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JUL EQUATION OF STATE COEFFICIENTS FOR HIGH EXPLOSIVES
E. Lee, M. Finger, W. Collins

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# JWL EQUATION OF STATE COEFFICIENTS FOR HIGH EXPLOSIVES 

E. Lee, M. Finger, W. Collins

## Introduction

The compilation of equations of state for high explosives now includes some 38 entries. Additions and revisions have recently introduced errors in the listirgs. To avoid transcribing errors, we have computerized the list and will issue computer updates periodically.

Previous lists should be discarded. If you are maintaining equation of state files for hydrodynamic codes and would like IBM card records of our lists, we will be happy to send you a copy of our card deck. We have noted those entries where changes or corrections have been made. Of special note for this update are the corrections to PBX-9404 and IX-04 from the most recent memo, dated August 23, 1972.

## HIGH EXPLOSIVE EQUATION OF STATE DESCRIPTION

The Jones-Wilkins-Lee (JWL) equation of state has been used to accurately describe the pressure-volume-energy behavior of the detonation products of explosives in metal acceleration applications. The equation is:

$$
P=A\left(1-\frac{\omega}{R_{1} V}\right) e^{-R_{1} V}+B\left(1-\frac{\omega}{R_{2} V}\right) e^{-R_{2} V}+\frac{\omega E}{V}
$$

The equation for $P$ as a function of $V$ at constant entropy, i.e., the isentrope, is

$$
P_{s}=A e^{-R_{1} V}+B e^{-R_{2} V}+C V^{-(\omega+1)}
$$

where:

$$
\begin{aligned}
& V=\text { (volume of detonation products)/(volume undetonated explosive) } \\
& P=\text { pressure in megabars } \\
& E=\text { energy in } \mathrm{Mb} \mathrm{cc} / \mathrm{cc}
\end{aligned}
$$

A limited number of explosives have been subjected to a rigorous comparison in which coefficients are determined by matching the equation with experimental C-J conditions, calorimetric data, and expansion behavior -- generally cylinder test data. ${ }^{(1,2,3)}$ These explosives are listed in the Table attached without additional notation. It has proven very useful to estimate coefficients for explosives for which a limited amount of data is available. For these explosives the estimated parameters are noted. The best estimates are for those explosives for which cylinder test data is available. We have estimated $P_{c j}$ in many instances by assuming $2.7<\Gamma<2.8$. In cases where data was extremely limited we have made estimates from Ruby calculations for $P_{c j}, D$, and $E_{0}$ and estimated $R_{1}, R_{2}$ and $\omega$.
${ }^{1}$ J. W. Kury, H. C. Hornig, E. L. Lee, J. L. McDonnel, D. L. Ornellas, M. Finger, F. M. Strange, M. L. Wilkins, "Metal Acceleration by Chemical Explosives", Fourth Symposium on Detonation, p. 3, Office of Naval Research (1965).
${ }^{2}$ E. L. Lee, H. C. Hornig and J. W. Kury, UCRL-50422, May 2, 1968, "Adiabatic Expansion of High Explosive Detonation Products".
$3_{\text {E. L. Lee and H. C. Hornig, "Equation of State of Detonation Product Gases", }}^{\text {, }}$ Twelfth Symposium (International) on Combustion, p. 493 (1969).


EZUATION OF STATE PARAMETERS FOR SOME EXPLOSIVES

| NAME |  | CJMPJSITION |  | C.J. PARAMETERS |  |  |  |  | J H L |  | STATE GOEFFICIENTS |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $P$ MBAK |  | $\begin{gathered} D \\ \text { CH PER } \\ \text { MICSEC } \end{gathered}$ | $\begin{gathered} \equiv 0 \\ M 8-\mathrm{CC} / \mathrm{CC} \end{gathered}$ | $\begin{aligned} & \text { RHO } \\ & \text { GH/C } \end{aligned}$ | SAMMA | A | 8 | C | R1 | R2 | $\downarrow$ |
|  | 4x-10 |  | $\begin{aligned} & \text { HMX } \\ & \text { YITON } \end{aligned}$ | $\begin{array}{r} 95.0 \\ 5.0 \end{array}$ | 0.375 | U. 882 | $0.1040 \%$ | 1.860 | 2.861 | 8.842 | 0.17437 | 0.00809 | 4.60 | 1.20 | 0.30 |
|  | Lx-11 | HMX <br> VITON | $\begin{aligned} & 80.0 \\ & 20.0 \end{aligned}$ | 0.330 | 0.832 | $0.090{ }^{*}$ | 1.875 | 2.930 | 7.791 | 0.10668 | 0.00885 | 4.50 | 1.15 | 0.30 |
|  | NH |  | 100.0 | 0.125 | 0.628 | 0.0510 | 1.128 | 2.538 | 2.092 | J. 05689 | 0.00770 | 4.45 | 1.20 | 0.30 |
|  | OCTOL | $\begin{aligned} & \text { HMX } \\ & \text { TNT } \end{aligned}$ | $\begin{aligned} & 70.0 \\ & 22.0 \end{aligned}$ | 0.342 | 0.848 | $0.4960 *$ | 1.821 | 2.830 | 7.486 | 0.13380 | 0.31167 | 4.50 | 1.20 | 0.38 |
|  | P8X 3020 | $\begin{aligned} & \text { RJX } \\ & \text { KEL F } \end{aligned}$ | $\begin{aligned} & 90.0 \\ & 10.0 \end{aligned}$ | 0.340 | 0.839 | 0.090 .5 | 1.787 | 2.700 | 5.814 | 0.06801 | 0.00234 | 4.10 | 1. ƠU | 0.35 |
| $\neq$ | P8X 9011 | $\begin{aligned} & \text { HMX } \\ & \text { ESTAVE } \end{aligned}$ | $\begin{aligned} & 90.0 \\ & 10.0 \end{aligned}$ | 0.340 | 0.85 u | $0.0890 \%$ | 1.777 | 2.775 | 6.347 | 0.07998 | 3.00727 | 4.20 | 1.00 | 0.30 |
| $\neq$ | P8X 9404-3 | $\begin{aligned} & \text { HMX } \\ & N= \\ & C E F \end{aligned}$ | $\begin{array}{r} 94.0 \\ 3.0 \\ 3.0 \end{array}$ | 0.370 | U. 88 u | 0.1020 | 1.840 | 2.850 | 3.545 | 0.20493 | 0.00754 | 4.60 | 1.35 | 0.25 |
| \# | PETN |  | 100.0 | U. 335 | 0.830 | 0.1010 | 1.770 | 2.640 | 0.170 | 0.16926 | 4.04699 | 4.40 | 1.20 | 0.25 |
| $\neq$ | PEIN |  | 100.0 | 0.220 | 0.745 | $0.0856 *$ | 1.500 | 2.788 | 6.253 | 0.23290 | 0.01152 | 5.25 | 1.60 | 0.28 |
|  | PETN |  | 100.0 | 0.140 | 0.654 | 0.67197 | 1.260 | 2.831 | 5.731 | 0.20160 | $\checkmark .01267$ | 6.00 | 1.80 | 0.23 |
|  | PETN** |  | 100.0 | 0.062 | 0.517 | $0.0502^{\circ}$ | 0.880 | 2.668 | 3.486 | $0.112 d 8$ | 0.00941 | 7.00 | 2.00 | 0.24 |
| \# | pentolite | $\begin{aligned} & \text { TNT } \\ & \text { PETN } \end{aligned}$ | $\begin{aligned} & 50.0 \\ & 50.0 \end{aligned}$ | 0.250* | 0.747 | 0.0800 | 1.670 | 2.727 | 4.911 | 0.09061 | 0.30876 | 4.4is | 1.16 | 0.30 |
|  | RX-01-AE | NM <br> SI 22 <br> GUAR | $\begin{array}{r} 87.0 \\ 10.0 \\ 3.0 \end{array}$ | $0.125^{*}$ | 0.611 | $0.0450 \%$ | 1.210 | 2.614 | 2.111 | 0.04754 | 0.00795 | 4.30 | 2.30 | 0.34 |
|  | RX-OS-OR | HyX EONP SIJ2 | $\begin{array}{r} 76.0 \\ 22.0 \\ 2.0 \end{array}$ | $0.290 *$ | 4.796 | $0.0800^{*}$ | 1.711 | 2.736 | 5.267 | 0.06823 | J.00991 | 4.20 | 1.45 | 0.36 |
| RX-04-DS |  | HyX <br> AL <br> VITUV | $\begin{aligned} & 80.0 \\ & 10.0 \\ & 10.0 \end{aligned}$ | $0.340 \%$ | 0.852 | $0.145 u^{*}$ | 1.865 | 2.981 | 9.073 | 0.16400 | 0.151473 | 4.70 | 1.40 | 0.40 |
|  |  | - estruateo zuantities |  |  |  | * - \%LIN | ER TEST | DATA N | AVAILA |  |  |  |  |  |



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[^0]:    - estiyateo zuantities
    * Eylinjer test data not availadle
    \# Revised data

