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URANIUM PRODUCTION—PROCESS DESIGNS
FOR LEACHED ZONE PLANTS

Volume III. Alumina Recovery Section

By

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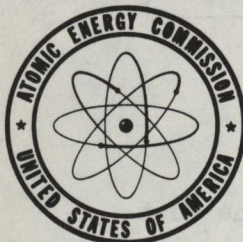
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September 25, 1953

International Minerals and Chemical Corporation
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AEC, Oak Ridge, Tenn.

URANIUM PRODUCTION
PROCESS DESIGNS FOR LEACHED ZONE PLANTS
VOLUME III -- ALUMINA RECOVERY SECTION

September 25, 1953

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I. INTRODUCTION

This volume is the third in a series of reports on processing Florida leached zone material for the recovery of uranium, alumina and phosphatic values.

Liquor from the proposed leaching operation is processed to crystallize ammonium alum which is treated with aqueous ammonia to precipitate an alumina hydrate. The alumina hydrate is dried and calcined to produce metallurgical grade alumina.

Basic design, plant capitalization and operating costs for the unit processes pertaining to the recovery of alumina are presented in this report. Data are presented for plants designed to produce 450, 225, and 100 tons of uranium per year.

Also included are estimates of capital and operating costs for a process which produces an impure alumina product suitable for feed to the Bayer process. In this process, alum is crystallized from the leached zone extract, washed, dehydrated and calcined to produce alumina. The estimates are for a plant producing 450 tons of uranium per year.

International Minerals and Chemical Corporation desires to acknowledge assistance received from Catalytic Construction Company in the preparation of this report.

II. SUMMARY

Process designs and cost estimates for two alternate processes in which alumina is recovered from leached zone are presented in this report.

In the first process, metallurgical grade alumina is produced from alum that has been purified by two crystallizations. Detailed design and cost estimates are presented for plants that have the following annual production:

Tons U/Year	450	225	100
Tons Al ₂ O ₃ /Year	393,120	196,560	87,360

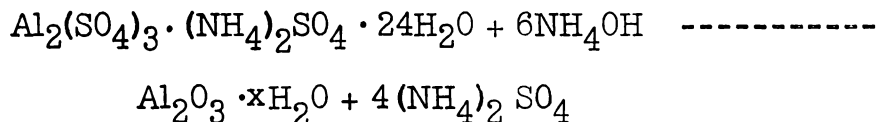
Although a very pure alumina is produced in this process, capital costs and operating costs are relatively high. Efforts are being made to redesign the process to include equipment that would be less expensive and would still give a metallurgical grade alumina. Efforts are also being made to develop process changes in the design, in order to reduce operating costs. It is believed that additional laboratory and pilot plant work will bring about a considerable reduction in both capital and operating costs.

Following is a discussion of the steps in the first alumina recovery process. The alumina recovery operation takes place after the four-stage countercurrent filtration operation described in Volume II of this series (RMO 2013). Alumina is removed at this point for the following reasons:

1. Uranium extraction is simplified due to a less viscous slurry and absence of interfering metallic (Al) ions.
2. Alumina can be removed easily from the slurry by precipitation of ammonium alum.
3. No uranium has been found to be removed with the alum crystals by this process.

In this step of the process, the acid filtrate from the leaching section is concentrated to approximately 30% dissolved solids. Ammonium sulfate is added to combine with the aluminum sulfate present to form ammonium alum. Upon cooling, ammonia alum is crystallized and removed by filtration. The filtrate bearing the uranium and phosphate values is pumped to the Uranium Recovery Section (RMO 2015) for further processing. The ammonium alum crystals are recrystallized twice to obtain the purity desired.

Purified ammonium alum is reacted with excess aqueous ammonia to produce an alumina hydrate that will filter easily. The theoretical reaction taking place is as follows:



Ammonium sulfate and ammonia are leached from the alumina hydrate with water in a countercurrent filtration operation.

Free ammonia is recovered, and the remaining ammonium sulfate is concentrated by evaporation, crystallized, and returned to the original alum precipitation operation in the forepart of the process. Excess ammonium sulfate is centrifuged and the cake sent to the ammonium sulfate decomposition process for recovery of ammonia and sulfur values.

The alumina hydrate cake is dried and calcined at a final temperature of 2190° F. to yield metallurgical grade alumina with the following analyses:

Chemical Analysis of Al₂O₃ Product

Na ₂ O	Trace
Fe ₂ O ₃	0.017%
SiO ₂	0.021%

Chemical Analysis of Al₂O₃ Product--Continued

P ₂ O ₅	0.0015%
TiO ₂	0.005%
CaO	0.01%
H ₂ O Sorption	1.0%

Screen Analysis of Al₂O₃ Product

-48 + 60	11%
-60 + 100	33%
-100 +200	51%
-200 + 325	5%

Summaries of the estimated capital cost and operating cost for the three plant sizes of the first process are as follows:

Summary of Estimated Capital Cost for Alumina Recovery

<u>Plant Size</u>	<u>Capital Cost</u>
100 Tons U/Year	\$21,171,000
225 Tons U/Year	\$37,689,000
450 Tons U/Year	\$66,578,000

Summary of Estimated Operating Cost for Alumina Recovery

<u>Plant Size</u>	<u>Dollars/Hour</u>
100 Tons U/Year	\$1,245.09
225 Tons U/Year	\$2,261.28
450 Tons U/Year	\$4,025.73

These cost estimates are based on presently available data, prices, experience and judgment.

Operating cost estimates include reagents, power, steam, fuel oil, water, direct labor, immediate supervision, maintenance and amortization based on a 15 year life for equipment and a 20 year life for buildings. Also included are insurance, local taxes and analytical expenses. Cost of feed solution, overhead, management, general plant facilities, interest and return on investment have not been included, but these items will be included in the summary report.

Ammonia used in this section of the process is obtained from the following sources:

1. Make-up Ammonia
2. Recycle from Ammonia Sulfate Decomposition Section.
3. Recycle from within the Alumina Section.

Make-up ammonia is produced in the New Orleans area and is charged at \$45.99, \$49.84, and \$58.34 per ton (delivered) for the 450, 225 and 100 ton plants, respectively. Recycle ammonia from the Decomposition Section is charged at \$18.09, \$19.25, and \$21.68 per ton for the 450, 225, and 100 ton plants, respectively. No charge is made for the ammonia recycled within the Alumina Section.

Following is a simplified flow sheet of the Alumina Section for the first process.

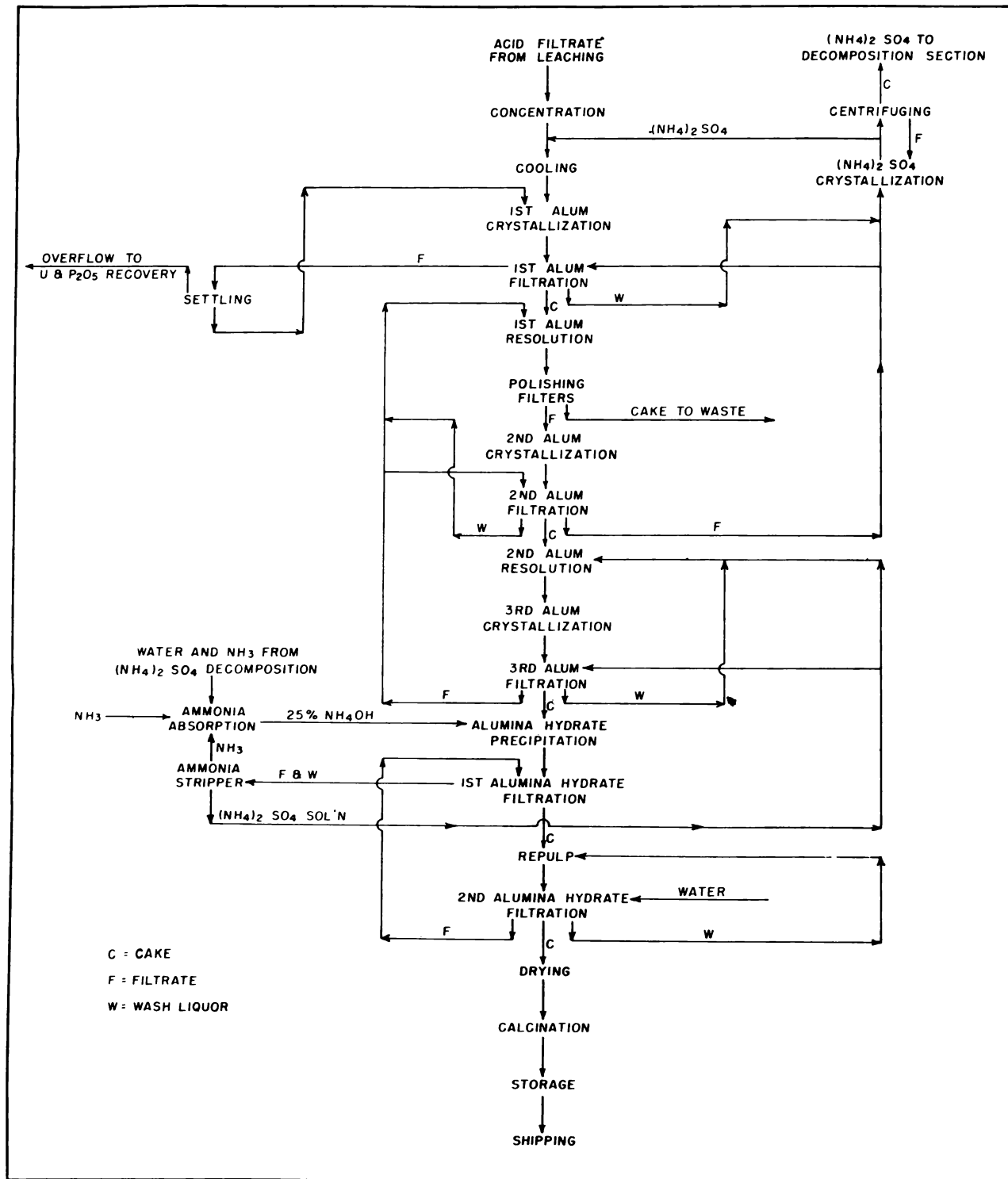
Preliminary investigation has been made for an alternate process which produces an impure alumina product suitable for feed to the Bayer process. In this process, alum is crystallized from the leached zone extract, filtered, washed, dissolved and passed through a spray dryer to dehydrate the alum.

The dehydrated alum is calcined to produce alumina and to recover sulfur values. The Ammonium Sulfate Decomposition Section is eliminated, but the capacity of the sulfuric acid and ammonia plants must be increased.

Cost estimates show that for a plant producing 450 tons uranium per year, using this alternate process, the total plant capital cost is \$52,000,000 less and the total plant operating cost is \$844 per hour less than the first process. However, the alumina product is not as pure as the alumina produced in the first process and, therefore, the sales value would be lower. The amount lost by the decrease in sales value would be greater than the amount gained by the decrease in operation costs. Better cost estimates could be obtained after this process is evaluated on a pilot plant scale.

FIGURE 1

**SIMPLIFIED FLOW SHEET
ALUMINA RECOVERY SECTION**



III. PROCESS

A. BASIS OF THE PROCESS

1. Raw Materials

The process to recover metallurgical grade alumina, and to remove and recover ammonium sulfate formed by this operation, has been investigated in the laboratory and further developed in pilot plant operations. The principle raw materials required for this step are:

- a. Clarified acid filtrate
- b. Ammonia
- c. Steam
- d. Fuel oil

These raw materials will be discussed as follows:

a. Clarified Acid Filtrate

The acid filtrate containing the values solubilized by digestion is received from the Leaching Section after being clarified as described in Volume II, Leaching Section, of this series (RMO 2013). Filtrate received in the alumina recovery unit contains 22.7% solids. The weight per cent distribution of the values on a dry basis is as follows:

Weight Per Cent (Dry Basis)

$\frac{\text{Al}_2\text{O}_3}{22.1}$	$\frac{\text{P}_2\text{O}_5}{18.0}$	$\frac{\text{Fe}_2\text{O}_3}{2.59}$	$\frac{\text{SO}_4}{47.2}$	$\frac{\text{U}_3\text{O}_8}{.0287}$
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Following is a breakdown of the estimated quantities of clarified acid filtrate feed to the three proposed alumina recovery units:

Clarified Acid Filtrate Requirements

<u>Plant Size</u>	<u>Dissolved Solids</u>	<u>Water</u>	<u>G. P. M.</u>	<u>Sp. Gr.</u>
450 Tons U/Year	213.2 T/Hr.	724.1 T/hr.	2989	1.26
225 Tons U/Year	106.6 T/Hr.	362.0 T/hr.	1490	1.26
100 Tons U/Year	47.3 T/Hr.	160.8 T/hr.	662	1.26

b. Ammonia

Ammonium hydroxide is used to precipitate alumina hydrate from the purified ammonium alum. A 25% solution of ammonia is preferred for this purpose. One hundred percent stoichiometric excess is fed to the precipitation tanks to assure complete reaction. Unreacted ammonia is recovered by means of a stripping column and returned to the precipitators.

Following is a table showing the sources of ammonia to the absorber:

<u>Ammonia to Absorber, Tons/Hr. NH₃</u>			
<u>Tons U/Year</u>	<u>450</u>	<u>225</u>	<u>100</u>
From Stripper	47.2	23.6	10.5
From Decomposition Sec.	41.4	20.7	9.2
NH ₃ from NH ₃ Plant at			
Another Site	5.8	2.9	1.3
Total NH ₃	94.4	47.2	21.0

c. Steam

Process steam is used to concentrate the clarified acid filtrate for steam jet cooling and crystallization, re-solution of alum, ammonia stripping and ammonium sulfate crystallization. All steam used will be back pressure steam from the electric power generating turbines. The source of the steam is described in the Utilities Report (RMO 2019).

Estimates of the steam requirements for the alumina recovery and ammonium sulfate crystallization for the three size plants are as follows:

<u>Unit Operation</u>	<u>Process Steam, Pounds/Hour</u>					
	<u>450 Tons U/Yr.</u>		<u>225 Tons U/Yr.</u>		<u>100 Tons U/Yr.</u>	
	<u>100 psig</u> <u>Steam</u>	<u>15 psig</u> <u>Steam</u>	<u>100 psig</u> <u>Steam</u>	<u>15 psig</u> <u>Steam</u>	<u>100 psig</u> <u>Steam</u>	<u>15 psig</u> <u>Steam</u>
(NH ₄) ₂ SO ₄ Crystallization	1,480	507,000	740	253,500	329	112,500
Evaporation of Acid Filtrate	285,675		143,175		63,550	
Steam Jet Cooling 1st Alum Cryst.	61,455		30,728		13,700	
1st Rediss. of Alum	135,000		62,500		30,000	
2nd Crystal. of Alum	397,590		198,795		88,376	
2nd Rediss. of Alum	36,000		18,000		8,000	
3rd Crystal. of Alum	407,650		203,825		90,589	
Ammonia Stripper		<u>290,000</u>		<u>142,500</u>		<u>63,400</u>
Total	1,324,850	797,000	657,763	396,000	294,544	175,900

d. Fuel Oil

Bunker C oil is proposed as fuel for drying the alumina hydrate cake and for calcining the dried cake to alumina.

The following table lists the estimated fuel oil requirements for the proposed plants:

Bunker C Fuel Oil Requirements, Gallons/Hour

<u>Tons U/Year</u>	<u>450</u>	<u>225</u>	<u>100</u>
Fuel Oil for Drying	5620	2810	1244
Fuel Oil for Calcining	<u>1402</u>	<u>701</u>	<u>311</u>
Total	7022	3511	1555

2. Ammonium Alum Crystallization & Purification

Acid filtrate received from the Leaching Section contains approximately 22% dissolved solids. It is advantageous to increase the percentage of dissolved solids before reacting with ammonium sulfate to form ammonium alum with the alumina sulfate present in the filtrate. However, concentration by evaporation is limited by the amount of water necessary to form $\text{alum}-(\text{NH}_4)_2\text{SO}_4 \cdot \text{Al}_2(\text{SO}_4)_3 \cdot 24\text{H}_2\text{O}$. Further evaporation, above approximately 30% solids, would reduce the yield.

Ammonium sulfate addition is of value up to a point where the solution is saturated with respect to both alum and ammonium sulfate. Beyond this point solid ammonium sulfate would crystallize and require removal in subsequent processing. This point is approximately three times the stoichiometric quantity of ammonium sulfate.

Alum is formed in a reaction between solid phase ammonium sulfate and dissolved aluminum sulfate in the leached zone liquor. Rate of solution of ammonium sulfate controls potential (degree of supersaturation) and rate of alum crystal growth so that well formed, relatively pure crystals, may be obtained.

Ammonium sulfate is added to 130° F. leached zone liquor, cooled to 77° F., and crystallized in 4-stage tank crystallizers (5 hours retention time). Discharge from the alum crystallizers is filtered and the filtrate containing the uranium and P_2O_5 values is pumped to the Uranium Recovery Section. In no case has alum precipitation interfered with U and P_2O_5 recovery in the filtrate. Cake from the first filtration

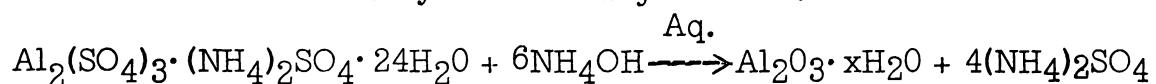
is dissolved and recrystallized twice. Ammonium sulfate solution is used for washing and is in countercurrent flow with the alum crystals. The wash solution is 20-25% ammonium sulfate from the alum-to-alumina conversion section and is therefore very pure since alum has low solubility in strong ammonium sulfate solutions (at normal temperatures).

Krystal units are provided for the second and third alum crystallization for the following reasons:

- a. Crystallization is controlled.
 - (1.) Desired crystal size is produced
 - (2.) Controlled growth of crystals yields purer crystals
- b. Operation is faster than with atmospheric or coil-type units.

3. Alumina Hydrate Precipitation & Filtration

The purified ammonium alum cake from the third alum filtration is reacted with two times the stoichiometric quantity of 25% aqua ammonia to convert the alum to alumina hydrate and to solubilize the ammonium sulfate released by the following reaction:



The quantity and strength of ammonia used has been determined experimentally as optimum for most complete conversion to the hydrate and for minimum inclusion of ammonium sulfate.

To assure a filterable precipitate of alumina hydrate, the above reaction is performed with minimum mechanical disturbance and sufficient time (3 hours) to permit the ammonia to penetrate the alum crystals for complete interaction.

The alumina hydrate is subjected to two filtrations with countercurrent washing to remove ammonia and ammonium sulfate from the cake.

4. Ammonia & Ammonium Sulfate Recovery

The filtrate and concentrated wash from the first alumina hydrate filtration is pumped to a stripping column for separation of the ammonia and ammonium sulfate. The ammonia overhead from the column is absorbed in the ammonia absorption unit and reused for alumina hydrate precipitation.

The stripping column bottom contains ammonium sulfate which is pumped to the ammonia sulfate crystallizer for concentration. The stream from the crystallizer is split; part is returned directly to the Alumina Section to form the ammonium alum and the remainder is centrifuged and forwarded to the Ammonium Sulfate Decomposition Section.

5. Drying & Calcining

The alumina hydrate received in the drying area will have the following composition:

Al ₂ O ₃	13.7%
SO ₄	2.3%
NH ₃	0.7%
H ₂ O	83.3%

The wet cake is dried to a final temperature of 240° F. The drying operation eliminates most of the free water and ammonia.

The composition of the dryer discharge (calciner feed) is as follows:

Al ₂ O ₃	58.6%
SO ₄	9.9%
NH ₃	.4%
Chemical Water	30.9%
Free Water	.1%

The calciner is operated at 2190° F. to remove the chemical water and the remainder of ammonia and sulfate to produce a metallurgi-

cal grade alumina with the following analysis:

Na ₂ O	Trace
Fe ₂ O ₃	0.017%
SiO ₂	0.021%
P ₂ O ₅	0.0015%
TiO ₂	.005%
CaO	.01%
H ₂ O Sorption	1.0%

The calcined alumina is stored in bins and shipped in bulk.

III. PROCESS

B. DETAILS OF THE PROCESS

1. Alumina Recovery

The attached flow diagrams for the alumina and aluminum sulfate recovery processes are numbered as follows:

<u>Plant Size, Tons U/Year</u>	<u>Drawing Numbers</u>
450	F-1-500 to F-1-504
225	F-2-500 to F-2-504
100	F-3-500 to F-3-504

After evaporation, the first step in alumina recovery consists of adding ammonium sulfate to the solution received from the Leaching Section. The resulting ammonium alum is freed from included P_2O_5 and other impurities by subjecting it to two crystallization and three filtration operations with countercurrent washes. The filtrate from the first filtration contains the U and P_2O_5 values and is sent to subsequent operations for their recovery. Alum from the final filtration is reacted with ammonium hydroxide to precipitate a crystalline alumina hydrate, which is easily filtered and washed free of ammonium sulfate in two filtrations. The hydrate is dried and calcined to metallurgical grade alumina. Ammonia and ammonium sulfate values are recovered as part of the process.

A more detailed explanation of the process follows:

Clear acid filtrate received from the Leaching Section, with 22% dissolved solids, is concentrated in the triple effect evaporator (EV-500) to 30% dissolved solids. Concentrated ammonium sulfate solution is added to the hot (130° F.) discharge from the final effect of the evaporators. The slurry is cooled to 77° F. in the steam jet refrigeration unit (SJ-500) and ammonium alum is then

crystallized from the slurry in the 4-stage crystallizer (T-500). Retention time in each crystallizer is five hours. Deep well water is circulated through the crystallizer cooling coils (E-502) to offset the heat of crystallization and maintain a temperature of 77° F.

Discharge from the final crystallizer is pumped to a distribution box (X-500) and flows from there to the first set of alum filters (F-501). Filtrate from the first alum filtration step is pumped to the filtrate surge and settling tank (T-508). Overflow from this tank is pumped to the Uranium Recovery Section; the underflow contains alum crystals and is returned to the fourth stage of the crystallizers (T-500). Filtrate from the second alum filtration is used to wash the horizontal filter cake and the washings are pumped to the ammonium sulfate removal unit. Cake from the first alum filtration is redissolved in wash liquor from the second alum filtration and filtrate from the third alum filtration. The 4-stage redissolving tanks (T-501) are steam heated to 160° F.

Hot (160° F.) liquor from the final redissolving tank is passed through a polishing filter (F-502) and collected in the filtrate surge tank (T-509). The cake from the polishing filter is discarded.

Filtrate from the surge tank is pumped to the steam jet refrigerated vacuum crystallizer (CR-501) which crystallizes the alum at 81° F.

Slurry from the crystallizers is pumped to the slurry distributor (X-502) and flows to the second alum filtration horizontal filters (F-503). The filtrate is pumped to the ammonium sulfate removal unit. Filter cake from this operation is washed with filtrate from the third alum filtration. This wash liquor is pumped to the first stage tank in the first re-solution of alum.

Cake from the second alum filtration is dissolved in ammonium sulfate solution from the ammonia stripper (K-501) and wash liquor from the third alum filtration in the second 4-stage re-solution of alum tanks (T-517). These tanks are steam heated to a discharge temperature of 160° F.

Redissolved alum is pumped to a distributor (X-504) and flows from the distributor to the third alum steam jet refrigerated crystallizer (CR-502). The cooled (81° F.) crystallized alum slurry is pumped to the slurry distributor (X-505) and flows from there to the third alum filtration filters (F-504). The filtrate is returned to the second alum filtration. Cake from the third filtration is washed with a cooled (81° F.) portion of the ammonium sulfate solution from the ammonia stripper (K-501) bottoms.

Alum cake from the third filtration is moved by screw conveyor (C-503) to the alumina hydrate precipitation tank (T-524). There ammonium alum crystals are reacted with 25% ammonia solution from the ammonia absorption column (K-500) to release ammonium sulfate to the solution and precipitate a crystalline alumina hydrate. Undissolved solids are conveyed by horizontal apron conveyors to the bottom of the precipitator and are removed by an inclined conveyor. Retention time in the precipitator is approximately 3 hours.

Precipitate and liquor from the precipitation tank are reunited in the slurry distributor (X-507) and flow to the first alumina hydrate filtration filter (F-505).

Filtrate from the second alumina hydrate filtration is recycled countercurrently through the filter cake for three washes. The concentrated wash is added to the filtrate in the filtrate surge tank (T-532) and is pumped to the ammonia stripper (K-501). Overhead from the ammonia stripper is cooled to 105° F. and sent to the ammonia absorber (K-500); the stripper bottom is pumped to the second set of alum re-solution tanks (T-517).

Cake from the first alumina hydrate filtration is reslurried in the repulping tanks (T-535). Repulped hydrate is pumped to a distributor (X-511) and flows to the second set of alumina hydrate filters (F-506). Clear water is recycled countercurrently through the cake to wash the cake three times. The concentrated wash liquor is pumped to the alumina hydrate repulping tanks.

Wet cake from the second alumina hydrate filtration is conveyed (C-505) to dryer feed bin (T-547) and fed to oil fired rotary dryers (D-500). A bucket elevator (L-500) raises the dried hydrate to calciner feed bin (T-548). The dried material is fed to the rotary calciner (D-501) and calcined to alumina at a final temperature of 2190° F. Hot calcined alumina is cooled to 400° F. in a rotary cooler (E-509) and discharged to a storage silo (T-549).

2. Ammonium Sulfate Removal

Filtrate from the second alum filtration is pumped to the ammonium sulfate crystallizer feed tank (T-501) and from there to the triple effect evaporator crystallizer (CR-500). The concentrated slurry from the crystallizer is centrifuged (F-500) and the cake is conveyed to the Ammonium Sulfate Decomposition Section. (RMO 2017) Filtrate from the centrifuge is returned to the crystallizer feed tank.

A portion of the slurry from the crystallizer is continuously added to the concentrated acid filtrate liquor to form ammonium alum.

3. Layout Drawings of the Alumina Section are attached and numbered as follows:

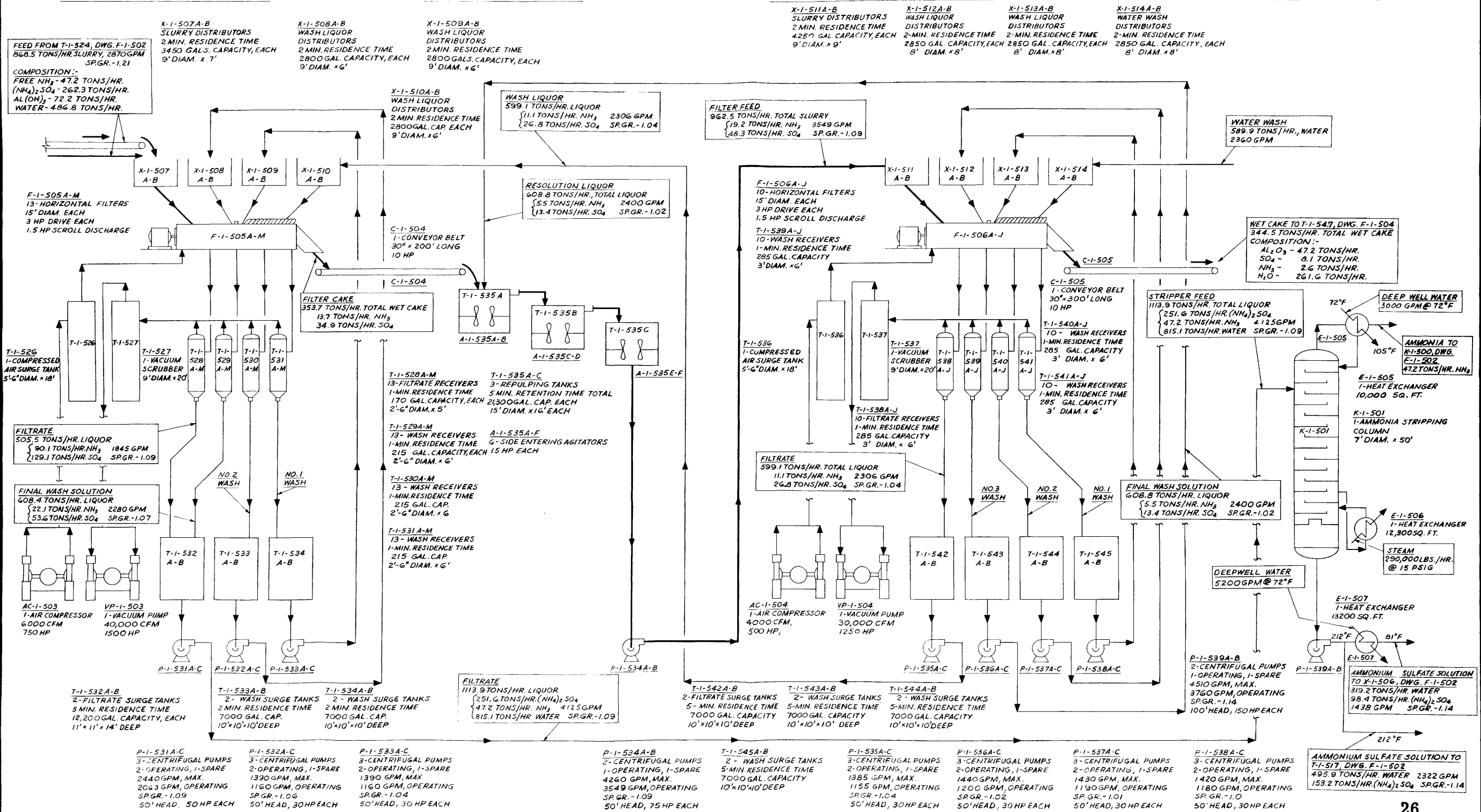
<u>Plant Size, Tons U/Year</u>	<u>Drawing Numbers</u>
450	L-1-500 and L-1-501
225	L-2-500 and L-2-501
100	L-3-500 and L-3-501

~ FIRST AL(OH)₃ FILTRATION ~

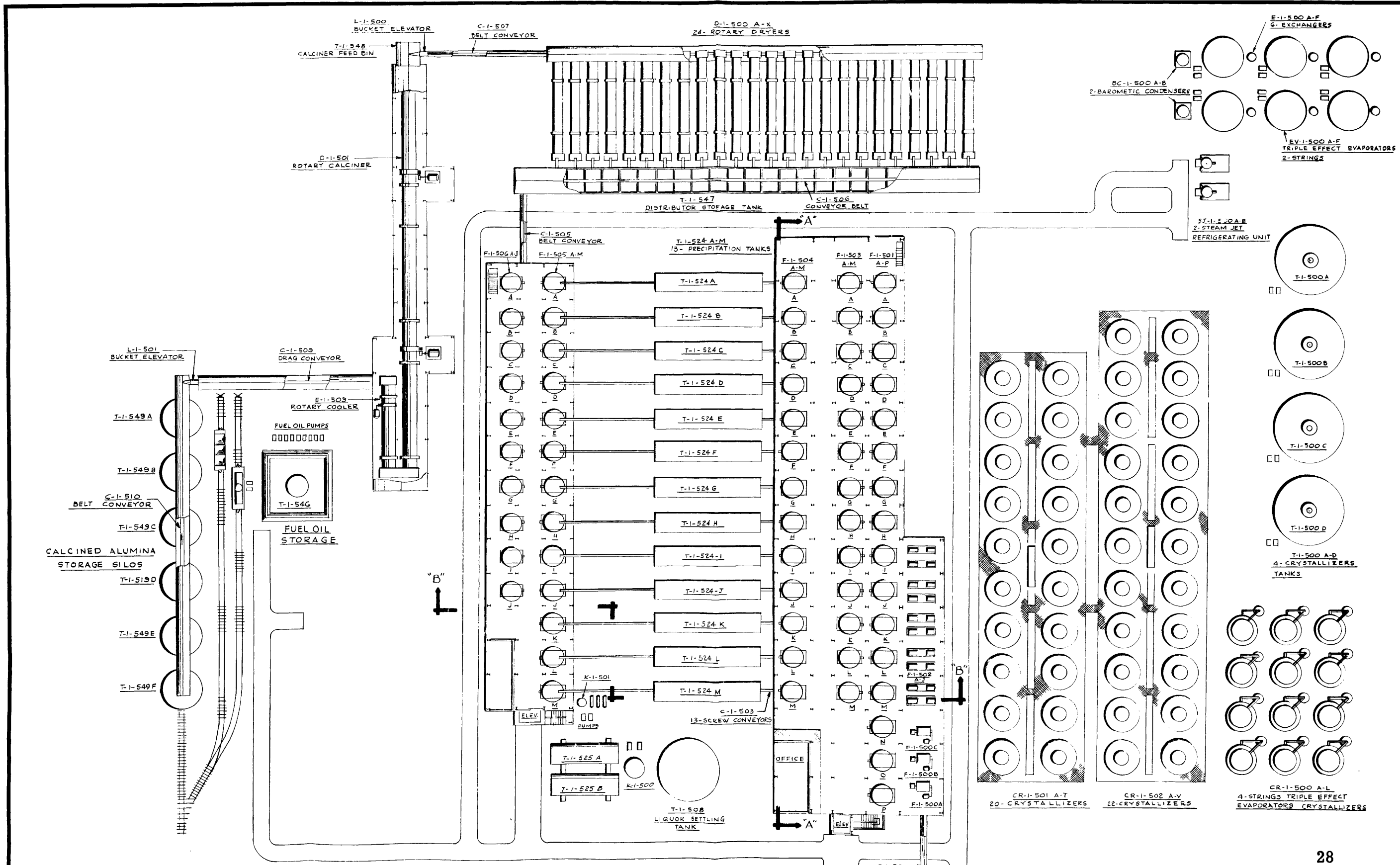
~ AL(OH)₃ REPULPING ~

~ SECOND AL(OH)₃ FILTRATION ~

~ AMMONIA RECOVERY ~



INTERNATIONAL MINERALS & CHEMICAL CORPORATION
MULBERRY, FLORIDA
RESEARCH

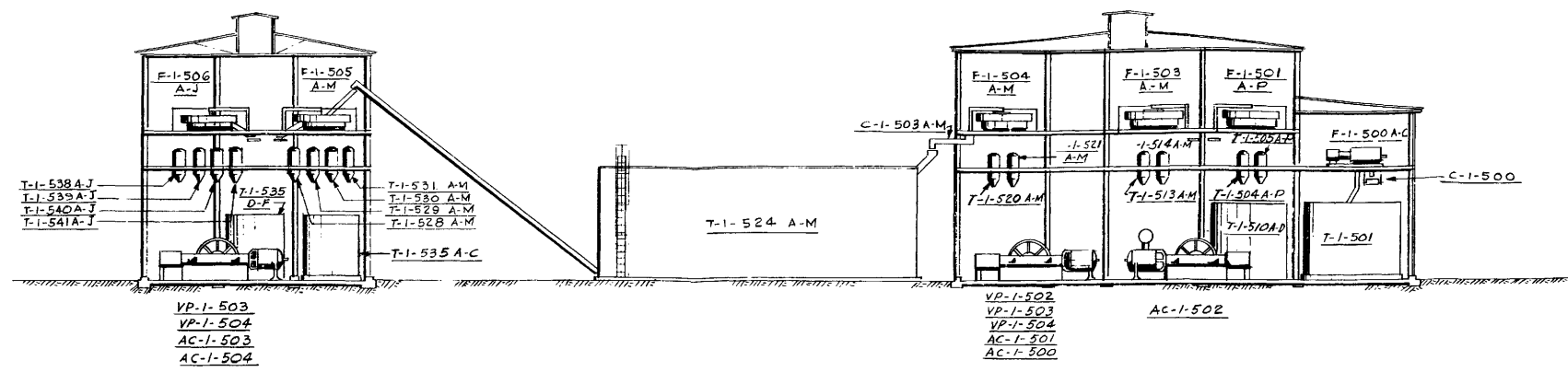


REFERENCE DRAWINGS	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	LOCATION OF JOB	TITLE	APPL. NO.
F-1-500 TO F-1-504 - FLOW DIAGRAMS SHEETS 1 TO 5.											SCALE 1/8" = 1'-0"		LAYOUT ALUMINA RECOVERY 450 TON UNIT	APPL. NO. L-1-500
													RESEARCH	DRWG. NO. L-1-500
														FILE NO.

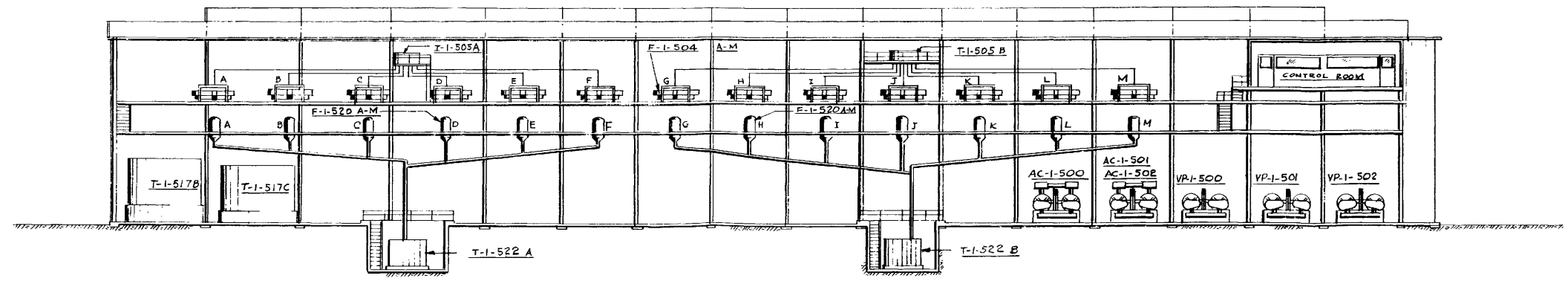
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 ADDRESS: MULBERRY, FLORIDA
 DIVISION: RESEARCH

TITLE: LAYOUT ALUMINA RECOVERY 450 TON UNIT


TO AMMONIA SULFATE DECOMPOSITION DWG. L-1-800



SECTION "B-B"

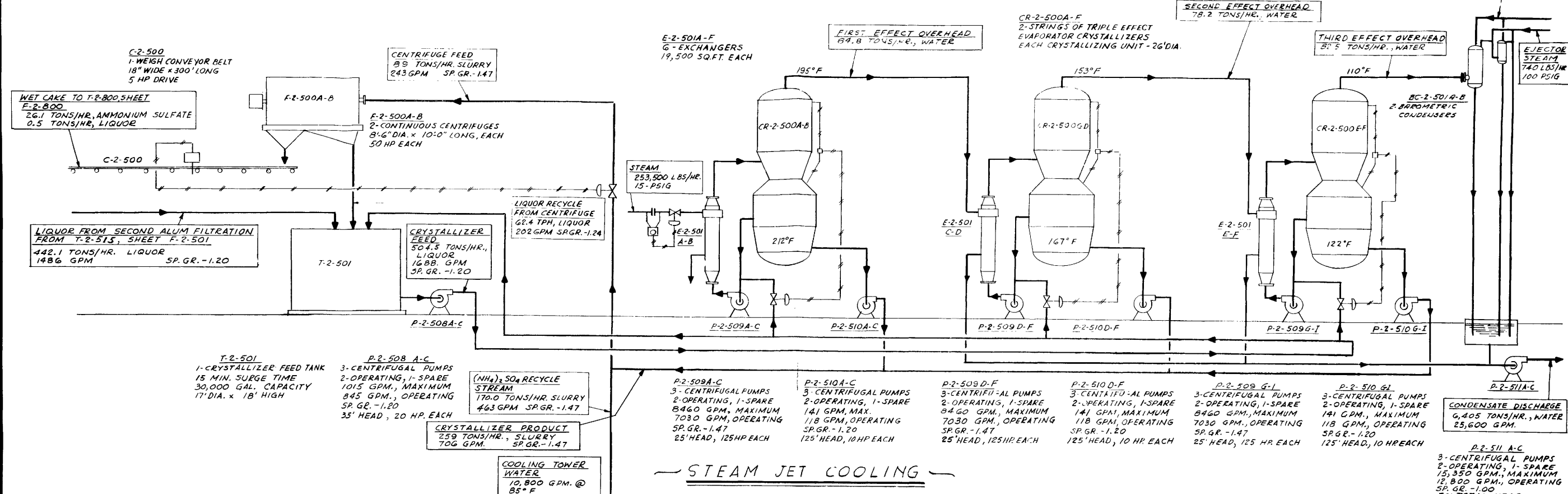


SECTION "A-A"

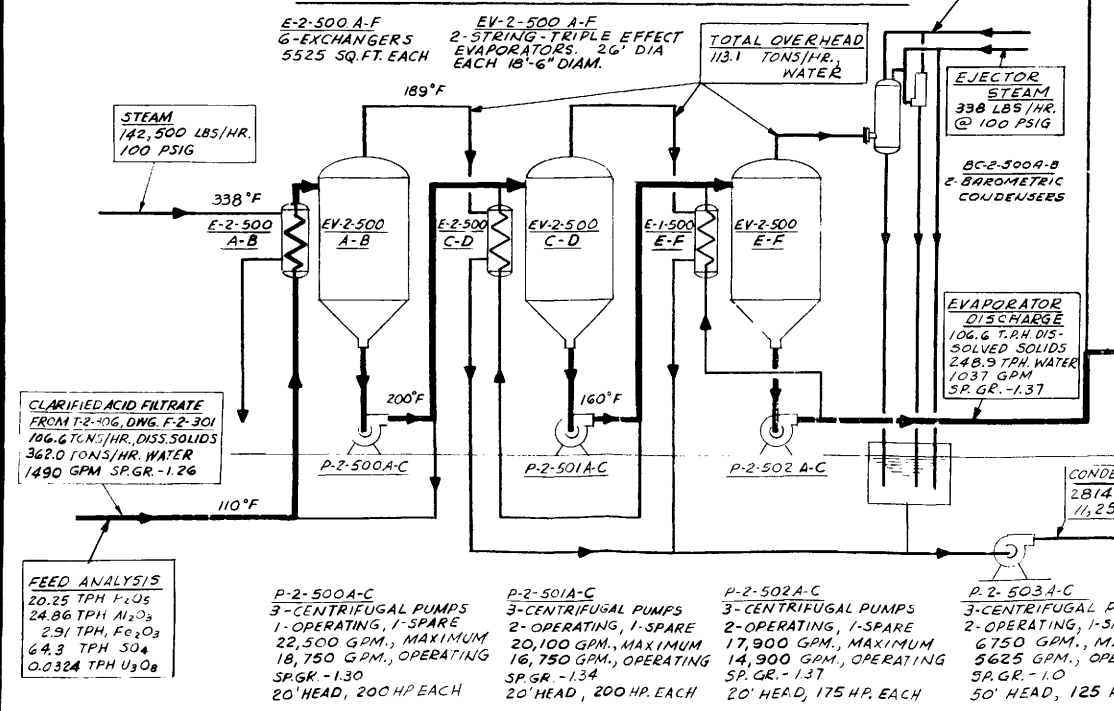
REFERENCE DRAWINGS L-1-500 LAYOUT	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE 0 5 10 15 20 FT	DATE	LOCATION OF JOB	 INTERNATIONAL MINERALS & CHEMICAL CORPORATION ADDRESS: MULBERRY, FLORIDA DIVISION: RESEARCH	TITLE SECTION C ALUMINA RECOVERY 450 TON UNIT	APPL. NO. DRWG. NO. L-1-501 FILE NO.
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AMMONIUM SULFATE REMOVAL

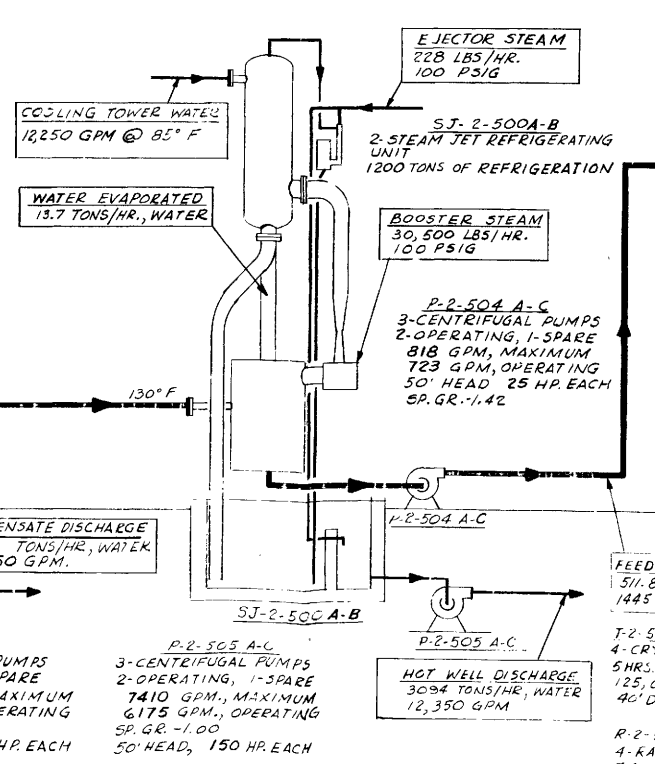
AMMONIUM SULFATE CRYSTALLIZATION



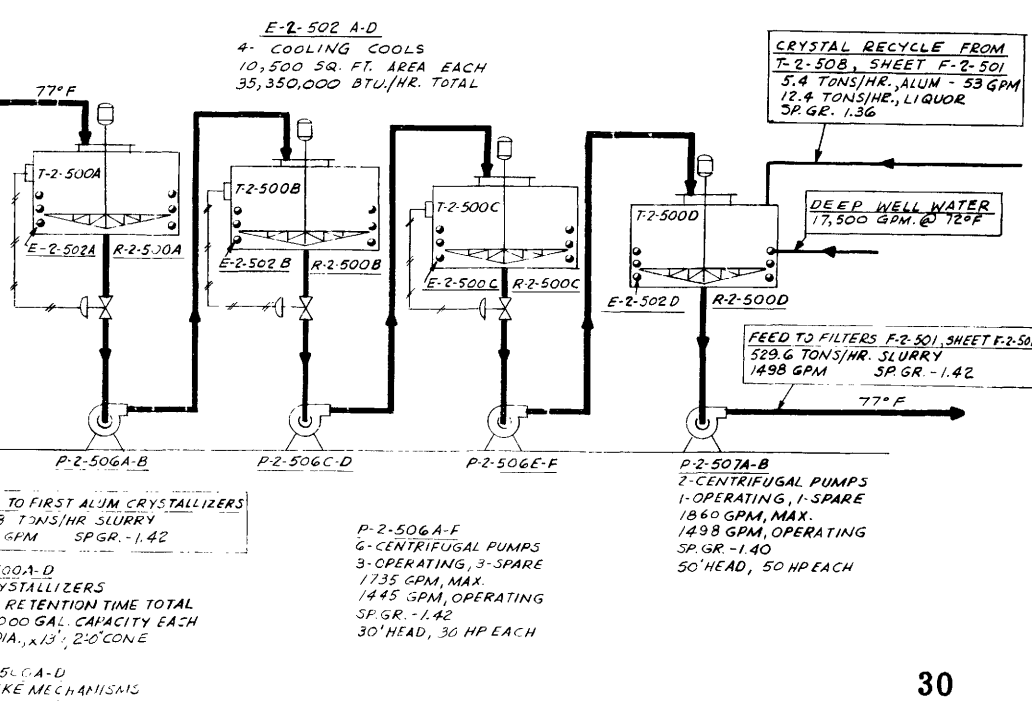
EVAPORATION OF ACID FILTRATE



STEAM JET COOLING



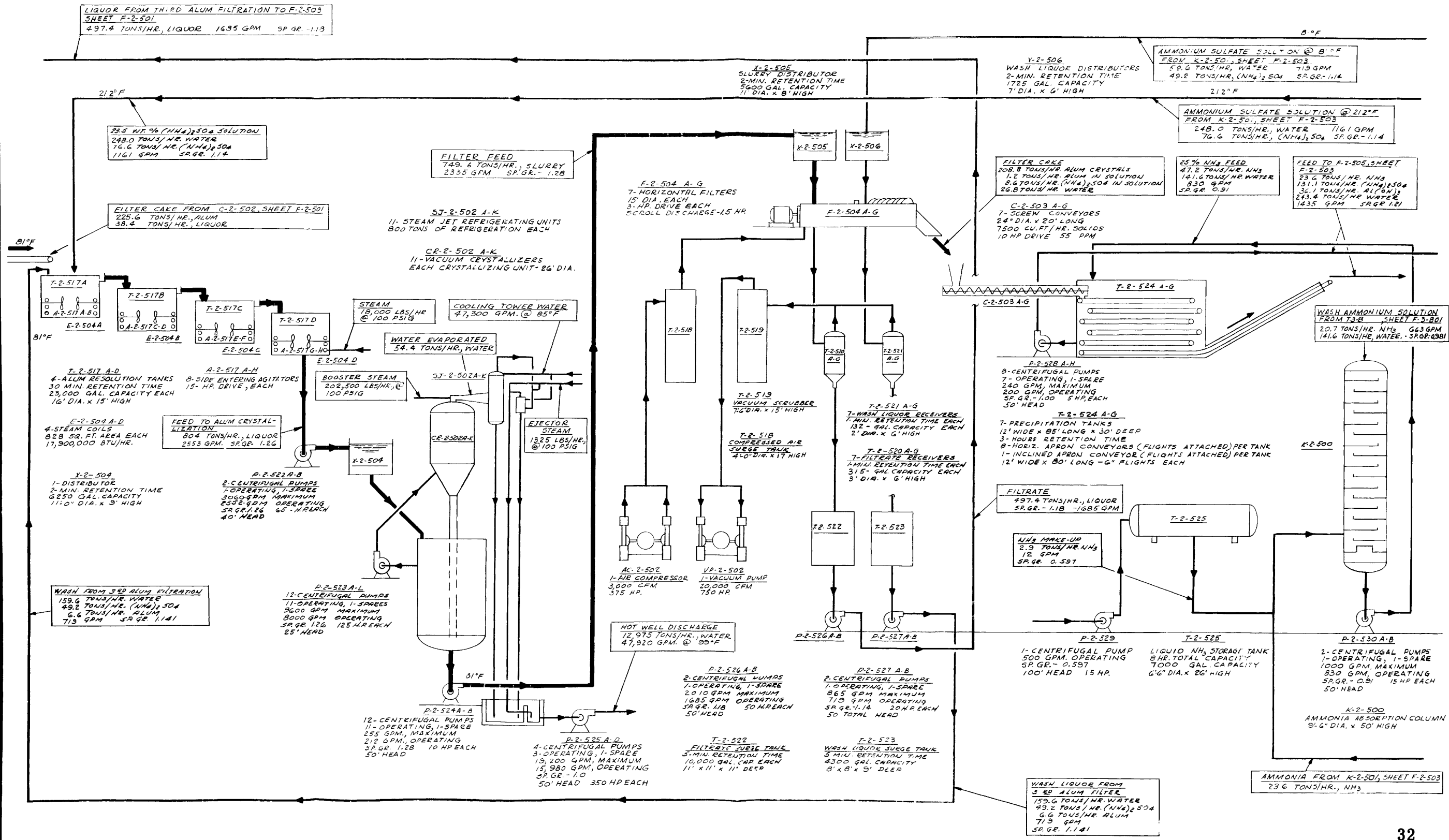
FIRST ALUM CRYSTALLIZATION



REFERENCE DRAWING	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	DATE	LOCATION OF JOB	TITLE	APPR. NO.	DRWG. NO.	FILE NO.
F-2-501 PROCESS FLOW DIAGRAM No. 2														PROCESS FLOW DIAGRAM			
F-2-502 " " " " " " " " " " " "														ALUMINA RECOVERY			
F-2-503 " " " " " " " " " " " "														225 TON UNIT			
F-2-504 " " " " " " " " " " " "														SHEET 1 OF 5			

INTERNATIONAL MINERALS & CHEMICAL CORPORATION
 ADDRESS: MURFREESBORO, TENN.
 DIVISION: RESEARCH

—SECOND REDISSOLVING OF ALUM— —THIRD ALUM CRYSTALLIZATION— —THIRD ALUM FILTRATION— —AL(OH)₃ PRECIPITATION— —NH₃ MAKE-UP—



REFERENCE DRAWING	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	DATE	LOCATION OF JOB	TITLE	APPR. NO.
F-2-500-PROCESS FLOW-SHEET No.1														PROCESS FLOW DIAGRAM	
F-2-501- " " " No.2														ALUMINA RECOVERY	F-2-502
F-2-503- " " " No.4														225 TON UNIT	
F-2-504- " " " No.5														SHEET-3 OF 5	

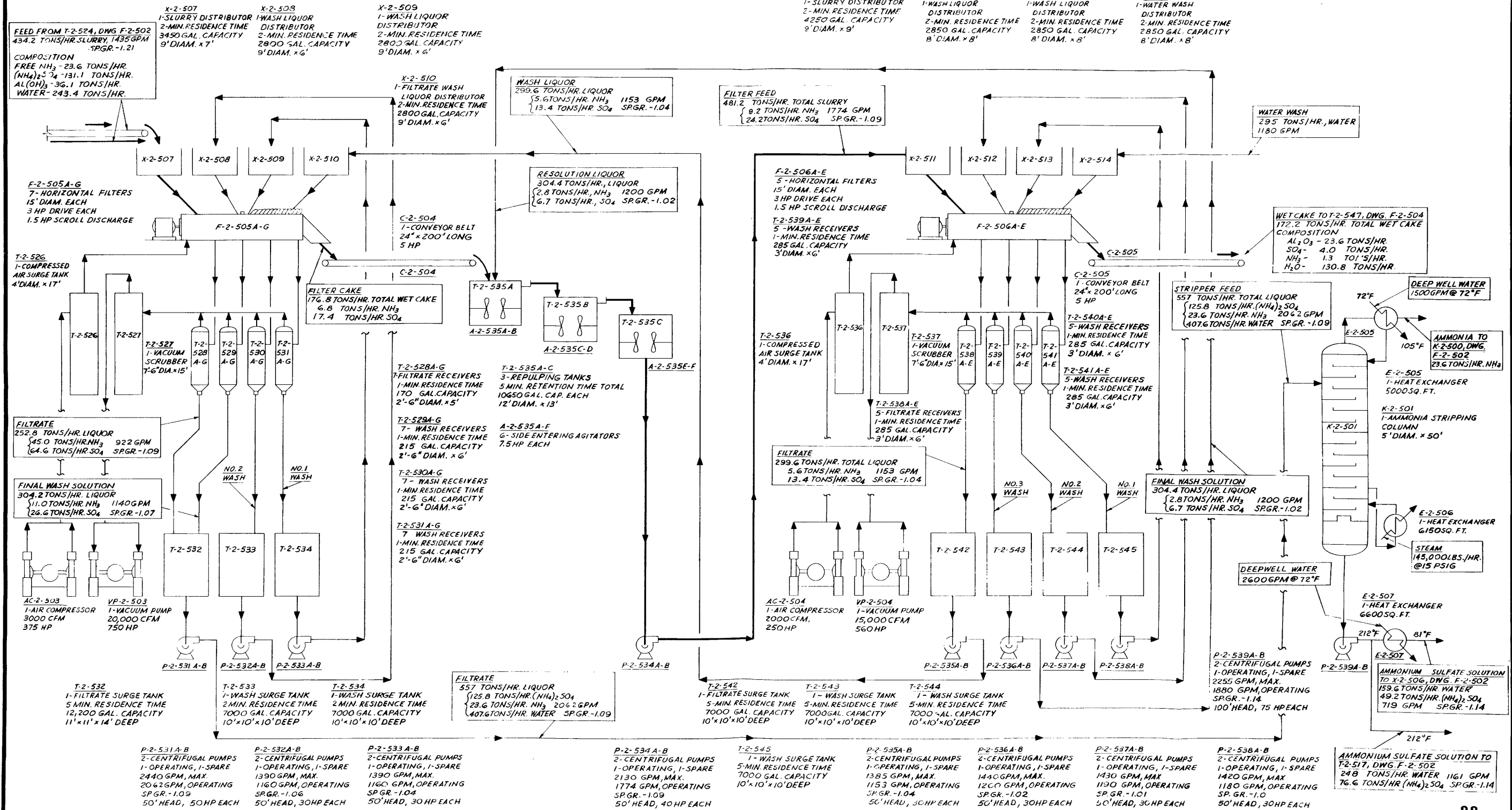
INTERNATIONAL MINERALS & CHEMICAL CORPORATION
 ADDRESS: MULBERN, FLORIDA
 DIVISION: RESEARCH

~ FIRST AL(OH)₃ FILTRATION ~

~ AL(OH)₃ REPULPING ~

~ SECOND AL(OH)₃ FILTRATION ~

~ AMMONIA RECOVERY ~

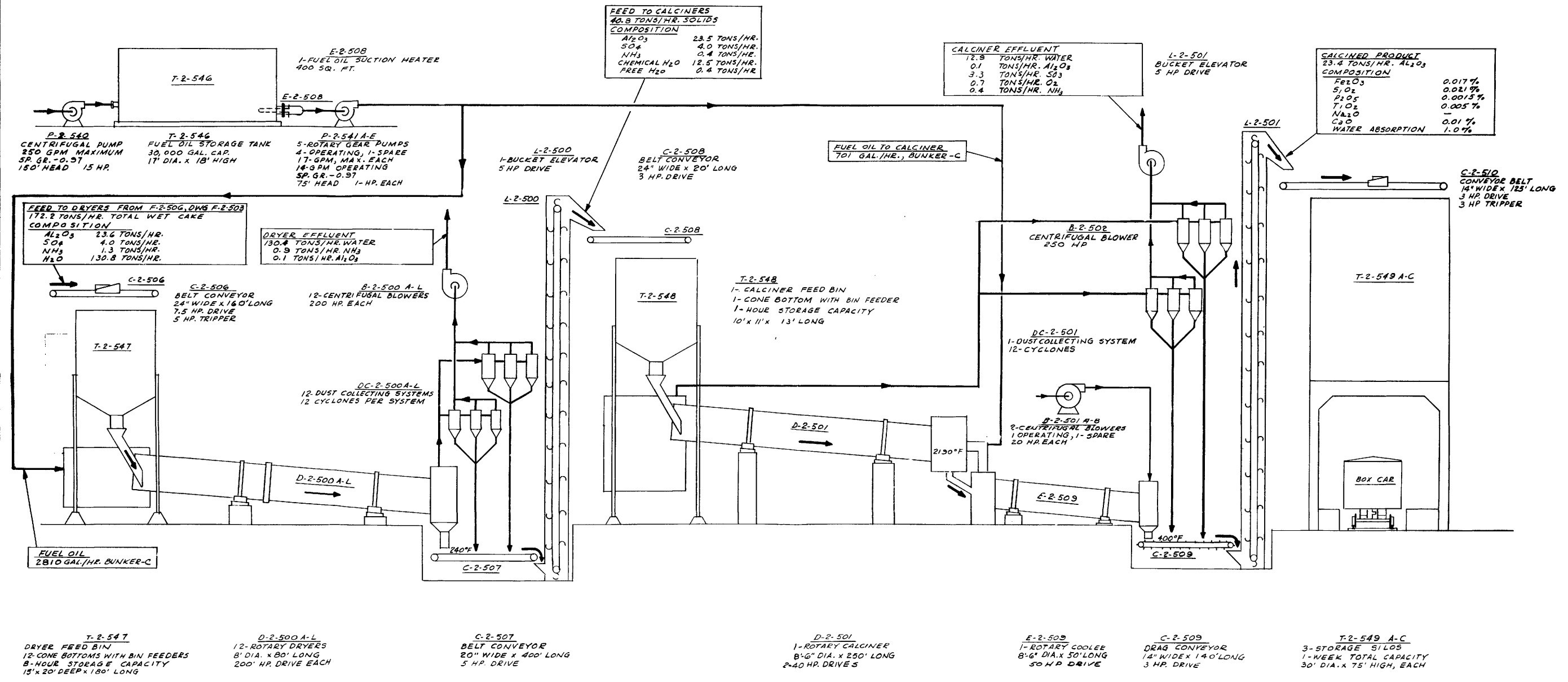


REFERENCE DRAWINGS	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	DATE	LOCATION OF JOB	INTERNATIONAL MINERALS & CHEMICAL CORPORATION	TITLE	APPN. NO.
F-2-500, PROCESS FLOW DIAG SHEET														ADDRESS: MILBERRY, FLORIDA	PROCESS FLOW DIAGRAM	
F-2-501, " " " "															ALUMINIA RECOVERY	
F-2-502, " " " "															225 TON UNIT	
F-2-504, " " " "															SHEET 4 OF 5	

— DRYING —

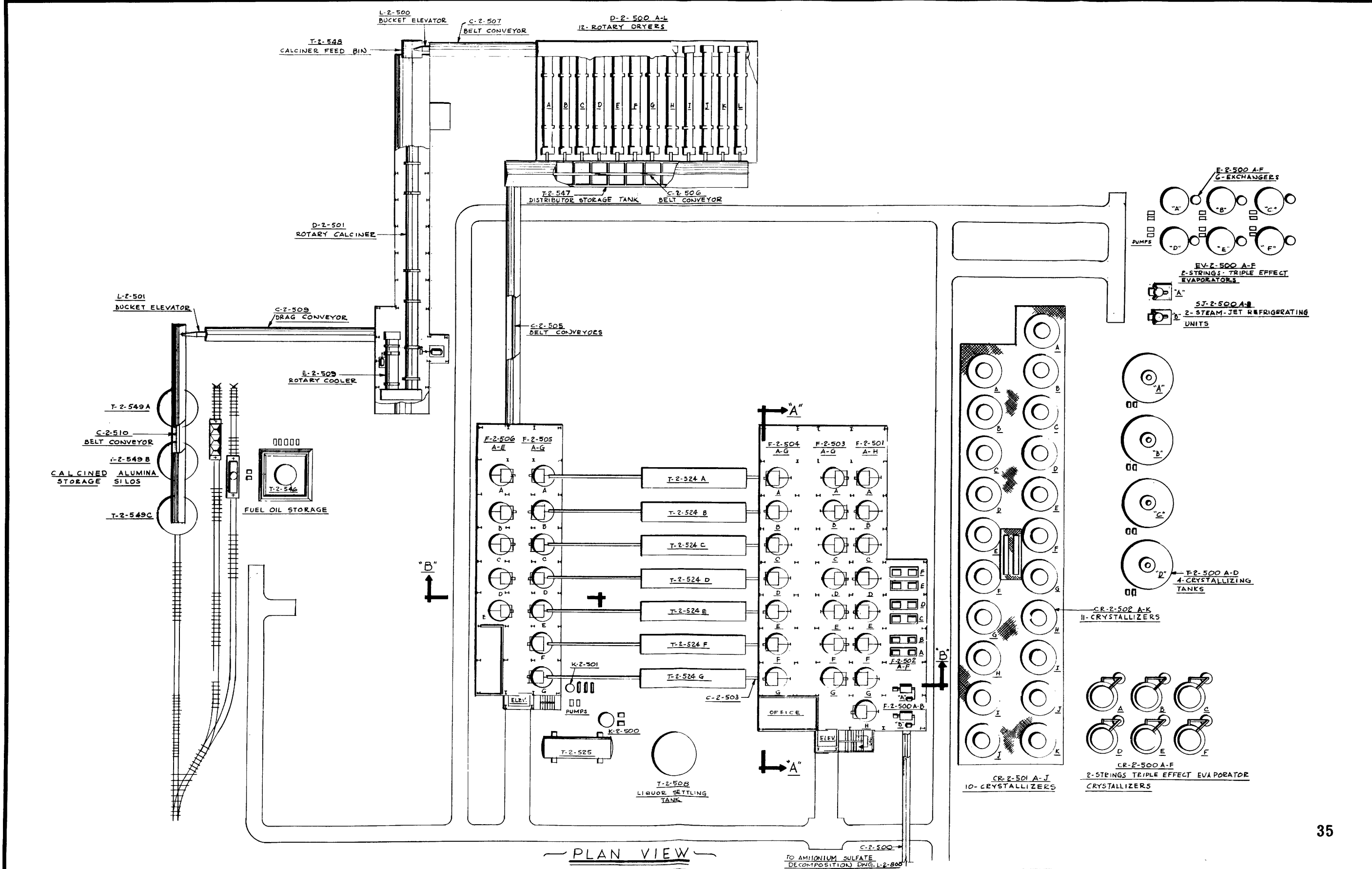
— CALCINING & COOLING —

— STORAGE & SHIPPING —



REFERENCE DRAWINGS	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	LOCATION OF JOB	TITLE	APPL. NO.
													PROCESS FLOW DIAGRAM ALUMINA RECOVERY 225 TON UNIT SHEET 5 OF 5	F-2-504

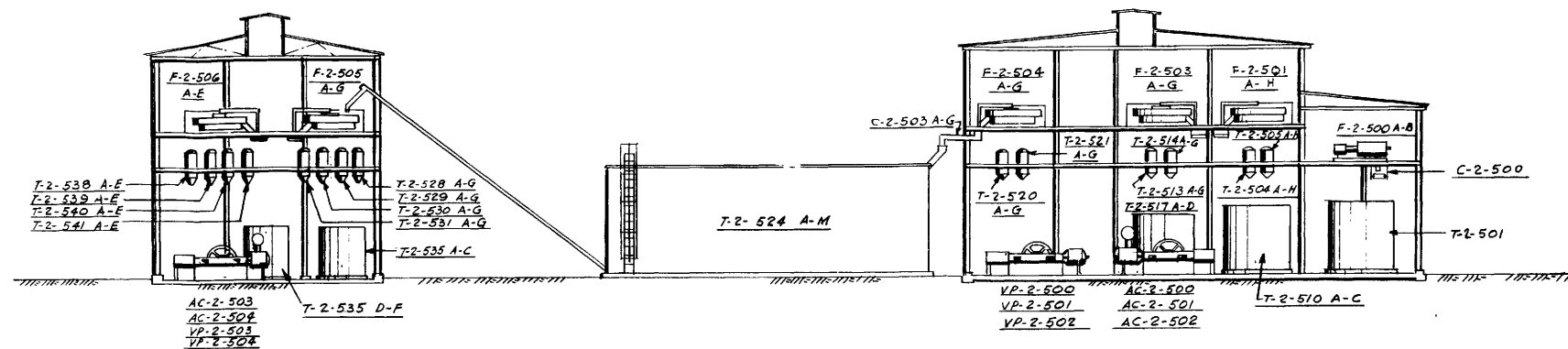
INTERNATIONAL MINERALS & CHEMICAL CORPORATION
ADDRESS: MULBERRY, FLORIDA
DIVISION: RESEARCH



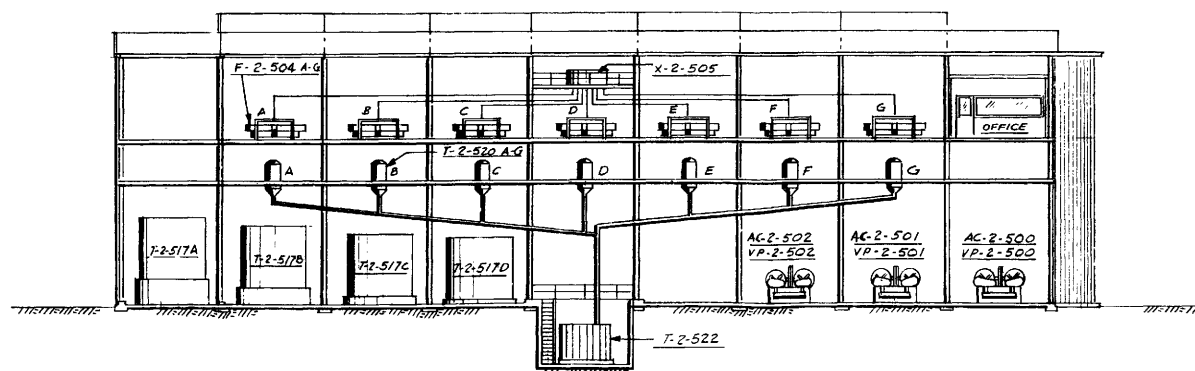
REFERENCE DRAWINGS	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	LOCATION OF JOB	TITLE	APPL. NO.
F-2-500 TO F-2-504 FLOW DIAGRAMS SHEETS 1 TO 5											1/4" = 1'-0"	RESEARCH	LAYOUT ALUMINA RECOVERY 225 TON UNIT	L-2-500

INTERNATIONAL MINERALS & CHEMICAL CORPORATION
 MULBERRY, FLORIDA
 DIVISION RESEARCH

TITLE
 LAYOUT
 ALUMINA RECOVERY
 225 TON UNIT
 APPL. NO. L-2-500
 FILE NO.



SECTION "B-B"



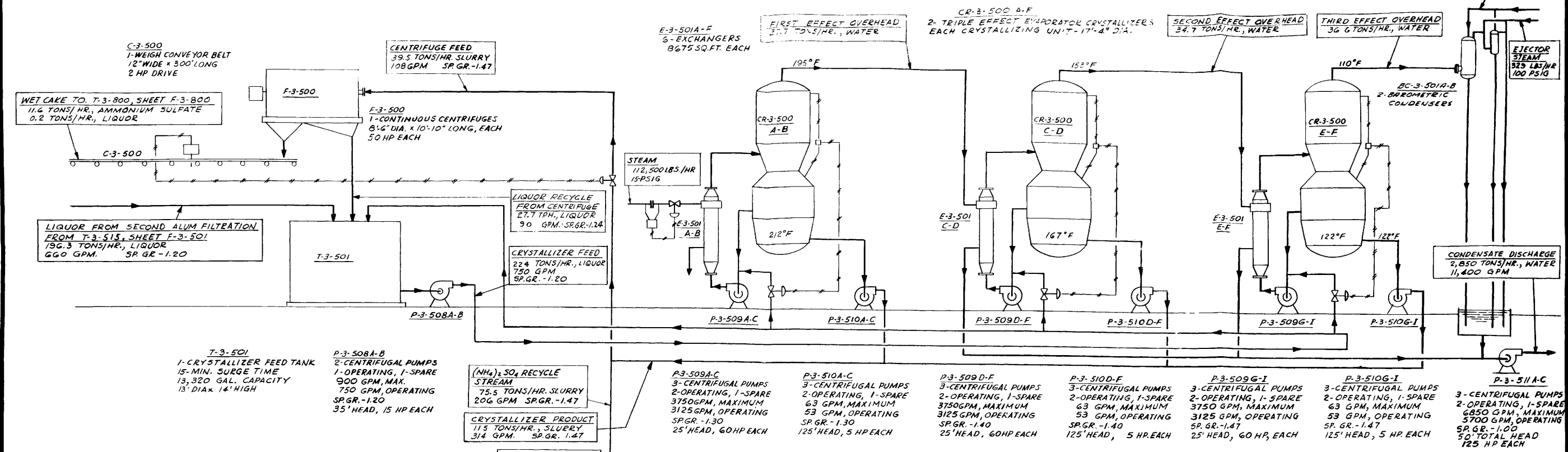
SECTION A-A

REFERENCE DRAWING	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	DATE	LOCATION OF JOB	DIVISION	SECTION	APPR. NO.
L-2-500 LAYOUT											SCALE 0 5 10 20 FT	6-16-53		RESEARCH	SECTIONS ALUMINA RECOVERY 225 TON UNIT	

INTERNATIONAL MINERALS & CHEMICAL CORPORATION
 ADDRESS: MULBERRY, FLORIDA
 DIVISION: RESEARCH

AMMONIUM SULFATE REMOVAL

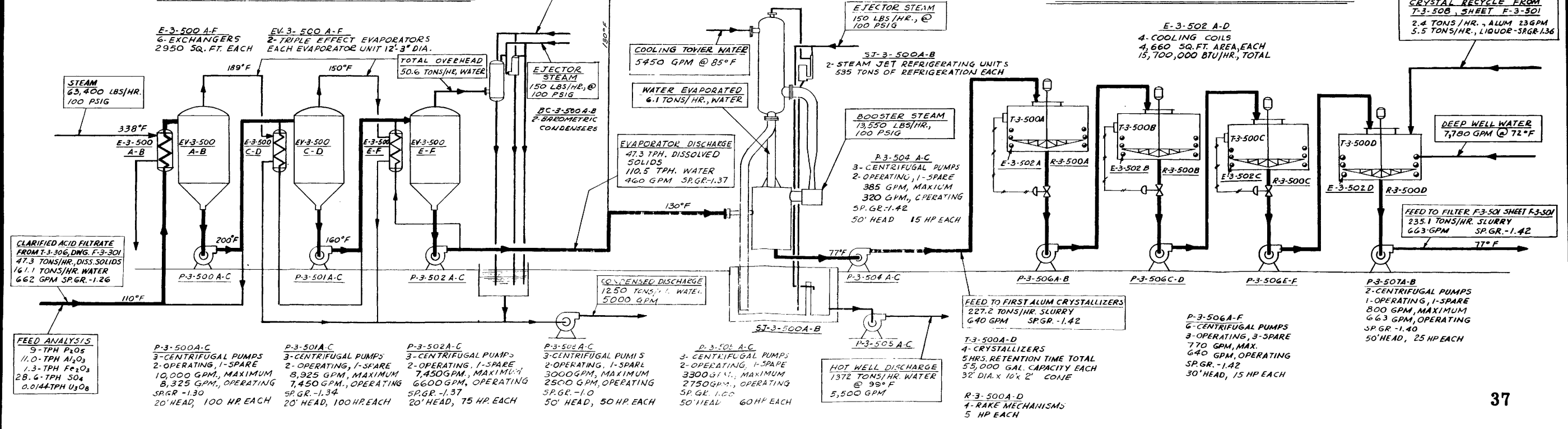
AMMONIUM SULFATE CRYSTALLIZATION



EVAPORATION OF ACID FILTRATE

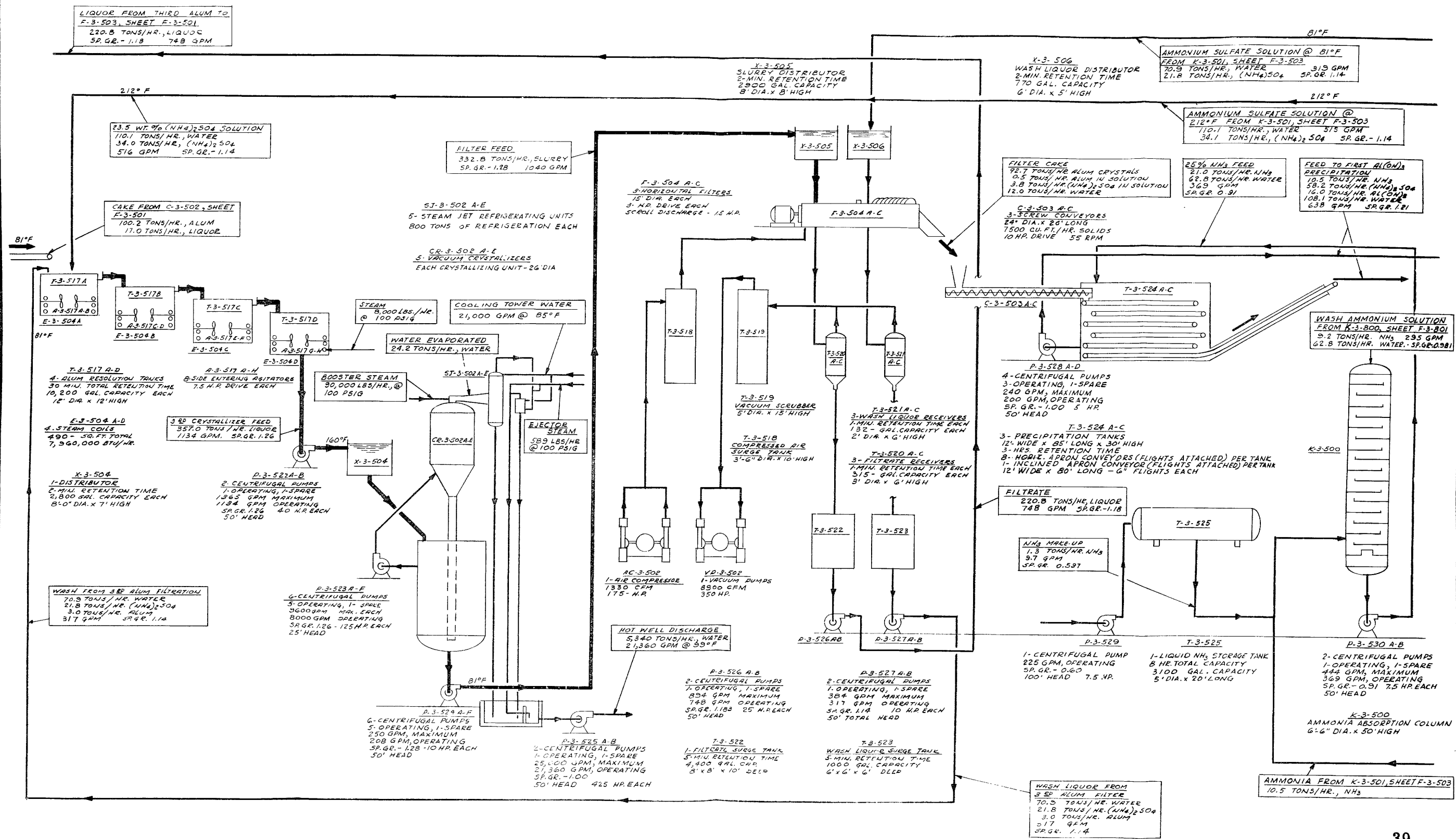
STEAM JET COOLING

FIRST ALUM CRYSTALLIZATION



REFERENCE DRAWINGS	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	DATE	LOCATION OF JOB	INTERNATIONAL MINERALS & CHEMICAL CORPORATION	TITLE	APPH. NO.
F-3-501 PROCESS FLOW DIAGRAM No. 2														RESEARCH	PROCESS FLOW DIAGRAM ALUMINA RECOVERY	
F-3-502															ALUMINA RECOVERY	
F-3-503															100 TON UNIT	
F-3-504															SHEET 1 OF 5	

— SECOND REDISSOLVING OF ALUM — — THIRD ALUM CRYSTALLIZATION — — THIRD ALUM FILTRATION — — $Al(OH)_3$ PRECIPITATION — — NH_4OH MAKE-UP —



REFERENCE DRAWINGS	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	DATE	LOCATION OF JOB	TITLE	APPN. NO.
F-3-500 - PROCESS FLOW DIAGRAM-SHT. 1														PROCESS FLOW DIAGRAM	
F-3-501	2													ALUMINA RECOVERY	F-3-502
F-3-503	4													100 TON UNIT	
F-3-504	5													SHEET No. 3 OF 5	

INTERNATIONAL MINERALS & CHEMICAL CORPORATION
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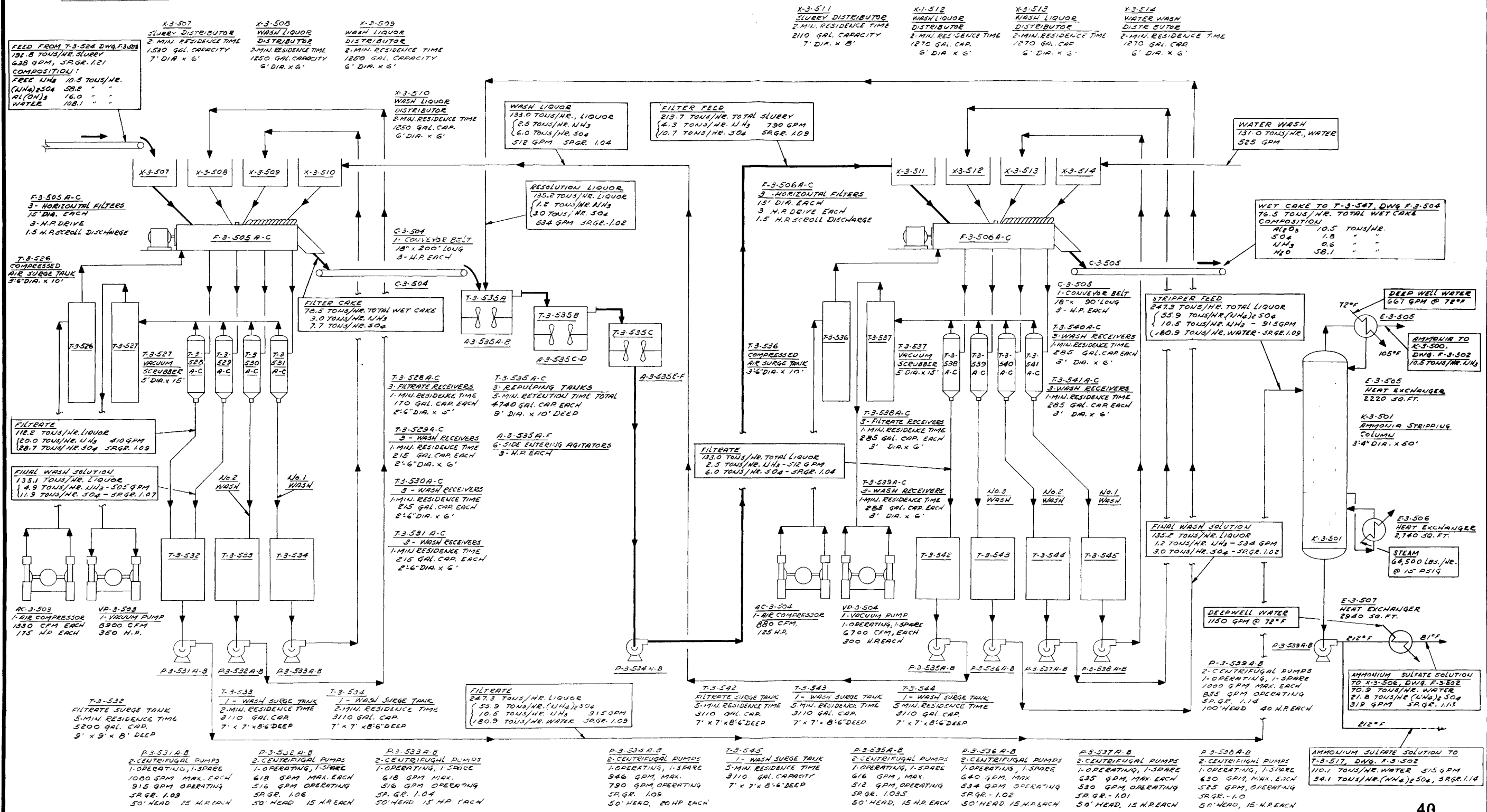
APPN. NO. F-3-502
 DRWG. NO. F-3-502
 FILE NO.

~ FIRST AL(OH)₃ FILTRATION ~

~ AL(OH)₃ REPULPING ~

~ SECOND AL(OH)₃ FILTRATION ~

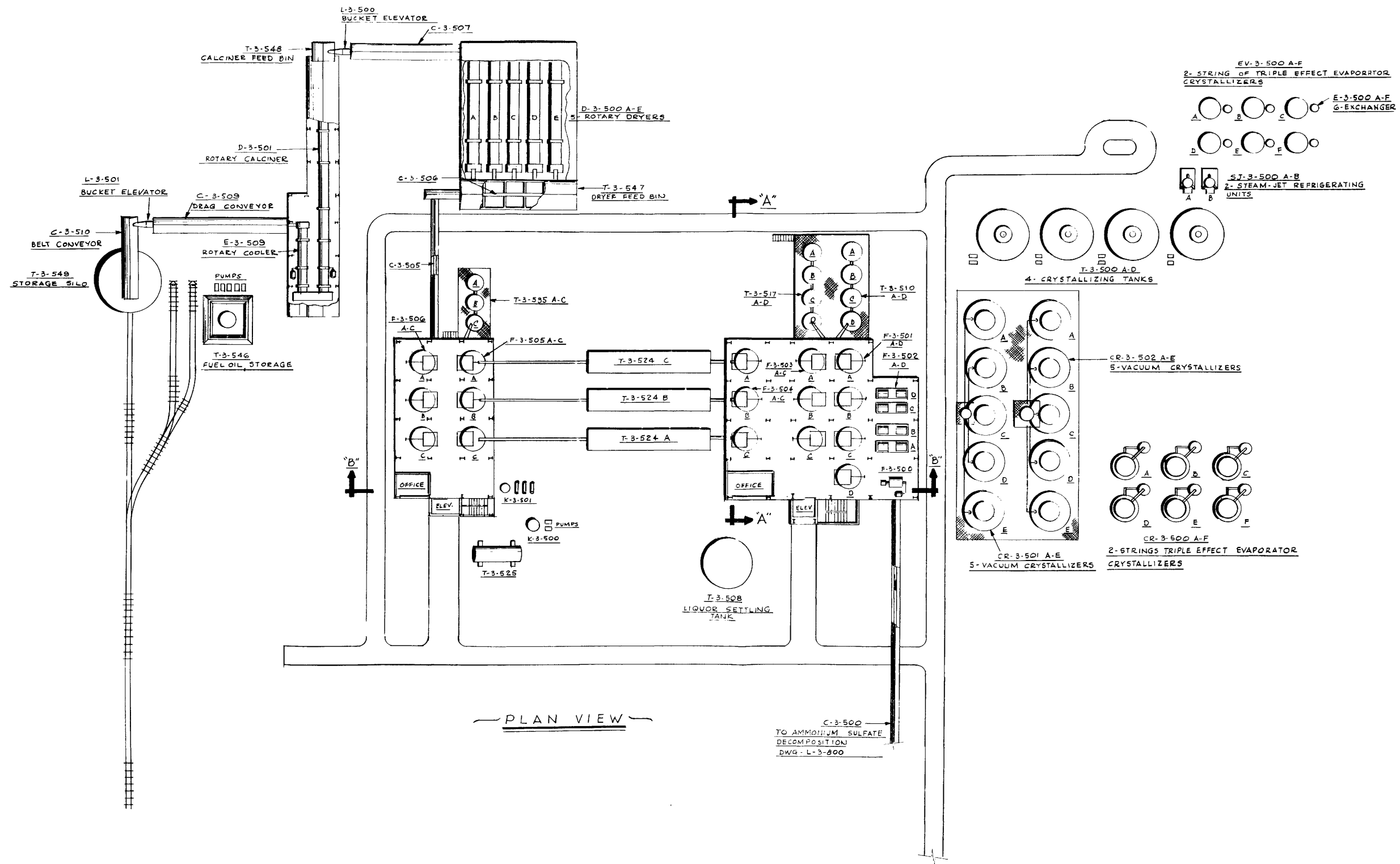
~ AMMONIA RECOVERY ~



REFERENCE DRAWING	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	LOCATION OF JOB	TITLE	APPH. NO.
F-3-500, PROCESS FLOW DIAG. SHEET 1											SCALE	RESEARCH	PROCESS FLOW DIAGRAM ALUMINA RECOVERY 100 TON UNIT SHEET 4 OF 5	
F-3-501, " " " " 2														
F-3-502, " " " " 3														
F-3-504, " " " " 5														

INTERNATIONAL MINERALS & CHEMICAL CORPORATION
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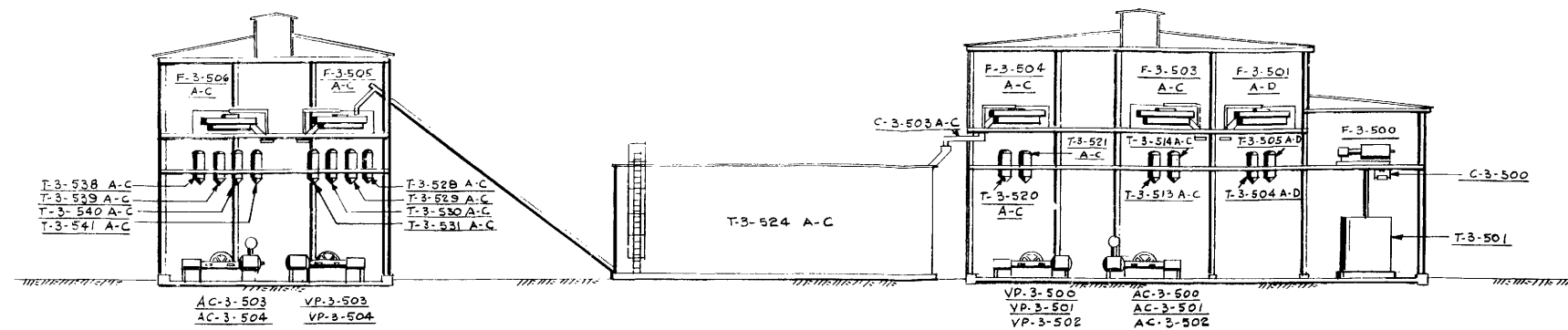
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 FILE NO.



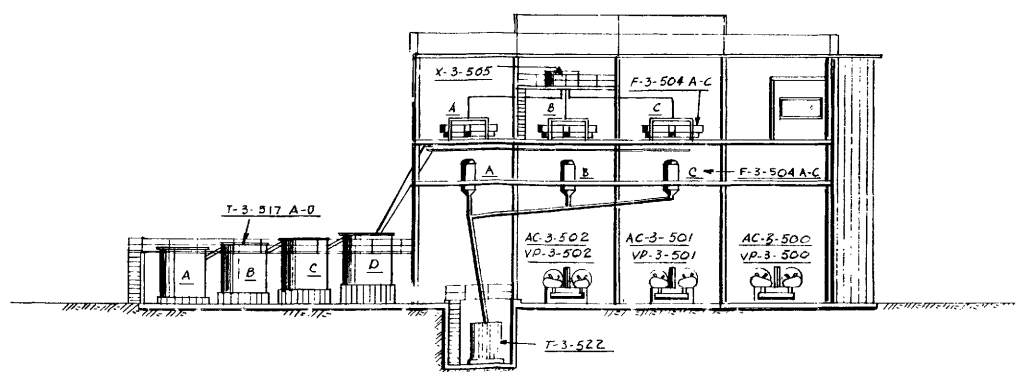
PLAN VIEW

C-3-500
TO AMMONIUM SULFATE
DECOMPOSITION
DWG. L-3-000


REFERENCE DRAWINGS	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE	DATE	LOCATION OF JOB	TITLE	APPL. NO.
F-3-500 TO F-3-504 FLOW DIAGRAM SHEETS 1 TO 5											SCALE 0.100 5/8"	6-24-53		LAYOUT ALUMINA RECOVERY 100 TON UNIT	L-3-500
													INTERNATIONAL & CHEMICAL CORPORATION MULBERRY, FLORIDA		
													RESEARCH		



SECTION "B-B"



SECTION "A-A"

REFERENCE DRAWINGS L-3-500 LAYOUT	MARK	REVISION	BY	DATE	MARK	REVISION	BY	DATE	APPROVED BY	DATE	SCALE 0 5 10 15 20 FT	DATE 6-23-53	LOCATION OF JOB	 INTERNATIONAL MINERALS & CHEMICAL CORPORATION ADDRESS: MULBERRY, FLORIDA DIVISION: RESEARCH	WLS SECTIONS ALUMINA RECOVERY 225 TON UNIT	APPR. NO. DRWG. NO. L-3-501 FILE NO.
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IV. ECONOMIC EVALUATION

A. DETAILED CAPITAL COST ESTIMATE

Detailed analyses of the capital cost estimates for the Alumina Recovery Section of the three different size plants follow. Estimates include cost of equipment, buildings and construction fees.

1. ALUMINA RECOVERY SECTION--450 Ton Unit

a. Process Equipment--

<u>Item No.</u>	<u>No.</u> <u>Items</u>	<u>Description</u>	<u>Installed</u> <u>Cost</u>
A-1-510A-H	8	Agitators, 25 hp.	\$ 42,820
A-1-517A-H	8	Agitators, 25 hp.	42,820
A-1-535A-F	6	Agitators, 15 hp.	27,080
AC-1-500	1	Air compressor, 6000 cfm, 750 hp.	87,000
AC-1-501	1	Air compressor, 6000 cfm, 750 hp.	87,000
AC-1-502	1	Air compressor, 6000 cfm, 750 hp.	87,000
AC-1-503	1	Air compressor, 6000 cfm, 750 hp.	87,000
AC-1-504	1	Air compressor, 4000 cfm, 500 hp.	60,400
C-1-500	1	Weigh conveyor belt, 18" x 300', 5 hp.	35,850
C-1-501	1	Belt conveyor, 36" x 200', 10 hp.	20,755
C-1-502	1	Belt conveyor, 36" x 200'	20,755
C-1-503A-M	13	Screw Conveyors, 24" x 30', 10 hp.	115,650
C-1-504	1	Belt conveyor, 30" x 200', 10 hp.	19,550
C-1-505	1	Belt conveyor, 30" x 200', 10 hp.	19,550
C-1-506	1	Belt conveyor, 30" x 350', 15 hp.	66,250
C-1-508	1	Belt conveyor, 24" x 25', 5 hp.	4,840
C-1-507	1	Belt conveyor, 24" x 400', 10 hp.	28,650
C-1-510	1	Belt conveyor, 18" x 250', 5 hp.	40,110
C-1-509	1	Belt conveyor, 18" x 140', 5 hp.	8,840
CR-1-500A-L	12	(Crystallizers, 26' dia.)	
E-1-501A-L	12	(Heat Exchangers)	
P-1-509 A-O	15	(Circulating Pumps)	4,406,500
P-1-510 A-O	15	(Slurry Pumps)	
CR-1-501A-T	20	Vacuum crystallizers, 26' dia.	4,027,000
CR-1-502A-V	22	Vacuum crystallizers, 26' dia.	4,429,700
D-1-500 A-X	24	Rotary Dryers, 8' dia. x 80'	5,040,000
DC-1-500A-X	24	Dust collectors,	792,000
B-1-500A-X	24	Centrifugal blowers, 200 hp.	650,400
D-1-501	1	Rotary calciner, 10' dia. x 300', 75 hp.	529,320
DC-1-501	1	Dust collectors	31,000
B-1-502	1	Fan, 300 hp.	25,800

a. Process Equipment --450 Ton Unit --Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
E-2-509	1	Rotary Cooler, 9'9"x 70', 100 hp.	\$ 181,860
B-1-501A-B	2	Blowers, 40 hp.	18,130
E-1-500A-F	6	Exchangers, 11,050 s. f.	414,600
E-1-502A-D	4	Cooling coils, 21,000 s. f.	90,000
E-1-503A-D	4	Heating coils, 6,200 s. f.	29,000
E-1-504A-D	4	Steam coils, 1,655 s. f.	8,500
E-1-505	1	Condenser, 3,400 s. f.	13,500
E-1-506	1	Reboiler, 12,300 s. f.	46,400
E-1-507	1	Cooler, 13,200 s. f.	48,400
E-1-508A-B	2	Suction heaters, 400 s. f.	3,100
EV-1-500A-F	6	Evaporators, 26' dia. x 20'	853,600
F-1-500A-C	3	Centrifuges, 178 tph, 100 hp.	111,240
F-1-501A-P	16	Horizontal filters, 15' dia., 3 hp.	765,320
F-1-502A-J	10	Polishing filters, 1304 s. f.	340,000
F-1-503A-M	13	Horizontal filters, 15' dia., 3 hp.	621,822
F-1-504A-M	13	Horizontal filters, 15' dia., 3 hp.	621,822
F-1-505A-M	13	Horizontal filters, 15' dia., 3 hp.	621,822
F-1-506A-J	10	Horizontal Filters, 15'dia., 3 hp.	482,585
K-1-500	1	Ammonia absorption column, 13'6x50'	41,200
K-1-501	1	Ammonia stripping column, 7' x 50'	20,240
L-1-500	1	Bucket elevator, 81.5 tph, 10 hp.	9,350
L-1-501	1	Bucket elevator, 46.8 tph, 10 hp.	9,350
P-1-500A-D	4	Pumps, 37,500 gpm, 400 hp.	206,000
P-1-501A-D	4	Pumps, 33,500 gpm, 350 hp.	202,000
P-1-502A-D	4	Pumps, 29,800 gpm, 325 hp.	202,000
P-1-503A-C	3	Pumps, 11,250 gpm, 225 hp.	80,400
P-1-504A-C	3	Pumps, 1445 gpm, 50 hp.	20,780
P-1-505A-C	3	Pumps, 13,500 gpm, 275 hp.	80,400
P-1-506A-F	6	Pumps, 2890 gpm, 60 hp.	57,160
P-1-507A-B	2	Pumps, 2995 gpm, 100 hp.	25,920
P-1-511A-E	5	Pumps, 12,800 gpm, 250 hp.	133,000
P-1-508A-E	5	Pumps, 845 gpm, 20 hp.	19,800
P-1-512A-C	3	Pumps, 840 gpm, 25 hp.	12,540
P-1-513A-C	3	Pumps, 740 gpm, 20 hp.	12,390
P-1-514A-B	2	Pumps, 105 gpm, 5 hp.	5,370
P-1-516A-B	2	Pumps, 4706 gpm, 125 hp.	34,500
P-1-517A-U	21	Pumps, 7580 gpm, 100 hp.	305,700
P-1-515A-B	2	Pumps, 4706 gpm, 300 hp.	56,000

a. Process Equipment -- 450 Ton Unit--Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>In stalled Cost</u>
P-1-518A-U	21	Pumps, 212 gpm, 10 hp.	\$ 59,925
P-1-519A-F	6	Pumps, 18,750 gpm, 350 hp.	177,000
P-1-520A-C	3	Pumps, 1485 gpm, 50 hp.	20,780
P-1-521A-C	3	Pumps, 760 gpm, 20 hp.	12,390
P-1-522A-B	2	Pumps, 5106 gpm, 150 hp.	37,600
P-1-523A-W	23	Pumps, 8000 gpm, 125 hp.	397,900
P-1-524A-W	23	Pumps, 212 gpm, 10 hp.	65,675
P-1-525A-F	5	Pumps, 19,150 gpm, 375 hp.	150,000
P-1-526A-C	3	Pumps, 1685 gpm, 50 hp.	20,780
P-1-527A-C	3	Pumps, 719 gpm, 20 hp.	11,490
P-1-528A-N	14	Pumps, 200 gpm, 5 hp.	23,590
P-1-529	1	Pump, 1000 gpm, 25 hp.	2,730
P-1-530A-B	2	Pumps, 1660 gpm, 30 hp.	7,380
P-1-531A-C	3	Pumps, 2035 gpm, 50 hp.	22,080
P-1-532A-C	3	Pumps, 1160 gpm, 30 hp.	17,100
P-1-533A-C	3	Pumps, 1160 gpm, 30 hp.	17,100
P-1-534A-B	2	Pumps, 3549 gpm, 75 hp.	22,040
P-1-535A-C	3	Pumps, 1200 gpm, 30 hp.	17,100
P-1-536A-C	3	Pumps, 1200 gpm, 30 hp.	17,100
P-1-537A-C	3	Pumps, 1190 gpm, 30 hp.	17,100
P-1-538A-C	3	Pumps, 1180 gpm, 30 hp.	17,100
P-1-539A-B	2	Pumps, 3760 gpm, 150 hp.	27,700
P-1-540	1	Pump, 500 gpm, 25 hp.	2,430
P-1-541A-I	9	Pumps, 13 gpm, 1 hp.	12,420
P-1-542A-B	2	Pumps, 1576 gpm, 100 hp.	21,520
SJ-1-500A-B	2	Steam Jet Refrigeration Units, 2400 tons	349,000
SJ-1-501A-T	20	Steam Jet Refrigeration Units, 860 tons	1,410,000
SJ-1-502A-V	22	Steam Jet Refrigeration Units, 800 tons	1,477,000
T-1-500A-D	4	Crystallizers, 250,000 gals.	590,000
R-1-500A-D	4	Rake mechanisms, 50' dia., 15 hp.	64,120
T-1-501	1	Feed Tank, 60,000 gals,	46,200
T-1-502	1	Compressed air receiver 5'6 x 18'	2,050
T-1-503	1	Vacuum scrubber, 9' x 20'	3,900
T-1-504 A-P	16	Filtrate Receivers, 117 gals.	19,200
T-1-505A-P	16	Wash Receivers, 117 gals.	19,200
T-1-506A-B	2	Filtrate Surge Tanks, 5000 gals.	9,400
T-1-507A-B	2	Wash Liquor Surge Tanks, 5000 gals.	9,400
T-1-508	1	Settling Tank, 500,000 gals.	179,000

a. Process Equipment---450 Ton Unit---Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
R-1-508	1	Rake mechanism, 25 hp.	\$ 16,740
T-1-509	1	Filtrate surge tank, 28,000 gals.	26,040
T-1-510A-D	4	Alum Redissolving tanks, 50,000 gals.	156,400
T-1-511	1	Compressed Air Receiver, 5'6" x 18'	2,050
T-1-512	1	Vacuum Scrubber, 9' dia. x 20'	3,900
T-1-513	1	Filtrate Receivers, 275 gals.	40,700
T-1-514	1	Wash Receivers, 140 gals.	16,200
T-1-515A-B	2	Filtrate Surge Tank, 9000 gals.	15,600
T-1-516A-B	2	Wash Liquor Surge Tank, 4500 gals.	9,400
T-1-517A-D	4	Alum Resolution Tanks, 46,000 gals.	158,600
T-1-518	1	Compressed Air Tank, 5'6 x 18'	2,050
T-1-519	1	Vacuum scrubber, 9' dia. x 20'	3,900
T-1-520A-M	13	Filtrate Receivers, 315 gals.	41,700
T-1-521A-M	13	Wash Liquor Receivers, 132 gals.	16,200
T-1-522A-B	2	Filtrate Surge Tank, 10,000 gals.	15,200
T-1-523A-B	2	Wash Liquor Surge Tank, 4,300 gals.	9,200
T-1-524A-M	13	Precipitation Tanks, 12' w x 85' lg. x 30' deep	5,074,050
T-1-525A-B	2	Liquid NH ₃ Storage Tanks, 76,000 gals.	97,000
T-1-526	1	Compressed Air Tank, 5'6 dia. x 18'	2,050
T-1-527	1	Vacuum Scrubber, 9' dia. x 20'	3,900
T-1-528A-M	13	Filtrate Receivers, 2'6 x 5'	16,300
T-1-529A-M	13	Filtrate Receivers, 2'6 x 6'	17,600
T-1-530A-M	13	Wash Receivers, 2'6 x 6'	17,600
T-1-531A-M	13	Wash Receivers, 2'6" x 6'	17,600
T-1-532A-B	2	Filtrate Surge Tanks, 12,200 gals.	18,200
T-1-533A-B	2	Wash Surge Tanks, 7000 gals.	12,200
T-1-534A-B	2	Wash Surge Tanks, 7000 gals.	12,200
T-1-535A-C	3	Repulping Tanks, 21,300 gals.	87,000
T-1-536 A-C	3	Compressed Air Surge Tank, 5'6" x 18"	2,050
T-1-537	1	Vacuum Scrubber, 9' x 20'	3,900
T-1-538 A-J	10	Filtrate Receivers, 285 gals.	30,700
T-1-539A-J	10	Wash Receivers, 285 gals.	30,700
T-1-540A-J	10	Wash Receivers, 285 gals.	30,700
T-1-541A-J	10	Wash Receivers, 285 gal.	30,700
T-1-542A-B	2	Filtrate Surge Tanks, 7000 gals.	12,200
T-1-543A-B	2	Wash Surge Tank, 7000 gals.	12,200
T-1-544A-B	2	Wash Surge Tank, 7000 gals.	12,200
T-1-545A-B	2	Wash Surge Tank, 7000 gals.	12,200
T-1-546	1	Fuel Oil Storage Tank, 60,000 gals.	9,200
T-1-547	1	Dryer Feed Bin & Feeders, 15' w x 20' x 360' lg.	295,200

a. Process Equipment --- 450 Ton Unit --- Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
T-1-548	1	Calciner Feed Bin, 14' w x 14' d x 14' lg.	\$ 21,600
T-1-549A-F	6	Storage Silos, 30' dia. x 75' high	553,800
VP-1-500	1	Vacuum pump, 40,000 cfm, 1500 hp.	120,750
VP-1-501	1	Vacuum pump, 40,000 cfm, 1500 hp.	120,750
VP-1-502	1	Vacuum pump, 40,000 cfm, 1500 hp.	120,750
VP-1-503	1	Vacuum pump, 40,000 cfm, 1500 hp.	120,750
VP-1-504	1	Vacuum pump, 30,000 cfm, 1250 hp.	104,200
X-1-500A-B	2	Slurry Distributors, 35000 gals,	21,400
X-1-501A-B	2	Wash Liquor Distributors, 1800 gals.	13,200
X-1-502A-B	2	Slurry Distributors, 5150 gals.	24,400
X-1-503A-B	2	Wash Liquor Distributor, 1820 gals.	13,200
X-1-515A-B	2	Liquor Distributors, 2825 gals.	9,700
X-1-504A-B	2	Distributors, 6250 gals.	25,400
X-1-505A-B	2	Distributors, 5600 gals.	24,400
X-1-506A-B	2	Wash Liquor Distributors, 1725 gals.	13,200
X-1-507A-B	2	Slurry Distributors, 3450 gals.	16,400
X-1-508A-B	2	Wash Liquor Distributors, 2800 gals.	14,400
X-1-509A-B	2	Wash Liquor Distributors, 2800 gals.	14,400
X-1-510A-B	2	Wash Liquor Distributors, 2800 gals.	14,400
X-1-511A-B	2	Slurry Distributors, 4250 gals.	18,400
X-1-512A-B	2	Wash Liquor Distributors, 2850 gals.	15,400
X-1-513A-B	2	Wash Liquor Distributors, 2850 gals.	15,400
X-1-514A-B	2	Water Wash Distributors, 2850 gals.	15,400
		Piping, Valves, & Fittings	6,915,000
		Hangers,	100,000
		Insulation	35,000
		Lighting, Yard Units	60,000
		Painting	90,000
		Power Centers	240,000
		Instruments & Controls	1,000,000
		SUB TOTAL	\$ 49,279,171

b. Structures -- 450 Ton Unit

	(30' w x 360' x 40')	
Calciner & Rotary Cooler Building,	(15' w x 120' x 40')	\$ 217,000
Rotary Dryer Building,	120' w x 330' lg x 40' high	681,000
Filter Building,	60' w x 330' lg. x 60' high	510,000
Filter Building,	90' w x 520' lg. x 60' high	
	30' w x 200' lg. x 44' high	<u>1,322,000</u>
	SUB TOTAL	\$ 2,730,000

c. Engineering & Construction Costs--450 Ton Unit

Construction Supplies, 4% of labor	\$ 261,000	
Insurance & Taxes, 8% of labor	522,000	
Supervision & Field Office, 12% of labor	783,000	
Use of Construction Equipment and Temporary Construction 5% of labor	326,000	
Engineering & Drafting)		
Process Engineering)		
Engineering Administration)	4,000,000	
Purchasing, Inspection & Expediting	500,000	
Contingency, 10%	5,840,117	
Engineering--Contractor Fee, 4%	<u>2,336,712</u>	
	SUB TOTAL	\$ 14,568,829

450 TON UNIT CAPITAL COST ESTIMATE TOTAL \$ 66,578,000

IV. ECONOMIC EVALUATION

A. DETAILED CAPITAL COST ESTIMATE

1. ALUMINA RECOVERY SECTION -- 225 Ton Unit

a. Process Equipment --

<u>Item No.</u>	<u>No.</u> <u>Items</u>	<u>Description</u>	<u>Installed</u> <u>Cost</u>
A-2-510 A-H	8	Agitators, 15 hp.	\$ 36,140
A-2-517A-H	8	Agitators, 15 hp.	36,140
A-2-535A-F	6	Agitators, 7.5 hp.	20,430
AC-2-500	1	Air compressor, 3000 cfm, 375 hp.	54,600
AC-2-501	1	Air compressor, 3000 cfm, 375 hp.	54,600
AC-2-502	1	Air compressor, 3000 cfm, 375 hp.	54,600
AC-2-503	1	Air compressor, 3000 cfm, 375 hp.	54,600
AC-2-504	1	Air compressor, 2000 cfm, 250 hp.	46,500
C-2-500	1	Weight conveyor belt, 18" x 300'	35,850
C-2-501	1	Belt conveyor, 24" x 200'	16,050
C-2-502	1	Belt conveyor, 24" x 200'	16,050
C-2-503A-G	7	Screw conveyors, 24" x 20'	55,150
C-2-504	1	Belt conveyor, 24" x 200'	15,540
C-2-505	1	Belt conveyor, 24" x 200'	15,540
C-2-506	1	Belt conveyor, 24" x 160'	17,140
C-2-507	1	Belt conveyor, 20" x 400'	26,140
C-2-508	1	Belt conveyor, 24" x 20'	4,540
C-2-509	1	Drag conveyor, 14" x 140'	7,340
C-2-510	1	Belt conveyor, 14" x 125'	21,480
CR-2-500A-F	6 (Crystallizers, 26' dia.)	
E-2-501A-F	6 (Heat Exchangers)	
P-2-509A-I	9 (Circulating Pumps,)	2,203,250
P-2-510A-I	9 (Slurry Pumps)	
CR-2-501 A-J	10	Vacuum crystallizers, 26' dia.	2,008,500
CR-2-502A-K	11	Vacuum crystallizers, 26' dia.	2,225,600
D-2-500A-L	12	Rotary Dryers, 8' x 80'	2,520,000
D-C-2-500A-L	12	Dust collectors, 12 cyclones	396,000
B-2-500A-L	12	Centrifugal blowers, 200 hp.	325,200
D-2-501	1	Calciner, 8'6" dia, x 250', 40 hp.	387,280
DC-2-501	1	Dust Collector, 12 cyclones	24,000
B-2-502	1	Fan, 250 hp.	23,700
E-2-509	1	Rotary cooler, 50 hp.	112,060

a. Process Equipment -- 225 Ton Unit -- continued

<u>Item No.</u>	<u>No.</u> <u>Items</u>	<u>Description</u>	<u>Installed</u> <u>Cost</u>
B-2-501A-B	2	Blowers, 20 hp.	\$ 11,430
E-2-500A-F	6	Heat exchangers, 5,525 s. f.	207,300
E-2-502A-D	4	Cooling coils, 10,500 s. f.	45,000
E-2-503A-D	4	Heating coils, 3100 s. f.	15,500
E-2-504A-D	4	Steam coils, 838 s. f.	5,200
E-2-505	1	Condenser, 1700 s. f.	7,400
E-1-506	1	Reboiler, steam, 6150 s. f.	24,000
E-2-507	1	Cooler, 6600 s. f.	25,000
E-2-508	1	Fuel oil suction heater, 400 s. f.	1,300
EV-2-500A-C	3	Evaporators, 26' dia.	428,800
F-2-500A-B	2	Continuous centrifuges, 89 tph, 50 hp.	57,920
F-2-501A-H	8	Horizontal filters, 15' dia., 3 hp.	382,660
F-2-502A-E	6	Polishing filters, 1304 s. f.	204,000
F-2-503A-G	7	Horizontal filters, 15' dia., 3 hp.	334,830
F-2-504A-G	7	Horizontal filters, 15' dia., 3 hp.	334,830
F-2-505A-G	7	Horizontal filters, 15' dia., 3 hp.	334,830
F-2-506A-E	5	Horizontal filters, 15' dia., 3 hp.	239,160
K-2-500	1	Ammonia absorption column, 9'6" x 50'	24,220
K-2-501	1	Ammonia stripping column, 5' x 50'	11,585
L-2-500	1	Bucket elevator, 40.8 tph, 5 hp.	5,840
L-2-501	1	Bucket elevator, 23.4 tph, 5 hp.	8,240
P-2-500A-C	3	Pumps, 18,750 gpm, 200 hp.	122,300
P-2-501A-C	3	Pumps, 16,750 gpm, 200 hp.	104,300
P-2-502A-C	3	Pumps, 14,900 gpm, 175 hp.	104,300
P-2-503A-C	3	Pumps, 5625 gpm, 125 hp.	39,250
P-2-504A-C	3	Pumps, 723 gpm, 25 hp.	10,740
P-2-505A-C	3	Pumps, 6175 gpm, 150 hp.	41,700
P-2-506A-F	6	Pumps, 1445 gpm, 30 hp.	36,540
P-2-507A-B	2	Pumps, 1498 gpm, 50 hp.	14,120
P-2-508A-C	3	Pumps, 845 gpm, 20 hp.	12,000
P-2-511A-C	3	Pumps, 12,800 gpm, 250 hp.	80,400
P-2-512A-B	2	Pumps, 840 gpm, 25 hp.	8,460
P-2-513A-B	2	Pumps, 740 gpm, 20 hp.	8,350
P-2-514A-B	2	Pumps, 53 gpm, 3 hp.	5,370
P-2-515A-B	2	Pumps, 2353 gpm, 150 hp.	27,140
P-2-516A-B	2	Pumps, 2353 gpm, 60 hp.	15,160
P-2-517A-K	11	Pumps, 7580 gpm, 100 hp.	160,160
P-2-518A-K	11	Pumps, 212 gpm, 10 hp.	31,405

a. Process Equipment -- 225 Ton Unit -- Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
P-2-519A-C	3	Pumps, 23,450 gpm, 450 hp.	\$ 91,500
P-2-520A-B	2	Pumps, 1485 gpm, 50 hp.	13,920
P-2-521A-B	2	Pumps, 760 gpm, 20 hp.	8,360
P-2-522A-B	2	Pumps, 2552 gpm, 75 hp.	21,420
P-2-523A-L	12	Pumps, 8000 gpm, 125 hp.	207,600
P-2-524A-L	12	Pumps, 212 gpm, 10 hp.	34,260
P-2-525A-D	4	Pumps, 15,950 gpm, 350 hp.	116,000
P-2-526A-B	2	Pumps, 1685 gpm, 50 hp.	13,920
P-2-527A-B	2	Pumps, 719 gpm, 20 hp.	7,660
P-2-528A-H	8	Pumps, 200 gpm, 5 hp.	13,440
P-2-529	1	Pump, 500 gpm, 15 hp.	2,160
P-2-530A-B	2	Pumps, 830 gpm, 15 hp.	4,720
P-2-531A-B	2	Pumps, 2062 gpm, 50 hp.	14,720
P-2-532A-B	2	Pumps, 1160 gpm, 30 hp.	11,400
P-2-533A-B	2	Pumps, 1160 gpm, 30 hp.	11,400
P-2-534A-B	2	Pumps, 1774 gpm, 50 hp.	13,840
P-2-535A-B	2	Pumps, 1153 gpm, 30 hp.	11,400
P-2-536A-B	2	Pumps, 1200 gpm, 30 hp.	11,400
P-2-537A-B	2	Pumps, 1190 gpm, 30 hp.	11,400
P-2-538A-B	2	Pumps, 1180 gpm, 30 hp.	11,400
P-2-539A-B	2	Pumps, 1880 gpm, 75 hp.	18,220
P-2-540	1	Pump, 250 gpm, 15 hp.	2,000
P-2-541A-E	5	Rotary gear pumps, 14 gpm, 1 hp.	6,350
P-2-542A-B	2	Pumps, 788 gpm, 50 hp.	10,520
SJ-2-500A-B	2	Steam Jet Refrigeration Unit, 1200 tons	174,500
SJ-2-501A-J	10	Steam Jet Refrigeration Unit, 860 tons	705,000
SJ-2-502A-K	11	Steam Jet Refrigeration Unit, 800 tons	738,500
T-2-500A-D	4	Crystallizers, 125,000 gals.	378,600
R-2-500A-D	4	Rake mechanisms, 40' dia.	53,900
T-2-501	1	Crystallizers, 30,000 gals.	30,800
T-2-502	1	Compressed air receiver, 4' x 17'	1,600
T-2-503	1	Vacuum scrubber, 7'6" x 15'	2,600
T-2-504A-H	8	Filtrate receivers, 117 gals.	9,600
T-2-505A-H	8	Wash receivers, 90 gals.	9,600
T-2-506	1	Surge tank, 5000 gals.	4,700
T-2-507	1	Wash liquor surge tank, 5000 gals.	4,700
T-2-508	1	Surge & Settling tank, 250,000 gals.	119,000

a. Process Equipment -- 225 Ton Unit --- Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
R-2-508	1	Rake mechanism, 40' dia, 15 hp.	\$ 11,970
T-2-509	1	Filtrate Surge tank, 14,000 gals.	16,640
T-2-510A-D	4	Alum Redissolving tanks, 25,000 gals.	108,600
T-2-511	1	Compressed air receiver, 4' x 17'	1,600
T-2-512	1	Vacuum scrubber, 7'6" x 15'	2,600
T-2-513A-G	7	Filtrate receivers, 275 gals.	21,700
T-2-514A-G	7	Wash receivers, 140 gals.	9,100
T-2-515	1	Filtrate surge tank, 9000 gals.	7,600
T-2-516	1	Wash liquor surge tank, 4500 gals.	4,700
T-2-517A-D	4	Alum resolution tanks, 23,000 gals.	102,000
T-2-518	1	Compressed air, 4' x 17'	1,600
T-2-519	1	Vacuum scrubber, 7'6" x 15'	2,600
T-2-520A-G	7	Filtrate receivers, 315 gals.	22,400
T-2-521A-G	7	Wash liquor receivers, 132 gals.	8,800
T-2-522	1	Filtrate surge tank, 10,000 gals.	7,600
T-2-523	1	Wash liquor surge tank, 4,300 gals.	4,600
T-2-524A-G	7	Precipitation tanks, 12' x 85' x 30'	2,729,680
T-2-525	1	Liquid NH ₃ storage tank, 76000 gals.	97,000
T-2-526	1	Compressed air surge tank, 4' x 17'	1,600
T-2-527	1	Vacuum scrubber, 7'6" x 15'	2,600
T-2-528A-G	7	Filtrate receivers, 170 gals.	8,400
T-2-529A-G	7	Wash receivers, 215 gals.	9,100
T-2-530A-G	7	Wash receivers, 215 gals.	9,100
T-2-531A-G	7	Wash receivers, 215 gals.	9,100
T-2-532	1	Filtrate surge tank, 12,200 gals.	9,100
T-2-533	1	Wash surge tank, 7,000 gals.	6,100
T-2-534	1	Wash surge tank, 7,000 gals.	6,100
T-2-535A-C	3	Repulping tanks, 10,650 gals.	76,000
T-2-536	1	Compressed air surge tank, 4' x 17'	1,600
T-2-537	1	Vacuum scrubber, 7'6" x 15'	2,600
T-2-538A-E	5	Filtrate receivers, 285 gals.	15,350
T-2-539A-E	5	Wash receivers, 285 gals.	15,350
T-2-540A-E	5	Wash receivers, 285 gals.	15,350
T-2-541A-E	5	Wash receivers, 285 gals.	15,350
T-2-542	1	Filtrate surge tank, 7,000 gals.	6,100
T-2-543	1	Wash surge tank, 7,000 gals.	6,100

a. Process Equipment -- 225 Ton Unit --- Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
T-2-544	1	Wash surge tank, 7000 gals.	\$ 6,100
T-2-545	1	Wash surge tank, 7000 gals.	6,100
T-2-546	1	Fuel oil storage tank, 30,000 gals.	5,900
T-2-547	1	Dryer feed bin, 15' x 20' x 180'	193,000
T-2-548	1	Calcliner feed bin, 10' x 11' x 13'	13,300
T-2-549A-C	3	Storage silos, 30' x 75'	284,000
VP-2-500	1	Vacuum pump, 20,000 cfm, 750 hp.	77,200
VP-2-501	1	Vacuum pump, 20,000 cfm, 750 hp.	77,200
VP-2-502	1	Vacuum pump, 20,000 cfm, 750 hp.	77,200
VP-2-503	1	Vacuum pump, 20,000 cfm, 750 hp.	77,200
VP-504	1	Vacuum pump, 15,000 cfm, 560 hp.	65,600
X-2-500	1	Slurry distributor, 3500 gals.	10,700
X-2-501	1	Wash liquor distributor, 1800 gal.	6,600
X-2-502	1	Slurry distributor, 5150 gals.	12,200
X-2-503	1	Wash liquor distributor, 1820 gals.	6,600
X-2-515	1	Liquor distributor, 2825 gals.	9,700
X-2-504	1	Distributor, 6250 gals.	12,700
X-2-505	1	Slurry distributor, 5600 gals.	12,200
X-2-506	1	Wash liquor distributor, 1725 gals.	6,600
X-2-507	1	Slurry distributor, 3450 gals.	8,200
X-2-508	1	Wash liquor distributor, 2800 gals.	7,200
X-2-509	1	Wash liquor distributor, 2800 gals.	7,200
X-2-510	1	Filtrate wash liquor distributor, 2800 gals.	7,200
X-2-511	1	Slurry distributor, 4250 gals.	9,200
X-2-512	1	Wash liquor distributor, 2850 gals.	7,700
X-2-513	1	Wash liquor distributor, 2850 gals.	7,700
X-2-514	1	Water wash distributor, 2850 gals.	7,700
		Piping, valves & fittings	4,200,000
		Hangers,	65,000
		Pipe Insulation	22,000
		Lighting, Yard Units	40,000
		Painting	60,000
		Power Centers	170,000
		Instruments & Controls	690,000
SUB TOTAL			\$ 26,891,860

b. Structures -- 225 Ton Unit

Rotary Dryer Bldg. , 72' x 180' x 40' high	\$ 222,000
Rotary Calciner Bldg. , 30' x 270' x 40' high 15' x 90' x 40' high	118,000
Filter Bldg. 60' x 210' x 60' high	325,000
Filter Bldg. 90' x 240' x 60' high 30' x 135' x 44' high	<u>634,000</u>
SUB TOTAL	\$ 1,299,000

C. Engineering & Construction Costs

Construction Supplies, 4% of Labor	\$ 148,922
Insurance & Taxes , 8% of Labor	297,844
Supervision & Field Office, 12% of Labor	446,766
Use of Construction Equipment and Temporary Construction, 5% of Labor	136,103
Engineering & Drafting Process Engineering Engineering administration	3,550,000
Purchasing, Expediting & Inspection	290,000
Contingency 10% of Total	3,306,049
Engineering- Contractor Fee 4% of Total	<u>1,322,456</u>
SUB TOTAL	\$ 9,498,140

225 Ton Unit---CAPITAL COST ESTIMATE TOTAL \$ 37,689,000

IV. ECONOMIC EVALUATION

A. DETAILED CAPITAL COST ESTIMATE

1. ALUMINA RECOVERY SECTION--100 Ton Unit

a. Process Equipment--

<u>Item No.</u>	<u>No.</u> <u>Items</u>	<u>Description</u>	<u>Installed</u> <u>Cost</u>
A-3-510A-H	8	Agitators, 5 hp.	24,190
A-3-517A-H	8	Agitators, 7 1/2 hp.	27,240
A-3-535A-F	8	Agitators, 3 hp.	16,110
AC-3-500	1	Air compressor, 1330 cfm, 175 hp.	17,220
AC-3-501	1	Air compressor, 1330 cfm, 175 hp.	17,220
AC-3-502	1	Air compressor, 1330 cfm, 175 hp.	17,220
AC-3-503	1	Air compressor, 1330 cfm, 175 hp.	17,220
AC-3-504	1	Air compressor, 880 cfm, 125 hp.	13,100
C-3-500	1	Conveyor belt, 12" w x 300', 2 hp.	32,405
C-3-501	1	Belt conveyor, 20" x 200', 3 hp.	15,940
C-3-502	1	Belt conveyor, 20" x 200', 3 hp.	15,940
C-3-503A-C	3	Screw conveyors, 24" x 20', 10 hp.	23,850
C-3-504	1	Belt conveyor, 18" x 200', 3 hp.	12,540
C-3-505	1	Belt conveyor, 18" x 200', 3 hp.	12,540
C-3-506	1	Belt conveyor, 16" x 75', 5 hp.	9,060
C-3-507	1	Belt conveyor, 12" x 130', 2 hp.	8,370
C-3-508	1	Belt conveyor, 12" x 20', 1 1/2 hp.	3,595
C-3-509	1	Drag conveyor, 12" x 250', 3 hp.	10,140
C-3-510	1	Belt conveyor, 12" x 30', 1 hp.	6,570
CR-3-500A-F	6 (Crystallizers, 17'4" dia.)	
E-3-501A-F	6 (Heat Exchangers)	
P-3-509A-I	9 (Circulating Pumps)	1,030,000
P-3-510A-I	9 (Slurry Pumps)	
CR-3-501A-E	5	Vacuum crystallizers, 26' dia.	1,010,000
CR-3-502A-E	5	Vacuum crystallizers, 26' dia.	1,010,000
D-3-500A-E	5	Rotary Dryers, 8' dia. x 80', 200 hp.	1,050,550
DC-3-500A-E	5	Dust collectors, 12 per dryer	165,000
B-3-500A-E	5	Centrifugal blowers, 200 hp.	135,500
D-3-501	1	Rotary calciner, 6' dia. x 150' lg.	219,100
DC-3-501	1	Dust collectors,	13,000
B-3-502	1	Fan, 125 hp.	13,400

a. Process Equipment -- 100 Ton Unit -- Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
E-3-509	1	Rotary cooler, 7' dia. x 50 lg, 25 hp.	\$ 81,740
B-3-501A-B	2	Blowers, 10 hp.	9,420
E-3-500A-F	6	Heat Exchangers, 2450 s. f.	92,350
E-3-502A-D	4	Cooling coils, 4,660 s. f.	23,000
E-3-503A-D	4	Steam Coils, 1380 s. f.	7,700
E-3-504A-D	4	Steam Coils, 490 s. f.	3,400
E-3-505	1	Condenser, 755 s. f.	4,400
E-3-506	1	Reboiler, 2740 s. f.	10,850
E-3-507	1	Cooler, 2940 s. f.	12,100
E-3-508	1	Fuel oil suction heater, 180 s. f.	650
EV-3-500A-F	6	Evaporators, 12'3" dia.	286,600
F-3-500	1	Centrifuge, 39.6 tph, 50 hp.	26,960
F-3-501A-D	4	Filters, 15' dia. , 3 hp.	191,330
F-3-503A-C	3	Filters, 15' dia. , 3 hp.	143,505
F-3-502A-D	4	Filters, 1204 s. f.	136,000
F-3-504A-C	3	Filters, 15' dia. , 3 hp.	143,505
F-3-505A-C	3	Filters, 15' dia. 3 hp.	143,505
P-3-506A-C	3	Filters, 15' dia. 3 hp.	143,505
K-3-500	1	Ammonia absorption column, 6'6" x 50'	14,300
K-3-501	1	Ammonia stripping column, 3'4" x 50'	8,010
L-3-500	1	Bucket elevator, 18.1 tph, 3 hp.	5,340
L-3-501	1	Bucket elevator, 10.4 tph, 3 hp.	7,740
P-3-500A-C	3	Pumps, 8325 gpm, 100 hp.	70,680
P-3-501A-C	3	Pumps, 7450 gpm, 100 hp.	67,680
P-3-502A-C	3	Pumps, 6600 gpm, 75 hp.	53,480
P-3-503A-C	3	Pumps, 2500 gpm, 50 hp.	20,380
P-3-504A-C	3	Pumps, 320 gpm, 15 hp.	9,940
P-3-505A-C	3	Pumps, 2750 gpm, 60 hp.	16,880
P-3-506A-F	6	Pumps, 640 gpm, 15 hp.	22,600
P-3-507A-B	2	Pumps, 665 gpm, 25 hp.	8,060
P-3-508A-B	2	Pumps, 750 gpm, 15 hp.	7,760
P-3-511A-B	2	Pumps, 11,400 gpm, 225 hp.	50,200
P-3-512A-B	2	Pumps, 374 gpm, 15 hp.	6,430
P-3-513A-B	2	Pumps, 329 gpm, 10 hp.	6,620
P-3-514A-B	2	Pumps, 23 gpm, 1 1/2 hp.	4,030
P-3-515A-B	2	Pumps, 1045 gpm, 75 hp.	15,820
P-3-516A-B	2	Pumps, 1045 gpm, 30 hp.	9,400
P-3-517A-F	6	Pumps, 7580 gpm, 100 hp.	87,460
P-3-518A-F	6	Pumps, 212 gpm, 10 hp.	17,130
P-3-519A-B	2	Pumps, 20,800 gpm, 400 hp.	57,200

a. Process Equipment -- 100 Ton Unit -- Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
P-3-520A-B	2	Pumps, 660 gpm, 25 hp.	\$ 7,860
P-3-521A-B	2	Pumps, 338 gpm, 10 hp.	6,620
P-3-522A-B	2	Pumps, 1134 gpm, 40 hp.	12,530
P-3-523A-F	6	Pumps, 8000 gpm, 125 hp.	103,800
P-3-524A-F	6	Pumps, 208 gpm, 10 hp.	17,130
P-3-525A-B	2	Pumps, 21,360 gpm, 425 hp.	61,200
P-3-526A-B	2	Pumps, 748 gpm, 25 hp.	7,560
P-3-527A-B	2	Pumps, 320 gpm, 10 hp.	5,720
P-3-528A-D	4	Pumps, 200 gpm, 5 hp.	3,370
P-3-529	1	Pump, 225 gpm, 7.5hp.	1,890
P-3-530A-B	2	Pumps, 369 gpm, 7 1/2 hp.	3,880
P-1-531A-B	2	Pumps, 915 gpm, 25 hp.	7,760
P-3-532A-B	2	Pumps, 516 gpm, 15 hp.	7,430
P-3-533A-B	2	Pumps, 516 gpm, 15 hp.	7,430
P-3-534A-B	2	Pumps, 790 gpm, 20 hp.	8,250
P-3-535A-B	2	Pumps, 512 gpm, 15 hp.	7,430
P-3-536A-B	2	Pumps, 534 gpm, 15 hp.	7,430
P-3-537A-B	2	Pumps, 530 gpm, 15 hp.	7,430
P-3-538A-B	2	Pumps, 525 gpm, 15 hp.	7,430
P-3-539A-B	2	Pumps, 835 gpm, 40 hp.	10,130
P-3-540	1	Pump, 110 gpm, 7 1/2 hp.	1,900
P-3-541A-E	5	Pumps, 6 gpm, 1/2 hp.	6,050
P-1-542A-B	2	Pumps, 351 gpm, 20 hp.	6,730
SJ-3-500A-B	2	Steam jet refrigeration units--1066 tons	101,000
SJ-3-501A-E	5	Steam jet refrigeration units--4300 tons	352,500
SJ-3-502A-E	5	Steam jet refrigeration units--4000 tons	336,000
T-3-500A-D	4	Crystallizers, 55,000 gals.	273,800
R-3-500A-D	4	Rake mechanisms for above, 32' dia.	38,260
T-3-501	1	Crystallizer feed tank, 13,320 gals.	20,560
T-3-502	1	Surge tank, 3' 6" x 10'	1,100
T-3-503	1	Vacuum scrubber, 5' dia. x 15'	2,100
T-3-504A-D	4	Filtrate receivers, 117 gals.	4,800
T-3-505A-D	4	Wash receivers, 117 gals.	4,800
T-3-506	1	Surge tank, 2220 gals.	2,800
T-3-507	1	Surge tank, 2220 gals.	2,800
T-3-508	1	Surge & settling tank, 101,000 gals.	70,200
R-3-508	1	Rake mechanism for above, 35' dia.	10,250

a. Process Equipment-- 100 Ton Unit -- Continued'

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
T-3-509	1	Surge Tank, 6300 gals.	\$ 10,480
T-3-510A-D	4	Alum dissolving tanks, 11,100 gals.	66,400
T-3-511	1	Compressed air receiver, 3'6" x 10'	1,100
T-3-512	1	Vacuum scrubber, 5' dia. x 15'	2,100
T-3-513A-C	3	Filtrate receivers, 275 gals.	9,300
T-3-514A-C	3	Wash receivers, 140 gals.	3,900
T-3-515	1	Filtrate surge tank, 4000 gals.	4,600
T-3-516	1	Wash liquor surge tank, 2000 gals.	2,900
T-3-517A-D	4	Alum resolution tanks, 10,200 gals.	60,400
T-3-518	1	Compressed air surge tank, 3'6" x 10'	1,100
T-3-519	1	Vacuum scrubber, 5' dia. x 15'	2,100
T-3-520A-C	3	Filtrate receivers, 315 gals.	9,600
T-3-521A-C	3	Wash Liquor receivers, 132 gals.	3,900
T-3-522	1	Filtrate surge tank, 4400 gals.	4,700
T-3-523	1	Wash liquor surge tank, 1000 gals.	2,300
T-3-524A-C	3	Precipitation tanks, 12' w x85'x 30'	1,172,930
T-3-525	1	Liquid NH ₃ storage tank, 17,000 gals.	17,740
T-3-526	1	Compressed air surge tank, 3'6" x 10'	1,100
T-3-527	1	Vacuum scrubber, 5' dia. x 15'	2,100
T-3-528A-C	3	Filtrate receivers, 170 gals.	3,600
T-3-529A-C	3	Wash receivers, 215 gals.	3,900
T-3-530A-C	3	Wash receivers, 215 gals.	3,900
T-3-531A-C	3	Wash receivers, 215 gals.	3,900
T-3-532	1	Filtrate surge tank, 5200 gals.	4,600
T-3-533	1	Wash surge tank, 3110 gals.	3,600
T-3-534	1	Wash surge tank, 3110 gals.	3,600
T-3-535A-C	3	Repulping tanks, 4740 gals.	35,600
T-3-536	1	Compressed air surge tank, 3'6" x 10'	1,100
T-3-537	1	Vacuum scrubber, 5' dia. x 15' high	2,100
T-3-538A-C	3	Filtrate Receivers, 285 gals.	9,600
T-3-539A-C	3	Wash receivers, 285 gals.	9,600
T-3-540A-C	3	Wash receivers, 285 gals.	9,600
T-3-541A-C	3	Wash receivers, 285 gals.	9,600
T-3-542	1	Filtrate Surge tank, 3110 gals.	3,600
T-3-543	1	Wash surge tank, 3110 gals.	3,600
T-3-544	1	Wash surge tank, 3110 gals.	3,600
T-3-545	1	Wash surge tank, 3110 gals.	3,600

a. Process Equipment -- 100 Ton Unit --- Continued

<u>Item No.</u>	<u>No. Items</u>	<u>Description</u>	<u>Installed Cost</u>
T-3-546	1	Fuel oil storage tank, 13,000 gals.	\$ 3,700
T-3-547	1	Dryer feed bin, 15' x 20' x 75'	83,150
T-3-548	1	Calcliner feed bin, 10'x 7' x 10'	11,510
T-3-549	1	Storage silo, 40' dia. x 60' high	102,400
VP-3-500	1	Vacuum pump, 8900 cfm, 350 hp.	49,700
VP-3-501	1	Vacuum pump, 8900 cfm, 350 hp.	49,700
VP-3-502	1	Vacuum pump, 8900 cfm, 350 hp.	49,700
VP-3-503	1	Vacuum pump, 8900 cfm, 350 hp.	49,700
VP-504	1	Vacuum pump, 6700 cfm, 300 hp.	46,700
X-3-500	1	Slurry distributor, 1590 gals.	3,400
X-3-501	1	Wash liquor distributor, 800 gals.	2,600
X-3-502	1	Slurry distributor, 2300 gals.	4,200
X-3-503	1	Wash liquor distributor, 810 gals.	2,600
X-3-504	1	Distributor, 2800 gals.	9,100
X-3-505	1	Slurry distributor, 2900 gals.	9,700
X-3-506	1	Wash liquor distributor, 770 gals.	2,700
X-3-507	1	Slurry distributor, 1530 gals.	6,600
X-3-508	1	Wash Liquor distributor, 1250 gals.	3,100
X-3-509	1	Wash liquor distributor, 1250 gals.	3,100
X-3-511	1	Slurry distributor, 2110 gals.	4,100
X-3-512	1	Wash liquor distributor, 1270 gals.	3,100
X-3-510	1	Wash liquor distributor, 1250 gals.	3,100
X-3-513	1	Wash liquor distributor, 1250 gals.	3,100
X-3-514	1	Wash liquor distributor, 1270 gals.	3,100
X-3-515	1	Liquor distributor, 1250 gals.	3,100
		Pipe, Valves & Fittings	2,623,000
		Hangers,	42,000
		Insulation	14,000
		Lighting - Yard Units	30,000
		Painting	45,000
		Power Centers	96,000
		Instruments and controls	500,000

SUB TOTAL \$ 13,873,020

b. Structures-- 100 Ton Unit

Rotary Drier Bldg. , 75' w x 120'lg x 40' high	\$ 158,000
Rotary Calciner Bldg. , 25'w x 180' lg x 40' high 10' w x 90' lg. x 40' high	95,000
Filter Bldg. , 60' w x 120' lg. x 60' high	190,000
Filter Bldg. , 90' w x 120' lg. x 60' high 30' w x 90' lg. x 44' high	<u>330,000</u>
SUB TOTAL	\$ 773,000

c. Engineering & Construction Costs

Construction Supplies, 4% of Labor	\$ 86,902
Insurance & Taxes, 8% of Labor	173,804
Supervision & Field Office, 12% of Labor	260,706
Use of Construction Equipment and Temporary Construction, 5% of Labor	108,629
Engineering & Drafting Process Engineering	
Engineering Administration	3,125,000
Purchasing, Expediting and Inspection	170,000
Contingency 10%, of Total	1,857,106
Engineering--Contractor Fee 4% of Total	<u>742,833</u>
SUB TOTAL	\$ 6,524,980
100 Ton Unit Capital Cost Estimate TOTAL	\$ 21,171,000

IV. ECONOMIC EVALUATION

B. OPERATING COST ESTIMATE

Operating cost estimates include ammonia, power, steam, water, fuel oil, direct labor and immediate supervision, maintenance and amortization, taxes, insurance and analytical expenses.

Make-up ammonia and recycled ammonia from the Ammonium Sulfate Decomposition Section are charged to this section. Cost of makeup ammonia is based on production in the New Orleans area, and varies with quantity of ammonia used for makeup in the three plants. Variation of ammonia costs with amount required is shown graphically in RMO 2018. The cost of producing ammonia in the decomposition unit is shown in RMO 2017.

Estimates of the cost of power, steam and water have been made in the Utility Section (RMO 2019). These costs are shown on the operating cost estimates on the following pages. Steam condensate recovered in this section is credited at the same rate as the cost of producing boiler feed water in the Utility Section. A demand factor of 0.8 has been used in determining the electric requirements for equipment.

Power requirements for inside lighting were calculated at 2.5 watts per square foot. Fuel oil has been charged at \$0.058 per gallon.

The basis for determining labor costs is as follows:

1. Operators @ \$1.77/hr. + \$0.04/hr. cost of living increase = \$1.81/hr.
2. Helpers @ \$1.42/hr. + \$0.04/hr. cost of living increase = \$1.46/hr.
3. Holiday pay = 1.7%
4. Paid vacations = 3.85%
5. Sick leave = 1.92%

6. Workmen's Compensation & Public Liability Insurance = 1.29%
7. Social Security and Unemployment Benefits = 1.9%
8. Shift differential and overtime = 7.5%
9. Group Insurance and pension = 6.0%
10. Down time = 2.86%
11. Direct supervision @ \$450/month

Payroll additions for supervision do not include pay for holidays, vacation, sick leave and down time. Only the lowest level of supervision has been included here. Charges will be added for additional supervision in the Summary Report.

Annual maintenance cost is the sum of 3% of building costs and 8% of equipment costs. Operating supplies are charged at 20% of the maintenance cost.

Annual amortization and depreciation costs are based on a 15 year life for equipment and a 20 year life for buildings. Taxes are charged at 3.8% with 50% evaluation of capital. Insurance is charged at \$0.22 per \$100 of capital investment.

Estimates of the number and cost of chemical analyses are as follows:

<u>Plant Size, Tons U/Yr.</u>	<u>Number Analyses/Shift</u>			<u>Cost/Analyses</u>
	<u>450</u>	<u>225</u>	<u>100</u>	
<u>Compound</u>				
Fe ₂ O ₃	9	9	9	\$0.92
SiO ₂	6	6	6	1.70
P ₂ O ₅	48	30	18	0.93
TiO ₂	6	6	6	1.65
Na ₂ O	6	6	6	1.50
U	3	3	3	1.25
H ₂ O	57	37	21	0.60
CaO	6	6	6	0.87
Al ₂ O ₃	51	30	15	1.09
SO ₄	42	24	12	1.05

These costs were increased 50% to include supervision and labor benefits.

Ammonium sulfate is recovered from the Alumina Section and used as part of the feed to the Ammonium Sulfate Decomposition Section (RMO 2017). The cost of processing ammonium sulfate is credited to the Alumina Section and charged to the Decomposition Section.

Cost of feed solution, overhead, management, general plant facilities, interest and return on investment have not been included, but these items will be included in the Summary Report.

IV. ECONOMIC EVALUATION

B. OPERATING COST ESTIMATE

1. Alumina Recovery Section -- 450 Ton Plant

	<u>\$/Hour</u>
Ammonia from Decomposition Section, 41.4 tph. @ \$18.09/ton	748.93
Ammonia, makeup, 5.8 tph. @ \$45.99/ton	266.74
Power, 25,000 KW @ \$0.0075/KWH	187.50
Steam, 100 psig, 1324.8 M lbs/hr. @ \$0.435/M. lb.	
15 psig, 753.7 M lbs/hr. @ \$0.380/M. lb.	771.97
less condensate, 1209.7 M lbs/hr. @ \$0.075/M. lb.	
Process Water, 17,092 M gal. /hr. @ \$0.0057/M. gal.	97.42
Well Water, 2436 M gal. /hr. @ \$0.0083/M. gal.	20.22
Fuel Oil, Bunker C, 7022 gal/hr. @ \$0.058/gal.	407.28
Labor & Direct Supervision, including 35 operators, 65 helpers, and 6 supervisors/shift.	219.21
Maintenance:	
Buildings = 3% of \$3,494,729/8400 hrs.	12.48
Equipment = 8% of \$63,083,271/8400 hrs.	600.79
Operating Supplies (20% of maintenance)	122.65
Filter cloth	1.55
Depreciation & Amortization	
Buildings, \$3,494,729 @ 20 years	20.80
Equipment, \$63,083,271 @ 15 years	500.66
Taxes, 0.038 x 0.5 x \$66,578,000/8400 hrs.	150.59
Insurance, 0.22% of \$66,578,000/8400 hrs.	17.44
Analytical expenses	42.17
Sub Total	\$4,188.40
Credit for processing 52.3 TPH (NH ₄) ₂ SO ₄	- 162.67
Operating Cost for Alumina Recovery Section	\$4,025.73

IV. ECONOMIC EVALUATION

B. OPERATING COST ESTIMATE

2. Alumina Recovery Section -- 225 Ton Plant

	<u>\$/Hour</u>
Ammonia from Decomposition Section, 20.7 tph. @ \$19.25/ton	398.48
Ammonia, makeup, 2.9 tph. @ \$49.84/ton	144.54
Power, 12,400 KW @ \$0.0086/KWH	106.64
Steam, 100 psig, 657.8 M. lbs/hr. @ \$0.446/M. lbs.	
15 psig, 377.5 M. lbs/hr. @ \$0.388/M. lbs.	393.78
less condensate, 598 M. lbs/hr. @ \$0.077/M. lbs.	
Process Water, 8,545 M. gal/hr. @ \$0.0061/M. gal.	52.12
Well Water, 1218 M. gal/hr. @ \$0.0103/M. gal.	12.55
Fuel Oil, Bunker C, 3511 gal/hr. @ \$0.058/gal.	203.64
Labor & Direct Supervision, including 30 operators, 58 helpers, and 5 supervisors/shift	191.70
Maintenance:	
Buildings = 3% of \$1,706,643/8400 hrs.	6.10
Equipment = 8% of \$35,982,357/8400 hrs.	342.70
Operating Supplies (20% of maintenance)	69.76
Filter Cloth	0.81
Depreciation & Amortization:	
Buildings, \$1,706,643 @ 20 years	10.16
Equipment, \$35,982,357 @ 15 years	285.58
Taxes, 0.038 x 0.5 x \$37,689,000/8400 hrs.	85.25
Insurance, 0.22% of \$37,689,000/8400 hrs.	9.87
Analytical expenses	28.94
Sub Total	<u>\$2,342.62</u>
Credit for processing 26.1 TPH (NH ₄) ₂ SO ₄	<u>- 31.34</u>
Operating Cost for Alumina Recovery Section	\$2,261.28

IV. ECONOMIC EVALUATION

B. OPERATING COST ESTIMATE

3. Alumina Recovery Section -- 100 Ton Plant

	<u>\$/Hour</u>
Ammonia from Decomposition Section, 9.2 tph. @ \$21.68/ton	199.46
Ammonia, makeup, 1.3 tph. @ \$58.34/ton	75.84
Power, 5800 KW @ \$0.0099/KWH	57.42
Steam, 100 psig, 294.5 M. lbs/hr. @ \$0.470/M. lbs.	
15 psig, 166.3 M. lbs/hr. @ \$0.411/M. lbs.	184.83
less condensate, 267.7 M. lbs/hr. @ \$0.082/M. lbs.	
Process Water, 3800 M. gal/hr. @ \$0.0080/M. gal.	30.40
Well Water, 540 M. gal/hr. @ \$0.0131/M. gal.	7.07
Fuel Oil, Bunker C, 1555 gal/hr. @ \$0.058/gal.	90.19
Labor & Direct Supervision, including 26 operators, 49 helpers and 4 supervisors/shift	162.79
Maintenance:	
Buildings = 3% of \$1,117,380/8400 hrs.	3.99
Equipment = 8% of \$20,053,620/8400 hrs.	190.99
Operating Supplies (20% of maintenance)	39.00
Filter Cloth	0.40
Depreciation & Amortization:	
Buildings, \$1,117,380 @ 20 years	6.65
Equipment, \$20,053,620 @ 15 years	159.16
Taxes, 0.038 x 0.5 x \$21,171,000/8400 hrs.	47.89
Insurance, 0.22% of \$21,171,000/8400 hrs.	5.54
Analytical expenses	19.62
Sub Total	<u>\$1,281.24</u>
Credit for processing 11.6 TPH (NH ₄) ₂ SO ₄	<u>- 36.15</u>
Operating Cost for Alumina Recovery Section	\$1,245.09

V. ALTERNATE PROCESS

Preliminary designs and cost estimates have been made for a process which produces an impure alumina product suitable for feed to the Bayer process.

In this alternate alum is recovered from the leached zone extract in a manner similar to the previous process. Extract from the Filtration Section is evaporated, cooled and reacted with ammonium sulfate to crystallize alum. Alum is filtered from the extract and washed. Instead of crystallizing alum twice to purify it (the procedure followed in the first process), alum is heated after the first crystallization until dissolved and passed through a spray dryer to dehydrate it. The dehydrated alum is calcined to drive off steam, ammonia and sulfur dioxide and to produce an alumina product containing iron and phosphate impurities.

This alternate would bring about changes in the design of the Ammonium Sulfate Decomposition, Sulfuric Acid and Ammonia plants. Ammonium sulfate required to crystallize alum is not recovered in this alternate process, but is decomposed in the calcining step as alum. Ammonium sulfate for alum crystallization is obtained from the Phosphate Recovery Section, (RMO 2016), and by reacting ammonia with sulfuric acid. Excess ammonium sulfate is not available in the process and, therefore, the reactor in the Ammonium Sulfate Decomposition Section is eliminated.

Since makeup ammonium sulfate is required, the size of the sulfuric acid and ammonia plants must be increased. The sulfur dioxide produced in the calcining step is recovered, converted to the trioxide and absorbed in water to form sulfuric acid. The remainder of the acid is produced from elemental sulfur. It is assumed that ammonia produced in the calcining step will not be recovered.

Following are tables showing the capital costs and operating costs of the Alumina, Decomposition, Sulfuric Acid and Ammonia Sections of the 450 tons U/year plants for the two alternates:

<u>Plant Section</u>	<u>Capital Cost Estimates</u>	
	<u>Purified Alumina</u>	<u>Bayer Feed Alumina</u>
Alumina Recovery	\$ 66,578,000	\$30,619,000
Decomposition & H ₂ SO ₄ Plants	46,894,000	
Sulfuric Acid Plants		25,275,000
Ammonia Plants	<u>14,200,000</u>	<u>19,800,000</u>
Total	\$127,672,000	\$75,694,000

<u>Plant Section</u>	<u>Operating Cost Estimates</u>	
	<u>Purified Alumina</u>	<u>Bayer Feed Alumina</u>
Alumina Recovery	\$ 3,276.80 *	\$ 1,862.95
Decomposition & H ₂ SO ₄ Plants	3,489.25	
Sulfuric Acid Plants		3,400.52
Ammonia Plants	<u>413.91 **</u>	<u>1,062.12</u>
Total	\$ 7,179.96	\$ 6,325.59

* Cost of recycled ammonia included in Decomposition operating cost.

** Cost of makeup ammonia in P₂O₅ Section.

The tables above show that for the alternate process the capital cost is \$52,000,000 less and the operating cost is \$854/hour less than the first process. However, the alumina product is not as pure as alumina produced in the first process and, therefore, the sales value would be lower. The amount lost by the decrease in sales value would be greater than the amount of money gained by the decrease in operating costs.

This alternate has not been fully evaluated on a pilot plant scale. Better estimates of capital costs and operating costs could be obtained after pilot plant studies are completed

