

PERCOL USER'S MANUAL

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1973

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by

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Water and Land Resources Department

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BATTELLE  
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## SUMMARY

Research being conducted under the Radionuclides in Soils Program is attempting to predict the distribution and movement of liquid wastes in the heterogeneous subsurface environment of the Hanford Reservation. As part of this program, a transport model is being developed to predict chemical phenomena in soil-waste reactions. This document describes the use of the PERCOL model, which was developed as a simplified one-dimensional precursor to the transport model. PERCOL numerically describes the complex chemical reactions which occur during percolation of a waste solution through a porous media. This User's Manual describes the main program (PERCOL) and two subroutines (NEWTIT and DIST) and gives procedures for accessing these programs, inputting data to them and interpreting the output.

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## PERCOL USER'S MANUAL

### INTRODUCTION

The objective of the "Radionuclides in Soils" program being conducted by Battelle-Northwest for the Atlantic Richfield Hanford Company is development of tools for managing groundwater resources. As part of this program a transport model has been developed to predict the movement of contaminants in groundwater systems. Another model, PERCOL, was developed to describe the complex chemical reactions which occur during percolation of waste solutions through porous media such as soils. The PERCOL model can also be used as a simplified one-dimensional transport model; in this capacity, with support from experimental studies utilizing soil columns, PERCOL has been used as a precursor of the more complex transport model. This report is intended to provide the necessary direction for use of the PERCOL computer model. More detailed theory can be found in BNWL 1718.<sup>1</sup>

The PERCOL program is an extended and revised version of a program developed by Dutt<sup>2</sup> and Tanji<sup>3</sup> for predicting the quality of water and breakthrough of contaminants at incremental lengths throughout a soil profile. Basically the use of the computer code entails the input of the initial values for all the chemical species present in solution and in the

soil as well as the values for the soil and solution volumes; in addition, the output values corresponding to the equilibrium conditions in solution and on the soil must be interpreted. The calculations thus produced are input to the transport model of the Radionuclides in Soils program.

PERCOL solves a one-dimensional version of the transport equation. Diffusion and dispersion are neglected and a Lagrangian coordinate system (following a fixed mass of fluid as it moves in space) is utilized.

This report gives detailed procedures for accessing the main program and two subroutines (NEWTIT AND DIST), inputting data, and interpreting the resulting output. The Appendices contain sample input cards, program listings, and output.

### THE PERCOL PROGRAM

A soil column is divided into K separate cells, called soil subdivisions, to facilitate numerical calculations of the macro species concentrations (macro constituents are those species which are present in sufficient concentrations to appreciably affect the ionic strength of the solution and cation exchange sites available on the soil). A soil subdivision represents a homogeneous layer of soil. Thus a column consisting of several soil types is modeled with integral numbers of different soil subdivisions.

To model trace constituent sorption it was found necessary to further subdivide each K<sup>th</sup> soil subdivision to prevent numerical dispersion. This partitioning is necessary only for modeling the sorption of the trace constituents and is represented by the variable JSUB.

All macro species chemical reactions take place in K soil subdivisions and all micro trace sorption reactions take place in (JSUB) X (K) partitions. In a saturated regime a pore volume of influent is introduced into the top subdivision and batch type chemical equilibria are calculated. The equilibrated effluent solution from the first subdivision becomes the influent to the second subdivision and batch type equilibria are again calculated. The pore volume of solute moves into successive subdivisions and equilibrates until it exits the last subdivision as effluent. A fresh aliquot is then initiated in the top cell and the sequence is repeated until the desired quantity of effluent is reached. Figure 1 is a conceptualization of the solute movement.

Additional assumptions which bear on the utilization of PERCOL are listed in Appendix A.

PERCOL has two subroutines, NEWTIT AND DIST. NEWTIT uses a numerical technique to solve for the real root of an equation  $F(x)=0$ . This equation determines the equilibrium concentrations of the chemical species which are reacting by precipitation, cation exchange, etc. Subroutine DIST calculates the empirical distribution constant Kd for sorption of each trace constituent. Details on the specific chemical reactions involved and a discussion of the empirical distribution constant can be found in BNWL 1718.<sup>1</sup>

PERCOL input consists of:

- soil column parameters - soil volume, number of soil subdivisions, bulk density, soluble salt content, cation exchange capacity, slightly soluble crystalline salt content

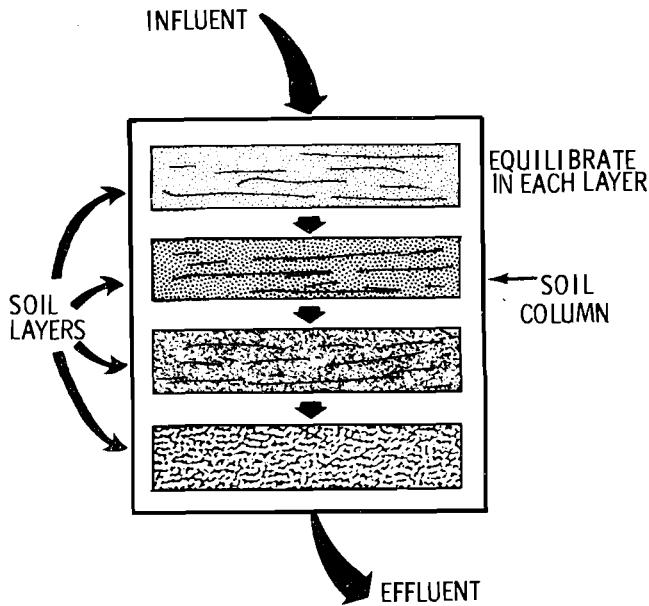


FIGURE 1. Solute Movement in PERCOL Model

- solution parameters - volume of soil to be percolated, concentration of all constituents in the solution, pH
- chemical reaction parameters - empirical ion exchange constants

Input for the subroutine NEWTIT consists of an approximation of the root  $x$ , the function  $F(x)$ , the first derivative of the function and several indices containing logical information. All of this input is automatically generated in PERCOL.

Input for the subroutine DIST consists of the concentrations of chemical species in the waste solution, the soil type present, and the  $K_d$  predictor equation for the trace constituent of interest. The  $K_d$  predictor equation is added to the subroutine by the user. The other input is automatically transferred from the main program.

#### ACCESS

At present the PERCOL program and its subroutines are available in a FORTRAN IV punched deck consisting of about 700 cards which is set up to run on a UNIVAC 1108 computer.

## INPUT REQUIREMENTS

The input requirements for the PERCOL model vary depending on the options chosen. Regardless of the options being used, all input data are transferred to the computer on data cards. The data needed if the soil column is originally dry are different from those used if the soil column is initially wet and well leached. If the soil column is nonhomogeneous each cell requires its own set of input data cards; only one set of data cards is necessary for a homogeneous soil column, however, as the computer program automatically generates the necessary input data for all the remaining soil cells.

The required input for PERCOL is arranged in four basic categories:

- descriptive or control parameters
- empirical data for ion exchange reactions
- soil column dimensions and constituents
- waste solution volumes and concentrations

Two examples of a typical input arrangement are given in Appendix B.

### Descriptive Parameters

For all options, the first card in the data deck contains a number of TRUE or FALSE answers concerning the program options to be used. The TRUE or FALSE input determines conditions to be simulated. The options for TRUE or FALSE responses are presented as statements, as follows (each option statement is coded into the computer as a variable):

The first statement is, "The soil column is dry and evaporated salts are present" (the variable which controls this statement is DRY). If the statement is true, the first aliquot of waste solution containing the soil will dissolve the soluble salts present in the dry soil. If the statement is false, the column is assumed to be wet and evaporated salts have already been leached from the soil.

The second statement is, "The soil profile is homogeneous and chemical concentrations are initially the same" (the variable which controls this statement is UNI). If the statement is true, only one set of chemical data cards is needed and the computer generates identical values for the rest of the soil cells throughout the column. If the statement is false, separate sets of data cards must be input for each soil subdivision.

The third statement reads, "Print all initial and equilibrium chemical concentrations at each soil subdivision" (the variable which controls this statement is PRINT). If the statement is true, a large amount of output is generated. For the average problem this output is unnecessary, but in the debugging phase the printing may aid the user. If the statement is false, only the equilibrium concentrations of the solution effluent and of the last soil subdivision are printed. In most applications these effluent concentration data are the desired quantities.

The fourth statement is, "Print all equilibrium chemical concentrations at each subdivision" (the variable which controls this statement is PRI). This statement, when true, allows only the equilibrium values at all subdivisions to be printed. This permits a more comprehensive output of the effluent from each subdivision and the equilibrium soil conditions, but neglects the initial values entering the soil subsections. Since the effluent from subdivision K-1 is the influent to subdivision K, initial data for all but the first cell can be gleaned from this output.

#### Empirical Data for Ion Exchanges

Three ion exchange reactions are included in the PERCOL model.<sup>1</sup> Each soil type is uniquely selective for the major competing ions in the Hanford waste streams. Numerical description of the ion exchange phenomena between two cations and the soil exchange sites requires two empirical constants; the procedures for measuring the constants are described in BNWL 1721.<sup>4</sup> At present three sets of cation exchange reactions are included in PERCOL. The necessary input variables follow:

P1 = empirical activity correction for solid phase  
ratio  $\frac{\text{MgX}}{\text{CaX}}$

FK1 = empirical ion exchange selectivity constant  
for  $\text{Mg}^{++}$  replacing  $\text{Ca}^{++}$  on the soil

P2 = empirical activity correction for solid phase  
ratio  $\frac{\text{NaX}}{\text{CaX}}$

FK2 = empirical ion exchange selectivity constant  
for  $\text{Na}^+$  replacing  $\text{Ca}^{++}$  on the soil

P3 = empirical activity correction for solid phase  
ratio  $\frac{\text{KX}}{\text{NaX}}$

FK3 = empirical ion exchange constant for  $K^+$   
replacing  $Na^+$

### Soil Column Parameters

The parameters which specify column sizes, numbers of subdivisions, and soil chemical characteristics are given below. Variables which must be specified whether the soil column is initially dry or wet include:

K = number of subdivisions in which soil column is divided. At present the program is dimensioned for a maximum K=20

VSOIL = total volume of soil column (units must correspond with units on solution aliquot size); i.e.,  $cm^3-cm^3$ , etc.

JSUB = number of partitions into which each soil subdivision is further divided to aid the mathematical computations involved in trace constituent sorption. Macro reactions are carried out in K subdivisions and micro (trace) sorption divided in JSUB partitions for each K<sup>th</sup> subdivision. A total trace partition (JSUB) X (K) equal to the physical length of the laboratory column (cm) has proven to give the best results. For example, a 50 cm column is modeled with K=10 and JSUB=5. At present, the column is dimensioned for a maximum JSUB=50

PORE = the empirically determined effective porosity of the soil column. The value is less than one and represents the drainable pore space

CAL = calcium carbonate (moles/gm) found in soil

GYP = calcium sulfate (moles/gm) found in soil

CAF = calcium fluoride (moles/gm) found in soil

SRS = initial trace constituent concentration sorbed on soil (for radioactive substances units cpm/gm, or mc/gm, etc.)

B11 = moisture percentage at which soil extract runs =  
100 (gms  $H_2O/gm$  Soil)

B2 = moisture percentage at saturation

$$100 \frac{(PD-BD)}{(PD \cdot BD)}$$

where PD = particle density in gm/cm<sup>3</sup>,  
usually set at 2.65, and BD = soil bulk  
density in gm/cm<sup>3</sup>

B3 = percent saturation in the soil column being  
modeled

Additional soil parameters for initially dry soils are:

SOCA = readily soluble calcium (meq/liter) found in  
the B1l soil-solution extract (example: 100 gms  
initially dry soil is equilibrated with X mls  
distilled water; the solution extract is then  
measured for Ca)

SOMG = readily soluble magnesium (meq/liter) found in  
the B1l soil-solution extract

SONA = readily soluble sodium (meq/liter) found in  
the B1l soil-solution extract

SOK = readily soluble potassium (meq/liter) found in  
the B1l soil-solution extract

SOSR = readily soluble stable strontium (meq/liter)  
found in the B1l soil-solution extract

SOCL = readily soluble chloride (meq/liter) found in  
the B1l soil-solution extract

SOSO4 = readily soluble sulfate (meq/liter) found in  
the B1l soil-solution extract

SOHCO3 = readily soluble bicarbonate (meq/liter) found  
in the B1l soil-solution extract

EC = cation exchange capacity of soil (meq/gm)

Additional parameters for initially wet soil from which readily  
soluble salts have already been removed are:

CT = exchangeable magnesium sorbed on the soil  
(moles/gm)

RSR = exchangeable stable strontium sorbed on the  
soil (moles/gm)

ET = exchangeable calcium sorbed on the soil  
(moles/gm)

RP = exchangeable potassium sorbed on the soil  
(moles/gm)

SAT = exchangeable sodium sorbed on the soil  
(moles/gm)

#### Waste Solution Parameters

The reactions which take place as a solution percolates through porous media depend upon the chemical makeup of the solution. Thus solution constituents are necessary input to the PERCOL model. Waste solution parameters are:

WCA = calcium ion concentration in solution  
(meq/liter)

WMG = magnesium concentration in solution  
(meq/liter)

WNA = sodium concentration in solution (meq/liter)

WK = potassium concentration in solution  
(meq/liter)

WSR = strontium concentration in solution  
(meq/liter)

WCL = chloride concentration in solution  
(meq/liter)

WSO<sub>4</sub> = sulfate concentration in solution (meq/liter)

WHCO<sub>3</sub> = bicarbonate concentration in solution  
(meq/liter)

WNO<sub>3</sub> = nitrate concentration in solution (meq/liter)

WFL = fluoride concentration in solution (meq/liter)

CASOI = associated calcium sulfate complex in solution  
(moles/liter)

APH = pH of solution

SRIN = influent concentration of trace ion being  
investigated; units to correspond to units  
on SRS (cpm/ml or mc/ml)

If more than one tracer is to be studied at once, SRIN1, SRIN2, etc., must be programmed in and appropriate variables throughout PERCOL added:

- ALI = volume equivalent to one aliquot (pore volume of column/column subdivisions) times percent saturation
- M = number of aliquots of this particular waste which should be percolated
- LB = total number of aliquots of waste to be percolated

As many different waste solutions as are desired can be percolated through the soil. Each waste requires its own set of data cards with the input values of the above variables.

#### OUTPUT INTERPRETATION

As mentioned, the bulk of the work in using PERCOL is data manipulation. The necessary input variables were described in the previous section. The interpretation of the large amount of computer generated output follows. Besides output such as initial and equilibrium values of all the chemical species interacting in the soil-waste solution regime, diagnostic output is possible if problems with the numerical calculations are encountered.

#### Printed Output

The first outputs generated by PERCOL are the four option statements and replies for the particular run being submitted, followed by the printout of the chemical concentrations of the variables read as input. This provides a check on the accuracy of the data cards. The number of output lines will depend on the option taken. The values fall directly under a heading which contains a list of the input variables, so identification should be obvious.

Provided the Newton-Raphson iteration techniques (see NEWTIT) converge in fewer than 90 iterations, all output will consist of lines of heading followed by lines of numerical output for either initial or equilibrium chemical concentrations. The headings state whether the values to follow are equilibrium or initial and give the solution aliquot numbers and soil subdivisions.

The two headings are as follows:

- INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE,  
COLUMN K ALIQUOT LL

- EQUILIBRIUM VALUES FOR ALL IONS, COLUMN K ALIQUOT LL

Chemical headings are explained below:

K = potassium concentration in solution, m/l  
KX = potassium concentration sorbed on soil, m/gm  
NA = sodium concentration in solution, m/l  
NAX = sodium concentration sorbed on soil, m/gm  
MG = magnesium concentration in solution, m/l  
MGX = magnesium concentration sorbed on soil, m/gm  
SR = strontium concentration in solution, m/l  
(stable macro portion)  
SRX = strontium concentration sorbed in soil, m/gm  
(stable macro portion)  
CA = calcium ion concentration in solution, m/l  
CAX = calcium concentration sorbed on soil, m/gm  
HCO<sub>3</sub> = bicarbonate concentration in solution, m/l  
NO<sub>3</sub> = nitrate concentration in solution, m/l  
SO<sub>4</sub> = sulfate concentration in solution, m/l  
CL = chloride concentration in solution, m/l  
FL = fluoride concentration in solution, m/l  
CASO<sub>4</sub>UN = associated calcium sulfate concentration in solution, m/l  
GYPSUM = calcium sulfate precipitated in soil, m/gm  
CAL = calcium carbonate precipitated in soil, m/gm  
CAF = calcium fluoride precipitated in soil, m/gm  
PH = pH of effluent solution  
KD = distribution constant for particular waste  
B = soil-to-solution ratio, gm/liter

U = square root of ionic strength of waste solution,  
 $\sqrt{m/l}$

SR85 = concentration of trace constituent sorbed on  
SOIL soil (cpm/gm or mc/gm)

SR85 = concentration of trace constituent in effluent  
SOL solution (cpm/ml or mc/ml)

VOLUME = total volume of effluent through column, mls  
(MLS) (but can change to any units)

COVOL = column volumes of effluent through column

C/CO = effluent trace concentration/influent trace  
concentration (breakthrough)

#### INTERNALY GENERATED DIAGNOSTICS

One further type of numerical output is possible if NEWTIT does not converge within 90 iterations. The output will be lines consisting of the fixed point variable, ION, with values of from 1 to 5, followed by 5 to 7 floating point numbers. The fixed point number identifies the chemical reaction which is not converging.

- 1 = Mg-Ca Ion Exchange
- 2 = Na-Ca Ion Exchange
- 3 = Na-K Ion Exchange
- 4 = Calcium Carbonate Solubility
- 5 = Calcium Fluoride Solubility

The floating point numbers give the value of F(x), the root (x), the first derivative of F(x) which is the variable FXP, and the values of the chemical species involved. The numbers help to determine why the system is not converging.

#### NEWTIT SUBROUTINE

The subroutine NEWTIT is a mathematical algorithm which solves for the real root of an equation in the form of  $F(x)-C=0$ , where  $F(x)$  is any polynomial function of  $x$  and  $C$  is a constant.

The ion exchange and precipitation reactions being modeled can be put in the above form. The subroutine utilizes the Newton-Raphson iterative technique.

#### ACCESS

The subroutine NEWTIT is available as a FORTRAN IV punched deck of about 70 cards. It is found directly behind the main program PERCOL. NEWTIT should not have to be altered unless new chemical species which enter into reactions solved by the Newton-Raphson technique are added to the main program. This subroutine is a modification of the Program NEWTIT found in the UNIVAC 1108 Math Pack, Section 4 UP 7545.5,6

#### INPUT REQUIREMENTS

Because all input requirements for the subroutine NEWTIT are generated in the main program PERCOL, the user need not input further information. The UNIVAC 1108 Math Pack may be consulted for details of the subroutine.

Briefly, the variables automatically generated in PERCOL for subsequent input to NEWTIT include:

- X an initial estimate of the real root
- FX the polynomial function of X
- FXP the first derivative of the polynomial function of X
- ERROR the tolerance limit near zero which will satisfy convergence (the digital computer will repeatedly attempt to reach zero exactly if this tolerance limit is not specified. Defining a narrow band on the number line around zero allows the computer to accept convergence tests which are not exactly zero)
- NUMB the number of iterations the program should try before stopping (this prevents the computer from entering an infinite loop due to lack of convergence)
- KAR an integer which acts as an indicator by NEWTIT (details can be found in Reference 5)
- ION identifies the chemical equation being solved

## OUTPUT INTERPRETATION

### Internal Diagnostics

Built into NEWTIT are two checks to insure that computations are proceeding properly. If the chemical computations do not converge after a designated number of iterations, N (set at 100 for this program), the diagnostic occurs: "ROOT DID NOT CONVERGE WITHIN MAXIMUM NUMBER OF ITERATIONS, PROGRAM RETURNING TO NEXT SET OF DATA." Following this diagnostic are three numbers showing the soil subdivision, K; the aliquot, ISOL; and the chemical equation in which the program was stuck, ION (described in the "Internally Generated Diagnostics" section). Unless data for a new soil column follows, the run terminates.

The second diagnostic is "OVERFLOW IN COMPUTATIONS, RETURNING TO NEXT SET OF DATA." This occurs when  $F(x)$  is very large and/or  $FXP$  is very small in the Newton-Raphson scheme. If this occurs for no apparent reason, the tolerance level, E, for  $F(x) \leq E$  must be increased. This is done by increasing the value of the variable ERROR in the PERCOL deck for the appropriate reaction.

### Output to Main Program

NEWTIT's output to the program PERCOL is internally interpreted and unless one of the two error diagnostics is indicated the run continues.

## SUBROUTINE DIST

The subroutine DIST contains the mathematical equation used to estimate the value of  $K_d$ . The equation is derived from experimental data described elsewhere.<sup>1,4</sup> The equation requires the input of equilibrium chemical variables of the waste solution which are automatically transferred from PERCOL.

### ACCESS

The subroutine DIST is available as a FORTRAN IV punched deck of about 15 cards. It is found directly behind NEWTIT and must be altered whenever a new  $K_d$  predictor equation is to be used.

The variable AKD is the predictor equation and must be repunched whenever a new equation is used. Monitoring of more than one trace constituent requires use of several  $K_d$  equations (such as AKD1, AKD2.....); cards are added to the deck for each of these. Variables for the new wastes would also be added in appropriate spots in the main program.

### INPUT REQUIREMENTS

The input requirements are the current equilibrium concentration values of all the macro constituents in the solution. These values are automatically transferred from the main program.

### OUTPUT INTERPRETATION

The output is the value of Kd for the particular waste solution, soil type and trace constituent of interest. The value is automatically returned to PERCOL and computations continue.

#### ACKNOWLEDGMENTS

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## APPENDIX A

### ASSUMPTIONS INTRINSIC TO PERCOL

## APPENDIX A

### ASSUMPTIONS INTRINSIC TO PERCOL

- Dispersion, diffusion and evaporation are neglected.
- Seepage velocity is slow enough for equilibrium to be attained.
- Cation exchange capacity is constant for each soil type.
- Binary equations approximate the complex cation exchange in porous media.
- Equilibrium states are path independent.
- Anion exchange is negligible.
- Limestone, fluorite and gypsum are considered to be the only slightly soluble salts present and their solubility is assumed to be that of the crystalline form.
- Undissociated calcium sulfate is the only complex ion formed.
- Activity coefficients follow the Davies extension of the Debye-Huckel theory.
- Moisture content is uniform.
- Reactions of macroions present are described by factorial design regression coefficients.

## APPENDIX B

SAMPLE INPUT CARDS AND PRINTED OUTPUT

## APPENDIX B

### SAMPLE INPUT CARDS AND PRINTED OUTPUT

1. GENERAL INPUT CARD DESCRIPTION
2. CASE ONE

COLUMN IS WET

COLUMN IS NONUNIFORM

PRINT ALL VALUES

COLUMN HAS FOUR SUBDIVISIONS

ONE WASTE SOLUTION

3. CASE TWO

COLUMN IS DRY

COLUMN IS UNIFORM

PRINT ONLY EQUILIBRIUM VALUES AT LAST SUBSECTION

COLUMN HAS TEN SUBDIVISIONS

ONE WASTE SOLUTION

### GENERAL INPUT CARD DESCRIPTION

The data card which contains values, or answers, for the True or False Program Option Statements should be as follows: (true or false) value for each statement occupying a card column field 10 columns wide and beginning with card column 1 must be punched in the card. Each value is left justified within its card column field and statements are punched in the order they are asked. SEE FORMAT STATEMENT 1150.

The data card containing values for the variables P1, FK1, P2, FK2, P3, and FK3 must be as follows: beginning with card column 1, each value must be a real number and occupy a card column field 10 columns wide. All values are punched on the card and each is right justified within its card column field. They must be in the same order on the card as they are above. SEE FORMAT STATEMENT 1200.

The data card containing values for the variables K, JSUB, VSOIL, PORE, and B3 must have the following format: the first two values are integers, each occupying a card column field 6 columns wide beginning with card column 1. Each value must be present on the card and right justified within its field. The next three values are real numbers; each occupies a card column field 10 columns wide beginning with card column 13. Each value must be present on the card and right justified within its card column field. All values on this card must be punched in the same order as they appear above. SEE FORMAT STATEMENT 1220.

The data card containing values for the variables SOCA, SONG, SONA, SOK, SOSR, SOCL, SOSO4, and SOHCO3 is as follows: all values are real numbers; each occupies a card column field 8 columns wide, beginning with card column 1. Each value must be right justified within its card column field. All values need not be present but card column fields for those missing must be left blank. All values punched on this card must be in the same order on the card as they are above. SEE FORMAT STATEMENT 1140.

The data card containing values for the variables SONO3, EC, CAL, B11, B2, GYP, SRS, and CAF follows the same rules and format as the data card containing values for the variables SOCA, SONG, SONA, SOK, SOSR, SOSO4, and SOHCO3. SEE FORMAT STATEMENT 1140.

The data card containing values for the variables SAT, RP, ET, CT, and RSR must be as follows: all the values must be punched in exponential notation and each value must occupy a card column field 15 columns wide, beginning with card column 1. Each value must be right justified within its card column field. All the values need not be present but card column fields for those missing must be left blank. All the values punched must be in the same order on the card as they are above. SEE FORMAT STATEMENT 1260.

The data card containing values for the variables GYP, CAL, B2, CAF, and SRS must follow the same rules and format as the data card containing values for the variables SAT, RP, ET, CT, and RSR. SEE FORMAT STATEMENT 1260.

The data card containing values for the variables WCA, WMG, WNA, WK, WSR, WCL, WSO4, WHCO3, and M should be as follows: the first eight values are real numbers, and each must occupy a card column field 8 columns wide, beginning with card column 1. Each value must be right justified within its card column field. The last value punched on the card must be an integer number; it must occupy a card column field 5 columns wide,

beginning with card column 70, and be right justified within its field. All values need not be present but card column fields for those missing must be left blank. The values must be in the same order on the card as they are above.  
SEE FORMAT STATEMENT 1140.

The data card containing values for the variables WNO3, SRIN, CASOI, APH, and WFL follows the same rules and format as the data card containing values for the variables WCA, WMG, WNA, WK, WSR, WCL, WSO4, WHCO3, and M. SEE FORMAT STATEMENT 1140.

The data card containing values for the variables ALI and LB must be as follows: the first value is punched in exponential notation and occupies a card column field 14 columns wide, beginning with card column 1. It must be right justified within this field. The second value punched in the card must be an integer and it must occupy a card column field 6 columns wide, beginning with card column 15. It must be right justified within its field. SEE FORMAT STATEMENT 1270.

#### CASE ONE (WET SOIL)

The first example of data input and computer output considers a soil column which is initially wet and has had the slightly soluble salts entirely leached from the soil. The soil column has four nonhomogeneous soil subdivisions for which input is needed. The computer generated output is in the mode which prints both the initial and final chemical concentrations for each soil cell.

The first data card contains a string of four words which answer true or false to the four questions posed by the program options. Each true or false answer is punched in a card column field 10 columns wide beginning with card column 1 and each word is left adjusted within its field. SEE FORMAT STATEMENT 1150.

The second data card contains values for the variables P1, FK1, P2, FK2, P3, and FK3, the empirical ion exchange constants for the cation exchange reactions. A real number value for each variable must occupy a 10 card column field, beginning with card column 1, and the values must be in the order specified above. SEE FORMAT STATEMENT 1200.

The third data card contains values for the variables K (the number of soil subdivisions), JSUB (the number of micro subdivisions), VSOIL (the volume of the soil column), PORE (the effective porosity), and B3 (the percent saturation) that the soil column will have. A value for each variable must be

entered in the following format. The first two variable values are integers and each occupies a card column field six columns wide beginning with card column 1. The column field is right adjusted. The next three variable values are real numbers, each occupying a card column field ten columns wide beginning with card column 13. They also must be in the order specified above on the card. SEE FORMAT STATEMENT 1220.

The first three data cards are present in the described format whether the soil is wet or dry. If the soil is wet, the fourth data card contains values for the variables SAT, RP, ET, CT, and RSR; these are the exchangeable sodium, potassium, calcium, magnesium and strontium concentrations sorbed on the soil. Each of these values present must occupy a card column field 15 columns wide beginning with card column 1 and must be written in exponential notation, such as (2.221E-05). The values must appear on the card in the order specified above and the 15 card column field of each missing variable value must be left blank, or zeroed. SEE FORMAT STATEMENT 1260.

The fifth data card contains values for the variables GYP, CAL, B2, CAF, AND SRS. These are calcium sulfate, calcium carbonate found in soil, moisture percentage at saturation, calcium fluoride found in the soil, and initial trace constituent concentrations sorbed on the soil. Every one of these values need not be present, but those that are must follow the format outlined for the fourth data card. SEE FORMAT STATEMENT 1260.

The fourth and fifth data cards will be present if the soil conditions are termed WET. For DRY soil conditions different variables and card formats will be used for data cards four and five. SEE CASE TWO.

The sixth through eleventh data cards pertain to a nonuniform soil column. These cards are input in pairs containing data for the same variables found on data cards four and five and follow the same format as cards four and five. The number of pairs depends upon the number of soil cells. For this particular case there were four soil cells, hence eight data cards (data cards four through eleven).

The next three data cards are considered to be a set, and at least one set is always present. The presence of additional sets signifies that additional waste solutions will be used.

The twelfth data card contains values for the variables WCA, WMG, WNA, WK, WSR, WCl, WSO4, WHCO3, and M. These represent the calcium, magnesium, sodium, potassium, strontium, chloride, sulfate, and bicarbonate concentrations in the solution and M represents the number of aliquots of this particular waste

which should be percolated. Values for all these variables need not be present; however, those that are must be in the following format: the first eight values must be real numbers and each must occupy a card column field eight columns wide beginning with card column 1. The last value to be punched on this card, "M", is an integer which occupies a card column field five columns wide beginning with card column 70; this value must be right adjusted within its card column field. All values punched must be in the order described above; the respective card column fields of those that are not to be punched must be left blank. SEE FORMAT STATEMENT 1140.

The 13th data card contains values for the variables WNO3 (the nitrate concentration in the solution), SRIN (the influent concentration of trace ion being investigated), CASOI (associated calcium sulfate complex in the solution), APH (the pH of the solution), and WFI (the fluoride concentration in the solution). All of these values need not be present, but those that are must follow the format rules of the 12th data card. Again, they must be punched on the card in the order specified, and blank card column fields must be retained. SEE FORMAT STATEMENT 1140.

The 14th data card contains values for the variables ALI (the volume equivalent to one aliquot) and LB (the total number of aliquots to be percolated). These must be present in the following format. The first variable value is punched in exponential notation and occupies a card column field 14 columns wide beginning with card column 1. The second value is an integer and occupies a card column field six columns wide beginning with card column 15. Each value must be right adjusted in its field. SEE FORMAT STATEMENT 1270.

The last card is the FIN card, signifying the end of data input. Sample CASE ONE input data cards and printed output will be found on the following pages.

The first portion of output indicates the options which are being used and the values of the data cards which were used to initialize the program. This allows a check to make sure the cards were correctly read by the computer and leaves a permanent record with the output for future reference.

Further output are the initial and equilibrium values for each soil subdivision for each aliquot of solution percolated through the soil cell.

```

    XQ1      SUPP
  FALSE   FALSE   TRUE    FALSE
  1.23    1.26    .494    2.24    1.15    8.23
        5 529.   .914    100.   6.121E-06
        7.221E-05 5.636E-06 2.670E-04 2.637E+01 2.455E-06
        1.447E-05 3.592E-06 2.570E-04 2.637E+01 1.777E-06
        5.028E-01 3.411E-06 2.570E-04 1.045E-05 6.261E+01
        1.240E-05 2.570E-04 2.637E+01 2.637E+01 3.801E-06
        2.311E-06 3.420E-06 2.570E-04 1.070E-05 3.855E+00
        1.169E-05 2.232E-06 2.570E-04 2.637E+01 1.792E-06
        4.52    152.   10.30  10.30  1.0791E-06
        1.66.82 2.0  +03  7.0   4.97E-03 2
        2.176  E+01  2
        FIN

```

X

THE SOIL COLUMN IS DRY .....  
 THE SOIL PROFILE IS UNIFORM.....  
 PRINT ALL INITIAL AND FINAL VALUES .....

PRINT ALL EQUILIBRIUM VALUES ONLY.....

PRINTED OUTPUT

P1 •123+01	Fk1 •126+01	P2 •494-00	Fk2 •224+01	P3 •115+01	Fk3 •823+01
K 4	JSUB 5	VSOIL •529+03	PURE •914-00	% SAT •100+03	
SAT •2221-04	RP •5636-05	ET •6121-05	CT •2455-05	RSR •0000	

GYP	CAL	B2	CAF	SRS	
- .0000	.2570-03	.2637+02	.1777-05	.6261+02	
SAT	RP	ET	CT	RSR	
.1447-04	.3592-05	.9666-05	.3801-05	-.0000	
GYP	CAL	B2	CAF	SRS	
.5028-06	.2570-03	.2637+02	.1792-05	.3855+01	
SAT	RP	ET	CT	RSR	
.1240-04	.3411-05	.1045-04	.4147-05	-.0000	
GYP	CAL	B2	CAF	SRS	
.2311-05	.2570-03	.2637+02	.1791-05	-.0000	
SAT	RP	ET	CT	RSR	
.1169-04	.3420-05	.1070-04	.4244-05	-.0000	
GYP	CAL	B2	CAF	SRS	
.2232-05	.2570-03	.2637+02	.1791-05	-.0000	
WCA	WG	WNA	WK	WSR	
.45200+01	-.00000	.15200+03	.1n300+02	-.00000	WCL
WNO3	SRIN	CASO1	APH	WCO3	
.16682+03	.20000+04	-.00000	.7n000+01	.49700-02	
ALI	LB				
.2176+02	2				

INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.						COLUMN	1 ALIQUOT	1 SRX	1 CA
	K	NA	MG	MGX	SR				
1.030-02	5.636-06	1.520-01	2.221-05	0.000	2.455-06	0.000	-0.000	2.260-03	
HC03	NO3	SO4	CL	CASO4UN	GYSUM	SR85 SOL	SR85 SOIL	CAL	
4.970-06	1.668-01	0.000	0.000	-0.000	-0.000	2.000+03	6.261+01	2.570-04	
FL	CAF							CAX	
0.000	1.777-06							6.121-06	
EQUILIBRIUM VALUES FOR ALL IONS						COLUMN	1 ALIQUOT	1 SRX	1 CA
	K	NA	MG	MGX	SR				
2.993-03	7.744-06	1.215-01	3.102-05	5.076-03	0.906-07	0.000	-0.000	1.638-02	
HC03	NO3	SO4	CL	SR85 SOL	SR85 SOIL	VOLUME (ML)	COLVOL	C/C0	
4.294-04	1.668-01	0.000	0.000	2.638+01	8.219+01	2.176+01	4.113-02	1.319-02	
PH	KD	CASO4UN	GYSUM	CAL	CAF	FL	B	U	
8.976+00	3.116+00	-0.000	-0.000	2.569-04	1.759-06	1.253-04	3.466+03	4.345-01	
INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.						COLUMN	2 ALIQUOT	1 SRX	CA 2.128-06
	K	NA	MG	MGX	SR				CAX
2.993-03	3.592-06	1.215-01	1.447-05	5.076-03	3.801-06	0.000	-0.000	1.638-02	
HC03	NO3	SO4	CL	CASO4UN	GYSUM	SR85 SOL	SR85 SOIL	CAL	
4.294-04	1.668-01	0.000	0.000	-0.000	5.029-07	2.638+01	3.855+00	2.570-04	
FL	CAF							CAX	
1.253-04	1.792-06							9.666-06	
EQUILIBRIUM VALUES FOR ALL IONS						COLUMN	2 ALIQUOT	1 SRX	1 CA
	K	NA	MG	MGX	SR				
1.854-03	3.921-06	1.012-01	2.032-05	7.372-03	1.138-06	0.000	-0.000	2.596-02	
HC03	NO3	SO4	CL	SR85 SOL	SR85 SOIL	VOLUME (ML)	COLVOL	C/C0	
3.474-04	1.668-01	1.227-03	0.000	1.612+00	4.224+00	2.176+01	4.113-02	8.062-04	
PH	KD	CASO4UN	GYSUM	CAL	CAF	FL	B	U	
8.751+00	2.619+00	5.162-04	0.000	2.570-04	1.795-06	1.013-04	3.466+03	4.520-01	
INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.						COLUMN	3 ALIQUOT	1 SRX	CA 7.239-06
	K	NA	MG	MGX	SR				CAX
1.854-03	3.411-06	1.012-01	1.240-05	7.772-03	4.147-06	0.000	-0.000	2.596-02	
HC03	NO3	SO4	CL	CASO4UN	GYSUM	SR85 SOL	SR85 SOIL	CAL	
3.474-04	1.668-01	1.227-03	0.000	5.162-04	2.311-06	1.612+00	-0.000	2.570-04	
FL	CAF							CAX	
1.013-04	1.791-06							1.045-05	
EQUILIBRIUM VALUES FOR ALL IONS						COLUMN	3 ALIQUOT	1 SRX	CA --- CAX
	K	NA	MG	MGX	SR				

	<b>2.202-03</b>	<b>3.310-06</b>	<b>9.549-02</b>	<b>1.404-05</b>	<b>A.264-03</b>	<b>3.890-06</b>	<b>0.000</b>	<b>-0.000</b>	<b>3.300-02</b>	<b>9.936-06</b>
HC03	NO3	SO4	CL	SR85	SOL	SR85	SOL	VOLUME (ML)	COLVOL	C/C0
3.160-04	1.668-01	6.501-03	0.000	1.P43-02	3.844-02	2.176+01	4.113-02			9.217-06
PH	KD	CAS04UN	GYPSUM	CAL	CAF	FL	B			U
	<b>8.638+00</b>	<b>2.085+00</b>	<b>3.252-03</b>	<b>0.000</b>	<b>2.570-04</b>	<b>1.792-06</b>	<b>9.218-05</b>	<b>3.466+03</b>	<b>4.775-01</b>	
<b>INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.</b>										
K	KX	NA	NAX	MG	MGX	SR	SRX		CA	CAX
2.202-03	3.420-06	9.549-02	1.169-05	8.264-03	4.244-06	0.000	-0.000		3.300-02	1.070-05
HC03	NO3	SO4	CL	CAS04UN	GYPSUM	SR85	SOL	SR85	SOL	CAL
3.160-04	1.668-01	6.501-03	0.000	3.252-03	2.232-06	1.843-02	-0.000		2.570-04	
FL	CAF									
	<b>9.218-05</b>	<b>1.791-06</b>								

	<b>EQUILIBRIUM VALUES FOR ALL IONS</b>	<b>COLUMN</b>	<b>4 ALIQUOT</b>	<b>1</b>	<b>SR</b>	<b>SRX</b>	<b>CA</b>	<b>CAX</b>		
K	KX	NA	NAX	MG	MGX	SR	SRX	CA		
2.569-03	3.314-06	9.396-02	1.213-05	8.766-03	4.099-06	0.000	-0.000	3.585-02		
HC03	NO3	SO4	CL	SR85	SOL	SR85	SOL	C/C0		
3.065-04	1.668-01	9.282-03	0.000	2.959-04	5.485-04	2.176+01	4.113-02	1.479-07		
PH	KD	CAS04UN	GYPSUM	CAL	CAF	FL	B	U		
	<b>8.600+00</b>	<b>1.854+00</b>	<b>4.897-03</b>	<b>9.551-07</b>	<b>2.570-04</b>	<b>1.791-06</b>	<b>8.942-05</b>	<b>3.466+03</b>		
<b>INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.</b>										
K	KX	NA	NAX	MG	MGX	SR	SRX	CA	CAX	
1.030-02	7.744-06	1.520-01	3.102-05	0.000	0.906-07	0.000	-0.000	2.260-03	2.128-06	
HC03	NO3	SO4	CL	CAS04UN	GYPSUM	SR85	SOL	SR85	SOL	
4.970-06	1.668-01	0.000	0.000	-0.000	-0.000	2.000+03	8.219+01		2.569-04	
FL	CAF									
	<b>0.000</b>	<b>1.759-06</b>								

	<b>EQUILIBRIUM VALUES FOR ALL IONS</b>	<b>COLUMN</b>	<b>1 ALIQUOT</b>	<b>2</b>	<b>SR</b>	<b>SRX</b>	<b>CA</b>	<b>CAX</b>		
K	KX	NA	NAX	MG	MGX	SR	SRX	CA		
3.937-03	9.580-06	1.406-01	3.432-05	2.P15-03	1.785-07	0.000	-0.000	8.721-03		
HC03	NO3	SO4	CL	SR85	SOL	SR85	SOL	C/C0		
5.809-04	1.668-01	0.000	0.000	4.143+01	1.401+02	4.352+01	8.227-02	2.072-02		
PH	KD	CAS04UN	GYPSUM	CAL	CAF	FL	B	U		
	<b>9.287+00</b>	<b>3.382+00</b>	<b>-0.000</b>	<b>2.569-04</b>	<b>1.734-06</b>	<b>1.695-04</b>	<b>3.466+03</b>	<b>4.232-01</b>		
<b>INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.</b>										
K	KX	NA	NAX	MG	MGX	SR	SRX	CA	CAX	
3.937-03	3.921-06	1.406-01	2.032-05	2.P15-03	3.138-06	0.000	-0.000	8.721-03	7.239-06	
HC03	NO3	SO4	CL	CAS04UN	GYPSUM	SR85	SOL	SR85	SOL	
5.809-04	1.668-01	0.000	0.000	-0.000	0.000	4.143+01	4.224+00		2.570-04	
FL	CAF									
	<b>1.695-04</b>	<b>1.795-06</b>								

EQUILIBRIUM VALUES FOR ALL IONS							COLUMN		2 ALIQUOT		2	
K	KX	NA	NA	NA	MG	MGX	SR	SRX	CA	CAX		
1.665-03	4.576-06	1.122-01	2.840-05	6.781-03	1.994-06	0.000	-0.000	1.993-02	3.970-06			
HC03	NO3	SO4	CL	SR85	SOL	SR85	SOIL	VOLUME (ML)	COLVOL	C/CO		
3.917-04	1.668-01	0.000	0.000	1.789+00	5.346+00	4.352+01	8.227-02	8.944-04	U			
PH	KD	CASO4UN	GYSUM	CAL	CAF	FL	B					
8.880+00	2.989+00	-0.000	0.000	2.570-04	1.803-06	1.143-04	3.466+03	4.405-01				
INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.							3 ALIQUOT	2	SRX	CA		
K	KX	NA	NA	MG	MGX	SR	SRX	CA	CAX			

EQUILIBRIUM VALUES FOR ALL IONS							COLUMN		2 ALIQUOT		2	
K	KX	NA	NA	NA	MG	MGX	SR	SRX	CA	CAX		
1.665-03	3.310-06	1.122-01	1.404-05	6.781-03	3.890-06	0.000	-0.000	1.993-02	9.936-06			
HC03	NO3	SO4	CL	CASO4UN	GYSUM	SR85	SOL	SR85	SOL	CAL		
3.917-04	1.668-01	0.000	0.000	-0.000	0.000	1.789+00	3.844-02	2.570-04	2.570-04			
FL	CAF											
INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.							3 ALIQUOT	2	SRX	CA		
K	KX	NA	NA	NA	MG	MGX	SR	SRX	CA	CAX		

EQUILIBRIUM VALUES FOR ALL IONS							COLUMN		2 ALIQUOT		2	
K	KX	NA	NA	NA	MG	MGX	SR	SRX	CA	CAX		
1.646-03	3.316-06	9.716-02	1.840-05	7.793-03	3.598-06	0.000	-0.000	2.644-02	8.049-06			
HC03	NO3	SO4	CL	SR85	SOL	SR85	SOIL	VOLUME (ML)	COLVOL	C/CO		
3.432-04	1.668-01	0.000	0.000	4.643-02	1.217-01	4.352+01	8.227-02	2.321-05	U			
PH	KD	CASO4UN	GYSUM	CAL	CAF	FL	B					
8.741+00	2.622+00	-0.000	0.000	2.570-04	1.794-06	1.001-04	3.466+03	4.489-01				
INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.							4 ALIQUOT	2	SRX	CA		
K	KX	NA	NA	NA	MG	MGX	SR	SRX	CA	CAX		
1.646-03	3.314-06	9.716-02	1.213-05	7.793-03	4.090-06	0.000	-0.000	2.644-02	1.068-05			
HC03	NO3	SO4	CL	CASO4UN	GYSUM	SR85	SOL	SR85	SOL	CAL		
3.432-04	1.668-01	0.000	0.000	-0.000	0.551-07	4.643-02	5.485-04	2.570-04				
FL	CAF											
INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.							4 ALIQUOT	2	SRX	CA		
K	KX	NA	NA	NA	MG	MGX	SR	SRX	CA	CAX		

EQUILIBRIUM VALUES FOR ALL IONS							COLUMN		2 ALIQUOT		2	
K	KX	NA	NA	NA	MG	MGX	SR	SRX	CA	CAX		
2.096-03	3.185-06	9.191-02	1.364-05	7.92-03	4.042-06	0.000	-0.000	3.085-02	1.004-05			
HC03	NO3	SO4	CL	SR85	SOL	SR85	SOIL	VOLUME (ML)	COLVOL	C/CO		
3.217-04	1.668-01	2.225-03	0.000	9.30-04	2.250-03	4.352+01	8.227-02	4.915-07	U			
PH	KD	CASO4UN	GYSUM	CAL	CAF	FL	B					
8.667+00	2.289+00	1.085-03	0.000	2.570-04	1.792-06	9.386-05	3.466+03	4.612-01				
INITIAL CONDITIONS AFTER SOLUTION DISSOLVES SOLUBLE.							4 ALIQUOT	2	SRX	CA		
K	KX	NA	NA	NA	MG	MGX	SR	SRX	CA	CAX		

### CASE TWO (DRY SOIL)

For Case Two the first, second and third data cards are the same as those described in Case One; refer to Case One for their format descriptions.

The variables on the fourth data card represent the amount of calcium, magnesium, sodium, potassium, strontium, chloride, sulfate and bicarbonate in the B11 soil extracts. These values may be in real or exponential form and may or may not be present. Each value occupies a card column field eight columns wide and all exponential notations must be right justified within the card column field. Zero variables may have blank card column fields. The variables must be punched in the order listed above. SEE FORMAT STATEMENT 1140.

The fifth data card contains values for the variables SONO3, EC, CAL, B11, B2, GYP, SRF, AND CAF, representing the nitrate in the B11 extract, cation exchange capacity, calcium carbonate in soil, % moisture at which soil extract was run, % moisture of a saturated soil column, calcium sulfate in soil, initial concentration of trace ion sorbed on soil and amount of calcium fluoride present in soil. The format is identical to that of the previous card. Variables EC, B11 and B2 must be present but the other variables may or may not be present. SEE FORMAT STATEMENT 1140.

Since the soil is designated as uniform, no further dry soil data cards are needed. If the soil is nonuniform, as in Case One, a set of data cards containing the same variables as cards four and five above would be present for each soil cell. Two x K gives the number of dry soil cards needed in the general non-uniform case.

In this uniform case, one set of data cards is present and the computer automatically generates the data for the remaining uniform soil cells.

The sixth, seventh and eighth data cards represent the waste solution data. The description is the same as for Case One. SEE FORMAT STATEMENTS 1140 and 1270. Again, only one waste solution was run, thus only one set of waste solution data cards is present. The last card is a FIN card to signify the end of input data cards. Sample Case Two input data cards and printed output follow.

```

! XQ1 SEP
TRUE   TRUF    FALSE   FALSE
1.23   1.26    .494    .914
      5      529    100.
      10     5731   27.97
      11.94  2.731   1.157
      29.13  4.5    -0.2257 -0.04
      4.52   152.    10.30
      166.82 2.0    +03
      2.176  E+01   16
      FIN
      X

```

THE SOIL COLUMN IS DRY .....

THE SOIL PROFILE IS UNIFORM.....

PRINT ALL INITIAL AND FINAL VALUES .....

PRINT ALL EQUILIBRIUM VALUES ONLY.....

T PRINTED OUTPUT

T T

F F

F F

P1	FK1	P2	FK2	P3	FK3
.123+01	.126+01	.494-00	.224+01	.115+01	.823+01
K	JSUB	VSOIL	PORE	% SAT	
10	5	.529+03	.914-00	.100+03	
SOCa	SOMG	SOMA	SOK	SOSR	SOC L
.11940+02	.57310+01	.27970+02	.11570+01	-.000000	-.00000
SONO3	EC	CAL	B11	B2	GYP
.29130+02	.45000-01	.25700-03	.10000+03	.26370+02	.31200-06
SRS	CAF				
					-.00000

WCA  
•45200+01  
WMG  
•00000

WN03  
•16682+03  
SRIN  
•20000+04  
CASOI  
•00000  
WK  
•1n300+02  
APH  
•7n000+01

ALI  
LB  
16  
•2176+02

EQUILIBRIUM VALUES FOR ALL IONS  
K KX  
9.690-03 5.725-06 5.222-01 2.934-05 1.440-01 2.061-06 0.000 -0.000  
HC03 NO3 SO4 CL SR85 SOL SR85 SOIL VOLUME (ML) COLVOL  
7.920-05 1.271-00 5.191-04 0.000 5.204-13 5.264-12 2.176+01 4.113-02 2.602-16  
PH KD CASO4UN GYPSUM CAL CAF FL B U  
7.436+00 1.011+01 4.897-03 6.098-06 2.570-04 -0.000 0.000 3.466+03 1.364+00

EQUILIBRIUM VALUES FOR ALL IONS  
K KX  
2.357-03 5.725-06 1.273-01 2.940-05 1.136-02 2.022-06 0.000 -0.000  
HC03 NO3 SO4 CL SR85 SOL SR85 SOIL VOLUME (ML) COLVOL  
3.895-04 1.668-01 1.504-02 0.000 1.472-07 3.872-07 4.352+01 8.227-02 7.362-11

PH KD CASO4UN GYPSUM CAL CAF FL B U  
8.835+00 2.630+00 4.897-03 6.098-06 2.570-04 -0.000 0.000 3.466+03 4.962-01  
EQUILIBRIUM VALUES FOR ALL IONS  
K KX  
2.357-03 5.726-06 1.277-01 2.947-05 1.064-02 1.932-06 0.000 -0.000  
HC03 NO3 SO4 CL SR85 SOL SR85 SOIL VOLUME (ML) COLVOL  
3.866-04 1.668-01 1.481-02 0.000 1.640-06 4.273-06 6.528+01 1.234-01 8.201-10  
PH KD CASO4UN GYPSUM CAL CAF FL B U  
8.829+00 2.605+00 4.897-03 6.088-06 2.570-04 -0.000 0.000 3.466+03 4.950-01  
EQUILIBRIUM VALUES FOR ALL IONS  
K KX  
2.357-03 5.725-06 1.282-01 2.959-05 0.501-03 1.791-06 0.000 -0.000

WN04  
-0.00000

WHC03  
•49700-02

CAX  
2.904-06  
CA  
3.150-01  
C/CO  
CAX  
CA  
3.150-01  
C/CO  
CAX  
CA  
3.053-06

EQUILIBRIUM VALUES FOR ALL IONS		K	NO3	S04	CL	SR85	SOL	SR85	SOIL	VOLUME (ML)	COLVOL	C/CO
3.822-04		1.668-01	1.447-02	0.000	1.126-05	2.634-05	8.704+01	1.645-01	1.645-01	5.130-09	5.130-09	
PH		KD	CAS04UN	GYSUM	CAL	CAL	FL	FL	B	U	C/CO	
8.818+00		2.568+00	4.897-03	6.832-06	2.570-04	-0.000	0.000	3.466+03	4.933-01	4.933-01	CAX	
EQUILIBRIUM VALUES FOR ALL IONS		COLMN	10 ALIQUOT	5	MGX	SR	SRX	SRX	CA 3.142-06	CA 3.142-06		
K		KX	NA	NAX	MG	MGX	SR	SRX	SRX	2.373-02	2.373-02	
2.353-03		5.724-06	1.290-01	2.977-05	8.272-03	1.600-06	0.000	-0.000	-0.000	2.348-08	2.348-08	
HC03		NO3	S04	CL	SR85	SOL	SR85	SOIL	VOLUME (ML)	COLVOL	COLVOL	C/CO
3.774-04		1.668-01	1.409-02	0.000	4.695-05	1.185-04	1.088+02	2.057-01	B	U	8.652-08	8.652-08
PH		KD	CAS04UN	GYSUM	CAL	CAL	FL	FL	B	U	4.914-01	4.914-01
8.807+00		2.524+00	4.897-03	6.794-06	2.570-04	-0.000	0.000	3.466+03	4.914-01	4.914-01	CAX	
EQUILIBRIUM VALUES FOR ALL IONS		COLMN	10 ALIQUOT	6	MG	MGX	SR	SRX	SRX	CA 3.206-06	CA 3.206-06	
K		KX	NA	NAX	MG	MGX	SR	SRX	SRX	2.420-02	2.420-02	
2.344-03		5.721-06	1.300-01	3.006-05	6.046-03	1.402-06	0.000	-0.000	-0.000	8.652-08	8.652-08	
HC03		NO3	S04	CL	SR85	SOL	SR85	SOIL	VOLUME (ML)	COLVOL	COLVOL	C/CO
3.730-04		1.668-01	1.375-02	0.000	1.730-04	4.293-04	1.306+02	2.468-01	B	U	4.879-01	4.879-01
PH		KD	CAS04UN	GYSUM	CAL	CAL	FL	FL	B	U	4.895-01	4.895-01
8.796+00		2.481+00	4.897-03	6.765-06	2.570-04	-0.000	0.000	3.466+03	4.895-01	4.895-01	CAX	
EQUILIBRIUM VALUES FOR ALL IONS		COLMN	10 ALIQUOT	7	MG	MGX	SR	SRX	SRX	CA 3.213-06	CA 3.213-06	
K		KX	NA	NAX	MG	MGX	SR	SRX	SRX	2.454-02	2.454-02	
2.326-03		5.715-06	1.314-01	3.049-05	5.695-03	1.182-06	0.000	-0.000	-0.000	7.274-07	7.274-07	
HC03		NO3	S04	CL	SR85	SOL	SR85	SOIL	VOLUME (ML)	COLVOL	COLVOL	C/CO
3.699-04		1.668-01	1.350-02	0.000	5.383-04	1.316-03	1.523+02	2.879-01	B	U	1.397-01	1.397-01
PH		KD	CAS04UN	GYSUM	CAL	CAL	FL	FL	B	U	4.879-01	4.879-01
8.789+00		2.445+00	4.897-03	6.758-06	2.570-04	-0.000	0.000	3.466+03	4.879-01	4.879-01	CAX	
EQUILIBRIUM VALUES FOR ALL IONS		COLMN	10 ALIQUOT	8	MG	MGX	SR	SRX	SRX	CA 3.144-06	CA 3.144-06	
K		KX	NA	NAX	MG	MGX	SR	SRX	SRX	2.469-02	2.469-02	
2.305-03		5.709-06	1.332-01	3.100-05	4.433-03	0.581-07	0.000	-0.000	-0.000	1.397-01	1.397-01	
HC03		NO3	S04	CL	SR85	SOL	SR85	SOIL	VOLUME (ML)	COLVOL	COLVOL	C/CO
3.683-04		1.668-01	1.338-02	0.000	1.455-03	3.512-03	1.741+02	3.291-01	B	U	1.749-06	1.749-06
PH		KD	CAS04UN	GYSUM	CAL	CAL	FL	FL	B	U	4.864-01	4.864-01
8.786+00		2.419+00	4.897-03	6.777-06	2.570-04	-0.000	0.000	3.466+03	4.864-01	4.864-01	CAX	
EQUILIBRIUM VALUES FOR ALL IONS		COLMN	10 ALIQUOT	9	MG	MGX	SR	SRX	SRX	CA 3.011-06	CA 3.011-06	
K		KX	NA	NAX	MG	MGX	SR	SRX	SRX	2.466-02	2.466-02	
2.279-03		5.702-06	1.353-01	3.179-05	3.465-03	7.404-07	0.000	-0.000	-0.000	1.397-01	1.397-01	
HC03		NO3	S04	CL	SR85	SOL	SR85	SOIL	VOLUME (ML)	COLVOL	COLVOL	C/CO
3.681-04		1.668-01	1.336-02	0.000	3.497-03	8.398-03	1.958+02	3.702-01	B	U	1.749-06	1.749-06

	PH	KD	CASO4UN	GYPSUM	CAL	CAF	FL	B	U
8.786+00	2.401+00	4.397-03	6.820-06	2.570-04	-0.000	0.000	3.466+03	4.0852-01	CAX
EQUILIBRIUM VALUES FOR ALL IONS COLUMN									
K	KX	NA	NAX	MG	SR	SRX	SRX	CA 2.818-06	
2.254-03	5.696-06	1.376-01	3.250-05	2.579-03	5.463-07	0.000	-0.000	2.443-02	
HCO3	NO3	SO4	CL	SR85	SOL	SR85	VOLUME (ML)	COLVOL	C/CO
3.695-04	1.668-01	1.345-02	0.000	7.591-03	1.818-02	2.176+02	4.113-01	3.796-06	
PH	KD	CASO4UN	GYPSUM	CAL	CAF	FL	B	U	
8.790+00	2.394+00	4.897-03	6.887-06	2.570-04	-0.000	0.000	3.466+03	4.0843-01	CAX
EQUILIBRIUM VALUES FOR ALL IONS COLUMN									
K	KX	NA	NAX	MG	SR	SRX	SRX	CA 2.568-06	
2.231-03	5.689-06	1.406-01	3.341-05	1.639-03	3.839-07	0.000	-0.000	2.400-02	
HCO3	NC3	SO4	CL	SR85	SOL	SR85	VOLUME (ML)	COLVOL	C/CO
3.727-04	1.663-01	1.368-02	0.000	1.506-02	3.610-02	2.394+02	4.525-01	7.528-06	
PH	KD	CASO4UN	GYPSUM	CAL	CAF	FL	B	U	
8.799+00	2.398+00	4.897-03	6.978-06	2.570-04	-0.000	0.000	3.466+03	4.0838-01	CAX
EQUILIBRIUM VALUES FOR ALL IONS COLUMN									
K	KX	NA	NAX	MG	SR	SRX	SRX	CA 2.279-06	
2.211-03	5.676-06	1.438-01	3.426-05	1.248-03	2.540-07	0.000	-0.000	2.337-02	
HCO3	NO3	SO4	CL	SR85	SOL	SR85	VOLUME (ML)	COLVOL	C/CO
3.776-04	1.668-01	1.404-02	0.000	2.753-02	6.635-02	2.611+02	4.936-01	1.377-05	
PH	KD	CASO4UN	GYPSUM	CAL	CAF	FL	B	U	
8.812+00	2.410+00	4.897-03	7.033-06	2.570-04	-0.000	0.000	3.466+03	4.0837-01	CAX
EQUILIBRIUM VALUES FOR ALL IONS COLUMN									
K	KX	NA	NAX	MG	SR	SRX	SRX	CA 2.196-06	
2.175-03	5.614-06	1.452-01	3.465-05	7.023-04	1.700-07	0.000	-0.000	2.324-02	
HCO3	NO3	SO4	CL	SR85	SOL	SR85	VOLUME (ML)	COLVOL	C/CO
3.786-04	1.668-01	1.410-02	0.000	4.612-02	1.111-01	2.829+02	5.347-01	2.309-05	
PH	KD	CASO4UN	GYPSUM	CAL	CAF	FL	B	U	
8.815+00	2.406+00	4.897-03	1.552-06	2.570-04	-0.000	0.000	3.466+03	4.0832-01	CAX
EQUILIBRIUM VALUES FOR ALL IONS COLUMN									
K	KX	NA	NAX	MG	SR	SRX	SRX	CA 7.522-07	
2.004-03	5.633-06	1.470-01	3.773-05	5.030-04	5.470-08	0.000	-0.000	1.307-02	
HCO3	NO3	SO4	CL	SR85	SOL	SR85	VOLUME (ML)	COLVOL	C/CO
4.857-04	1.668-01	4.413-03	0.000	5.099-02	1.555-01	3.046+02	5.759-01	2.550-05	
PH	KD	CASO4UN	GYPSUM	CAL	CAF	FL	B	U	
9.090+00	3.051+00	9.654-04	0.000	2.571-04	-0.000	0.000	3.466+03	4.0406-01	

EQUILIBRIUM VALUES FOR ALL IONS						COLUMN	10 ALIQUOT	15	
K	KX	NA	NAX	M6Y	SR	SRX	CAX	9.356-08	
2.035-03	5.651-06	1.551-01	3.914-05	2.091-04	8.529-09	0.000	-0.000	5.012-03	
HC03	NO3	S04	CL	SR85 SOL SR85 SOIL	VOLUME (ML)	COLVOL	C/CO		
7.597-04	1.668-01	0.000	0.000	5.853-02	2.016-01	3.264+02	6.170-01	2.926-05	
PH	KD	CASO4UN	GYSUM	CAL	CAF	FL	B	U	
9.562+00	3.445+00	-0.000	0.000	2.571-04	-0.000	0.000	3.466+03	4.157-01	
EQUILIBRIUM VALUES FOR ALL IONS						COLUMN	10 ALIQUOT	16	
K	KX	NA	NAX	M6X	SR	SRX	CAX		
2.089-03	5.657-06	1.597-01	3.928-05	2.018-05	7.969-10	0.000	-0.000	2.980-03	
HC03	NO3	S04	CL	SR85 SOL SR85 SOIL	VOLUME (ML)	COLVOL	C/CO		
9.825-04	1.668-01	0.000	0.000	4.476-02	2.349-01	3.482+02	6.581-01	2.238-05	

CAX  
2.921-08

PH	KD	CASO4UN	GYSUM	CAL	CAF	FL	B	U
9.821+00	5.248+00	-0.000	0.000	2.571-04	-0.000	0.000	3.466+03	4.133-01

## APPENDIX C

FORTRAN IV LISTING  
OF PERCOL, DIST, NEWTIT

' RUN,S 8,CUR594,,RJS, 80,5000

FR5 SEP

JEFF SERNE SEP PROGRAM

C SOIL EQUILIBRIUM PROGRAM

```
DIMENSION CHCO3(120),CN03(20),SRSS(20,50),CALL(20),GYPP(20)
DIMENSION CSNA(20),CSMG(20),CSCA(20),CSSR(20),CCL(20),CSO4(20)
DIMENSION CNA(20),CK(20),CMG(20),CCA(20),CSR(20),CSK(20)
DIMENSION BR1(20),BB2(20),CAFF(20)
DIMENSION XNR(10),FXR(10)
COMMON F,ET,B,S,AP,SAT,CT,RP,A,HCO3,FL
REAL TSOLF
LOGICAL DRY,UNI,PRINT,PRI
RFAD-(5,1150) DRY,UNI,PRINT,PRI
WRITE (6,1160) DRY
WRITE (6,1170) UNI
WRITE (6,1180) PRINT
WRITE (6,1190) PRT
READ (5,1200) P1,FK1,P2,FK2,P3,FK3
WRITE (6,1210) P1,FK1,P2,FK2,P3,FK3
READ (5,1220) K,JSUB,VSOIL,PORE,B3
WRITE-(6,1230) K,JSUB,VSOIL,PORE,B3
LL=0
J=0
AKD=0.0
AAPH=0.0
ISOL=1
TMAX=1
IF ((NOT.DRY) GO TO 150
READ(5,1140) SOCA,SONG,SONA,OK,SOSR,SOCL,SOCR,SOSO4,SOHC03
WRITE (6,1090) SOCA,SONG,SONA,SOK,SOSR,SOCL,SOCR,SOSO4,SOHC03
RFAD(15,1140) SONO3,EC,CAL,B11,B2,GYP,SRS,CAF
WRITE (6,1100) SONO3,EC,CAL,B11,B2,GYP,SRS,CAF
TA=K
R1=B11
R=B2
SOCA=SOCA*B1/B
SONG=SONG*B1/B
SONA=SONA*B1/B
SOK=SOK*B1/B
SOSR=SOSR*B1/B
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SOCCL=SOCCL*B1/B
SOS04=SOS04*B1/B
SOHC03=SOHC03*B1/B
SON03=SON03*B1/B
1F-T•NOT•UNIT GO TO 120
IA=0
IA=IA+1
120 J=J+1
      SEP 31
      SEP 32
      SEP 33
      SEP 34

SAR=SONA/SQRT((SOCA+SOMG)/2.)
ESP=0.01475*SAR/(1.+0.01475*SAR)
CNA(J)=ESP*EC
PAR=SQR(SQRT((SOCA+SOMG)/2.))
FPP=(0.0360+0.1051*PAR)/(1.+(0.0360+0.1051*PAR))
CK(J)=EPP*EC
ZE=EC-CK(J)-CNA(J)
IF((SOMG.EQ.0.0) CMG(J)=0.0
IF((SOMG.EQ.0.0) GO TO 130
RA=SOCA/(SOMG*(0.625))
CMG(J)=ZE/(RA+1.)
130 CK(J)=CMG(J)+ZE
CSR(J)=CCA(J)*SOSR/(1.3*SOCA)
CNA(J)=CNA(J)/1000.
CK(J)=CK(J)/1000.
CMG(J)=CMG(J)/2000.
CCA(J)=CCA(J)/2000.
CSR(J)=CSR(J)/1000.
CSNA(J)=SONA/1000.
CSK(J)=SOK/1000.
CSMG(J)=SOMG/2000.
CSCA(J)=SOCA/2000.
CSSR(J)=SOSR/2000.
J1=0
      SEP 35
      SEP 36
      SEP 37
      SEP 38
      SEP 39
      SEP 40
      SEP 41
      SEP 42
      SEP 43
      SEP 44
      SEP 45
      SEP 46
      SEP 47
      SEP 48
      SEP 49
      SEP 50
      SEP 51
      SEP 52
      SEP 53
      SEP 54
      SEP 55
      SEP 56
      SEP 57
      SEP 58
      SEP 59
      SEP 60
      SEP 61
      SEP 62
CONTINUE
DO 140 LBJ=1,JSUB
J1=J1+1
SPSS(J,J1)=SPSS

```

```

CCL(J)=SOC(L/1000.
      C504 RJY=5050472000.
      CHCO3(J)=50HC03/1000.
      CNO3(J)=SONO3/1000.
      CALL(J)=CAL
      GYPP(J)=GYP
      CAF(F(J)=CAF
      RRTT(J)=BIT
      RR2(J)=R2
      IF (IA.NE.K) GO TO 110
      IF (J.LT.K) GO TO 100
      J=0
      L=1
      GO TO 200
150  READ(5,1260) SAT,RP,FT,CT,RSR
      WRITE(6,1240) SAT,RP,FT,CT,RSR
      READ(5,1260) GYP,CAL,R2,CAF,SRS
      WRITE(6,1250) GYP,CAL,R2,CAF,SRS
      IA=K
      IF (1.NOT.NE1) GO TO 170
      IA=0
      160  IA=IA+1
      J=J+1
      GYPP(J)=GYP
      RR1(J)=B2
      BR2(J)=B2
      CSRT(J)=RSR
      CMG(J)=CT
      CCA(J)=ET
      CALL(J)=CAL
      CK(J)=RP
      J1=0
      DO 180 LBJ=1,JSUB
      J1=J1+1
      SRSS(J,J1)=SRS
      180  CONTINUE
      SEP 63
      SEP 64
      SEP 65
      SEP 66
      SEP 68
      SEP 69
      SEP 70
      SEP 71
      SEP 72
      SEP 73
      SEP 74
      SEP 75
      SEP 76
      SEP 77
      SEP 78
      SEP 79
      SEP 80
      SEP 81
      SEP 82
      SEP 83
      SEP 84
      SEP 85
      SEP 86
      SEP 87
      SEP 88
      SEP 89
      SEP 90
      SEP 91
      SEP 93
      SEP 94
      SEP 95
      SEP 96
      SEP 97
      SEP 98

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```

CNA(J)=SAT
CAFF(J)=CAF
R=BB2(J)
----- SEP 99
----- SEP 100
----- SEP 101
----- SEP 102
----- SEP 103
----- SEP 104
----- SEP 105
----- SEP 106
----- SEP 107
----- SEP 108
----- SEP 109
----- SEP 110
----- SEP 111
----- SEP 112
----- SEP 113
----- SEP 114
----- SEP 115
----- SEP 116
----- SEP 117
----- SEP 118
----- SEP 119
----- SEP 120
----- SEP 121
----- SEP 122
----- SEP 123
----- SEP 124
----- SEP 125
----- SEP 126
----- SEP 127
----- SEP 128
----- SEP 129
----- SEP 130
----- SEP 131

```

IF (IA.NE.K) GO TO 160  
 TF-TJ.TT.RY GO TO 150  
 J=0  
 L=2  
 GO TO 200  
190 IF (M.NE.L) GO TO 220  
 READ (5,1140) WCA,WMG,WNA,WK,WSR,WCL,WSO4,WHCO3,M  
 WRITF(5,1110) WCA,WMG,WNA,WK,WSR,WCL,WSO4,WHCO3,M  
 RFAD (5,1140) WNO3,SRIN,CASOI,APH,WFL  
 WRITE(5,1120) WNO3,SRIN,CASOT,APH  
 READ (5,1270) ALI,LB  
 WRITE(5,1280) ALT,LB  
 J=J+1  
 IF TC=1) 230,230,210  
 210 WCA=WCA/2000.  
 WMG=WMG/2000.  
 WSR=WSR/2000.  
 WSO4=WSO4/2000.  
 WNA=WNA/1000.  
 WK=WK/1000.  
 WHCO3=WHCO3/1000.  
 WCL=WCL/1000.  
 WNO3=WNO3/1000.  
 WFL=WFL/1000.  
 A=WCA  
 F=WMG  
 S=WNA  
 ASR=WSR  
 AP=WK  
 HC03=WHCO3  
 H=WCL

$G = WSO_4$   
 $A_N = WNO_3$   
 $F_L = WF_L$   
 $R_1 = BB1(J)$   
 $R = BB2(J)$   
 $CASO = CASOI$   
 $SR = SRIN$   
 $G_O TO 240$   
 $A = WCA$   
 $F = WMG$   
 $S = WNA$   
 $\overline{ASR} = WSR$   
 $AP = WK$   
 $HCO_3 = WHCO_3$   
 $H = WCL$   
 $C = WSO_4$   
 $A_N = WNO_3$   
 $F_L = WF_L$   
 $J = J + 1$   
 $R_1 = BB1(J)$   
 $R = BB2(J)$   
 $CASO = CASOI$   
 $SR = SRIN$   
 $G_O TO 240$   
 $WCA = WCA / 2000.$   
 $WMG = WMG / 2000.$   
 $WNA = WNA / 1000.$   
 $WK = WK / 1000.$   
 $WSR = WSR / 2000.$   
 $WNO_3 = WNO_3 / 1000.$   
 $WHCO_3 = WHCO_3 / 1000.$   
 $WSO_4 = WSO_4 / 2000.$   
 $WCL = WCL / 1000.$   
 $WF_L = WF_L / 1000.$   
 $B_1 = BB1(J)$   
 $R = BB2(J)$   
 $H = WCL + CCL(J) * 100. / B_3$

$SEP 132$   
 $SEP 133$   
 $SEP 134$   
 $SEP 135$   
 $SEP 136$   
 $SEP 137$   
 $SEP 138$   
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 $SEP 140$   
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 $SEP 142$   
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 $SEP 155$   
 $SEP 156$   
 $SEP 157$   
 $SEP 158$   
 $SEP 159$   
 $SEP 160$   
 $SEP 161$   
 $SEP 162$   
 $SEP 163$   
 $SEP 164$   
 $SEP 165$   
 $SEP 166$   
 $SEP 167$   
 $SEP 168$

```

G=WS04+C$04*(J)*100./B3          SEP 169
AN=WNO3+CN03(J)*100./B3          SEP 170
HCO3=WHCO3+CHCO3(J)*100./B3      SEP 171
AP=WK +CSK (J)*100./B3           SEP 172
ASR=WSR+CSSR(J)*100./B3          SEP 173
S =WNA+CSNA(J)*100./B3           SEP 174
F=WMG+CSMG(J)*100./B3           SEP 175
A =WCA+CSCA(J)*100./B3           SEP 176
FL=FL
CASO=CASO1                         SEP 177
SRESRTN                           SEP 178
                                         SEP 179
                                         SEP 180
                                         SEP 181
                                         SEP 182
                                         SEP 183
                                         SEP 184
                                         SEP 185
                                         SEP 186
                                         SEP 187
                                         SEP 188
                                         SEP 189
                                         SEP 190
                                         SEP 191
                                         SEP 192
                                         SEP 193
                                         SEP 194
                                         SEP 195
                                         SEP 196
                                         SEP 197
                                         SEP 198
                                         SEP 199
                                         SEP 200
                                         SEP 201
                                         SEP 202
                                         SEP 203
240   XXT=GYP(J)
R=1.0E+05*PORE/(B*B3/100.)
RSR=CSR(J)
CT=CMG(J)
FT=CCAT(J)
CAL=CALL(J)
RP=CKT(J)
SRS=SRSS(J,JSUR)
SAT=CNAT(J)
CAF=CAFF(J)
IF (PRINT.OR.PRI.AND.J.EQ.K) WRITE (6,1360) J,ISOL
IF (PRINT.OR.PRI.AND.J.EQ.K) WRITE (6,1380)
IF (PRINT.OR.PRIT.AND.J.EQ.K) WRITE (6,1370)
1SR,A,ET
TF (PRINT.OR.PRI.AND.J.EQ.K) WRITE (6,1290)
IF (PRINT.OR.PRI.AND.J.EQ.K) WRITE (6,1370) HCO3,AN,G,H,CASO,XXT,SSEP
1RS,CAF
IF (PRINT.OR.PRI.AND.J.EQ.K) WRITE (6,1300)
IF (PRINT.OR.PRIT.AND.J.EQ.K) WRITE (6,1370) FL,CAF
250   A11=A
IF (XXT) 260,260,270
260   U=SQRT(2.0*(A+F+G+ASR)+0.5*(S+H+HCO3+AP+AN+FL))
      AT=EXP(-9.366*(U/(U+1.)-2*U*U))
      IF (2.4E-5-A*G*AA) 270,330,330

```

```

270 X=0.0
U=SQRT(2.0*(A+F+G+ASR)+0.5*(S+H+HCO3+AP+AN+FL))
BR=A+G
FX=(2.366*(U/(1.+U))-2*U*U)
CC=A*G-(2.4E-5)*EXP(EX)
R=SQRT((BB*BR-4.0*CC))
X=T-RB+R)/2.0
CAS1=4.897E-3-CASO
DFL=R*XXT-CAS1
IF (DEL-X) 280,360,360
X=XXT*B
XXT=0.0
CAS1=0.0
A=A+X
G=G+X
G=SQRT(2.0*(A+F+G+ASR)+0.5*(S+H+HCO3+AP+AN+FL))
AA=EXP(-9.366*(U/(U+1.))-2*U*U)
BR=-(4.9E-03+AA*AA*G)
CC=AA*A*G-4.9E-3*CASO
XXXX=BR*BR-4.0*AA*CC
IF (XXX) 300,300,310
X1=0.0
GO TO 320
X1=(-BR-SQRT(XXXX))/(2.0*AA)
CASO=CASO+X1
A=A-X1

```

```

270 X=0.0
U=SQRT(2.0*(A+F+G+ASR)+0.5*(S+H+HCO3+AP+AN+FL))
BR=A+G
FX=(2.366*(U/(1.+U))-2*U*U)
CC=A*G-(2.4E-5)*EXP(EX)
R=SQRT((BB*BR-4.0*CC))
X=T-RB+R)/2.0
CAS1=4.897E-3-CASO
DFL=R*XXT-CAS1
IF (DEL-X) 280,360,360
X=XXT*B
XXT=0.0
CAS1=0.0
A=A+X
G=G+X
G=SQRT(2.0*(A+F+G+ASR)+0.5*(S+H+HCO3+AP+AN+FL))
AA=EXP(-9.366*(U/(U+1.))-2*U*U)
BR=-(4.9E-03+AA*AA*G)
CC=AA*A*G-4.9E-3*CASO
XXXX=BR*BR-4.0*AA*CC
IF (XXX) 300,300,310
X1=0.0
GO TO 320
X1=(-BR-SQRT(XXXX))/(2.0*AA)
CASO=CASO+X1
A=A-X1

```

```

270 X=0.0
U=SQRT(2.0*(A+F+G+ASR)+0.5*(S+H+HCO3+AP+AN+FL))
BR=A+G
FX=(2.366*(U/(1.+U))-2*U*U)
CC=A*G-(2.4E-5)*EXP(EX)
R=SQRT((BB*BR-4.0*CC))
X=T-RB+R)/2.0
CAS1=4.897E-3-CASO
DFL=R*XXT-CAS1
IF (DEL-X) 280,360,360
X=XXT*B
XXT=0.0
CAS1=0.0
A=A+X
G=G+X
G=SQRT(2.0*(A+F+G+ASR)+0.5*(S+H+HCO3+AP+AN+FL))
AA=EXP(-9.366*(U/(U+1.))-2*U*U)
BR=-(4.9E-03+AA*AA*G)
CC=AA*A*G-4.9E-3*CASO
XXXX=BR*BR-4.0*AA*CC
IF (XXX) 300,300,310
X1=0.0
GO TO 320
X1=(-BR-SQRT(XXXX))/(2.0*AA)
CASO=CASO+X1
A=A-X1

```

```

370 A2=A          SEP 240
      SFT=S          SEP 241
      IF ((RP.EQ.0.0.OR.S.EQ.0.0).AND.(AP.EQ.0.0.OR.SAT.EQ.0.0)) GO TO 4 SEP 242
160          SEP 243
      ERROR=1.200E-06          SEP 244
      KAR=0          SEP 245
      NUMB=100          SEP 246
      X=.5*AP7B-.5*OE-.09          SEP 247
      IF (X.GE.SAT) X=.6*SAT-.5*OE-.10          SEP 248
      IF (-X.GT.RP) X=-RP+.1*OE-.11          SEP 249
      IF (-X.GT.S/B) X=-S/R+.1*OE-.11          SEP 250
      ION=3          SEP 251
      GO TO 390          SEP 252
380 X=X+.1*X          SEP 253
      X70=X          SEP 254
      SI=S+B*X          SEP 255
      AP1=AP-B*X          SEP 256
      SATI=SAT-X          SEP 257
      RP1=RP+X          SEP 258
      IF (SI.LT.0.0.OR.SATI.LT.0.0.OR.RPI.LT.0.0.OR.AP1.LT.0.0) GO TO 41 SEP 259
10          SEP 260
      GO TO 420          SEP 261
      X=.5*X70          SEP 262
      X70=X          SEP 263
      GO TO 400          SEP 264
      FX=TSITAP1*TRP1*SAT1**P3-FK3          SEP 265
      FXP=(FX+FK3)*(P3/RP1+P3/SAT1+B/SI+B/AP1)
      CALL NEWTIT (X,FX,FXP,ERROR,NUMB,KAR,ION)
      IF (NUMB.GE.50) WRITE (6,1130) ION,FX,X,FXP,S1,AP1,SAT1,RP1
      GO TO (400,450,430,450,380,440), KAR
430 WRITE (6,1310)
      WRITE (6,1320) J,TSOL,ION
      GO TO 1080
      GO TO 1080
      WRITE (6,1330)
      WRITE (6,1320) J,ISOL,ION
      GO TO 1080
450 Y=X          SEP 271
      SEP 272
      SEP 273
      SEP 274
      SEP 275
      SEP 276
      SEP 277
      SEP 278
      S=S+B*Y
      AP=AP-B*Y

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```

SAT=SAT-Y          SEP 279
RP=RP+Y          SEP 280
INDEX=8          SEP 281
SF2=S          SEP 282
IF ((ET.EQ.0.0.OR.S.EQ.0.0).AND.(A.EQ.0.0.OR.SAT.EQ.0.0)) GO TO 53SEP 283
TO          SEP 284
FERROR=1.000E-06    SEP 285
NUMB=100          SEP 286
KAR=0          SEP 287
TONE=2          SEP 288
X=.1*S/B-5.0E-09    SEP 289
TF (X.GE.ET) X=.8*ET=.5.0E-10    SEP 290
IF (-X.GT.SAT/2.) X=-SAT/2.+1.0E-11    SEP 291
TF (FX.GT.A/B) X=-A/B+1.0E-11    SEP 292
GO TO 480          SEP 293
470          X=X+.1*X    SEP 294
480          X70=X    SEP 295
C          SEP 296
S1=S-2.*R*X    SEP 297
FT1=ET-X    SEP 298
SAT1=SAT+2.*X    SEP 299
IF (AI.LT.0.0.OR.S1.LT.0.0.OR.ET1.LT.0.0.OR.SAT1.LT.0.0) GO TO 500SEP 300
GO TO 510          SEP 301
500          X=.5*X70    SEP 302
X70=X          SEP 303
GO TO 490          SEP 304
510          U=SQRT((2.0*(A+F+G+ASR)+0.5*(S+H+HCO3+AP+AN+FL)))
AA=EXP1-2.344*(U/(U+1.0)-.2*U*U)    SEP 305
FX=AA*(A1/(S1*S1))*(SAT1/ET1)**P2-FK2    SEP 306
FP=P*FP*FK2**P2**P2**P2/ET1+B*AI+(4.*B)/SI    SEP 307
CALL NEWIT (X,FX,FXP,ERROR,NUMB,KAR,ION)    SEP 308
TF TNUMB.GE.901 WRITE (6,1130) TON,FX,X,FXP,S1,A1,SAT1,ET1    SEP 309
GO TO (490,520,430,520,470,440), KAR    SEP 310
520          Y=X    SEP 311
A=A+B*Y    SEP 312
S=5-2.*B*Y    SEP 313
ET=ET-Y    SEP 314
SAT=SAT+2.*Y    SEP 315

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```

530 A3=A
      IF (CT.LT.1.01E-11) CT=0.0
      IF ((ET.EQ.0.0.OR.F.EQ.0.0).AND.(A.EQ.0.0.OR.CT.EQ.0.0)) GO TO 600
      FERROR=1.000E-06
      NUMB=100
      KAR=0
      ION=1
      X=ET*F7B-5.0E-09
      IF (X.GE.ET) X=.8*ET-5.0E-10
      IF (-X.GT.CT) X=-CT+1.0E-11
      IF (-X.GT.A/B) X=-A/B+1.0E-11
      GO TO 550
      X=X+.1*X
      X70=X
      550 AI=A+B*X
      F1=F-B*X
      ET1=ET-X
      CT1=CT+X
      IF (AI.LT.0.0.OR.F1.LT.0.0.OR.CT1.LT.0.0) GO TO 570
      GO TO 580
      570 X=.5*X70
      X70=X
      GO TO 560
      560 FX=(AI/F1)*(CT1/ET1)**P1-FK1
      FXP=(FX+FK1)*(P1/ET1+P1/CT1+B/A1+B/F1)
      CALL NEWTIT (X,FX,FXP,ERROR,NUMB,KAR,ION)
      IF (NUMB.GE.90) WRITE (6,I130) ION,FX,X,FXP,P1,A1,CT1,FT1
      GO TO (560,590,430,590,540,440), KAR
      590 Y=X
      A=A+B*Y
      F=F-B*Y
      ET=ET-Y
      CT=CT+Y
      600 A4=A
      TF TRSRT 620,620,610
      RR=A+B*(RSR+1.23*FT)+1.23*ASR

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```

AA=B*(1.0-1.23*ASR*ET)           SEP 353
CC=(A*RSR-1.23*ASR*ET)           SEP 354
R=SQR(T(BB*BB-4.0*AA*CC))       SEP 355
Y=(-BB+R)/(2.0*AA)                SEP 356
A=A+B*Y                           SEP 357
ASR=ASR-B*Y                      SEP 358
ET=ET-Y                           SEP 359
RSR=RSR+Y                         SEP 360
A5=A                           SEP 361
620 U=SQRT(2.0*(A+F+G+ASR)+0.5*(S+H+HCO3+AP+AN+FL))    SEP 362
AA=EXP(-7.034*(UTTU+1.5)*2*UTU)  SEP 363
Z3=4.676E-10-A*HCO3**2*AA        SEP 364
IF (Z3) 630,700,700              SEP 365
ERROR=1.0E-11                     SEP 366
KAREO                           SEP 367
NUMB=100                          SEP 368
TON=4                           SEP 369
XJ=SQRT(4.676E-10/(AA*AA))      SEP 370
X=(XJ-HCO3)/2                   SEP 371
IF (-X.GT.A) X=-(.93*A-5.0E-07) SEP 372
GO TO 650                         SEP 373
630 X=X+.1*X                     SEP 374
X70=X                           SEP 375
CA1=A+X                         SEP 376
HCO3+2.*X                        SEP 377
IF (CA1.LT.0.0.OR.HC1.LT.0.0) GO TO 670 SEP 378
GO TO 680                         SEP 379
670 X=.5*X70                      SEP 380
X70=X                           SEP 381
GO TO 660                         SEP 382
680 FX=CA1*HC1**2-4.676E-10/AA   SEP 383
FXP=HC1**2+4.*CA1*HC1            SEP 384
CALL NEWTIT(X,FX,FXP,ERROR,NUMB,KAR,ION) SEP 385
IF (NUMB.GE.90) WRITE (6,1130) ION,FX,X,FXP,CA1,HC1,A,HCO3 SEP 386
GO TO (660,690,430,690,640,440), KAR SEP 387

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```

690 A=A+X          SEP 388
      HC03=HC03+2.*X
      CAL=CAL-X/B
      IF (A.LT.0.0.OR.HC03.LT.0.0) GO TO 1080
      GO TO 730
      IF (CAL.GT.0.0) GO TO 710
      GO TO 730
      700 IF (CAL.GT.0.0) GO TO 710
      GO TO 730
      710 XM=CAL*B
      HCOLD=HC03
      COLD=CAL
      AOLD=A
      A=A+XM
      HC03=HC03+2.*XM
      QU=SQRT(2.0*(A+F+G+ASR)+•5*(S+H+HC03+AP+AN+FL))
      CAL=0.0
      QA=EXP(-7.034*(QU/(QU+1.0)-•2*QU*QU))
      Z3=4.676E-10=A**HC03**2*QA
      IF (Z3) 720,730,730
      720 A=AOLD
      HC03=HCOLD
      CAL=COLD
      GO TO 630
      730 A6=A
      U=SQRT(2.0*(A+F+G+ASR)+•0.5*(S+H+HC03+AP+AN+FL))
      AA=EXP(-7.034*(U/U+1.0)-•2*U*UT)
      Z4=3.98E-11-A*FL**2*AA
      TF TZ4) 740,840,840
      740 FRRQ=3.0E-12
      KAR=0
      NUMB=100
      TON=5
      XJ=SQRT(3.98E-11/(AA*AA))
      X=(XJ-FT)72
      IF (-X.GT.A) X=-1.93*A-5.0E-07
      XS=X
      TNR=0
      GO TO 760
      750 X=X+.1*X
      SEP 389
      SEP 390
      SEP 391
      SEP 392
      SEP 393
      SEP 394
      SEP 395
      SEP 396
      SEP 397
      SEP 398
      SEP 399
      SEP 400
      SEP 401
      SEP 402
      SEP 403
      SEP 404
      SEP 405
      SEP 406
      SEP 407
      SEP 408
      SEP 409
      SEP 410
      SEP 411
      SEP 412
      SEP 413
      SEP 414
      SEP 415
      SEP 416
      SEP 417
      SEP 418
      SEP 419
      SEP 420
      SEP 421
      SEP 422
      SEP 423
      SEP 424
      SEP 425

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----- 760 WRITE (6,1340) X70=X
----- 770 CA2=A+X
----- FL2=FL+2.*X
----- IF (CA2.LT.0..OR.FL2.LT.0..) GO TO 800
----- GO TO 810
----- 780 IF (ABS(FXR(4)).GT.ABS(FXR(3)).AND.ABS(FXR(3)).GT.ABS(FXR(2)).AND.FXR(2).LT.0..) GO TO 800
----- 1ARS(FXR(2)).GT.ABS(FXR(1)) GO TO 790
----- GO TO 770
----- 790 X=(XS+XNR(1))/2.
----- GO TO 830
----- 800 X=•5*X70
----- X70=X
----- GO TO 770
----- 810 FX=CA2*FL2**2-3•98E-11/AA
----- FXR=FL2**2+4.*A2*FL2
----- CALL NEWTT (X,FX,FXP,ERROR,NUMB,KAR,ION)
----- TF (NUMB.GE.901) WRITE (6,1301) ION,FX,X,FXP,CA2,FL2,A,FL
----- GO TO (820,830,430,830,750,440), KAR
----- 820 INR=INR+1
----- XNR(INR)=X
----- FXR(INR)=FX
----- IF (INR.EQ.4) GO TO 780
----- GO TO 770
----- 830 A=A+X
----- FL=FL+2.*X
----- CAF=CAF-X/B
----- TF (A.LT.0..OR.FL.LT.0..) GO TO 1080
----- GO TO 870
----- 840 IF (CAF.GT.0..) GO TO 850
----- GO TO 870
----- 850 XM=CAF*B
----- AOLD=A
----- FOLD=FL
----- COLD=CAF
----- SEP 426
----- SEP 427
----- SEP 428
----- SEP 429
----- SEP 430
----- SEP 431
----- SEP 432
----- SEP 433
----- SEP 434
----- SEP 435
----- SEP 436
----- SEP 437
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----- SEP 453
----- SEP 454
----- SEP 455
----- SEP 456
----- SEP 457
----- SEP 458
----- SEP 459
----- SEP 460

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FL=FL+2.*XM          SEP 461
CAF=0.                SEP 462
QU=SQR((2.*((A+F+G+ASR)+.5*(S+H+HC03+AP+AN+FL))) SEP 463
QA=EXP(-7.034*((QU/(QU+1.))-2*QU*QU))    SEP 464
Z4=3.98E-11-A*FL**2*QA      SEP 465
IF (24) 860,870,870      SEP 466
A=AOLD                SEP 467
FL=FOLD                SEP 468
CAF=COLD               SEP 469
GO TO 740               SEP 470
870 DEL=A-A1           SEP 471
IF (DEL+1.0E-5) 250,880,880      SEP 472
IF (DET=R.0E-5) 890,890,250      SEP 473
DEL=A-A2               SEP 474
900 IF (DEL+1.0E-5) 250,900,900      SEP 475
IF (DEL=1.0E-5) 910,910,250      SEP 476
910 DFL=A-A3           SEP 477
TF-(DEL+1.0E-5) 250,920,920      SEP 478
920 IF (DEL-1.0E-5) 930,930,250      SEP 479
930 DEL=A-A4           SEP 480
IF (DEL+1.0E-5) 250,940,940      SEP 481
TF-(DEL=1.0E-5) 950,950,250      SEP 482
950 DFL=S-SF1          SEP 483
IF (ABS(DFL)-1.0E-5) 960,960,250      SEP 484
960 DEL=S-SF2          SEP 485
TF-(ABS(DEL)-1.0E-5) 970,970,250      SEP 486
970 IF (RSR) 990,990,980      SEP 487
980 DEL=A-A5           SEP 488
IF (ABS(DEL)-1.0E-5) 990,990,250      SEP 489
990 DFL=A-A6           SEP 490
IF (ABS(DEL)-1.0E-5) 1000,1000,250      SEP 491
1000 CALL DST(F,A,AP,S,F,ASR,APH,AKD,HCO3,AN,Na,Graphite)  SEP 492
IF (AKD.LT.0.0) AKD=0.0      SEP 493
J1=0                  SEP 494
R=B/FLOAT (JSUB)      SEP 495

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```

      DO 1040 LB,J=1,JSUB
      J1=J1+1
      TAKD**SR=SRSS(J,J1)*(1.+AKD**B)
      IF (Y) 1010,1020,1020
      T0TO - IF (-Y.GT.SRSS(J,J1)) Y=-SRSS(J,J1)
      GO TO 1030
      1020 - IF (Y*B.GT.SR) Y=SR/YB
      1030 SR=SR-Y*B
      SRSST(J,J1)=SRSSST(J,J1)+Y
      1040 CONTINUE
      R=B*1000.*FLOAT(JSUB)
      SRS=SRSS(J,JSUB)
      TSOLF=ISOL
      VOL=ALI*ISOLF
      COVOL=VOL*VSOL
      BREAK=SR/SRIN
      1F (PRINT.OR.PRI.OR.J.EQ.K) WRITE(6,1350) J,ISOL
      1F (PRINT.OR.PRI.OR.J.EQ.K) WRITE(6,1380)
      1F (PRINT.OR.PRI.OR.J.EQ.K) WRITE(6,1370) AP,RP,S,SAT,F,CT,ASR,RSR,A,
      CET
      1F (PRINT.OR.PRI.OR.J.EQ.K) WRITE(6,1390)
      1F (PRINT.OR.PRI.OR.J.EQ.K) WRITE(6,1410) HC03,AN,G,H,SR,SRS,VOL,COVOL,
      CL,BREAK
      1F (PRINT.OR.PRI.OR.J.EQ.K) WRITE(6,1400)
      1F (PRINT.OR.PRI.OR.J.EQ.K) WRITE(6,1420) APH,AKD,CASO,XXT,CAL,CAF,FL,B
      C,B,U
      CERTRJTERSR
      CMG(J)=CT
      CCA(J)=ET
      CK(J)=RP
      CNA(J)=SAT
      GYPP(J)=XXT
      CALL(J)=CAL
      CAFF(J)=CAF
      IF X=0
      SEP 496
      SEP 497
      SEP 498
      SEP 499
      SEP 500
      SEP 501
      SEP 502
      SEP 503
      SEP 504
      SEP 505
      SEP 506
      SEP 507
      SEP 508
      SEP 509
      SEP 510
      SEP 511
      SEP 521
      SEP 522
      SEP 523
      SEP 524
      SEP 525
      SEP 526
      SEP 528
      SEP 529

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1200 FORMAT (6F10.4) SEP 567
1210 FORMAT (T6,3H P1,T16,4H FK1,T26,3H P2,T36,4H FK2,T46,3H P3,T56,4H SEP 568
1FK3/6E10.3//) SEP 569
14//) SEP 570

T270 FORMAT (2I5,3F10.3)
1230 FORMAT (T6,2H K,T13,5H JSUB,T19,6H VSOIL,T31,5H PORE,T40,6H ( SAT/
C218,3E10.3//) SEP 571
1240 FORMAT (T10,4H SAT,T25,3H RP,T40,3H ET,T55,3H CT,T70,4H RSR,/5E15. SEP 572
14//) SEP 573
1250 FORMAT (T10,4H GYP,T25,4H CAL,T40,3H B2,T55,4H CAF,T70,4H SRS/5E15SEP 574
1.4//) SEP 575
1260 FORMAT (5E15.4) SEP 576
1270 FORMAT (E14.4,16) SEP 577
1280 FORMAT (T9,4H AL1,T19,2HLB/E14.4,16//) SEP 578
1290 FORMAT (89H HCO3 NO3 SO4 GSEP 579
1300 TYPSUM SR85 SOL SR85 SOIL CAL ) SEP 580
1300 FORMAT (21H FL CAF ) SEP 581
1310 FORMAT (96HROOT DID NOT CONVERGE WITHIN MAXIMUM NUMBER OF ITERATIONS SEP 582
1310, PROGRAM RETURNING TO NEXT SET OF DATA) SEP 583
1320 FORMAT (316) SEP 584
1330 FORMAT (54HOVERFLOW IN COMPUTATION,RETURNING TO NEXT SET OF DATA) SEP 585
1340 FORMAT (18H WENT THRU NUMBERS 21) SEP 586
1350 FORMAT (40H EQUILIBRIUM VALUES FOR ALL IUNS COLUMN,15,8H ALIQUOT) SEP 587
1350(F) SEP 588

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1360 JOLUMN,15,8H ALIQUOT,15) SEP 590
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1380 FORMAT (102H K NA NAX MG SEP 592
1 MAX SR SRX CA CAX CL SR85 SOL-SR85SEP 593
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1410 FORMAT (1X,10(1PE10.3)) SEP 598
1420 FORMAT (1X,10(1PE10.3)) SEP 599
1420(F) SEP 600

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      *M   FR5 DIST
      *M   SUBROUTINE DIST (R,A,AP,S,F,ASR,APH,AKD,HCO3,AN,H,G,AAPH,U,FL)    DIS 1
      *M   IF (HCO3.LE.0.0) GO TO 100
      *M   T=SQRT(2.0*(A+F+G+ASR)+0.5*S+H+HCO3+AP+AN+FL)
      *M   APH=6.65-.5*ALOG(A)+1.018*(U/(1.+U))-2.*U*U)
      *M   AAPH=6.6-.5*ALOG(1/T(A))
      100 R=B/1000.
      *M   IF T>LT•T005) GO TO 110
      *M   AKD=1.9337-60.72*(A-.0275)-5287*(40.*AP-1.)*17.831*(40.*AP-1.)*(ADIS
      *M   1-.0275)-3.263*(S-.11)+126.52*(S-.11)*(A-.0275)+5.43*(S-.11)*(40.*ADIS
      *M   2P-1.)*222.864*(S-.11)*(40.*AP-1.)*(A-.0275)
      *M   RETURN
      110 AKD=4.325-683.3*(A-.0035)-1.67*(40.*AP-1.)*493.3*(A-.0035)*(40.*APDIS
      *M   12
      *M   T=1.Y=T1.*1(S-.11)+3259.26*(S-.11)*(A-.0035)+11.94*(S-.11)*(40.*AP-1DIS
      *M   13
      *M   2.)*1000.*1(S-.11)*(A-.0035)*(40.*AP-1.)
      *M   RETURN
      *M   END
      *M   FR5 NEWTIT•NEWTTIT
      *M   SUBROUTINE NEWTIT (X,FX,FXP,E,N,K,ION)
      *M   COMMON F,ET,B,S,AP,SAT,CT,RP,A,HCO3,FL
      *M   IF (K.GT.0) GO TO 100
      *M   J=K
      *M   K=1
      *M   NMAX=N
      *M   N=0
      100 T=FX
      *M   IF (J.EQ.0) GO TO 110
      *M   IF (ABS(X).LT.1.E-34) GO TO 120
      *M   T=X
      *M   110 IF (.NOT.ABS(T).GT.E) GO TO 260
      *M   120 IF (N.EQ.NMAX) GO TO 270
      *M   IF (.NOT.ABS(FXP).GT.0.) GO TO 290
      *M   T=X
      *M   X=X-FX/FXP
      *M   GO TO (130,160,190,220,230), ION
      130 IF (F.EQ.0.) GO TO 140
      *M   IF (B**X.GE.FT) X=.95*FX

```

```

      IF (FT.EQ.0.) GO TO 150
      IF (X.GE.FT) X=.95*FT
      IF (-X.GT.CT) X=-CT+1.0E-11
      IF (-X.GT.A7BT) X=-A/B+1.0E-11
      GO TO 240
160   IF (S.EQ.0.) GO TO 170
      IF (2.*B*X.GE.S) X=.95*S/(2.*B)
      IF (ET.EQ.0.) GO TO 180
170   IF (X.GE.ET) X=.95*ET
180   IF (-X.GT.SAT/2.) X=-SAT/2.+1.0E-11
      IF (-X.GT.A/B) X=-A/B+1.0E-11
      GO TO 240
190   IF (AP.EQ.0.) GO TO 200
      IF (B*X.GE.AP) X=.95*AP/B
      IF (SAT.EQ.0.) GO TO 210
200   IF (X.GE.SAT) X=.95*SAT
      IF (-X.GT.RP) X=-RP+1.0E-11
210   IF (-X.GT.S7BT) X=-S7B+1.0E-11
      GO TO 240
220   XY=X
      IF (-X.GT.A) X=-.95*A
      IF (-X/2.GT.HC03) X=-.45*HC03
      IF (XY.NE.X) WRITE (6,310) XY,X
      GO TO 240
230   XY=X
      IF (-X.GT.A) X=-.95*A
      IF (-X/2.GT.FL) GO TO 250
240   N=N+1
      CALL OVERFL (I)
      IF (I.EQ.1) GO TO 300
      IF (.NOT.ABS(1-X).GT.0.) GO TO 280
      RETURN
250   X=9.4E-05
      WRITE (6,320) XY,X,A,F
      GO TO 230

```

260	K=2	NEW 55
	RETURN	NEW 56
270	K=3	NEW 57
	RETURN	NEW 58
280	K=4	NEW 59
	RETURN	NEW 60
290	K=5	NEW 61
	RETURN	NEW 62
300	K=6	NEW 63
	RETURN	NEW 64
C		NEW 65
310	FORMAT T22H-NEWTON RAPHSON CHANGE,2E10.4)	NEW 66
320	FORMAT (17H WENT THRU NEWTIT,4E10.4)	NEW 67
	END	NEW 68
* XQT SEP		

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