(t)$ is the unit impulse function (or delta function).

4.3 Error Analysis and Criteria

Due to the nature of the assumptions and approximations made in the development of the FREQUENCY RESPONSE program, the output is subject to error; and some care must be exercised in the use of the program if meaningful results are to be obtained. This section is devoted to (a) a discussion of the various errors which may occur, (b) the development of criteria for determining bounds on the errors, and (c) the development of means whereby the errors may be minimized. The errors which may occur in the output of FREQUENCY RESPONSE can be divided into three categories.

- (1) Errors due to round-off in the computer
- (2) Errors due to truncation of the function, $f(t)$, with the assumption that $f(t) = f(t_n)$ for $t \geq t_n$
- (3) Errors arising from the representation of $f(t)$ in the interval $0 \leq t \leq t_n$ by a sequence of straight lines.

Each type error is treated separately below.

4.31 Round-off Error. In this program, certain integrals are evaluated by numerical processes; and the possibility, therefore, exists that the error due to round off of numerical quantities may accumulate and become significant. To test the program for errors of this type, use has been made of the following theorem: (Proofs of all theorems are given in Appendix A.)

THEOREM I: If $f(t) = f(t_n - t)$ in the interval $0 \leq t \leq t_n$ and zero elsewhere and if

$$F(\omega) = \int_0^{\infty} f(t) e^{-i\omega t} dt \quad (124)$$

then for

$$\omega = (2m - 1)\pi/t_n$$

(m an integer) the real part of $F(t)$ is zero and for

$$\omega = 2m\pi/t_n$$

the imaginary part of $F(t)$ is zero.

From Theorem I it follows that if the hypothesis of the theorem is satisfied so that the real or imaginary part of the unilateral Fourier transform is zero, then the value of the real or imaginary part of the transform as computed by FREQUENCY RESPONSE is the absolute round-off error. Two test problems have been run in order to evaluate the round-off error. In each test, data points were arranged to satisfy the hypothesis of Theorem I. In Test Problem 1, frequencies were selected such that $\omega = (2m - 1)\pi/t_n$. As shown on page 30, the real part obtained is essentially zero. Similarly, in Test Problem 2, frequencies were selected such that $\omega = 2m\pi/t_n$; and the imaginary part obtained is essentially zero, as shown on page 31. These results indicate that error due to round-off is negligible in this program.

4.32 Truncation Error. In order to obtain an exact evaluation of the unilateral Fourier transform of a function, $f(t)$, the function must be known for all $t \geq 0$. In practical problems the function $f(t)$ is never known for all time, and some approximation is required. In the FREQUENCY RESPONSE program it has been assumed that for $t \geq t_n$, $f(t) = f(t_n)$, ie, the function is truncated at t_n and assumed constant thereafter. Hence, if $f(t_n)$ is not in fact equal to $f(t)$ when $t > t_n$, some error must be expected in the results given by FREQUENCY RESPONSE. The nature of the error resulting from truncation is given by the following theorem and its corollaries: (Proofs are given in Appendix A.)

THEOREM II:

Let
$$F(\omega) = \int_0^{\infty} f(t) e^{-i\omega t} dt .$$

$$f^*(t) = f(t) \text{ for } 0 \leq t \leq t_n$$

$$f^*(t) = f(t_n) \text{ for } t > t_n$$

then

$$F(\omega) - F^*(\omega) = \int_{t_n}^{\infty} [f(t) - f(t_n)] e^{-i\omega t} dt . \quad (125)$$

Corollary 1:
$$|F(\omega) - F^*(\omega)| \leq \int_{t_n}^{\infty} |f(t) - f(t_n)| dt . \quad (126)$$

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TEST PROBLEM ONE FOR FREQUENCY RESPONSE

RECORD NO 444449003 CHANNEL 3 NUMERATOR WAS WORD 1

FREQUENCIES IN CPS

FREQUENCY	LOG W	REAL G(IW)	IMAG. G(IW)	MAG. G	PHASE ANGLE	20 LOG(MAG. G)
0.5000	-0.301	8.6456467E-05	-5.1602150E 01	5.1602149E 01	-89.99990463	34.2533560
1.5000	0.176	3.8600274E-05	-1.9111872E 00	1.9111872E 00	-89.99884415	5.6260645
2.5000	0.398	1.8169063E-05	-4.1281453E-01	4.1281453E-01	-89.99747849	-7.6849006
5.5000	0.740	3.7220438E-06	-3.8767978E-02	3.8767978E-02	-89.99450302	-28.2305374
7.5000	0.875	1.9717948E-06	-1.5288522E-02	1.5288522E-02	-89.99261475	-36.3126903
9.5000	0.978	1.1921578E-06	-7.5225215E-03	7.5225215E-03	-89.99092484	-42.4727311
14.5000	1.161	5.3867123E-07	-2.1153061E-03	2.1153061E-03	-89.98541260	-53.4925356
19.5000	1.290	1.7688884E-07	-8.6949405E-04	8.6949406E-04	-89.98834610	-61.2146688
24.5000	1.389	1.7638720E-07	-4.3832581E-04	4.3832584E-04	-89.97694397	-67.1640587
29.5000	1.470	1.2222332E-07	-2.5099536E-04	2.5099538E-04	-89.97210312	-72.0066853
39.5000	1.597	6.8442393E-08	-1.0448620E-04	1.0448622E-04	-89.96247101	-79.6188202
49.5000	1.695	3.2656957E-08	-5.3022265E-05	5.3022275E-05	-89.96471405	-85.5108328
59.5000	1.775	2.9752275E-08	-3.0507418E-05	3.0507432E-05	-89.94412613	-90.3118868
69.5000	1.842	1.2397946E-08	-1.9090617E-05	1.9090621E-05	-89.96279144	-94.3835993
79.5000	1.900	1.8401851E-08	-1.2735394E-05	1.2735407E-05	-89.91721344	-97.8997440
99.5000	1.998	1.6762870E-08	-6.4757601E-06	6.4757817E-06	-89.85168838	-103.7741575

CALCULATIONS REQUIRED 1 MIN 34.8 SEC

TOTAL PROBLEM TIME WAS 3 MIN 6.8 SEC

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TEST PROBLEM TWO FOR FREQUENCY RESPONSE

RECORD NO 444449003 CHANNEL 3 NUMERATOR WAS WORD 1

FREQUENCIES IN CPS

FREQUENCY	LOG W	REAL G(IW)	IMAG. G(IW)	MAG. G	PHASE ANGLE	20 LOG(MAG. G)
1.0000	-0.000	-2.0264149E 01	6.4875532E-05	2.0264149E 01	-180.00018120	26.1345675
2.0000	0.301	-5.0660414E 00	6.7583003E-06	5.0660414E 00	-180.0007439	14.0933748
3.0000	0.477	-2.2515695E 00	2.1101175E-06	2.2515695E 00	-180.0005150	7.0497073
6.0000	0.778	-5.6289249E-01	4.9901540E-09	5.6289249E-01	-179.9999809	-4.9914908
8.0000	0.903	-3.1662709E-01	-1.5826264E-07	3.1662709E-01	-179.99996948	-9.9890387
10.0000	1.000	-2.0264128E-01	-1.0645052E-07	2.0264128E-01	-179.99996758	-13.8654418
15.0000	1.176	-9.0062792E-02	-1.3396287E-07	9.0062791E-02	-179.99991417	-20.9090919
20.0000	1.301	-5.0660339E-02	-7.9316752E-08	5.0660338E-02	-179.99990845	-25.9066386
25.0000	1.398	-3.2422619E-02	-9.9581325E-08	3.2422618E-02	-179.99982071	-29.7830386
30.0000	1.477	-2.2515687E-02	-7.6169123E-08	2.2515687E-02	-179.99980354	-32.9502964
40.0000	1.602	-1.2665081E-02	-4.7837641E-08	1.2665081E-02	-179.99978256	-37.9478407
50.0000	1.699	-8.1056552E-03	-5.7173657E-08	8.1056551E-03	-179.99959373	-41.8242373
60.0000	1.778	-5.6289322E-03	-4.7825430E-08	5.6289321E-03	-179.99950981	-44.9914799
70.0000	1.845	-4.1355295E-03	-2.4348635E-08	4.1355295E-03	-179.99966049	-47.6693778
80.0000	1.903	-3.1662633E-03	-2.6159365E-08	3.1662633E-03	-179.99952316	-49.9890599
100.0000	2.000	-2.0264188E-03	-2.3338057E-08	2.0264187E-03	-179.99933815	-53.8654165

CALCULATIONS REQUIRED 1 MIN 34.8 SEC

TOTAL PROBLEM TIME WAS 2 MIN 18.1 SEC

Corollary 2: If $\phi(\omega)$ and $\phi^*(\omega)$ are the phase angles of $F(\omega)$ and $F^*(\omega)$, respectively, then

$$|\sin(\phi - \phi^*)| \leq \frac{\int_{t_n}^{\infty} |f(t) - f(t_n)| dt}{|F^*(\omega)|} \quad (127)$$

Corollaries 1 and 2 give, respectively, the limits on the gain and phase error due to truncation. It is apparent that these errors may be minimized by selecting $f(t_n)$ such that

$$\int_{t_n}^{\infty} |f(t) - f(t_n)| dt$$

is minimized. Hence, in order to ensure that the truncation error is small or to determine the limits on the error resulting from truncation, some knowledge of the behavior of $f(t)$ for $t > t_n$ is necessary. For most practical cases the behavior of $f(t)$ for $t > t_n$ can be approximated, and the errors due to truncation can be estimated by Corollaries 1 and 2.

In a number of practical cases, the function, $f(t)$, ultimately decays in an exponential manner to a final value. For this rather common case, the errors due to truncation are given by the following corollary to Theorem II.

Corollary 3: If, for $t \geq t_n$,

$$f(t) = \frac{f(t_n) - f(\infty)}{m} \sum_{k=1}^m e^{-\alpha_k (t-t_n)} + f(\infty) \quad (128)$$

and

$$f^*(t) = f(t_n)$$

then

$$|F(\omega) - F^*(\omega)| = \frac{|f(t_n) - f(\infty)|}{m} \left[\left(\sum \frac{\alpha_k}{\alpha_k^2 + \omega^2} \right)^2 + \left(\frac{m}{\omega} - \sum \frac{\omega}{\alpha_k^2 + \omega^2} \right)^2 \right]^{1/2} \quad (129)$$

If coefficients, α_k , can be found which adequately describe the real function, $f(t)$, and a reasonable estimate for $f(\infty)$ is available, this corollary can be applied directly to data. This, however, is generally not the case; for if these parameters were known, a better estimate of $f^*(t)$ would have been made originally. The usefulness of this corollary, then, lies in the fact that for extreme values of ω ($\omega \rightarrow 0$ and $\omega \rightarrow \infty$) the ratio $|F - F^*|/|F^*|$ (and consequently $|\sin(\phi - \phi^*)|$) varies inversely as $\omega |F^*|$.

For the case where $|F^*|$ approaches a constant as $\omega \rightarrow 0$ (as is the case for a linear system), the error due to truncation will become large for small

values of ω . If answers at small frequencies are desired, the number $f(t_n) - f(\infty)$ must be small. On the other hand, it follows from this corollary that if $|F^*|$ decreases as $1/\omega$ (for $\omega \rightarrow \infty$, $|F^*|$ decreases at 20 dB per decade), then the error due to truncation is constant. At higher rates of decreases for $|F^*|$, the truncation error becomes insignificant. For analyzing power transients such as those recorded from the Spert reactors, one can conclude that truncation error may be of concern for small values of ω , but of no concern otherwise.

To illustrate the nature of the truncation error, the Fourier transforms of the following two functions were computed by means of FREQUENCY RESPONSE.

$$f_1(t) = \begin{cases} e^{-t} & , \quad 0 \leq t \leq 10 \\ 0 & , \quad t > 10 \end{cases} \quad (130)$$

$$f_2(t) = \begin{cases} e^{-t} & , \quad 0 \leq t \leq 5 \\ e^{-5} = 0.00673 & , \quad t > 5 \end{cases} \quad (131)$$

It can easily be shown that the transform of $f_1(t)$ as computed by FREQUENCY RESPONSE is essentially free of truncation error, ie,

$$\int_0^{\infty} f_1(t) e^{-i\omega t} dt \approx \frac{1}{1 + j\omega} \quad (132)$$

For $f_2(t)$, however, Corollary 3 indicated that at $\omega = 10^{-1}$,

$$F_1(\omega) - F_2(\omega) = 0.067 = 0.56 \text{ db} \quad (133)$$

and

$$|\psi_1 - \phi_2| \leq 3.90 \quad (134)$$

At $\omega = 10^{-2}$,

$$|F_1(\omega) - F_2(\omega)| = 0.67 = 4.4 \text{ db} \quad (135)$$

and

$$|\phi_1(\omega) - \phi_2(\omega)| \leq 42^\circ \quad (136)$$

Thus, the phase error due to truncation should be evident for $\omega \geq 10^{-1}$, and the magnitude error should be evident for $\omega \geq 10^{-2}$. This is illustrated in Figures 7 and 8.

In summary, the principal effect of truncation of the function, $f(t)$, is to produce a low frequency error in the unilateral Fourier transform. This error can be minimized by minimizing

$$\int_0^{\infty} |f(t_n) - f(\infty)| dt \quad .$$

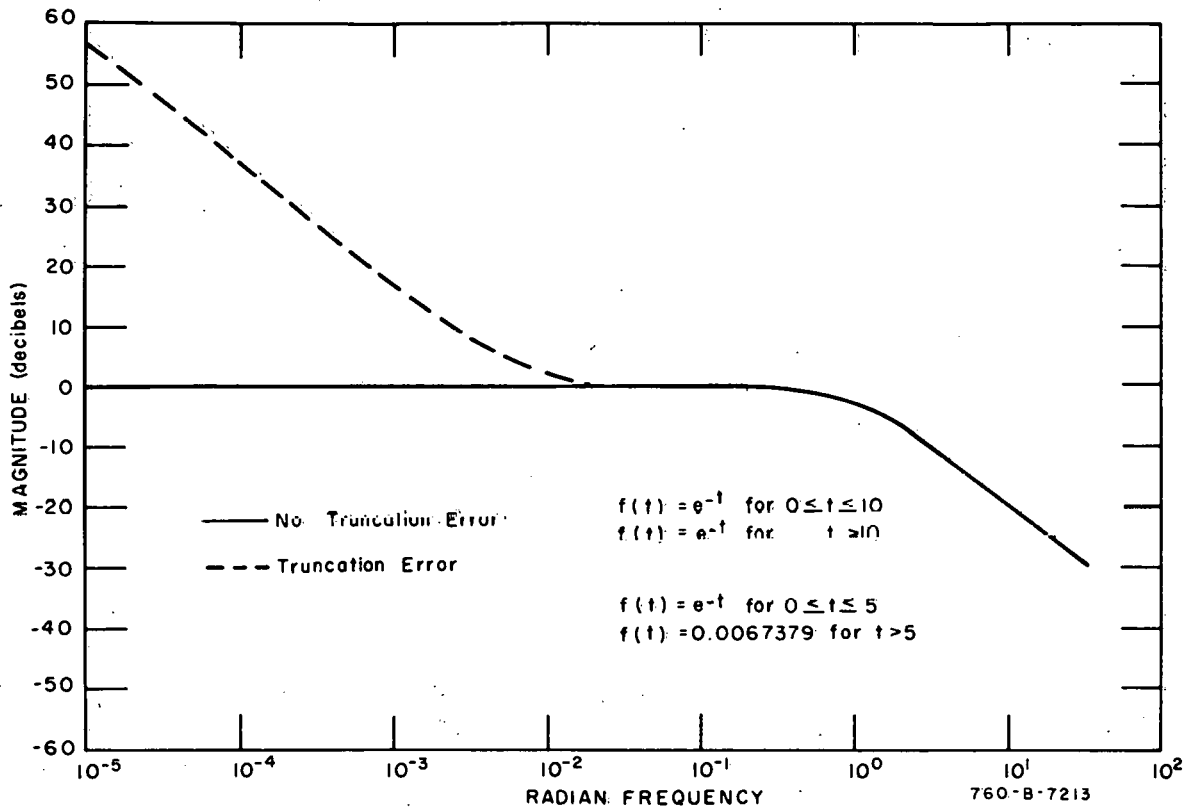


Fig. 7 Magnitude of transform as computed by FREQUENCY RESPONSE to demonstrate round-off error.

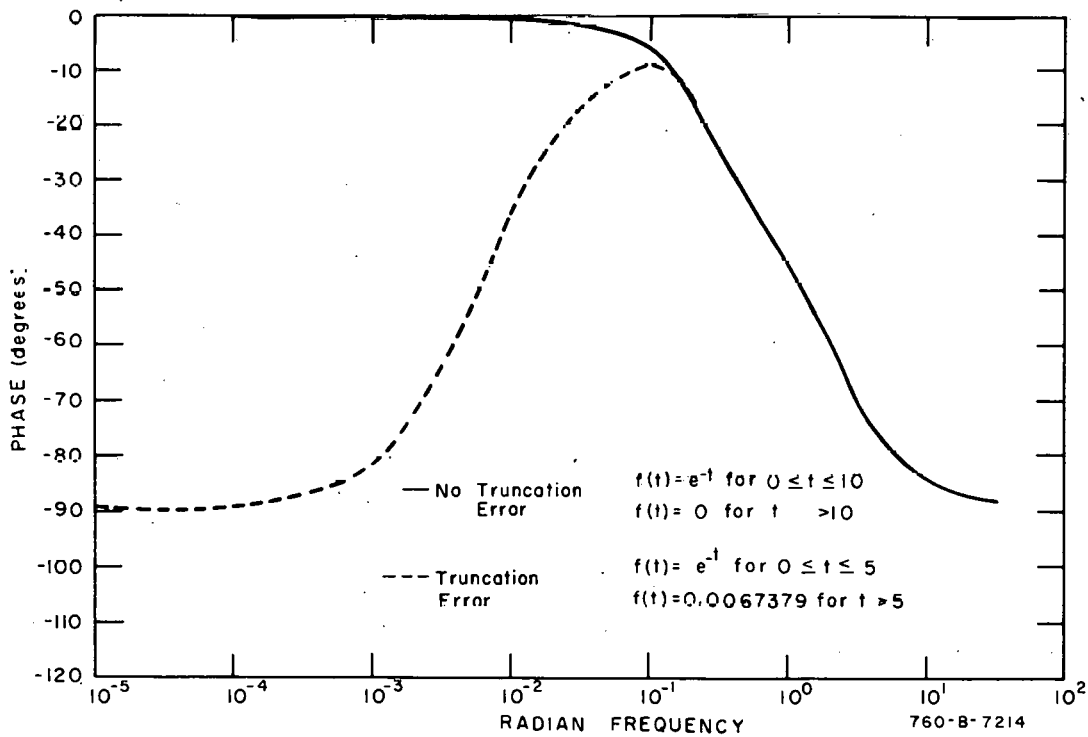


Fig. 8 Phase of transform as computed by FREQUENCY RESPONSE to demonstrate round-off error.

If care is used in selecting $f(t_n)$, the truncation error can usually be made negligible in the frequency range of interest.

4.33 Error Resulting from Straight Line Approximation to the Input Functions. In the input to FREQUENCY RESPONSE, each function for which the unilateral Fourier transform is desired is represented by a set of points of the form, $[t_j, f(t_j)]$. For convenience in evaluating the integrals, it is assumed in the program that the variation of the input function between successive points is linear; ie, the set of points is connected by a sequence of straight lines. The Fourier transform computed, therefore, is that of a sequence of straight lines and is exact to within the numerical accuracy of the computer. Since the straight line frequency is usually not the desired function but an approximation of the function, some error is present in the resultant transform. In general, if $f(t)$ is the desired function and $f^*(t)$ is an approximation of $f(t)$, the bounds of the errors in the magnitude and phase of the resultant Fourier transform are given respectively by Theorems III and IV. (Proofs appear in Appendix A.)

THEOREM III:

Let

$$F(\omega) = \int_0^{t_n} f(t) e^{-i\omega t} dt \quad (137)$$

and suppose

$$|f(t) - f^*(t)| \leq \epsilon \text{ for } 0 \leq t \leq t_n \quad (138)$$

If

$$\frac{\epsilon t_n}{|F^*(\omega)|} \leq k \quad (139)$$

then

$$\frac{|F(\omega) - F^*(\omega)|}{|F^*(\omega)|} \leq k \quad (140)$$

THEOREM IV:

Let

$$F(\omega) = \int_0^{t_n} f(t) e^{-i\omega t} dt$$

and let ϕ be the phase of $F(\omega)$. Suppose

$$|f(t) - f^*(t)| \leq \epsilon \text{ for } 0 \leq t \leq t_n \quad (141)$$

If

$$\frac{\epsilon t_n}{|F^*(\omega)|} \leq k \quad (141)$$

then

$$|\sin(\phi - \phi^*)| \leq k \quad (142)$$

In addition of Theorems III and IV, one may also apply the following theorem and its corollaries to determine the bounds of the error.

THEOREM V:

Let

$$F(\omega) = \int_0^{t_n} f(t) e^{-\omega t} dt .$$

Suppose that

$$f(0) = f^*(0) \text{ and } f(t_n) = f^*(t_n)$$

and that on $(0, t_n)$, the i^{th} derivatives of $f(t)$ and $f^*(t)$ are continuous for all $i < m$ and that the m^{th} derivative is sectionally continuous. If

$$\left| \frac{d^m}{dt^m} [f(t) - f^*(t)] \right| \leq \epsilon_m \text{ on } (0, t_n) \quad (143)$$

then

$$\begin{aligned} \frac{\left| |F(\omega)| - |F^*(\omega)| \right|}{|F^*(\omega)|} &\leq \sum_{j=1}^{m-1} \frac{1}{\omega^{j+1} |F^*(\omega)|} \left| \frac{d^j}{dt^j} [f(t) - f^*(t)] \right|_0^{t_n} \\ &+ \frac{\epsilon_m t_n}{\omega^m |F^*(\omega)|} \end{aligned} \quad (144)$$

$$\begin{aligned} |\sin(\phi) - \sin(\phi^*)| &\leq \sum_{j=1}^{m-1} \frac{1}{\omega^{j+1} |F^*(\omega)|} \left| \frac{d^j}{dt^j} [f(t) - f^*(t)] \right|_0^{t_n} \\ &+ \frac{\epsilon_m t_n}{\omega^m |F^*(\omega)|} \end{aligned} \quad (145)$$

Because of the difficulty in determining ϵ_n , application of Theorem V is generally practical only for $m=1$. For this case, Theorem V can be written in a simplified form.

Let

$$F(\omega) = \int_0^{t_n} f(t) e^{-\omega t} dt$$

and suppose that $f(0) = f^*(0)$ and $f(t_n) = f^*(t_n)$.

If

$$\left| \frac{d}{dt} [f(t) - f^*(t)] \right| \leq \epsilon$$

then

$$\frac{|F(\omega) - F^*(\omega)|}{|F^*(\omega)|} \leq \frac{\epsilon t_n}{\omega |F^*(\omega)|} \quad (146)$$

and

$$|\sin(\phi - \phi^*)| \leq \frac{\epsilon t_n}{\omega |F^*(\omega)|} \quad (147)$$

In certain cases, the bounds on the errors as given by the corollaries to Theorem V may be smaller in some frequency ranges than the bounds given by Theorems III and IV. Therefore, both of the above methods should be applied wherever possible in order to minimize the estimated error. The following examples demonstrate the use of the above theorems and corollaries to determine the envelope within which the transform, F , must lie.

To demonstrate the effect of various time steps and, consequently, various errors in the straight line approximations, four test problems are given below. The function

$$\begin{aligned} f(t) &= e^{-2t} - e^{-4t} \quad \text{for } 0 \leq t \leq 10 \\ f(t) &= 0 \quad \text{for } t > 10 \end{aligned} \quad (148)$$

was approximated by the method described in Section II-4.2 using time steps of 0.5, 0.25, 0.1, and 0.025. Plots of the magnitude of the results are given in Figures 9 through 12.

To apply Theorem III, the maximum difference between $f(t)$ and $f^*(t)$ must be known. For a time step of 0.1, the maximum error in this case can be determined to be 0.1; ie,

$$|f - f^*| < 0.1 \quad (149)$$

Therefore, since

$$\left| \frac{|F|}{|F^*|} - 1 \right| \leq \frac{|F - F^*|}{|F^*|} \quad (150)$$

from Theorem III,

$$\left| \frac{|F|}{|F^*|} - 1 \right| \leq \frac{0.1}{|F^*|} \quad (151)$$

or

$$20 \log \left(1 - \frac{0.1}{|F^*|} \right) \leq 20 \log \frac{|F|}{|F^*|} \leq 20 \log \left(1 + \frac{0.1}{|F^*|} \right) \quad (152)$$

A plot of the envelope is given in Figure 11.

To apply Theorem V, the maximum difference between the derivatives of $f(t)$ and $f^*(t)$ must be known. For a time step of 0.1, this maximum difference can be determined to be 0.27. Therefore, from Theorem V,

$$\left| \frac{|F|}{|F^*|} - 1 \right| \leq \frac{2.7}{\omega |F^*|} \quad (153)$$

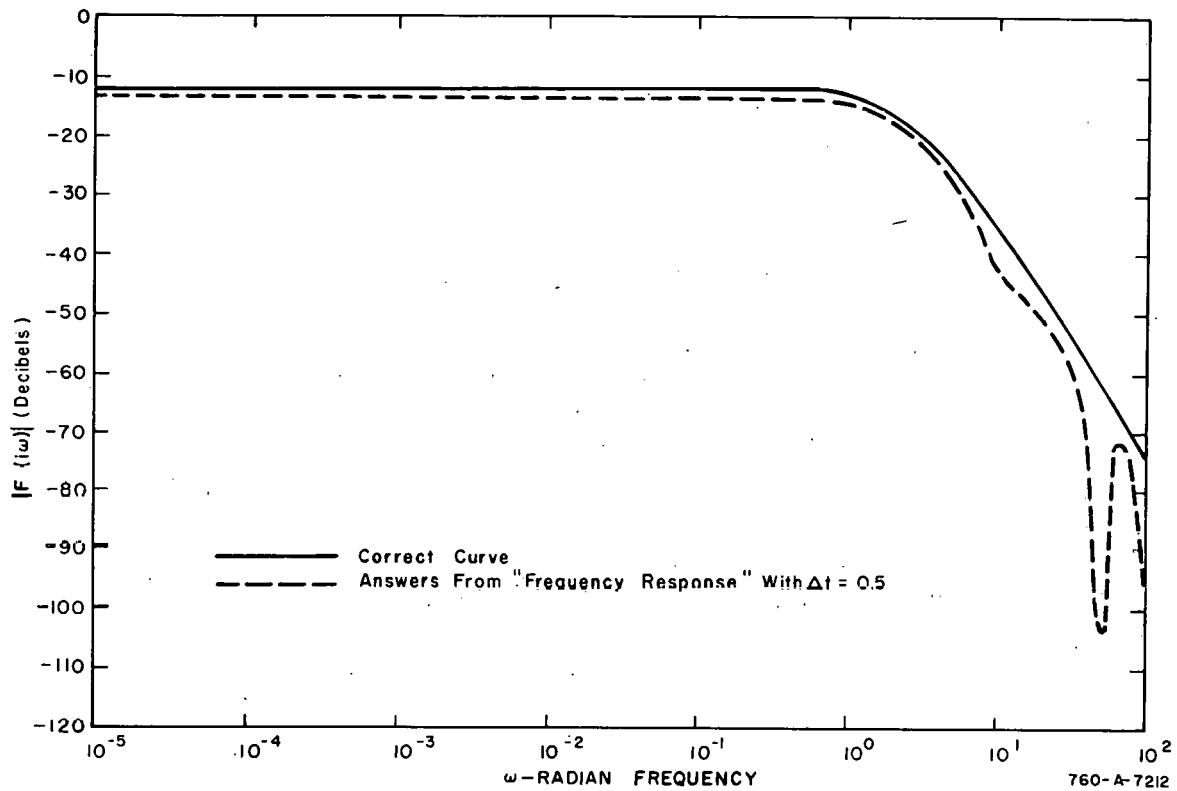


Fig. 9 Magnitude of transform as computed by FREQUENCY RESPONSE to demonstrate effect of Δt ($\Delta t = 0.5$).

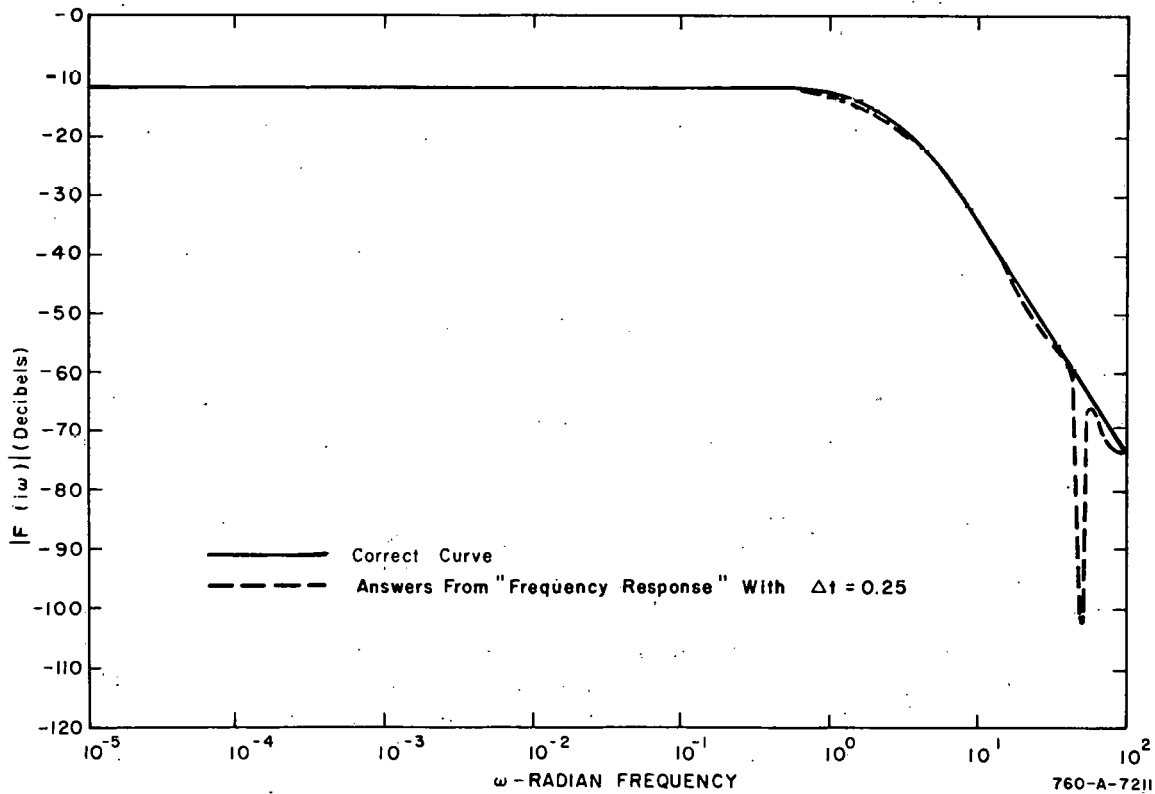


Fig. 10 Magnitude of transform as computed by FREQUENCY RESPONSE to demonstrate effect of Δt ($\Delta t = 0.25$).

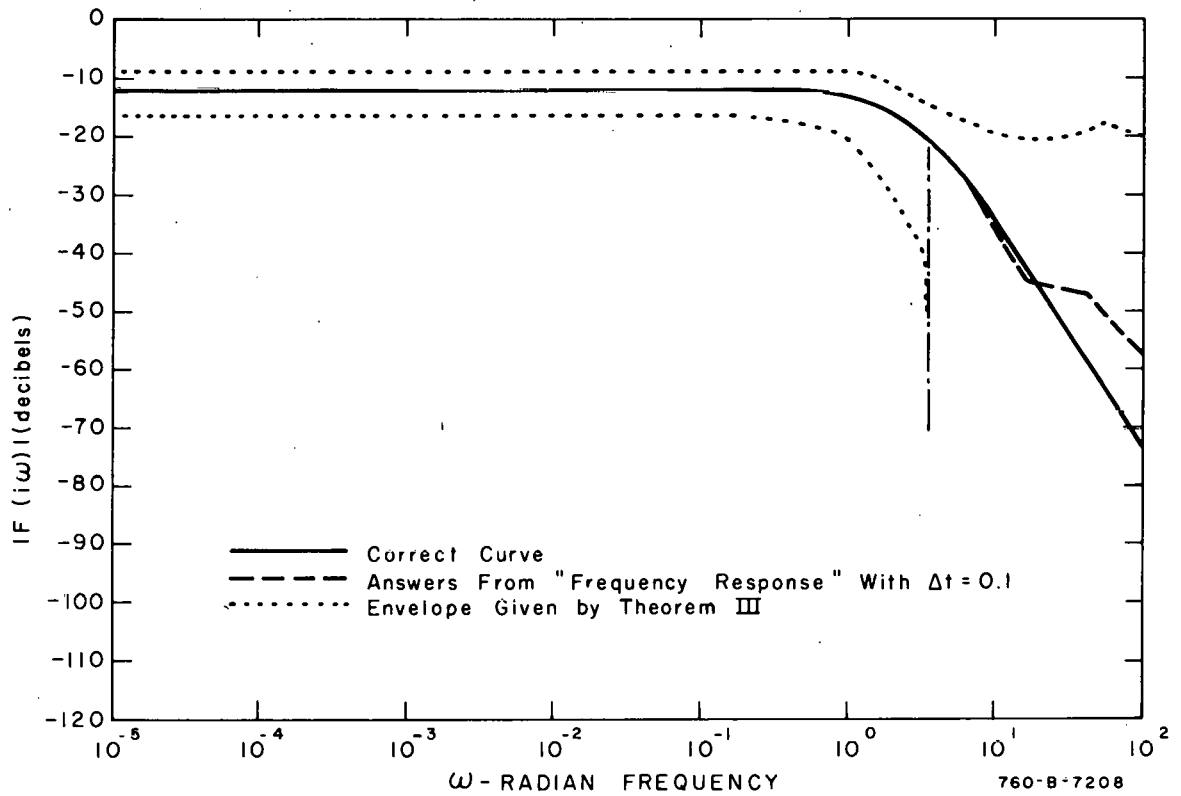


Fig. 11 Magnitude of transform as computed by FREQUENCY RESPONSE and error envelope to demonstrate effect of Δt ($\Delta t = 0.1$).

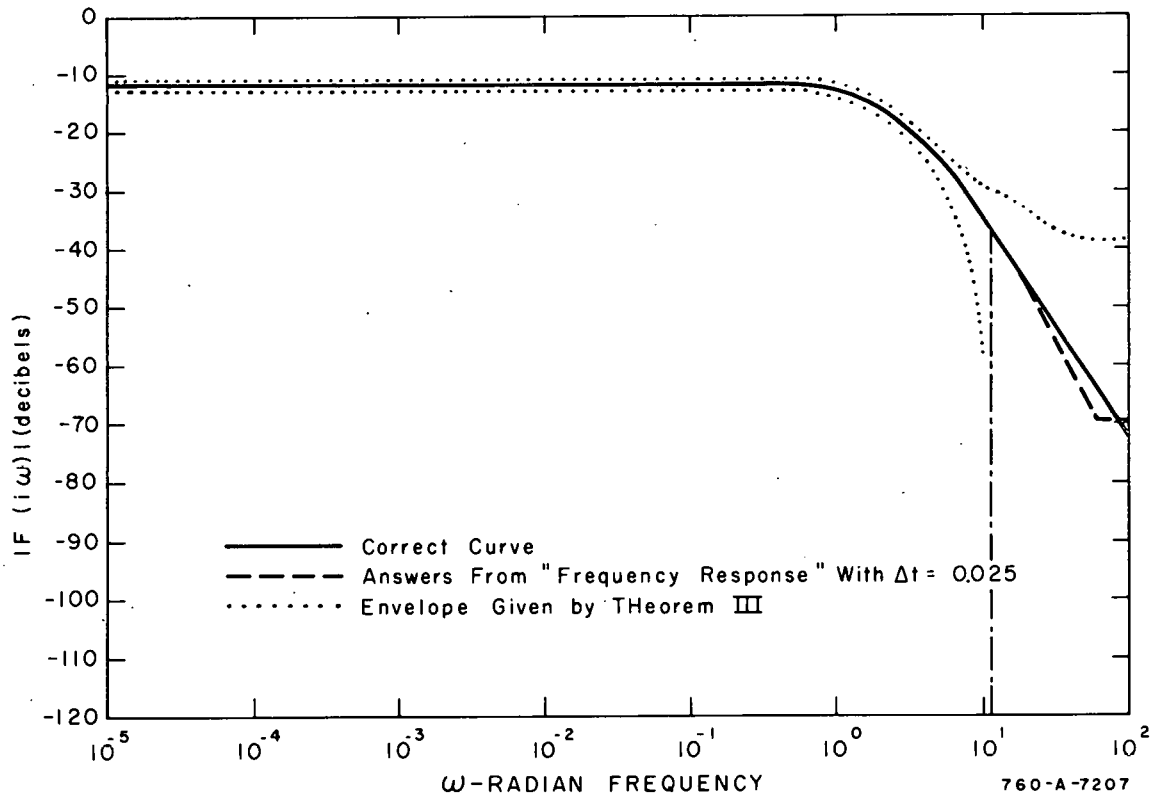


Fig. 12 Magnitude of transform as computed by FREQUENCY RESPONSE and error envelope to demonstrate effect of Δt ($\Delta t = 0.025$).

For this particular test problem, the upper limit of the error as given by Theorem III is smaller for values of $\omega < 27$ than that given by Theorem V. Practically, nothing is gained by using Theorem V, and the envelope shown in Figure 11 was calculated using Theorem III exclusively. The envelope calculated for the case of $t = 0.025$ is shown in Figure 12 and is, as would be expected, somewhat smaller than that obtained for $t = 0.1$. As indicated by the example, for a reasonably well-behaved function, the error criteria are overly restrictive. This is to be expected from the general nature of the theorems.

To summarize, the errors in the output of FREQUENCY RESPONSE due to straight line approximation are unavoidable in this program. However, the actual transform lies within the envelope determined by Theorems III, IV, and V and their corollaries; and the size of the envelope can be reduced by reducing the time increment (and consequently $|f - f^*|$) of the input data.

4.34 Error in the Ratio of Two Functions. The discussion above has been restricted to the transform of a single function; ie, the case

$$f(\omega) \doteq \int_0^{\infty} f(t) e^{-i\omega t} dt$$

However, the error analysis may be extended to the ratio of two transforms by applying the criteria developed. Following the notation scheme used in the above discussion, let

$A(s)$ = exact transform of the numerator, $a(t)$

$B(s)$ = exact transform of the denominator, $b(t)$

$A^*(s)$ = transform of $a(t)$ calculated by FREQUENCY RESPONSE

$B^*(s)$ = transform of $b(t)$ calculated by FREQUENCY RESPONSE

From Equations (139) and (140),

$$||A| - |A^*|| \leq \epsilon_A t_n = \delta_A \quad (154)$$

and

$$||B| - |B^*|| \leq \epsilon_B t_n = \delta_B \quad (155)$$

Then

$$- \delta_A \leq |A| - |A^*| \leq \delta_A \quad (156)$$

so that

$$|A^*| - \delta_a \leq |A| \leq |A^*| + \delta_A \quad (157)$$

and

$$- \delta_B \leq |B| - |B^*| \leq \delta_B \quad (158)$$

so that

$$|B^*| - \delta_B \leq |B| \leq \delta_B + |B^*| \quad (159)$$

It follows that

$$\frac{|A^*| - \delta_a}{|B^*| + \delta_b} - \frac{|A^*|}{|B^*|} \leq \frac{|A|}{|B|} - \frac{|A^*|}{|B^*|} \leq \frac{|A^*| + \delta_a}{|B^*| - \delta_b} - \frac{|A^*|}{|B^*|} \quad (160)$$

This expression can be reduced to

$$-\frac{\frac{|A^*|}{|B^*|} \delta_b + \delta_a}{|B^*| + \delta_b} \leq \frac{|A|}{|B|} - \frac{|A^*|}{|B^*|} \leq \frac{\frac{|A^*|}{|B^*|} \delta_b + \delta_a}{|B^*| - \delta_a} \quad (161)$$

The output from FREQUENCY RESPONSE in this case will be A^*/B^* . To determine an error envelope, an additional run must be made to determine $|B^*|$. The quantities δ_a and δ_b are equal to ϵ_{At_n} and ϵ_{Bt_n} , respectively. [See Equation (138) for definition of ϵ .] Using these values and Equation (161), an error envelope can be calculated.

The error in the calculated phase can be determined in a similar manner. From Equation (142) it is seen that, for a single integral, the phase error has the form

$$|\sin(\phi - \phi^*)| \leq K \quad (162)$$

Following the notation defined on page 40, the phase of A^*/B^* is

$$\phi^* = \phi_A^* - \phi_B^*$$

(ϕ_A^* is the phase of A^*); and the phase error is

$$\phi - \phi^* = \phi_A - \phi_B - (\phi_A^* - \phi_B^*) = (\phi_A - \phi_A^*) - (\phi_B - \phi_B^*) \quad (163)$$

As before, it is convenient to consider

$$\sin(\phi - \phi^*)$$

rather than $(\phi - \phi^*)$. Note that

$$\begin{aligned} \sin(\phi - \phi^*) &= \sin(\phi_A - \phi_A^*) \cos(\phi_B - \phi_B^*) \\ &\quad - \cos(\phi_A - \phi_A^*) \sin(\phi_B - \phi_B^*) \end{aligned} \quad (164)$$

and

$$|\sin(\phi - \phi^*)| \leq |\sin(\phi_A - \phi_A^*)| + |\sin(\phi_B - \phi_B^*)| \leq k_A + k_B \quad (165)$$

where, by Theorem IV,

$$k_A \geq \frac{\epsilon_{At_n}}{|A^*|}$$

and

$$k_B \geq \frac{\epsilon_{Bt_n}}{|B^*|}$$

Thus,

$$|\sin (\phi - \phi^*)| \leq \left(\frac{1}{|B^*|} \frac{|B^*|}{|A^*|} \epsilon_A t_n + \epsilon_B t_n \right) \quad (166)$$

Again, to find the maximum error envelope, an additional run is required to determine $|B^*|$.

This argument has been made by applying Theorem III. It should be noted that a similar argument could be made using Theorem V. Application of Theorem V will result in the replacement of ϵ_A and ϵ_B by $\frac{\epsilon_m A}{\omega}$ and $\frac{\epsilon_m B}{\omega}$ throughout the above discussion. (See Theorem V; page 36, for the definition of ϵ_m .)

III. INPUT FORMAT

1. INTRODUCTION

The data preparation routines and the three major programs SMOOTH, REACTIVITY, and FREQUENCY RESPONSE of SPORT may be used either separately or in sequence to process data recorded either on tape or on cards. Due to the various ways data may be processed, it is necessary that a number of options be made available to the user. These options, the necessary control cards, and the control card sequence are described in this section.

Subsection 2 of this section, Data System Options, is subdivided into five major parts: (a) Description of types of data which may be processed; (b) Options available in the Data Preparation phase of SPORT; (c) Options available in SMOOTH; (d) Options available in REACTIVITY; and (e) Options available in FREQUENCY RESPONSE. Options discussed in each part include input options, processing options, and output options.

Subsection 3, System Control Cards, is subdivided into two major parts: (a) general control cards and (b) program control cards. The type of data to be processed, the initial data preparation and output of raw or prepared data, and the major programs to be applied to the data are specified with the general control cards. Processing by the major programs (including output options) is controlled by the program control cards.

Subsection 4, Card Sequence, is a description of the cards which must be used and the proper sequence for processing data.

If it is desired to use the various plotting options described in this chapter, SPORT must be adopted to the digital plotting facilities available.

The routine "PLOT" supplied in binary form in the standard SPORT program deck will generate plot tapes for use on an IBM-1401 Computer with attached CALCOMP (California Computing Products Company) series 500 incremental digital plotter.

This PLOT routine should be replaced by an equivalent routine which will perform the functions assigned to PLOT in the CALCOMP plotting manual "SCOOP" and which will produce plot tapes in the proper form. The entry point "FINI" in PLOT should close out and unload the plot tape.

2. DATA SYSTEM OPTIONS

2.1 Types of Data That May Be Processed

2.11 Type 0 Data: Card Data Output From SMOOTH to be entered into REACTIVITY or card output from REACTIVITY to be entered into FREQUENCY RESPONSE.

2.12 Type 1 Data: Card Data In Spert 1-3 Form. The format of Spert 1-3 data is as follows: A 10-digit integer identification number in Columns 1

through 10, a 6-digit integer time value in Columns 13 through 18, and as many as six 3-digit integer data values in Columns 26 through 28, 36 through 38, , 76 through 78, with the signs of the data values being in Columns 29, 39, , 79. Data values not used may be left completely blank but a data value that is used may not contain blank columns.

2.13 Type 2 Data: Card Data In 650 Floating-Point Form with a 10-digit integer identification number in Columns 1 through 10. The time value must be in columns 11 through 20 and the 1 to 6 data channel values in Columns 20 through 30, 31 through 40, , 71 through 80, all in 650 floating-point form.

2.14 Type 3 Data: Type 2 Data With a Sign Over-Punched In Column 10.

2.15 Type 3 Data: Card Data To Be Read In Under A Specified Format.

Each data card must have an integer identification number and a time value, in that order, preceding the first data value. A maximum of six data channels per card may be used. With these restrictions, data in any form which can be described by a single-precision FORTRAN format statement may be read into the system.

2.16 Type 5 Data: Data stored on a magnetic tape in 2000-point, 2021-word, FORTRAN Type 3 records. (See IBM 7040 Programmer's Guide: FORTRAN Files.) The 15th word in each record may be an integer number indicating the order of the records on the tape. The 17th word in each record must be an integer identification number, the 18th word the initial time, and the 19th word the time increment between successive data points in the record. The 20th through 2019th words in each record must contain the 2000 data values. A "channel" of Type 5 data on a magnetic tape may consist of any number of 2000-point data records with the same identification number logically arranged on the tape in order of increasing time. In Appendix C, an example is given of the type of scheme that should be used to convert data to SPORT Type 5 data. Appendix C contains a listing of a program which may be used to generate Type 5 data.

2.17 Data Time Sequence. The SPORT data cards (data Types 1, 2, 3 and 4) must be arranged in order of increasing time. No two data cards may have the same time value.

2.2 Options Available in the Data Preparation Phase

2.21 Input Options. Data Types 1, 2, 3, 4, and 5 may be used as input in the Data Preparation phase of SPORT.

2.22 Processing Options.

(1) Data Normalization. Each channel of data used in a problem may be individually normalized according to the following scheme.

Normalized time value = (original time value times normalizing coefficient for time) + time shift.

Normalized data value = (original data value times normalizing coefficient for data) + data shift.

(2) Data Compositing. The normalized data channels used in a problem may be combined into a single "composite" data channel during data preparation.

(3) Logarithmic Conversion. The normalized data to be used in a problem may be converted into natural logarithmic form during data preparation.

2.23 Output Options.

(1) Data listing and card output. The prepared data may be listed in decimal form. In addition, the prepared data may be punched out on IBM cards, one data value per card, in exponential and normalized decimal form.

(2) Plots of prepared data. The prepared data may be plotted in semilog or linear form.

2.3 Options Available in the SMOOTH Program

2.31 Input Options. Data Types 1, 2, 3, 4 and 5. Data which is to be smoothed for use in the REACTIVITY program must be in natural logarithmic form.

2.32 Processing Options. Input data may be smoothed on any odd number of points from 3 to 99 inclusive. One set of data may be resmoothed as many as 9 times. It should be noted that if the input data are separated by equal time increments and if the output values have this same time increment, the time required to smooth a set of data will be reduced by approximately one-third.

2.33 Output Options. The SMOOTH output listing and SMOOTH output cards are optional. A binary output tape for use as input to other programs is optional. Linear or semilog plots of coefficient C and linear plots of coefficient B are optional. Plot size, scaling, and range of data plotted may be designated.

2.4 Options Available in the REACTIVITY Program

2.41 Input Options. Input to the REACTIVITY program may be in two forms: (a) input data which are processed in sequence by the SMOOTH and REACTIVITY programs or (b) direct card input.

2.42 Processing Options. Up to 50 delayed neutron groups may be used. Initial delayed neutron precursor concentrations may be read in or calculated by the program. The initial energy may be read in or calculated and a neutron source term may be specified.

2.43 Output Options. The REACTIVITY output listing and output cards are optional. Plots of power, reactivity, and energy are optional. Form (linear or semilog), size, scaling, and range of data plotted may be designated.

2.5 Options Available in the FREQUENCY RESPONSE Program

2.51 Input Options. Input to the FREQUENCY RESPONSE program may be in several forms: (a) input data processed in sequence by the REACTIVITY and FREQUENCY RESPONSE programs, (b) input data processed in sequence by the SMOOTH and FREQUENCY RESPONSE programs, (c) Type 5 (tape) data, or (d) direct card input.

2.52 Processing Options. Frequencies may be entered in rad/sec or in cps. The transform of a single data trace or the ratio of transforms of two data traces may be calculated. The input data may be multiplied by an exponential function of time. Two traces of input data may be smoothed and then processed simultaneously, one as the numerator and the other as the denominator in the ratio of transforms. Alternately, the difference between data values in the two traces may be calculated, and the transform of this difference used as the numerator and the transform of one of the two channels as the denominator in the ratio of transforms.

2.53 Output Options. Card output and plots of the magnitude and phase of the FREQUENCY RESPONSE output are optional.

3. SYSTEM CONTROL CARDS

The system control cards may be divided into two categories: (a) general control cards and (b) program control cards. The general control cards serve to initiate processing while the program control cards control the actual processing of the data with the various programs.

3.1 General Control Cards

3.11 PART Card. The PART card serves to (a) designate the programs that will be applied to the data and (b) to control the data preparation portion of the processing.

(1) Column 1: Basic Processing Scheme.

- | | |
|----------------|--|
| Blank or zero: | Data preparation only (as described under DATA SYSTEMS OPTIONS, Sub-section 2.2). |
| One: | Data preparation and SMOOTH. |
| Two: | Data preparation, SMOOTH and REACTIVITY. REACTIVITY results are then available (in the computer) as input to FREQUENCY RESPONSE (see column 2 below). |
| Three: | Data preparation and SMOOTH. SMOOTH results are then available (in the computer) as input to FREQUENCY RESPONSE (see column 2 below). |
| Four: | Direct card input (no preparation) into REACTIVITY. REACTIVITY results are then available (in the computer) as input to FREQUENCY RESPONSE (see column 2 below). |
| Five: | Case 1 -- For data Types 0, 2, 3 and 4: direct card input (no preparation) to FREQUENCY RESPONSE. Case 2 -- For |

data Type 5: Data preparation. The prepared data is then available as input to FREQUENCY RESPONSE.

(2) Column 2: Processing with Frequency Response. (Column 2 has significance only if a 2, 3, 4, or 5 is entered in Column 1.)

Blank or zero: No processing with FREQUENCY RESPONSE.

One: Data will be processed with FREQUENCY RESPONSE.

(3) Column 3: Data Type (as described in Subsection 2).

(4) Columns 4, 5, and 6: Number of data Channel Sections to be Used in the Problem. If each channel section is to be processed separately as indicated by Columns 1 and 2, this number must be positive. If the channel sections are to be composited into a single data curve and then processed, this number must be negative.

(5) Column 7: Output of Data Before Processing with Principal Programs.

Blank or zero: No data output.

One: Listing of prepared data.

Two: Listing and card output of prepared data.

(6) Column 8: Logarithmic Conversion

Blank or zero: Input data will remain in original form.

One: Natural logarithm of normalized input data will be processed.

(7) Column 9: Reserved for Additional Options. Should be left blank.

(8) Column 10: Plots of Data before Processing with Principal Programs.

Blank or zero: No plots.

One: 10- by 7-inch semilog plots.
(10-inch abscissa, 7-inch ordinate)

Two: 10- by 7-inch linear plots.
(10-inch abscissa, 7-inch ordinate)

(A two should be entered if the data were originally in logarithmic form.)

(9) Columns 11 through 72: Problem Title. Used to head each page in the problem output and to title all normalized data plots.

3.12 CHANNEL Card. The purpose of the CHANNEL card is to control the selection and normalization of a section from a single channel of input data. If a composite data channel is to be formed during data preparation, the CHANNEL card must also specify the position of the section in the composite channel.

(1) Columns 1 through 10: Channel Identification Number. Card data (Types 1 through 4): Columns 1 through 9 are left blank, and the channel number of the data to be processed is entered in Column 10. The channel number of data in word three on the data cards is 1, that of word four is 2, and so on up to a maximum of 6 channels per card. Tape data (Type 5). Columns 1 through 10 must contain the identification number that is stored in the 17th word of the data record.

(2) Columns 11 through 30: (Floating point) Time range in which data are to be made available for processing.

Minimum time: Columns 11 through 20 (assumed zero if left blank).

Maximum time: Columns 21 through 30 (assumed 10^{30} if left blank).

(3) Columns 31 through 50: (Floating point) Normalizing Coefficient as defined by Equation (1). (Applied before correctional shifts entered in Columns 51 through 70.)

Normalizing coefficient for time: Columns 31 through 40. (Assumed one if left blank.)

Normalizing coefficient for data: Columns 41 through 50. (Assumed one if left blank.)

(4) Columns 51 through 70: (Floating point) Correctional Shifts as defined by Equation (1). (Applied to normalized time and data values.)

Time shift: Columns 51 through 60. (Assumed zero if left blank.)

Data shift: Columns 61 through 70. (Assumed zero if left blank.)

(5) Columns 71 through 74: Data Reel Number (Type 5 data only). If the reel number of the data tape is known, it should be entered on the first CHANNEL Card. If not, Columns 71 through 74 should be left blank, and the data tape will be called for by the Channel Identification Number on the first CHANNEL Card.

(6) Columns 75 through 78: File Index Number (Type 5 data only). The index number (word 15 in a SPORT Type 5 data record) may be entered if it is necessary to distinguish between several data records with the same identification number.

3.13 FORMAT Card. The purpose of the FORMAT card is to specify how Type 4 data values (see Subsection 2.1) are arranged on the data cards.

(1) Column 1: The number of data channel values per card.

(2) Columns 2 through 80: A single-precision FORTRAN format statement, excluding the word "FORMAT". This format statement must describe the form and arrangement of the identification number, time value, and 1 to 6 data channels.

3.14 END-OF-DATA Card. The purpose of the END-OF-DATA card is to indicate that the preceding card was the last card in the data deck. It is simply a blank card.

3.15 INPUT Card. The purpose of the INPUT card is to identify card data which is to be read directly into the REACTIVITY or FREQUENCY RESPONSE subroutines.

(1) Columns 1 through 10: Identification Number on the data cards.

(2) Columns 11 through 20: (Floating point) Time Increment between successive data cards.

3.16 CONTINUE Card. The purpose of the CONTINUE card is to indicate that at the completion of the current problem, processing is to continue on a new problem. This card contains *CONTINUE starting in Column 1.

3.17 STOP Card. The purpose of the STOP card is to indicate that at the completion of the current problem, processing is to stop and that the plot tape is to be closed out and unloaded. This card contains *STOP starting in Column 1.

3.2 Program Control Cards

3.21 SMOOTH TITLE Card. The purpose of the SMOOTH TITLE Card is to title and identify the SMOOTH output. It may contain any characters in column 2 through 80.

3.22 SMOOTH CONTROL Card. The purpose of the SMOOTH CONTROL Card is to control the processing done by SMOOTH.

(1) Columns 1 through 10: Identification Number of the Data.

(2) Columns 11 through 20: (Floating point) Time Step between Output Points.

(3) Columns 21 through 40: (Floating point) Time Range. Data at time values less than the value listed in Columns 21 through 30 will be ignored.

(4) Columns 41 through 60: (Floating point) Time for First SMOOTH Calculation. Columns 41 through 50 contain the value (on the input data time scale) at which the first SMOOTH calculation will be made. If this value is left blank (or is too small), the minimum possible time value will be used. Columns 51 through 60 contain the value that will be given to the first point in the output data. If the value in Columns 41 through 50 is reset, the value in Columns 51 through 60 will also be reset to maintain the same shift.

(5) Columns 61 through 62: Number of Points on which to Smooth. (May be any odd number from 3 to 99, inclusive.)

(6) Column 63: Output Control.

- 0: Listing
- 1: Listing and cards
- 3: No listing or card output.

(7) Column 64: Type of Plot.

- 0: No plots
- 1: Semilog plot of coefficient C.
- 2: Linear plot of coefficient C.
- 3: Semilog plot of coefficient C with a linear plot of coefficient B superimposed.
- 4: Linear plot of coefficient C with a linear plot of coefficient B superimposed.

(8) Column 65: Form of Data to be Plotted.

- 0: Data is log-base-e.
- 2: Data is linear.

(9) Column 66: Plot Size and Scaling Control. A non-zero integer in Column 66 indicates that a SMOOTH Plot Scaling Card will follow the SMOOTH Control Card.

(10) Column 68: Number of Smoothing Passes to be made. If Column 68 is left blank, one pass will be made. All the available data that lies in the time range specified in Columns 21 through 40 will be smoothed in preliminary passes. All the SMOOTH output options will be suppressed until the final pass.

(11) Column 69: Binary Tape Output. (May be ignored if binary tape is not desired.)

1: Binary tape will be rewound before writing.

2: Binary tape will not be rewound before writing.

(12) Column 70: Binary Tape Unload. A non-zero integer in Column 70 will cause the binary tape to unload. The last data record on the tape will be followed by a record with its first word set to 2000000002 and then an end-of-file mark.

3.23 SMOOTH PLOT SCALING Card: The purpose of the SMOOTH PLOT SCALING Card is to provide various sizes of SMOOTH plots. (See Column 66, SMOOTH CONTROL Card.)

(1) Columns 1 through 20: (Floating point) Abscissa Scaling. (Optional; must be in linear form.)

1 through 10: Minimum value on abscissa.

11 through 20: Maximum value on abscissa.

(2) Columns 21 through 40: (Floating point) Ordinate Scaling. (Optional; must be in linear form for a linear plot or log-base-10 form for a semilog plot.)

21 through 30: Minimum value on ordinate.

31 through 40: Maximum value on ordinate.

(3) Columns 41 through 60: (Floating point) Scaling Coefficient B. (Optional; must be in linear form.)

41 through 50: Minimum value on B axis.

51 through 60: Maximum value on B axis.

(4) Columns 61 through 64: Plot Size (Optional; assumed 10-inch abscissa, 7-inch ordinate if left blank.)

61 through 62: Length of abscissa in inches (Minimum 3-inches, maximum 99-inches).

63 through 64: Length of ordinate in inches (Minimum 3-inches, maximum 26-inches).

3.24 REACTIVITY TITLE Card. The purpose of the REACTIVITY TITLE Card is to identify output from REACTIVITY. It may contain any characters in Columns 2 through 80.

3.25 REACTIVITY CONTROL Card. The purpose of the REACTIVITY CONTROL Card is to control input and output procedures and supply certain basic parameters.

(1) Columns 1 through 10: (Floating point) Δ/β . (See definitions page 18).

(2) Columns 11 through 20. (Floating point) α ; The Initial Reciprocal Period.

(3) Columns 21 through 22. The Number of Delayed Neutron Groups.

(4) Column 23. Initial Precursor Concentrations

0: REACTIVITY calculates concentrations.

1: Concentrations to be furnished as input.

(5) Column 24. Output Control

0: Listing of output.

1: Listing and card output.

3: No listing or card output.

(6) Column 25. Initial Energy

0: Initial energy will be calculated.

1: Initial energy will be supplied in Columns 31 through 40.

(7) Columns 26 through 28. Plot Control. In each column, a 1 indicates a semilog plot while a 2 indicates a linear plot of the corresponding parameter.

Column 26: Linear power.

Column 27: Reactivity.

Column 28: Energy.

(8) Column 29. Plot Size and Scaling Control. A non-zero integer indicates that a REACTIVITY PLOT SCALING Card will follow the REACTIVITY Control Card.

(9) Columns 31 through 40. (Floating point) Initial Energy (see Column 25).

(10) Columns 41 through 50. (Floating point) Source Term (must be entered in units of power per unit time).

3.26 REACTIVITY PLOT SCALING Card. The purpose of the REACTIVITY PLOT SCALING Card is to provide various size plots of the output from REACTIVITY.

(1) Columns 1 through 10. (Floating point) Abscissa Scaling in Power Plot. (Optional, may be left blank.)

1 through 5: Minimum abscissa value.

6 through 10: Maximum abscissa value.

(2) Columns 11 through 20. (Floating point) Ordinate Scaling in Power Plot. (Optional; must be in linear form for a linear plot; or log-base-10 form for a semilog plot.)

11 through 15: Minimum ordinate value.

16 through 20: Maximum ordinate value.

(3) Columns 21 through 24. Plot Size for Power Plot. (Assumed 10-inch abscissa, 7-inch ordinate if left blank.)

21 through 22: Length of abscissa in inches. (minimum 3-inches, maximum 99-inches).

23 through 24: Length of ordinate in inches (minimum 3-inches, maximum 26-inches).

(4) Columns 26 through 35. (Floating point) Abscissa Scaling in Reactivity Plots (Optional).

26 through 30: Minimum abscissa value.

31 through 35: Maximum abscissa value.

(5) Columns 36 through 45. (Floating point) Ordinate Scaling in Reactivity Plots. (Optional; form must agree with that of the plot.)

36 through 40: Minimum ordinate value.

41 through 45: Maximum ordinate value.

(6) Columns 46 through 49. Plot Size for Reactivity Plot. (Assumed 10-inch abscissa, 7-inch ordinate if left blank.)

46 through 47: Length of abscissa in inches (minimum 3-inches, maximum 99-inches).

48 through 49: Length of ordinate in inches (minimum 3-inches, maximum 26-inches).

(7) Columns 51 through 60. (Floating point) Abscissa Scaling in Energy Plots (optional).

51 through 55: Minimum abscissa value.

56 through 60: Maximum abscissa value.

(8) Columns 61 through 70. (Floating point) Ordinate Scaling in Energy Plots. (Optional; form must agree with that of the plot.)

61 through 65: Minimum ordinate value.

66 through 70: Maximum ordinate value.

(9) Columns 71 through 74. Plot Size for Energy Plots. (Assumed 10-inch abscissa, 7-inch ordinate if left blank.)

71 through 72: Length of abscissa in inches (minimum 3-inches, maximum 99-inches).

73 through 74: Length of ordinate in inches (minimum 3-inches, maximum 26-inches).

3.27 LAMBDA Card. (Floating point) The purpose of the LAMBDA Card is to enter the decay constants of the delayed neutron groups. The decay constants are entered, eight per card, in ten column fields.

3.28 F Card. (Floating point) The purpose of the F Card is to enter the values of f_i for each delay group. The values of f_i are entered eight per card in ten column fields.

3.29 W Card. (Floating point) The purpose of the W Card is to enter the initial values of W_i if this option is chosen. (See Column 23 of the REACTIVITY CONTROL Card.) The values of W_i (see definitions, page 18) are entered eight per card in ten column fields.

3.210 FREQUENCY RESPONSE TITLE Card. The purpose of the FREQUENCY RESPONSE TITLE Card is to identify the FREQUENCY RESPONSE output. It may contain any characters in Columns 2 through 80.

3.211 FREQUENCY RESPONSE CONTROL Card. The purpose of the FREQUENCY RESPONSE CONTROL Card is to control the options available in this program.

(1) Columns 1 through 3: Number of Frequencies

(2) Column 4: Word [a] which Contains the Numerator.

(3) Column 5: Word [a] which Contains the Denominator.

[a] Significance of numerator and denominator word numbers.

REACTIVITY output

Word 1: linear power
Word 2: reactivity
Word 3: compensated reactivity
Word 4: energy
Word 5: shutdown coefficient (see page 22)

SMOOTH output

Word 1: coefficient C (smoothed data value)
Word 2: coefficient B (slope of smoothed data)
Word 3: coefficient A

Direct card input

Word 1 corresponds to the first data value on the card, word 2 to the second, etc.

(4) Column 6: Ratio Control

- 1: The ratio of the transform of the numerator to the transform of the denominator will be calculated.
- 2: Only the transform of the numerator will be calculated.
- 3: Two data traces are smoothed, and the first run is used as the numerator while the second run is used as the denominator.
- 4: Same as Option 3 except the denominator is first subtracted from the numerator and then the ratio is calculated.

(5) Column 7: Plot Control

- 1: Plot of only the magnitude of the results.
- 2: Plot of both the magnitude and the phase of the results.

(6) Column 8: Card Output

Card output of results is obtained by entering a non-zero integer in Column 8.

(7) Column 9: Units Control

- 0: Frequencies will be entered in radians per second.
- 1: Frequencies will be entered in cycles per second.

(8) Columns 21 through 30: Alpha. If a non-zero, floating point quantity α is entered in Columns 21 through 30, the input values will be multiplied by $\exp(-\alpha t)$.

3.212 OMEGA Card. (Floating point) The purpose of the OMEGA Card is to enter the values of the frequencies at which calculations will be made. These values are entered eight per card in the ten column fields.

4. CARD SEQUENCE

- (1) A PART Card is always the first control card in any problem.
- (2) The CHANNEL Card(s) follow the PART Card. Up to 50 CHANNEL Cards may be used.

For individual processing of several channels of data [a], N, the value entered in Columns 4, 5, and 6 on the PART Card should be positive, and there should be one CHANNEL Card for each channel of data to be processed.

For assembly of the prepared data into a composite channel [a], N, should be negative, and there should be one CHANNEL Card for each section of data to be incorporated in the composite channel. The order of the CHANNEL Cards must be the order in which the sections are to be assembled. Time values on CHANNEL Cards must be in the normalized and shifted time scale and must form a logical sequence. Data may be eliminated by entering a large time shift on the corresponding CHANNEL Card. An INPUT card replaces the set of N CHANNEL Cards in the special case of card data which are to be entered directly into the REACTIVITY or FREQUENCY RESPONSE Program.

(3) FORMAT Card (Type 4 data only).

(4) DATA DECK (data Types 0, 1, 2, 3, and 4)

(5) END-OF-DATA Card (data Types 0, 1, 2, 3, and 4)

(6) Program Control Card Sets. A Program Control Card Set contains either all the Program Control Cards necessary to process one of the N individual channels specified on the CHANNEL Cards or all the Program Control Cards necessary to control the processing of the one composite channel formed during data preparation.

If N (Columns 4, 5, and 6 on PART card) is positive, N sets of Program Control Cards are needed, in the same order as and corresponding to, the N CHANNEL cards.

If N is negative, only one set of Program Control Cards is needed.

(a) SMOOTH Program: The control card sequence necessary to control data smoothing is

SMOOTH Title card

SMOOTH Control Card

SMOOTH Plot Scaling Card (Used only if Column 66 on the SMOOTH Control Card contains a non-zero integer.)

[a] Data Availability

1. Data Types 1, 2, 3 and 4 (card data): Any of the data channels on the data channels on the data cards may be selected on any of the CHANNEL Cards.
2. Data Type 5 (tape data): Any of the data channels stored in the data tape may be selected except those that precede the channel specified on the first CHANNEL Card. The first CHANNEL Card may be a "dummy" that serves only to position the data tape. In this case, the minimum and maximum times entered on the first CHANNEL Card should be the same as the minimum time entered on the second CHANNEL Card.

(b) REACTIVITY Program: The control card sequence necessary to calculate reactivity and energy from SMOOTH data is

REACTIVITY Title Card

REACTIVITY Control Card

REACTIVITY Plot Scaling Card (Used only if Column 29 on the REACTIVITY Control Card contains a non-zero integer.)

LAMBDA Card(s)

F Card(s)

W Card(s) (Used only if Column 23 on the REACTIVITY Control Card is non-zero.)

(c) FREQUENCY RESPONSE Program: The necessary control card sequence is

FREQUENCY RESPONSE Title Card

FREQUENCY RESPONSE Control Card

OMEGA Card(s)

(7) PROBLEM TERMINATION Card (The last card in any problem).

CONTINUE Card: Used if another problem follows the current one.

STOP Card: Used if the current problem is the last one to be processed.

IV. OUTPUT FORMAT

1. INTRODUCTION

The SPORT processing system generates output in four forms: (a) output listings, (b) punched output on cards, (c) CALCOMP computer plots, and (d) output in binary form on tape. In this section, the form and arrangement of output generated by SPORT in the data preparation section and in the SMOOTH, REACTIVITY, and FREQUENCY RESPONSE programs are described.

2. DATA PREPARATION OUTPUT

The PART card and the CHANNEL cards or INPUT card are listed on the first page in the SPORT output (page 59). Next (if called for), is a listing of the input data in final normalized form (page 60). The normalized data is punched on cards in the format:

(I10, 5X, F12.6, 5X, E14.7, 5X, F20.8)

where the first quantity is the identification number, the second the time value, and the third and fourth the data value in exponential and normalized decimal form, respectively.

Figure 13 is an example of a SPORT normalized data plot.

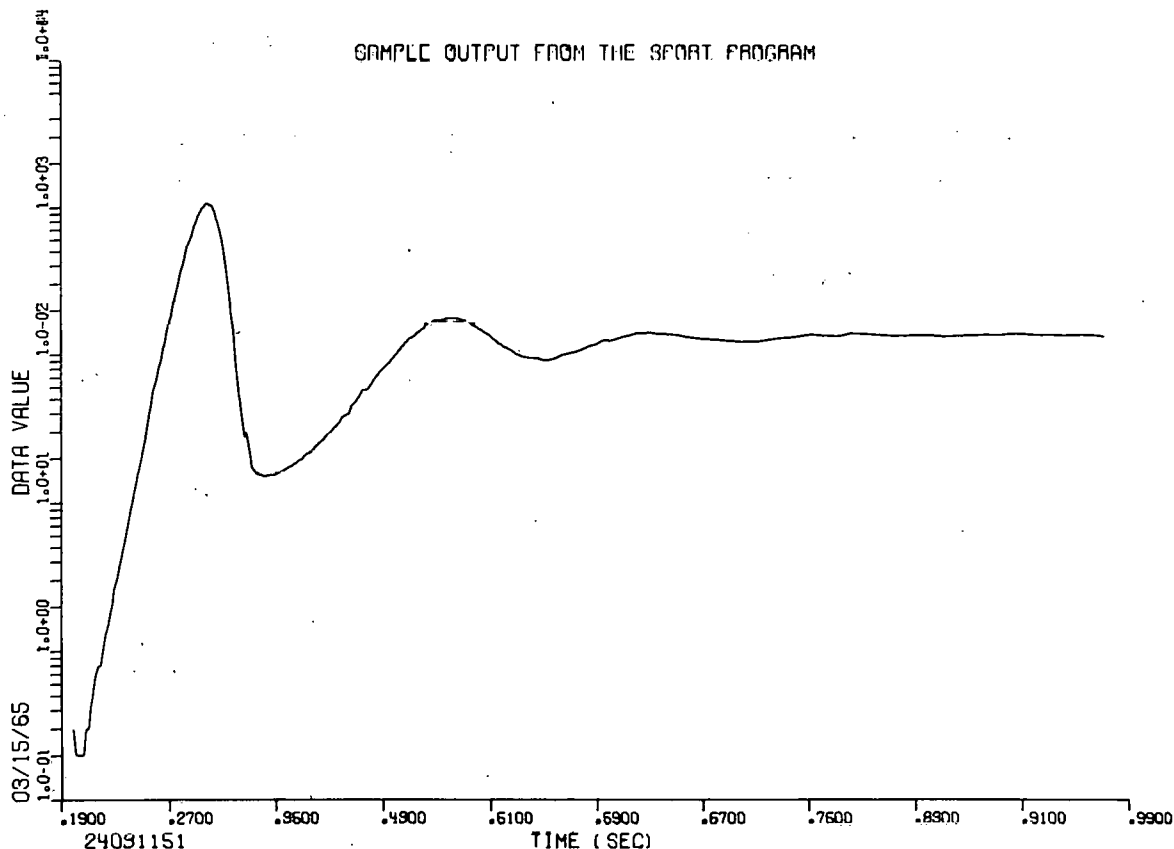


Fig. 13 Plot of power data as prepared by the SMOOTH program.

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SYSTEM FOR PROCESSING REACTOR TRANSIENT DATA

PART CARD WAS 211 -71101

SAMPLE OUTPUT FROM THE SPORT PROGRAM

CHANNEL ID NO	FILE NO (IF ANY)	MINIMUM TIME	MAXIMUM TIME	NORMALIZING COEFFICIENTS TIME	DATA	TIME SHIFT	DATA SHIFT
3	-0	-0.	0.255000	0.000100	1.0000000E-01	-0.	-0.
5	-0	0.255000	0.280000	0.000100	1.0000000E 00	-0.	-0.
6	-0	0.280000	0.313000	0.000100	1.0000000E 01	-0.	-0.
5	-0	0.313000	0.333000	0.000100	1.0000000E 00	-0.	-0.
3	-0	0.333000	0.399000	0.000100	1.0000000E-01	-0.	-0.
5	-0	0.399000	1.023000	0.000100	1.0000000E 00	-0.	-0.
3	-0	1.023000	X.XXXXXX	0.000100	1.0000000E-01	-0.	-0.

NORMALIZED COMPOSITE DATA 24031151

LN(DATA) TAKEN IN INPUT SUBROUTINE

0.200000	-1.204E 00	0.278900	5.838E 00	0.344000	2.728E 00	0.455500	4.942E 00	0.700000	4.812E 00
0.202000	-1.609E 00	0.280100	5.940E 00	0.346500	2.747E 00	0.458000	4.984E 00	0.709800	4.820E 00
0.204100	-1.609E 00	0.281100	6.016E 00	0.348300	2.741E 00	0.460000	5.017E 00	0.719800	4.852E 00
0.205400	-1.609E 00	0.282500	6.109E 00	0.350000	2.747E 00	0.462800	5.081E 00	0.729700	4.875E 00
0.207500	-1.609E 00	0.284000	6.292E 00	0.352600	2.773E 00	0.465100	5.100E 00	0.739600	4.890E 00
0.209300	-1.204E 00	0.286000	6.380E 00	0.354500	2.797E 00	0.468000	5.142E 00	0.749600	4.934E 00
0.211000	-1.204E 00	0.287800	6.492E 00	0.356300	2.815E 00	0.470100	5.159E 00	0.759600	4.913E 00
0.212300	-9.163E-01	0.289200	6.607E 00	0.358200	2.839E 00	0.472500	5.153E 00	0.769900	4.898E 00
0.214000	-6.931E-01	0.290600	6.685E 00	0.360000	2.862E 00	0.475000	5.159E 00	0.780000	4.949E 00
0.216300	-3.567E-01	0.292300	6.791E 00	0.362300	2.890E 00	0.477400	5.182E 00	0.790100	4.942E 00
0.218300	-2.231E-01	0.293600	6.835E 00	0.364000	2.912E 00	0.480100	5.193E 00	0.800000	4.927E 00
0.220000	-2.231E-01	0.294900	6.888E 00	0.366200	2.944E 00	0.483600	5.182E 00	0.810000	4.913E 00
0.222200	9.531E-02	0.296400	6.928E 00	0.368100	2.976E 00	0.487200	5.176E 00	0.820000	4.920E 00
0.223600	2.624E-01	0.297900	6.985E 00	0.370000	2.996E 00	0.490100	5.147E 00	0.830000	4.927E 00
0.225400	4.055E-01	0.299000	6.975E 00	0.371800	3.040E 00	0.494000	5.130E 00	0.840000	4.920E 00
0.227200	5.878E-01	0.299800	6.975E 00	0.373600	3.073E 00	0.497100	5.075E 00	0.850000	4.905E 00
0.228800	7.419E-01	0.300400	6.947E 00	0.375800	3.096E 00	0.500000	5.043E 00	0.860000	4.920E 00
0.230500	9.933E-01	0.301800	6.947E 00	0.378000	3.131E 00	0.505700	4.970E 00	0.870000	4.927E 00
0.232500	1.131E 00	0.302700	6.928E 00	0.379900	3.186E 00	0.510300	4.898E 00	0.880000	4.934E 00
0.234600	1.386E 00	0.303700	6.888E 00	0.382500	3.235E 00	0.515500	4.804E 00	0.890000	4.927E 00
0.236300	1.548E 00	0.304800	6.835E 00	0.384100	3.266E 00	0.520400	4.736E 00	0.900000	4.949E 00
0.238200	1.740E 00	0.306200	6.709E 00	0.385800	3.300E 00	0.525300	4.691E 00	0.910000	4.942E 00
0.239600	1.887E 00	0.307300	6.659E 00	0.388400	3.360E 00	0.530300	4.615E 00	0.920000	4.927E 00
0.241200	2.054E 00	0.308400	6.551E 00	0.389900	3.388E 00	0.535400	4.575E 00	0.930000	4.934E 00
0.242900	2.230E 00	0.309200	6.492E 00	0.392300	3.440E 00	0.540100	4.554E 00	0.940000	4.920E 00
0.244800	2.434E 00	0.310200	6.380E 00	0.394400	3.487E 00	0.545000	4.554E 00	0.950100	4.934E 00
0.246600	2.639E 00	0.311300	6.273E 00	0.396400	3.529E 00	0.550000	4.522E 00	0.960000	4.927E 00
0.247600	2.728E 00	0.312500	6.109E 00	0.398000	3.561E 00	0.554800	4.533E 00	0.970100	4.905E 00
0.248700	2.839E 00	0.313300	5.996E 00	0.400000	3.638E 00	0.559900	4.564E 00	X.XXXXX 0.	
0.250600	3.025E 00	0.315200	5.652E 00	0.403500	3.689E 00	0.565100	4.615E 00		
0.252300	3.199E 00	0.316400	5.460E 00	0.405400	3.689E 00	0.569900	4.635E 00		
0.253100	3.285E 00	0.317700	5.204E 00	0.407600	3.829E 00	0.574900	4.663E 00		
0.254000	3.378E 00	0.319000	4.977E 00	0.410000	3.871E 00	0.580000	4.700E 00		
0.255200	3.526E 00	0.319900	4.736E 00	0.413100	3.970E 00	0.585000	4.754E 00		
0.256400	3.689E 00	0.320900	4.533E 00	0.415400	4.060E 00	0.590100	4.779E 00		
0.257600	3.807E 00	0.323700	3.989E 00	0.417800	4.060E 00	0.595500	4.844E 00		
0.259300	4.043E 00	0.324800	3.829E 00	0.420000	4.094E 00	0.600000	4.828E 00		
0.261000	4.174E 00	0.325700	3.689E 00	0.422800	4.174E 00	0.605200	4.860E 00		
0.262300	4.290E 00	0.326700	3.526E 00	0.425300	4.263E 00	0.610000	4.890E 00		
0.263800	4.454E 00	0.328100	3.332E 00	0.427800	4.331E 00	0.615000	4.920E 00		
0.265100	4.522E 00	0.329200	3.401E 00	0.429900	4.382E 00	0.619900	4.949E 00		
0.266700	4.710E 00	0.330500	3.296E 00	0.432800	4.443E 00	0.625100	4.949E 00		
0.267800	4.796E 00	0.332200	3.045E 00	0.435200	4.489E 00	0.629800	4.956E 00		
0.269200	4.949E 00	0.333600	2.851E 00	0.438000	4.554E 00	0.635100	4.934E 00		
0.270900	5.100E 00	0.335100	2.809E 00	0.440000	4.605E 00	0.639800	4.934E 00		
0.272200	5.209E 00	0.337100	2.754E 00	0.442600	4.682E 00	0.649700	4.920E 00		
0.273600	5.357E 00	0.338600	2.747E 00	0.445200	4.745E 00	0.659700	4.875E 00		
0.275100	5.505E 00	0.339900	2.734E 00	0.448000	4.812E 00	0.669800	4.852E 00		
0.276700	5.631E 00	0.340000	2.734E 00	0.450000	4.860E 00	0.680000	4.844E 00		
0.277900	5.740E 00	0.342000	2.721E 00	0.453500	4.905E 00	0.690000	4.820E 00		

DATA PREPARATION REQUIRED 0 MIN 46.8 SEC AND DATA PLOT REQUIRED 0 MIN 9.8 SEC

3. SMOOTH PROGRAM OUTPUT

The values on the SMOOTH CONTROL Card are listed on the first page in the SMOOTH program output in the same order in which they were entered (page 62). The labels identifying the code words entered in Columns 61 through 70 must be read from top to bottom. If the time at which the first SMOOTH calculation is to be made has to be reset, SMOOTH will print out the corrected value. The identification number, time, and coefficients, C, B, and A, may be listed at each output point, 50 points per page, and punched on cards in the format:

(I10, F16.6, 3F16.7) .

Pages 63 and 64 are examples of the first and last pages in the SMOOTH output listing.

The smoothed data values may be transferred in binary form to a special output tape. This tape contains a number of 400-word, FORTRAN Type 3 records. In the first record, only the first four words are significant. Word one is the integer identification number of the smoothed data; word two is the integer channel number; word three is the time increment in the smoothed data; and word four is the integer number of smoothed data points. The second and succeeding records contain the time value and coefficients, C, B, and A (in that order), for 100 successive data points. All of the 400 words in the last record may not be significant. Appendix C contains a listing of a program which may be used to read the binary tape generated by SMOOTH.

Figure 14 is an example of a SMOOTH output plot of coefficients C and B.

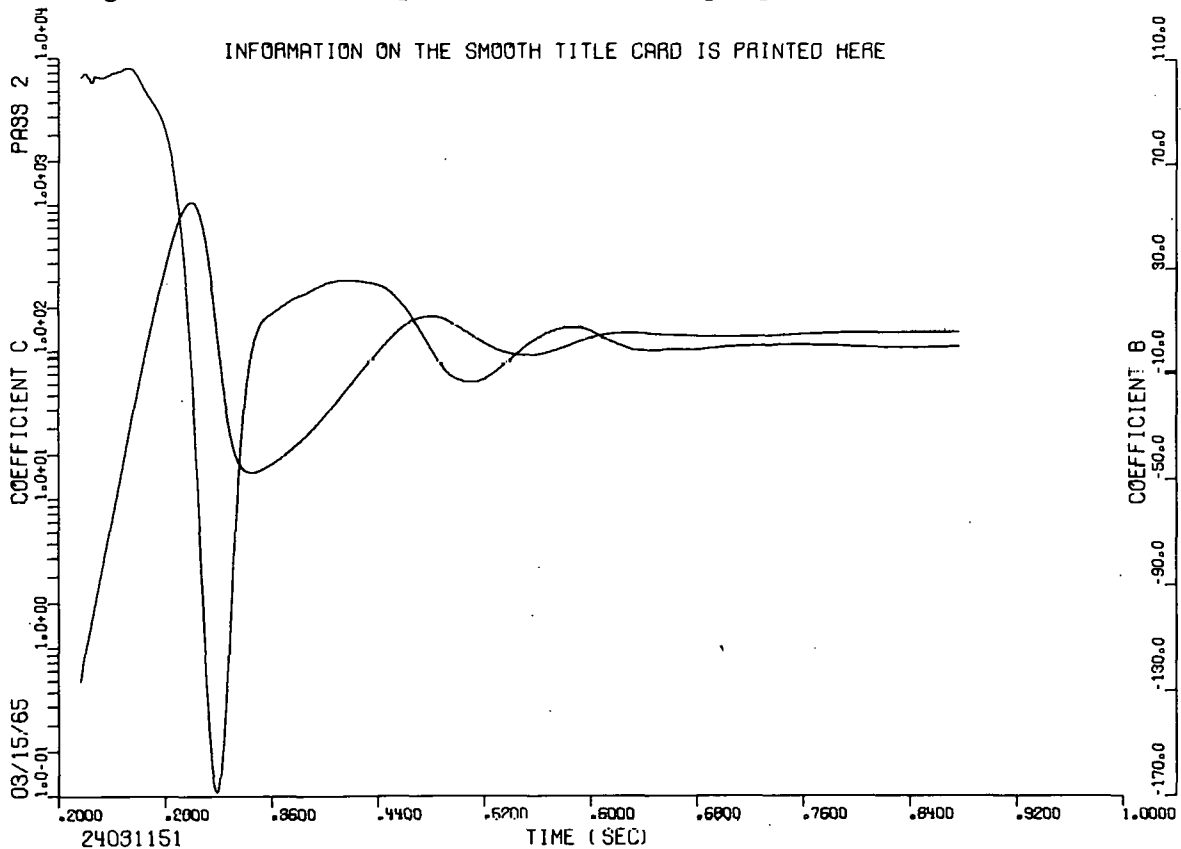


Fig. 14 Plot of power data and slope as prepared by the SMOOTH program.

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SAMPLE OUTPUT FROM THE SPORT PROGRAM

QUADRATIC SMOOTHING PROGRAM

N L S O R T D
U I P D C R E R S
M S L A A D C A M
B T O T L E Y N N
R G T A E R L S T

INFORMATION ON THE SMOOTH TITLE CARD IS PRINTED HERE

PASS NUMBER 1	ID NO	DELTA T	T MINIMUM	T MAXIMUM	T START CAL	1ST OUTPUT T	
SMOOTH CONTROL CARD WAS-	24031151	0.001000	-0.	-0.	-0.	-0.	21 0 300 0 2 00
CONTROL WORDS RESET -					0.217300	0.217300	

CALCULATIONS REQUIRED 0 MIN 7.6 SEC

BEGIN PASS 2

CONTROL WORDS RESET -					0.217300	0.217300	
-----------------------	--	--	--	--	----------	----------	--

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SAMPLE OUTPUT FROM THE SPORT PROGRAM

SMOOTH PROGRAM OUTPUT LISTING FOR CHANNEL 0

ID NUMBER	TIME	C	B	A
24031151	0.217300	-0.4996546	103.1513481	2257.1232910
24031151	0.218300	-0.3399733	103.7023516	874.3408203
24031151	0.219300	-0.2109451	104.1741114	207.8264160
24031151	0.220300	-0.0913869	104.5178101	-239.9172363
24031151	0.221300	0.0237759	104.1818142	-555.6202393
24031151	0.222300	0.1165129	102.7672749	-199.1550903
24031151	0.223300	0.2244377	102.8508348	-376.7765732
24031151	0.224300	0.3146244	101.1550493	74.2547607
24031151	0.225300	0.4124821	100.8328056	189.3391113
24031151	0.226300	0.5147860	101.3788919	143.3051758
24031151	0.227300	0.6272528	103.6343822	-307.3791504
24031151	0.228300	0.7265447	103.0831270	-123.3586426
24031151	0.229300	0.8283663	102.9740791	-68.7431641
24031151	0.230300	0.9295034	102.7939072	10.3012695
24031151	0.231300	1.0298466	102.5432405	115.5253906
24031151	0.232300	1.1313293	102.5753593	164.2382812
24031151	0.233300	1.2327661	102.6138821	216.6264648
24031151	0.234300	1.3353653	102.8016453	221.5419922
24031151	0.235300	1.4384027	103.0311441	216.0673828
24031151	0.236300	1.5427382	103.3143482	163.4516602
24031151	0.237300	1.6479278	103.6170912	85.4482422
24031151	0.238300	1.7522640	103.8473673	58.1206055
24031151	0.239300	1.8569342	104.1073437	26.7661133
24031151	0.240300	1.9621183	104.3871880	-15.6210937
24031151	0.241300	2.0666708	104.5208359	-20.0810547
24031151	0.242300	2.1709748	104.7135792	-5.9042969
24031151	0.243300	2.2748967	104.8554544	33.1259766
24031151	0.244300	2.3787201	104.9985676	83.0644531
24031151	0.245300	2.4825248	105.1213951	139.8642578
24031151	0.246300	2.5862420	105.2268457	205.7871094
24031151	0.247300	2.6909777	105.4858828	233.8730469
24031151	0.248300	2.7971041	105.8095922	212.2128906
24031151	0.249300	2.9039655	106.1084976	171.3818359
24031151	0.250300	3.0110043	106.2774277	133.1093750
24031151	0.251300	3.1184892	106.3675909	80.5078125
24031151	0.252300	3.2261320	106.3934708	23.3906250
24031151	0.253300	3.3339328	106.3542700	-41.1699219
24031151	0.254300	3.4418737	106.2259665	-115.8701172
24031151	0.255300	3.5496849	105.9564419	-193.6962891
24031151	0.256300	3.6573533	105.5618258	-280.0888672
24031151	0.257300	3.7641913	104.9732380	-351.1533203
24031151	0.258300	3.8698580	104.2437353	-399.0292969
24031151	0.259300	3.9749616	103.4585485	-455.6992187
24031151	0.260300	4.0792487	102.5253763	-514.3085937
24031151	0.261300	4.1820185	101.5158148	-548.2050781
24031151	0.262300	4.2831175	100.4835253	-552.6992187
24031151	0.263300	4.3829668	99.5045776	-546.1503906
24031151	0.264300	4.4817572	98.5055304	-536.4394531
24031151	0.265300	4.5791535	97.5833216	-507.1152344
24031151	0.266300	4.6754189	96.7018213	-467.4238281

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SAMPLE OUTPUT FROM THE SPORT PROGRAM

SMOOTH PROGRAM OUTPUT LISTING FOR CHANNEL 0

ID NUMBER	TIME	C	B	A
24031151	0.867300	4.9278864	0.1007919	12.4816895
24031151	0.868300	4.9285777	0.1961441	4.7578125
24031151	0.869300	4.9297699	0.4112244	-6.3645020
24031151	0.870300	4.9299526	0.3952179	-5.7084961
24031151	0.871300	4.9305982	0.4895706	-8.6699219
24031151	0.872300	4.9303113	0.3314590	-4.8402100
24031151	0.873300	4.9304335	0.2890320	-4.0540771
24031151	0.874300	4.9310476	0.3873062	-6.1068115
24031151	0.875300	4.9314288	0.3750916	-6.1068115
24031151	0.876300	4.9317978	0.3628769	-6.1066895

CALCULATIONS REQUIRED 0 MIN 34.4 SEC AND PLOT REQUIRED 0 MIN 25.0 SEC

4. REACTIVITY PROGRAM OUTPUT

The values on the REACTIVITY CONTROL Card are listed on the first page in the REACTIVITY program output in the same order in which they were entered (page 66). The labels identifying the code words entered in columns 21 through 30 must be read from top to bottom. The REACTIVITY PLOT SCALING Card (if used) is listed next, then the LAMBDA cards, the F cards, and, finally, the W cards (if any). The identification number, time, linear power, total reactivity, compensated reactivity, energy, and shutdown coefficient may be listed at each output point, 50 points to a page, and punched on cards in the format:

(I10, F10.6, F12.4, 2F12.6, F12.4, F12.8) .

Pages 67 and 68 are examples of the first and last pages in the REACTIVITY output listing.

Figures 15, 16, and 17 are examples of REACTIVITY output plots.

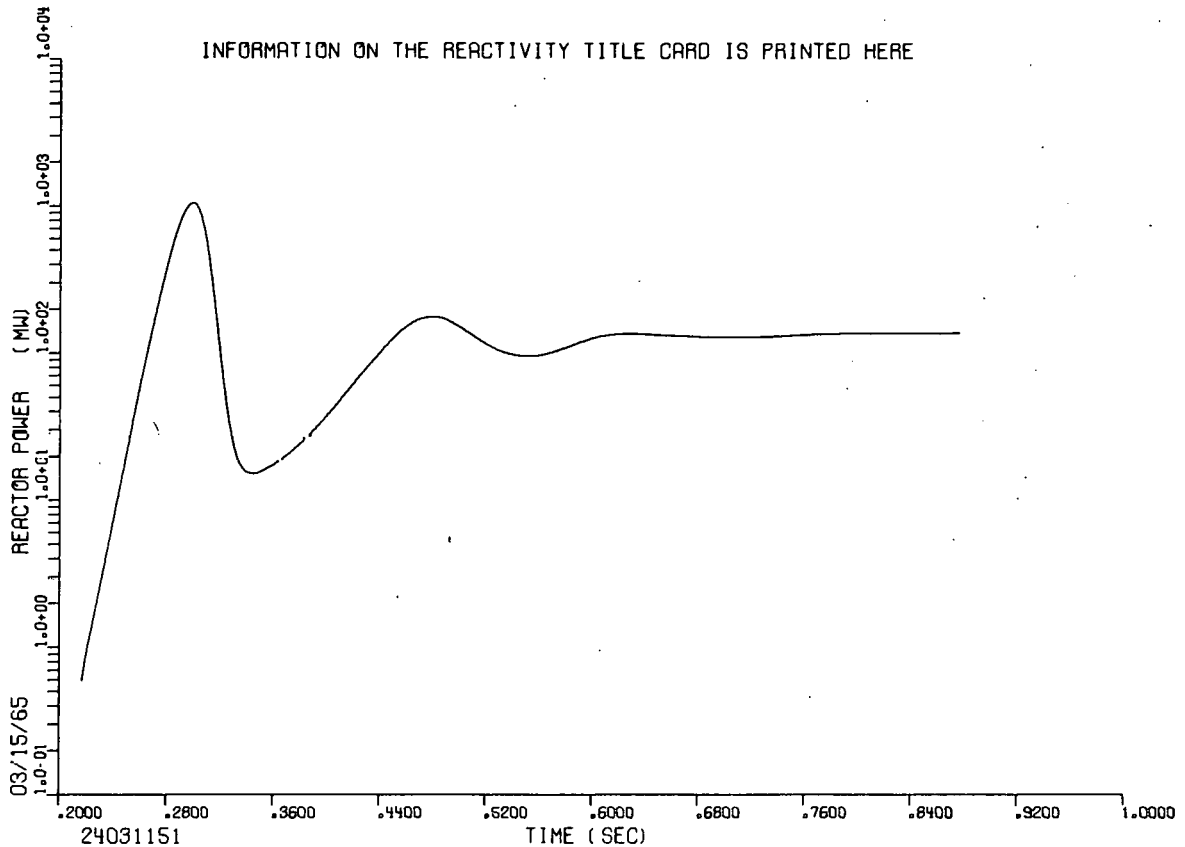


Fig. 15 Plot of power data as prepared by the REACTIVITY program.

SPORT 03/15765

SAMPLE OUTPUT FROM THE SPORT PROGRAM

REACTIVITY PROGRAM

DG P L I PRE S
ER C I N WTN C
LO S T A

INFORMATION ON THE REACTIVITY TITLE CARD IS PRINTED HERE

AU C T PPP L
YP O N E LLL E

LAMBDA / BETA BAR

INITIAL AVERAGE RECIPR. PERIOD

PS N G N TTT S INITIAL ENERGY

SOURCE

CONTROL CARD WAS-

0.00300000

104.0000000

6 0 0 0 121 00

-0.

-0.

LAMBDA'S

0.01270000

0.03170000

0.11600000

0.31100001

1.40000006

5.87000005

F'S

0.03800000

0.21300000

0.18799999

0.40700002

0.12800000

0.02600000

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	BIT
24031151	0.217300	0.6067	1.3078745	0.	0.005834	0.
24031151	0.218300	0.7118	1.3071824	-0.0006921	0.006510	-0.106304343
24031151	0.219300	0.8098	1.3086649	0.0007904	0.007280	0.108572101
24031151	0.220300	0.9127	1.3091228	0.0012483	0.008146	0.153233303
24031151	0.221300	1.0241	1.3087236	0.0008491	0.009119	0.093118912
24031151	0.222300	1.1236	1.3044104	-0.0034641	0.010186	-0.340075195
24031151	0.223300	1.2516	1.3046512	-0.0032234	0.011376	-0.283356536
24031151	0.224300	1.3697	1.2994919	-0.0083826	0.012678	-0.661168493
24031151	0.225300	1.5106	1.2984872	-0.0093873	0.014116	-0.665033519
24031151	0.226300	1.6733	1.3001074	-0.0077672	0.015707	-0.494505748
24031151	0.227300	1.8725	1.3068947	-0.0009798	0.017486	-0.056035528
24031151	0.228300	2.0679	1.3052120	-0.0026625	0.019450	-0.136886811
24031151	0.229300	2.2896	1.3048679	-0.0030066	0.021626	-0.139027270
24031151	0.230300	2.5333	1.3043095	-0.0035650	0.024034	-0.148332996
24031151	0.231300	2.8006	1.3035385	-0.0043361	0.026696	-0.162425866
24031151	0.232300	3.0998	1.3036218	-0.0042527	0.029642	-0.143469768
24031151	0.233300	3.4307	1.3037254	-0.0041491	0.032903	-0.126100987
24031151	0.234300	3.8014	1.3042823	-0.0035922	0.036516	-0.098373856
24031151	0.235300	4.2140	1.3049667	-0.0029078	0.040521	-0.071761592
24031151	0.236300	4.6774	1.3058175	-0.0020570	0.044965	-0.045747375
24031151	0.237300	5.1962	1.3067300	-0.0011445	0.049901	-0.022934882
24031151	0.238300	5.7676	1.3074216	-0.0004529	0.055380	-0.008177867
24031151	0.239300	6.4041	1.3082035	0.0003290	0.061462	0.005353150
24031151	0.240300	7.1144	1.3090468	0.0011723	0.068218	0.017184582
24031151	0.241300	7.8985	1.3094488	0.0015743	0.075718	0.020791612
24031151	0.242300	8.7668	1.3100271	0.0021526	0.084042	0.025613395
24031151	0.243300	9.7269	1.3104514	0.0025769	0.093277	0.027626310
24031151	0.244300	10.7911	1.3108792	0.0030047	0.103522	0.029024948
24031151	0.245300	11.9715	1.3112463	0.0033718	0.114887	0.029348587
24031151	0.246300	13.2798	1.3115610	0.0036865	0.127493	0.028915305
24031151	0.247300	14.7461	1.3123405	0.0044660	0.141490	0.031564058
24031151	0.248300	16.3971	1.3133190	0.0054445	0.157051	0.034666803
24031151	0.249300	18.2464	1.3142251	0.0063506	0.174365	0.036421101
24031151	0.250300	20.3078	1.3147410	0.0068665	0.193633	0.035461315
24031151	0.251300	22.6122	1.3150213	0.0071468	0.215086	0.033227668
24031151	0.252300	25.1821	1.3151084	0.0072338	0.238976	0.030270142
24031151	0.253300	28.0484	1.3149998	0.0071252	0.265585	0.026828478
24031151	0.254300	31.2454	1.3146234	0.0067489	0.295229	0.022859966
24031151	0.255300	34.8024	1.3138220	0.0059475	0.328250	0.018118859
24031151	0.256300	38.7586	1.3126440	0.0047695	0.365031	0.013066015
24031151	0.257300	43.1288	1.3108804	0.0030059	0.405971	0.007404138
24031151	0.258300	47.9356	1.3086894	0.0008149	0.451488	0.001804854
24031151	0.259300	53.2481	1.3063294	-0.0015451	0.502069	-0.003077530
24031151	0.260300	59.1011	1.3035228	-0.0043518	0.558233	-0.007795628
24031151	0.261300	65.4979	1.3004819	-0.0073926	0.620507	-0.011913825
24031151	0.262300	72.4660	1.2973678	-0.0105068	0.689441	-0.015239540
24031151	0.263300	80.0752	1.2944105	-0.0134640	0.765650	-0.017585065
24031151	0.264300	88.3899	1.2913908	-0.0164837	0.849813	-0.019396873
24031151	0.265300	97.4319	1.2885984	-0.0192762	0.942630	-0.020449343
24031151	0.266300	107.2775	1.2859261	-0.0219485	1.044871	-0.021005922

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	BIT)
24031151	0.867300	138.0873	0.8067284	-0.5011461	91.780723	-0.005460254
24031151	0.868300	138.1828	0.8069343	-0.5009403	91.918892	-0.005449807
24031151	0.869300	138.3477	0.8075962	-0.5002783	92.057210	-0.005434429
24031151	0.870300	138.3730	0.8073696	-0.5005049	92.195555	-0.005428731
24031151	0.871300	138.4623	0.8075639	-0.5003106	92.333982	-0.005418488
24031151	0.872300	138.4226	0.8068203	-0.5010543	92.472382	-0.005418421
24031151	0.873300	138.4395	0.8065032	-0.5013713	92.610801	-0.005413746
24031151	0.874300	138.5246	0.8067039	-0.5011706	92.749298	-0.005403498
24031151	0.875300	138.5774	0.8065280	-0.5013465	92.887849	-0.005397331
24031151	0.876300	138.6285	0.8063499	-0.5015246	93.026451	-0.005391204

CALCULATIONS REQUIRED

0 MIN 34.9 SEC AND PLOT(S) REQUIRED 0 MIN 44.3 SEC

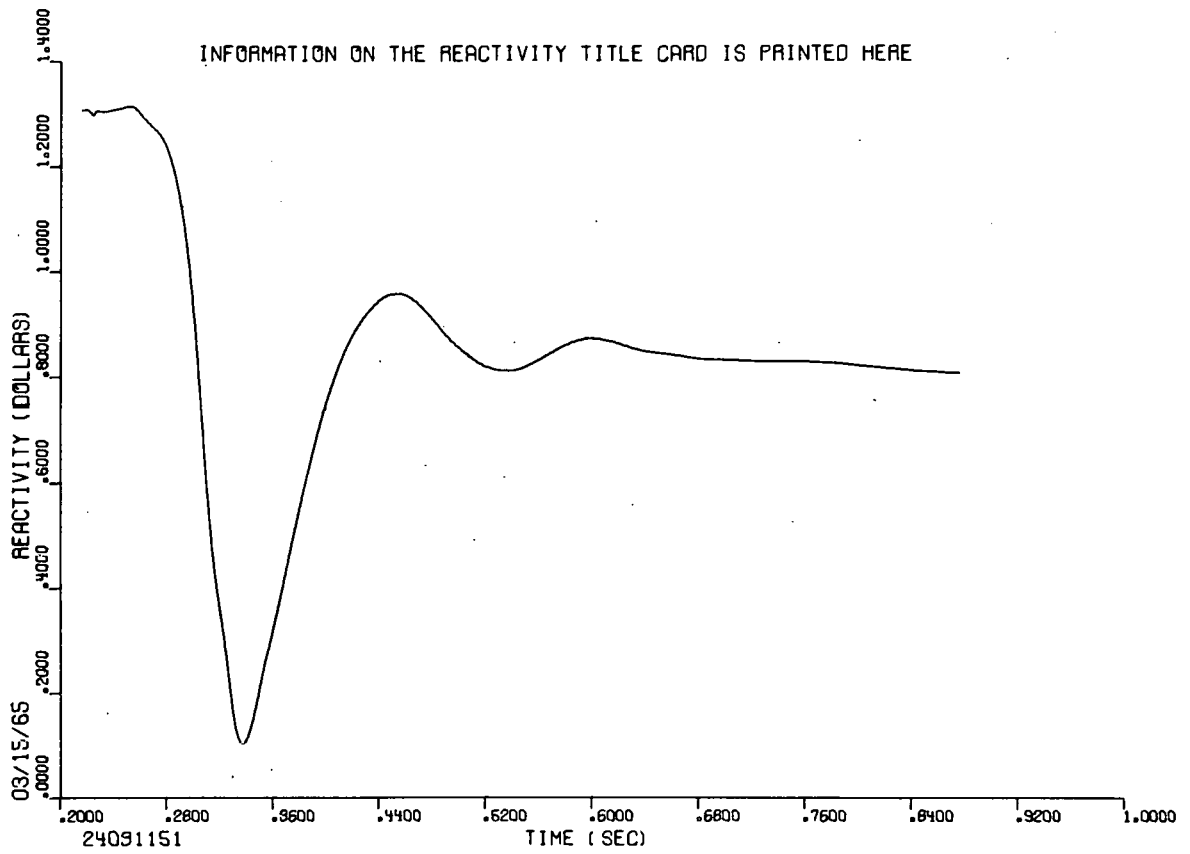


Fig. 16 Plot of reactivity as prepared by the REACTIVITY program.

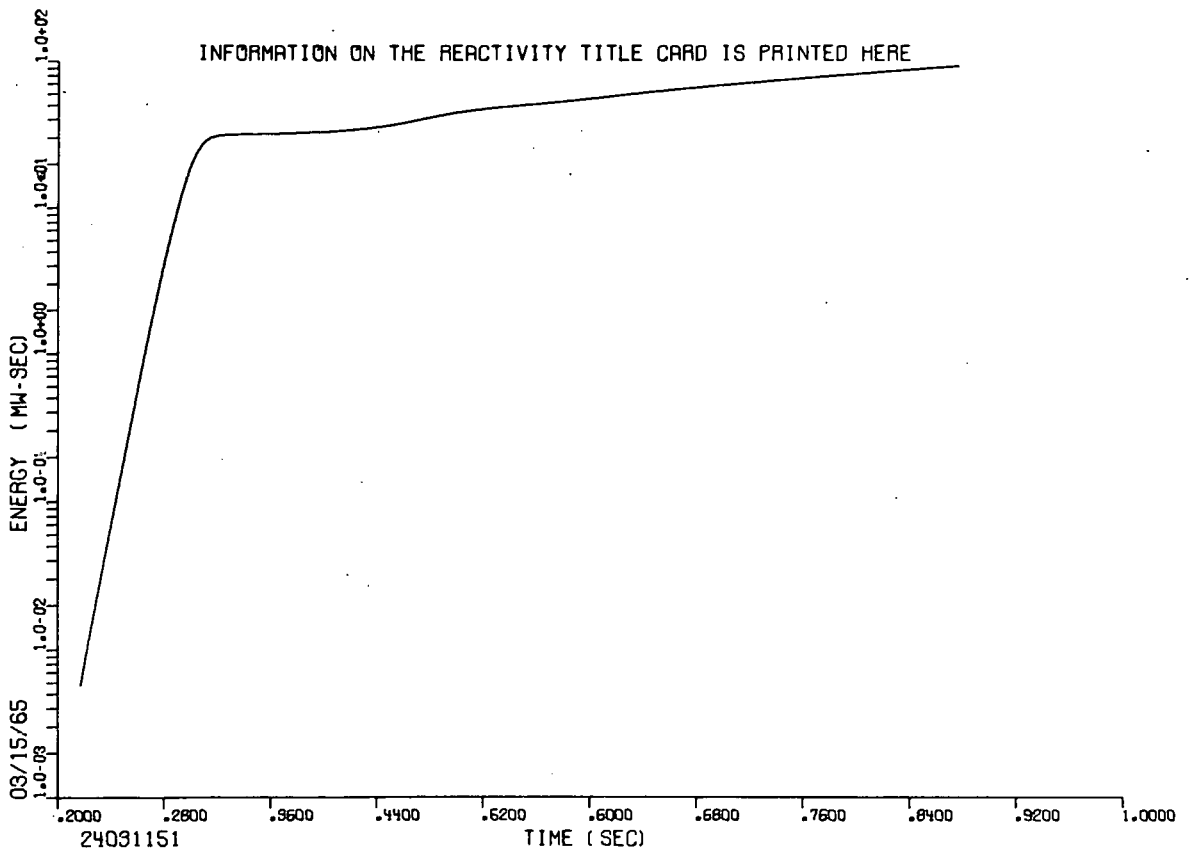


Fig. 17 Plot of energy as prepared by the REACTIVITY program.

5. FREQUENCY RESPONSE PROGRAM OUTPUT

The values on the FREQUENCY RESPONSE CONTROL Card are listed on the first page in the FREQUENCY RESPONSE program output in the same order in which they were entered (page 71). The OMEGA cards are listed next. Page 72 is an example of the FREQUENCY RESPONSE output listing. The identification number, frequency, and the real part, imaginary part, phase in degrees, and decibel magnitude of the FREQUENCY RESPONSE output may be punched on cards in the format:

(I10, F14.4, 2E14.7, F14.8, F14.7) .

Figures 18 and 19 are examples of FREQUENCY RESPONSE output plots.

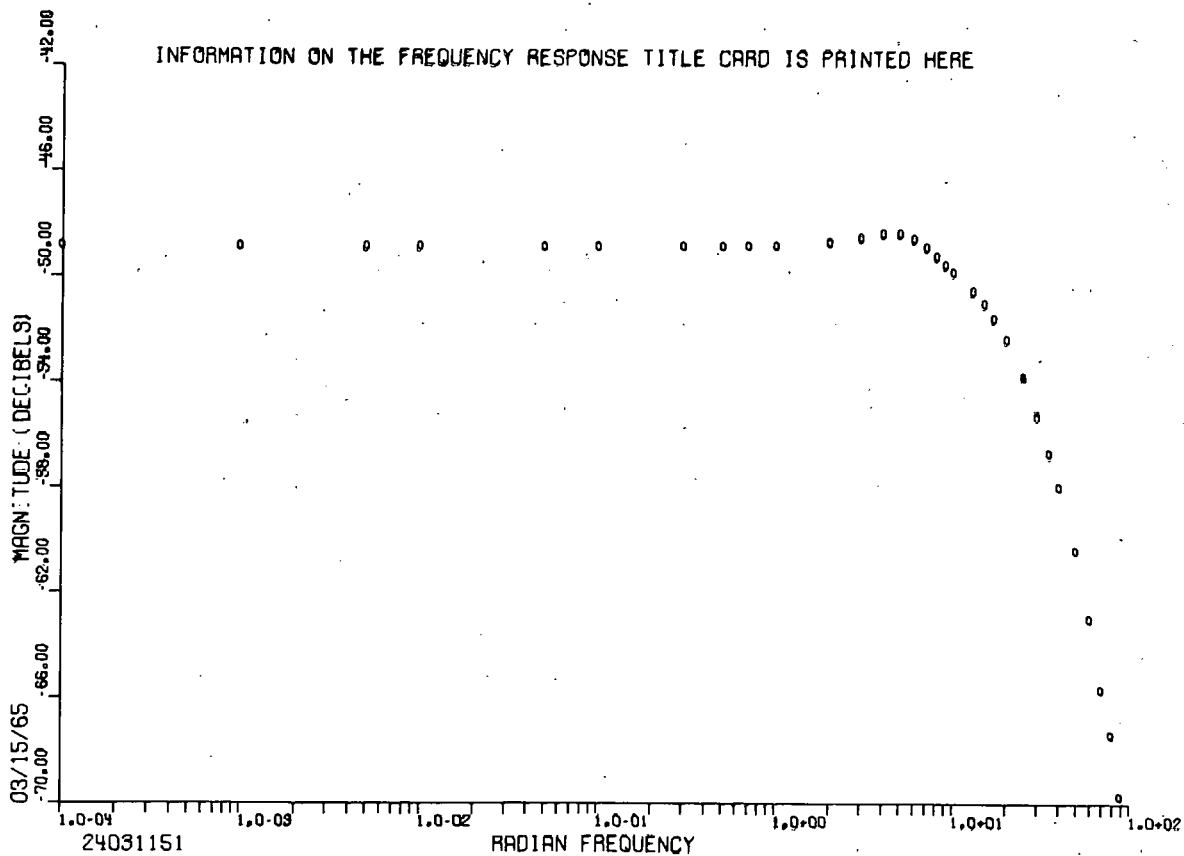


Fig. 18 Plot of the magnitude of the transformation calculated (and plotted) by FREQUENCY RESPONSE.

FREQUENCY RESPONSE PROGRAM

INFORMATION ON THE FREQUENCY RESPONSE TITLE CARD IS PRINTED HERE

CONTROL CARD WAS- 32 311 2 0 0 ALPHA = -0.

RADIAN FREQUENCIES

0.0001000	0.0010000	0.0050000	0.0100000	0.0500000	0.1000000	0.3000000	0.5000000
0.7000000	1.0000000	2.0000000	3.0000000	4.0000000	5.0000000	6.0000000	7.0000000
8.0000000	9.0000000	10.0000000	13.0000000	15.0000000	17.0000000	20.0000000	25.0000000
30.0000000	35.0000000	40.0000000	50.0000000	60.0000000	70.0000000	80.0000000	90.0000000

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SAMPLE OUTPUT FROM THE SPORT PROGRAM

RECORD NO 24031151 CHANNEL 0 NUMERATOR WAS WORD 3, DENOMINATOR WAS WORD 1

FREQUENCY	LOG W	REAL G(IW)	IMAG. G(IW)	MAG. G	PHASE ANGLE	20 LOG(MAG. G)
0.0001	-4.000	-3.6177646E-03	1.7699922E-08	3.6177646E-03	-180.00027847	-48.8311939
0.0010	-3.000	-3.6177646E-03	1.7699933E-07	3.6177646E-03	-180.00279999	-48.8311939
0.0050	-2.301	-3.6177632E-03	8.8499522E-07	3.6177633E-03	-180.01401520	-48.8311973
0.0100	-2.000	-3.6177646E-03	1.7699877E-06	3.6177650E-03	-180.02803040	-48.8311934
0.0500	-1.301	-3.6178045E-03	8.8504316E-06	3.6178153E-03	-180.14016342	-48.8310728
0.1000	-1.000	-3.6179305E-03	1.7704835E-05	3.6179739E-03	-180.28038025	-48.8306913
0.3000	-0.523	-3.6192648E-03	5.3233030E-05	3.6196562E-03	-180.84265709	-48.8266540
0.5000	-0.301	-3.6219167E-03	8.9117620E-05	3.6230129E-03	-181.40948105	-48.8186026
0.7000	-0.155	-3.6258499E-03	1.2559846E-04	3.6280246E-03	-181.98391342	-48.8065958
1.0000	0.	-3.6340241E-03	1.8197164E-04	3.6385773E-03	-182.86665726	-48.7813687
2.0000	0.301	-3.6763129E-03	3.9439289E-04	3.6974075E-03	-186.12323952	-48.6420541
3.0000	0.477	-3.7190838E-03	6.6696938E-04	3.7784167E-03	-190.16717339	-48.4538035
4.0000	0.602	-3.7088761E-03	1.0101001E-03	3.8439646E-03	-195.23481750	-48.3044124
5.0000	0.699	-3.5873769E-03	1.3802759E-03	3.8437527E-03	-201.04468346	-48.3048921
6.0000	0.778	-3.3558752E-03	1.6932368E-03	3.7588494E-03	-206.77363396	-48.4989014
7.0000	0.845	-3.0813802E-03	1.9052667E-03	3.6228365E-03	-211.72916222	-48.8190260
8.0000	0.903	-2.8223450E-03	2.0375660E-03	3.4809921E-03	-215.82705116	-49.1659393
9.0000	0.954	-2.5951356E-03	2.1281088E-03	3.3561251E-03	-219.35303879	-49.4832377
10.0000	1.000	-2.3926430E-03	2.2009502E-03	3.2509879E-03	-222.61040306	-49.7596936
13.0000	1.114	-1.8359321E-03	2.3668752E-03	2.9954540E-03	-232.20006371	-50.4707470
15.0000	1.176	-1.4750904E-03	2.4130323E-03	2.8281825E-03	-238.56248474	-50.9698515
17.0000	1.230	-1.1420761E-03	2.3988066E-03	2.6568046E-03	-244.54079437	-51.5128078
20.0000	1.301	-7.1790998E-04	2.3099813E-03	2.4189684E-03	-252.73547935	-52.3273969
25.0000	1.398	-1.5856793E-04	2.0515625E-03	2.0576813E-03	-265.58031845	-53.7324386
30.0000	1.477	1.8235952E-04	1.7148876E-03	1.7245563E-03	-276.06996536	-55.2664523
35.0000	1.544	3.7551903E-04	1.4235724E-03	1.4722679E-03	-284.77723694	-56.6402636
40.0000	1.602	4.8770136E-04	1.1720293E-03	1.2694508E-03	-292.59302521	-57.9276829
50.0000	1.699	6.0532038E-04	7.4749436E-04	9.6185267E-04	-309.00052643	-60.3378296
60.0000	1.778	5.4954005E-04	4.5451175E-04	7.1314458E-04	-320.40664291	-62.9364491
70.0000	1.845	4.5704383E-04	2.5425516E-04	5.2300548E-04	-330.91265106	-65.6298752
80.0000	1.903	3.9681780E-04	1.6368226E-04	4.2925079E-04	-337.58447647	-67.3457785
90.0000	1.954	3.2480752E-04	3.8100442E-05	3.2703450E-04	-353.30968475	-69.7081289

CALCULATIONS REQUIRED 1 MIN 4.1 SEC AND PLOT(S) REQUIRED 0 MIN 22.4 SEC

TOTAL PROBLEM TIME WAS 4 MIN 60.0 SEC

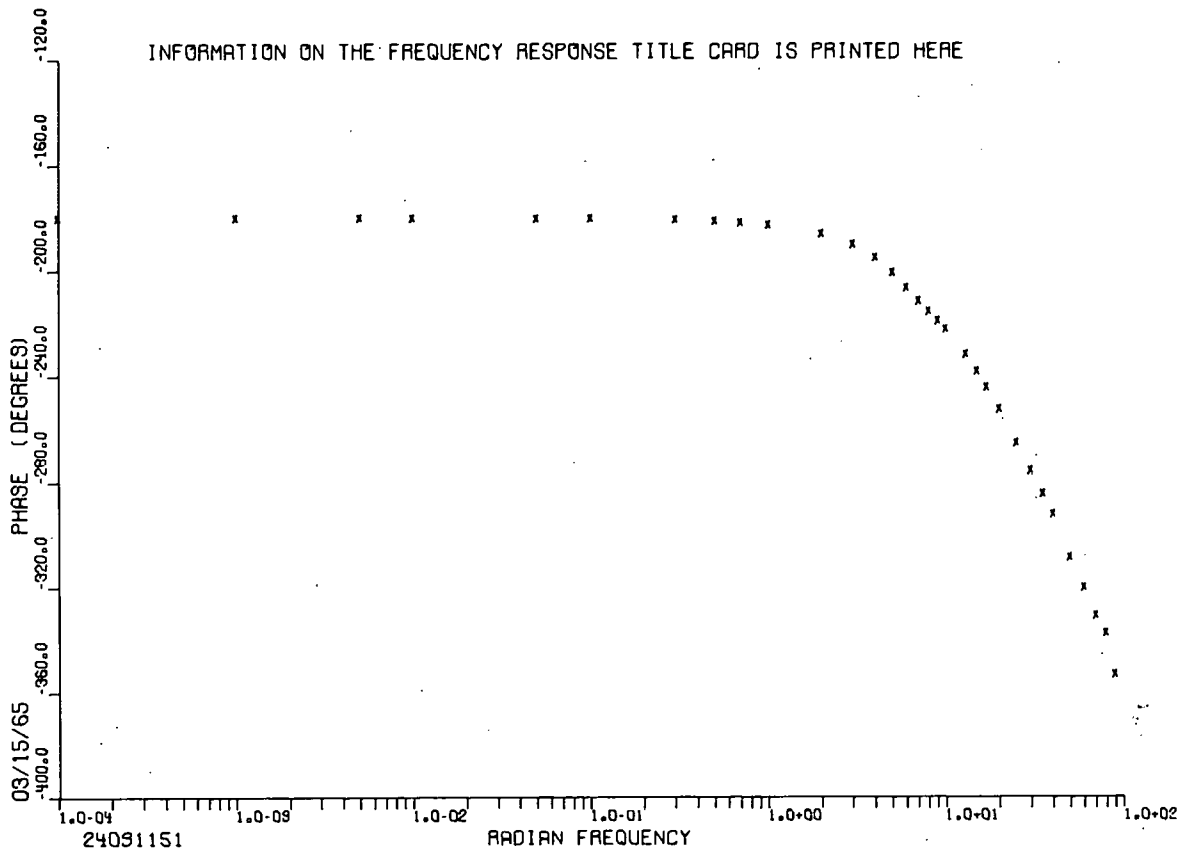


Fig. 19 Plot of the phase of the transformation calculated (and plotted) by FREQUENCY RESPONSE.

V. SAMPLE PROBLEMS

This section is presented in two parts: (a) an example of one of the most typical SPORT processing applications and (b) sample sets of control cards that might be used for other common processing schemes.

1. TYPICAL PROBLEM

On the following pages, the input control cards and the resulting output for a typical SPORT problem are listed. In this problem, SPORT assembles a composite power channel from three "saturating" channels and one "peaking" channel of Spert I power data recorded during the destructive test in October, 1962. The composite power is plotted and then smoothed three times in preparation for the REACTIVITY program calculations which complete the problem. Plots of coefficients C and B in the SMOOTH program output and of the reactivity in the REACTIVITY program output are generated. The output listings from the SMOOTH and REACTIVITY programs are suppressed for the sake of brevity.

INPUT CONTROL CARDS SPERT I DESTRUCTIVE TEST

PAGE 1

0000000001111111112222222223333333334444444445555555556666666667777777778
 12345678901234567890123456789012345678901234567890123456789012345678901234567890

205 -60101	SPERT I DESTRUCTIVE TEST 10/26/62					
0040541104	0.098000	0.103220	1.170550			0932
0040541103		0.109250				
0040541102		0.116000				
0040541101		0.131300				
0040541102		0.136250				
0040541103		0.138880	1.059840			
	SPERT I DESTRUCTIVE TEST 10/26/62					
0040541000	0.000030					63330003
SPERT I DESTRUCTIVE TEST 10/26/62						
0.008160	312.5	0603002000				
0.0127	0.0317	0.116	0.311	1.40	3.87	'LAMBDA' CARD
0.038	0.213	0.188	0.407	0.128	0.026	'F' CARD

*STOP

SPORT 03/15/65

SYSTEM FOR PROCESSING REACTOR TRANSIENT DATA

PART CARD WAS 205 -60101

SPERT I DESTRUCTIVE TEST OCTOBER 26, 1962

REEL NUMBER 932

CHANNEL ID NO	FILE NO (IF ANY)	MINIMUM TIME	MAXIMUM TIME	NORMALIZING COEFFICIENTS DATA		TIME SHIFT	DATA SHIFT
40541104	-0	0.098000	0.103220	1.000000	1.1705500E 00	-0.	-0.
40541103	-0	0.103220	0.109250	1.000000	1.0000000E 00	-0.	-0.
40541102	-0	0.109250	0.116000	1.000000	1.0000000E 00	-0.	-0.
40541101	-0	0.116000	0.131300	1.000000	1.0000000E 00	-0.	-0.
40541102	-0	0.131300	0.136250	1.000000	1.0000000E 00	-0.	-0.
40541103	-0	0.136250	0.138880	1.000000	1.0598400E 00	-0.	-0.

DATA TAPE MOUNTING TIME - 0 MIN 2.3 SEC

SPERT I DESTRUCTIVE TEST OCTOBER 26, 1962

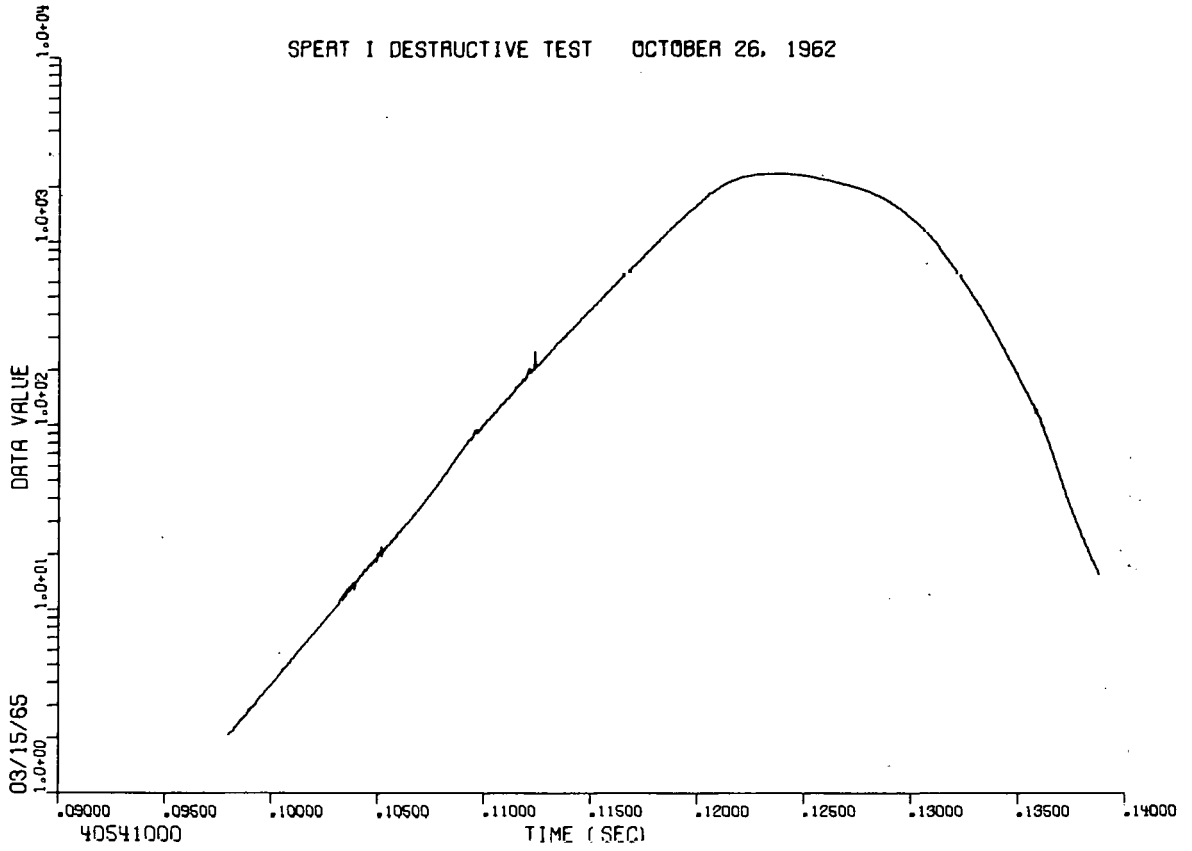


Fig. 20 Sample plot of power data as prepared in the data preparation phase of SPORT.

SPORT 03/15/65

SPERT I DESTRUCTIVE TEST OCTOBER 26, 1962

DATA PREPARATION REQUIRED 0 MIN 39.1 SEC AND DATA PLOT REQUIRED 0 MIN 14.0 SEC

SPORT 03/15/65

SPERT I DESTRUCTIVE TEST OCTOBER 26, 1962

QUADRATIC SMOOTHING PROGRAM

N L S O R T D
U I P D C R E R S
M S L A A D C A M
B T O T L E Y N N
R G T A E R L S T

SPERT I DESTRUCTIVE TEST OCTOBER 26, 1962

PASS NUMBER 1	ID NO	DELTA T	T MINIMUM	T MAXIMUM	T START CAL	1ST OUTPUT T	
SMOOTH CONTROL CARD WAS-	40541000	0.000030	-0.	-0.	-0.	-0.	63 3 300 0 3-00
CONTROL WORDS RESET -					0.098960	0.098960	

CALCULATIONS REQUIRED 0 MIN 54.5 SEC

BEGIN PASS 2

CONTROL WORDS RESET -					0.098960	0.098960	
-----------------------	--	--	--	--	----------	----------	--

CALCULATIONS REQUIRED 1 MIN 4.1 SEC

BEGIN PASS 3

CONTROL WORDS RESET -					0.098960	0.098960	
-----------------------	--	--	--	--	----------	----------	--

CALCULATIONS REQUIRED 1 MIN 4.7 SEC AND PLOT REQUIRED 0 MIN 34.4 SEC

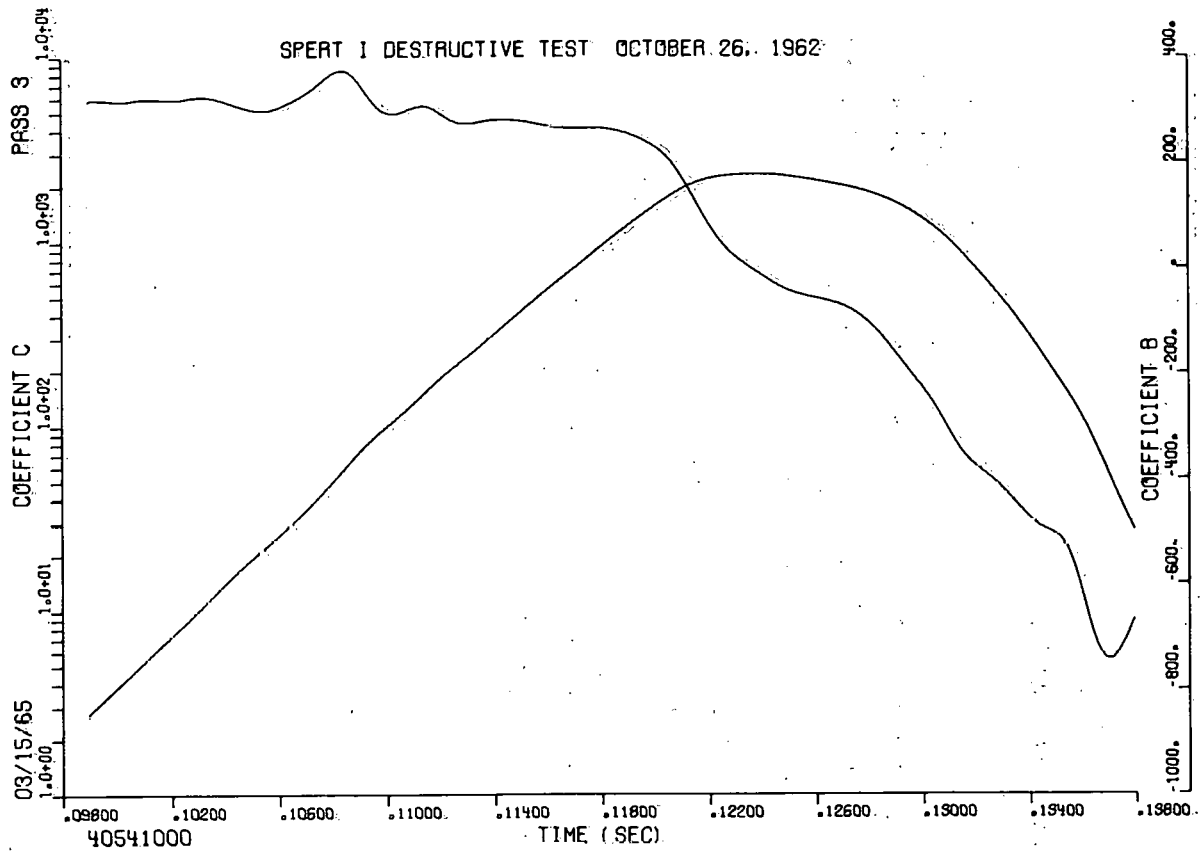


Fig. 21. Sample plot of power data and slope as prepared by SMOOTH.

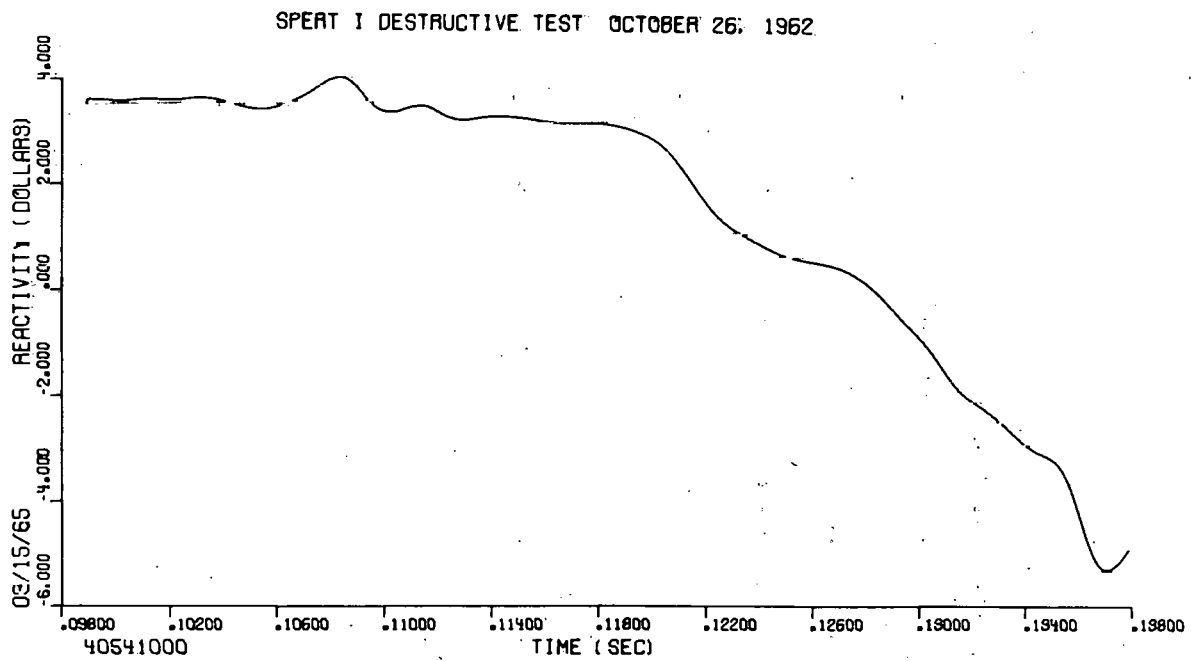


Fig. 22. Sample plot of calculated reactivity as prepared by the REACTIVITY program.

SPERT 03/15/65

SPERT I DESTRUCTIVE TEST OCTOBER 26, 1962

REACTIVITY PROGRAM

DG P L I P R E S
E R C I N W T N C
L O S T A

SPERT I DESTRUCTIVE TEST OCTOBER 26, 1962

A U C T P P P L
Y P O N E L L E
P S N G N T T S

LAMBDA / BETA BAR

INITIAL AVERAGE RECIPR. PERIOD

INITIAL ENERGY

SOURCE

CONTROL CARD WAS-

0.00816000

312.5000000

6 0 3 0 020 00

-0.

-0.

LAMBDA'S

0.012700000

0.031700000

0.116000000

0.311000001

1.400000006

3.870000005

F'S

0.038000000

0.213000000

0.187999999

0.407000002

0.128000000

0.026000000

CALCULATIONS REQUIRED

0 MIN 28.9 SEC AND PLOT(S) REQUIRED 0 MIN 19.1 SEC

TOTAL PROBLEM TIME WAS

5 MIN 19.4 SEC

2. SAMPLE SETS OF CONTROL CARDS FOR COMMON APPLICATIONS

On the following pages, a number of sets of SPORT control cards are listed. A brief description of the significance of each set is included below.

Example 1. Example 1 illustrates the SPORT control cards necessary to prepare and plot a section of Type 5 data from data Channel 0240602108 stored on Computing Center Reel Number 596.

Example 2. Example 2 illustrates the SPORT control cards necessary to prepare and plot a section of Type 1 data from Channel 6 in the deck of Spert 1 through 3 data cards included in the input card deck.

Example 3. Example 3 illustrates the SPORT control cards necessary to prepare, plot, and repunch a composite power channel from 7 sections of Channels 3, 5, and 6 in the deck of Spert 1-3 data cards included in the control card sequence.

Example 4. Example 4 illustrates the SPORT control cards necessary to prepare and plot all the data from Channel 1 in the deck of 650 floating-point data cards included in the control card sequence and to process the prepared data with the SMOOTH, REACTIVITY, and FREQUENCY RESPONSE programs.

Example 5. Example 5 illustrates the SPORT control cards necessary to prepare and smooth two channels of data stored on the same reel of magnetic tape with the primary purpose of obtaining decks of smoothed even time increment card data for use in another program. Since the Computing Center Reel Number is not specified in this case, the machine operator must be told where to locate the data.

Example 6. Example 6 illustrates the SPORT control cards necessary to prepare and smooth Channels 3, 5, and 6 in the deck of Spert 1-3 data cards included in the control card sequence.

Example 7. Example 7 illustrates the SPORT control cards necessary to prepare and smooth 3 channels of Type 5 data stored on Computing Center Reel Number 910 with the primary purpose of obtaining plots which can be used to estimate where the three data channels could best be joined together to form a single composite data channel.

Example 8. Example 8 illustrates the SPORT control cards necessary to assemble sections of data from two channels stored on Computing Center Reel Number 166 into a single composite channel while suppressing all data in a "bad" section near the center of the two channels.

Example 9. Example 9 illustrates the SPORT control cards necessary to process a channel of data in a deck of Type 4 data cards (included in the control card sequence) directly with the FREQUENCY RESPONSE PROGRAM.

Example 10. Example 10 illustrates the SPORT control cards necessary to process a channel of Type 5 reactor noise data directly with the FREQUENCY RESPONSE program. The composite data channel assembled by SPORT has the last data value set equal to zero.

Example 11. Example 11 illustrates the SPORT control cards necessary to prepare and smooth two channels of Type 5 data stored on Computing Center Reel 113 and then process the two smoothed channels with the FREQUENCY RESPONSE program. Notice that two separate problems are used.

00000000111111112222222233333333444444445555555566666666777777778
 1234567890123456789012345678901234567890123456789012345678901234567890

101 +31101	EXAMPLE 6	*SPORT PROCESSING SYSTEM*					
3		0.0001	0.1				
5		0.0001					
6		0.0001	10.0				
***** DATA CARD DECK ***** (BLANK END-OF-DATA CARD)							
0024031151	SMOOTH TITLE CARD					*SPORT PROCESSING SYSTEM*	
	0.001				21	3 2	
0024031151	SMOOTH TITLE CARD					*SPORT PROCESSING SYSTEM*	
	0.001				21	3 2	
0024031151	SMOOTH TITLE CARD					*SPORT PROCESSING SYSTEM*	
	0.001				21	3 2	
*STOP							

105 +31101	EXAMPLE 7	*SPORT PROCESSING SYSTEM*					
0210542106	0.0	2.00		0.852		910	
0210542107	0.0	2.00					
0210542108	0.0	2.0000					
0210542106	SMOOTH TITLE CARD					*SPORT PROCESSING SYSTEM*	
	0.001				25	3 1 3	
0.500	2.000	-2.0	+3.0	-5.0	15.0	1510	
0210542107	SMOOTH TITLE CARD					*SPORT PROCESSING SYSTEM*	
	0.001				25	3 1 3	
0.500	2.000	-2.0	+3.0	-5.0	15.0	1510	
0210542108	SMOOTH TITLE CARD					*SPORT PROCESSING SYSTEM*	
	0.001				25	3 1 3	
0.500	2.000	-2.0	+3.0	-5.0	15.0	1510	
*STOP							

205 -31101	EXAMPLE 8	*SPORT PROCESSING SYSTEM*					
0240602106	6.99025			0.88540683		166	
0240602107	7.16535			1.11291271	100000.0		
0240602108							
0240602678	SMOOTH TITLE CARD					*SPORT PROCESSING SYSTEM*	
	0.0085				25	3 1 2	
6.0	9.0	-1.0	+2.0	-3.0	+7.0	1510	
0.064	0.0	15	0101				
		6.0	9.0	0.3	1.3	1510	
0.0127	0.0317	0.115	0.311	1.4	3.87	0.277 0.0169	
0.00481	0.0015	0.000428	0.000117	.0000437	.00000363	.000000624	
0.0329	0.185	0.163	0.353	0.110	0.0223	0.0865 0.027	
0.00932	0.00447	0.00275	0.00312	0.000433	0.000139	.000068	
*STOP							

0000000011111111222222222233333333333344444444445555555555666666666677777777778
 12345678901234567890123456789012345678901234567890123456789012345678901234567890

514 1 EXAMPLE 9 *SPORT PROCESSING SYSTEM*
 333333333 0.005
 4 (I10,5E14.8)

***** DATA CARD DECK *****
 (BLANK END-OF-DATA CARD)

FREQUENCY RESPONSE		TITLE CARD		*SPORT PROCESSING SYSTEM*			
811121	12.0						
0.01	0.012	0.014	0.016	0.018	0.02	0.023	0.026
0.03	0.035	0.04	0.05	0.06	0.07	0.08	0.09
0.1	0.12	0.14	0.16	0.18	0.2	0.23	0.26
0.30	0.35	0.4	0.5	0.6	0.7	0.8	0.9
1.0	1.2	1.4	1.6	1.8	2.0	2.3	2.6
3.0	3.5	4.0	5.0	6.0	7.0	8.0	9.0
10.0	12.0	14.0	16.0	18.0	20.0	23.0	26.0
30.0	35.0	40.0	50.0	60.0	70.0	80.0	90.0
100.0	120.0	140.0	160.0	180.0	200.0	230.0	260.0
300.0	350.0	400.0	500.0	600.0	700.0	800.0	900.0
1000.0							

*STOP

515 -31002 EXAMPLE 10 *SPORT PROCESSING SYSTEM*
 0111113025 6.996780 4.0 1.0+3 -0.40 649
 0111113025 6.999300 4.0 1.0-29 -0.40
 0111113025 6.999300 4.0 1.0+3 -0.40

FREQUENCY RESPONSE		TITLE CARD		*SPORT PROCESSING SYSTEM*			
013102101							
4.00	5.00	6.30	8.00	10.0	12.5	16.0	20.0
25.0	31.5	40.0	50.0	63.0			

*STOP

105 +11001 EXAMPLE 11-A *SPORT PROCESSING SYSTEM*
 150063206 SMOOTH TITLE CARD *SPORT PROCESSING SYSTEM* 113
 0150063206.0009 6.0891 7.2564 6.3231 81 31

*CONTINUE
 315 +11001 EXAMPLE 11-B *SPORT PROCESSING SYSTEM*
 150063207 SMOOTH TITLE CARD *SPORT PROCESSING SYSTEM* 113
 0150063207.0009 6.0891 7.2564 6.3231 81 31

FREQUENCY RESPONSE		TITLE CARD		*SPORT PROCESSING SYSTEM*			
481142							
0.0001	0.001	0.01	0.1	0.2	0.3	0.4	0.5
0.6	0.7	0.8	0.9	1.0	1.5	2.0	3.0
4.0	5.0	5.5	6.0	7.0	8.0	9.0	10.0
12.0	15.0	17.0	20.0	21.0	22.0	23.0	24.0
26.0	27.0	28.0	30.0	32.0	34.0	36.0	38.0
40.0	42.0	44.0	46.0	48.0	50.0	52.0	54.0

*STOP

VI. CHECKOUT OF PROGRAMS

1. INTRODUCTION

In addition to functional checkout of SPORT, tests were conducted to determine if the calculations made by the programs, SMOOTH, REACTIVITY, and FREQUENCY RESPONSE, were correct within the limits of numerical evaluation. Three phases of SMOOTH were tested: (a) the effect of smoothing an increasing exponential function, (b) the effect of smoothing tape data which contains noise, and (c) the effect of resmoothing data. To determine the accuracy of the calculations made by REACTIVITY, two tests were run: (a) reactivity was calculated from power data represented by $\exp(\alpha t)$, and (2) reactivity was calculated from power data recorded during a transient in which the reactivity was known as a function of time. The accuracy of the FREQUENCY RESPONSE program is discussed in some detail in Section II.

2. CHECKOUT OF SMOOTH

The simplest demonstration of SMOOTH is that of using as input data the function, $\exp(\alpha t)$. If this is done and if the natural logarithm of the input data is taken, the output from SMOOTH should be a straight line with slope α . The results of such a test are shown on pages 88 through 91 where the first two and the last pages of output are given. These answers are considered to be quite adequate.

Once it has been demonstrated that the SMOOTH calculations are adequate for fictitious data, one must determine the effect of smoothing data which contains noise of relatively small magnitude. The results of such a test are presented in Figure 23. The dotted circles indicate recorded data points while the continuous curve represents output from SMOOTH.

The third test which was applied to the SMOOTH program was to determine the effectiveness of the program in removing sinusoidal noise oscillations superimposed on a function. The program was tested by generating data which contained 60-cycle noise and smoothing this data. Figures 24 through 28 demonstrate the effect of multiple smoothing both on data values and slope values.

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TEST PROBLEM TO CHECK THE ACCURACY OF SMOOTH AND REACTIVITY

QUADRATIC SMOOTHING PROGRAM

TEST PROBLEM TO CHECK THE ACCURACY OF SMOOTH AND REACTIVITY

PASS NUMBER 1	ID NO	DELTA T	T MINIMUM	T MAXIMUM	T START CAL	1ST OUTPUT T	N L S O R TD U I PDC R E RS M S LAA D C AM B T OTL E Y NN R G TAE R L ST
SMOOTH CONTROL CARD WAS-	888888888	0.000050	-0.	-0.	-0.	-0.	25 0 000 0 0 00
CONTROL WORDS RESET	-				0.000600	0.000600	

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TEST PROBLEM TO CHECK THE ACCURACY OF SMOOTH AND REACTIVITY

SMOOTH PROGRAM OUTPUT LISTING FOR CHANNEL 888

ID NUMBER	TIME	C	B	A
88888888	0.000600	1.1286122	49.9999943	-0.2500000
88888888	0.000650	1.1311122	49.9999943	-0.1250000
88888888	0.000700	1.1336122	49.9999938	-0.
88888888	0.000750	1.1361122	49.9999962	-0.1250000
88888888	0.000800	1.1386122	49.9999967	-0.1250000
88888888	0.000850	1.1411122	49.9999967	-0.1250000
88888888	0.000900	1.1436122	49.9999957	-0.1250000
88888888	0.000950	1.1461122	49.9999962	-0.
88888888	0.001000	1.1486122	49.9999967	-0.1250000
88888888	0.001050	1.1511122	49.9999933	-0.
88888888	0.001100	1.1536121	49.9999938	0.2500000
88888888	0.001150	1.1561122	49.9999948	-0.
88888888	0.001200	1.1586122	49.9999943	-0.
88888888	0.001250	1.1611122	49.9999928	-0.1250000
88888888	0.001300	1.1636122	49.9999933	-0.
88888888	0.001350	1.1661122	49.9999928	-0.
88888888	0.001400	1.1686122	49.9999914	-0.
88888888	0.001450	1.1711122	49.9999900	0.1250000
88888888	0.001500	1.1736122	49.9999938	-0.1250000
88888888	0.001550	1.1761122	49.9999957	-0.
88888888	0.001600	1.1786122	49.9999943	-0.
88888888	0.001650	1.1811122	49.9999957	-0.5000000
88888888	0.001700	1.1836122	49.9999924	-0.2500000
88888888	0.001750	1.1861122	49.9999948	-0.2500000
88888888	0.001800	1.1886122	49.9999962	-0.
88888888	0.001850	1.1911122	49.9999990	-0.1250000
88888888	0.001900	1.1936122	49.9999981	-0.1250000
88888888	0.001950	1.1961122	49.9999962	-0.1250000
88888888	0.002000	1.1986122	49.9999962	-0.2500000
88888888	0.002050	1.2011122	49.9999990	-0.
88888888	0.002100	1.2036122	49.9999995	-0.2500000
88888888	0.002150	1.2061122	50.0000005	-0.2500000
88888888	0.002200	1.2086122	50.0000000	-0.
88888888	0.002250	1.2111122	49.9999990	-0.2500000
88888888	0.002300	1.2136122	49.9999990	-0.1250000
88888888	0.002350	1.2161122	50.0000010	-0.
88888888	0.002400	1.2186122	50.0000024	-0.1250000
88888888	0.002450	1.2211122	50.0000033	-0.2500000
88888888	0.002500	1.2236122	50.0000029	-0.1250000
88888888	0.002550	1.2261122	50.0000038	-0.3750000
88888888	0.002600	1.2286122	50.0000014	-0.1250000
88888888	0.002650	1.2311122	50.0000014	-0.1250000
88888888	0.002700	1.2336122	50.0000005	-0.2500000
88888888	0.002750	1.2361122	50.0000014	-0.2500000
88888888	0.002800	1.2386122	49.9999976	-0.3750000
88888888	0.002850	1.2411122	49.9999938	-0.1250000
88888888	0.002900	1.2436122	49.9999943	-0.3750000
88888888	0.002950	1.2461122	49.9999943	-0.2500000
88888888	0.003000	1.2486122	49.9999967	-0.2500000
88888888	0.003050	1.2511122	49.9999971	-0.1250000

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TEST PROBLEM TO CHECK THE ACCURACY OF SMOOTH AND REACTIVITY

SMOOTH PROGRAM OUTPUT LISTING FOR CHANNEL 888

ID NUMBER	TIME	C	B	A
888888888	0.003100	1.2536122	49.9999995	-0.1250000
888888888	0.003150	1.2561122	49.9999990	-0.1250000
888888888	0.003200	1.2586122	49.9999995	-0.1250000
888888888	0.003250	1.2611122	49.9999967	-0.
888888888	0.003300	1.2636122	49.9999967	-0.1250000
888888888	0.003350	1.2661122	49.9999943	-0.1250000
888888888	0.003400	1.2686122	49.9999943	-0.2500000
888888888	0.003450	1.2711122	49.9999914	-0.1250000
888888888	0.003500	1.2736122	49.9999905	-0.
888888888	0.003550	1.2761122	49.9999914	-0.
888888888	0.003600	1.2786121	49.9999938	0.1250000
888888888	0.003650	1.2811122	49.9999967	-0.
888888888	0.003700	1.2836121	49.9999976	-0.
888888888	0.003750	1.2861122	49.9999971	-0.1250000
888888888	0.003800	1.2886122	49.9999971	-0.1250000
888888888	0.003850	1.2911122	49.9999976	-0.
888888888	0.003900	1.2936121	50.0000014	0.2500000
888888888	0.003950	1.2961121	50.0000033	0.2500000
888888888	0.004000	1.2986122	50.0000043	-0.1250000
888888888	0.004050	1.3011122	50.0000014	-0.
888888888	0.004100	1.3036121	50.0000005	0.1250000
888888888	0.004150	1.3061123	50.0000010	-0.6250000
888888888	0.004200	1.3086122	50.0000038	-0.1250000
888888888	0.004250	1.3111122	50.0000057	-0.2500000
888888888	0.004300	1.3136122	50.0000067	0.1250000
888888888	0.004350	1.3161122	50.0000091	-0.2500000
888888888	0.004400	1.3186121	50.0000076	0.2500000
888888888	0.004450	1.3211122	50.0000119	-0.
888888888	0.004500	1.3236122	50.0000091	-0.1250000
888888888	0.004550	1.3261122	50.0000086	-0.1250000
888888888	0.004600	1.3286122	50.0000057	-0.2500000
888888888	0.004650	1.3311121	50.0000048	-0.
888888888	0.004700	1.3336122	50.0000005	-0.
888888888	0.004750	1.3361121	50.0000010	0.1250000
888888888	0.004800	1.3386122	49.9999971	-0.
888888888	0.004850	1.3411121	49.9999990	0.1250000
888888888	0.004900	1.3436122	49.9999962	-0.1250000
888888888	0.004950	1.3461121	49.9999957	0.3750000
888888888	0.005000	1.3486121	49.9999938	0.1250000
888888888	0.005050	1.3511122	49.9999914	-0.2500000
888888888	0.005100	1.3536122	49.9999914	-0.
888888888	0.005150	1.3561122	49.9999928	-0.
888888888	0.005200	1.3586121	49.9999938	-0.
888888888	0.005250	1.3611121	49.9999938	0.2500000
888888888	0.005300	1.3636121	49.9999957	-0.
888888888	0.005350	1.3661122	50.0000000	0.1250000
888888888	0.005400	1.3686122	49.9999995	-0.
888888888	0.005450	1.3711122	50.0000010	-0.1250000
888888888	0.005500	1.3736121	50.0000024	-0.
888888888	0.005550	1.3761121	50.0000014	0.1250000

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TEST PROBLEM TO CHECK THE ACCURACY OF SMOOTH AND REACTIVITY

SMOOTH PROGRAM OUTPUT LISTING FOR CHANNEL 888

ID NUMBER	TIME	C	B	A
888888888	0.118100	7.0036117	50.0000110	-2.0000000
888888888	0.118150	7.0061116	50.0000067	-0.
888888888	0.118200	7.0086117	49.9999900	-0.
888888888	0.118250	7.0111115	49.9999843	-0.
888888888	0.118300	7.0136113	49.9999671	-0.
888888888	0.118350	7.0161119	49.9999609	-3.0000000
000000000	0.110400	7.0106110	49.9999537	1.0000000
888888888	0.118450	7.0211117	49.9999452	-1.0000000
888888888	0.118500	7.0236118	49.9999480	-2.0000000
888888888	0.118550	7.0261116	49.9999385	1.0000000
888888888	0.118600	7.0286114	49.9999514	1.0000000
888888888	0.118650	7.0311115	49.9999409	-1.0000000
888888888	0.118700	7.0336118	49.9999514	-1.0000000
888888888	0.118750	7.0361116	49.9999509	-1.0000000
888888888	0.118800	7.0386117	49.9999609	-1.0000000
888888888	0.118850	7.0411116	49.9999585	-0.
888888888	0.118900	7.0436118	49.9999681	-1.0000000
888888888	0.118950	7.0461116	49.9999881	-0.
888888888	0.119000	7.0486116	49.9999967	1.0000000
888888888	0.119050	7.0511116	50.0000157	-0.
888888888	0.119100	7.0536118	50.0000229	-1.0000000
888888888	0.119150	7.0561117	50.0000415	-0.
888888888	0.119200	7.0586118	50.0000477	-1.0000000
888888888	0.119250	7.0611115	50.0000415	1.0000000
888888888	0.119300	7.0636117	50.0000448	-1.0000000
888888888	0.119350	7.0661117	50.0000358	-1.0000000
888888888	0.119400	7.0686116	50.0000367	-0.

CALCULATIONS REQUIRED 1 MIN 44.8 SEC

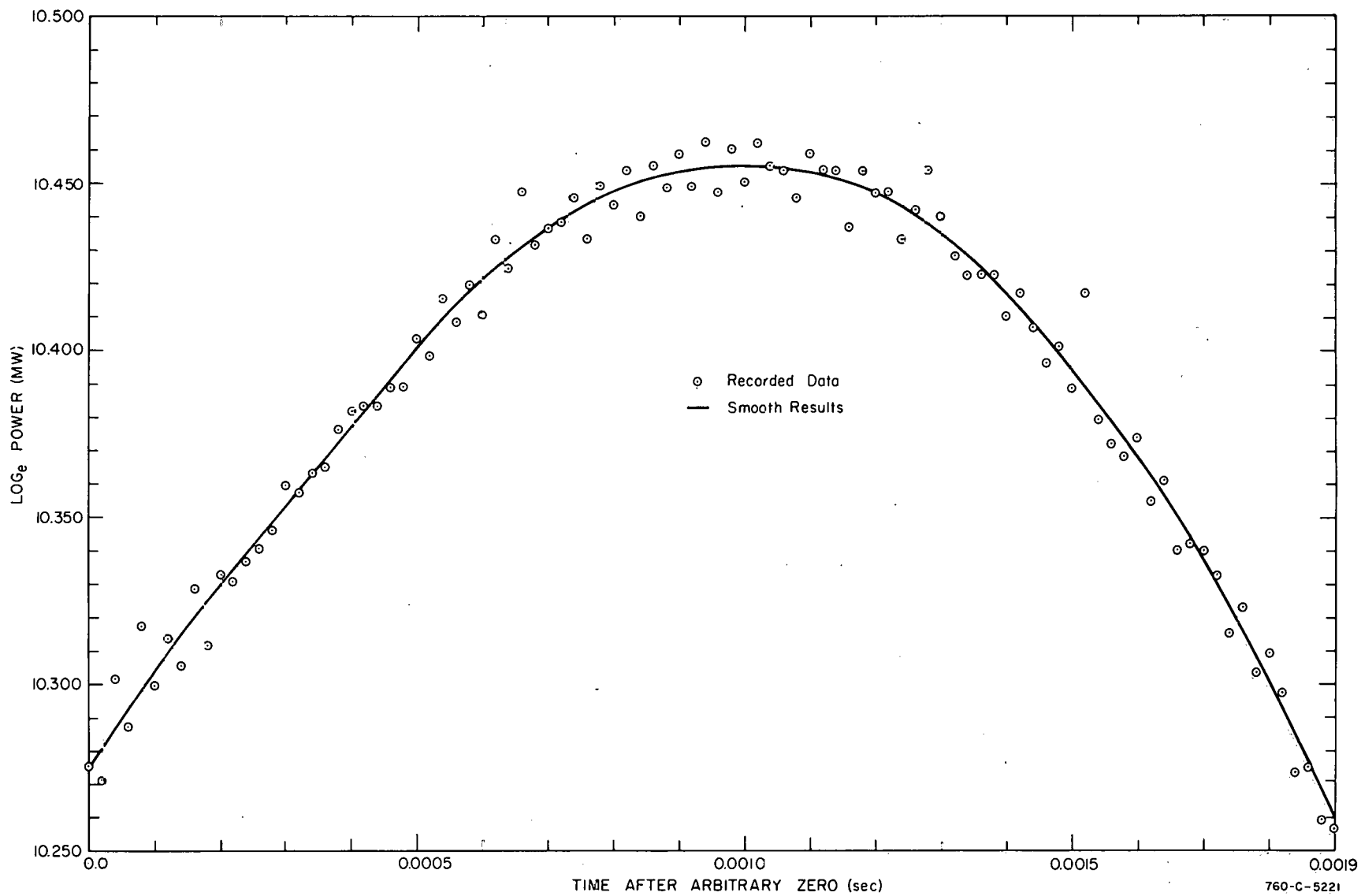


Fig. 23 Effect of smoothing data with small noise oscillations.

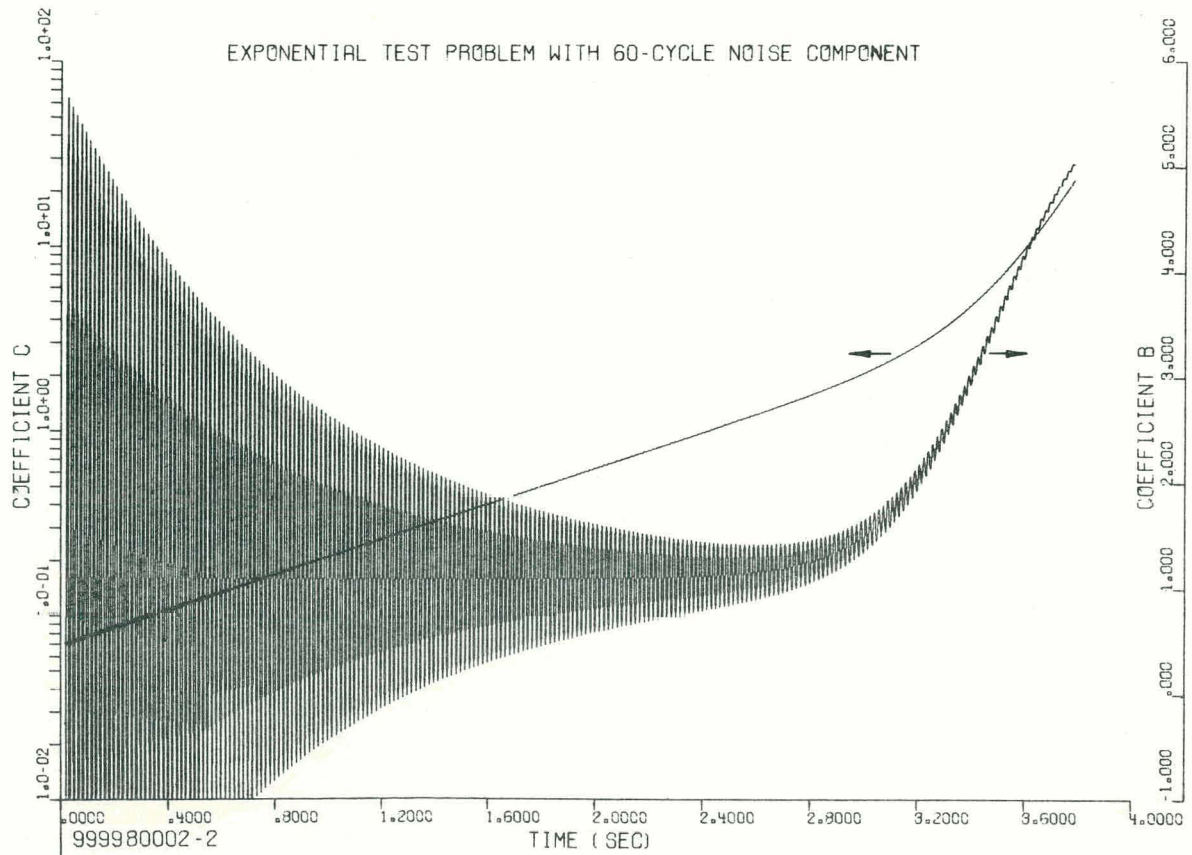


Fig. 24 Results of one smoothing pass on data which contain 60-cycle noise.

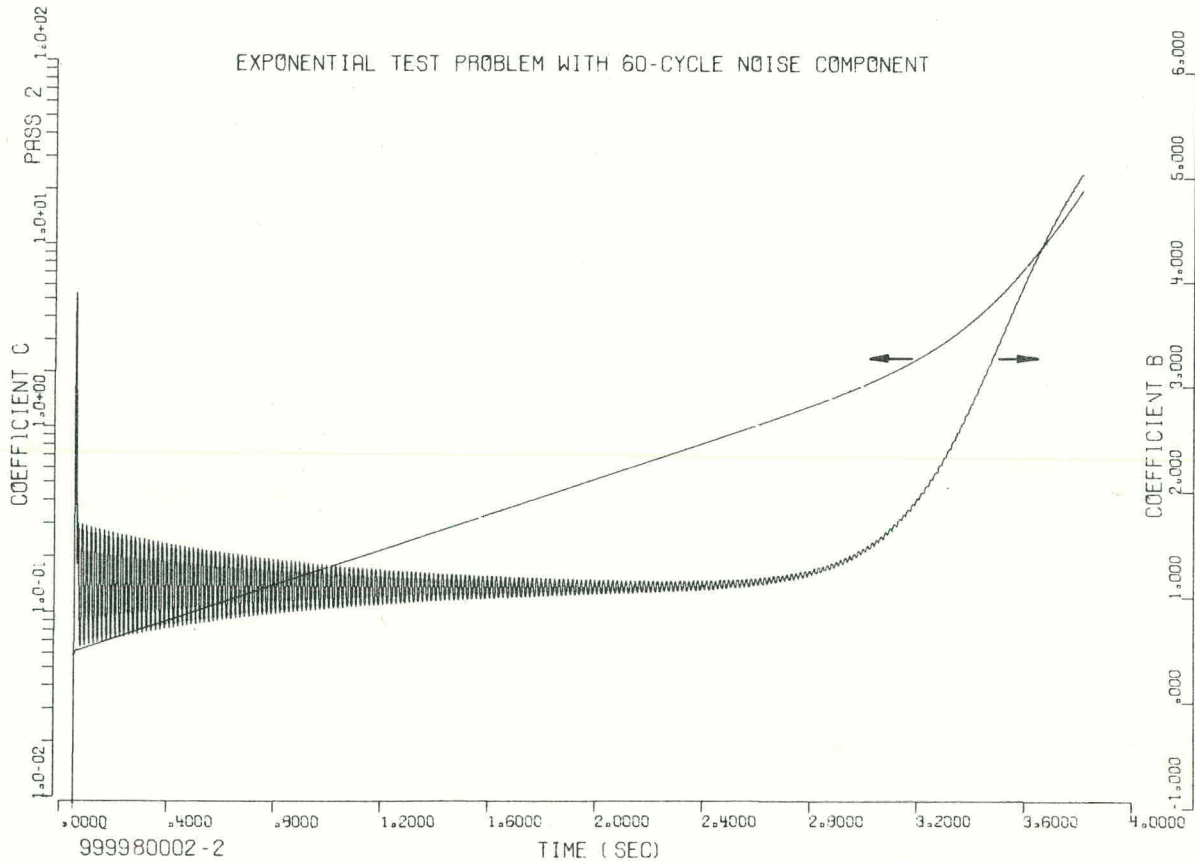


Fig. 25 Results of two smoothing passes on data which contain 60-cycle noise.

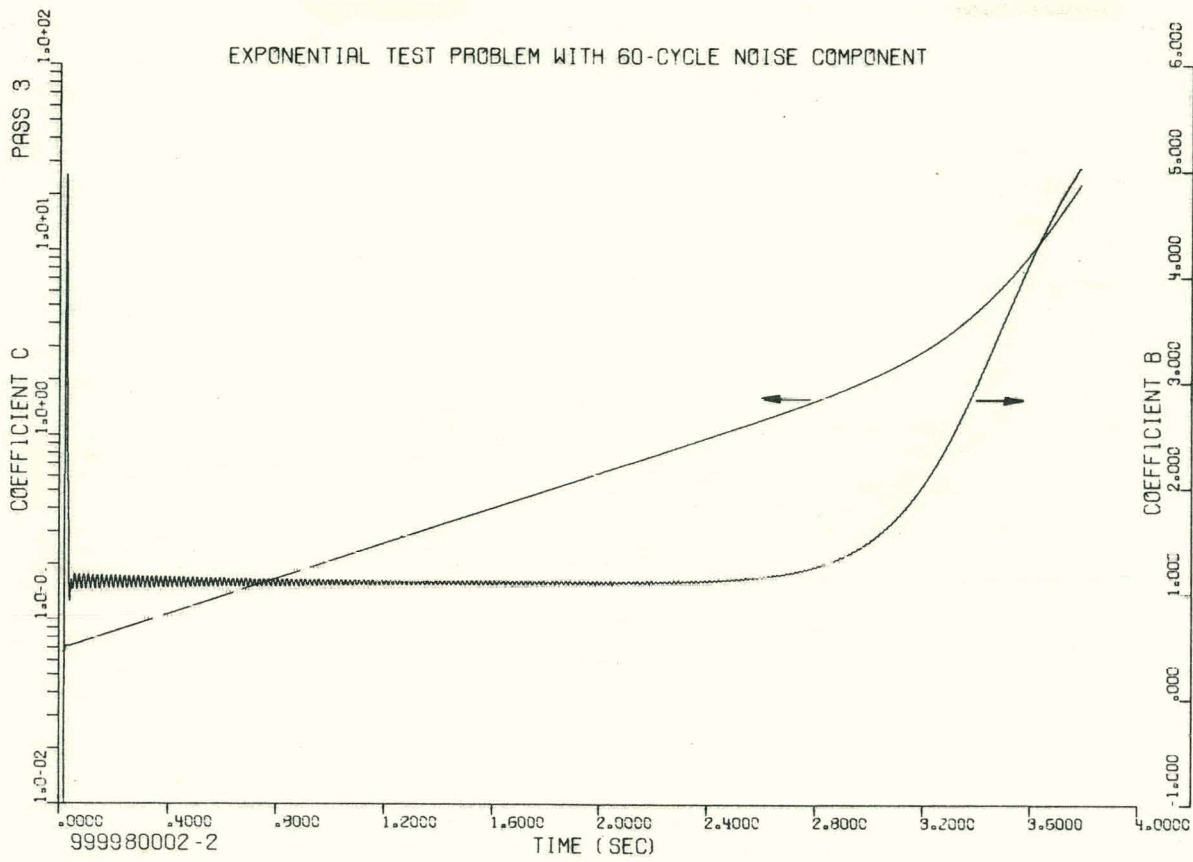


Fig. 26 Results of three smoothing passes on data which contain 60-cycle noise.

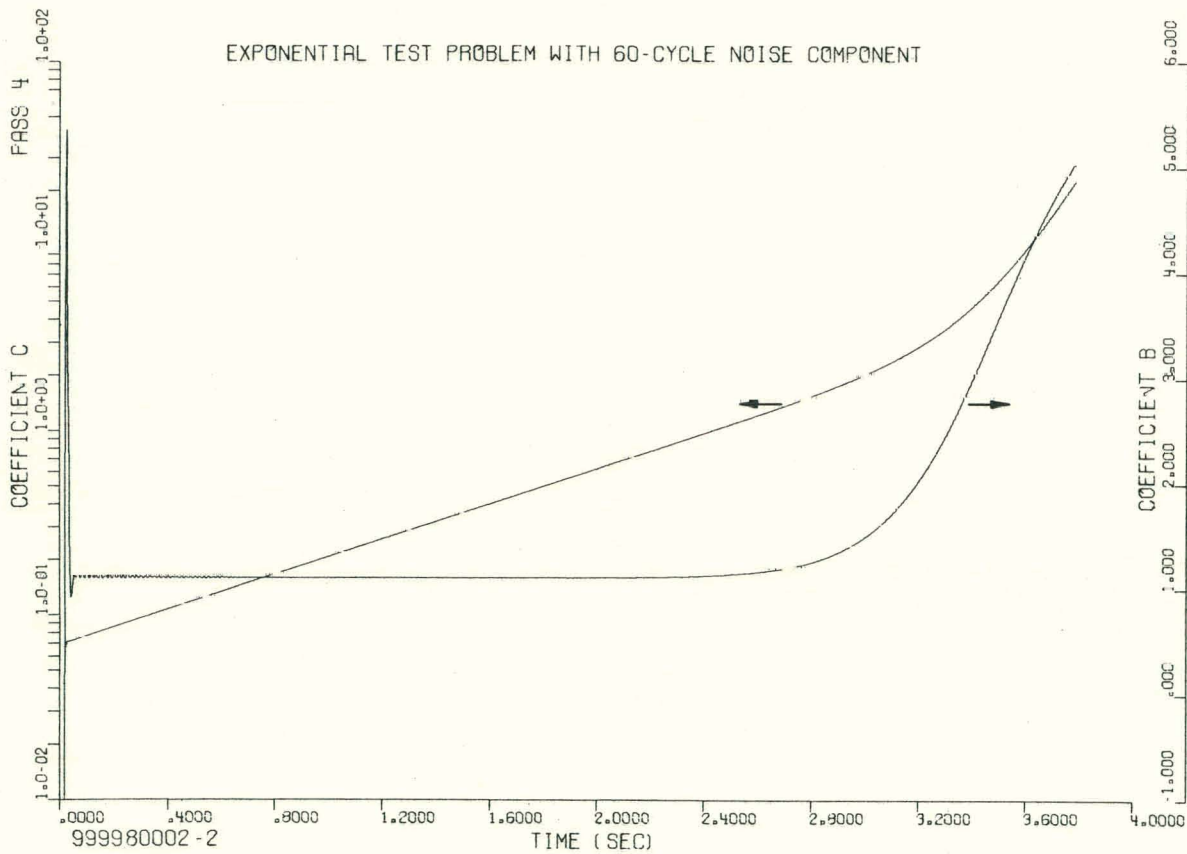


Fig. 27 Results of four smoothing passes on data which contain 60-cycle noise.

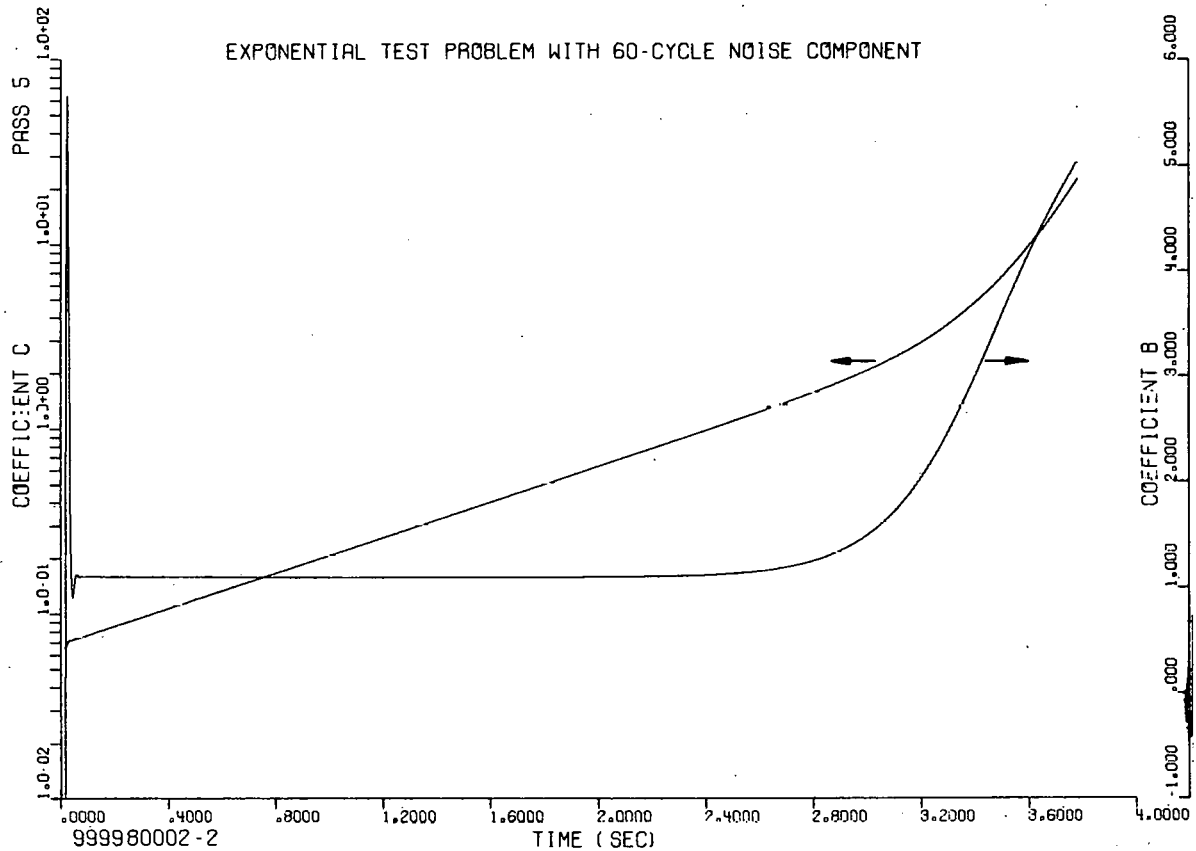


Fig. 28 Results of five smoothing passes on data which contain 60-cycle noise.

3. CHECKOUT OF REACTIVITY

To determine that the calculations made by REACTIVITY were correct, power data given by the equation

$$\phi(t) = \phi(0)e^{\alpha t} \quad (167)$$

were generated and processed by REACTIVITY. For the constants used in the test problem, the reactivity should be given by

$$\$(t) = 1.1415 - 0.002e^{-50t} \quad (168)$$

(Note that the initial reactivity value is calculated from the inhour equation which ignores the source term.) Listings of the first two pages and the last page of REACTIVITY outputs are shown on pages 96 through 99, and a plot of the calculated reactivity is given in Figure 29. These results indicate that the desired calculations are being made correctly.

An additional test which was applied to REACTIVITY is that of Spert I Transient 13398. In this particular transient, a reactivity step insertion of 91¢ was applied to the reactor resulting in an initial exponential power rise with a period of approximately 31.1 msec. Before the reactor power was

REACTIVITY PROGRAM

DG P L I P R E S
 E R C I N W T N C
 L O S T A

TEST PROBLEM TO CHECK THE ACCURACY OF SMOOTH AND REACTIVITY

A U C T P P P L
 Y P O N E L L E

LAMBDA / BETA BAR

INITIAL AVERAGE RECIPR. PERIOD

P S N G N T T S

INITIAL ENERGY

SOURCE

CONTROL CARD WAS-

0.003000C0

50.00000000

6 0 0 0 500 00

0:

2:00000000

LAMBDA'S

0.012700000

0.031700000

0.116000000

0.311000001

1.400000006

3.870000005

IF'S

0.038000000

0.213000000

0.187999999

0.407000002

0.128000000

0:026000000

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 888

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(I)
88888888	0.000600	3.0914	1.1415501	0.	0.061827	0.
88888888	0.000650	3.0991	1.1396141	-0.0019360	0.061982	-0.031235399
88888888	0.000700	3.1069	1.1396189	-0.0019312	0.062137	-0.031079710
88888888	0.000750	3.1146	1.1396237	-0.0019264	0.062293	-0.030924603
88888888	0.000800	3.1224	1.1396285	-0.0019216	0.062449	-0.030770315
88888888	0.000850	3.1302	1.1396333	-0.0019168	0.062605	-0.030616844
88888888	0.000900	3.1381	1.1396381	-0.0019120	0.062762	-0.030464184
88888888	0.000950	3.1459	1.1396429	-0.0019072	0.062919	-0.030312333
88888888	0.001000	3.1538	1.1396477	-0.0019024	0.063076	-0.030161050
88888888	0.001050	3.1617	1.1396524	-0.0018977	0.063234	-0.030010805
88888888	0.001100	3.1696	1.1396571	-0.0018930	0.063392	-0.029861122
88888888	0.001150	3.1776	1.1396619	-0.0018882	0.063551	-0.029711999
88888888	0.001200	3.1855	1.1396666	-0.0018835	0.063710	-0.029563903
88888888	0.001250	3.1935	1.1396713	-0.0018788	0.063870	-0.029416594
88888888	0.001300	3.2015	1.1396760	-0.0018741	0.064030	-0.029269837
88888888	0.001350	3.2095	1.1396807	-0.0018695	0.064190	-0.029123862
88888888	0.001400	3.2175	1.1396853	-0.0018648	0.064350	-0.028978664
88888888	0.001450	3.2256	1.1396900	-0.0018601	0.064512	-0.028834241
88888888	0.001500	3.2337	1.1396946	-0.0018555	0.064673	-0.028690128
88888888	0.001550	3.2417	1.1396993	-0.0018508	0.064835	-0.028547015
88888888	0.001600	3.2499	1.1397039	-0.0018462	0.064997	-0.028404667
88888888	0.001650	3.2580	1.1397085	-0.0018416	0.065160	-0.028262851
88888888	0.001700	3.2662	1.1397131	-0.0018370	0.065323	-0.028122251
88888888	0.001750	3.2743	1.1397177	-0.0018324	0.065487	-0.027981722
88888888	0.001800	3.2825	1.1397223	-0.0018279	0.065650	-0.027842173
88888888	0.001850	3.2907	1.1397268	-0.0018233	0.065815	-0.027703147
88888888	0.001900	3.2990	1.1397314	-0.0018187	0.065980	-0.027565093
88888888	0.001950	3.3072	1.1397359	-0.0018142	0.066145	-0.027427556
88888888	0.002000	3.3155	1.1397405	-0.0018097	0.066310	-0.027290758
88888888	0.002050	3.3238	1.1397450	-0.0018051	0.066476	-0.027154473
88888888	0.002100	3.3321	1.1397495	-0.0018006	0.066643	-0.027019145
88888888	0.002150	3.3405	1.1397540	-0.0017961	0.066809	-0.026884323
88888888	0.002200	3.3488	1.1397585	-0.0017916	0.066977	-0.026750229
88888888	0.002250	3.3572	1.1397629	-0.0017872	0.067144	-0.026616859
88888888	0.002300	3.3656	1.1397674	-0.0017827	0.067312	-0.026484210
88888888	0.002350	3.3740	1.1397719	-0.0017782	0.067481	-0.026351836
88888888	0.002400	3.3825	1.1397763	-0.0017738	0.067650	-0.026220398
88888888	0.002450	3.3910	1.1397807	-0.0017694	0.067819	-0.0260889673
88888888	0.002500	3.3994	1.1397852	-0.0017650	0.067989	-0.025959436
88888888	0.002550	3.4080	1.1397896	-0.0017605	0.068159	-0.025829907
88888888	0.002600	3.4165	1.1397939	-0.0017562	0.068330	-0.025701298
88888888	0.002650	3.4250	1.1397983	-0.0017518	0.068501	-0.025573170
88888888	0.002700	3.4336	1.1398027	-0.0017474	0.068672	-0.025445522
88888888	0.002750	3.4422	1.1398071	-0.0017430	0.068844	-0.025318569
88888888	0.002800	3.4508	1.1398114	-0.0017387	0.069016	-0.025192522
88888888	0.002850	3.4595	1.1398157	-0.0017344	0.069189	-0.025066948
88888888	0.002900	3.4681	1.1398201	-0.0017300	0.069362	-0.024942058
88888888	0.002950	3.4768	1.1398244	-0.0017257	0.069536	-0.024817635
88888888	0.003000	3.4855	1.1398287	-0.0017214	0.069710	-0.024693679
88888888	0.003050	3.4942	1.1398330	-0.0017171	0.069885	-0.024570613

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 886

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(T)
888888888	0.003100	3.5030	1.1398373	-0.0017128	0.070059	-0.024447795
888888888	0.003150	3.5117	1.1398416	-0.0017085	0.070235	-0.024325861
888888888	0.003200	3.5205	1.1398458	-0.0017043	0.070411	-0.024204596
888888888	0.003250	3.5293	1.1398501	-0.0017000	0.070587	-0.024083995
888888888	0.003300	3.5382	1.1398543	-0.0016958	0.070764	-0.023963846
888888888	0.003350	3.5470	1.1398586	-0.0016915	0.070941	-0.023844357
888888888	0.003400	3.5559	1.1398628	-0.0016873	0.071118	-0.023725525
888888888	0.003450	3.5648	1.1398670	-0.0016831	0.071296	-0.023607346
888888888	0.003500	3.5737	1.1398712	-0.0016789	0.071475	-0.023489610
888888888	0.003550	3.5827	1.1398754	-0.0016747	0.071654	-0.023372315
888888888	0.003600	3.5917	1.1398796	-0.0016705	0.071833	-0.023255666
888888888	0.003650	3.6006	1.1398838	-0.0016664	0.072013	-0.023139661
888888888	0.003700	3.6097	1.1398879	-0.0016622	0.072193	-0.023024296
888888888	0.003750	3.6187	1.1398921	-0.0016580	0.072374	-0.022909364
888888888	0.003800	3.6277	1.1398962	-0.0016539	0.072555	-0.022795067
888888888	0.003850	3.6368	1.1399003	-0.0016498	0.072737	-0.022681403
888888888	0.003900	3.6459	1.1399045	-0.0016456	0.072919	-0.022568165
888888888	0.003950	3.6551	1.1399086	-0.0016415	0.073101	-0.022455554
888888888	0.004000	3.6642	1.1399127	-0.0016374	0.073284	-0.022343365
888888888	0.004050	3.6734	1.1399168	-0.0016333	0.073468	-0.022232205
888888888	0.004100	3.6826	1.1399208	-0.0016293	0.073651	-0.022121259
888888888	0.004150	3.6918	1.1399249	-0.0016252	0.073836	-0.022010929
888888888	0.004200	3.7010	1.1399290	-0.0016211	0.074021	-0.021901013
888888888	0.004250	3.7103	1.1399330	-0.0016171	0.074206	-0.021791709
888888888	0.004300	3.7196	1.1399371	-0.0016130	0.074392	-0.021683015
888888888	0.004350	3.7289	1.1399411	-0.0016090	0.074578	-0.021574727
888888888	0.004400	3.7382	1.1399451	-0.0016050	0.074765	-0.021467244
888888888	0.004450	3.7476	1.1399491	-0.0016010	0.074952	-0.021359965
888888888	0.004500	3.7570	1.1399531	-0.0015970	0.075139	-0.021253483
888888888	0.004550	3.7664	1.1399571	-0.0015930	0.075327	-0.021147599
888888888	0.004600	3.7758	1.1399611	-0.0015890	0.075516	-0.021042110
888888888	0.004650	3.7853	1.1399651	-0.0015851	0.075705	-0.020937213
888888888	0.004700	3.7947	1.1399690	-0.0015811	0.075894	-0.020833102
888888888	0.004750	3.8042	1.1399730	-0.0015772	0.076084	-0.020728988
888888888	0.004800	3.8137	1.1399769	-0.0015732	0.076275	-0.020625850
888888888	0.004850	3.8233	1.1399808	-0.0015693	0.076466	-0.020522903
888888888	0.004900	3.8329	1.1399847	-0.0015654	0.076657	-0.020420731
888888888	0.004950	3.8425	1.1399886	-0.0015615	0.076849	-0.020318747
888888888	0.005000	3.8521	1.1399925	-0.0015576	0.077041	-0.020217532
888888888	0.005050	3.8617	1.1399964	-0.0015537	0.077234	-0.020116888
888888888	0.005100	3.8714	1.1400003	-0.0015498	0.077428	-0.020016429
888888888	0.005150	3.8811	1.1400042	-0.0015460	0.077621	-0.019916537
888888888	0.005200	3.8908	1.1400080	-0.0015421	0.077816	-0.019817212
888888888	0.005250	3.9005	1.1400119	-0.0015382	0.078011	-0.019718449
888888888	0.005300	3.9103	1.1400157	-0.0015344	0.078206	-0.019619865
888888888	0.005350	3.9201	1.1400196	-0.0015305	0.078402	-0.019521841
888888888	0.005400	3.9299	1.1400234	-0.0015267	0.078598	-0.019424563
888888888	0.005450	3.9397	1.1400272	-0.0015229	0.078795	-0.019327649
888888888	0.005500	3.9496	1.1400310	-0.0015191	0.078992	-0.019231098
888888888	0.005550	3.9595	1.1400348	-0.0015153	0.079190	-0.019135285

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 888

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(T)
88888888	0.118100	1100.6010	1.1415448	-0.0000053	22.011969	-0.000000243
88888888	0.118150	1103.3559	1.1415448	-0.0000053	22.067068	-0.000000242
88888888	0.118200	1106.1178	1.1415447	-0.0000054	22.122304	-0.000000244
88888888	0.118250	1108.8863	1.1415447	-0.0000054	22.177679	-0.000000243
88888888	0.118300	1111.6618	1.1415447	-0.0000054	22.233193	-0.000000245
88888888	0.118350	1114.4451	1.1415447	-0.0000054	22.288846	-0.000000244
88888888	0.118400	1117.2346	1.1415447	-0.0000054	22.344637	-0.000000243
88888888	0.118450	1120.0311	1.1415447	-0.0000055	22.400569	-0.000000243
88888888	0.118500	1122.8347	1.1415447	-0.0000054	22.456640	-0.000000242
88888888	0.118550	1125.6451	1.1415447	-0.0000055	22.512852	-0.000000242
88888888	0.118600	1128.4626	1.1415447	-0.0000054	22.569205	-0.000000239
88888888	0.118650	1131.2873	1.1415447	-0.0000054	22.625699	-0.000000240
88888888	0.118700	1134.1194	1.1415447	-0.0000054	22.682334	-0.000000237
88888888	0.118750	1136.9580	1.1415447	-0.0000054	22.739110	-0.000000236
88888888	0.118800	1139.8040	1.1415448	-0.0000053	22.796029	-0.000000233
88888888	0.118850	1142.6571	1.1415448	-0.0000053	22.853091	-0.000000233
88888888	0.118900	1145.5175	1.1415448	-0.0000053	22.910295	-0.000000230
88888888	0.118950	1148.3846	1.1415449	-0.0000052	22.967642	-0.000000226
88888888	0.119000	1151.2593	1.1415450	-0.0000052	23.025133	-0.000000224
88888888	0.119050	1154.1409	1.1415450	-0.0000051	23.082768	-0.000000221
88888888	0.119100	1157.0301	1.1415451	-0.0000051	23.140547	-0.000000218
88888888	0.119150	1159.9262	1.1415451	-0.0000050	23.198471	-0.000000215
88888888	0.119200	1162.8297	1.1415452	-0.0000049	23.256540	-0.000000213
88888888	0.119250	1165.7401	1.1415451	-0.0000050	23.314754	-0.000000213
88888888	0.119300	1168.6584	1.1415452	-0.0000049	23.373114	-0.000000211
88888888	0.119350	1171.5837	1.1415452	-0.0000049	23.431620	-0.000000211
88888888	0.119400	1174.5162	1.1415452	-0.0000049	23.490272	-0.000000210

CALCULATIONS REQUIRED 2 MIN 1.3 SEC AND FLOT(S) REQUIRED 0 MIN 29.9 SEC

TOTAL PROBLEM TIME WAS 3 MIN 45.4 SEC

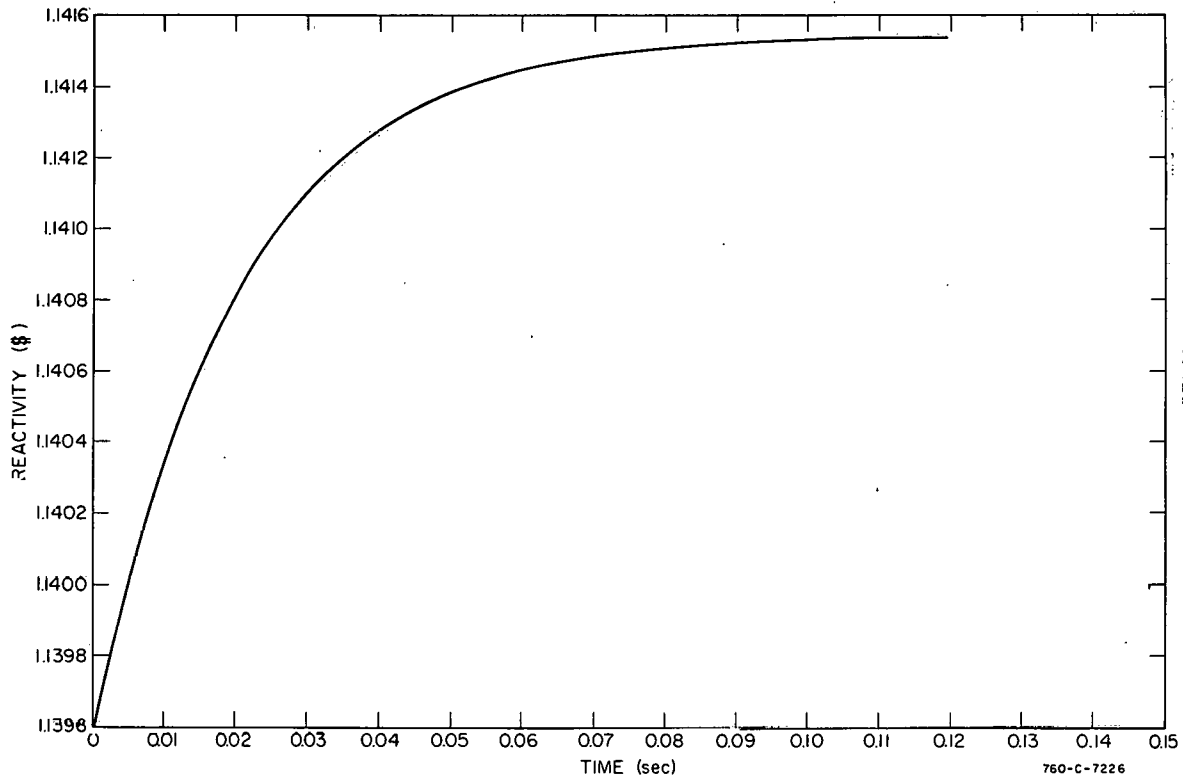


Fig. 29 REACTIVITY calculation on exponential test data.

sufficiently high to induce self-shutdown by the reactor, control rods were inserted at a constant, known rate. From the calibration of the control rods and the known rate of insertion, the reactivity of the system was calculated to decrease at a rate of $17\text{¢}/\text{sec}$. This transient then provides a means of comparing the REACTIVITY program with a power transient in which the reactivity of the system is known.

A listing of the results of the REACTIVITY program is given on pages 101 through 105 and a plot in Figure 30. The answers obtained from REACTIVITY are well within experimental accuracy.

SPORT 03/15/65

SPERT I KNOWN RATE OF INSERTION - 17 CENTS/SECOND

PAGE 4

REACTIVITY PROGRAM

DG P L I P F E S
E R C I N W I N C
L O S T A

SPERT I KNOWN RATE OF INSERTION - 17 CENTS/SECOND

A U C T P F P L
Y P O N E L L E
P S N G N T I T S

LAMBDA / BETA BAR

INITIAL AVERAGE RECIPR. PERIOD

INITIAL ENERGY

SOURCE

CONTROL CARD WAS-

0.00287000

3.21000001

6 0 0 0 0 0 0 0

-0.

-0.

LAMBDA'S

0.012700000

0.031700000

0.116000000

0.311000001

1.400000006

3.870000005

F'S

0.038000000

0.213000000

0.187999999

0.407000002

0.128000000

0.026000000

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	BIT)
20133981	1.425000	0.0016	0.9113902	0.	0.000508	0.
20133981	1.435000	0.0017	0.9120884	0.0006982	0.000524	1.332000017
20133981	1.445000	0.0017	0.9120458	0.0006556	0.000541	1.211124808
20133981	1.455000	0.0018	0.9120050	0.0006149	0.000559	1.099907696
20133981	1.465000	0.0019	0.9119378	0.0005476	0.000577	0.948507495
20133981	1.475000	0.0019	0.9118315	0.0004413	0.000596	0.740118459
20133981	1.485000	0.0020	0.9116994	0.0003092	0.000616	0.502131678
20133981	1.495000	0.0020	0.9115547	0.0001646	0.000636	0.258780934
20133981	1.505000	0.0021	0.9113986	0.0000084	0.000657	0.012808031
20133981	1.515000	0.0022	0.9112265	-0.0001637	0.000678	-0.241290793
20133981	1.525000	0.0023	0.9110244	-0.0003658	0.000700	-0.522263221
20133981	1.535000	0.0023	0.9107678	-0.0006224	0.000723	-0.860528246
20133981	1.545000	0.0024	0.9104304	-0.0009597	0.000747	-1.285126075
20133981	1.555000	0.0025	0.9100570	-0.0013332	0.000771	-1.728978544
20133981	1.565000	0.0025	0.9096720	-0.0017181	0.000796	-2.158400506
20133981	1.575000	0.0026	0.9093023	-0.0020879	0.000822	-2.540856272
20133981	1.585000	0.0027	0.9089556	-0.0024345	0.000848	-2.870405883
20133981	1.595000	0.0028	0.9086413	-0.0027488	0.000875	-3.140341789
20133981	1.605000	0.0028	0.9083645	-0.0030257	0.000903	-3.349598467
20133981	1.615000	0.0029	0.9081085	-0.0032817	0.000932	-3.520798475
20133981	1.625000	0.0030	0.9078882	-0.0035020	0.000962	-3.641344249
20133981	1.635000	0.0031	0.9076954	-0.0036948	0.000992	-3.723750204
20133981	1.645000	0.0032	0.9075082	-0.0038820	0.001024	-3.792393029
20133981	1.655000	0.0033	0.9073154	-0.0040747	0.001056	-3.858794630
20133981	1.665000	0.0034	0.9070989	-0.0042912	0.001089	-3.939651012
20133981	1.675000	0.0035	0.9068549	-0.0045353	0.001123	-4.036754429
20133981	1.685000	0.0036	0.9065882	-0.0048020	0.001159	-4.144254327
20133981	1.695000	0.0037	0.9063101	-0.0050801	0.001195	-4.251358926
20133981	1.705000	0.0038	0.9060505	-0.0053397	0.001232	-4.333565593
20133981	1.715000	0.0039	0.9058262	-0.0055639	0.001270	-4.379535019
20133981	1.725000	0.0040	0.9056611	-0.0057291	0.001310	-4.374061882
20133981	1.735000	0.0041	0.9055732	-0.0058170	0.001350	-4.308037519
20133981	1.745000	0.0042	0.9055772	-0.0058130	0.001392	-4.176290274
20133981	1.755000	0.0044	0.9056886	-0.0057015	0.001435	-3.973870367
20133981	1.765000	0.0045	0.9059135	-0.0054766	0.001479	-3.703147203
20133981	1.775000	0.0046	0.9062476	-0.0051426	0.001524	-3.373427421
20133981	1.785000	0.0048	0.9066816	-0.0047085	0.001571	-2.996331662
20133981	1.795000	0.0049	0.9072019	-0.0041882	0.001620	-2.585353702
20133981	1.805000	0.0051	0.9077855	-0.0036047	0.001670	-2.158228219
20133981	1.815000	0.0053	0.9084038	-0.0029864	0.001722	-1.734036580
20133981	1.825000	0.0055	0.9090171	-0.0023730	0.001776	-1.336109161
20133981	1.835000	0.0057	0.9095891	-0.0018011	0.001832	-0.983152799
20133981	1.845000	0.0059	0.9100888	-0.0013014	0.001890	-0.688581787
20133981	1.855000	0.0061	0.9104727	-0.0009175	0.001950	-0.470483061
20133981	1.865000	0.0063	0.9107053	-0.0006849	0.002012	-0.340326738
20133981	1.875000	0.0066	0.9107555	-0.0006347	0.002077	-0.305574030
20133981	1.885000	0.0068	0.9105917	-0.0007984	0.002144	-0.372465719
20133981	1.895000	0.0070	0.9102404	-0.0011497	0.002213	-0.519623816
20133981	1.905000	0.0072	0.9097476	-0.0016425	0.002284	-0.719279155
20133981	1.915000	0.0074	0.9091785	-0.0022116	0.002357	-0.538471794

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(T)
20133981	1.925000	0.0076	0.9085974	-0.0027927	0.002432	-1.148494124
20133981	1.935000	0.0078	0.9080673	-0.0033228	0.002509	-1.324508250
20133981	1.945000	0.0080	0.9076467	-0.0037435	0.002588	-1.446547508
20133981	1.955000	0.0082	0.9073757	-0.0040144	0.002669	-1.504020423
20133981	1.965000	0.0085	0.9072788	-0.0041114	0.002753	-1.493572444
20133981	1.975000	0.0087	0.9073662	-0.0040240	0.002839	-1.417513594
20133981	1.985000	0.0090	0.9076255	-0.0037647	0.002927	-1.285975203
20133981	1.995000	0.0093	0.9080160	-0.0033742	0.003019	-1.117609099
20133981	2.005000	0.0096	0.9084705	-0.0029196	0.003114	-0.937616497
20133981	2.015000	0.0100	0.9089093	-0.0024808	0.003212	-0.772375993
20133981	2.025000	0.0103	0.9092494	-0.0021408	0.003313	-0.646072343
20133981	2.035000	0.0107	0.9094453	-0.0019449	0.003419	-0.568922870
20133981	2.045000	0.0110	0.9094858	-0.0019043	0.003527	-0.539889194
20133981	2.055000	0.0114	0.9093678	-0.0020224	0.003639	-0.555678844
20133981	2.065000	0.0118	0.9090963	-0.0022938	0.003755	-0.610830560
20133981	2.075000	0.0121	0.9086985	-0.0026917	0.003875	-0.694714770
20133981	2.085000	0.0125	0.9082162	-0.0031739	0.003997	-0.794028431
20133981	2.095000	0.0128	0.9077047	-0.0036855	0.004123	-0.893798128
20133981	2.105000	0.0131	0.9072185	-0.0041717	0.004253	-0.980903886
20133981	2.115000	0.0135	0.9068150	-0.0045752	0.004386	-1.043142512
20133981	2.125000	0.0139	0.9065387	-0.0048514	0.004523	-1.072695673
20133981	2.135000	0.0143	0.9064149	-0.0049753	0.004663	-1.066927701
20133981	2.145000	0.0147	0.9064450	-0.0049452	0.004808	-1.028586105
20133981	2.155000	0.0151	0.9066162	-0.0047740	0.004957	-0.963147841
20133981	2.165000	0.0156	0.9068984	-0.0044918	0.005110	-0.878974244
20133981	2.175000	0.0161	0.9072613	-0.0041289	0.005269	-0.783663295
20133981	2.185000	0.0166	0.9076886	-0.0037015	0.005432	-0.681374937
20133981	2.195000	0.0172	0.9081515	-0.0032386	0.005602	-0.578148715
20133981	2.205000	0.0178	0.9086187	-0.0027715	0.005777	-0.479757167
20133981	2.215000	0.0184	0.9090605	-0.0023297	0.005958	-0.391016286
20133981	2.225000	0.0191	0.9094571	-0.0019330	0.006146	-0.314534768
20133981	2.235000	0.0198	0.9097954	-0.0015948	0.006340	-0.251546964
20133981	2.245000	0.0204	0.9100598	-0.0013304	0.006541	-0.203396156
20133981	2.255000	0.0212	0.9102474	-0.0011427	0.006749	-0.169318682
20133981	2.265000	0.0219	0.9103607	-0.0010295	0.006964	-0.147824226
20133981	2.275000	0.0226	0.9104066	-0.0009836	0.007187	-0.136862850
20133981	2.285000	0.0234	0.9103844	-0.0010058	0.007417	-0.135612121
20133981	2.295000	0.0241	0.9103016	-0.0010886	0.007654	-0.142223516
20133981	2.305000	0.0249	0.9101722	-0.0012180	0.007899	-0.154191429
20133981	2.315000	0.0257	0.9100216	-0.0013686	0.008152	-0.167888502
20133981	2.325000	0.0265	0.9098741	-0.0015160	0.008412	-0.180213528
20133981	2.335000	0.0273	0.9097532	-0.0016370	0.008681	-0.188567240
20133981	2.345000	0.0281	0.9096639	-0.0017262	0.008958	-0.192700526
20133981	2.355000	0.0290	0.9095924	-0.0017977	0.009244	-0.194473758
20133981	2.365000	0.0300	0.9095357	-0.0018544	0.009539	-0.194406372
20133981	2.375000	0.0309	0.9094808	-0.0019093	0.009843	-0.193972522
20133981	2.385000	0.0319	0.9094043	-0.0019859	0.010157	-0.195514079
20133981	2.395000	0.0329	0.9093031	-0.0020870	0.010481	-0.199122330
20133981	2.405000	0.0339	0.9091733	-0.0022168	0.010815	-0.204975959
20133981	2.415000	0.0350	0.9090095	-0.0023807	0.011159	-0.213331200

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(T)
20133981	2.425000	0.0360	0.9087903	-0.0025999	0.011514	-0.225793611
20133981	2.435000	0.0371	0.9085183	-0.0028718	0.011880	-0.241742099
20133981	2.445000	0.0382	0.9082191	-0.0031711	0.012256	-0.258738451
20133981	2.455000	0.0393	0.9079230	-0.0034672	0.012643	-0.274242055
20133981	2.465000	0.0404	0.9076624	-0.0037278	0.013041	-0.285850003
20133981	2.475000	0.0416	0.9074644	-0.0039257	0.013451	-0.291862804
20133981	2.485000	0.0428	0.9073269	-0.0040633	0.013872	-0.292905901
20133981	2.495000	0.0441	0.9072429	-0.0041473	0.014306	-0.289890405
20133981	2.505000	0.0454	0.9072215	-0.0041687	0.014753	-0.282557640
20133981	2.515000	0.0468	0.9072543	-0.0041358	0.015214	-0.271841578
20133981	2.525000	0.0482	0.9073293	-0.0040608	0.015689	-0.258833844
20133981	2.535000	0.0497	0.9074436	-0.0039465	0.016179	-0.243934235
20133981	2.545000	0.0513	0.9075813	-0.0038089	0.016684	-0.228296459
20133981	2.555000	0.0530	0.9077210	-0.0036692	0.017205	-0.213261338
20133981	2.565000	0.0546	0.9078413	-0.0035488	0.017743	-0.200009227
20133981	2.575000	0.0564	0.9079398	-0.0034504	0.018299	-0.188560858
20133981	2.585000	0.0582	0.9080205	-0.0033697	0.018872	-0.178557238
20133981	2.595000	0.0601	0.9080855	-0.0033047	0.019463	-0.169794122
20133981	2.605000	0.0620	0.9081380	-0.0032521	0.020073	-0.162012639
20133981	2.615000	0.0640	0.9081722	-0.0032180	0.020703	-0.155435028
20133981	2.625000	0.0660	0.9081800	-0.0032101	0.021353	-0.150335712
20133981	2.635000	0.0681	0.9081604	-0.0032297	0.022024	-0.146648156
20133981	2.645000	0.0702	0.9081223	-0.0032678	0.022715	-0.143861959
20133981	2.655000	0.0724	0.9080691	-0.0033211	0.023428	-0.141755417
20133981	2.665000	0.0747	0.9080022	-0.0033880	0.024164	-0.140208205
20133981	2.675000	0.0770	0.9079161	-0.0034740	0.024922	-0.139395736
20133981	2.685000	0.0794	0.9078112	-0.0035789	0.025704	-0.139238114
20133981	2.695000	0.0818	0.9076896	-0.0037006	0.026509	-0.139594283
20133981	2.705000	0.0843	0.9075505	-0.0038397	0.027340	-0.140442761
20133981	2.715000	0.0868	0.9073906	-0.0039996	0.028195	-0.141852846
20133981	2.725000	0.0894	0.9072073	-0.0041829	0.029077	-0.143857382
20133981	2.735000	0.0921	0.9069931	-0.0043971	0.029985	-0.146645403
20133981	2.745000	0.0948	0.9067426	-0.0046476	0.030919	-0.150312224
20133981	2.755000	0.0976	0.9064435	-0.0049467	0.031882	-0.155157369
20133981	2.765000	0.1004	0.9060938	-0.0052963	0.032872	-0.161120543
20133981	2.775000	0.1032	0.9056845	-0.0057056	0.033890	-0.168355877
20133981	2.785000	0.1061	0.9052157	-0.0061745	0.034937	-0.176731406
20133981	2.795000	0.1090	0.9046825	-0.0067077	0.036013	-0.186258974
20133981	2.805000	0.1118	0.9040775	-0.0073127	0.037117	-0.197018020
20133981	2.815000	0.1147	0.9033853	-0.0080049	0.038250	-0.209278753
20133981	2.825000	0.1176	0.9026070	-0.0087831	0.039411	-0.222857080
20133981	2.835000	0.1204	0.9017377	-0.0096524	0.040601	-0.237736957
20133981	2.845000	0.1231	0.9007728	-0.0106173	0.041819	-0.253888052
20133981	2.855000	0.1258	0.8997069	-0.0116832	0.043064	-0.271301609
20133981	2.865000	0.1284	0.8985382	-0.0128520	0.044335	-0.289885066
20133981	2.875000	0.1309	0.8972648	-0.0141253	0.045631	-0.309553616
20133981	2.885000	0.1333	0.8958919	-0.0154983	0.046952	-0.330087103
20133981	2.895000	0.1355	0.8944213	-0.0169688	0.048296	-0.351352081
20133981	2.905000	0.1376	0.8928660	-0.0185242	0.049661	-0.373009771
20133981	2.915000	0.1396	0.8912436	-0.0201466	0.051047	-0.396664712

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(T)
20133981	2.925000	0.1415	0.8895715	-0.0218186	0.052453	-0.415967170
20133981	2.935000	0.1433	0.8878747	-0.0235154	0.053877	-0.436467070
20133981	2.945000	0.1451	0.8861642	-0.0252260	0.055318	-0.456013806
20133981	2.955000	0.1468	0.8844472	-0.0269430	0.056777	-0.474537898
20133981	2.965000	0.1484	0.8827327	-0.0286575	0.058253	-0.491951123
20133981	2.975000	0.1500	0.8810302	-0.0303600	0.059744	-0.508165911
20133981	2.985000	0.1515	0.8793416	-0.0320486	0.061252	-0.523227535
20133981	2.995000	0.1531	0.8776633	-0.0337268	0.062775	-0.537266038
20133981	3.005000	0.1546	0.8759924	-0.0353978	0.064313	-0.550394937
20133981	3.015000	0.1561	0.8743227	-0.0370675	0.065867	-0.562762745
20133981	3.025000	0.1576	0.8726482	-0.0387419	0.067435	-0.574505560
20133981	3.035000	0.1590	0.8709684	-0.0404218	0.069018	-0.585672021
20133981	3.045000	0.1603	0.8692860	-0.0421042	0.070614	-0.596256770
20133981	3.055000	0.1617	0.8676114	-0.0437787	0.072224	-0.606149167
20133981	3.065000	0.1630	0.8659456	-0.0454445	0.073848	-0.615379550
20133981	3.075000	0.1644	0.8642989	-0.0470913	0.075485	-0.623849839
20133981	3.085000	0.1657	0.8626638	-0.0487264	0.077135	-0.631701715
20133981	3.095000	0.1670	0.8610423	-0.0503479	0.078799	-0.638944350
20133981	3.105000	0.1683	0.8594316	-0.0519586	0.080475	-0.645648509
20133981	3.115000	0.1696	0.8578321	-0.0535581	0.082164	-0.651839934
20133981	3.125000	0.1709	0.8562340	-0.0551562	0.083867	-0.657664336
20133981	3.135000	0.1721	0.8546330	-0.0567571	0.085582	-0.663192511
20133981	3.145000	0.1733	0.8530231	-0.0583670	0.087309	-0.668511681
20133981	3.155000	0.1745	0.8513963	-0.0599939	0.089048	-0.673723377
20133981	3.165000	0.1757	0.8497519	-0.0616383	0.090799	-0.678842224
20133981	3.175000	0.1768	0.8480964	-0.0632938	0.092561	-0.683804341
20133981	3.185000	0.1778	0.8464297	-0.0649605	0.094334	-0.688620202
20133981	3.195000	0.1789	0.8447596	-0.0666306	0.096118	-0.693217099
20133981	3.205000	0.1799	0.8430863	-0.0683038	0.097912	-0.697604947
20133981	3.215000	0.1809	0.8414119	-0.0699783	0.099716	-0.701776251
20133981	3.225000	0.1819	0.8397371	-0.0716531	0.101530	-0.705734953
20133981	3.235000	0.1828	0.8380633	-0.0733269	0.103353	-0.709479384
20133981	3.245000	0.1837	0.8363890	-0.0750012	0.105186	-0.713035151
20133981	3.255000	0.1846	0.8347114	-0.0766787	0.107028	-0.716438867
20133981	3.265000	0.1855	0.8330298	-0.0783604	0.108878	-0.719706908
20133981	3.275000	0.1863	0.8313463	-0.0800438	0.110737	-0.722826272
20133981	3.285000	0.1872	0.8296601	-0.0817300	0.112605	-0.725813590
20133981	3.295000	0.1879	0.8279711	-0.0834191	0.114480	-0.728677653
20133981	3.305000	0.1887	0.8262829	-0.0851073	0.116363	-0.731392711
20133981	3.315000	0.1895	0.8245989	-0.0867912	0.118254	-0.733938426
20133981	3.325000	0.1902	0.8229213	-0.0884689	0.120152	-0.736306101
20133981	3.335000	0.1909	0.8212552	-0.0901349	0.122058	-0.738460913
20133981	3.345000	0.1916	0.8195998	-0.0917904	0.123971	-0.740420789
20133981	3.355000	0.1923	0.8179547	-0.0934355	0.125890	-0.742197074
20133981	3.365000	0.1930	0.8163193	-0.0950709	0.127817	-0.743803024
20133981	3.375000	0.1937	0.8146961	-0.0966941	0.129751	-0.745227948
20133981	3.385000	0.1944	0.8130834	-0.0983068	0.131692	-0.746491618
20133981	3.395000	0.1951	0.8114723	-0.0999179	0.133639	-0.747668609
20133981	3.405000	0.1957	0.8098599	-0.1015303	0.135593	-0.748784371
20133981	3.415000	0.1964	0.8082468	-0.1031434	0.137554	-0.749838203

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	P(T)
20133981	3.425000	0.1970	0.8066287	-0.1047614	0.139521	-0.750863820
20133981	3.435000	0.1976	0.8050011	-0.1063891	0.141494	-0.751896054
20133981	3.445000	0.1982	0.8033596	-0.1080305	0.143473	-0.752965234
20133981	3.455000	0.1987	0.8017070	-0.1096832	0.145458	-0.754052721
20133981	3.465000	0.1993	0.8000405	-0.1113497	0.147448	-0.755177490
20133981	3.475000	0.1998	0.7983519	-0.1130383	0.149444	-0.756394505
20133981	3.485000	0.2002	0.7966378	-0.1147524	0.151443	-0.757724158
20133981	3.495000	0.2006	0.7948968	-0.1164933	0.153448	-0.759172954
20133981	3.505000	0.2010	0.7931311	-0.1182591	0.155456	-0.760725185
20133981	3.515000	0.2013	0.7913480	-0.1200421	0.157467	-0.762330353
20133981	3.525000	0.2016	0.7895462	-0.1218439	0.159482	-0.763997674
20133981	3.535000	0.2019	0.7877203	-0.1236699	0.161500	-0.765759930
20133981	3.545000	0.2021	0.7858759	-0.1255143	0.163519	-0.767580412
20133981	3.555000	0.2023	0.7840241	-0.1273660	0.165541	-0.769391239
20133981	3.565000	0.2025	0.7821706	-0.1292195	0.167565	-0.771160394
20133981	3.575000	0.2026	0.7803223	-0.1310679	0.169590	-0.772849433
20133981	3.585000	0.2028	0.7784864	-0.1329038	0.171617	-0.774419501
20133981	3.595000	0.2029	0.7766673	-0.1347228	0.173646	-0.775848851
20133981	3.605000	0.2031	0.7748634	-0.1365267	0.175675	-0.777153127
20133981	3.615000	0.2032	0.7730794	-0.1383108	0.177707	-0.778309479
20133981	3.625000	0.2033	0.7713198	-0.1400703	0.179739	-0.779297329
20133981	3.635000	0.2035	0.7695879	-0.1418023	0.181773	-0.780104309
20133981	3.645000	0.2037	0.7678826	-0.1435076	0.183809	-0.780741550
20133981	3.655000	0.2038	0.7661991	-0.1451911	0.185847	-0.781239763
20133981	3.665000	0.2040	0.7645299	-0.1468603	0.187886	-0.781644002
20133981	3.675000	0.2042	0.7628673	-0.1485229	0.189928	-0.781997189
20133981	3.685000	0.2044	0.7612104	-0.1501798	0.191971	-0.782306135
20133981	3.695000	0.2046	0.7595609	-0.1518293	0.194015	-0.782563239
20133981	3.705000	0.2047	0.7579130	-0.1534771	0.196062	-0.782799557
20133981	3.715000	0.2049	0.7562548	-0.1551353	0.198110	-0.783077016
20133981	3.725000	0.2050	0.7545786	-0.1568116	0.200159	-0.783433564
20133981	3.735000	0.2051	0.7528789	-0.1585113	0.202210	-0.783894315
20133981	3.745000	0.2052	0.7511576	-0.1602326	0.204261	-0.784448475
20133981	3.755000	0.2052	0.7494192	-0.1619710	0.206314	-0.785071999
20133981	3.765000	0.2053	0.7476639	-0.1637263	0.208366	-0.785762936
20133981	3.775000	0.2053	0.7458887	-0.1655014	0.210419	-0.786534511
20133981	3.785000	0.2052	0.7440939	-0.1672963	0.212471	-0.787384845
20133981	3.795000	0.2052	0.7422894	-0.1691008	0.214523	-0.788265258
20133981	3.805000	0.2051	0.7404874	-0.1709027	0.216574	-0.789119929
20133981	3.815000	0.2050	0.7387016	-0.1726886	0.218624	-0.789887026
20133981	3.825000	0.2050	0.7369434	-0.1744468	0.220674	-0.790516719
20133981	3.835000	0.2049	0.7352244	-0.1761658	0.222724	-0.790960498
20133981	3.845000	0.2049	0.7335426	-0.1778476	0.224773	-0.791231334
20133981	3.855000	0.2049	0.7318861	-0.1795040	0.226822	-0.791386023
20133981	3.865000	0.2049	0.7302520	-0.1811382	0.228872	-0.791440554
20133981	3.875000	0.2049	0.7286346	-0.1827556	0.230921	-0.791420959
20133981	3.885000	0.2049	0.7270282	-0.1843620	0.232970	-0.791354105
20133981	3.895000	0.2049	0.7254186	-0.1859715	0.235020	-0.791301288
20133981	3.905000	0.2049	0.7237924	-0.1875977	0.237069	-0.791319713
20133981	3.915000	0.2049	0.7221281	-0.1892620	0.239119	-0.791497909

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(T)
20133981	3.925000	0.2048	0.7204235	-0.1909667	0.241168	-0.791842274
20133981	3.935000	0.2047	0.7186851	-0.1927051	0.243215	-0.792322561
20133981	3.945000	0.2046	0.7169134	-0.1944767	0.245262	-0.792934254
20133981	3.955000	0.2044	0.7151165	-0.1962736	0.247307	-0.793642871
20133981	3.965000	0.2043	0.7133013	-0.1980889	0.249351	-0.794418894
20133981	3.975000	0.2041	0.7114745	-0.1999156	0.251392	-0.795234114
20133981	3.985000	0.2038	0.7096361	-0.2017541	0.253432	-0.796088912
20133981	3.995000	0.2036	0.7077912	-0.2035990	0.255469	-0.796962351
20133981	4.005000	0.2034	0.7059479	-0.2054423	0.257504	-0.797823213
20133981	4.015000	0.2031	0.7041188	-0.2072714	0.259536	-0.798623018
20133981	4.025000	0.2029	0.7023073	-0.2090829	0.261566	-0.799350165
20133981	4.035000	0.2027	0.7005051	-0.2108850	0.263594	-0.800037786
20133981	4.045000	0.2024	0.6987086	-0.2126816	0.265619	-0.800700933
20133981	4.055000	0.2022	0.6969126	-0.2144775	0.267642	-0.801359236
20133981	4.065000	0.2019	0.6951227	-0.2162675	0.269663	-0.801992618
20133981	4.075000	0.2017	0.6933445	-0.2180457	0.271681	-0.802580975
20133981	4.085000	0.2014	0.6915788	-0.2198114	0.273696	-0.803121872
20133981	4.095000	0.2012	0.6898343	-0.2215559	0.275709	-0.803585097
20133981	4.105000	0.2010	0.6881123	-0.2232778	0.277720	-0.803967178
20133981	4.115000	0.2007	0.6864068	-0.2249833	0.279729	-0.804291345
20133981	4.125000	0.2005	0.6847181	-0.2266721	0.281735	-0.804557748
20133981	4.135000	0.2003	0.6830454	-0.2283448	0.283739	-0.804769479
20133981	4.145000	0.2001	0.6813863	-0.2300038	0.285742	-0.804936469
20133981	4.155000	0.1999	0.6797419	-0.2316483	0.287742	-0.805055946
20133981	4.165000	0.1997	0.6781043	-0.2332859	0.289740	-0.805155635
20133981	4.175000	0.1995	0.6764584	-0.2349318	0.291736	-0.805288233
20133981	4.185000	0.1993	0.6748027	-0.2365875	0.293730	-0.805458106
20133981	4.195000	0.1991	0.6731345	-0.2382557	0.295722	-0.805673897
20133981	4.205000	0.1988	0.6714530	-0.2399372	0.297712	-0.805937879
20133981	4.215000	0.1986	0.6697650	-0.2416252	0.299699	-0.806226619
20133981	4.225000	0.1983	0.6680747	-0.2433155	0.301684	-0.806525692
20133981	4.235000	0.1981	0.6663846	-0.2450056	0.303666	-0.806826845
20133981	4.245000	0.1978	0.6646899	-0.2467003	0.305645	-0.807146102
20133981	4.255000	0.1976	0.6629899	-0.2484003	0.307622	-0.807485215
20133981	4.265000	0.1973	0.6612866	-0.2501036	0.309596	-0.807837568
20133981	4.275000	0.1970	0.6595704	-0.2518198	0.311568	-0.808234207
20133981	4.285000	0.1967	0.6578379	-0.2535523	0.313536	-0.808685161
20133981	4.295000	0.1964	0.6560862	-0.2553039	0.315502	-0.809198871
20133981	4.305000	0.1961	0.6543113	-0.2570789	0.317465	-0.809787668
20133981	4.315000	0.1957	0.6525070	-0.2588831	0.319424	-0.810469553
20133981	4.325000	0.1954	0.6506740	-0.2607162	0.321379	-0.811241515
20133981	4.335000	0.1950	0.6488050	-0.2625851	0.323331	-0.812124856
20133981	4.345000	0.1946	0.6469087	-0.2644815	0.325279	-0.813091733
20133981	4.355000	0.1942	0.6450001	-0.2663900	0.327222	-0.814094581
20133981	4.365000	0.1937	0.6430840	-0.2683062	0.329162	-0.815119058
20133981	4.375000	0.1933	0.6411635	-0.2702266	0.331097	-0.816155300
20133981	4.385000	0.1929	0.6392448	-0.2721454	0.333028	-0.817184784
20133981	4.395000	0.1924	0.6373401	-0.2740500	0.334955	-0.818170875
20133981	4.405000	0.1920	0.6354479	-0.2759422	0.336877	-0.819119148
20133981	4.415000	0.1916	0.6335617	-0.2778285	0.338795	-0.820049278

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(I)
20133981	4.425000	0.1912	0.6316811	-0.2797091	0.340709	-0.820962772
20133981	4.435000	0.1907	0.6298045	-0.2815857	0.342618	-0.821864381
20133981	4.445000	0.1903	0.6279249	-0.2834652	0.344523	-0.822774820
20133981	4.455000	0.1899	0.6260371	-0.2853531	0.346424	-0.823709562
20133981	4.465000	0.1894	0.6241323	-0.2872578	0.348321	-0.824693270
20133981	4.475000	0.1890	0.6222109	-0.2891792	0.350213	-0.825724624
20133981	4.485000	0.1885	0.6202984	-0.2910917	0.352100	-0.826730371
20133981	4.495000	0.1881	0.6184029	-0.2929873	0.353983	-0.827688210
20133981	4.505000	0.1876	0.6165289	-0.2948612	0.355861	-0.828585766
20133981	4.515000	0.1872	0.6146869	-0.2967032	0.357735	-0.829394661
20133981	4.525000	0.1868	0.6128867	-0.2985035	0.359604	-0.830088831
20133981	4.535000	0.1864	0.6111363	-0.3002539	0.361470	-0.830647223
20133981	4.545000	0.1860	0.6094371	-0.3019531	0.363332	-0.831067525
20133981	4.555000	0.1856	0.6077883	-0.3036019	0.365190	-0.831353769
20133981	4.565000	0.1853	0.6061874	-0.3052027	0.367045	-0.831514195
20133981	4.575000	0.1850	0.6046268	-0.3067634	0.368896	-0.831571221
20133981	4.585000	0.1847	0.6030891	-0.3083011	0.370745	-0.831572473
20133981	4.595000	0.1844	0.6015656	-0.3098246	0.372590	-0.831542060
20133981	4.605000	0.1841	0.6000426	-0.3113475	0.374433	-0.831517071
20133981	4.615000	0.1838	0.5985163	-0.3128739	0.376273	-0.831507698
20133981	4.625000	0.1835	0.5969886	-0.3144016	0.378110	-0.831508435
20133981	4.635000	0.1832	0.5954391	-0.3159510	0.379944	-0.831572875
20133981	4.645000	0.1829	0.5938658	-0.3175243	0.381775	-0.831705616
20133981	4.655000	0.1826	0.5922662	-0.3191239	0.383603	-0.831912838
20133981	4.665000	0.1823	0.5906288	-0.3207614	0.385427	-0.832223296
20133981	4.675000	0.1819	0.5889532	-0.3224369	0.387248	-0.832636766
20133981	4.685000	0.1815	0.5872394	-0.3241508	0.389065	-0.833152704
20133981	4.695000	0.1811	0.5854862	-0.3259040	0.390879	-0.833772555
20133981	4.705000	0.1807	0.5836990	-0.3276912	0.392688	-0.834482022
20133981	4.715000	0.1803	0.5818825	-0.3295077	0.394493	-0.835268110
20133981	4.725000	0.1799	0.5800469	-0.3313432	0.396294	-0.836104326
20133981	4.735000	0.1794	0.5782033	-0.3331868	0.398091	-0.836962290
20133981	4.745000	0.1790	0.5763578	-0.3350324	0.399883	-0.837826855
20133981	4.755000	0.1785	0.5745198	-0.3368704	0.401670	-0.838674068
20133981	4.765000	0.1781	0.5727004	-0.3386898	0.403453	-0.839476869
20133981	4.775000	0.1777	0.5709042	-0.3404860	0.405232	-0.840224423
20133981	4.785000	0.1773	0.5691475	-0.3422427	0.407007	-0.840876937
20133981	4.795000	0.1769	0.5674237	-0.3439664	0.408777	-0.841451578
20133981	4.805000	0.1765	0.5657212	-0.3456690	0.410544	-0.841977723
20133981	4.815000	0.1761	0.5640349	-0.3473552	0.412307	-0.842467755
20133981	4.825000	0.1757	0.5623511	-0.3490391	0.414066	-0.842955753
20133981	4.835000	0.1753	0.5606560	-0.3507342	0.415821	-0.8434474627
20133981	4.845000	0.1749	0.5589499	-0.3524403	0.417572	-0.844023325
20133981	4.855000	0.1745	0.5572276	-0.3541626	0.419319	-0.844614215
20133981	4.865000	0.1741	0.5554910	-0.3558992	0.421062	-0.845242292
20133981	4.875000	0.1737	0.5537414	-0.3576488	0.422801	-0.845904343
20133981	4.885000	0.1733	0.5519893	-0.3594009	0.424535	-0.846575104
20133981	4.895000	0.1728	0.5502424	-0.3611478	0.426266	-0.847236469
20133981	4.905000	0.1724	0.5485165	-0.3628736	0.427992	-0.847891530
20133981	4.915000	0.1720	0.5468294	-0.3645608	0.429714	-0.848379575

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(T)
20133981	4.925000	0.1717	0.5451915	-0.3661986	0.431433	-0.848796502
20133981	4.935000	0.1713	0.5435947	-0.3677954	0.433148	-0.849122658
20133981	4.945000	0.1709	0.5420385	-0.3693516	0.434859	-0.849359773
20133981	4.955000	0.1706	0.5405214	-0.3708688	0.436567	-0.849512182
20133981	4.965000	0.1703	0.5390281	-0.3723621	0.438271	-0.849615291
20133981	4.975000	0.1700	0.5375442	-0.3738460	0.439973	-0.849702336
20133981	4.985000	0.1697	0.5360652	-0.3753249	0.441671	-0.849783637
20133981	4.995000	0.1693	0.5345665	-0.3768257	0.443366	-0.849919446
20133981	5.005000	0.1690	0.5330206	-0.3783696	0.445058	-0.850157298
20133981	5.015000	0.1687	0.5314274	-0.3799628	0.446747	-0.850510322
20133981	5.025000	0.1683	0.5297739	-0.3816163	0.448432	-0.851001896
20133981	5.035000	0.1679	0.5280335	-0.3833567	0.450113	-0.851689965
20133981	5.045000	0.1675	0.5261967	-0.3851934	0.451790	-0.852594130
20133981	5.055000	0.1670	0.5242501	-0.3871401	0.453462	-0.853742421
20133981	5.065000	0.1665	0.5221869	-0.3892032	0.455130	-0.855147526
20133981	5.075000	0.1660	0.5200094	-0.3913808	0.456792	-0.856802896
20133981	5.085000	0.1654	0.5177318	-0.3936583	0.458449	-0.858675048
20133981	5.095000	0.1648	0.5153844	-0.3960058	0.460099	-0.860696942
20133981	5.105000	0.1641	0.5129881	-0.3984021	0.461743	-0.862821765
20133981	5.115000	0.1635	0.5105912	-0.4007990	0.463381	-0.864944562
20133981	5.125000	0.1629	0.5082154	-0.4031748	0.465013	-0.867018782
20133981	5.135000	0.1623	0.5058677	-0.4055225	0.466638	-0.869029716
20133981	5.145000	0.1616	0.5035675	-0.4078227	0.468258	-0.870936595
20133981	5.155000	0.1611	0.5013517	-0.4100384	0.469871	-0.872661486
20133981	5.165000	0.1605	0.4992140	-0.4121762	0.471479	-0.874219343
20133981	5.175000	0.1600	0.4971379	-0.4142523	0.473082	-0.875646226
20133981	5.185000	0.1595	0.4950999	-0.4162902	0.474679	-0.876992807
20133981	5.195000	0.1590	0.4930745	-0.4183157	0.476271	-0.878313579
20133981	5.205000	0.1585	0.4910506	-0.4203396	0.477859	-0.879631653
20133981	5.215000	0.1580	0.4890204	-0.4223698	0.479441	-0.880963542
20133981	5.225000	0.1574	0.4869853	-0.4244049	0.481018	-0.882306330
20133981	5.235000	0.1569	0.4849702	-0.4264199	0.482589	-0.883608073
20133981	5.245000	0.1564	0.4829805	-0.4284096	0.484156	-0.884858102
20133981	5.255000	0.1560	0.4810342	-0.4303560	0.485718	-0.886019647
20133981	5.265000	0.1555	0.4791270	-0.4322631	0.487276	-0.887102030
20133981	5.275000	0.1550	0.4772609	-0.4341293	0.488828	-0.888102047
20133981	5.285000	0.1546	0.4754583	-0.4359319	0.490376	-0.888974130
20133981	5.295000	0.1542	0.4737354	-0.4376547	0.491920	-0.889686249
20133981	5.305000	0.1538	0.4720804	-0.4393098	0.493460	-0.890263706
20133981	5.315000	0.1534	0.4704807	-0.4409095	0.494996	-0.890732668
20133981	5.325000	0.1531	0.4689106	-0.4424795	0.496529	-0.891145676
20133981	5.335000	0.1527	0.4673692	-0.4440210	0.498058	-0.891505137
20133981	5.345000	0.1524	0.4658489	-0.4455412	0.499583	-0.891826309
20133981	5.355000	0.1520	0.4643456	-0.4470445	0.501105	-0.892117694
20133981	5.365000	0.1517	0.4628552	-0.4485350	0.502623	-0.892387830
20133981	5.375000	0.1513	0.4613698	-0.4500203	0.504139	-0.892651938
20133981	5.385000	0.1510	0.4598571	-0.4515331	0.505651	-0.892974593
20133981	5.395000	0.1507	0.4583000	-0.4530902	0.507159	-0.893388703
20133981	5.405000	0.1503	0.4566800	-0.4547101	0.508664	-0.893930219
20133981	5.415000	0.1499	0.4549719	-0.4564182	0.510165	-0.894647926

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(T)
20133981	5.425000	0.1495	0.4531794	-0.4582107	0.511662	-0.895533361
20133981	5.435000	0.1491	0.4513021	-0.4600880	0.513155	-0.896586180
20133981	5.445000	0.1486	0.4493311	-0.4620591	0.514644	-0.897822902
20133981	5.455000	0.1482	0.4472651	-0.4641251	0.516128	-0.899244614
20133981	5.465000	0.1477	0.4451344	-0.4662557	0.517607	-0.900791645
20133981	5.475000	0.1471	0.4429631	-0.4684271	0.519080	-0.902417131
20133981	5.485000	0.1466	0.4407699	-0.4706202	0.520549	-0.904084101
20133981	5.495000	0.1461	0.4385956	-0.4727946	0.522013	-0.905714579
20133981	5.505000	0.1456	0.4364635	-0.4749267	0.523471	-0.907263979
20133981	5.515000	0.1451	0.4343885	-0.4770017	0.524925	-0.908704638
20133981	5.525000	0.1447	0.4323812	-0.4790089	0.526374	-0.910016693
20133981	5.535000	0.1442	0.4304517	-0.4809384	0.527818	-0.911182158
20133981	5.545000	0.1438	0.4285966	-0.4827936	0.529258	-0.912208222
20133981	5.555000	0.1434	0.4268156	-0.4845746	0.530694	-0.913096264
20133981	5.565000	0.1430	0.4251010	-0.4862892	0.532126	-0.913861439
20133981	5.575000	0.1426	0.4234338	-0.4879564	0.533554	-0.914540179
20133981	5.585000	0.1422	0.4217568	-0.4896334	0.534978	-0.915239982
20133981	5.595000	0.1419	0.4200498	-0.4913404	0.536399	-0.915998586
20133981	5.605000	0.1415	0.4182995	-0.4930906	0.537815	-0.916840136
20133981	5.615000	0.1411	0.4164882	-0.4949020	0.539228	-0.917797469
20133981	5.625000	0.1406	0.4146229	-0.4967672	0.540636	-0.918856502
20133981	5.635000	0.1402	0.4127231	-0.4986670	0.542041	-0.919980921
20133981	5.645000	0.1398	0.4107940	-0.5005961	0.543441	-0.921160623
20133981	5.655000	0.1394	0.4088466	-0.5025436	0.544836	-0.922375217
20133981	5.665000	0.1389	0.4068945	-0.5044957	0.546228	-0.923599422
20133981	5.675000	0.1385	0.4049451	-0.5064451	0.547615	-0.924819730
20133981	5.685000	0.1381	0.4030035	-0.5083867	0.548998	-0.926026836
20133981	5.695000	0.1376	0.4010654	-0.5103247	0.550376	-0.927228555
20133981	5.705000	0.1372	0.3991282	-0.5122619	0.551751	-0.928429931
20133981	5.715000	0.1368	0.3971825	-0.5142077	0.553121	-0.929647900
20133981	5.725000	0.1364	0.3951928	-0.5161974	0.554487	-0.930946358
20133981	5.735000	0.1359	0.3931521	-0.5182381	0.555848	-0.932337701
20133981	5.745000	0.1355	0.3910556	-0.5203346	0.557205	-0.933829889
20133981	5.755000	0.1350	0.3889443	-0.5224459	0.558557	-0.935348958
20133981	5.765000	0.1345	0.3868200	-0.5245702	0.559905	-0.936891593
20133981	5.775000	0.1341	0.3846915	-0.5266987	0.561248	-0.938441984
20133981	5.785000	0.1336	0.3825653	-0.5288249	0.562586	-0.939988628
20133981	5.795000	0.1332	0.3804672	-0.5309229	0.563920	-0.941485614
20133981	5.805000	0.1327	0.3784153	-0.5329748	0.565250	-0.942901351
20133981	5.815000	0.1323	0.3764154	-0.5349748	0.566575	-0.944225997
20133981	5.825000	0.1319	0.3744765	-0.5369137	0.567896	-0.945543988
20133981	5.835000	0.1315	0.3725987	-0.5387915	0.569213	-0.946555831
20133981	5.845000	0.1311	0.3708165	-0.5405736	0.570526	-0.947501220
20133981	5.855000	0.1307	0.3690959	-0.5422943	0.571835	-0.948340856
20133981	5.865000	0.1304	0.3673984	-0.5439918	0.573140	-0.949142195
20133981	5.875000	0.1300	0.3656818	-0.5457083	0.574442	-0.949979141
20133981	5.885000	0.1296	0.3639391	-0.5474511	0.575741	-0.950863712
20133981	5.895000	0.1293	0.3621783	-0.5492118	0.577036	-0.951781631
20133981	5.905000	0.1289	0.3603397	-0.5510505	0.578326	-0.952836372
20133981	5.915000	0.1285	0.3584272	-0.5529630	0.579613	-0.954020359

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	(BIT)
20133981	5.925000	0.1281	0.3564577	-0.5549324	0.580896	-0.955303855
20133981	5.935000	0.1277	0.3544929	-0.5568973	0.582175	-0.956580497
20133981	5.945000	0.1273	0.3525618	-0.5588283	0.583450	-0.957800157
20133981	5.955000	0.1269	0.3506956	-0.5606946	0.584721	-0.958910152
20133981	5.965000	0.1265	0.3489427	-0.5624475	0.585988	-0.959828041
20133981	5.975000	0.1262	0.3473290	-0.5640612	0.587251	-0.960510470
20133981	5.985000	0.1259	0.3458666	-0.5655236	0.588512	-0.960938051
20133981	5.995000	0.1256	0.3444871	-0.5669031	0.589770	-0.961227976
20133981	6.005000	0.1253	0.3431660	-0.5682241	0.591024	-0.961422458
20133981	6.015000	0.1251	0.3418721	-0.5695181	0.592276	-0.961574756
20133981	6.025000	0.1248	0.3405927	-0.5707975	0.593526	-0.961706229
20133981	6.035000	0.1245	0.3393043	-0.5720858	0.594773	-0.961856514
20133981	6.045000	0.1243	0.3379514	-0.5734387	0.596017	-0.962118819
20133981	6.055000	0.1240	0.3365400	-0.5748502	0.597258	-0.962482713
20133981	6.065000	0.1237	0.3350656	-0.5763245	0.598496	-0.962954819
20133981	6.075000	0.1234	0.3335577	-0.5778324	0.599731	-0.963485688
20133981	6.085000	0.1231	0.3320183	-0.5793719	0.600963	-0.964071803
20133981	6.095000	0.1228	0.3304604	-0.5809298	0.602193	-0.964690961
20133981	6.105000	0.1225	0.3288976	-0.5824926	0.603419	-0.965320662
20133981	6.115000	0.1221	0.3273282	-0.5840619	0.604642	-0.965963453
20133981	6.125000	0.1218	0.3257126	-0.5856776	0.605862	-0.966685146
20133981	6.135000	0.1215	0.3240211	-0.5873690	0.607079	-0.967533916
20133981	6.145000	0.1212	0.3222656	-0.5891245	0.608292	-0.968489915
20133981	6.155000	0.1208	0.3204543	-0.5909359	0.609502	-0.969539262
20133981	6.165000	0.1205	0.3186149	-0.5927753	0.610708	-0.970636055
20133981	6.175000	0.1201	0.3167493	-0.5946408	0.611911	-0.971776858
20133981	6.185000	0.1197	0.3148546	-0.5965356	0.613110	-0.972966582
20133981	6.195000	0.1194	0.3129582	-0.5984320	0.614306	-0.974160068
20133981	6.205000	0.1190	0.3110870	-0.6003032	0.615497	-0.975313865
20133981	6.215000	0.1187	0.3092986	-0.6020916	0.616686	-0.976334415
20133981	6.225000	0.1184	0.3076277	-0.6037625	0.617871	-0.977166079
20133981	6.235000	0.1180	0.3060779	-0.6053123	0.619053	-0.977803849
20133981	6.245000	0.1178	0.3046474	-0.6067428	0.620232	-0.978251271
20133981	6.255000	0.1175	0.3033260	-0.6080641	0.621408	-0.978525683
20133981	6.265000	0.1173	0.3020532	-0.6093370	0.622582	-0.978725158
20133981	6.275000	0.1170	0.3008241	-0.6105661	0.623754	-0.978857689
20133981	6.285000	0.1168	0.2996129	-0.6117772	0.624923	-0.978964642
20133981	6.295000	0.1165	0.2983986	-0.6129915	0.626089	-0.979080014
20133981	6.305000	0.1163	0.2971631	-0.6142271	0.627254	-0.979232460
20133981	6.315000	0.1160	0.2958267	-0.6155635	0.628415	-0.979548827
20133981	6.325000	0.1158	0.2943708	-0.6170194	0.629574	-0.980057850
20133981	6.335000	0.1155	0.2928205	-0.6185697	0.630731	-0.980719149
20133981	6.345000	0.1152	0.2912003	-0.6201899	0.631884	-0.981493227
20133981	6.355000	0.1149	0.2895351	-0.6218551	0.633034	-0.982340135
20133981	6.365000	0.1146	0.2878251	-0.6235650	0.634182	-0.983259171
20133981	6.375000	0.1143	0.2860168	-0.6253734	0.635326	-0.984334737
20133981	6.385000	0.1139	0.2841360	-0.6272542	0.636467	-0.985525332
20133981	6.395000	0.1136	0.2821863	-0.6292039	0.637604	-0.986825004
20133981	6.405000	0.1132	0.2801490	-0.6312411	0.638738	-0.988262475
20133981	6.415000	0.1129	0.2780201	-0.6333700	0.639869	-0.989843599

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	CCMP. REACT.	ENERGY	B(T)
20133981	6.425000	0.1125	0.2757573	-0.6356329	0.640995	-0.991633989
20133981	6.435000	0.1121	0.2733397	-0.6380504	0.642118	-0.993665293
20133981	6.445000	0.1116	0.2707398	-0.6406504	0.643236	-0.995979555
20133981	6.455000	0.1111	0.2679226	-0.6434676	0.644350	-0.998630114
20133981	6.465000	0.1107	0.2649167	-0.6464734	0.645459	-1.001571313
20133981	6.475000	0.1101	0.2617789	-0.6496112	0.646563	-1.004714340
20133981	6.485000	0.1096	0.2585394	-0.6528508	0.647662	-1.008011878
20133981	6.495000	0.1091	0.2552213	-0.6561688	0.648755	-1.011427596
20133981	6.505000	0.1085	0.2518418	-0.6595483	0.649843	-1.014934823
20133981	6.515000	0.1080	0.2484120	-0.6629782	0.650925	-1.018516257
20133981	6.525000	0.1074	0.2450393	-0.6663509	0.652002	-1.022006676
20133981	6.535000	0.1069	0.2417608	-0.6696293	0.653074	-1.025349528
20133981	6.545000	0.1064	0.2385866	-0.6728036	0.654141	-1.028530240
20133981	6.555000	0.1059	0.2355023	-0.6758879	0.655202	-1.031571150
20133981	6.565000	0.1054	0.2324957	-0.6788945	0.656259	-1.034491330
20133981	6.575000	0.1050	0.2295408	-0.6818493	0.657311	-1.037330940
20133981	6.585000	0.1045	0.2266017	-0.6847884	0.658359	-1.040144831
20133981	6.595000	0.1040	0.2236445	-0.6877457	0.659401	-1.042984724
20133981	6.605000	0.1036	0.2206447	-0.6907455	0.660440	-1.045887440
20133981	6.615000	0.1031	0.2175958	-0.6937944	0.661473	-1.0488862785
20133981	6.625000	0.1026	0.2144898	-0.6969004	0.662502	-1.051922575
20133981	6.635000	0.1021	0.2113333	-0.7000568	0.663525	-1.055056572
20133981	6.645000	0.1017	0.2081374	-0.7032528	0.664544	-1.058248058
20133981	6.655000	0.1012	0.2049259	-0.7064643	0.665559	-1.061460808
20133981	6.665000	0.1007	0.2017374	-0.7096528	0.666568	-1.064636886
20133981	6.675000	0.1002	0.1986333	-0.7127568	0.667573	-1.067684457
20133981	6.685000	0.0998	0.1956193	-0.7157709	0.668573	-1.070595428
20133981	6.695000	0.0994	0.1926901	-0.7187001	0.669568	-1.073378101
20133981	6.705000	0.0989	0.1898345	-0.7215556	0.670560	-1.076049581
20133981	6.715000	0.0985	0.1870156	-0.7243745	0.671547	-1.078665391
20133981	6.725000	0.0981	0.1842046	-0.7271856	0.672530	-1.081268534
20133981	6.735000	0.0977	0.1813745	-0.7300157	0.673509	-1.083899185
20133981	6.745000	0.0973	0.1785040	-0.7328862	0.674483	-1.086588785
20133981	6.755000	0.0968	0.1755825	-0.7358077	0.675454	-1.089352891
20133981	6.765000	0.0964	0.1726165	-0.7387737	0.676420	-1.092181817
20133981	6.775000	0.0960	0.1696506	-0.7417396	0.677382	-1.095009461
20133981	6.785000	0.0956	0.1666804	-0.7447097	0.678340	-1.097842127
20133981	6.795000	0.0951	0.1637146	-0.7476755	0.679293	-1.100667253
20133981	6.805000	0.0947	0.1607786	-0.7506116	0.680242	-1.103447512
20133981	6.815000	0.0943	0.1579492	-0.7534410	0.681187	-1.106070086
20133981	6.825000	0.0939	0.1552351	-0.7561551	0.682129	-1.108522698
20133981	6.835000	0.0936	0.1526133	-0.7587768	0.683066	-1.110839590
20133981	6.845000	0.0932	0.1500721	-0.7613180	0.684000	-1.113038331
20133981	6.855000	0.0928	0.1476081	-0.7637821	0.684930	-1.115124300
20133981	6.865000	0.0925	0.1452260	-0.7661641	0.685857	-1.117090821
20133981	6.875000	0.0922	0.1429542	-0.7684360	0.686780	-1.118897036
20133981	6.885000	0.0918	0.1407841	-0.7706061	0.687700	-1.120555833
20133981	6.895000	0.0915	0.1387212	-0.7726689	0.688617	-1.122059435
20133981	6.905000	0.0912	0.1367837	-0.7746065	0.689531	-1.123382241
20133981	6.915000	0.0910	0.1350035	-0.7763867	0.690442	-1.124478266

REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL 0

RECORD NO.	TIME	POWER	REACTIVITY	COMP. REACT.	ENERGY	B(T)
20133981	6.925000	0.0907	0.1333441	-0.7780460	0.691350	-1.12540088E
20133981	6.935000	0.0905	0.1318141	-0.7795760	0.692256	-1.12613840E
20133981	6.945000	0.0902	0.1304235	-0.7809667	0.693159	-1.12667670E
20133981	6.955000	0.0900	0.1291836	-0.7822066	0.694061	-1.12700001E
20133981	6.965000	0.0898	0.1280718	-0.7833183	0.694960	-1.12714140E
20133981	6.975000	0.0896	0.1269866	-0.7844036	0.695857	-1.12724748E
20133981	6.985000	0.0894	0.1259115	-0.7854786	0.696753	-1.12734179E
20133981	6.995000	0.0892	0.1248348	-0.7865553	0.697646	-1.12744133E
20133981	7.005000	0.0891	0.1237485	-0.7876417	0.698538	-1.12755751E
20133981	7.015000	0.0889	0.1226475	-0.7887427	0.699428	-1.12769737E
20133981	7.025000	0.0887	0.1214596	-0.7899305	0.700315	-1.12796405E
20133981	7.035000	0.0885	0.1201900	-0.7912002	0.701201	-1.12834999E
20133981	7.045000	0.0883	0.1188458	-0.7925443	0.702085	-1.12884444E
20133981	7.055000	0.0880	0.1174340	-0.7939562	0.702966	-1.12943740E
20133981	7.065000	0.0878	0.1159522	-0.7954380	0.703845	-1.13013182E
20133981	7.075000	0.0876	0.1144246	-0.7969655	0.704722	-1.13089303E
20133981	7.085000	0.0874	0.1128635	-0.7985266	0.705597	-1.13170361E
20133981	7.095000	0.0871	0.1112750	-0.8001152	0.706469	-1.13255468E
20133981	7.105000	0.0869	0.1096542	-0.8017360	0.707339	-1.13345304E
20133981	7.115000	0.0866	0.1079789	-0.8034113	0.708207	-1.13442997E
20133981	7.125000	0.0864	0.1062924	-0.8050977	0.709072	-1.13542403E
20133981	7.135000	0.0862	0.1045879	-0.8068023	0.709935	-1.13644501E
20133981	7.145000	0.0859	0.1028754	-0.8085148	0.710796	-1.13747863E
20133981	7.155000	0.0857	0.1011608	-0.8102294	0.711654	-1.13851654E
20133981	7.165000	0.0854	0.0994373	-0.8119529	0.712509	-1.13956831E
20133981	7.175000	0.0852	0.0977462	-0.8136440	0.713362	-1.14057593E
20133981	7.185000	0.0850	0.0961007	-0.8152895	0.714213	-1.14152106E
20133981	7.195000	0.0847	0.0945068	-0.8168833	0.715062	-1.14239534E
20133981	7.205000	0.0845	0.0929628	-0.8184274	0.715908	-1.14320163E
20133981	7.215000	0.0843	0.0915783	-0.8198119	0.716752	-1.14378660E
20133981	7.225000	0.0841	0.0901943	-0.8211959	0.717595	-1.14437297E
20133981	7.235000	0.0839	0.0888133	-0.8225768	0.718435	-1.14495688E
20133981	7.245000	0.0837	0.0874391	-0.8239511	0.719273	-1.14553342E
20133981	7.255000	0.0835	0.0860610	-0.8253291	0.720109	-1.14611713E
20133981	7.265000	0.0833	0.0846735	-0.8267167	0.720943	-1.14671596E

CALCULATIONS REQUIRED 0 MIN 28.1 SEC

TOTAL PROBLEM TIME WAS 1 MIN 38.5 SEC

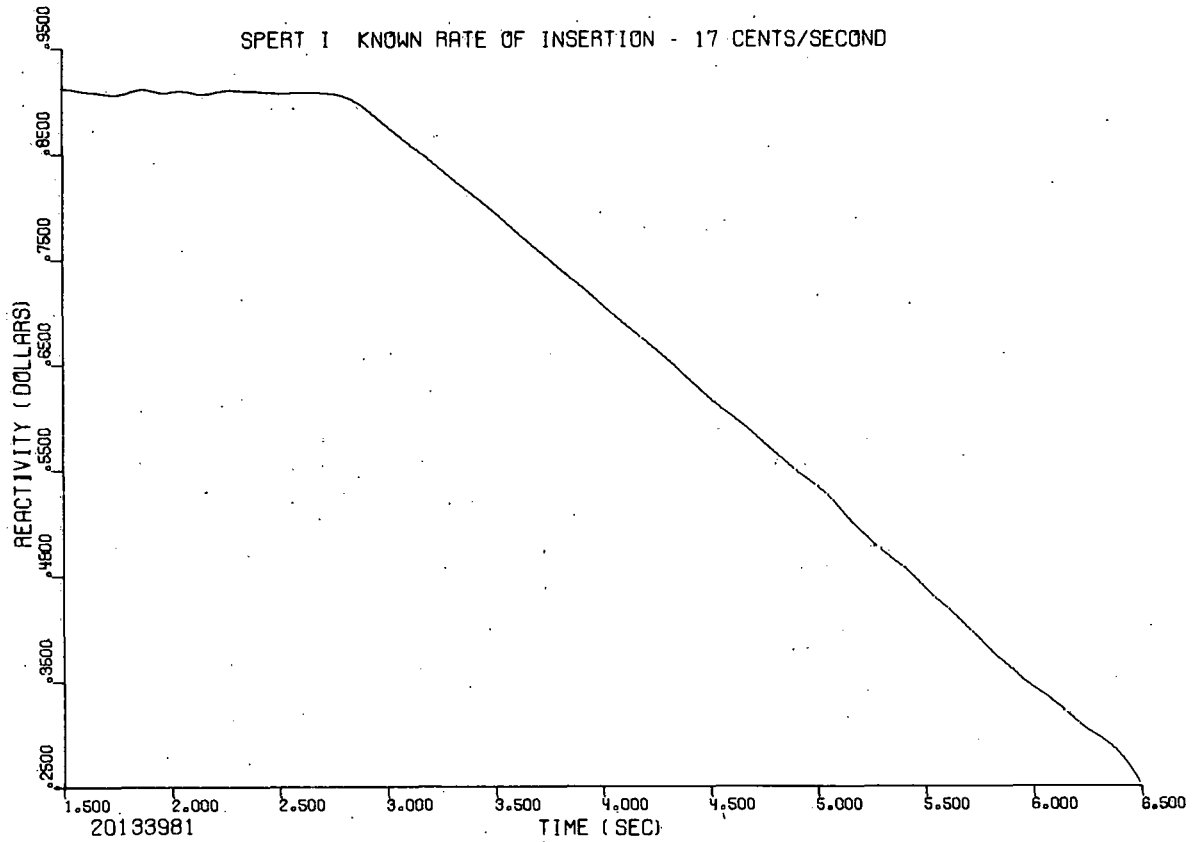


Fig. 30 REACTIVITY calculations on power data with a known rate of compensated reactivity insertion.

4. CHECKOUT OF FREQUENCY RESPONSE

Because of the nature of the calculations made in the FREQUENCY RESPONSE program, a rather detailed error analysis and checkout was necessary. This analysis is presented in Section II, page 3.

VII. OPERATING TIME

In this section, some estimates are given of the time required to select, prepare and process SPORT input data.

1. DATA SELECTION AND CONVERSION

The time required for BCD-to-binary conversion and normalization of one Spert 1-3 data card is on the order of 200 milliseconds. The time required to prepare other types of card data is generally less. Type 5 or "tape" data is already in binary form. However, approximately 300 milliseconds (729 tape drive) are required for each data record that must be passed over in order to reach the first data record used in the problem.

2. THE SMOOTH PROGRAM

Approximately 50 milliseconds per output point are required to smooth even time increment data on 25 points and obtain an output listing. Smoothing the same data on 99 points would require about 95 milliseconds per output point. A time saving of about 50 percent may be realized by deleting the output listing. Smoothing data separated by unequal time increments requires that an additional 10 to 30 percent be added to the estimates given above.

3. THE REACTIVITY PROGRAM

REACTIVITY calculations using 6 delayed neutron groups require about 50 milliseconds per point. Fifteen-group calculations require about 55 milliseconds per point.

4. THE FREQUENCY RESPONSE PROGRAM

FREQUENCY RESPONSE calculations require about 3 milliseconds per input point per frequency. In other words, a transient response of 2000 points may be analyzed at 100 separate frequencies in approximately 10 minutes.

5. PLOTS

Approximately 10 to 15 seconds of computer time are required to generate a standard-size 10- by 7-inch plot. Increasing the size of the plot to 30 by 26 inches nearly doubles the required computer time. CALCOMP plotter time for a 10- by 7-inch plot is about 2 minutes and for a 30- by 26-inch plot is about 10 minutes.

VIII. REFERENCES

1. F. Schroeder (ed.), Quarterly Technical Report Spert Project, April, May, June, 1962, IDO-16806 (September 1962) pp 29-30.
2. F. Schroeder (ed.), Quarterly Technical Report Spert Project, July, August, September, 1962, IDO-16829 (February 1963) pp 27-28.
3. F. Schroeder (ed.), Quarterly Technical Report Spert Project, January, February, March, 1962, IDO-16788 (August 1962) pp 14-15.
4. C. R. Wylie, Jr., Advance Engineering Mathematics, 2d ed. New York: McGraw-Hill Publishing Co., 1960.
5. R. V. Churchill, Complex Variables and Applications. New York: McGraw-Hill Publishing Co., 1948.

APPENDIX A -- PROOF OF THEOREMS USED IN SECTION II

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APPENDIX A -- PROOF OF THEOREMS USED IN SECTION II

THEOREM I: If $f(t)$ is a real-valued function such that $f(t) = f(t_n - t)$ for $0 \leq t \leq t_n$ and zero elsewhere and if

$$F(\omega) = \int_0^{\infty} f(t) e^{-i\omega t} dt, \quad (\text{A-1})$$

then, for $\omega = \frac{(2m-1)\pi}{t_n}$ (m an integer), the real part of $F(\omega)$ is zero; and for $\omega = \frac{2m\pi}{t_n}$, the imaginary part of $F(\omega)$ is zero.

Proof: Since $f(t) = 0$ for $t > t_n$,

$$F(\omega) = \int_0^{\infty} f(t) e^{-i\omega t} dt = \int_0^{t_n} f(t) e^{-i\omega t} dt. \quad (\text{A-2})$$

Furthermore, if $f(t) = f(t_n - t)$ for $0 \leq t \leq t_n$,

$$F(\omega) = \int_0^{\frac{1}{2}t_n} f(t) e^{-i\omega t} dt + \int_{\frac{1}{2}t_n}^{t_n} f(t_n - t) e^{-i\omega t} dt \quad (\text{A-3})$$

and with the change of variables $t' = t_n - t$,

$$F(\omega) = \int_0^{\frac{1}{2}t_n} f(t) e^{-i\omega t} dt + e^{-i\omega t_n} \int_0^{\frac{1}{2}t_n} f(t') e^{i\omega t'} dt'. \quad (\text{A-4})$$

Now if

$$G(\omega) = \int_0^{\frac{1}{2}t_n} f(t) e^{-i\omega t} dt, \quad (\text{A-5})$$

Equation (A-4) may be written as

$$F(\omega) = G(\omega) + e^{-i\omega t_n} \overline{G(\omega)} \quad (\text{A-6})$$

where $\overline{G(\omega)}$ is the complex conjugate of $G(\omega)$.

Now if $\omega = (2m-1)\pi/t_n$,

$$e^{-i\omega t_n} = -1 \quad (\text{A-7})$$

and

$$F(\omega) = 2 i \text{ Imag } [G(\omega)] \quad . \quad (\text{A-8})$$

Consequently, the real part of $F(\omega)$ is zero.

Similarly, if $\omega = 2m\pi/t_n$,

$$e^{-i\omega t_n} = 1 \quad (\text{A-9})$$

and

$$F(\omega) = 2 \text{ Real } [G(\omega)] \quad (\text{A-10})$$

and the imaginary part of $F(\omega)$ is zero.

Lemma I: If $F(\omega)$ and $F^*(\omega)$ are complex functions with phase angles ϕ and ϕ^* , respectively, then

$$|\sin (\phi - \phi^*)| \leq \frac{|F(\omega) - F^*(\omega)|}{|F^*(\omega)|} \quad (\text{A-11})$$

Proof: Let $F(\omega) = F = R + i I$ and $F^*(\omega) = F^* = R^* + i I^*$.

$$\frac{|F - F^*|}{|F^*|} = \frac{\left\{ (R - R^*)^2 + (I - I^*)^2 \right\}^{\frac{1}{2}}}{|F^*|} \quad (\text{A-12})$$

$$= \frac{|F| \left\{ |F|^2 + (R^{*2} + I^{*2}) - 2(RR^* + II^*) \right\}^{\frac{1}{2}}}{|F| |F^*|} \quad (\text{A-13})$$

$$= \frac{\left\{ |F|^4 - 2(R^2 + I^2)(RR^* + II^*) + (RR^* + II^*)^2 - (RR^* + II^*)^2 \right.}{|F| |F^*|}$$

$$\left. + \frac{(R^2 + I^2)(R^{*2} + I^{*2}) \right\}^{\frac{1}{2}}}{|F| |F^*|} \quad (\text{A-14})$$

$$= \frac{\left\{ [|F|^2 - (RR^* + II^*)]^2 + R^2 I^{*2} - 2RR^* II^* + R^{*2} I^2 \right\}^{\frac{1}{2}}}{|F| |F^*|} \quad (\text{A-15})$$

$$= \frac{\left\{ [|F|^2 - (RR^* + II^*)]^2 + (R^* I - I^* R)^2 \right\}^{\frac{1}{2}}}{|F| |F^*|} \quad (\text{A-16})$$

$$\geq \frac{|IR^* - RI^*|}{|F| |F^*|} = |\sin (\phi - \phi^*)| \quad . \quad (\text{A-17})$$

THEOREM II: Let

$$F(\omega) = \int_0^{\infty} f(t) e^{-i\omega t} dt \quad . \quad (\text{A-18})$$

If

$$f^*(t) = f(t) \text{ for } 0 \leq t \leq t_n \quad (\text{A-19})$$

and

$$f^*(t) = f(t_n) \text{ for } t > t_n \quad (\text{A-20})$$

then

$$F(\omega) - F^*(\omega) = \int_{t_n}^{\infty} [f(t) - f(t_n)] e^{-i\omega t} dt \quad (\text{A-21})$$

Proof:

$$\begin{aligned} F(\omega) - F^*(\omega) &= \int_0^{\infty} f(t) e^{-i\omega t} dt - \int_0^{t_n} f(t) e^{-i\omega t} dt \\ &\quad - \int_{t_n}^{\infty} f(t_n) e^{-i\omega t} dt \end{aligned} \quad (\text{A-22})$$

$$= \int_{t_n}^{\infty} f(t) e^{-i\omega t} dt - \int_{t_n}^{\infty} f(t_n) e^{-i\omega t} dt \quad (\text{A-23})$$

$$= \int_{t_n}^{\infty} [f(t) - f(t_n)] e^{-i\omega t} dt \quad (\text{A-24})$$

Corollary 1:

$$|F(\omega) - F^*(\omega)| \leq \int_{t_n}^{\infty} |f(t) - f(t_n)| dt \quad (\text{A-25})$$

Proof:

$$\begin{aligned} |F(\omega) - F^*(\omega)| &= \left| \int_{t_n}^{\infty} [f(t) - f(t_n)] e^{-i\omega t} dt \right| \\ &\leq \int_{t_n}^{\infty} |f(t) - f(t_n)| |e^{-i\omega t}| dt \end{aligned} \quad (\text{A-26})$$

$$= \int_{t_n}^{\infty} |f(t) - f(t_n)| dt \quad (\text{A-27})$$

(Proof of the inequality is given in standard texts [5].)

Corollary 2: If $\phi(\omega)$ and $\phi^*(\omega)$ are the phase angles of $F(\omega)$ and $F^*(\omega)$, respectively, then

$$|\sin(\phi - \phi^*)| \leq \frac{\int_{t_n}^{\infty} |f(t) - f(t_n)| dt}{|F^*(\omega)|} \quad (\text{A-28})$$

Proof: This is an obvious result of Lemma 1 and Corollary 1.

Corollary 3: If, for $t \geq t_n$,

$$f(t) = \frac{f(t_n) - f(\infty)}{m} \sum_k e^{-\alpha_k(t-t_n)} + f(\infty)$$

$$\begin{aligned} \text{then } |F(\omega) - F^*(\omega)| &= \frac{|f(t_n) - f(\infty)|}{m} \left[\left(\sum_k \frac{\alpha_k}{\alpha_k^2 + \omega^2} \right)^2 \right. \\ &\quad \left. + \left(\frac{m}{\omega} - \sum_k \frac{\omega}{\alpha_k^2 + \omega^2} \right)^2 \right]^{\frac{1}{2}} \end{aligned} \quad (\text{A-29})$$

Proof:

$$|F - F^*| = \left| \int_{t_n}^{\infty} \left[\frac{f(t_n) - f(\infty)}{m} \sum_k e^{-\alpha_k(t-t_n)} + f(\infty) - f(t_n) \right] e^{-st} dt \right| \quad (\text{A-30})$$

$$= \left| \frac{f(t_n) - f(\infty)}{m} \sum_k \alpha_k t_n \int_{t_n}^{\infty} e^{-(\alpha_k+s)t} dt + \frac{f(\infty) - f(t_n)}{s} e^{-st_n} \right| \quad (\text{A-31})$$

$$= \left| \frac{f(t_n) - f(\infty)}{m} \sum_k \frac{1}{\alpha_k + s} e^{-st_n} - \frac{f(t_n) - f(\infty)}{s} e^{-st_n} \right| \quad (\text{A-32})$$

$$|F(\omega) - F^*(\omega)| = \left| \frac{f(t_n) - f(\infty)}{m} \sum_k \frac{1}{\alpha_k + i\omega} - \frac{f(t_n) - f(\infty)}{i\omega} \right| \quad (\text{A-33})$$

$$= |f(t_n) - f(\infty)| \left| \frac{1}{m} \sum_k \frac{1}{\alpha_k + i\omega} + \frac{i}{\omega} \right| \quad (\text{A-34})$$

$$= \frac{|f(t_n) - f(\infty)|}{m} \left| \sum_k \frac{\alpha_k}{\alpha_k^2 + \omega^2} + i \left(\frac{m}{\omega} - \sum_k \frac{\omega}{\alpha_k^2 + \omega^2} \right) \right| \quad (\text{A-35})$$

THEOREM III: Let

$$F(\omega) = \int_0^{t_n} f(t) e^{-i\omega t} dt \quad (\text{A-36})$$

and suppose

$$|f(t) - f^*(t)| \leq \epsilon \text{ for } 0 \leq t \leq t_n \quad (\text{A-37})$$

If

$$\frac{\epsilon t_n}{|F^*(\omega)|} \leq k, \quad (\text{A-38})$$

then

$$\frac{|F(\omega) - F^*(\omega)|}{|F^*(\omega)|} \leq k \quad (\text{A-39})$$

Proof: From Corollary 1 to Theorem II,

$$|F(\omega) - F^*(\omega)| \leq \int_0^{t_n} |f(t) - f^*(t)| dt \leq \epsilon t_n \quad (\text{A-40})$$

Therefore,

$$\frac{|F(\omega) - F^*(\omega)|}{|F^*(\omega)|} \leq \frac{\epsilon t_n}{|F^*(\omega)|} \leq k \quad (\text{A-41})$$

THEOREM IV: Let

$$F(\omega) = \int_0^{t_n} f(t) e^{-i\omega t} dt \quad (\text{A-42})$$

and let $\phi(\omega)$ be the phase angle of $F(\omega)$. Suppose $f(t) - f^*(t) \leq \epsilon$ for $0 \leq t \leq t_n$. If

$$\frac{\epsilon t_n}{|F^*|} \leq k, \quad (\text{A-43})$$

then

$$|\sin(\phi - \phi^*)| \leq k \quad (\text{A-44})$$

Proof: From Lemma I,

$$|\sin(\phi - \phi^*)| \leq \frac{|F - F^*|}{|F^*|} \quad (\text{A-45})$$

and from Theorem III,

$$\frac{|F - F^*|}{|F^*|} \leq \frac{\epsilon t_n}{|F^*|} \quad (\text{A-46})$$

Therefore,

$$|\sin(\phi - \phi^*)| \leq \frac{\epsilon t_n}{|F^*|} \leq k \quad (\text{A-47})$$

THEOREM V: Let

$$F(\omega) = \int_0^{t_n} f(t) e^{-i\omega t} dt \quad (A-48)$$

Suppose that $f(0) = f^*(0)$ and $f(t_n) = f^*(t_n)$ and suppose that on $(0, t_n)$, the i^{th} derivatives of $f(t)$ and $f^*(t)$ are continuous for all $i < m$ and that the m^{th} derivatives are sectionally continuous. If

$$\frac{d^m}{dt^m} [f(t) - f^*(t)] \leq \epsilon_m \text{ on } (0, t_n) \quad (A-49)$$

then

$$\begin{aligned} \frac{||F(\omega) - F^*(\omega)||}{|F^*(\omega)|} &\leq \sum_{j=1}^{m-1} \frac{1}{\omega^{j+1} |F^*(\omega)|} \left| \frac{d^j}{dt^j} [f(t) - f^*(t)] \right|_0^{t_n} \\ &+ \frac{\epsilon_m t_n}{\omega^m |F^*(\omega)|} \end{aligned} \quad (A-50)$$

and

$$\begin{aligned} |\sin(\psi - \psi^*)| &\leq \sum_{j=1}^{m-1} \frac{1}{\omega^{j+1} |F^*(\omega)|} \left| \frac{d^j}{dt^j} [f(t) - f^*(t)] \right|_0^{t_n} \\ &+ \frac{\epsilon_m t_n}{\omega^m |F^*(\omega)|} \end{aligned} \quad (A-51)$$

Proof:

$$F(\omega) - F^*(\omega) = \int_0^{t_n} [f(t) - f^*(t)] e^{-i\omega t} dt \quad (A-52)$$

Integrating by parts,

$$\begin{aligned} F(\omega) - F^*(\omega) &= - \{ [f(t) - f^*(t)] \} \frac{1}{(i\omega)} e^{-i\omega t} \Big|_0^{t_n} \\ &- \left\{ \frac{d}{dt} [f(t) - f^*(t)] \right\} \left\{ \frac{1}{(i\omega)^2} e^{-i\omega t} \right\} \Big|_0^{t_n} \dots \\ &- \left\{ \frac{d^{m-1}}{dt^{m-1}} [f(t) - f^*(t)] \right\} \left\{ \frac{1}{(i\omega)^m} e^{-i\omega t} \right\} \Big|_0^{t_n} \end{aligned} \quad (A-53)$$

$$+ \int_0^{t_n} \frac{1}{(i\omega)^m} e^{-i\omega t} \frac{d^m}{dt^m} [f(t) - f^*(t)] dt \quad (\text{A-53})$$

$$= - e^{-i\omega t} \sum_{j=1}^{m-1} \frac{d^j}{dt^j} [f(t) - f^*(t)] \frac{1}{(i\omega)^{j+1}} \Big|_0^{t_n} \\ + \frac{1}{(i\omega)^m} \int_0^{t_n} e^{-i\omega t} \frac{d^m}{dt^m} [f(t) - f^*(t)] dt \quad (\text{A-54})$$

then

$$|F(\omega) - F^*(\omega)| \leq \sum_{j=1}^{m-1} \frac{1}{\omega^{j+1}} \left| \frac{d^j}{dt^j} [f(t) - f^*(t)] \right| \Big|_0^{t_n} \\ + \frac{1}{\omega^m} \int_0^{t_n} \left| \frac{d^m}{dt^m} [f(t) - f^*(t)] \right| dt \quad (\text{A-55})$$

By hypothesis,

$$\left| \frac{d^m}{dt^m} [f(t) - f^*(t)] \right| \leq \epsilon_m$$

and since

$$\left| |F(\omega)| - |F^*(\omega)| \right| \leq |F(\omega) - F^*(\omega)|$$

$$\frac{\left| |F(\omega)| - |F^*(\omega)| \right|}{|F^*(\omega)|} \leq \sum_{j=1}^{m-1} \frac{1}{\omega^{j+1} |F^*(\omega)|} \left| \frac{d^j}{dt^j} [f(t) - f^*(t)] \right| \Big|_0^{t_n} \\ + \frac{\epsilon_m t_n}{\omega^m |F^*(\omega)|} \quad (\text{A-56})$$

Using Lemma I,

$$|\sin(\psi - \psi^*)| \leq \sum_{j=1}^n \frac{1}{\omega^{j+1} |F^*(\omega)|} \left| \frac{d^j}{dt^j} [f(t) - f^*(t)] \right| \Big|_0^{t_n} \\ + \frac{\epsilon_m t_n}{\omega^m |F^*(\omega)|} \quad (\text{A-57})$$

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APPENDIX B -- LISTING OF THE FORTRAN AND MAP SOURCE
PROGRAMS USED IN SPORT

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\$FILE	'FTC03.',U03,U03,BLOCK=0801,SINGLE,LRL=0800,RCT=0001
\$ETC	EOR=REORX.,EDF=REDFX.,ERR=RERRX.,TYPE3
\$FILE	'FTC04.',U04,U04,BLOCK=0601,SINGLE,LRL=0600,RCT=0001
\$ETC	EOR=REORX.,EDF=REDFX.,ERR=RERRX.,TYPE3
\$FILE	'FTC08.',U05,U05,BLOCK=0401,SINGLE,LRL=0400,RCT=0001
\$ETC	EOR=REORX.,EDF=REDFX.,ERR=RERRX.,TYPE3
\$FILE	'FTC09.',U06,U06,BLOCK=0401,SINGLE,LRL=0400,RCT=0001
\$ETC	EOR=REORX.,EDF=REDFX.,ERR=RERRX.,TYPE3

C	FORTRAN ROUTINE WHICH READS THE PART AND CHANNEL CARDS, CALLS	MAIN0000
C	THE INPUT SUBROUTINES AND CALLS THE PROCESSING SUBROUTINES	MAIN0010
C	THROUGH SUBROUTINE SUBCNT.	MAIN0020
C		MAIN0030
	COMMON DATA(2021),LOM,IFINC,IPGNO,IHED(14),DATE(2)	MAIN0040
	DIMENSION IDNO(50),TMIN(50),TMAX(50),NCFDAT(50),TMSHF(50),	MAIN0050
1	NCFTIM(50),DTSHF(50),IFILNO(50),TITLE(12)	MAIN0060
	EQUIVALENCE (IHED(2),TITLE)	MAIN0070
	INTEGER FRCODE,CHCODE,PART,AUTO	MAIN0080
	LOGICAL SWTCH1	MAIN0090
	REAL NCFI,NCFDAT,NCFD,NCFTIM	MAIN0100
C		MAIN0110
	IA=315	MAIN0120
	CALL SET(IA)	MAIN0130
	CALL TIMX(ITM)	MAIN0140
	CALL TODAY(DATE)	MAIN0150
	IHED(1) = -17997958192	MAIN0180
	IHED(14) = -17997958192	MAIN0170
	IFINC=0	MAIN0180
	ILRLNO=0	MAIN0190
50	IPGNO=1	MAIN0200
C		MAIN0210
C	READ *PART* CARD	MAIN0220
C		MAIN0230
	READ(5,1)PART,FRCODE,ICODE,CHCODE,IPNLST,LCODE,AUTO,IRDP,TITLE	MAIN0240
1	FORMAT(3I1,I3,2I1,A1,I1,11A6,1A4)	MAIN0250
	WRITE(6,2) DATE,PART,FRCODE,ICODE,CHCODE,IPNLST,LCODE,AUTO,IRDP,	MAIN0260
1	TITLE	MAIN0270
2	FORMAT(11H1,8H SPORT A6,A2,27X,45H SYSTEM FOR PROCESSING REACTOR	MAIN0280
	ITRANSIENT DATA34X,9H PAGE 1 // 16H PART CARD WAS 3I1,I3,2I1,A1,	MAIN0290
2	I1,IX,11A6,1A4)	MAIN0300
	IF(IFINC.EQ.0 .AND. AUTO.EQ. -20145441840) IFINC=-0	MAIN0310
	SWTCH1=CHCODE.L1.0	MAIN0320
	NOCHNL=IABS(CHCODE)	MAIN0330
	IF((PART.LT.4).OR.(ICODE.EQ.5)) GO TO 100	MAIN0340
C		MAIN0350
	CALL SUBCNT(PART,FRCODE,ICODE,IPNLST,K,DT)	MAIN0360
	GO TO 150	MAIN0370
C		MAIN0380
C	READ CHANNEL CARDS	MAIN0390
C		MAIN0400
100	DO 105 I=1,NOCHNL	MAIN0410
	READ(5,4) IDNO(I),TMIN(I),TMAX(I),NCFTIM(I),NCFDAT(I),TMSHF(I),	MAIN0420
1	DTSHF(I),IRLNO,IFILNO(I)	MAIN0430
4	FORMAT(I10,6E10.8,2I4)	MAIN0440
	IF((TMAX(I)).EQ.-0.0) TMAX(I)=1.0E+30	MAIN0450
	IF((NCFTIM(I)).EQ.-0.0) NCFTIM(I)=1.0	MAIN0460
	IF((NCFDAT(I)).EQ.-0.0) NCFDAT(I)=1.0	MAIN0470
	IF(I.EQ.1) GO TO 101	MAIN0480
	IF(SWTCH1) TMIN(I)=TMAX(I-1)	MAIN0490
	GO TO 105	MAIN0500
C		MAIN0510
C	CHECK REEL NUMBER (IF ANY)	MAIN0520
C		MAIN0530
101	IF(ICODE.NE.5) GO TO 102	MAIN0540

	IRLNMB=IRLNO	MAIN0550
	IF(IRLNMB.EQ.0) GO TO 103	MAIN0560
	WRITE(6,104) IRLNMB	MAIN0570
104	FORMAT(1H0,12H REEL NUMBER15)	MAIN0580
	IF(IRLNMB.EQ.IRLNO) IRLNMB=22200000222	MAIN0590
103	IRLNO=IRLNO	MAIN0600
102	WRITE(6,3)	MAIN0610
	3 FORMAT(1H0,30H CHANNEL FILE NO MINIMUM,8X,8H MAXIMUM,8X,	MAIN0620
	1 25H NORMALIZING COEFFICIENTS,6X,27H TIME SHIFT DATA SHIFT /	MAIN0630
	2 29H ID NO (IF ANY) TIME,11X,5H TIME,12X,5H TIME,11X,	MAIN0640
	3 5H DATA /)	MAIN0650
C		MAIN0660
105	WRITE(6,5) IDNO(I),IFILNO(I),TMIN(I),TMAX(I),NCFTIM(I),NCFDAT(I),	MAIN0670
	1 TMSHF(I),DTSHF(I)	MAIN0680
	5 FORMAT(I11,17,3X,3(F14.6,2X),1PE14.7,2X,OPF14.6,2X,1PE14.7)	MAIN0690
C		MAIN0700
C	MAIN LOOP	MAIN0710
C		MAIN0720
	IA=90	MAIN0730
	IF(.NOT.SWTC1) CALL SET(IA)	MAIN0740
110	DO 120 I=1,NOCHNL	MAIN0750
	IE=0	MAIN0760
	IX=0	MAIN0770
	IF(.NOT.SWTC1) IE=1	MAIN0780
	IF(I.EQ.1) IE=2*CHCODE/NOCHNL	MAIN0790
	IF(.NOT.SWTC1 .OR. I.EQ.NOCHNL) IX=1	MAIN0800
	CALL GNTAPE(PART,ICODE,IE,IX,IPNLST,LCODE,IDNO(I),K,	MAIN0810
	1 TMIN(I),TMAX(I),NCFTIM(I),NCFDAT(I),TMSHF(I),DTSHF(I),	MAIN0820
	2 IRLNMB,IRDP,IFILNO(I))	MAIN0830
119	IF(IX.EQ.1) CALL SUBCNT(PART,FRCODE,ICODE,IPNLST,K,TMAX(I))	MAIN0840
120	CONTINUE	MAIN0850
C		MAIN0860
C	END OF PROBLEM	MAIN0870
C		MAIN0880
150	CALL ETIMX(ITM,IETM,RETS)	MAIN0890
	WRITE(6,7)IETM,RETS	MAIN0900
7	FORMAT(1H0,27H TOTAL PROBLEM TIME WAS 14,5H MIN F4.1,4H SEC)	MAIN0910
151	READ(5,6)NOM	MAIN0920
6	FORMAT(1A2)	MAIN0930
	IF(NOM.EQ. -13216451632) GO TO 50	MAIN0940
	IF(NOM.NE. -13736545328) GO TO 151	MAIN0950
C		MAIN0960
C	END OF PROBLEM SET	MAIN0970
C		MAIN0980
160	IF(IFINC.EQ.0) STOP	MAIN0990
C		MAIN1000
C	INDICATE END OF PLOT REEL	MAIN1010
C		MAIN1020
	CALL DRAW(0,0,0,0,0,0,0,0,0,0,12,0,0,8,0,0,0,0,0,0,0)	MAIN1030
	CALL SYMBLJ(0,0,0,0,0,14,19H END OF SPORT PLOTS,90,0,19)	MAIN1040
	CALL PLOT(5,0,-1,0,-3)	MAIN1050
C		MAIN1060
C	DISMOUNT PLOT TAPE	MAIN1070
C		MAIN1080
	CALL TYPE(1H ,1,0)	MAIN1090

CALL TYPE(16H	THERE WERE,16,0)	MAIN1100
CALL TYPEN(IFINC-1)		MAIN1110
CALL TYPE(19H	PLOTS GENERATED,19,0)	MAIN1120
CALL TYPE(1H ,1,0)		MAIN1130
CALL FINI		MAIN1140
STOP		MAIN1150
C		MAIN1160
END		MAIN1170

C	FORTRAN SUBROUTINE WHICH READS THE SPORT INPUT DATA (EITHER	GNTPOC0C
C	DIRECTLY OR BY CALLING SUBROUTINES SPERT1,DAT650 OR TREAD)	GNTPO010
C	AND PERFORMS THE DATA PREPARATION INDICATED ON THE PART AND	GNTPOC20
C	CHANNEL CARDS.	GNTPOC30
C		GNTPO040
	SUBROUTINE GNTAPE(PART,ICODE,IE,IX,IPNLST,LCCDE,ID,K,TMN,TMX,	GNTPO050
	1 NCFT,NCFD,TSHFT,DSHFT,IRLNMB,IRDP,IFILNO)	GNTPO060
C		GNTPO070
	COMMON DATA(2021),LOM,IFINC,IPGNO,HEAD(14)	GNTPOC8C
	DIMENSION X(8),A(7),B(7),FMT(14),C(6C0),D(800),ISTCR(800),SCT(2),	GNTPO090
	1 SCD(2)	GNTPO100
	INTEGER PART	GNTPO110
	REAL NCFT,NCFD	GNTPO120
	LOGICAL SWCH1,SWCH2,SWCH3,SWCH4,SWCH5,SWCH6,SWCH7,SWCH8	GNTPO130
	EQUIVALENCE (DATA(19),ND,X),(DATA(20),TO,A),(DATA(21),DT),	GNTPO140
	1 (DATA(27),D,ISTOR),(KR,K2),(JFILNO,SWCH6),(DATA(17),IRECNG)	GNTPO150
C		GNTPO160
	SWCH8=IABS(IE).EQ.2	GNTPO170
	IF(IE.EQ.0) GO TO 6400	GNTPO180
	CALL TIMX(ITL)	GNTPO190
	REWIND 4	GNTPO200
	SCD(1)=+1.0E+30	GNTPO210
	SCD(2)=-1.0E+30	GNTPO220
	IF(.NOT.SWCH8) GO TO 6400	GNTPO230
	IBLANK = -17997958192	GNTPO240
	SWCH7=ICODE.NE.5	GNTPO250
	SWCH4=LCODE.EQ.0	GNTPO260
	SWCH5=IRDP.NE.0	GNTPO270
	6400 IF(.NOT.SWCH7) GO TO 500	GNTPO280
C		GNTPO290
C	CARD SECTION	GNTPO300
C		GNTPO310
	IF(IE.EQ.0) GO TO 449	GNTPO320
	SWCH1=.FALSE.	GNTPO330
	K3=0	GNTPO340
	KR=-1	GNTPO350
	IEOF=0	GNTPO360
	IF(IF.EQ.1) GO TO 440	GNTPO370
	IF(ICODE.EQ.4) READ(5,3) NOCHNL,FMT	GNTPO380
	3 FORMAT(I1,13A6,1A1)	GNTPO390
	KS=-7	GNTPO400
	REWIND 3	GNTPO410
C		GNTPO420
C	PREPARE BINARY DATA TAPE- ALL CHANNELS	GNTPO430
C		GNTPO440
	30 GO TO(100,200,300,400),ICODE	GNTPO450
	100 CALL SPRT13(X)	GNTPO460
	IF(LOM.EQ.1) GO TO 100	GNTPO470
	GO TO 470	GNTPO480
	200 READ(5,1)ND,(A(J),B(J),J=1,7)	GNTPO490
	1 FORMAT(110,7(F8.8,A2))	GNTPO500
	GO TO 310	GNTPO510
	300 READ(5,2)ND,NDL,(A(J),B(J),J=1,7)	GNTPO520
	2 FORMAT(19,A1,7(F8.8,A2))	GNTPO530
	CALL ID650(ND,NDL)	GNTPO540

310	CALL DAT650(A,8,7)	GNTPO550
	GO TO 470	GNTPO560
400	READ(5,FMT)ND,A(1),(A(J+1),J=1,NOCHNL)	GNTPO570
470	KS=KS+8	GNTPO580
	ISTOR(KS)=ND	GNTPO590
	D(KS+1)=X(2)	GNTPO600
	D(KS+2)=X(3)	GNTPO610
	D(KS+3)=X(4)	GNTPO620
	D(KS+4)=X(5)	GNTPO630
	D(KS+5)=X(6)	GNTPO640
	D(KS+6)=X(7)	GNTPO650
	D(KS+7)=X(8)	GNTPO660
	IF((KS.LT.793).AND.(ND.NE.0)) GO TO 30	GNTPO670
	KS=-7	GNTPO680
	WRITE(3) D	GNTPO690
	IF(ND.NE.0) GO TO 30	GNTPO700
C		GNTPO710
C	PREPARE NORMALIZED DATA TAPE- CHANNEL 'ID'	GNTPO720
C		GNTPO730
440	REWIND 3	GNTPO740
448	KS=-7	GNTPO750
	READ(3) D	GNTPO760
450	KS=KS+8	GNTPO770
	IF(KS.EQ.801) GO TO 448	GNTPO780
	LD=ISTOR(KS)	GNTPO790
	IF(LD.EQ.0) GO TO 522	GNTPO800
	IF(SWICH1) GO TO 449	GNTPO810
C		GNTPO820
C	ASSEMBLE PARAMETERS FOR FIRST RECORD	GNTPO830
C		GNTPO840
601	SWTCH1=.TRUE.	GNTPO850
	NID=ID	GNTPO860
	IF(IE.NE.-2) GO TO 4602	GNTPO870
	NID=0	GNTPO880
4602	DELT=(D(794)-D(2))/99.0	GNTPO890
	WRITE(4) LD,NID,DELT	GNTPO900
	GO TO 4010	GNTPO910
C		GNTPO920
449	T=D(KS+1)*NCFT+TSHFT	GNTPO930
451	IF(T.LT.TMN) GO TO 450	GNTPO940
	IF(T.GE.TMX) GO TO 522	GNTPO950
460	IKS=KS+1+ID	GNTPO960
	VALUE=D(IKS)*NCFD+DSHFT	GNTPO970
602	GU IU 566	GNTPO980
C		GNTPO990
C	DIGITAL TAPE SECTION	GNTP1000
C		GNTP1010
500	IF(.NOT.SWTC8) GO TO 502	GNTP1020
	IF(IRLNMB.EQ.222C0000222) GO TO 4005	GNTP1030
C		GNTP1040
C	MOUNT DATA TAPE	GNTP1050
C		GNTP1060
501	CALL TYPE(1H ,1,0)	GNTP1070
	IF(IRLNMB.NE.0) GO TO 4501	GNTP1080
	CALL TYPE(22H MOUNT REEL CUNTAING,22,0)	GNTP1090

	CALL TYPE(16H DATA RECORD,16,0)	GNTPI100
	KD=ID	GNTPI110
	GO TO 4502	GNTPI120
4501	CALL TYPE(15H MOUNT REEL,15,0)	GNTPI130
	KD=IRLNMB	GNTPI140
4502	CALL TYPEN(KD)	GNTPI150
	CALL TYPE(14H ON T,C,6,14,0)	GNTPI160
	CALL TYPE(1H ,1,0)	GNTPI170
	CALL TIMX(ITM)	GNTPI180
	CALL TYPC(24H PRESS START TO CONTINUE,24,1)	GNTPI190
	CALL ETIMX(ITM,IETM,RETS)	GNTPI200
	WRITE(6,4000) IETM,RETS	GNTPI210
4000	FORMAT(1H0,27H DATA TAPE MOUNTING TIME - 14,5H MIN F4.1,4H SEC)	GNTPI220
C		GNTPI230
4005	REWIND IO	GNTPI240
	NTCT=1	GNTPI250
	GO TO 1502	GNTPI260
C		GNTPI270
502	CALL BACK(NTCT,0)	GNTPI280
	NTCT=0	GNTPI290
1502	IF(IE.EQ.0) GO TO 503	GNTPI300
C		GNTPI310
C	ASSEMBLE PARAMETERS FOR FIRST RECORD	GNTPI320
C		GNTPI330
	LD=ID	GNTPI340
	NID=(LD/1000)*1000	GNTPI350
	IF(IE.EQ.-2) LD=NID	GNTPI360
	NID=LD-NID	GNTPI370
4010	CALL HEADER	GNTPI380
	IF(IPNLST.EQ.0) GO TO 2503	GNTPI390
	IF(IE.EQ.-2) GO TO 2502	GNTPI400
	IF(NID.EQ.0) NID=1	GNTPI410
	WRITE(6,4) LD,NID	GNTPI420
4	FORMAT(1H0,41X,26HNORMALIZED DATA RECORD NO I11,9H CHANNEL I4 /)	GNTPI430
	GO TO 3502	GNTPI440
2502	WRITE(6,12) LD	GNTPI450
12	FORMAT(1H0,48X,27HNORMALIZED COMPOSITE DATA I10 /)	GNTPI460
3502	IF(IPNLST.EQ.2) PUNCH 8,LD	GNTPI470
8	FORMAT(5X,27HNORMALIZED DATA RECORD NO I10,10H CHANNEL I3)	GNTPI480
	IF(.NOT.SWTC4) WRITE(6,7)	GNTPI490
7	FORMAT(1H ,49X,35H LN(DATA) TAKEN IN INPUT SUBROUTINE /)	GNTPI500
2503	IF(SWTC7) GO TO 449	GNTPI510
	K3=0	GNTPI520
	K2=-1	GNTPI530
C		GNTPI540
C		GNTPI550
C	FIND RECORD WITH ID=ND	GNTPI560
C		GNTPI570
503	JFILNO=IFILNO	GNTPI580
3503	CALL TREAD(IEOF)	GNTPI590
	IF(IEOF.NE.0) GO TO 522	GNTPI600
	IF(.NOT.SWTC8) NTCT=NTCT+1	GNTPI610
	IF(.NOT.SWTC6 .AND. IRECNO.NE.IFILNC) GO TO 3503	GNTPI620
	IF(ID.EQ.ND) GO TO 3504	GNTPI630
	IF(SWTC6) GO TO 3503	GNTPI640

	WRITE(6,3505) IFILNO,ND,ID	GNTP1650
3505	FORMAT(1H0,16H ID NO OF RECORDI4 ,5H WAS I10,6H, NOT I1C)	GNTP1660
	GO TO 522	GNTP1670
C		GNTP1680
3504	DELT=DT*NCFT	GNTP1690
	IF(IE.NE.0) WRITE(4) LD,NID,DELT	GNTP1700
C		GNTP1710
504	T02=TO*NCFT+TSHFT	GNTP1720
C		GNTP1730
C	PROCESS CURRENT RECORD	GNTP1740
C		GNTP1750
	DO 526 J=22,2021	GNTP1760
	T=FLOAT(J-22)*DELT+T02	GNTP1770
	IF(T.LT.TMX) GO TO 526	GNTP1780
	IF(T.LT.TMX) GO TO 530	GNTP1790
C		GNTP1800
C	PROCESS FINAL RECORD	GNTP1810
C		GNTP1820
522	IF(IX.EQ.0) RETURN	GNTP1830
	TMX=DELT	GNTP1840
	K=K3*300+(K2+1)/2	GNTP1850
	KK2=K2+2	GNTP1860
	C(KK2)=1.0E+30	GNTP1870
	C(KK2+1)=0.0	GNTP1880
	IF(K.EQ.0) GO TO 576	GNTP1890
	IF(SWTC5 .AND. K3.EQ.0) SCT(1)=C(1)	GNTP1900
	IF(IPNLST.EQ.0) GO TO 535	GNTP1910
C		GNTP1920
C	PRINT FINAL PAGE	GNTP1930
C		GNTP1940
705	IF(K2.EQ.-1) GO TO 550	GNTP1950
	KT=K2/100+1	GNTP1960
	GO TO(536,537,538,539,540,541),KT	GNTP1970
536	WRITE(6,17)C(1),C(2),(C(I+2),C(I+3),I=1,K2,2)	GNTP1980
17	FORMAT(1X,OPF10.6,1X,1PE10.3)	GNTP1990
	GO TO 535	GNTP2000
537	WRITE(6,18)(C(I-98),C(I-97),C(I+2),C(I+3),I=99,K2,2)	GNTP2010
18	FORMAT(2(1X,OPF10.6,1X,1PE10.3))	GNTP2020
	WRITE(6,17)(C(I-96),C(I-95),I=K2,195,2)	GNTP2030
	GO TO 535	GNTP2040
538	WRITE(6,19)(C(I-198),C(I-197),C(I-98),C(I-97),C(I+2),C(I+3),	GNTP2050
1	I=199,K2,2)	GNTP2060
19	FORMAT(3(1X,OPF10.6,1X,1PE10.3))	GNTP2070
	WRITE(6,18)(C(I-196),C(I-195),C(I-96),C(I-95),I=K2,295,2)	GNTP2080
	GO TO 535	GNTP2090
539	WRITE(6,20)(C(I-298),C(I-297),C(I-198),C(I-197),C(I-98),C(I-97),	GNTP2100
1	C(I+2),C(I+3),I=299,K2,2)	GNTP2110
20	FORMAT(4(1X,OPF10.6,1X,1PE10.3))	GNTP2120
	WRITE(6,19)(C(I-296),C(I-295),C(I-196),C(I-195),C(I-96),C(I-95),	GNTP2130
1	I=K2,395,2)	GNTP2140
	GO TO 535	GNTP2150
540	WRITE(6,21)(C(I-398),C(I-397),C(I-298),C(I-297),C(I-198),	GNTP2160
1	C(I-197),C(I-98),C(I-97),C(I+2),C(I+3),I=399,K2,2)	GNTP2170
21	FORMAT(5(1X,OPF10.6,1X,1PE10.3))	GNTP2180
	WRITE(6,20)(C(I-396),C(I-395),C(I-296),C(I-295),C(I-196),	GNTP2190

1	C(I-195),C(I-96),C(I-95),I=K2,495,2)	Gntp2200
	GO TO 535	Gntp2210
541	WRITE(6,10)(C(I-498),C(I-497),C(I-398),C(I-397),C(I-298),	Gntp2220
1	C(I-297),C(I-198),C(I-197),C(I-98),C(I-97),C(I+2),C(I+3),	Gntp2230
2	I=499,K2,2)	Gntp2240
10	FORMAT(6(1X,OPF10.6,1X,1PE10.3))	Gntp2250
	WRITE(6,21)(C(I-496),C(I-495),C(I-396),C(I-395),C(I-296),	Gntp2260
1	C(I-295),C(I-196),C(I-195),C(I-96),C(I-95),I=K2,595,2)	Gntp2270
	GO TO 535	Gntp2280
550	WRITE(6,17)C(1),C(2)	Gntp2290
	GO TO 535	Gntp2300
576	IF(IEOF.EQ.0) WRITE(6,22)	Gntp2310
22	FORMAT(1H0,27H NO DATA IN RANGE SPECIFIED)	Gntp2320
	IF(IEOF.NE.0) WRITE(4) LD,NID,DELT	Gntp2330
535	IF(IEOF.NE.0) WRITE(6,13)	Gntp2340
13	FORMAT(1H0,42H END-OF-FILE MARK ENCOUNTERED CN DATA TAPE)	Gntp2350
	WRITE(4) C	Gntp2360
	IF(IPNLST.NE.2) GO TO 3001	Gntp2370
	PUNCH 6,(LD,C(I),C(I+1),C(I+1),I=1,K2,2)	Gntp2380
6	FORMAT(110,5X,OPF12.6,5X,1PE14.7,5X,CPF20.8)	Gntp2390
3001	CALL ETIMX(ITL,IPREPM,RPREPS)	Gntp2400
	IF(SWCH5) GO TO 3005	Gntp2410
	WRITE(6,3003) IPREPM,RPREPS	Gntp2420
3003	FORMAT(1H0,27H DATA PREPARATION REQUIRED 14,5H MIN F4.1,4H SECA1,	Gntp2430
1	22HAND DATA PLOT REQUIREDI3,5H MIN F4.1,4H SEC)	Gntp2440
	RETURN	Gntp2450
C		Gntp2460
C	COMPUTE DATA VALUE AND STORE IN ARRAY 'C'	Gntp2470
C		Gntp2480
530	VALUE=DATA(J)*NCFD+DSHFT	Gntp2490
566	IF(SWCH4) GO TO 531	Gntp2500
	IF(VALUE.LE.0.0) GO TO 525	Gntp2510
	VALUE=ALOG(VALUE)	Gntp2520
531	K2=K2+2	Gntp2530
	C(K2)=T	Gntp2540
	C(K2+1)=VALUE	Gntp2550
	IF(K2.LT.599) GO TO 525	Gntp2560
	WRITE(4) C	Gntp2570
	K3=K3+1	Gntp2580
	K2=-1	Gntp2590
	IF(SWCH5.AND.K3.EQ.1) SCT(1)=C(1)	Gntp2600
	IF(SWCH5) CALL MAXMIN(SCD,C,2,600,2)	Gntp2610
	IF(IPNLST.EQ.0) GO TO 525	Gntp2620
	WRITE(6,10)(C(I),C(I+1),C(I+100),C(I+101),C(I+200),C(I+201),	Gntp2630
1	C(I+300),C(I+301),C(I+400),C(I+401),C(I+500),C(I+501),I=1,99,2)	Gntp2640
	CALL HEADER	Gntp2650
	WRITE(6,4) LD,NID	Gntp2660
	IF(IPNLST.NE.2) GO TO 525	Gntp2670
	PUNCH 6,(LD,C(I),C(I+1),C(I+1),I=1,599,2)	Gntp2680
525	IF(SWCH7) GO TO 450	Gntp2690
526	CONTINUE	Gntp2700
C		Gntp2710
C	CHECK NEXT RECORD	Gntp2720
C		Gntp2730
	CALL TREAD(IEOF)	Gntp2740

	IF(IEOF.NE.0) GO TO 522	Gntp2750
	NTCT=NTCT+1	Gntp2760
	IF(ND.NE.ID) GO TO 522	Gntp2770
	DELT=DT*NCFT	Gntp2780
	IF(INT((T+DELT-TSHFT-TO*NCFT)*1.0E+6) .NE.0) GO TO 522	Gntp2790
	GO TO 504	Gntp2800
C		Gntp2810
C	DATA PLOT SECTION	Gntp2820
C		Gntp2830
3005	IF(K.EQ.0) GO TO 1923	Gntp2840
	SCT(2)=C(599)	Gntp2850
	IF(K2.NE.-1) SCT(2)=C(K2)	Gntp2860
	REWIND 4	Gntp2870
C		Gntp2880
C	DRAW PLOT	Gntp2890
C		Gntp2900
	IPPR=IRDP	Gntp2910
	IF(.NOT.SWTCH4) IPPR=IPPR+2	Gntp2920
	CALL DRAW(0,1,IPPR,K,300,2,.TRUE.,C,SCT,SCD,	Gntp2930
	1 10.0,TMIN,DTM,7.C,DMIN,DDAT,	Gntp2940
	2 HEAD,20H DATA VALUE)	Gntp2950
C		Gntp2960
1923	CALL ETIMX(ITL,IPLTM,RPLTS)	Gntp2970
	WRITE(6,3003) IPREPM,RPREPS,IBLANK,IPLTM,RPLTS	Gntp2980
	RETURN	Gntp2990
C		Gntp3000
	END	Gntp3010

C	FORTTRAN SUBROUTINE WHICH CONTROLS THE ORDER IN WHICH THE PRO-	SBCT0000
C	CESSING PROGRAMS(SMOOTH,REACTIVITY AND FREQUENCY RESPONSE) ARE	SBCT0010
C	CALLED.	SBCT0020
C		SBCT0030
C	SUBROUTINE SUBCNT(PART,FRCODE,ICODE,IPNLST,K,DT)	SBCT0040
C		SBCT0050
C	COMMON DATA(2021),LOM,IFINC,IPGNO,IHEAD(14),DATE(2)	SBCT0060
C	INTEGER PART,FRCODE	SBCT0070
C		SBCT0080
C	IF(PART.EQ.0) RETURN	SBCT0090
C	GO TO(100,100,100,400,500),PART	SBCT0100
C		SBCT0110
C	100 CALL SMOOTH(PART,ICODE,K,DT)	SBCT0120
C	IF(LOM.EQ.1) K=0	SBCT0130
C	120 GO TO(600,150,190),PART	SBCT0140
C	150 CALL REACT(K,DT,FRCODE)	SBCT0150
C	190 IF(FRCODE.EQ.0) GO TO 600	SBCT0160
C	CALL FREQ(PART,ICODE,K,DT)	SBCT0170
C	600 RETURN	SBCT0180
C		SBCT0190
C	500 IF(ICODE.EQ.5) GO TO 190	SBCT0200
C	400 CALL INPUT(PART,ICODE,K,DT,IPNLST)	SBCT0210
C	IF(K.EQ.0) RETURN	SBCT0220
C	IF(PART.EQ.4) GO TO 150	SBCT0230
C	GO TO 190	SBCT0240
C		SBCT0250
C	END	SBCT0260

```

**
** MAP SUBROUTINE USED TO READ TYPE-5 SPORT DATA. G A CAZIER
**
** ENTRY TREAD
**
TREAD PZE ** TRED0000
      SXA X4,4 TRED0010
      TSX S.IOOP,4 TRED0020
      IORBS TBUFF TRED0030
      PZE S.SU07 TRED0040
      CAL S.SSCH TRED0050
      TZE ENDFIL TRED0060
      LAC TREAD,4 TRED0070
      CLA =00 TRED0080
      STO* 2,4 TRED0090
X4 AXT **,4 TRED0100
  TRA* TREAD TRED0110
ENDFIL LAC TREAD,4 TRED0120
      CLA =07 TRED0130
      STO* 2,4 TRED0140
      TRA X4 TRED0150
TBUFF PZE DATA,2021 TRED0160
      CONTRL // TRED0170
      USE // TRED0180
DATA BSS 2021 TRED0190
      USE PREVIOUS TRED0200
      LITERALS TRED0250
      EXTERN S.SSCH GENERATED
      EXTERN S.SU07 GENERATED
      EXTERN S.IOOP GENERATED
      END TRED0260

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**
** MAP SUBROUTINE USED TO POSITION INPUT DATA TAPE. G A CAZIER
**
** ENTRY BACK
**
BACK PZE **
SXA SAV4,4
LAC BACK,4
CLA* 2,4
STA SPAC
CLA* 3,4
ALS 18
STD SPAC
TSX S.IOOP,4
IOSKP SPAC
PZE S.SU07
SAV4 AXT **,4
TRA* BACK
SPAC MZE **,**
EXTERN S.SU07 GENERATED
EXTERN S.IOOP GENERATED
END BACK0190

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**
** MAP SUBROUTINE USED TO PRINT CONSOLE MESSAGES. K R DICKEY
**
** ENTRY TYPE
**
TYPE PZE ** TYPE0000
SXA NOPAUS,4 TYPE0010
LAC TYPE,4 TYPE0020
CLA 2,4 HOLL ADRESS. IN AC TYPE0030
STA SEQUEN TYPE0040
CLA* 3,4 COUNT TYPE0050
ALS 18 TYPE0060
STD SEQUEN TYPE0070
TSX S.XPRT,4 TYPE0080
SEQUEN PZE **, ** TYPE0090
LAC TYPE,4 TYPE0100
CLA* 4,4 TYPE0110
TZE NOPAUS TYPE0120
TSX S.XPSE,4 TYPE0130
NOPAUS AXT **,4 TYPE0140
TRA* TYPE TYPE0150
EXTERN S.XPRT GENERATED TYPE0160
EXTERN S.XPSE GENERATED TYPE0170
END TYPE0180
TYPE0190
TYPE0200
TYPE0210

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C	FORTTRAN SUBROUTINE USED TO PRINT INTEGER NUMBERS AS CONSOLE	TYPN0000
C	MESSAGES.	TYPN0010
C		TYPN0020
	SUBROUTINE TYPEN(ID)	TYPN0030
C		TYPN0040
	DIMENSION QUAN(2)	TYPN0050
C		TYPN0060
	CALL BBCD1(ID,QUAN(1),QUAN(2))	TYPN0070
	CALL TYPE(QUAN,12,0)	TYPN0080
	RETURN	TYPN0090
C		TYPN0100
	END	TYPN0110

TFS	CAL*	1,4		BBCD0500	
	ANA	STEST		BBCD0510	
	TZE	PACK		BBCD0520	
	CAL	MINUS		BBCD0530	
PACK	STO	UPBCD+10,2		BBCD0540	
	CAL	UPBCD+4		BBCD0550	
	LGR	6		BBCD0560	
	CAL	UPBCD+3		BBCD0570	
	LGR	6		BBCD0580	
	CAL	UPBCD+2		BBCD0590	
	LGR	6		BBCD0600	
	CAL	UPBCD+1		BBCD0610	
	LGR	6		BBCD0620	
	CAL	UPBCD		BBCD0630	
	LGR	6		BBCD0640	
	CAL	BLANK		BBCD0650	
	LGR	6		BBCD0660	
WRD2	STQ*	2,4		BBCD0670	
	CAL	UPBCD+10		BBCD0680	
	LGR	6		BBCD0690	
	CAL	UPBCD+9		BBCD0700	
	LGR	6		BBCD0710	
	CAL	UPBCD+8		BBCD0720	
	LGR	6		BBCD0730	
	CAL	UPBCD+7	PACK SECOND BCD WORD		BBCD0740
	LGR	6			BBCD0750
	CAL	UPBCD+6			BBCD0760
LGR	6			BBCD0770	
	CAL	UPBCD+5		BBCD0780	
	LGR	6		BBCD0790	
WRD1	STQ*	3,4		BBCD0800	
SAVE2	AXT	0,2		BBCD0810	
	BRA	BBCD1+5		BBCD0820	
	AXT	** ,4		BBCD0830	
BBCD1	TRA	**	CALL ENTRY..CALL BBCD1(BIN,BCD1,BCD2)	BBCD0840	
	MSP	BBCD1-2		BBCD0850	
	SXA	BBCD1-1,4	(... CYCLES)	BBCD0860	
	LAC	BBCD1,4		BBCD0870	
	TXI	BBCD1.+1,4,-1		BBCD0880	
	TRA	4,4		BBCD0890	
PTEN	DEC	1000000000	10 TO 10TH	BBCD0900	
	DEC	1000000000	10 TO 9TH	BBCD0910	
	DEC	1000000000	10 TO 8TH	BBCD0920	
	DEC	1000000000	10 TO 7TH	BBCD0930	
	DEC	1000000000	10 TO 6TH	BBCD0940	
	DEC	1000000000	10 TO 5TH	BBCD0950	
	DEC	1000000000	10 TO 4TH	BBCD0960	
	DEC	1000000000	10 TO 3RD	BBCD0970	
	DEC	1000000000	10 TO 2ND	BBCD0980	
	DEC	1000000000	10 TO 1ST	BBCD0990	
BLANK	OCT	°606060606060		BBCD1000	

STEST	OCT	400000000000	BBCD1010
MINUS	OCT	000000000040	BBCD1020
ZERO	PZE		BBCD1030
UPBCD	BSS	11	BBCD1040
	END		BBCD1050

C	FORTTRAN SUBROUTINE TO PRINT PAGE HEADINGS.	HEAD0000
C	-----	HEAD0010
	SUBROUTINE HEADER	HEAD0020
C	-----	HEAD0030
	COMMON DATA(2021),LOM,IEINC,IPGNO,IHEAD(14),DATE(2)	HEAD0040
C	-----	HEAD0050
	IPGNO=IPGNO+1	HEAD0060
	WRITE(6,1) DATE,IHEAD,IPGNO	HEAD0070
	1 FORMAT(1H1,8H SPORT A6,A2,9X,12A6,2A4,17X,5H PAGE14)	HEAD0080
	RETURN	HEAD0090
C	-----	HEAD0100
	END	HEAD0120

**	MAP SUBROUTINE USED TO REFERENCE CURRENT DATE.		N H MARSHALL	TDAY0000
**				TDAY0010
**				TDAY0020
	ENTRY	TODAY		TDAY0030
**				TDAY0040
TODAY	TRA	**		TDAY0050
	SXA	X4,4		TDAY0060
	LAC	TODAY,4		TDAY0070
	CLA	2,4		TDAY0080
	PAC	,4		TDAY0090
	ZAC			TDAY0100
	LGR	36		TDAY0110
	CAL	S.SDAT		TDAY0120
	LGR	24		TDAY0130
	ALS	6		TDAY0140
	ADD	=H00000/		IUAY0150
	LGL	12		TDAY0160
	ALS	6		TDAY0170
	ADD	=H00000/		TDAY0180
	SLW	0,4	STORE MM/DD/ IN FIRST WORD	TDAY0190
	ZAC			TDAY0200
	LGL	36		TDAY0210
	ADD	=H00		TDAY0220
	SLW	1,4	STORE YY IN SECOND WORD	TDAY0230
<hr/>				
X4	AXT	** ,4		TDAY0240
	TRA*	TODAY		TDAY0250
	LITERALS			
<hr/>				
EXTERN	S.SDAT	GENERATED		TDAY0260
END				

C	FORTTRAN SUBROUTINE WHICH COMPUTES THE PHASE ANGLE OF A COMPLEX	ANGR0000
C	QUANTITY. L E REFSE	ANGR0010
C		ANGR0020
C	SUBROUTINE ANGRAD(X,Y,TMAG,PHASE)	ANGR0030
C		ANGR0040
C	COMMON DATA(2021),LOM	ANGR0050
C		ANGR0060
C	TMAG=SQRT(X*X+Y*Y)	ANGR0070
	IF (X) 3,2,4	ANGR0080
2	IF (Y) 5,7,6	ANGR0090
5	PHASE=4.7123890	ANGR0100
	RETURN	ANGR0110
6	PHASE=1.5707963	ANGR0120
	RETURN	ANGR0130
3	PHASE=ATAN(Y/X)+3.1415927	ANGR0140
	RETURN	ANGR0150
4	IF (Y) 8,9,9	ANGR0160
8	PHASE=ATAN(Y/X)+6.2831853	ANGR0170
	RETURN	ANGR0180
9	PHASE=ATAN(Y/X)	ANGR0190
	RETURN	ANGR0200
7	PHASE=0.0	ANGR0210
	RETURN	ANGR0220
C		ANGR0230
	END	ANGR0240

**				SPRT0000
**	MAP SUBROUTINE USED TO READ TYPE-1 SPORT DATA.	R J WAGNER		SPRT0010
**	ENTRY	SPRT13		SPRT0020
**				SPRT0030
**	EXTERN	TSHIO.,RTNIO.,FMTSC.,FILO5.,HNLIO.,STHIO.,FILO6.,FILIO.		SPRT0040
SPRT13	PZE	**		SPRT0050
	SXA	X4,4		SPRT0060
	SXA	X4+1,2		SPRT0070
	SXA	X4+2,1		SPRT0080
	LAC	SPRT13,4		SPRT0090
	CLA	2,4		SPRT0100
	STA	XSIU		SPRT0110
	STZ	LOM		SPRT0120
				SPRT0130
AGAIN	TSX	TSHIO.,4		SPRT0140
	PZE	FILO5.		SPRT0150
	MZE	FMT,,FMTSC.		SPRT0160
	AXT	14,4		SPRT0170
	TSL	HNLIO.		SPRT0180
	STO	CARD+14,4		SPRT0190
	TIX	*-2,4,1		SPRT0200
	TSX	RTNIO.,4		SPRT0210
	AXT	0,4		SPRT0220
	TSL	BCDBG	GET ID	SPRT0230
	TXI	**3,0,0		SPRT0240
	PZE	CARD,,0		SPRT0250
	P7E	10		SPRT0260
	CLA	VALUE		SPRT0270
XSIU	STO	**4		SPRT0280
	TSL	BCDBG	GET TIME	SPRT0290
	TXI	**3,0,0		SPRT0300
	PZE	CARD+2,,0		SPRT0310
	P7F	A		SPRT0320
	PCS	CARD+3,,0		SPRT0330
	TSX	MINUS,2		SPRT0340
	TSL	BCDBG	GET CH 1	SPRT0350
	TXI	**3,0,0		SPRT0360
	PZE	CARD+4,,1		SPRT0370
	PZE	3		SPRT0380
	PCS	CARD+4,,4		SPRT0390
	TSX	MINUS,2		SPRT0400
	TSL	BCDBG	GET CH2	SPRT0410
	TXI	**3,0,0		SPRT0420
	P7E	CARD+5,,5		SPRT0430
	PZE	3		SPRT0440
	PCS	CARD+6,,2		SPRT0450
	TSX	MINUS,2		SPRT0460
	TSL	BCDBG	GET CH3	SPRT0470
	TXI	**3,0,0		SPRT0480

	PZE	CARD+7,,3		SPRT0490
	PZE	3		SPRT0500
	PCS	CARD+8,,0		SPRT0510
	TSX	MINUS,2		SPRT0520
	TSL	BCDBG	GET CH4	SPRT0530
	TXI	**3,0,0		SPRT0540
	PZE	CARD+9,,1		SPRT0550
	PZE	3		SPRT0560
	PCS	CARD+9,,4		SPRT0570
	TSX	MINUS,2		SPRT0580
	TSL	BCDBG	GET CH5	SPRT0590
	TXI	**3,0,0		SPRT0600
	PZE	CARD+10,,5		SPRT0610
	PZE	3		SPRT0620
	PCS	CARD+11,,2		SPRT0630
	TSX	MINUS,2		SPRT0640
	TSL	BCDBG	GET CH6	SPRT0650
	TXI	**3,0,0		SPRT0660
	PZE	CARD+12,,3		SPRT0670
	PZE	3		SPRT0680
	PCS	CARD+13,,0		SPRT0690
	TSX	MINUS,2		SPRT0700
X4	AXT	** ,4		SPRT0710
	AXT	** ,2		SPRT0720
	AXT	** ,1		SPRT0730
	TRA*	SPRT13		SPRT0740
	* BCD TO BINARY ROUTINE			SPRT0750
BCDBG	PZE	**		SPRT0760
	SXA	BCAX,4		SPRT0770
	LAC	BCDBG,4		SPRT0780
	CLA	1,4		SPRT0790
	STA	PICK		SPRT0800
	ARS	18		SPRT0810
	SAC	PICK,,2		SPRT0820
	SUB	=6		SPRT0830
	PAX	,2		SPRT0840
	CLA	2,4		SPRT0850
	PAX	,4		SPRT0860
	AXT	0,1		SPRT0870
	STZ	VALUE		SPRT0880
	STZ	COUNT		SPRT0890
	ZAC			SPRT0900
PICK	PCS	** ,1,**		SPRT0910
	CCS	JUNK,,5		SPRT0920
	TRA	ERRM		SPRT0930
	TRA	ERR		SPRT0940
	LDQ	JUNK		SPRT0950
	VMA	VALUE,,4		SPRT0960
	LLS	4		SPRT0970
	STO	VALUE		SPRT0980
	TNX	BCAX-1,4,1		SPRT0990

ZAC			SPRT1000
	TNX	**+5,2,1.	SPRT1010
	PCS	PICK,,2.	SPRT1020
	ADD	=1	SPRT1030
	SAC	PICK,,2	SPRT1040
	TRA	PICK	SPRT1050
	AXT	6,2	SPRT1060
	TXI	**3,1,-1	SPRT1070
BRA	BRN	ERMA	SPRT1080
BCAX	AXT	**4	SPRT1090
	TRA*	BCDBG	SPRT1100
	* MINUS ROUTINE		SPRT1110
MINUS	CCS	JUNK,,2	SPRT1120
	IRA	**2	SPRT1130
	TRA	**5	SPRT1140
	CCS	JUNK,,1	SPRT1150
	TRA	ERR	SPRT1160
	TRA	**3	SPRT1170
	TRA	ERR	SPRT1180
	MSM	VALUE	SPRT1190
	CLA	VALUE	SPRT1200
	DRA	=02330000000000	SPRT1210
	FAD	=02330000000000	SPRT1220
	TXI	**1,4,-1	SPRT1230
	STO*	XSTO	SPRT1240
	TRA	1,2	SPRT1250
	* ERRO ^D ROUTINE		SPRT1260
ERR	TSX	STIID.,4	SPRT1270
	PZE	FIL06.	SPRT1280
	MZE	FMT1,,FMTSC.	SPRT1290
	AXT	14,4	SPRT1300
	CLA	CARD+14,4	SPRT1310
	TSL	HNLIO.	SPRT1320
	TIX	**2,4,1	SPRT1330
	TSX	FILIO.,4	SPRT1340
	CLA	=1	SPRT1350
	STO	LOM	SPRT1360
	TRA	X4	SPRT1370
ERRM	CCS	JUNK,,1	SPRT1380
	TRA	ERR	SPRT1390
	TRA	**2	SPRT1400
	TRA	ERR	SPRT1410
	CLA	COUNT	SPRT1420
	ADD	=1	SPRT1430
	STO	COUNT	SPRT1440
	MSM	BRA	SPRT1450
	TRA	PICK+8	SPRT1460
ERMA	MSP	BRA	SPRT1470

LAC	BCDBG,4		SPRT1480
CLA	2,4		SPRT1490
SUB	COUNT		SPRT1500
TNZ	FRR		SPRT1510
MSM	VALUE		SPRT1520
LXA	BCAX,4		SPRT1530
TRA*	BCDBG		SPRT1540
ERMA1	TXL	ERMA2,4,-2	SPRT1550
	CLS	=6	SPRT1560
	TRA	ERMA12	SPRT1570
ERMA2	CLS	=3	SPRT1580
	TRA	ERMA2	SPRT1590
FMT	BCI	1,(14A6)	SPRT1600
JUNK	OCT	006040000012	SPRT1610
FMT1	BCI	5,(15H CARD REJECTED-13A6,A2)	SPRT1620

COUNT	BSS	1	SPRT1630
VALUE	BSS	1	SPRT1640
CARD	BSS	14	SPRT1650
	CONTRL	//	SPRT1660
	USE	//	SPRT1670
DATA	BSS	2021	SPRT1680
LOM	BSS	1	SPRT1690
	USE	PREVIOUS	SPRT1700
	LITERALS		

END			SPRT1710
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**				DT650000
**	MAP	SUBROUTINE USED TO READ TYPE-2 AND TYPE-3 SPORT DATA.		DT650010
**	L J	GANNON AND R J WAGNER		DT650020
**				DT650030
	ENTRY	DAT650		DT650040
**				DT650050
	EXTERN	.EXP2.		DT650060
*				DT650070
DAT650	TRA	**	EXIT INSTRUCTION	DT650080
	SXA	XA,4		DT650090
	SXA	XA+1,1		DT650100
	SXA	XA+2,2		DT650110
	LAC	DAT650,4		DT650120
	CLA	2,4		DT650130
	ADD*	4,4		DT650140
	STA	ADD1	ADDRESS OF A + N	DT650150
	STA	ADD2	ADDRESS OF A + N	DT650160
	CLA	3,4		DT650170
	ADD*	4,4		DT650180
	STA	BADD1	ADDRESS OF B + N	DT650190
	STA	BADD2	ADDRESS OF B + N	DT650200
	CLA*	4,4		DT650210
	PAX	.2	N IN INDEX REG 2	DT650220
*				DT650230
ADD1	CLA	** , 2	FRACTION	DT650240
	TZE	CONT	IF THE NO IS ZERO, NO CONVERSION	DT650250
	STO	TEMP		DT650260
BADD1	LDQ	** , 2	EXPONENT	DT650270
BADD2	CAL	** , 2	EXPONENT	DT650280
	ANA	=000400000000	MASK TO KEEP MINUS SIGN	DT650290
	ALS	6	SHIFT SIGN INTO P BIT	DT650300
	ORA	TEMP		DT650310
	SLW	TEMP	PUT SIGN ON FRACTION	DT650320
	SLW*	ADD1		DT650330
	ZAC			DT650340
	LGL	6		DT650350
	STO	TEMP1	HIGH ORDER DIGIT OF EXPONENT	DT650360
	ZAC			DT650370
	LGL	6		DT650380
	ANA	=017	TAKE OFF SIGN BITS	DT650390
	CAS	=012	SEE IF ZERO, + OR - ZERO HAS XX1010 CORE CODE	DT650400
	TRA	**+2	NO	DT650410
	ZAC		YES, SET TO ZERO	DT650420
	STO	TEMP2	LOW ORDER DIGIT OF EXPONENT	DT650430
	LDQ	TEMP1		DT650440
	MPY	=10	BCD TO BINARY	DT650450
	LLS	35		DT650460
	ADD	TEMP2		DT650470
	SUB	=50	SUBTRACT BASE 50	DT650480
	TZE	CONT	IF EXPONENT IS ZERO	DT650490

	LRS	35	PLACE IN MQ	DT650500
	CLA	=10.		DT650510
	TSL	.EXP2.	GO TO FLOAT NUMBER TO FIX POWER SUBROUTINE	DT650520
	LRS	35		DT650530
	FMP	TEMP		DT650540
ADD2	STO	**2		DT650550
CONT	TIX	ADD1,2,1		DT650560
*				DT650570
XA	AXT	**4		DT650580
	AXT	**1		DT650590
	AXT	**2		DT650600
	TRA*	DAT650		DT650610
*				DT650620
TEMP	BSS	1		DT650630
TEMP1	BSS	1		DT650640
TEMP2	BSS	1		DT650650
	LITERALS			

END

DT650660

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**			TIMX0000
**	MAP SUBROUTINE USED TO REFERENCE COMPUTER TIME CLOCK.		TIMX0010
**	L A SCHMITTROTH		TIMX0020
**			TIMX0030
	ENTRY	TIMX	TIMX0040
**			TIMX0050
TIMX	PZE	**	TIMX0060
	CLA	TIMX	TIMX0070
	ADD	=2	TIMX0080
	STA	STORE	TIMX0090
	CLA	5	TIMX0100
STORE	STO*	**	TIMX0110
	TRA*	TIMX	TIMX0120
	LITERALS		
	END		TIMX0130

C	FORTRAN SUBROUTINE WHICH CALCULATES ELAPSED COMPUTER TIME.	ETMX0000
C		ETMX0010
	SUBROUTINE ETIMX(ITX,IETM,RETS)	ETMX0020
C	CALL TIMX(JTX)	ETMX0030
	IETM=(JTX-ITX)/3600	ETMX0040
	RETS=FLOAT(JTX-ITX)/60.0-FLOAT(IETM*60)	ETMX0050
	ITX=JTX	ETMX0060
	RETURN	ETMX0070
C		ETMX0080
	END	ETMX0090
		ETMX0100

C	FORTRAN SUBROUTINE WHICH SELECTS THE MINIMUM AND MAXIMUM VALUES	MXMNO000
C	FROM AN ARRAY.	MXMNO010
C	SUBROUTINE MAXMIN(SCALE,ARRAY,ISTART,ITOTAL,IJUMP)	MXMNO020
C		MXMNO030
C	DIMENSION SCALE(2),ARRAY(1)	MXMNO040
C		MXMNO050
C	DO 25 I=ISTART,ITOTAL,IJUMP	MXMNO060
	IF (ARRAY(I).LT.SCALE(1)) SCALE(1)=ARRAY(I)	MXMNO070
	IF (ARRAY(I).LT.1.0E+30.AND.ARRAY(I).GT.SCALE(2))SCALE(2)=ARRAY(I)	MXMNO080
25	CONTINUE	MXMNO090
	RETURN	MXMNO100
C		MXMNO110
	END	MXMNO120
		MXMNO130


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**
** MAP SUBROUTINE WHICH UNLOADS SPORT OUTPUT TAPES. T O ELSETHAGEN UNLD0000
** ENTRY UNLOAD UNLD00010
** UNLD00020
** UNLD00030
** UNLD00040
UNLOAD PZE ** UNLD00050
SXA X4,4 SAVE INDEX REGISTER 4 UNLD00060
LAC UNLOAD,4 UNLD00070
CLA* 2,4 PICKUP FORTRAN FILE NUMBER UNLD00080
LAS NFILES IS FORTRAN FILE NUMBER GT. 11 UNLD00090
TRA STOP1 YES UNLD00100
NOP UNLD00110
PAC ,4 NO UNLD00120
CLA TABLE,4 PICKUP CORRECT BCD FILE NAME UNLD00130
STO TEMP UNLD00140
TMI STOP2 TRANSFER IF SYS. INPUT,OUTPUT,PUNCH UNLD00150
LAC S.SLOC+1,4 ADDRESS OF FILE CONTROL BLOCK IN XR4 UNLD00160

LXD S.SLOC+1,2 DECREMENT OF FCB IN XR2 UNLD00170

CLA 17,4 UNLD00180
CAS TEMP UNLD00190

TRA **2 UNLD00200
TRA FOUND FOUND CORRECT FILE CONTROL BLOCK UNLD00210
TXI **1,4,-19 UNLD00220
TIX *-5,2,1 UNLD00230
TRA STOP3 CANNOT FIND CORRECT FCB UNLD00240
FOUND PXA ,4 UNLD00250
PAC ,4 UNLD00260
SXA TEMP1,4 UNLD00270
TSX S.CLOSE,4 UNLD00280
TEMP1 PTW ** UNLD00290
X4 AXT **,4 UNLD00300
TRA* UNLOAD UNLD00310
* UNLD00320
* * STORAGE AND TABLE OF FILES * UNLD00330
* UNLD00340
STOP1 CLA UNLOAD UNLD00350
TSX S.XOVA,4 UNLD00360
STO FMT1+10 UNLD00370
TSX STHIO.,4 UNLD00380
PZE F1L06. UNLD00390
PZE FMT1 UNLD00400
TSX F1L10.,4 UNLD00410

PZE UNLD00420
STOP2 CLA UNLOAD UNLD00430
TSX S.XOVA,4 UNLD00440
STO FMT2+10 UNLD00450

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	TSX	STHIO.,4	UNLD0460
	PZE	FIL06.	UNLD0470
	PZE	FMT2	UNLD0480
	TSX	FILIO.,4	UNLD0490
	PZE		UNLD0500
STOP3	TSX	STHIO.,4	UNLD0510
	PZE	FIL06.	UNLD0520
	PZE	FMT3	UNLD0530
	TSX	FILIO.,4	UNLD0540
	PZE		UNLD0550
FMT1	TSX	IOHHC.,4	UNLD0560
	PZE	36	UNLD0570
	BCI	6,FILE NAME GT 11 ERROR LOCATION	UNLD0580

	TRA	IOHEF.	UNLD0590
FMT2	TSX	IOHHC.,4	UNLD0600
	PZE	54	UNLD0610
	BCI	9, ATTEMPTING TO REWIND SYSTEM INPUT,OUTPUT,PUNCH	UNLD0620

	TRA	IOHEF.	UNLD0630
FMT3	TSX	IOHHC.,4	UNLD0640
	PZE	41	UNLD0650
	BCI	7,COULD NOT FIND CORRECT FILE CONTROL BLOCK	UNLD0660

TEMP	BSS	1	UNLD0670
TABLE	BCI	1,FTC00.	UNLD0680
	BCI	1,FTC01.	UNLD0690
	BCI	1,FTC02.	UNLD0700
	BCI	1,FTC03.	UNLD0710
	BCI	1,FTC04.	UNLD0720
	MZE		UNLD0730
	MZE		UNLD0740
	MZE		UNLD0750
	BCI	1,FTC08.	UNLD0760
	BCI	1,FTC09.	UNLD0770

BCI	1,FTC10.		UNLD0780
BCI	1,FTC11.		UNLD0790
NFILES	PZE	*-TABLE-1	UNLD0800
EXTERN	STHIO., IOHHC., IOHEF., FILIO., FILO6.		UNLD0810
EXTERN	S.SLOC	GENERATED	
EXTERN	S.CLSE	GENERATED	
EXTERN	S.XOVA	GENERATED	
END			UNLD0820

D

**			SET 0000
**	MAP SUBROUTINE WHICH SETS UP TRANSFER TO THE NEXT PROBLEM IF		SET 0010
**	CERTAIN ERRORS OCCUR. R L COATES		SET 0020
**			SET 0030
**	EXTERN	READY	SET 0040
**	ENTRY	SET	SET 0050
**			SET 0060
**			SET 0070
SET	PZE	**	SET 0080
	SXA	SET,4	SET 0090
	LAC	SET,4	SET 0100
	CLA*	2,4	SET 0110
	ADD	SET	SET 0120
	STO	NO	SET 0130
	CALL	READY(NO)	SET 0140
SET1	AXT	** , 4	SET 0150
	TRA*	SET	SET 0160
NO	BSS	1	SET 0170
	END		SET 0180

UPDATE PROCEDURE USED TO OBTAIN MODIFIED
XEM FOR USE WITH SUBROUTINE 'SET'

\$PAUSE	MOUNT REEL NO. 348 ON S.SU05, SCRATCH ON S.SU07		
\$EXECUTE	UPDATE		
\$RUN EXTRACT			
\$LOCATE XEM			
ENTRY	READY		FTL22590
READY PZE	**		FTL22680
SXA	**4,4		FTL22681
LAC	READY,4		FTL22682
CLA*	2,4		FTL22683
STA	OPEXIT		FTL22684
AXI	**4		FTL22685
TRA*	READY		FTL22686
\$DELETE FTL22760			
CELL1 OCT	+377777777777		FTL23890
CELL2 OCT	+377777777777		FTL23910
\$ENDRUN			
\$IBSYS			
\$IBJOB	NOGO		
\$IEDIT	U07,SRCH		
\$IBMAP XEM			
\$IEDIT			

C	FORTRAN PROCESSING SUBROUTINE PROGRAM SMOOTH.	SMTH0000
C	SMTH0010
	SUBROUTINE SMOOTH(PART,ICODE,KSF,DT)	SMTH0020
C	SMTH0030
	COMMON DATA(2021),LOM,IFINC	SMTH0040
	DIMENSION T(100),U(100),BUFF(600),STOR(400),	SMTH0050
	1 HEAD(14),SCT(2),SCP(2),SSL(2)	SMTH0060
	REAL MT1,MT2,MT3,MT4,M1,M2,M3,M4,M5,M6,MAG,L1,L2	SMTH0070
	INTEGER CHNLNO,PCODE,PLCODE,PART	SMTH0080
	LOGICAL SWTCH1,SWTCH2,SWTCH3,SWTCH4,SWTCH5,SWTCH6,SWTCH7,SWTCH8,	SMTH0090
	1 SWTCH9,SWCH10,SWCH11,SWCH12,SWCH13,SWCH14,SWCH15	SMTH0100
	EQUIVALENCE (DATA(1),T),(DATA(101),U),(DATA(201),BUFF),	SMTH0110
	1 (DATA(801),STOR),(K,SWCH13)	SMTH0120
C	SMTH0130
C	READ SMOOTH TITLE CARD	SMTH0140
C	SMTH0150
	CALL TIMX(ITM)	SMTH0160
	READ(5,1) HEAD	SMTH0170
	1 FORMAT(13A6,1A2)	SMTH0180
	LD=20000000002	SMTH0190
	IBLANK=-17997958192	SMTH0200
	IPASNO=1	SMTH0210
	15 LOM=0	SMTH0220
	1655 SCP(1)=1.0E+30	SMTH0230
	SCP(2)=-1.0E+30	SMTH0240
	SSL(1)=1.0E+30	SMTH0250
	SSL(2)=-1.0E+30	SMTH0260
	XLT=10.0	SMTH0270
	XLP=7.0	SMTH0280
C	SMTH0290
C	READ SMOOTH CONTROL CARD	SMTH0300
C	SMTH0310
	READ(5,607)ND,NDL,DT,TO,TF,TRR,TRP,N,PCODE,PLCODE,IFORM,ISCAL,	SMTH0320
	1 ORDER,IRECYL,ITRANS,ISAVE	SMTH0330
	607 EDRMATE(19,A1,5E10.8,12,811)	SMTH0340
	CALL ID650(ND,NDL)	SMTH0350
	REWIND 4	SMTH0360
	READ(4) IU,CHNLNO,DT2	SMTH0370
	IF(ICODE.EQ.5 .AND. CHNLNO.EQ.0) ND=ND/1000*1000	SMTH0380
	CALL HEADER	SMTH0390
	WRITE(6,2)	SMTH0400
	2 FORMAT(1H0,28H QUADRATIC SMOOTHING PROGRAM78X,15H N L S O R T)	SMTH0410
	5 WRITE(6,9)HEAD,IPASNO,ND,DT,TO,TF,TRR,TRP,N,PCODE,PLCODE,IFORM,	SMTH0420
	1 ISCAL,ORDER,IRECYL,ITRANS,ISAVE	SMTH0430
	9 FORMAT(107X15H U I PDC R E RS/1X,13A6,1A2,26X15H M S LAA D C AM /	SMTH0440
	1 107X,15H B T O T L E Y NN / 13H PASS NUMBER12,12X,6H ID NO,5X,8H DS	SMTH0450
	2ELTA T,6X,10H T MINIMUM,4X,10H T MAXIMUM,3X,28H T START CAL 1ST OS	SMTH0460
	3UTPUT T 15H R G TAE R L ST//26H SMOOTH CONTROL CARD WAS-,110,	SMTH0470
	4 5F14.6,13,212,211,312,11,13,12,13,12)	SMTH0480
	IF(ID.EQ.ND) GO TO 657	SMTH0490
	WRITE(6,601) ID	SMTH0500
	601 FORMAT(1H0,25H WRONG ID NUMBER DATA ID-110)	SMTH0510
	N=-1	SMTH0520
C	SMTH0530
C	SET SMOOTH PARAMETERS	SMTH0540

C		SMT0550
657	IF(TO.EQ.-0.0) TO = -1.0E+28	SMT0560
	IF(TF.EQ.-0.0) TF = +1.0E+28	SMT0570
	IF(DT.EQ.0.0) DT=DT2	SMT0580
	IF(ICODE.NE.5) DT2=0.0	SMT0590
	IF(IRECYL.LT.2) GO TO 1657	SMT0600
1557	SWTCH1=.TRUE.	SMT0610
	SWTCH2=.FALSE.	SMT0620
	SWTCH4=.FALSE.	SMT0630
	SWTCH8=.TRUE.	SMT0640
	SWTCH3=.TRUE.	SMT0650
1558	TSR=TO	SMT0660
	TSP=TO	SMT0670
	GO TO 1659	SMT0680
1657	IF(PCODF.EQ.1) PUNCH 1,HEAD	SMT0690
	TSP=TRP	SMT0700
	SWTCH1=PCODE.EQ.3	SMT0710
	SWTCH2=PCODE.EQ.1	SMT0720
	SWTCH3=PLCODE.EQ.0	SMT0730
	SWTCH4=SWTCH3.AND.PART.EQ.1.AND.ITRANS.EQ.0	SMT0740
	SWTCH8=ISCAL.EQ.0	SMT0750
	SWCH14=PLCODE.LT.3	SMT0760
1658	TSR=TRR	SMT0770
1659	TS=TSR	SMT0780
	K=-0	SMT0790
	K2=-3	SMT0800
	NCT=50	SMT0810
	IF(SWTCH4) GO TO 923	SMT0820
	REWIND B	SMT0830
	WRITE(8) NO,CHNLNO,DT	SMT0840
923	IF(SWTCH8) GO TO 924	SMT0850
C		SMT0860
C	READ IN SCALE FACTORS FOR PLOT	SMT0870
C		SMT0880
	READ(5,613) TMIN,TMAX,PMIN,PMAX,SMIN,SMAX,LT,LP	SMT0890
613	FORMAT(6E10.3,2I2)	SMT0900
	IF(LT.NE.0) XLT=LT	SMT0910
	IF(LP.NE.0) XLP=LP	SMT0920
	DTM=(TMAX-TMIN)/XLT	SMT0930
	DPR=(PMAX-PMIN)/XLP	SMT0940
	DSR=(SMAX-SMIN)/XLP	SMT0950
		SMT0960
924	IF(N.LE.2) GO TO 17	SMT0970
	IF(((1-N)*N).GT.0) N=N-1	SMT0980
	SWTCH5=INT(ABS(DT2-DT)*1.0E+7).EQ.0	SMT0990
925	LL=N-1	SMT1000
	XN=N	SMT1010
	IF(SWTCH5) UT=DT2	SMT1020
	SWTCH6=.FALSE.	SMT1030
		SMT1040
C		SMT1050
C	FILL DATA ARRAY	SMT1060
C		SMT1070
710	READ(4) BUFF	SMT1070
	KR=-1	SMT1080
10	KR=KR+2	SMT1090

	IF(KR.EQ.601) GO TO 710	SMTH1100
	T(1)=BUFF(KR)	SMTH1110
	IF(T(1).GT.TF) GO TO 17	SMTH1120
	IF(T(1).LT.TO) GO TO 10	SMTH1130
	U(1)=BUFF(KR+1)	SMTH1140
	DO 30 I=2,N	SMTH1150
28	KR=KR+2	SMTH1160
	IF(KR.LT.601) GO TO 728	SMTH1170
	READ(4) BUFF	SMTH1180
	KR=1	SMTH1190
	GO TO 28	SMTH1200
728	T(I)=BUFF(KR)	SMTH1210
	IF(T(I).GT.TF) GO TO 17	SMTH1220
	IF(T(I).LE.T(I-1)) GO TO 55	SMTH1230
	TIME=T(I)	SMTH1240
30	U(I)=BUFF(KR+1)	SMTH1250
	I1=(N-1)/2	SMTH1260
	I2=(N+1)/2	SMTH1270
	I3=(N+3)/2	SMTH1280
C		SMTH1290
C	READ IN DATA UNTIL SMOOTHING CAN BEGIN AT T = T&R	SMTH1300
C		SMTH1310
110	TEMP=(T(I1)+T(I2))*0.5	SMTH1320
	IF(SWTCH5 .OR. IRECYL.LT.2) GO TO 111	SMTH1330
	TS=TRR-FLOAT(INT((TRR-TEMP)/DT))*DT	SMTH1340
	IF(TS.LT.TEMP) TS=TS+DT	SMTH1350
	TSR=TS	SMTH1360
	TSP=TS	SMTH1370
111	IF(TS-TEMP) 50,70,60	SMTH1380
C		SMTH1390
C	RESET TSR TO MIN ACCEPTABLE VALUE RETAINING ORIG TIMESHIFT	SMTH1400
C		SMTH1410
50	IF(SWTCH5) GO TO 70	SMTH1420
	TSP=TSP-TSR+TEMP	SMTH1430
	TSR=TEMP	SMTH1440
	TS=TEMP	SMTH1450
	WRITE(6,612) TSR,TSP	SMTH1460
612	FORMAT(1H,25H CONTROL WORDS RESET -.52X,2F14.6)	SMTH1470
	GO TO 70	SMTH1480
C		SMTH1490
C	READ IN ANOTHER DATA VALUE	SMTH1500
C		SMTH1510
41	KR=KR+2	SMTH1520
	IF(KR.LT.601) GO TO 741	SMTH1530
	READ(4) BUFF	SMTH1540
	KR=1	SMTH1550
741	T(N)=BUFF(KR)	SMTH1560
	IF(T(N).LE.T(N-1)) GO TO 55	SMTH1570
	TIME=T(N)	SMTH1580
	IF(TIME.GT.TF) GO TO 841	SMTH1590
	U(N)=BUFF(KR+1)	SMTH1600
	GO TO 60	SMTH1610
C		SMTH1620
C	ERROR RETURNS	SMTH1630
C		SMTH1640

55	WRITE(6,56) TIME	SMTH1650
56	FORMAT(1H041H TIME SEQUENCE ERROR IN INPUT DATA AT T =F12.6)	SMTH1660
17	LOM=1	SMTH1670
C		SMTH1680
C	NORMAL RETURN	SMTH1690
C		SMTH1700
841	IF(SWTCH4) GO TO 3842	SMTH1710
	IF(IPASNO.LT.IRECYL) GO TO 6080	SMTH1720
6841	WRITE(8) STOR	SMTH1730
	IF(ITRANS.EQ.0) GO TO 3842	SMTH1740
C		SMTH1750
C	TRANSFER SMOOTHED DATA TO OUTPUT TAPE	SMTH1760
C		SMTH1770
	REWIND 8	SMTH1780
	IF(ITRANS.FQ.1) REWIND 9	SMTH1790
	READ(8) ND,CHNLNO,DT	SMTH1800
	WRITE(9) ND,CHNLNO,DT,K	SMTH1810
	NORECS=(K-1)/100+1	SMTH1820
	DO 3843 J=1,NORECS	SMTH1830
	READ(8) STOR	SMTH1840
3843	WRITE(9) STOR	SMTH1850
	WRITE(6,3845)	SMTH1860
3845	FORMAT(1H0,41H SMOOTHED DATA TRANSFERRED TO OUTPUT TAPE)	SMTH1870
	IF(ISAVE.EQ.0) GO TO 3842	SMTH1880
C		SMTH1890
C	UNLOAD OUTPUT TAPE	SMTH1900
C		SMTH1910
	WRITE(9) LD,CHNLNO,DT,K	SMTH1920
	END FILE 9	SMTH1930
	CALL UNLOAD(9)	SMTH1940
	CALL TYPE(1H,1,0)	SMTH1950
	CALL TYPE(38H REMOVE DATA TAPE GENERATED ON T,8,6,38,0)	SMTH1960
	CALL TYPE(20H AND RECORD REEL NUMBER,28,U)	SMTH1970
	WRITE(6,3846)	SMTH1980
3846	FORMAT(1H0,21H OUTPUT TAPE UNLOADED)	SMTH1990
C		SMTH2000
C	END OF CALCULATIONS	SMTH2010
L		SMTH2020
3842	CALL ETIMX(ITM,ICALM,RCALS)	SMTH2030
	IF(.NOT.SWTCH3 .AND. K.GT.25) GO TO 800	SMTH2040
	WRITE(6,609) ICALM,RCALS	SMTH2050
609	FORMAT(1H0,27H CALCULATIONS REQUIRED 14,5H MIN F4.1,4H SECA1,	SMTH2060
	1 17HAND PLOT REQUIREDI3,5H MIN F4.1,4H SEC)	SMTH2070
842	IF(IPASNO.LT.IRECYL) GO TO 4090	SMTH2080
	KSF=K	SMTH2090
	RETURN	SMTH2100
C		SMTH2110
C	TRANSFER OUTPUT TO S.SU04 FOR RESMOOTHING	SMTH2120
C		SMTH2130
4090	IF(K.GT.0) GO TO 5000	SMTH2140
	K=-K	SMTH2150
	LOM=1	SMTH2160
	IF(K.LT.50) K=0	SMTH2170
5000	REWIND 8	SMTH2180
	READ(8) ND,CHNLNO	SMTH2190

	REWIND 4	SMTH2200
6050	WRITE(4) ND,CHNLNO,DT	SMTH2210
C		SMTH2220
	NOCRO4=K/300	SMTH2230
	NOCRO8=K/100	SMTH2240
	IF(NOCRO4.EQ.0) GO TO 5001	SMTH2250
	IEND=600	SMTH2260
	GO TO 5004	SMTH2270
C		SMTH2280
5001	IEND=(NOCRO8-NOCRO4)*200	SMTH2290
	IF(IEND.EQ.0) GO TO 5002	SMTH2300
	J=0	SMTH2310
	GO TO 5009	SMTH2320
C		SMTH2330
5002	ISTART=-199	SMTH2340
5003	ISTART=ISTART+200	SMTH2350
	IDONE=ISTART+(K-NOCRO8*100)*2-1	SMTH2360
	BUFF(IDONE+1)=1.0E+30	SMTH2370
	IEND=0	SMTH2380
	J=NOCRO4+1	SMTH2390
	IF(IDONE.GT.ISTART) GO TO 5012	SMTH2400
	GO TO 5013	SMTH2410
C		SMTH2420
5004	J=0	SMTH2430
5005	J=J+1	SMTH2440
5009	ISTART=-199	SMTH2450
5010	ISTART=ISTART+200	SMTH2460
	IDONE=ISTART+199	SMTH2470
5012	READ(8) (BUFF(I),BUFF(I+1),B,B,I=ISTART,IDONE,2)	SMTH2480
	IF(IDONE.LT.IEND) GO TO 5010	SMTH2490
	IF(J.EQ.0) GO TO 5003	SMTH2500
C		SMTH2510
5013	WRITE(4) BUFF	SMTH2520
	IF(J.LT.NOCRO4) GO TO 5005	SMTH2530
	IF(IEND.EQ.600) GO TO 5001	SMTH2540
C		SMTH2550
	IPASNO=IPASNO+1	SMTH2560
	REWIND 4	SMTH2570
	READ(4) ID,CHNLNO,DT2	SMTH2580
	WRITE(6,5017) IPASNO	SMTH2590
5017	FORMAT(1H0,11H BEGIN PASSI2)	SMTH2600
	IF(IPASNO.EQ.IRECYL) GO TO 1657	SMTH2610
	GO TO 1558	SMTH2620
C		SMTH2630
C	CHECK TO SEE IF MORE DATA IS NEEDED TO CAL NEXT SMOOTHED VALUE	SMTH2640
C		SMTH2650
60	TEMP=(T(I2)+T(I3))/2	SMTH2660
61	IF(TS-TEMP)70,70,80	SMTH2670
80	ICNT=ICNT+1	SMTH2680
	DO 90 I=1,LL	SMTH2690
	T(I)=T(I+1)	SMTH2700
90	U(I)=U(I+1)	SMTH2710
	GO TO 41	SMTH2720
C		SMTH2730
C	CALCULATE SMOOTH COEFFICIENTS	SMTH2740

C		SMTH2750
70	IF(SWCH13) GO TO 6060	SMTH2760
3070	K=K+1	SMTH2770
	IF(.NOT.SWCH5) GO TO 970	SMTH2780
C		SMTH2790
C	EVEN TIME INCREMENT SMOOTHING SECTION	SMTH2800
C		SMTH2810
	IF(SWICH6) GO TO 71	SMTH2820
	TSP=TSP-TSR+T(I2)	SMTH2830
	TSR=T(I2)	SMTH2840
	TS=TSR	SMTH2850
	WRITE(6,612) TSR,TSP	SMTH2860
971	L1=DT*DT*FLOAT((N*N-1)*N)/12.0	SMTH2870
	L2=(DT**4)*FLOAT((3*N**4-10*N*N+7)*N)/240.0	SMTH2880
	XNC=(XN 0.7)*DT	SMTH2890
	DETT=XN*L1-L2-L1*L1	SMTH2900
	A1=XN*L1/DETT	SMTH2910
	B1=(XN*L2-L1*L1)/DETT	SMTH2920
	C1=L1*L2/DETT	SMTH2930
	C2=-L1*L1/DETT	SMTH2940
	LQ=N+1	SMTH2950
	HFDT=DT*0.5	SMTH2960
	QDTS=HFDT/HFDT	SMTH2970
	SWTCH6=.TRUE.	SMTH2980
71	IF(T(N)-T(1).GT.XNC) GO TO 970	SMTH2990
72	FO=0.0	SMTH3000
	F1=0.0	SMTH3010
	F2=0.0	SMTH3020
	DO 73 I=1,I1	SMTH3030
	L=LQ-I	SMTH3040
	SX=LQ-2*I	SMTH3050
	F1=F1+(U(L)-U(I))*SX	SMTH3060
73	F2=F2+(U(L)+U(I))*SX*SX	SMTH3070
	DO 74 I=1,N	SMTH3080
74	FO=FO+U(I)	SMTH3090
	F1=F1*HFDT	SMTH3100
	F2=F2*QDTS	SMTH3110
	C=C1*FO+C2*F2	SMTH3120
	B=B1*F1	SMTH3130
	A=C2*FO+A1*F2	SMTH3140
	GO TO 75	SMTH3150
C		SMTH3160
C	SAVE INITIAL VALUES FOR RECYCLING	SMTH3170
C		SMTH3180
6060	IF(IPASNO.GE.IRECYL) GO TO 3070	SMTH3190
	TMSHFT=TSP-TSR	SMTH3200
	DO 6070 J2=1,I1	SMTH3210
	K2=K2+4	SMTH3220
	STOR(K2)=T(J2)+TMSHFT	SMTH3230
	STOR(K2+1)=U(J2)	SMTH3240
6070	STOR(K2+2)=1.5E+30	SMTH3250
	KADDT0=I1	SMTH3260
	GO TO 3070	SMTH3270
C		SMTH3280
C	SAVE FINAL VALUES FOR RECYCLING	SMTH3290

C		SMTH3300
6080	NRL=N	SMTH3310
	IF(TIME.LT.TF) GO TO 6081	SMTH3320
	I3=I2	SMTH3330
	NRL=N-1	SMTH3340
6081	DO 6090 J2=I3,NRL	SMTH3350
	K2=K2+4	SMTH3360
	STOR(K2)=T(J2)+TMSHFT	SMTH3370
	STOR(K2+1)=U(J2)	SMTH3380
	STOR(K2+2)=1.5E+30	SMTH3390
	IF(K2.LT.397) GO TO 6090	SMTH3400
	WRITE(8) STOR	SMTH3410
	K2=-3	SMTH3420
6090	CONTINUE	SMTH3430
	WRITE(8) STOR	SMTH3440
	K=K+KADDT0+N-I2	SMTH3450
	GO TO 3842	SMTH3460
C		SMTH3470
C	UNEVEN TIME INCREMENT SMOOTHING SECTION	SMTH3480
C		SMTH3490
970	DO 140 I=1,N	SMTH3500
140	T(I)=T(I)-TS	SMTH3510
	F0=0.	SMTH3520
	FT=0.	SMTH3530
	FT2=0.	SMTH3540
	MT1=0.	SMTH3550
	MT2=0.	SMTH3560
	MT3=0.	SMTH3570
	MT4=0.	SMTH3580
	DO 120 I=1,N	SMTH3590
	MT1 = MT1 + T(I)	SMTH3600
	XT2 = T(I) * T(I)	SMTH3610
	MT2 = MT2 + XT2	SMTH3620
	XT3 = XT2 * T(I)	SMTH3630
	MT3 = MT3 + XT3	SMTH3640
	XT4 = XT3 * T(I)	SMTH3650
	MT4 = MT4 + XT4	SMTH3660
	F0 = F0 + U(I)	SMTH3670
	FT = FT + U(I) * T(I)	SMTH3680
120	FT2 = FT2 + U(I) * XT2	SMTH3690
	DET = XN*(MT2*MT4 - MT3*MT3) - MT1*(MT1*MT4 - MT3*MT2)	SMTH3700
	+ MT2*(MT1*MT3 - MT2*MT2)	SMTH3710
	M1 = (MT2*MT4 - MT3*MT3)/DET	SMTH3720
	M2 = -(MT1*MT4 - MT2*MT3)/DET	SMTH3730
	M3 = (MT1*MT3 - MT2*MT2)/DET	SMTH3740
	M4 = (XN*MT4 - MT2*MT2)/DET	SMTH3750
	M5 = -(XN*MT3 - MT1*MT2)/DET	SMTH3760
	M6 = (XN*MT2 - MT1*MT1)/DET	SMTH3770
	C = F0*M1 + FT*M2 + FT2*M3	SMTH3780
	B = F0*M2 + FT*M4 + FT2*M5	SMTH3790
	A = F0*M3 + FT*M5 + FT2*M6	SMTH3800
149	DO 150 I = 1, N	SMTH3810
150	T(I) = T(I) + TS	SMTH3820
C		SMTH3830
C	PRINT, PUNCH AND STORE SMOOTHED VALUE	SMTH3840

C			SMTH3850
	75	TSO=TSP+FLOAT(K-1)*DT	SMTH3860
		IF(SWTCH1) GO TO 929	SMTH3870
		NCT=NCT+1	SMTH3880
		IF(NCT.GT.50) GO TO 35	SMTH3890
	29	WRITE(6,605) ID,TSO,C,B,A	SMTH3900
	605	FORMAT(1X,I10,F14.6,3F16.7,3(2X,1PE14.7))	SMTH3910
	2030	IF(SWTCH2) PUNCH 604,ID,TSO,C,B,A	SMTH3920
	604	FORMAT(I10,F16.6,3F16.7)	SMTH3930
		IF(SWTCH4) GO TO 151	SMTH3940
	929	K2=K2+4	SMTH3950
		STOR(K2)=TSO	SMTH3960
		STOR(K2+1)=C	SMTH3970
		STOR(K2+2)=B	SMTH3980
		STOR(K2+3)=A	SMTH3990
	915	IF(K2.LT.397) GO TO 151	SMTH4000
		WRITE(8) STOR	SMTH4010
		K2=-3	SMTH4020
		IF(SWTCH3) GO TO 151	SMTH4030
		IF(SWTCH8 .OR. DPR.EQ.0.0) CALL MAXMIN(SCP,STOR,2,400,4)	SMTH4040
		IF(.NOT.SWCH14 .AND. (SWTCH8.OR.DSR.EQ.0.0))	SMTH4050
	1	CALL MAXMIN(SSL,STOR,3,400,4)	SMTH4060
C			SMTH4070
C		RESET TS AND START NEXT SMOOTH CALCULATION	SMTH4080
C			SMTH4090
	151	TS=TSR+FLOAT(K)*DT	SMTH4100
		GO TO 61	SMTH4110
C			SMTH4120
C		WRITE PAGE HEADING	SMTH4130
C			SMTH4140
	35	CALL HEADER	SMTH4150
		WRITE(6,7) CIIINLC	SMTH4160
	7	FORMAT(1H0,42H SMOOTH PROGRAM OUTPUT LISTING FOR CHANNEL14 /)	SMTH4170
		WRITE(6,606)	SMTH4180
	606	FORMAT(1H ,21H ID NUMBER TIME,12X,2H C,14X,2H B,14X,2H A /)	SMTH4190
		NCT=1	SMTH4200
		GO TO 29	SMTH4210
C			SMTH4220
C		PLOT SMOOTH COEFFICIENTS B AND C	SMTH4230
C			SMTH4240
	800	IRPOS=0	SMTH4250
		IF(SWCH14) GO TO 874	SMTH4260
		PLCODE=PLCODE-2	SMTH4270
		IRPOS=1	SMTH4280
	874	SCT(1)=TSP	SMTH4290
		SCT(2)=TSO	SMTH4300
	875	IF(IFORM.LT.2) PLCODE=PLCODE+2	SMTH4310
		IF(SWTCH8) GO TO 877	SMTH4320
		NCT=0	SMTH4330
		IF(.NOT.SWTCH1) CALL HEADER	SMTH4340
	876	WRITE(6,614) TMIN,TMAX,PMIN,PMAX,SMIN,SMAX,LT,LP	SMTH4350
	614	FORMAT(1H0,24H PLOT SCALING CARD WAS -2F14.6,4F16.8,2I2)	SMTH4360
C			SMTH4370
C		COEFFICIENT C	SMTH4380
C			SMTH4390

877	CALL DRAW(IRPOS,1,PLCODE,K,100,4,SWTCH8,STOR,SCT,SCP,	SMTH4400
	1 XLT,TMIN,DTM,XLP,PMIN,DPR,	SMTH4410
	2 HEAD,20H COEFFICIENT C)	SMTH4420
	IF(SWCH14) GO TO 1802	SMTH4430
C		SMTH4440
C	COEFFICIENT B	SMTH4450
C		SMTH4460
	CALL DRAW(-2,2,2,K,100,4,SWTCH8,STOR,SCT,SSL,	SMTH4470
	1 XLT,TMIN,DTM,XLP,SMIN,DSR,	SMTH4480
	2 HEAD,20H COEFFICIENT B)	SMTH4490
	1802 IF(IPASNU.LT.2) GO TO 1924	SMTH4500
C		SMTH4510
	CALL SYMBLJ(-0.3,XLP -0.875,0.14,4HPASS,90.0,4)	SMTH4520
	CALL NUMBERI(-0.3,XLP -0.250,0.14,FLOAT(IPASNG),90.0,-1)	SMTH4530
C		SMTH4540
1924	CALL ETIMX(ITM,IPLTM,RPLTS)	SMTH4550
	WRITE(6,609) ICALM,RCALS,IBLANK,IPLTM,RPLTS	SMTH4560
	GO TO 842	SMTH4570
C		SMTH4580
	END	SMTH4590

C	FORTTRAN PROCESSING SUBROUTINE PROGRAM REACTIVITY.	REAC0000
C		REAC0010
	SUBROUTINE REACT(K,D,FRCODE)	REAC0020
C		REAC0030
	COMMON DATA(2021),LOM,IFINC	REAC0040
	DIMENSION XL(50),T(50),A(50),XK1(50),XK2(50),XK3(50),E(50),	REAC0050
1	W(50),HEAD(14),STOR(400),BUFF(600),SCT(2),SCP(2),SCR(2),SCE(2)	REAC0060
	EQUIVALENCE (DATA(1),XL),(DATA(51),T),(DATA(101),A),(DATA(151),	REAC0070
1	XK1),(DATA(201),XK2),(DATA(251),XK3),(DATA(301),E),(DATA(351),W),	REAC0080
2	(DATA(401),STOR),(DATA(801),BUFF),(DATA(2001),HEAD)	REAC0090
	INTEGER PCODE,PLCODE,CHNLNO,PLOT,RPLOT,ELOT,PLCODE,FRCODE	REAC0100
	LOGICAL SWTCH1,SWTCH2,SWTCH3,SWTCH4,SWTCH5,SWTCH6,SWTCH7	REAC0110
C		REAC0120
C	READ CONTROL CARDS	REAC0130
C		REAC0140
	CALL TIMX(ITM)	REAC0150
101	READ(5,1)HEAD	REAC0160
1	FORMAT(13A6,1A2)	REAC0170
	READ(5,2) XLOB,AL,N,ICODE,PCODE,IECODE,PLOT,RPLOT,ELOT,ISCAL,	REAC0180
1	ISAME,XE,SOURCE	REAC0190
2	FORMAT(2E10.8,I2,8I1,2E10.8)	REAC0200
	IF(ISCAL.NE.0)READ(5,4003)TMINP,TMAXP,PMIN,PMAX,LTP,LPP,TMINR,	REAC0210
1	TMAXR,RMIN,RMAX,LTR,LRR,TMINE,TMAXE,EMIN,EMAX,LTE,LEE	REAC0220
4003	FORMAT(3(4E5.3,2I2,1X))	REAC0230
102	READ(5,3)(XL(I),I=1,N)	REAC0240
	READ(5,3)(A(I),I=1,N)	REAC0250
	IF(ICODE.NE.0) READ(5,3) (W(I),I=1,N)	REAC0260
3	FORMAT(8E10.8)	REAC0270
	IF(K.EQ.0) RETURN	REAC0280
C		REAC0290
C	READ IN FIRST DATA RECORD AND WRITE HEADING	REAC0300
C		REAC0310
	REWIND 8	REAC0320
	READ(8)ID,CHNLNO	REAC0330
	CALL HEADER	REAC0340
	WRITE(6,6) HEAD,XLOB,AL,N,ICODE,PCODE,IECODE,PLOT,RPLOT,ELOT,	REAC0350
1	ISCAL,ISAME,XE,SOURCE	REAC0360
6	FORMAT(1H0,19H REACTIVITY PROGRAM,61X,15H DG P L I P R E S /	REAC0370
1	81X,15H ER C I N W T N C / 81X,15H LO S T A / 1X,13A6,1A2,	REAC0380
2	15H AU C T P P P L / 81X,15H Y P O N E L L E / 25X,18H LAMBDA / 3	REAC0390
	BETA BAR,5X,33H INITIAL AVERAGE RECIPR. PERIOD ,42H P S N G N I T T	REAC0400
4	INITIAL ENERGY SOURCE // 19H CONTROL CARD WAS-F22.8,F30.8,	REAC0410
5	I13,4I2,2I1,I2,I1,F15.8,F16.8)	REAC0420
C		REAC0430
C	SET LOGICAL SWITCHES AND INTERNAL CONSTANTS	REAC0440
C		REAC0450
	SWTCH1=PCODE.EQ.3	REAC0460
	SWTCH2=PCODE.EQ.1	REAC0470
	SWTCH3=PLOT+RPLOT+ELOT.EQ.0	REAC0480
	SWTCH5=K.LT.0	REAC0490
	SWTCH4=SWTCH3 .AND. (SWTCH5.OR.FRCODE.EQ.0)	REAC0500
	SWTCH6=ISCAL.EQ.0	REAC0510
	SWTCH7=SOURCE.NE.0.0	REAC0520
	IBLANK=-17997958192	REAC0530
	IAXIS=0	REAC0540

	SCP(1)=1.0E+30	REAC055C
	SCP(2)=-1.0E+30	REAC0560
	SCR(1)=1.0E+30	REAC0570
	SCR(2)=-1.0E+30	REAC0580
	XLTP=10.0	REAC0590
	XLTR=10.0	REAC0600
	XLTE=10.0	REAC0610
	XLPP=7.0	REAC0620
	XLRR=7.0	REAC0630
	XLEE=7.0	REAC0640
	IF(SWICH4) GO TO 4020	REAC0650
	REWIND 4	REAC0660
	WRITE(4) ID,CHNLNO,D,K	REAC0670
4020	IF(SWICH5) K=-K	REAC0680
	IF(SWICH2) PUNCH 1,HEAD	REAC0690
	IF(SWICH6) GO TO 4021	REAC0700
C		REAC0710
C	COMPUTE PLOT PARAMETERS	REAC0720
C		REAC0730
	IF(LTP.NE.0) XLTP=LTP	REAC0740
	IF(LTR.NE.0) XLTR=LTR	REAC0750
	IF(LTE.NE.0) XLTE=LTE	REAC0760
	IF(ISAME.EQ.0) GO TO 4007	REAC0770
	XLTP=AMAX1(XLTP,XLTR,XLTE)	REAC0780
	XLTR=XLTP	REAC0790
	XLTE=XLTP	REAC0800
	TMAXP=AMAX1(TMAXP,TMAXR,TMAXE)	REAC0810
	TMAXR=TMAXP	REAC0820
	TMAXE=TMAXP	REAC0830
	TMINP=AMIN1(TMINP,TMINR,TMINE)	REAC0840
	TMINR=TMINP	REAC0850
	TMINE=TMINP	REAC0860
4007	IF(LPP.NE.0) XLPP=LPP	REAC0870
	IF(LRR.NE.0) XLRR=LRR	REAC0880
	IF(LEE.NE.0) XLEE=LEE	REAC0890
	DTMP=(TMAXP-TMINP)/XLTP	REAC0900
	DTMR=(TMAXR-TMINR)/XLTR	REAC0910
	DTME=(TMAXE-TMINE)/XLTE	REAC0920
	DPR=(PMAX-PMIN)/XLPP	REAC0930
	DRT=(RMAX-RMIN)/XLRR	REAC0940
	DEX=(EMAX-EMIN)/XLEE	REAC0950
	WRITE(6,4008)TMINP,TMAXP,PMIN,PMAX,LTP,LPP,TMINR,TMAXR,RMIN,RMAX,	REAC0960
	1 LTR,LRR,TMINE,TMAXE,EMIN,EMAX,LTE,LEE	REAC0970
4008	FORMAT(1H0,6X,29H SCALE FACTORS FOR POWER PLCT,12X,34H SCALE FACT	REAC0980
	1ORS FOR REACTIVITY PLOT ,10X,30H SCALE FACTORS FOR ENERGY PLOT //	REAC0990
	2 3(43H T MIN T MAX MIN MAX X Y) //	REAC1000
	3 1X,1P3(4E9.2,2I3,1X))	REAC1010
C		REAC1020
C	WRITE CONTROL CARDS	REAC1030
C		REAC1040
4021	WRITE(6,612)	REAC1050
612	FORMAT(1H / 59X,9H LAMBDA'S /)	REAC1060
	WRITE(6 ,8)(XL(I),I=1,N)	REAC1070
8	FORMAT(1H ,8F16.12)	REAC1080
	WRITE(6,613)	REAC1090

613	FORMAT(1H / 59X,9H F'S /)	REAC1100
	WRITE(6,8)(A(I),I=1,N)	REAC1110
	IF(ICODE.NE.0) WRITE(6,614)	REAC1120
614	FORMAT(1H / 59X,9H W'S /)	REAC1130
	IF(ICODE.NE.0) WRITE(6,8)(W(I),I=1,N)	REAC1140
	IF(SWTCH1) GO TO 1234	REAC1150
1233	CALL HEADER	REAC1160
	WRITE(6,611) CHNLNO	REAC1170
	WRITE(6,703)	REAC1180
C		REAC1190
C	PRELIMINARY CALCULATIONS	REAC1200
C		REAC1210
1234	DO 120 I=1,N	REAC1220
	T(I)=XL(I)*D	REAC1230
	SUM=T(I)	REAC1240
	SUM1=1(I)	REAC1250
	TEMP=T(I)	REAC1260
	Z=1.0	REAC1270
11	Z=Z+1.0	REAC1280
	TEMP=TEMP*T(I)/Z	REAC1290
	SUM=SUM-TEMP	REAC1300
	Z=Z+1.0	REAC1310
	TEMP=TEMP*T(I)/Z	REAC1320
	SUM=SUM+TEMP	REAC1330
	IF(SUM - SUM1 - 0.00001) 20, 20, 10	REAC1340
10	SUM1=SUM	REAC1350
	GO TO 11	REAC1360
20	XK3(I)=SUM	REAC1370
	TEMP=-0.5*T(I)*T(I)	REAC1380
	SUM1=TEMP	REAC1390
	SUM=TEMP	REAC1400
	Z=2.0	REAC1410
30	Z=Z+1.0	REAC1420
	TEMP=TEMP*T(I)*(Z-1.0)/(Z*Z-2.0*Z)	REAC1430
	SUM=SUM-TEMP	REAC1440
	Z=Z+1.0	REAC1450
	TEMP=TEMP*T(I)*(Z-1.0)/(Z*Z-2.0*Z)	REAC1460
	SUM=SUM+TEMP	REAC1470
	IF (SUM - SUM1 + 0.00001) 40, 50, 50	REAC1480
40	SUM1=SUM	REAC1490
	GO TO 30	REAC1500
50	XK2(I)=SUM/XL(I)	REAC1510
	TEMP=-T(I)*T(I)*T(I)/3.0	REAC1520
	SUM=TEMP	REAC1530
	SUM1=TEMP	REAC1540
	Z=2.0	REAC1550
60	Z=Z+1.0	REAC1560
	TEMP=TEMP*T(I)*Z/(Z*Z-Z-2.0)	REAC1570
	SUM=SUM-TEMP	REAC1580
	Z=Z+1.0	REAC1590
	TEMP=TEMP*T(I)*Z/(Z*Z-Z-2.0)	REAC1600
	SUM=SUM+TEMP	REAC1610
	IF (SUM - SUM1 + 0.00001) 70, 80, 80	REAC1620
70	SUM1=SUM	REAC1630
	GO TO 60	REAC1640

80	XK1(I)=-SUM/(XL(I)*XL(I))	REAC1650
120	CONTINUE	REAC1660
C		REAC1670
C	FINAL CALCULATIONS FOR FIRST OUTPUT POINT	REAC1680
C		REAC1690
	READ(8) STOR	REAC1700
	TIME=STOR(1)	REAC1710
	C=STOR(2)	REAC1720
	B=STOR(3)	REAC1730
	XA=STOR(4)	REAC1740
	CLIN=EXP(C)	REAC1750
	SUM = 0.0	REAC1760
	DO 200 I=1,N	REAC1770
	TEMP=A(I)/(XL(I)+AL)	REAC1780
	SUM=SUM+TEMP	REAC1790
200	CONTINUE	REAC1800
	DOLTO=AL*(XLOB+SUM)	REAC1810
	IF(ICODE.EQ.0 .AND. AL.NE.0.0) XE=CLIN/AL	REAC1820
	DOLTC=0.0	REAC1830
	BTO=0.0	REAC1840
	NCT=1	REAC1850
C		REAC1860
C	PRINT FIRST OUTPUT POINT	REAC1870
C		REAC1880
	IF(PCODE.NE.3) WRITE(6,5) ID,TIME,CLIN,DOLTO,DOLTC,XE,BTO	REAC1890
	IF(PCODE.EQ.1) PUNCH 600,ID,TIME,CLIN,DOLTO,DOLTC,XE,BTO	REAC1900
	IF(SWCH4) GO TO 4323	REAC1910
C		REAC1920
C	STORE FIRST OUTPUT POINT	REAC1930
C		REAC1940
	BUFF(1)=TIME	REAC1950
	BUFE(2)=CLIN	REAC1960
	BUFF(3)=DOLTO	REAC1970
	BUFF(4)=DOLTC	REAC1980
	BUFF(5)=XE	REAC1990
	BUFF(6)=BTO	REAC2000
	SCT(1)=TIME	REAC2010
	SCE(1)=XE	REAC2020
	K3=1	REAC2030
C		REAC2040
C	CALCULATE W'S AND E'S	REAC2050
C		REAC2060
4323	IF(ICODE.NE.0) GO TO 4322	REAC2070
	DO 4324 I=1,N	REAC2080
4324	W(I)=XL(I)*CLIN/(XL(I)+AL)	REAC2090
4322	DO 90 I=1,N	REAC2100
90	E(I)=EXP(-T(I))	REAC2110
	K2=1	REAC2120
C		REAC2130
C	MAIN LOOP	REAC2140
C		REAC2150
	DO 100 M=2,K	REAC2160
C		REAC2170
C	LOCATE DATA NEEDED	REAC2180
C		REAC2190

	K2=K2+4	REAC2200
	IF(K2.LT.400) GO TO 3090	REAC2210
	READ(8) STOR	REAC2220
	K2=1	REAC2230
3090	TIME=STOR(K2)	REAC2240
	C=STOR(K2+1)	REAC2250
	B=STOR(K2+2)	REAC2260
	XA=STOR(K2+3)	REAC2270
C		REAC2280
C	FINAL CALCULATIONS	REAC2290
C		REAC2300
500	CLIN=EXP(C)	REAC2310
	BLIN=B*CLIN	REAC2320
	ALIN=CLIN*(XA+0.5*B*B)	REAC2330
	XE=((0.333333333*ALIN*D-0.5*BLIN)*D+CLIN)*D+XE	REAC2340
	SUM=0.0	REAC2350
	DO 110 I=1,N	REAC2360
	W(I)=W(I)*E(I)+ALIN*XK1(I)+BLIN*XK2(I)+CLIN*XK3(I)	REAC2370
110	SUM=SUM+W(I)*A(I)	REAC2380
	IF(SWICH7) B=B-SOURCE/CLIN	REAC2390
	DOLS=1.0+(XLOB*B-SUM/CLIN)	REAC2400
	DOLC=DOLS-DOLTO	REAC2410
	BT=DOLC/XE	REAC2420
	IF(SWICH1) GO TO 925	REAC2430
C		REAC2440
C	PRINT OUTPUT VALUES	REAC2450
C		REAC2460
	NCT=NCT+1	REAC2470
	IF(NCT-5)25,26,26	REAC2480
25	WRITE(6,5)ID,TIME,CLIN,DOLS,DOLC,XE,BT	REAC2490
5	FORMAT(2X,I10,F14.6,F16.4,2F16.7,F16.6,F16.10)	REAC2500
	IF(SWICH2) PUNCH 600,ID,TIME,CLIN,DOLS,DOLC,XE,BT	REAC2510
600	FORMAT(I10,F10.6,F12.4,2F12.6,F12.4,F12.8)	REAC2520
	IF(SWICH4) GO TO 100	REAC2530
C		REAC2540
C	STORE OUTPUT VALUES	REAC2550
C		REAC2560
925	K3=K3+6	REAC2570
	BUFF(K3)=TIME	REAC2580
	BUFF(K3+1)=CLIN	REAC2590
	BUFF(K3+2)=DOLS	REAC2600
	BUFF(K3+3)=DOLC	REAC2610
	BUFF(K3+4)=XE	REAC2620
	BUFF(K3+5)=BT	REAC2630
	IF(K3.LT.595) GO TO 100	REAC2640
	WRITE(4) BUFF	REAC2650
	K3=-5	REAC2660
C		REAC2670
C	SCALE DATA POINTS IN ARRAY 'BUFF'	REAC2680
C		REAC2690
	IF(SWICH3) GO TO 100	REAC2700
	IF((PLOT.NE.0).AND.(SWICH6.OR.(DPR.EQ.0.0)))	REAC2710
1	CALL MAXMIN(SCP,BUFF,2,600,6)	REAC2720
	IF((RLOT.NE.0).AND.(SWICH6.OR.(DRT.EQ.0.0)))	REAC2730
1	CALL MAXMIN(SCR,BUFF,3,600,6)	REAC2740

	GO TO 100	REAC2750
C		REAC2760
C	WRITE PAGE HEADING	REAC2770
C		REAC2780
	26 CALL HEADER	REAC2790
	WRITE(6,611) CHNLNO	REAC2800
611	FORMAT(1H0,46H REACTIVITY PROGRAM OUTPUT LISTING FOR CHANNEL I4 /)	REAC2810
702	WRITE(6,703)	REAC2820
703	FORMAT(1X,11H RECORD NO.,4X,5H TIME12X,6H POWER,9X,26H REACTIVITY	REAC2830
	1 COMP. REACT.,6X,7H ENERGY,8X,5H B(T) /)	REAC2840
	NCT=1	REAC2850
	GO TO 25	REAC2860
100	CONTINUE	REAC2870
C		REAC2880
C	END OF CALCULATIONS	REAC2890
C		REAC2900
	IF(.NOT.SWTC4) WRITE(4) BUFF	REAC2910
	CALL ETIMX(ITM,ICALM,RCALS)	REAC2920
	IF(.NOT.SWTC3) GO TO 7000	REAC2930
	WRITE(6,615) ICALM,RCALS	REAC2940
615	FORMAT(1H0,27H CALCULATIONS REQUIRED 14,5H MIN F4.1,4H SECA1,	REAC2950
	1 2OHAND PLOT(S) REQUIREDI3,5H MIN F4.1,4H SEC)	REAC2960
	GO TO 3000	REAC2970
C		REAC2980
C	PLOT SECTION	REAC2990
C		REAC3000
7000	SCT(2)=TIME	REAC3010
	IF(PPLOT+RPLOT.EQ.0) GO TO 7005	REAC3020
	IF(PPLOT.EQ.0) GO TO 7002	REAC3030
C		REAC3040
C	PLOT POWER	REAC3050
C		REAC3060
	IF(ISAME.NE.0) IAXIS=IAXIS+1	REAC3070
	CALL DRAW(IAXIS,1,PPLOT,K,100,6,SWTC6,BUFF,SCT,SCP,	REAC3080
	1 XLTP,TMINP,DIMP,XLPP,PMIN,DPR,	REAC3090
	2 HEAD,20HREACTOR POWER (MW))	REAC3100
	IF(RPLOT.EQ.0) GO TO 7003	REAC3110
C		REAC3120
C	PLOT REACTIVITY	REAC3130
C		REAC3140
7002	IF(ISAME.NE.0) IAXIS=IAXIS+1	REAC3150
	IF(EPLOT.EQ.0) IAXIS=-IAXIS	REAC3160
	CALL DRAW(IAXIS,2,RPLOT,K,100,6,SWTC6,BUFF,SCT,SCR,	REAC3170
	1 XLTR,TMINR,DTMR,XLRR,RMIN,DRT,	REAC3180
	2 HEAD,20HREACTIVITY (DOLLARS))	REAC3190
7003	IF(EPLOT.EQ.0) GO TO 7006	REAC3200
C		REAC3210
C	PLOT ENERGY	REAC3220
C		REAC3230
7005	SCE(2)=XF	REAC3240
	IF(ISAME.NE.0) IAXIS=-IAXIS-1	REAC3250
	CALL DRAW(IAXIS,4,EPLOT,K,100,6,SWTC6,BUFF,SCT,SCE,	REAC3260
	1 XLTE,TIME,DTME,XLEE,EMIN,DEX,	REAC3270
	2 HEAD,20H ENERGY (MW-SEC))	REAC3280
C		REAC3290

.7006	CALL ETIMX(ITM,IPLTM,RPLTS)	REAC3300
	WRITE(6,615) ICALM,RCALS,IBLANK,IPLTM,RPLTS	REAC3310
C		REAC3320
3000	IF(SWTCH5) K=0	REAC3330
	RETURN	REAC3340
C		REAC3350
	END	REAC3360

C	FORTRAN SUBROUTINE WHICH CONTROLS SPORT PLOTS.	DRAW0000
C		DRAW0010
C	SUBROUTINE DRAW(IK,JX,PLOT,K,NPR,ISKIP,SWTCH6,ARAY,SCT,SCP,	DRAW0020
	1 XLTP,TMINP,DTMP,XLPP,PMIN,DPR,	DRAW0030
	2 HEAD,LABEL)	DRAW0040
C		DRAW0050
	COMMON DATA(2021),LJM,IFINC,IPGNO,IHED(14),DATE(2)	DRAW0060
	DIMENSION SCT(2),SCP(2),ARAY(2),BUFF(600),STOR(400),S2T(2),	DRAW0070
	1 HEAD(14),LABEL(4),QJAN(2)	DRAW0080
	EQHIVAI FNCE (DATA(1401),BUFF,STOR),(IFINC,SMALL1)	DRAW0090
	LOGICAL SWTCH1,SWTCH2,SWTCH3,SWTCH4,SWTCH5,SWTCH6,SWTCH7,SWTCH8,	DRAW0100
	1 SWTCH9,SMALL1,SMALL2	DRAW0110
	INTEGER PLOT,CHNLVD	DRAW0120
C		DRAW0130
	SWTCH5=IK.FQ.999	DRAW0140
	SWTCH2=.NOT.SWTCH5 .AND. IK.GT.0	DRAW0150
	I2=IABS(IK)	DRAW0160
	SWTCH3=.NOT.SWTCH5 .AND. I2.GT.1	DRAW0170
	SWTCH4=SWTCH5 .OR. I2.LT.7	DRAW0180
	SWTCH9=SWTCH6 .OR. DPR.EQ.0.0	DRAW0190
	XSTR=FLDAT(1-I2/5)+(XLTP+FLDAT(I2-1)*.5)+FLOAT((I2/5)*(4-I2))*5	DRAW0200
	IF(I2.LT.2 .OR. SWTCH5) XSTR=0.0	DRAW0210
	IF(SWTCH3) GO TO 6995	DRAW0220
		DRAW0230
C	POSITION PLOT	DRAW0240
C		DRAW0250
C	IF(IFINC.GT.0) GO TO 200	DRAW0260
C	IF(.NOT.SMALL1) GO TO 100	DRAW0270
C		DRAW0280
C	SET UP FOR SMALL PLOTTER	DRAW0290
C		DRAW0300
	SMALL2=.TRUE.	DRAW0310
	CALL PLOTS(0.0,-2.0,-3)	DRAW0320
	GO TO 200	DRAW0330
C		DRAW0340
100	SMALL2=.FALSE.	DRAW0350
	CALL PLOT(0.0,-2.0,-3)	DRAW0360
200	SWTCH1=SMALL2.OR.XLTP.GT.10.5.OR.XLPP.GT.7.5	DRAW0370
	IFINC=IFINC+1	DRAW0380
	ICOJNT=ICOJNT+1	DRAW0390
	IF(IFINC.GT.1 .AND. ICOJNT.EQ.1) GO TO 7000	DRAW0400
	IF(IFINC.EQ.1) ICOJNT=1	DRAW0410
	XXX=0.0	DRAW0420
	YYY=0.5	DRAW0430
	IF(ICOJNT.EQ.1) GO TO 7000	DRAW0440
	IIE5I=ICOJNT - (ICOJNT-1)/3*3 - 1	DRAW0450
	YYY=10.0	DRAW0460
	IF(IIE5I.NE.0) GO TO 6990	DRAW0470
	XXX=15.0	DRAW0480
	YYY=-20.0	DRAW0490
6990	IF(.NOT.SWTCH1) GO TO 7000	DRAW0500
	XXX=15.0	DRAW0510
	YYY=YYY-FLOAT(IIE5I)*10.0	DRAW0520
7000	CALL PLOT(XXX,YYY,-3)	DRAW0530
C		DRAW0540

C	SCALE DATA AND DRAW AXIS	DRAW0550
C		DRAW0560
6995	IF(<.EQ.0) RETURN	DRAW0570
	K6=</NPR	DRAW0580
	K7=<-K6*NPR	DRAW0590
	K8=<7*ISKIP	DRAW0600
	S2T(1)=SCT(1)	DRAW0610
	S2T(2)=SCT(2)	DRAW0620
	IF(.NOT.SWTC9) GO TO 830	DRAW0630
	CALL MAXMIN(SCP,ARRAY,1+JX,K8,ISKIP)	DRAW0640
	IF(PPLOT.LT.3) GO TO 830	DRAW0650
	IF(SCP(1).LT.-88.0 .OR. SCP(2).GT.88.0) GO TO 855	DRAW0660
	SCP(1)=EXP(SCP(1))	DRAW0670
	SCP(2)=EXP(SCP(2))	DRAW0680
830	IF((-1)*PPLOT.LT.0.AND.(SCP(1).GT.0..OR..NOT.SWTC9)) GO TO 835	DRAW0690
	IF(PPLOT.NE.1) GO TO 831	DRAW0700
	PPLDT=2	DRAW0710
	IF(SWTC9) GO TO 831	DRAW0720
	SCP(1)=10.0**(SCP(1))	DRAW0730
	SCP(2)=10.0**(SCP(2))	DRAW0740
831	IF(SWTC9) CALL SCALE(SCP,2,XLPP,PMIN,DPR,1)	DRAW0750
	IF(SWTC4) CALL AXIS(XSTR,0.0,LABEL,20,XLPP,90.0,PMIN,DPR)	DRAW0760
	GO TO 836	DRAW0770
835	IF(SWTC9)CALL LSCALE(SCP,2,XLPP,PMIN,DPR,1)	DRAW0780
	IF(SWTC4)CALL LAXIS(XSTR,0.0,LABEL,20,XLPP,90.0,PMIN,DPR)	DRAW0790
836	IF(ISKIP.EQ.2) GO TO 825	DRAW0800
	IF(ISKIP.EQ.6) GO TO 837	DRAW0810
	REWIND 8	DRAW0820
	READ(8) ID,CHNLNO	DRAW0830
	GO TO 838	DRAW0840
837	REWIND 4	DRAW0850
825	READ(4) ID,CHNLNO	DRAW0860
838	IF(SWTC5) GO TO 870	DRAW0870
	IF(SWTC45 .OR. DTMP.EQ.0.0) CALL SCALE(S2T,2,XLTP,TMINP,DTMP,1)	DRAW0880
	IF(SWTC3) GO TO 839	DRAW0890
	CALL AXIS(0.0,0.0,10HTIME (SEC),10,XLTP,0.0,TMINP,DTMP)	DRAW0900
C		DRAW0910
C	DRAW LINE	DRAW0920
C		DRAW0930
839	JRK=MIN0(NPR*ISKIP,<*ISKIP-1)	DRAW0940
	IPEV=3	DRAW0950
	XLAST=0.0	DRAW0960
	YLAST=0.0	DRAW0970
	SWTC5=.TRUE.	DRAW0980
	SWTC7=.FALSE.	DRAW0990
801	DO 815 I=0,K6	DRAW1000
	IF(ISKIP.EQ.4) READ(8) STOR	DRAW1010
	IF(ISKIP.NE.4) READ(4) BUFF	DRAW1020
	IF(I.LT.K6) GO TO 802	DRAW1030
	IF(<7.EQ.0) GO TO 815	DRAW1040
	JRK=K8	DRAW1050
802	DO 815 J=1,JRK,ISKIP	DRAW1060
	BUFF(J)=(RUFF(J)-TMINP)/DTMP	DRAW1070
804	JJJ=J+JX	DRAW1080
	GO TO(806,807,808,809),PLOT	DRAW1090

808	BUFF(JJJ)=(BUFF(JJJ)*0.43429448-PMIN)/DPR	DRAW1100
	GO TO 810	DRAW1110
809	BUFF(JJJ)=EXP(BUFF(JJJ))	DRAW1120
	GO TO 807	DRAW1130
806	BUFF(JJJ)=ALOG10(BUFF(JJJ))	DRAW1140
807	BUFF(JJJ)=(BUFF(JJJ)-PMIN)/DPR	DRAW1150
810	SWTCH8= BUFF(J).LT.0.0 .OR. BUFF(J).GT.XLTP	DRAW1160
	1 .OR. BUFF(JJJ).LT.0.0 .OR. BUFF(JJJ).GT.XLPP	DRAW1170
	IF(.NOT.SWTCH7 .AND. .NOT.SWTCH8) GO TO 813	DRAW1180
	IF(SWTCH7.AND.SWTCH8) GO TO 814	DRAW1190
C		DRAW1200
C	CURRENT OR PREVIOUS POINT OFF-SCALE	DRAW1210
C		DRAW1220
	GOODX=XLAST	DRAW1230
	GOODY=YLAST	DRAW1240
	BADX=BUFF(J)	DRAW1250
	BADY=BUFF(JJJ)	DRAW1260
	IF(.NOT.SWTCH7) GO TO 811	DRAW1270
	GOODX=BUFF(J)	DRAW1280
	GOODY=BUFF(JJJ)	DRAW1290
	BADX=XLAST	DRAW1300
	BADY=YLAST	DRAW1310
811	XSUB=0.0	DRAW1320
	YSUB=0.0	DRAW1330
	IF(BADY.GT.GOODY) YSUB=XLPP	DRAW1340
	IF(BADX.GT.GOODX) XSUB=XLTP	DRAW1350
	SLOPE=1.0E+10	DRAW1360
	IF(BADX.NE.GOODX) SLOPE=(BADY-GOODY)/(BADX-GOODX)	DRAW1370
	BUFF(JJJ)=GOODY+(XSUB-GOODX)*SLOPE	DRAW1380
	BUFF(J)=GOODX+(YSUB-GOODY)/SLOPE	DRAW1390
	IF(BUFF(JJJ).GT.XLPP) BUFF(JJJ)=XLPP	DRAW1400
	IF(BUFF(JJJ).LT.0.0) BUFF(JJJ)=0.0	DRAW1410
	IF(BUFF(J).GT.XLTP) BUFF(J)=XLTP	DRAW1420
	IF(BUFF(J).LT.0.0) BUFF(J)=0.0	DRAW1430
	CALL PLOT(BUFF(J),BUFF(JJJ),IPEN)	DRAW1440
	IF(SWTCH7) GO TO 812	DRAW1450
	IPEN=3	DRAW1460
	SWTCH5=.TRUE.	DRAW1470
	GO TO 814	DRAW1480
812	IPEN=0	DRAW1490
	SWTCH5=.FALSE.	DRAW1500
813	CALL PLOT(BUFF(J),BUFF(JJJ),IPEN)	DRAW1510
	IF(.NOT.SWTCH5) GO TO 814	DRAW1520
	IPEN=0	DRAW1530
	SWTCH5=.FALSE.	DRAW1540
814	XLAST=BUFF(J)	DRAW1550
	YLAST=BUFF(JJJ)	DRAW1560
	SWTCH7=SWTCH8	DRAW1570
815	CONTINUE	DRAW1580
	IF(SWTCH3) GO TO 7200	DRAW1590
C		DRAW1600
C	DRAW LABELS	DRAW1610
C		DRAW1620
870	CALL SYMBLJ(0.0,XLPP+0.05,AMIN1(0.014*XLTP,0.42),HEAD,0.0,80)	DRAW1630
	CALL BBOD1(ID,QUAN(1),QUAN(2))	DRAW1640

	CALL SYMBLJ(-0.250,-0.46,0.14,QUAN,0.0,12)	DRAW1650
	CALL SYMBLJ(-0.3,0.0,0.14,DATE,90.0,8)	DRAW1660
	IF(CHNLNO.GT.0 .AND. CHNLNO.LT.7) CALL NUMBER(1.250,-0.44,0.14,	DRAW1670
	1 -FLJAT(CHNLNO),0.0,-1)	DRAW1680
7200	IF(.NOT.SWTCH1 .OR. SWTCH2) RETURN	DRAW1690
C		DRAW1700
C	REPOSITION PEN IF THIS PLOT WAS LARGER THAN 10 X 7	DRAW1710
C		DRAW1720
	ICOUNT=0	DRAW1730
	XXX=XLTP+5.0	DRAW1740
	YYY=0.0	DRAW1750
	RETJRN	DRAW1760
C		DRAW1770
C	ERRDR RETURN	DRAW1780
C		DRAW1790
055	WRITE(6,056)	DRAW1800
856	FORMAT(1H021H UNABLE TO SCALE DATA)	DRAW1810
	RETJRN	DRAW1820
C		DRAW1830
	END	DRAW1840

C	FJRTRAN PROCESSING SUBROUTINE PROGRAM FREQUENCY RESPONSE.	FREQ0000
C		FREQ0010
	SUBROUTINE FREQ(TART,ICODE,X,DELTA)	FREQ0020
C		FREQ0030
	COMMON DATA(2021),LJM,IFINC	FREQ0040
	DIMENSION W(100),R(100),P(100),D(100),S(100),A(5),HEAD(14),	FREQ0050
1	X(100),Y(100),Z(100),STOR(400),BUFF(600),STOR2(400),LABELX(3)	FREQ0060
	EQUIVALENCE (DATA(1),W),(DATA(101),R),(DATA(201),P),(DATA(301),D)	FREQ0070
1	,(DATA(401),S),(DATA(501),A),(DATA(506),HEAD),(DATA(520),X),	FREQ0080
2	(DATA(620),Y),(DATA(720),Z),(DATA(820),STOR),(DATA(1220),BUFF,	FREQ0090
3	STOR2)	FREQ0100
	REAL NUM	FREQ0110
	INTEGER PLCODE,TART,CHNLNO,PCODE	FREQ0120
	LOGICAL SWITCH1,SWTCH2,SWTCH3,SWTCH4,SWTCH5,SWTCH6,SWTCH7,SWTCH8	FREQ0130
C		FREQ0140
	CALL TIMX(ITM)	FREQ0150
400	READ(5,13)HEAD	FREQ0160
13	FORMAT(13A6,1A2)	FREQ0170
	READ(5,10) N,I,J,L,PLCODE,PCODE,IWSCPS,ALPHA	FREQ0180
10	FORMAT(I3,6I1,11X,E10.8)	FREQ0190
	READ(5,11)(W(M),M=1,N)	FREQ0200
11	FORMAT(8E10.8)	FREQ0210
	IF(K.LE.0) RETURN	FREQ0220
	IF(N.EQ.0 .OR. I.EQ.0) RETURN	FREQ0230
	K4=1	FREQ0240
	IBLANK=-17997958192	FREQ0250
	SWTCH1=PCODE.NE.0	FREQ0260
	SWTCH2=TART.NE.3	FREQ0270
	SWTCH3=TART.NE.5 .OR. ICODE.NE.5	FREQ0280
	SWTCH4=ALPHA.NE.0.0	FREQ0290
	SWTCH5=L.EQ.4	FREQ0300
	SWTCH6=L.EQ.3	FREQ0310
	SWTCH7=SWTCH5 .OR. SWTCH6	FREQ0320
	SWTCH8=IWSCPS.NE.0	FREQ0330
	IF(.NOT.SWTCH2) GO TO 401	FREQ0340
	REWIND 4	FREQ0350
	READ(4)ID,CHNLNO	FREQ0360
401	CALL HEADER	FREQ0370
	WRITE(6,14) HEAD	FREQ0380
14	FORMAT(1H0,27H FREQUENCY RESPONSE PROGRAM // 1X,13A6,1A2 /)	FREQ0390
	IF(SWTCH1) PUNCH 13,HEAD	FREQ0400
	WRITE(6,16) N,I,J,L,PLCODE,PCODE,IWSCPS,ALPHA	FREQ0410
16	FORMAT(1H ,18H CONTROL CARD WAS-,I3,I2,2I1,3I2,9H ALPHA =F14.8)	FREQ0420
	IF(.NOT.SWTCH8) WRITE(6,18)	FREQ0430
18	FORMAT(1X/ 51X,19H RADIAN FREQUENCIES /)	FREQ0440
	IF(SWTCH8) WRITE(6,4018)	FREQ0450
4018	FORMAT(1X/ 51X,19H FREQUENCIES IN CPS /)	FREQ0460
	WRITE(6,17)(W(M),M=1,N)	FREQ0470
17	FORMAT(1H ,8F16.7)	FREQ0480
	IF(.NOT.SWTCH2 .OR. (.NOT.SWTCH3)) L=2	FREQ0490
	IF(SWTCH7) L=1	FREQ0500
	HALFO=DELTA* .5	FREQ0510
	TD=2.0	FREQ0520
C		FREQ0530
C	READ IN FIRST DATA POINT	FREQ0540

C		FREQ0550
800	IF(SWTCH2) GO TO 802	FREQ0560
801	REWIND 9	FREQ0570
	READ(8) ID, CHNLNO	FREQ0580
	READ(8) STOR	FREQ0590
	IF(SWTCH7) GO TO 1801	FREQ0600
	AD=STOR(I+1)	FREQ0610
	GO TO 703	FREQ0620
1801	REWIND 9	FREQ0630
	READ(9) ND, INTWO, DTOK, KOK	FREQ0640
	READ(9) STOR2	FREQ0650
	IF(KOK.LT.K) K=KOK	FREQ0660
	IF(INT((DELTA-DTOK)*1.0E+7).NE.0) GO TO 2005	FREQ0670
	AD=STOR2(I+1)	FREQ0680
	IF(SWTCH5) AD=AD-STOR(I+1)	FREQ0690
	GO TO 777	FREQ0700
2005	WRITE(6,608)	FREQ0710
608	FORMAT(1H046H DELTA T'S WERE DIFFERENT FOR THE TWO CHANNELS)	FREQ0720
	RETJRN	FREQ0730
902	READ(4) BUFF	FREQ0740
	IF(SWTCH3) GO TO 803	FREQ0750
	AD=BUFF(2)	FREQ0760
	GO TO 703	FREQ0770
803	AD=BUFF(I+1)	FREQ0780
	IF(L.EQ.2) GO TO 703	FREQ0790
777	BD=BUFF(J+1)	FREQ0800
	IF(SWTCH4) BD=BD*EXP(-ALPHA*TO)	FREQ0810
C		FREQ0820
703	IF(SWTCH4) AD=AD*EXP(-ALPHA*TO)	FREQ0830
	CALL TYPE(1H ,1,0)	FREQ0840
	CALL TYPE(36H PROGRAM NOW ENTERS LONG NORMAL LOOP,36,0)	FREQ0850
	GO TO (1,2),L	FREQ0860
1	DD 3 M=1,N	FREQ0870
	IF(SWTCH8) W(M)=W(M)*6.2831853072	FREQ0880
	R(M)=0.	FREQ0890
	D(M)=0.	FREQ0900
	DEN=2.*SIN(W(M)*HALFD)	FREQ0910
	NJM=W(M)*DELTA	FREQ0920
	P(M)=(AD*NUM)/DEN	FREQ0930
3	S(M)=(BD*NUM)/DEN	FREQ0940
	GO TO 20	FREQ0950
2	DD 8 M=1,N	FREQ0960
	IF(SWTCH8) W(M)=W(M)*6.2831853072	FREQ0970
	R(M)=0.	FREQ0980
	S(M)=0.	FREQ0990
	DEN=2.*SIN(W(M)*HALFD)	FREQ1000
	NJM=W(M)*DELTA	FREQ1010
	P(M)=(AD*NUM)/DEN	FREQ1020
8	D(M)=-((W(M)*NUM)/DEN)	FREQ1030
20	DD 19 NL=2,K	FREQ1040
	T1=FLJAT(NL-1)*DELTA	FREQ1050
C		FREQ1060
C	READ IN ANOTHER DATA POINT	FREQ1070
C		FREQ1080
810	IF(SWTCH2) GO TO 812	FREQ1090

811	K4=<4+4	FREQ1100
	IF(<4.LT.400) GO TO 3811	FREQ1110
	READ(8) STOR	FREQ1120
	IF(SWTCH7) READ(9) STOR2	FREQ1130
	K4=1	FREQ1140
3811	II=<4+1	FREQ1150
	IF(SWTCH7) GO TO 1811	FREQ1160
	A1=STOR(II)	FREQ1170
	GO TO 713	FREQ1180
1811	A1=STOR2(II)	FREQ1190
	IF(SWTCH5) A1=A1-STOR(II)	FREQ1200
	GO TO 888	FREQ1210
312	K4=<4+2	FREQ1220
	IF(SWTCH3) K4=K4+4	FREQ1230
	IF(K4.LT.600) GO TO 3812	FREQ1240
	READ(4) BUFF	FREQ1250
	K4=1	FREQ1260
3812	IF(SWTCH3) GO TO 813	FREQ1270
	A1=BUFF(<4+1)	FREQ1280
	GO TO 713	FREQ1290
813	II=<4+1	FREQ1300
	A1=8UFF(II)	FREQ1310
	IF(L.EQ.2) GO TO 713	FREQ1320
888	IJ=<4+J	FREQ1330
	B1=3UFF(IJ)	FREQ1340
	IF(SWTCH4) B1=B1*EXP(-ALP+A*T1)	FREQ1350
C		FREQ1360
713	IF(SWTCH4) A1=A1*EXP(-ALPHA*T1)	FREQ1370
	DIFA=A1-A0	FREQ1380
	DIFB=B1-B0	FREQ1390
	TIME=TD+HALFD	FREQ1400
	GO TO (5,6),L	FREQ1410
5	DO 7 M=1,N	FREQ1420
	AN=A(M)*TIME	FREQ1430
	PART=SIN(AN)	FREQ1440
	PART1=COS(AN)	FREQ1450
	R(M)=R(M)+DIFA*PART	FREQ1460
	P(M)=P(M)+DIFA*PART1	FREQ1470
	D(M)=D(M)+DIFB*PART	FREQ1480
7	S(M)=S(M)+DIFB*PART1	FREQ1490
22	AJ=A1	FREQ1500
	BJ=B1	FREQ1510
	TJ=T1	FREQ1520
	GO TO 19	FREQ1530
6	DO 9 M=1,N	FREQ1540
	AN=A(M)*TIME	FREQ1550
	PART=SIN(AN)	FREQ1560
	PART1=COS(AN)	FREQ1570
	R(M)=R(M)+DIFA*PART	FREQ1580
	P(M)=P(M)+DIFA*PART1	FREQ1590
9	CONTINUE	FREQ1600
	GO TO 22	FREQ1610
19	CONTINUE	FREQ1620
C		FREQ1630
C	PRINT OUT RESULTS	FREQ1640

C.		FREQ1650
	NCT=50	FREQ1660
	IQC= -29809118256	FREQ1670
	IQM= -5113056304	FREQ1680
	DD 41 M=1,N	FREQ1690
	DEN = D(M)*D(M) + S(M)*S(M)	FREQ1700
	REA = (R(M)*D(M)+P(M)*S(M))/DEN	FREQ1710
	ASIN=(D(M)*P(M)-R(M)*S(M))/DEN	FREQ1720
	CALL ANGRAD(REA,ASIN,G,ANG)	FREQ1730
C		FREQ1740
	IF(SWTCH8) W(M)=W(M)*0.159154943.	FREQ1750
	X(M)=ALOG10(W(M))	FREQ1760
C		FREQ1770
	IF(G.EQ.0.0) G=1.0E-30	FREQ1780
	Y(M)=20.0*ALOG10(G)	FREQ1790
	Z(M)-ANG=57.2957795-360.0	FREQ1800
		FREQ1810
C		FREQ1820
	NCT=NCT+1	FREQ1830
	IF(NCT.GT.45) GO TO 39	FREQ1840
40	WRITE(6,15) W(M),X(M),REA,ASIN,G,Z(M),Y(M)	FREQ1850
15	FORMAT(3X,F14.4,3X,F7.3,3(3X,1PE14.7),3X,OPF14.8,3X,OPF14.7)	FREQ1860
	IF(SWTCH1)PUNCH 604, ID,W(M),REA,ASIN,Z(M),Y(M)	FREQ1870
604	FORMAT(I10,F14.4,1P2E14.7,OPF14.8,OPF14.7)	FREQ1880
	GO TO 41	FREQ1890
C		FREQ1900
C	WRITE PAGE HEADING	FREQ1910
C		FREQ1920
39	CALL HEADER	FREQ1930
	IF(SWTCH7) GO TO 3039	FREQ1940
	IF(L.EQ.1) WRITE(6,500) ID,CHNLNO,I,IOC,J	FREQ1950
600	FORMAT(1H0,11H RECORD NO I10,9H CHANNEL I3,5X,20H NUMERATOR WAS	FREQ1960
	1WORD12,A1,21H DENOMINATOR WAS WORD12)	FREQ1970
	IF(L.EQ.2) WRITE(6,600) ID,CHNLNO,I	FREQ1980
	GO TO 3040	FREQ1990
C		FREQ2000
3039	IF(SWTCH5) WRITE(6,605) NO,INTWO,IQM,ID,CHNLNO	FREQ2010
	IF(SWTCH6) WRITE(6,605) NO,INTWO	FREQ2020
505	FORMAT(1H0,46H NUMERATOR WAS SMOOTHED DATA FROM RECORD NO I10,	FREQ2030
	1 9H CHANNEL I3,1X,A1,34HINUS SMOOTHED DATA FROM RECORD NO I10,9H	FREQ2040
	2CHANNEL I3)	FREQ2050
	WRITE(6,606) ID,CHNLNO	FREQ2060
606	FORMAT(1X/47H DENOMINATOR WAS SMOOTHED DATA FROM RECORD NO I10,	FREQ2070
	1 9H CHANNEL I3)	FREQ2080
C		FREQ2090
3040	IF(SWTCH8) WRITE(6,3045)	FREQ2100
3045	FORMAT(1H019H FREQUENCIES IN CPS)	FREQ2110
	WRITE(6,601)	FREQ2120
501	FORMAT(15H0 FREQUENCY5X,6H LDG W4X,11H REAL G(IW),5X,12H IMA	FREQ2130
	IG. G(IW),7X,7H MAG. 3,8X,12H PHASE ANGLE,3X,15H 20 LOG(MAG. G) /)	FREQ2140
	NCT=1	FREQ2150
	GO TO 40	FREQ2160
C		FREQ2170
41	CONTINUE	FREQ2180
C		FREQ2190
	CALL ETIMX(ITM,ICALM,RCALS)	

	IF(PLCODE.GT.0) GO TO 7000	FREQ2200
	WRITE(6,502) ICALM,RCALS	FREQ2210
602	FORMAT(1H0,27H CALCULATIONS REQUIRED 14,5H MIN F4.1,4H SECA1,	FREQ2220
	1 20H AND PLOT(S) REQUIRED I3,5H MIN F4.1,4H SEC)	FREQ2230
	RETJRN	FREQ2240
C		FREQ2250
C	PLOT SECTION	FREQ2260
C		FREQ2270
7000	ITPORT=4	FREQ2280
	IF(SWTC8) ITPORT=6	FREQ2290
	CALL LSCALE(W,N,10.0,WMIN,DW,1)	FREQ2300
C		FREQ2310
C	MAGNITUDE PLOT	FREQ2320
C		FREQ2330
	LABELX(1)= -17559804468	FREQ2340
	LABELX(2)= 23174548505	FREQ2350
	LABELX(3)= -6179159216	FREQ2360
	IF(SWTC8) GO TO 7002	FREQ2370
	LABELX(1)= -17872275025	FREQ2380
	LABELX(2)= -6179951976	FREQ2390
	LABELX(3)= -21836938800	FREQ2400
7002	CALL SCALE(Y,N,7.0,YMIN,DY,1)	FREQ2410
C		FREQ2420
	CALL DRAW(999,1,2,N,100,ITPORT,.FALSE.,Y,R,P,	FREQ2430
	1 10.0,WMIN,DW,7.0,YMIN,DY,	FREQ2440
	2 HEAD,20H MAGNITUDE (DECIBELS))	FREQ2450
	DD 503 M=1,N	FREQ2460
503	CALL SYMBLJ(W(M)-0.03125,Y(M)-0.035,0.07,1H0,0.0,1)	FREQ2470
	CALL LAXIS(0.0,0.0,LABELX,18,10.0,0.0,WMIN,DW)	FREQ2480
	IF(PLCODE.EQ.1) GO TO 2505	FREQ2490
C		FREQ2500
C	PHASE PLOT	FREQ2510
C		FREQ2520
7003	CALL SCALE(Z,N,7.0,ZMIN,DZ,1)	FREQ2530
C		FREQ2540
	CALL DRAW(999,1,2,N,100,ITPORT,.FALSE.,Z,R,P,	FREQ2550
	1 10.0,WMIN,DW,7.0,ZMIN,DZ,	FREQ2560
	2 HEAD,20H PHASE (DEGREES))	FREQ2570
	DD 505 M=1,N	FREQ2580
505	CALL SYMBLJ(W(M)-0.03125,Z(M)-0.035,0.07,1HX,0.0,1)	FREQ2590
	CALL LAXIS(0.0,0.0,LABELX,18,10.0,0.0,WMIN,DW)	FREQ2600
C		FREQ2610
2505	CALL ETIMX(ITM,IPLTM,RPLTS)	FREQ2620
	WRITE(6,602) ICALM,RCALS,IBLANK,IPLTM,RPLTS	FREQ2630
	RETURN	FREQ2640
C		FREQ2650
	END	FREQ2660

C	FORTRAN SUBROUTINE WHICH READS CARD INPUT DIRECTLY INTO	INPT0000
C	PROCESSING PROGRAMS REACTIVITY AND FREQUENCY RESPONSE.	INPT0010
C		INPT0020
C	SUBROUTINE INPUT(PART,ICODE,K,DT,IPNLST)	INPT0030
C		INPT0040
	COMMON DATA(2021)	INPT0050
	DIMENSION A4(4),B4(4),A6(6),B6(6),FMT(14),STOR(400),BUFF(600)	INPT0060
	EQUIVALENCE (DATA(1),A4,A6),(DATA(7),STOR),(DATA(407),BUFF)	INPT0070
	INTEGER PART,CHNLNO	INPT0080
	LOGICAL SWTCH1,SWTCH2	INPT0090
C		INPT0100
	CALL TIMX(ITM)	INPT0110
	READ(5,901) ID,IDL,DT	INPT0120
901	FORMAT(I9,A1,E10.5)	INPT0130
	CALL IN650(ID,IDL)	INPT0140
925	WRITE(6,13)ID,DT	INPT0150
13	FORMAT(IH0,I6H INPUT CARD WAS I10,F13.6)	INPT0160
	SWTCH1=IPNLST.EQ.0	INPT0170
	IF(SWTCH1) WRITE(6,813)	INPT0180
813	FORMAT(IH0,I6H LISTING DELETED)	INPT0190
C		INPT0200
	KX=0	INPT0210
	SWTCH2=-FALSE.	INPT0220
	INM=0	INPT0230
	CHNLNO=1	INPT0240
	IF(SWTCH1) GO TO 912	INPT0250
	CALL HEADER	INPT0260
	WRITE(6,913) ID	INPT0270
913	FORMAT(IH0,45X,29H DATA READ IN RECORD NUMBER I10 /)	INPT0280
912	PART=PART-3	INPT0290
	GO TO(14,16),PART	INPT0300
14	REWIND 8	INPT0310
	WRITE(8)ID,CHNLNO	INPT0320
	KS=-3	INPT0330
	GO TO 18	INPT0340
16	REWIND 4	INPT0350
	WRITE(4)ID,CHNLNO	INPT0360
	KS=-5	INPT0370
18	IF(ICODE.EQ.0) ICODE=1	INPT0380
	IF(ICODE.NE.4) GO TO 20	INPT0390
	READ(5,9)NOCHNL,FMT	INPT0400
9	FORMAT(I1,13A6,1A1)	INPT0410
	DO 19 I=1,6	INPT0420
19	A6(I)=0.0	INPT0430
C		INPT0440
C	READ DATA CARDS	INPT0450
C		INPT0460
20	GO TO(100,200,300,400),ICODE	INPT0470
100	GO TO(101,102),PART	INPT0480
101	READ(5,2)ND,A4	INPT0490
2	FORMAT(I10,4E16.9)	INPT0500
	GO TO 600	INPT0510
102	READ(5,3)ND,A6	INPT0520
3	FORMAT(I10,E10.8,5E12.9)	INPT0530
	GO TO 600	INPT0540

200	GO TO (201,202),PART	INPT0550
201	READ(5,4)ND,(A4(I),B4(I),I=1,4)	INPT0560
4	FORMAT(I10,4(F8.8,A2))	INPT0570
	GO TO 344	INPT0580
202	READ(5,5)ND,(A6(I),B6(I),I=1,6)	INPT0590
5	FORMAT(I10,6(F8.8,A2))	INPT0600
203	GO TO 346	INPT0610
300	GO TO(301,302),PART	INPT0620
301	READ(5,6)ND,NDL,(A4(I),B4(I),I=1,4)	INPT0630
6	FORMAT(I9,A1,6(F8.8,A2))	INPT0640
	GO TO 344	INPT0650
302	READ(5,6)ND,NDL,(A6(I),B6(I),I=1,6)	INPT0660
346	CALL DAT650(A6,B6,6)	INPT0670
	GO TO 345	INPT0680
344	CALL DAT650(A4,B4,4)	INPT0690
345	CALL ID650(ND,NDL)	INPT0700
	GO TO 600	INPT0710
400	GO TO(401,402),PART	INPT0720
401	READ(5,FMT)ND,A4(I),(A4(I+1),I=1,NOCHNL)	INPT0730
	GO TO 600	INPT0740
402	READ(5,FMT)ND,A6(I),(A6(I+1),I=1,NOCHNL)	INPT0750
		INPT0760
C		INPT0770
600	IF(ND.EQ.0) GO TO 618	INPT0780
601	IF(ND.NE.ID) GO TO 620	INPT0790
C		INPT0800
C	CHECK TIME SEQUENCE OF CURRENT CARD	INPT0810
C		INPT0820
	IF(SWTCH2) GO TO 602	INPT0830
	SWTCH2=.TRUE.	INPT0840
	GO TO 603	INPT0850
602	IF((ABS(A4(1)-OLDT-DT)).GT.(DT*1.0E-01)) GO TO 630	INPT0860
603	OLDT=A4(I)	INPT0870
C		INPT0880
C	STORE AND PRINT INPUT DATA	INPT0890
C		INPT0900
	GO TO(604,606),PART	INPT0910
C		INPT0920
604	KS=KS+4	INPT0930
	STOR(KS)=A4(1)	INPT0940
	STOR(KS+1)=A4(2)	INPT0950
	STOR(KS+2)=A4(3)	INPT0960
	STOR(KS+3)=A4(4)	INPT0970
	IF(KS.LT.397) GO TO 20	INPT0980
	WRITE(8) STOR	INPT0990
	KX=KX+1	INPT1000
	KS=-3	INPT1010
	IF(SWTCH1) GO TO 20	INPT1020
	WRITE(6,914)(STOR(I),STOR(I+1),STOR(I+2),STOR(I+3),STOR(I+200),	INPT1030
1	STOR(I+201),STOR(I+202),STOR(I+203),I=1,197,4)	INPT1040
914	FORMAT(1H,F13.6,3F16.7,F20.6,3F16.7)	INPT1050
	CALL HEADER	INPT1060
	WRITE(6,916)	INPT1070
916	FORMAT(1H0,52X,24H DATA READ IN, CONTINUED / 1)	INPT1080
	GO TO 20	INPT1090
C		

606	KS=KS+6	INPT1100
	BUFF(KS)=A6(1)	INPT1110
	BUFF(KS+1)=A6(2)	INPT1120
	BUFF(KS+2)=A6(3)	INPT1130
	BUFF(KS+3)=A6(4)	INPT1140
	BUFF(KS+4)=A6(5)	INPT1150
	BUFF(KS+5)=A6(6)	INPT1160
	IF(KS.LT.595) GO TO 20	INPT1170
	WRITE(4) BUFF	INPT1180
	KX=KX+1	INPT1190
	KS=-5	INPT1200
	IF(SWTCH1) GO TO 20	INPT1210
	WRITE(6,915) (BUFF(I),I=1,300)	INPT1220
915	FORMAT(1H ,F19.6,5F21.8)	INPT1230
	CALL HEADER	INPT1240
	WRITE(6,916)	INPT1250
	WRITE(6,915) (BUFF(I),I=301,600)	INPT1260
	CALL HEADER	INPT1270
	WRITE(6,916)	INPT1280
	GO TO 20	INPT1290
C		INPT1300
620	INM=1	INPT1310
	GO TO 618	INPT1320
630	INM=2	INPT1330
C		INPT1340
C	PRINT OUT LAST RECORD	INPT1350
C		INPT1360
618	GO TO(704,706),PART	INPT1370
C		INPT1380
704	IF(KS.LT.397) WRITE(8) STOR	INPT1390
	K=KX+100+(KS+3)/4	INPT1400
	IF(SWTCH1 .OR. KS.EQ.397) GO TO 619	INPT1410
	IF(KS-200)701,701,702	INPT1420
701	WRITE(6,814) (STOR(I),STOR(I+1),STOR(I+2),STOR(I+3),I=1,KS,4)	INPT1430
814	FORMAT(1H ,F13.6,3F16.7)	INPT1440
	GO TO 619	INPT1450
702	WRITE(6,914) (STOR(I-200),STOR(I-199),STOR(I-198),STOR(I-197),	INPT1460
	1 STOR(I),STOR(I+1),STOR(I+2),STOR(I+3),I=201,KS,4)	INPT1470
	WRITE(6,814) (STOR(I-196),STOR(I-195),STOR(I-194),STOR(I-193),	INPT1480
	1 I=KS,393,4)	INPT1490
	GO TO 619	INPT1500
C		INPT1510
706	IF(K4.LT.595) WRITE(4) BUFF	INPT1520
	K=KX+100+(KS+5)/6	INPT1530
	IF(SWTCH1 .OR. KS.EQ.595) GO TO 619	INPT1540
	LST=MIN0(295,KS)	INPT1550
	WRITE(6,915) BUFF(1),BUFF(2),BUFF(3),BUFF(4),BUFF(5),	INPT1560
	1 (BUFF(J+5),J=1,LST)	INPT1570
	IF(KS.LT.301) GO TO 619	INPT1580
	CALL HEADER	INPT1590
	WRITE(6,916)	INPT1600
	WRITE(6,915) BUFF(301),BUFF(302),BUFF(303),BUFF(304),BUFF(305),	INPT1610
	1 (BUFF(J+5),J=301,KS)	INPT1620
619	PART=PART+3	INPT1630
	IF(INM.EQ.0) GO TO 970	INPT1640

C		INPT1650
C	ERROR MESSAGES	INPT1660
C	GO TO (720,730),INM	INPT1670
	720 WRITE(6,10) ND,A4(1)	INPT1680
	10 FORMAT(1H0,17H WRONG ID NUMBER I10,F19.6)	INPT1690
	GO TO 635	INPT1700
	730 WRITE(6,11)ND,A4(1)	INPT1710
	11 FORMAT(1H0,19H CARD OUT OF ORDER I10,F19.6)	INPT1720
	635 READ(5,6)NPM	INPT1730
	IF(NOM.NE.0) GO TO 635	INPT1740
	K=0	INPT1750
	970 CALL ETIMX(ITM,IETM,RETS)	INPT1760
	WRITE(6,975) IETM,RETS	INPT1770
	975 FORMAT(1H0,27H DIRECT DATA INPUT REQUIREDI4,5H MIN F4.1,4H SEC)	INPT1780
	RETURN	INPT1790
C		INPT1800
	END	INPT1810
		INPT1820

M E M O R Y M A P

SYSTEM, INCLUDING IOCS 00000 THRU 12123

FILE BLOCK ORIGIN 12132

NUMBER OF FILES - 8

1.	FTC03.	12132
2.	FTC04.	12155
3.	FTC08.	12200
4.	FTC09.	12223
5.	S.FBIN	12246
6.	S.FBOU	12271
7.	S.FBPP	12314
8.	FTC10.	12337

OBJECT PROGRAM 12362 THRU 5467C

1.	DECK '/FILES'	00000
2.	DECK 'MAIN' *	12362
3.	DECK 'GNTAPE' *	14513
4.	DECK 'SUBCNT' *	21147
5.	DECK 'TREAD' *	21342
6.	DECK 'BACK' *	21365
7.	DECK 'TYPE' *	21403
8.	DECK 'TYPEN' *	21423
9.	DECK 'BBCD1' *	21474
10.	DECK 'HEADER' *	21650
11.	DECK 'TODAY' *	21750
12.	DECK 'ANGRAD' *	21777
13.	DECK 'SPERT1' *	22164
14.	DECK 'DAT650'	22446
15.	DECK 'PLOT' *	22542
16.	DECK 'LINE' *	24003
17.	DECK 'SCAL' *	24054
18.	DECK 'LSCALE' *	24151
19.	DECK 'DXDY' *	24257
20.	DECK 'AXIS' *	24463
21.	DECK 'LCXDY' *	24773
22.	DECK 'LAXIS' *	25030
23.	DECK 'NUMBER' *	25367
24.	DECK 'BCDFL' *	25526
25.	DECK 'SYMBLJ' *	25563
26.	DECK 'TIMX' *	26317
27.	DECK 'ETIMX' *	26327
28.	DECK 'MAXMIN' *	26453
29.	DECK 'ID650' *	26573
30.	DECK 'SCA' *	26620
31.	DECK 'UNLOAD' *	27106
32.	DECK 'SET' *	27242
33.	DECK 'XEM' *	27257
34.	DECK 'SMOOTH' *	27514
35.	DECK 'REACT' *	34302

36.	DECK	'DRAW	' *	40041
37.	DECK	'FREQ	' *	42105
38.	DECK	'INPUT	' *	45222
39.	SUBR	'INSYFB'		00000
40.	SUBR	'OUSYFB'		00000
41.	SUBR	'POSTX	'	47210
42.	SUBR	'PPSYFB'		00000
43.	SUBR	'FPC	'	47327
44.	SUBR	'F03	'	47330
45.	SUBR	'F04	'	47331
46.	SUBR	'F05	'	47332
47.	SUBR	'F06	'	47333
48.	SUBR	'F08	'	47334
49.	SUBR	'F09	'	47335
50.	SUBR	'F10	'	47336
51.	SUBR	'IOS	' *	47337
52.	SUBR	'RWB	'	47636
53.	SUBR	'RWD	'	50264
54.	SUBR	'ACV	' *	51202
55.	SUBR	'ECV	' *	51235
56.	SUBR	'FCV	' *	51401
57.	SUBR	'GCV	'	51733
58.	SUBR	'HCV	'	52032
59.	SUBR	'ICV	' *	52157
60.	SUBR	'LCV	' *	52525
61.	SUBR	'OCV	' *	52576
62.	SUBR	'XCV	'	52704
63.	SUBR	'SLI	'	52732
64.	SUBR	'SLO	'	52755
65.	SUBR	'EFT	'	53000
66.	SUBR	'RWT	'	53017
67.	SUBR	'FPT	'	53036
68.	SUBR	'XIT	'	53320
69.	SUBR	'XP1	'	53322
70.	SUBR	'XP2	'	53430
71.	SUBR	'XP3	'	53542
72.	SUBR	'XPN	'	53633
73.	SUBR	'ATN	'	53741
74.	SUBR	'LOG	'	54155
75.	SUBR	'SCN	'	54341
76.	SUBR	'SCR	'	54573

(* - INSERTIONS OR DELETIONS MADE IN THIS DECK)

INPUT - OUTPUT BUFFERS	64714 THRU 74005
BLANK COMMON ORIGIN	74006
UNUSED CCRE	54671 THRU 64672

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APPENDIX C -- SUPPLEMENTARY PROGRAMS

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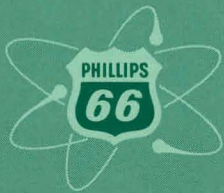
C	FORTRAN ROUTINE TO PUT CARD DATA INTO SPORT TYPE-5 FORMAT.	CDTP0000
C		CDTP0010
C	REQUIRES SUBROUTINES TYPE,BCFX,BCDFL,UNLOAD AND THESE FILE CARDS	CDTP0020
C		CDTP0030
C	\$FILE 'FTC03.',U03,U03,BLOCK=2022,DOUBLE,LRL=2021,RCT=0001	CDTP0040
C	\$ETC EOR=REORX.,EOF=REOFX.,ERR=RERRX.,TYPE3	CDTP0050
C	\$FILE 'FTC04.',U04,U04,BLOCK=2022,DOUBLE,LRL=2021,RCT=0001	CDTP0060
C	\$ETC EOR=REORX.,EOF=REOFX.,ERR=RERRX.,TYPE3	CDTP0070
C		CDTP0080
	DIMENSION STOR(2019),DATA(2000),PMT(14),DUMMY(10)	CDTP0090
	EQUIVALENCE (STOR(15),KOUNT),(STOR(17),ID),(STOR(18),TO),	CDTP0100
	1 (STOR(19),DT),(STOR(20),DATA)	CDTP0110
C		CDTP0120
C	READ CONTROL CARD	CDTP0130
C		CDTP0140
	READ(5,1) MOUNT,IREEL,ND,TSTART,DELTAT	CDTP0150
	1 FORMAT(I2,I6,2X,I10,2E10,8)	CDTP0160
C		CDTP0170
C	IF MOUNT = 1, OPERATOR WILL MOUNT REEL 'IREEL' ON S.SU03.	CDTP0180
C	IF MOUNT = 0, THIS DATA WILL BE FIRST ON THE OUTPUT TAPE.	CDTP0190
C		CDTP0200
C	THIS DATA WILL HAVE IDENTIFICATION NUMBER 'ND'. THE FIRST DATA	CDTP0210
C	VALUE WILL BE AT 'TSTART' AND THE TIME INCREMENT BETWEEN SUC-	CDTP0220
C	CESSIVE DATA VALUES WILL BE ASSUMED TO BE 'DELTAT'.	CDTP0230
C		CDTP0240
C	REWIND 4	CDTP0250
	ICONT=0	CDTP0260
C		CDTP0270
C	MOUNT PREVIOUS DATA TAPE (IF ANY) AND TRANSFER RECORDS TO S.SU04	CDTP0280
C		CDTP0290
	IF(MOUNT.EQ.0) GO TO 5	CDTP0300
	CALL TYPE(1H,1,0)	CDTP0310
	CALL TYPE(18H PLEASE MOUNT REEL,18,0)	CDTP0320
	CALL BCFX(IREEL,IREEL2)	CDTP0330
	CALL TYPE(IREEL2,5,0)	CDTP0340
	CALL TYPE(38H ON S.SU03 AND PRESS START TO CONTINUE,38,1)	CDTP0350
C		CDTP0360
	REWIND 3	CDTP0370
	WRITE(6,2) IREEL	CDTP0380
	2 FORMAT(1H1,40H RECORDS TRANSFERRED TO S.SU04 FROM REEL IS //	CDTP0390
	1 59H FILE INDX IDENTIFICATION NO INITIAL TIME DELTA T//)	CDTP0400
C		CDTP0410
	3 READ(3) STOR	CDTP0420
	IF(ID.EQ.0) GO TO 5	CDTP0430
	KOUNT=ICONT	CDTP0440
	WRITE(4) STOR	CDTP0450
	WRITE(6,4) KOUNT, ID, ID, DT	CDTP0460
	4 FORMAT(1H, I7, I18, F20.6, F14.6)	CDTP0470
	ICONT=ICONT+1	CDTP0480
	GO TO 3	CDTP0490
C		CDTP0500
C	READ IN CARD FORMAT	CDTP0510
C		CDTP0520
	5 READ(5,6) IDATNO,FMT	CDTP0530
	6 FORMAT(I1,13A6,1A1)	CDTP0540

C		CDTP0550
C	A NON-ZERO INTEGER IDENTIFICATION NUMBER MUST PRECEDE THE TIME	CDTP0560
C	AND DATA VALUES ON EACH DATA CARD. IF THERE IS MORE THAN ONE	CDTP0570
C	DATA VALUE PER CARD, 'IDATNO' IN COLUMN ONE MUST BE THE NUMBER	CDTP0580
C	OF THE DATA TO BE USED. TO PICK UP THE SECOND DATA VALUE, ENTER	CDTP0590
C	A TWO IN COLUMN ONE, ETC. THE FORTRAN FORMAT STATEMENT DESCRIB-	CDTP0600
C	ING THE DATA SHOULD BE ENTERED (MINUS THE WORD FORMAT) SOMEWHERE	CDTP0610
C	IN COLUMNS 2-80.	CDTP0620
C	READ THE DATA CARDS	CDTP0630
C		CDTP0640
C	ID=ND	CDTP0650
C	TO=TSTART	CDTP0660
C	DT=DELTAT	CDTP0670
C	7 DO 8 I=1,2000	CDTP0680
C	READ(5,GMT) ND,(DUMMY(J),J=1,IDAINU),DATA(I)	CDTP0690
C	IF(ND.EQ.0) GO TO 10	CDTP0700
C	8 CONTINUE	CDTP0710
C	KOUNT=ICONT	CDTP0720
C	WRITE(4) STOR	CDTP0730
C	WRITE(6,9) KOUNT,ID,TO,DT,DATA	CDTP0740
C	9 FORMAT(1H0,I7,I18,F20.6,F14.6 // 12(1X,1PE10.3))	CDTP0750
C	ICONT=ICONT+1	CDTP0760
C	TO=TO+2000.0*DT	CDTP0770
C	GO TO 7	CDTP0780
C		CDTP0790
C	ZERO OUT THE REMAINDER OF THE LAST RECORD	CDTP0800
C		CDTP0810
C	10 DO 11 L=I,2000	CDTP0820
C	11 DATA(L)=0.0	CDTP0830
C		CDTP0840
C	KOUNT=ICONT	CDTP0850
C	WRITE(4) STOR	CDTP0860
C	WRITE(6,9) KOUNT,ID,TO,DT,(DATA(L-1),L=2,I)	CDTP0870
C	READ(5,1) MOUNT,IREEL,ND,TSTART,DELTAT	CDTP0880
C	IF(ND.NE.0) GO TO 5	CDTP0890
C		CDTP0900
C	EACH DATA DECK SHOULD BE FOLLOWED BY A BLANK CARD.	CDTP0910
C	THE LAST DECK SHOULD BE FOLLOWED BY TWO BLANK CARDS.	CDTP0920
C		CDTP0930
C	WRITE TERMINAL RECORD WITH ZERO ID NUMBER AND CLOSE OUT S.SU04	CDTP0940
C		CDTP0950
C	12 ID=0	CDTP0960
C	KOUNT=ICONT+1	CDTP0970
C	WRITE(4) STOR	CDTP0980
C	WRITE(6,9) KOUNT,ID	CDTP0990
C	END FILE 4	CDTP1000
C	CALL UNLOAD(4)	CDTP1010
C	STOP	CDTP1020
C		CDTP1030
C	END	CDTP1040
C		CDTP1050

C	FORTRAN SUBROUTINE TO READ SMOOTH BINARY OUTPUT TAPES	GULP0000
C		GULP0010
C	IF THE FIRST ARGUMENT IS NON-ZERO, THE DATA TAPE WILL BE CALLED	GULP0020
C	FOR AND THE RECORDS CONTAINING SMOOTHED DATA CORRESPONDING TO	GULP0030
C	IDENTIFICATION NUMBER 'ID' AND CHANNEL NUMBER 'ICHAN' (THE FIRST	GULP0040
C	TWO ARGUMENTS) WILL BE LOCATED ON THE DATA TAPE.	GULP0050
C		GULP0060
C	SUBSEQUENT CALLS WITH ZERO IN THE FIRST ARGUMENT WILL RETURN	GULP0070
C	WITH SUCCESSIVE VALUES OF TIME AND COEFFICIENTS C, B, AND A IN	GULP0080
C	THE LAST FOUR ARGUMENTS.	GULP0090
C		GULP0100
C	REQUIRES SUBROUTINE TYPE AND THE FF FILE CARDS-	GULP0110
C		GULP0120
C	\$FILE 'FTC04.',U04,U04,BLOCK=0401,DOUBLE,LRL=0400,RCT=0001	GULP0130
C	\$ETC EOR=REORX.,EOF=REOFX.,ERR=RERRX.,TYPE3	GULP0140
C		GULP0150
C	SUBROUTINE GULP(ID,ICHAN,T,C,B,A)	GULP0160
C		GULP0170
C	DIMENSION STOR(400)	GULP0180
C	INTEGER CHNLNO	GULP0190
C		GULP0200
C	IF(ID.EQ.0) GO TO 100	GULP0210
C		GULP0220
C	MOUNT DATA TAPE	GULP0230
C		GULP0240
C	CALL TYPE(1H ,1,0)	GULP0250
C	CALL TYPE(26H MOUNT DATA TAPE ON S.SU04,26,0)	GULP0260
C	CALL TYPE(1H ,1,0)	GULP0270
C	CALL TYPE(24H PRESS START TO CONTINUE,24,1)	GULP0280
C		GULP0290
C	FIND RECORD	GULP0300
C		GULP0310
C	REWIND 4	GULP0320
C	2 READ(4) ND,CHNLNO,DT,K	GULP0330
C	IF(ND.EQ.20000000002) GO TO 20	GULP0340
C	IF(ND.NE.ID) GO TO 2	GULP0350
C	IF(ICHAN.EQ.0 .OR. CHNLNO.EQ.ICHAN) GO TO 10	GULP0360
C	GO TO 2	GULP0370
C		GULP0380
C	SET UP INITIAL PARAMETERS	GULP0390
C		GULP0400
C	10 IF(K.EQ.0) GO TO 500	GULP0410
C	NCR=(K-1)/100	GULP0420
C	NMAX=4*K-NCR*400-3	GULP0430
C	KR=397	GULP0440
C	NRR=0	GULP0450
C	RETURN	GULP0460
C		GULP0470
C	ERROR MESSAGE IF UNABLE TO FIND CORRECT CHANNEL	GULP0480
C		GULP0490
C	20 WRITE(6,21) ID,ICHAN	GULP0500
C	21 FORMAT(1H0,36H NO DATA WITH IDENTIFICATION NUMBER I10,20H AND CHA	GULP0510
C	INNEL NUMBER I1,13H ON DATA TAPE)	GULP0520
C	ID=ND	GULP0530
C	RETURN	GULP0540

C		GULP0550
C	READ IN NEW DATA POINT.	GULP0560
C		GULP0570
100	IF(ND.EQ.20000000002) RETURN	GULP0580
	KR=KR+4	GULP0590
	IF(KR.LT.400) GO TO 105	GULP0600
	IF(NRR.GT.NCR) GO TO 500	GULP0610
	READ(4) STOR	GULP0620
	NRR=NRR+1	GULP0630
	KR=1	GULP0640
105	IF(NRR.LE.NCR) GO TO 106	GULP0650
	IF(KR.GT.NMAX) GO TO 500	GULP0660
106	T=STOR(KR)	GULP0670
	C=STOR(KR+1)	GULP0680
	B=STOR(KR+2)	GULP0690
	A=STOR(KR+3)	GULP0700
	RETURN	GULP0710
C		GULP0720
C	ERROR MESSAGE IF END OF DATA IS REACHED	GULP0730
C		GULP0740
500	WRITE(6,501)	GULP0750
501	FORMAT(1H0,37H END-OF-DATA ENCOUNTERED ON DATA TAPE)	GULP0760
	ID=20000000002	GULP0770
	ND=ID	GULP0780
	RETURN	GULP0790
C		GULP0800
	END	GULP0810

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